



Multi-Rotor UAV Observations of the Atmospheric Boundary Layer over Complex Terrain: Accuracy Validation and Dynamic Mechanisms of Flight Disturbances

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30

Abstract

31 Unmanned aerial vehicle (UAV)-based sounding has become a flexible and cost-effective
32 approach for probing the atmospheric boundary layer (ABL), yet its measurement credibility
33 over complex terrain and the dynamic response of UAV flight attitude to boundary-layer
34 dynamics remain insufficiently quantified. Here, we implement multi-rotor UAV field campaigns
35 equipped with well-calibrated meteorological payloads, including co-located intercomparison
36 observations against a 100-m gradient meteorological tower at the Xingtai Field Scientific
37 Experiment Base, and vertical-profile surveys across the lower ABL over the eastern Taihang
38 piedmont. The comparative observations demonstrate excellent agreement between UAV and
39 tower measurements: vertical profiles of wind speed, wind direction, air temperature, and relative
40 humidity exhibit strong correlations, negligible systematic biases, and coherent vertical
41 structures. Stability parameters derived from high-frequency hovering observations, including
42 potential temperature and gradient Richardson number (Ri), also closely match tower references,
43 verifying the platform's capability to reliably resolve ABL thermal stratification and dynamic
44 stability. Three successive evening soundings capturing the transition from a convective to a
45 stable boundary layer reveal that UAV attitude disturbances are strongly suppressed within stably
46 stratified layers, but markedly amplified in near-neutral to weakly unstable layers where intense
47 vertical wind shear coincides with weak thermal suppression, with the most severe perturbations
48 occurring near the cloud base. The joint distribution of Ri and vertical wind shear further
49 indicates that turbulence-induced flight bumpiness generally intensifies with increasing shear
50 and peaks under unstable stratification, while a localized anomaly suggests possible resonance-
51 like coupling between turbulent eddy scales and airframe dynamics. These findings establish a
52 quantitative observational basis for reliable UAV-based ABL sensing and low-altitude flight-
53 safety assessment over complex terrain.

54



55 **1 Introduction**

56 Through turbulent exchange of momentum, heat, water vapour, aerosols, and trace gases,
57 the ABL regulates near-surface weather evolution, cloud and fog formation, and the
58 meteorological environment experienced by low-altitude operations (Stull, 1988; Garratt, 1992;
59 Wulfmeyer et al., 2015). Its most dynamically active portion commonly lies within the lowest
60 several hundred metres to approximately 1–2 km above ground level, where wind shear, thermal
61 stratification, and turbulent mixing can change rapidly over minutes to hours and over short
62 horizontal distances (Seibert et al., 2000; Stith et al., 2018). Accurate, vertically resolved
63 observations in this layer are therefore essential for boundary-layer parameterization, numerical
64 weather prediction, air-quality assessment, and low-level flight-safety evaluation.

65 Despite this importance, the lower ABL remains structurally under-sampled by conventional
66 observing systems. Surface meteorological stations provide long-term and reliable measurements,
67 but they represent only fixed points near the ground and cannot resolve the vertical gradients that
68 determine boundary-layer stability and turbulence. Radiosondes provide vertical profiles of
69 temperature, humidity, pressure, and wind, yet their launches are typically sparse in time and
70 space; once released, the balloon drifts passively with the ambient flow and cannot repeatedly
71 sample a prescribed location or be recovered for targeted near-surface profiling (Seibert et al.,
72 2000; Stith et al., 2018). Meteorological towers, wind profilers, radar, and lidar systems can
73 partly improve vertical coverage, but their deployment is constrained by fixed siting, installation
74 and maintenance costs, minimum detectable range, terrain dependence, and reduced
75 representativeness away from the instrument location (Illingworth et al., 2019; Wulfmeyer et al.,
76 2015). As a result, a persistent observational gap exists between near-surface point measurements
77 and coarser upper-air or remote-sensing observations, particularly in the lowest 1–2 km where
78 boundary-layer structure is most relevant to weather, pollution, and low-altitude activity. Filling
79 this gap requires an observing approach capable of providing flexible, repeatable, and vertically
80 resolved in-situ measurements within the lower atmosphere.

81 Unmanned aerial vehicles (UAVs) provide a practical means of reducing this observational
82 gap because they can obtain targeted in-situ measurements in layers that are difficult to sample
83 repeatedly with conventional platforms. Their mobility, relatively low operational cost, and



flexible deployment allow observations to be conducted over heterogeneous underlying surfaces, complex terrain, and rapidly evolving boundary-layer conditions. Over the past two decades, UAV-based atmospheric measurements have been used to characterize temperature and humidity profiles, turbulence, aerosols, trace gases, and urban or polar boundary-layer processes, demonstrating their value as an intermediate observing platform between fixed ground stations and conventional upper-air soundings (Cassano, 2014; Hobbs et al., 2002; Jonassen et al., 2015; Mamali et al., 2018; Reuder et al., 2012; Shelekhov et al., 2022). Recent studies have further shown that UAVs can provide high-resolution measurements of aerosol distributions and pollutant-related variables in the lower atmosphere, where vertical gradients are often strongest but least constrained by routine networks (Li et al., 2022; Pusfitasari et al., 2023; Weber et al., 2017).

Different UAV configurations, however, are suited to different observational objectives. Fixed-wing platforms offer longer endurance and broader horizontal coverage, making them useful for transects and regional surveys, but they generally require forward motion, larger operating space, and more complex flight paths when profiling a fixed column of air. Multi-rotor UAVs, by contrast, can take off and land vertically, hover at prescribed altitudes, and operate from confined sites without runways. These capabilities make them particularly suitable for fine-scale, layer-by-layer sounding of the lower ABL, where repeated measurements at selected heights are required to resolve vertical gradients of wind, temperature, humidity, and stability. Multi-rotor platforms have also been used to estimate low-altitude wind fields from onboard flight and attitude information, further extending their usefulness for boundary-layer observation when equipped with meteorological sensors (Palomaki et al., 2017; Wang et al., 2018). Therefore, for applications requiring vertically resolved, site-focused, and repeatable in-situ observations within the lower atmosphere, multi-rotor UAVs represent an appropriate observational choice.

Several studies have made important progress in validating UAV-based meteorological measurements. For wind observations, Shimura et al. (2018) compared hexarotor-derived wind profiles with tower observations and demonstrated the feasibility of wind-vector retrieval up to approximately 1000 m above the surface. Wetz et al. (2021) further showed that multiple quadrotor UAVs could provide distributed wind measurements in the ABL with good agreement against a 99 m tower. For thermodynamic measurements, Chang et al. (2020) developed an



114 optimized multicopter sounding technique and emphasized that sensor response delay can affect
115 temperature and humidity profiles during ascent and descent. At the campaign scale, Barbieri et
116 al. (2019) intercompared multiple small UAVs and showed that measurement quality depends
117 strongly on sensor configuration, aspiration, radiation shielding, and platform integration. These
118 studies collectively demonstrate that UAVs can provide useful lower-atmospheric observations
119 when appropriately configured and calibrated.

120 However, existing validation efforts still leave several limitations. First, many comparisons
121 have been conducted over relatively flat or horizontally homogeneous terrain, where flow
122 distortion, thermal heterogeneity, and local circulations are less complex than in mountainous or
123 terrain-transition regions. Second, validation has often focused on either a single reference height
124 or a limited vertical range, whereas boundary-layer applications require confidence across
125 multiple levels. Third, many studies have emphasized one category of variables, such as wind or
126 thermodynamic profiles, rather than jointly evaluating wind speed, wind direction, temperature,
127 humidity, and pressure together with derived stability-related parameters. Parameters such as
128 potential temperature and the gradient Richardson number are especially important because they
129 are not directly measured but are calculated from multiple basic variables; their uncertainty
130 therefore accumulates from both sensor error and vertical-gradient estimation. Consequently, a
131 key unresolved issue is whether a multi-rotor UAV can provide accurate, internally consistent
132 measurements of both conventional meteorological elements and derived ABL parameters across
133 multiple heights over complex terrain. Addressing this gap is a prerequisite for using UAV
134 observations not only as descriptive profiles, but also as quantitative evidence for boundary-layer
135 stability and turbulence analysis.

136 UAV observations are especially valuable in mountains, plateaus, glaciers, polar regions,
137 and other station-sparse environments, where complex terrain and heterogeneous surfaces
138 produce boundary-layer structures that are difficult to capture with fixed or routine observing
139 systems (Zhou et al., 2025; Groos et al., 2025; Hansche et al., 2023; Jonassen et al., 2015). Yet
140 these are also the environments in which strong vertical wind shear, terrain-induced turbulence,
141 gravity-wave disturbances, and localized updrafts or downdrafts most frequently occur. Such
142 dynamic forcing acts directly on multi-rotor aircraft, perturbing pitch, roll, yaw, angular velocity,
143 and vertical acceleration, and therefore affects both flight safety and platform stability (Wang et



144 al., 2019).

145 This coupling is particularly important because multi-rotor wind retrieval often depends on
146 aircraft attitude or control-response information (Palomaki et al., 2017; Wang et al., 2018). Thus,
147 atmospheric disturbances do not merely shake the platform; they can also contaminate the
148 meteorological signal inferred from the platform response itself. Existing studies have commonly
149 treated measurement accuracy and flight stability as separate issues, leaving insufficient evidence
150 on how vertical wind shear and stratification stability jointly regulate UAV attitude disturbances
151 under complex-terrain conditions. In particular, quantitative thresholds for stable operation
152 remain poorly constrained. A co-located, synchronized analysis of the environment–attitude
153 coupling is therefore necessary for both reliable UAV-based ABL observation and safe low-
154 altitude deployment.

155 Motivated by these two gaps, this study investigates both the measurement performance and
156 the environment–platform coupling of a multi-rotor UAV for ABL observation over complex
157 terrain. Specifically, we aim to: (1) systematically evaluate the accuracy of UAV-derived
158 conventional meteorological variables and stability-related parameters through co-located
159 comparison with a gradient meteorological tower; and (2) clarify how vertical wind shear and
160 stratification stability jointly modulate UAV attitude disturbances and identify quantitative
161 thresholds for stable operation. The analysis relies on fixed-point hovering and vertical-profile
162 observations collected during field campaigns at the Xingtai Field Scientific Experiment Base of
163 the China Meteorological Administration, together with mountain sounding observations in
164 Qianxian Township, Hebei Province. The remainder of this paper describes the observational
165 platforms and methods, presents the accuracy validation and attitude-response analysis, and
166 finally summarizes the implications for UAV-based ABL sensing and low-altitude flight-safety
167 assessment.

168

169 **2 Meteorological observations and methods**

170 *2.1 Gradient wind tower and UAVs measurements*

171 The meteorological tower at the experimental base is used to provide benchmark data for
172 the in-situ comparative verification of UAV-mounted meteorological sensors (Figure 1a). The



173 tower is vertically equipped with 10 observation layers at heights of 1 m, 2 m, 4 m, 8 m, 16 m,
174 32 m, 48 m, 64 m, 80 m and 96 m AGL, enabling minute-level vertical gradient observations of
175 air temperature, relative humidity, wind direction, wind speed, atmospheric pressure, and three-
176 dimensional ultrasonic wind within the ABL.

177 And a DJI MATRICE 350 RTK quadrotor UAV was deployed for all detection missions
178 (Figure 1b). The UAV platform has a maximum ascent speed of 6 m/s, a maximum descent speed
179 of 5 m/s, a maximum flight altitude of 5000 m, a maximum tolerable wind speed of 12 m/s, and
180 an endurance time up to 55 minutes. Prior to the field campaigns, laboratory metrological
181 calibration was conducted on the UAV-borne temperature, humidity, pressure, and wind sensors.
182 The measurement errors at all calibration points were lower than the specified qualified
183 thresholds, with no obvious data drift or missing records observed. The calibration results verify
184 that the equipped sensors achieve the measurement accuracy required for the experiment and
185 meet the technical requirements for low-altitude meteorological detection in this study.

186 To mitigate interference of propeller turbulence on meteorological observations, the
187 airborne meteorological payload was mounted 0.6 m directly above the UAV fuselage. This
188 optimized layout supports continuous, high-frequency in-situ observations of air temperature,
189 atmospheric pressure, relative humidity, atmospheric wind direction and wind speed at a 1 Hz
190 temporal resolution.

191 *2.2 Experimental design and methodology*

192 The experiments were designed with two objectives, each carried out at a separate site. To
193 validate the measurement accuracy of the UAV meteorological sensors, comparative observation
194 experiments were conducted at the Xingtai Field Scientific Experiment Base for Atmospheric
195 Environment, China Meteorological Administration (Figure 2), located in Liulin Town, Neiqiu
196 County, Xingtai City, Hebei Province, China (elevation: 163.6 m). This base is equipped with a
197 100 m gradient meteorological tower and supporting UAV observation facilities, whose tower-
198 based reference measurements enabled direct accuracy assessment of the UAV sensors.
199 Investigating the impact of atmospheric boundary layer dynamics on UAV flight stability,
200 however, required flights at considerably greater altitudes. Owing to airspace control restrictions
201 at the Xingtai base, these could not be performed there; accordingly, boundary layer flight



202 disturbance experiments were instead conducted in Qianxian Township, Yuanshi County, where
203 the airspace conditions permitted the higher-altitude flights needed for this part of the study.

204 The comparative observation experiments were conducted with synchronous measurements
205 from the UAV and the gradient meteorological tower. The UAV operated in two flight modes:
206 vertical ascent/descent and fixed-point hovering at specified heights, with the hovering heights
207 corresponding to the gradient tower levels of 8 m, 16 m, 32 m, 48 m, 64 m, 80 m, and 96 m AGL,
208 respectively. At each corresponding hovering height, a minimum hovering duration of 15 seconds
209 was maintained to ensure sampling stability. And to eliminate mutual observational interference
210 between UAV and gradient tower measurements, the UAV's horizontal flight path was arranged
211 approximately 50 m upwind of the meteorological tower during all field experiments. This spatial
212 layout effectively minimizes the disturbances induced by tower wake flow and UAV rotor
213 downwash on both sets of observational datasets, thereby enabling high-quality simultaneous
214 comparative measurements. The experiments were conducted from July 26th to July 30th, 2025.
215 Each dataset was defined as one complete observation segment comprising a vertical ascent or
216 descent process together with the corresponding fixed-point hovering measurements at each
217 height. On this basis, a total of 39 fixed-point hovering datasets were collected throughout the
218 experimental campaign.

219 In the boundary layer flight disturbance experiments, the UAV's hovering heights started
220 from 200 m AGL and increased at 200 m intervals up to 1500 m, with a minimum hovering
221 duration of 15 s at each height, consistent with the comparative observation experiments. The
222 experiments were conducted on July 31th, 2025. In addition to conventional meteorological
223 variables, the UAV system continuously synchronously records multi-dimensional data,
224 including flight attitude parameters (pitch angle, roll angle, yaw angle) and real-time flight
225 trajectories. A total of 46 vertical profile datasets were collected throughout the experimental
226 campaign.

227 *2.3 Data processing*

228 For both fixed-point hovering datasets and vertical profile datasets, the same data quality
229 control procedure was applied. Owing to the influence of UAV motion during flight, all non-
230 hovering segments were excluded, and only the data acquired during stable hovering segments



231 were retained. On this basis, the interquartile range (IQR) method was adopted to identify and
232 remove outliers in meteorological variables, including temperature, atmospheric pressure,
233 relative humidity, wind direction, and wind speed.

234 To fully exploit the UAV's 1 Hz observations, instead of averaging within each hovering
235 layer before differencing, this study computed pairwise finite differences between every 1 Hz
236 sample of adjacent hovering layers. Let the segment at height z_i contain N_i valid 1 Hz samples of
237 potential temperature ($\theta_{i,m}$) and horizontal wind ($u_{i,m}, v_{i,m}, m = 1, \dots, N_i$), and that at z_{i+1} contain
238 N_{i+1} samples ($n = 1, \dots, N_{i+1}$).

239 For each sample pair (m, n), the vertical gradients of potential temperature and wind shear
240 were computed as:

$$241 \quad \left(\frac{\partial \theta}{\partial z}\right)_{m,n} = \frac{\theta_{i+1,n} - \theta_{i,m}}{z_{i+1} - z_i} \quad (1)$$

$$242 \quad \left(\frac{\partial u}{\partial z}\right)_{m,n} = \frac{u_{i+1,n} - u_{i,m}}{z_{i+1} - z_i} \quad (2)$$

$$243 \quad \left(\frac{\partial v}{\partial z}\right)_{m,n} = \frac{v_{i+1,n} - v_{i,m}}{z_{i+1} - z_i} \quad (3)$$

244 Substituting Eqs.1-3 into the definition of the gradient Richardson number equation yields the
245 following expression for $Ri_{m,n}$:

$$246 \quad Ri_{m,n} = \frac{g}{\bar{\theta}_{m,n}} \cdot \frac{\left(\frac{\partial \theta}{\partial z}\right)_{m,n}}{\left(\frac{\partial u}{\partial z}\right)_{m,n}^2 + \left(\frac{\partial v}{\partial z}\right)_{m,n}^2} \quad (4)$$

247 where $\bar{\theta}_{m,n} = (\theta_{i,m} + \theta_{i+1,n})/2$ is the pair-mean potential temperature and g is the gravitational
248 acceleration. This procedure produces $N_i \times N_{i+1}$ Ri samples for each pair of adjacent hovering
249 measurement layers. The resulting output is a full distribution of Ri values, rather than a single
250 representative value derived from bulk layer-averaged meteorological quantities.

251 The flight attitude of a UAV responds directly to atmospheric turbulence; therefore, the
252 characteristics of its attitude disturbance can serve as an indirect indicator of turbulence intensity.
253 Accordingly, an attitude turbulence index is constructed from the pitch and roll angular velocities
254 to quantitatively characterize the overall intensity of the UAV flight attitude disturbance induced



255 by atmospheric turbulence:

$$256 \quad T = \sqrt{\omega^2 + \phi^2} \quad (5)$$

257

258 where ω and ϕ are the pitch angular velocity and roll angular velocity, respectively, and T
259 represents the attitude turbulence index. A higher T value corresponds to stronger atmospheric
260 turbulence and more intense UAV attitude disturbance.

261 **3 Results and discussion**

262 *3.1 Analysis of basic meteorological elements from field campaign*

263 To demonstrate the capability of the UAV system in observing the vertical structural
264 characteristics of the near-surface ABL, vertical ascent and descent profile experiments were
265 conducted from July 26 to 30, 2025. These experiments acquired continuous vertical distribution
266 datasets of near-surface meteorological variables, including air temperature, relative humidity,
267 and wind fields. The vertical profile comparisons of meteorological parameters at different
268 heights are summarized in Figure 3.

269 Overall, the vertical profiles of temperature, relative humidity, wind speed, and wind
270 direction derived from the UAV measurements (red lines) and the gradient tower observations
271 (blue lines) achieve excellent morphological consistency with low statistical errors. Specifically,
272 the wind speed profiles show a negligible bias of 0.02 m/s and an RMSE of 1.11 m/s, while the
273 temperature profiles yield a small bias of 0.10 °C and an RMSE of 0.90 °C, indicating nearly
274 identical profile shapes and minimal systematic deviations between the two observation
275 platforms. Slight fluctuating discrepancies at individual heights are observed for wind direction
276 and relative humidity, with biases of 8.56° and 0.17% and RMSEs of 20.35° and 4.14%,
277 respectively. Despite these minor height-dependent fluctuations, the overall vertical variation
278 trends of the UAV observations align well with the tower benchmark data, and all deviations
279 remain within a reasonable and acceptable range. These results verify that the UAV-borne
280 meteorological payload can accurately capture the vertical distribution patterns of ABL
281 meteorological variables and maintain stable observational precision across all detected heights,
282 demonstrating that the UAV platform fully meets the technical requirements for refined vertical
283 profile detection of low-altitude atmospheric environments.



284 Synchronized observations from the UAV and the gradient meteorological tower were
285 further adopted to compare and validate the vertical profiles of key thermodynamic and dynamic
286 parameters within the ABL, with the comparative results illustrated in Figure 4. The vertical
287 profiles of potential temperature (θ) and gradient Richardson number (Ri) derived from the UAV
288 measurements achieve favorable consistency with the tower observations. For potential
289 temperature, the CC reaches 0.64, with a bias of 0.15 K and an RMSE of 0.85 K; its vertical
290 profile morphology and gradient characteristics are in good agreement with the tower benchmark
291 data, demonstrating that the UAV system can accurately resolve the vertical thermal stratification
292 structure of the ABL. For the gradient Ri , the CC is likewise 0.64, accompanied by an extremely
293 low bias of -0.01 and an RMSE of 0.05, indicating that the UAV reliably identifies the dynamic
294 stability regimes at all vertical layers of the ABL without noticeable altitude-dependent
295 systematic deviations. These findings indicate that the UAV-borne meteorological system is
296 capable of not only directly acquiring high-quality profiles of conventional meteorological
297 variables but also accurately retrieving key thermodynamic and dynamic parameters of the
298 boundary layer, further validating that the multi-rotor UAV platform is well suited for refined
299 observational characterization and stability mechanism analysis of low-altitude atmospheric
300 processes.

301 *3.2 Impacts of ABL Spatiotemporal Evolution on UAV Flight Attitude*

302 Three typical UAV low-level sounding campaigns, conducted during three successive
303 periods (18:24–18:43, 18:55–19:22, and 19:43–19:55 BJT) on the evening of July 31, 2025 in
304 Qianxian Township, Yuanshi County, Hebei Province, were selected for representative case
305 analysis. The study area is located in the hilly transitional zone on the eastern piedmont of the
306 Taihang Mountains, featuring a typical mountain–plain transition terrain dominated by
307 alternating hills and low mountains. The local weather condition shifted from cloudy to overcast
308 on the afternoon of July 31. Analysis of hourly ECMWF ERA5 pressure-level synoptic fields
309 (Figure 5a) shows that a shallow upper-level trough moved eastward. Below 850 hPa, the region
310 was dominated by southerly winds and weak moisture advection, accompanied by weak easterly
311 wind convergence at 925 hPa, with low-level relative humidity ranging from 60% to 80%. Under
312 this synoptic background, sporadic light drizzle occurred in Qianxian Township from 18:00 to



313 20:00 BJT.

314 Time–height cross sections of low-level vertical wind shear (Figure 5c) indicate that the
315 observation window corresponded to a transition stage during which the convective atmospheric
316 boundary layer (CABL) gradually evolved into a stable atmospheric boundary layer (SABL).
317 The wind shear field exhibited distinct layered structures and evident temporal evolutionary
318 characteristics. In the near-surface layer (60–200 m AGL), jointly modulated by diurnal ABL
319 evolution and topographic forcing, steady positive vertical wind shear persisted and increased
320 with height (red shaded areas), with shear magnitudes predominantly ranging from 0 to $3 \times 10^{-3} \text{ s}^{-1}$.
321 ¹. This phenomenon is closely associated with evening surface radiative cooling and weakened
322 turbulent mixing. By contrast, the middle and upper layers (200–1500 m AGL) presented
323 fluctuating vertical structures characterized by alternating positive and negative wind shear zones.
324 Notably, prominent negative shear regimes occurred at 200–800 m AGL during 17:45–18:30 and
325 19:15–20:00 BJT (blue shaded areas), with maximum shear intensities reaching $3 \times 10^{-3} \text{ s}^{-1}$. The
326 three UAV sounding trajectories (ascent and descent segments denoted by solid/dashed black,
327 red, and blue lines, respectively) fully captured this critical ABL transition process.

328 (1) Case of UAV sounding Experiment from 18:24 to 18:43

329 Combined with the vertical structure of atmospheric physical environmental fields (Figure
330 6) and UAV attitude response profiles (Figure 7), the near-surface stable ABL (200–400 m AGL)
331 is characterized by a rapid increase in potential temperature with height, forming a strongly stable
332 stratification regime with Richardson number (Ri) greater than 0.25, where turbulent motions are
333 substantially suppressed. In this layer, wind speed increases gently with height, generating weak
334 vertical wind shear. Under the coupled constraints of strong thermal stability and insignificant
335 dynamic shear, the deviations of UAV pitch and roll angles are both limited within $\pm 1^\circ$, the
336 fluctuation range of attitude angular velocity is lower than $0.05^\circ/\text{s}$, and the turbulence index
337 remains below 5, corresponding to generally stable UAV flight attitudes.

338 In the weakly stratified middle-upper layer (400–1000 m AGL), the potential temperature
339 gradient decreases significantly, and the atmospheric stratification approaches a neutral state,
340 with Ri fluctuating between 0 and 0.25, which provides favorable conditions for turbulent
341 development. Meanwhile, wind speed rises sharply with height, producing intense vertical wind
342 shear. In this layer, UAV pitch and roll angles exhibit distinct oscillatory disturbances; the



343 fluctuation amplitude of attitude angular velocity expands to $\pm 0.15^\circ/\text{s}$, and the turbulence index
344 peaks at 8–15. This layer dominates the most prominent attitude perturbations and flight
345 bumpiness throughout the entire radiosounding process.

346 The upper strongly stable layer (1000–1400 m AGL) features a re-intensified potential
347 temperature gradient, with Ri rebounding above 0.25. The atmospheric stratification returns to a
348 highly stable state that effectively inhibits turbulent activities. Wind speed decreases slightly with
349 height, accompanied by weakened vertical shear. Restricted by the combined effects of restored
350 thermal stability and weakened dynamic shear, the fluctuations of UAV attitude angular velocity
351 gradually decay, the turbulence index declines steadily, and flight stability recovers, presenting
352 consistent response characteristics with the near-surface stable layer.

353 Furthermore, the relative humidity profile reveals a persistent high-humidity zone ($RH >$
354 80%) at 200–400 m AGL during the UAV descent phase. However, this moist layer corresponds
355 to weak turbulent activity and stable flight attitudes, demonstrating that water vapor
356 concentration alone is not a dominant factor inducing UAV attitude disturbances. During the
357 descent process, local cloud clusters shift southeastward, increasing low-level atmospheric
358 moisture content and reducing ambient wind speed, which slightly enhances local atmospheric
359 instability within the low-level and in-cloud layers. In contrast, the middle and upper layers are
360 predominantly dry and cloud-free, eliminating additional interference from cloud droplet impacts
361 and in-cloud buoyancy perturbations. These observational phenomena further confirm that UAV
362 attitude disturbances in complex terrain are primarily governed by dynamic turbulence
363 modulated by the synergistic effects of vertical wind shear and atmospheric stratification stability,
364 rather than moisture conditions..

365 (2) Case of UAV Radiosounding Experiment from 18:55 to 19:22

366 The thermal, dynamic, and humidity variables of the ABL exhibited pronounced vertically
367 stratified evolutionary characteristics during the observation period (Figure 8), with the
368 corresponding UAV attitude responses shown in Figure 9.. In the near-surface layer of 200–600
369 m AGL, the Ri consistently exceeded 0.25, corresponding to strongly stable atmospheric
370 stratification, weak vertical wind shear, and substantially suppressed turbulent motion, thereby
371 forming an overall quiescent low-altitude atmospheric environment.

372 In the middle layer of 600–1000 m AGL, the vertical gradient of potential temperature



373 weakened markedly, and the atmospheric stratification gradually approached a neutral state.
374 Meanwhile, the vertical wind speed gradient increased sharply, providing favorable dynamical
375 conditions for the development of flow instability. Additionally, the vertical moisture distribution
376 presented notable discrepancies between UAV ascent and descent observations

377 The upper layer of 1000~1400 m AGL near the cloud base was characterized by weakly
378 unstable stratification and the maximum vertical wind shear throughout the profile. Enhanced
379 entrainment processes promoted vigorous turbulent development, substantially facilitating
380 momentum and water vapor exchange between upper and lower atmospheric layers. Accordingly,
381 atmospheric disturbance intensity increased steadily with altitude in this zone.

382 In the stably stratified near-surface layer with low turbulence levels, the RMSE fluctuation
383 amplitudes of UAV pitch and roll angles were all below 1.8° , the mean dynamic attitude angular
384 velocity remained within $0.3^\circ \cdot s^{-1}$, and the vertical acceleration fluctuations were confined within
385 $\pm 0.10 \text{ m} \cdot s^{-2}$. These quantitative metrics further verify that strong static stability effectively
386 suppresses local airflow pulsations. And at high altitudes near the cloud base with intense
387 dynamic disturbances, UAV attitude perturbations reached their maximum magnitudes across the
388 entire vertical profile. Specifically, the RMSE attitude angle fluctuation exceeded 3.9° , the
389 instantaneous peak angular velocity reached $0.82^\circ \cdot s^{-1}$, and the extreme vertical acceleration
390 fluctuations surpassed $\pm 0.30 \text{ m} \cdot s^{-2}$. The superposition of intensive local turbulence and
391 compound vertical wind shear ultimately triggered severe in-flight bumpiness and prominent
392 attitude oscillations.

393 The combined effects of downdraft convergence beneath the cloud base, spatial
394 heterogeneity of local flow fields, and divergent dynamic environments along ascent and descent
395 trajectories generated distinctly asymmetric evolutionary patterns in UAV dynamic attitude
396 responses during outbound and return flights. These findings demonstrate that vertical
397 stratification differences in atmospheric thermal structures and dynamic flow fields are the
398 dominant factors driving the spatiotemporal heterogeneity of multi-rotor UAV flight attitude
399 disturbances over complex terrain.

400 (3) A case of UAV sounding experiment from 19:43 to 19:55

401 The atmospheric thermal and dynamic structures over the study area exhibited remarkable



402 vertical stratification and spatial inhomogeneity (Figure 10). In terms of thermal characteristics,
403 potential temperature generally increased with height under predominantly stable stratification,
404 with distinct differences observed between in-cloud and out-of-cloud layers (approximately
405 900~1200 m). A steeper vertical gradient of potential temperature occurred when the UAV
406 penetrated the cloud layer, indicating substantially enhanced static stability within the cloud.
407 Relative humidity profiles differed considerably between ascent and descent phases, notably
408 lower low-level humidity during descent revealed prominent horizontal inhomogeneity in
409 moisture distributions across cloudy and clear-sky regions. Dynamically, the wind field was
410 dominated by intense vertical shear, with wind speed generally increasing with height and wind
411 shear drastically amplified near the cloud layer. In the lower layer (200~800 m), the Ri
412 approached zero, representing dynamically unstable conditions that favored turbulent generation
413 and development. Above the cloud layer, Ri increased sharply, restoring atmospheric stability
414 and suppressing turbulent activities. Such vertical disparities in thermal stratification and
415 dynamic stability constituted the dominant atmospheric background modulating UAV flight
416 states. Quantitative correlations between spatiotemporal variations in atmospheric
417 thermodynamic conditions and UAV flight attitude parameters are illustrated in Figure 11, which
418 reveals significant layered differences in the perturbation magnitudes of attitude angles,
419 turbulence indices, and vertical motion between UAV ascent and descent processes.

420 In terms of attitude angle variations, the UAV pitch angle remained consistently positive at
421 2~6° during ascent, declining gently with altitude with a small standard deviation and smooth
422 flight performance. Correspondingly, the roll angle stabilized near 0° , with overall deviations
423 constrained within $\pm 1^\circ$. In contrast, the pitch angle was predominantly negative (-5~-1°)
424 throughout the descent phase. Dramatically amplified angle fluctuations were observed within
425 the dynamically unstable 200~800 m layer, where the standard deviation of pitch angle nearly
426 doubled relative to the ascent phase. Meanwhile, the roll angle exhibited substantial negative
427 offsets exceeding -3° . These distinct discrepancies demonstrate that crosswind disturbances
428 and lift fluctuations induced by spatially heterogeneous low-level wind and thermal conditions
429 significantly distort the UAV airframe attitude during descent.

430 With respect to turbulence intensity and vertical motion metrics, the dynamically unstable



431 200~800 m layer exhibited a markedly higher turbulence index during descent than during ascent,
432 with the maximum turbulence magnitude occurring near the surface. By comparison, the ascent
433 phase maintained low turbulence levels and weak fluctuations across this layer. Driven by
434 ambient turbulent pulsations, high-frequency oscillations of vertical acceleration were detected
435 at low altitudes during both flight phases. The peak-to-trough difference in vertical acceleration
436 exceeded $0.15 \text{ m}\cdot\text{s}^{-2}$ during ascent, indicative of intense local aerodynamic perturbations. In the
437 stable cloud-top layer above 1000 m, enhanced atmospheric dynamic stability effectively
438 suppressed turbulent activities, restricting vertical acceleration fluctuations within $\pm 0.03 \text{ m}\cdot\text{s}^{-2}$
439 and restoring all attitude parameters to a stable state.

440 Collectively, the quantitative observational results confirm a strong negative correlation
441 between atmospheric dynamic stability and the fluctuation amplitude of UAV flight parameters.
442 Intense low-level turbulence and vertically heterogeneous thermal-dynamic atmospheric
443 structures are identified as the primary drivers of asymmetric attitude disturbances and divergent
444 unsteady flight performance between UAV ascent and descent trajectories over complex terrain.
445

446 *3.3 Vertical wind shear and Ri impacts on UAV attitude in flight disturbance experiments*

447 The joint distribution of the Ri and vertical wind shear (Figure 12) illustrates how
448 atmospheric stratification stability and dynamic forcing jointly modulate turbulence intensity,
449 thereby governing UAV flight attitude disturbances. The number within each grid cell denotes
450 the sample count, the cell color indicates the mean turbulence index (TI), and the top and right
451 marginal distributions present the mean TI averaged along the Ri and wind-shear directions,
452 respectively. Vertical wind shear, the primary dynamic source of mechanical turbulence, couples
453 with Ri—which quantifies stratification stability—to jointly control boundary-layer turbulence.

454 The observations are predominantly concentrated within vertical wind shear of
455 approximately $0.005\text{--}0.020 \text{ s}^{-1}$ and Ri between -1 and 3 , narrowing toward $\text{Ri} \approx 0\text{--}1$ as wind
456 shear increases and forming a triangular distribution. This indicates that strong wind shear tends
457 to co-occur with near-neutral stratification, whereas large shear combined with strongly stable
458 stratification is rare.

459 Overall, the TI tends to increase with vertical wind shear, consistent with the expectation



460 that stronger dynamic shear intensifies mechanical turbulence and aggravates flight bumpiness.
461 Under unstable stratification ($Ri < 0$), the mean TI is further elevated (exceeding 2.9 in the top
462 marginal distribution), as thermal convection superimposed on shear-induced disturbances
463 enhances turbulence, readily triggering pronounced pitch, roll, and yaw oscillations and
464 increasing the flight control burden.

465 Notably, a localized zone of anomalously high TI (approaching or exceeding 3.0) appears
466 at moderate wind shear (approximately $0.007\text{--}0.010\text{ s}^{-1}$) combined with near-zero to negative Ri ,
467 deviating from the general monotonic trend. This may not stem from atmospheric forcing alone.
468 One plausible explanation is that, within this range, the characteristic scale of turbulent eddies
469 may become comparable to the airframe dimensions and approach the intrinsic dynamic response
470 frequency of the multi-rotor UAV, potentially inducing a resonance-like amplification of the
471 attitude response beyond what the ambient turbulence intensity alone would suggest. This
472 interpretation remains tentative and warrants further verification through controlled experiments
473 and platform-specific dynamic response analysis.

474 Within the near-neutral to weakly stable regime, samples are most densely populated,
475 forming a high-frequency turbulence zone where stratification only weakly inhibits turbulent
476 development, so that even moderate wind shear can excite noticeable perturbations and minor
477 attitude oscillations. As stratification transitions toward the strongly stable regime, thermal
478 suppression intensifies and partially counteracts shear-induced disturbances, corresponding to
479 relatively stable flight states.

480 In summary, the coupling of vertical wind shear and stratification stability jointly shapes
481 ABL turbulence, with flight bumpiness generally intensifying as wind shear strengthens. Beyond
482 this atmospheric forcing, the potential coupling between turbulence scales and the UAV's own
483 dynamic characteristics may further modulate the attitude response in certain regimes. Together,
484 these factors dominate UAV attitude disturbances and fundamentally determine the flight
485 stability of low-altitude UAV observations over complex terrain.

486 **4 Concluding remarks**

487 This study investigated the measurement performance and the environment–platform
488 coupling of a multi-rotor UAV (DJI Matrice 350 RTK) for atmospheric boundary layer (ABL)



489 observation over complex terrain, based on co-located comparison experiments at the Xingtai
490 Field Scientific Experiment Base and boundary layer flight disturbance experiments in Qianxian
491 Township, Yuanshi County, Hebei Province. Two objectives were addressed: validating the
492 accuracy of UAV-derived meteorological and stability parameters against a gradient
493 meteorological tower and clarifying how vertical wind shear and stratification stability jointly
494 modulate UAV attitude disturbances.

495 The accuracy validation demonstrates that the UAV-borne meteorological payload can
496 reliably capture the vertical structure of the near-surface ABL. Compared with the 100 m gradient
497 tower, the UAV measurements achieved excellent morphological consistency and low statistical
498 errors across all detected heights, with negligible biases in wind speed (0.02 m/s) and temperature
499 (0.10 °C), and acceptable deviations in wind direction and relative humidity. Importantly, the
500 UAV also accurately retrieved derived thermodynamic and dynamic parameters, including
501 potential temperature ($CC = 0.64$, $RMSE = 0.85$ K) and the gradient Richardson number ($CC =$
502 0.64 , $RMSE = 0.05$), confirming that the platform resolves not only conventional variables but
503 also the thermal stratification and dynamic stability regimes of the boundary layer.

504 The attitude-response analysis reveals that UAV flight disturbances over complex terrain
505 are primarily governed by dynamic turbulence generated through the coupling of vertical wind
506 shear and stratification stability, rather than by moisture conditions. Across three representative
507 sounding cases spanning the transition from a convective to a stable boundary layer, attitude
508 disturbances (pitch, roll, angular velocity, and the turbulence index T) were suppressed in
509 strongly stable layers ($Ri > 0.25$) and amplified in near-neutral or weakly unstable layers ($0 < Ri$
510 < 0.25 or $Ri < 0$) where intense wind shear coincided with weak thermal suppression. Pronounced
511 asymmetries between ascent and descent trajectories further indicate that spatially heterogeneous
512 low-level flow and thermal structures drive the spatiotemporal heterogeneity of flight
513 disturbances.

514 The joint distribution of Ri and vertical wind shear shows that turbulence intensity, and
515 hence flight bumpiness, generally intensifies as wind shear strengthens, with the strongest
516 disturbances under unstable stratification, while strongly stable stratification ($Ri > 2-3$) partially
517 counteracts shear-induced disturbances. A localized anomaly of elevated turbulence response at
518 moderate shear and near-zero to negative Ri suggests a possible resonance-like coupling between



519 turbulent eddy scales and the UAV's own dynamic response, though this interpretation remains
520 tentative and requires further study. Overall, these findings establish quantitative thresholds
521 relevant to both reliable UAV-based ABL sensing and safe low-altitude flight-safety assessment,
522 supporting the use of multi-rotor UAVs as a valuable intermediate observing platform for refined
523 boundary-layer characterization over station-sparse, complex-terrain regions.

524

525 **Data availability**

526 All observational data used in this study, comprising the 1-min gradient meteorological
527 tower records for July 2025 and the 1-Hz UAV-borne sonde measurements are accessible from
528 Yang, R (2026).

529 **Author contribution**

530 Conceptualization: JianpingGuo, RongfangYang

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533 Fundingacquisition: RongfangYang

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535 Methodology: RongfangYang, DeliMeng, Lihui Liu, Guocui Li, Guanglei Zhang

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545 **Competing interests**

546 The authors declare no conflicts of interest relevant to this study.

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552 Beijing-Tianjin-Hebei Region" (grant no. CXFZ2025J107).

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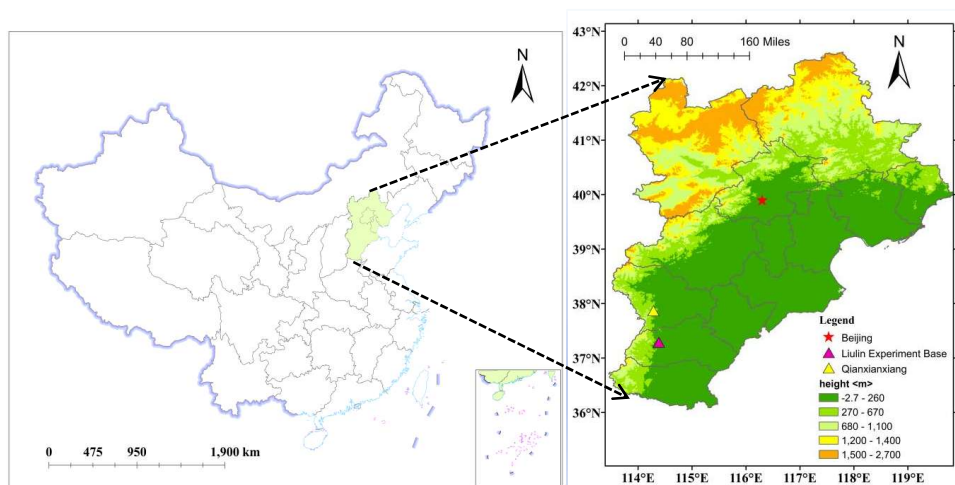
Figures



Figure 1. (a) Snap shot of the meteorological tower deployed at the Xingtai Field Scientific Experiment Base; (b) The multi-rotor UAV platform and integrated airborne meteorological payload used for field observations in this study.



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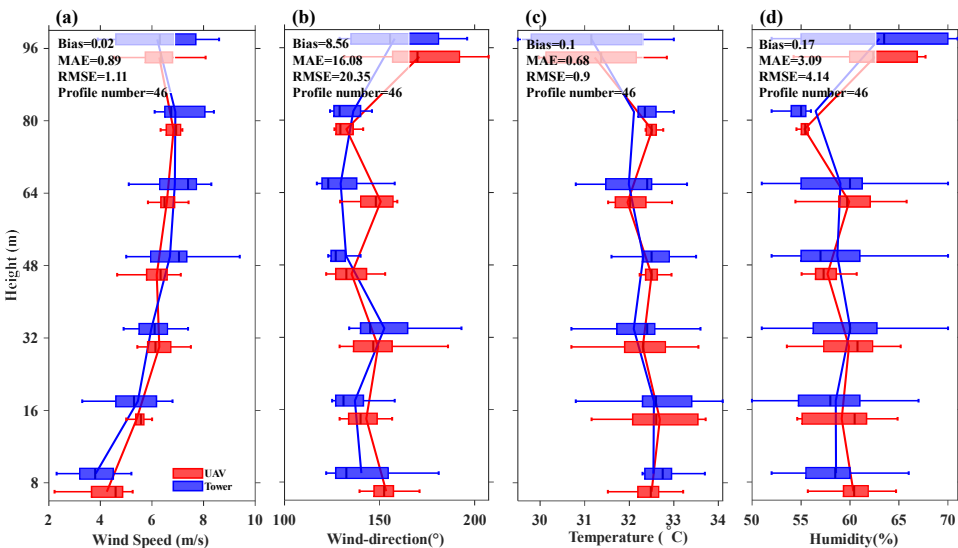
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657 **Figure 2.** Topographical map of the surrounding area of the Aerodynamic Environment Field
658 Scientific Experiment Base, showing the location of the gradient meteorological tower (red
659 triangle).
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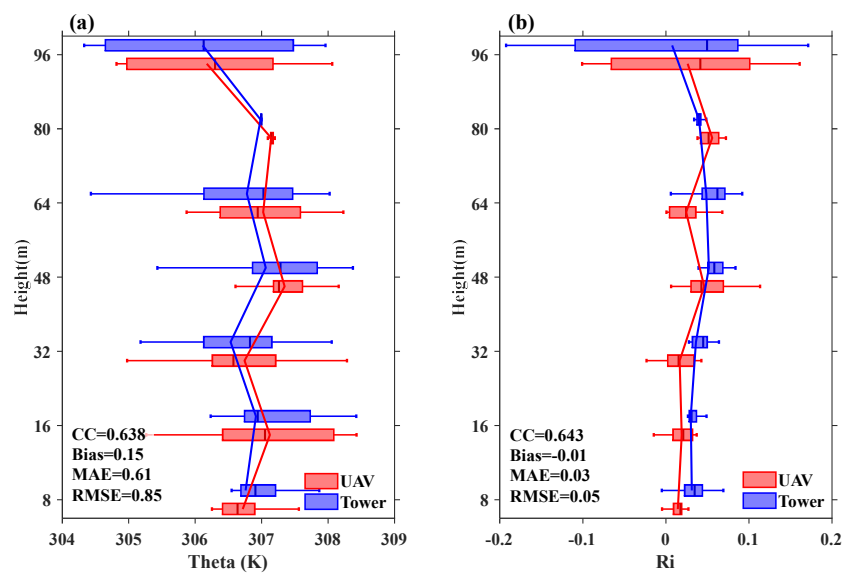
663

664 **Figure 3.** Vertical profiles of meteorological elements observed by the UAV platform and
665 gradient meteorological tower during the period from July 26 to 30, 2025: (a) wind speed, (b)
666 wind direction, (c) air temperature, (d) relative humidity.

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669

670 **Figure 4.** Vertical profiles of key atmospheric parameters observed by the UAV platform and

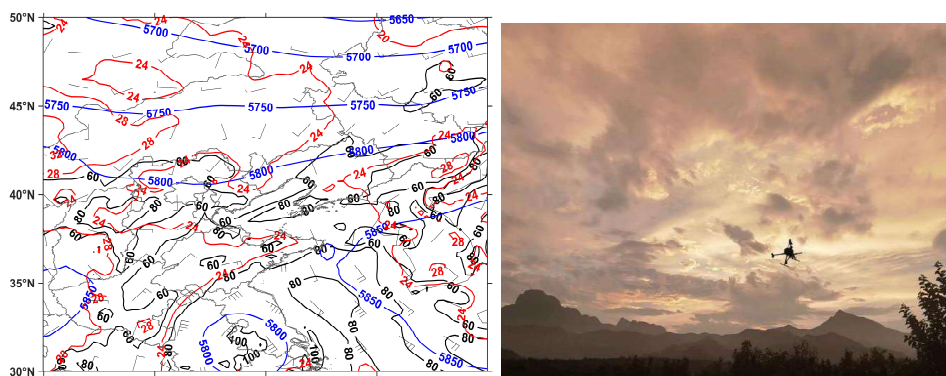
671 gradient meteorological tower during the period from July 26 to 30, 2025: (a) potential

672 temperature (θ), (b) gradient Richardson number (Ri)

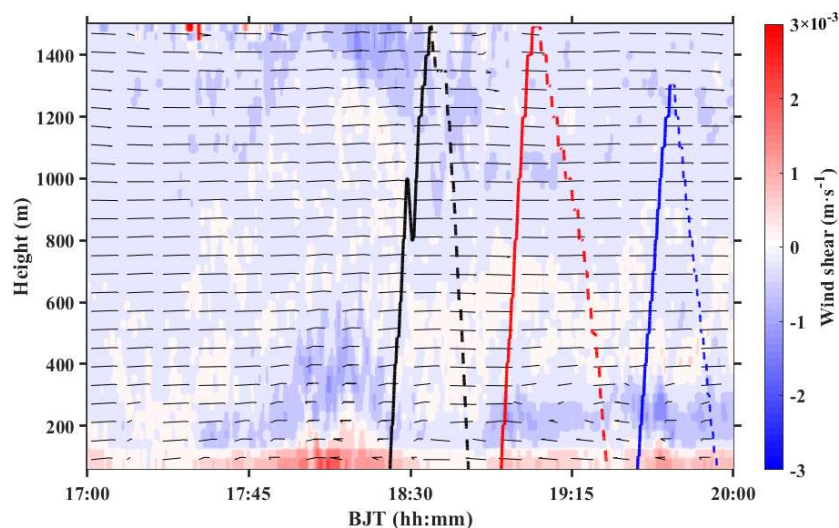
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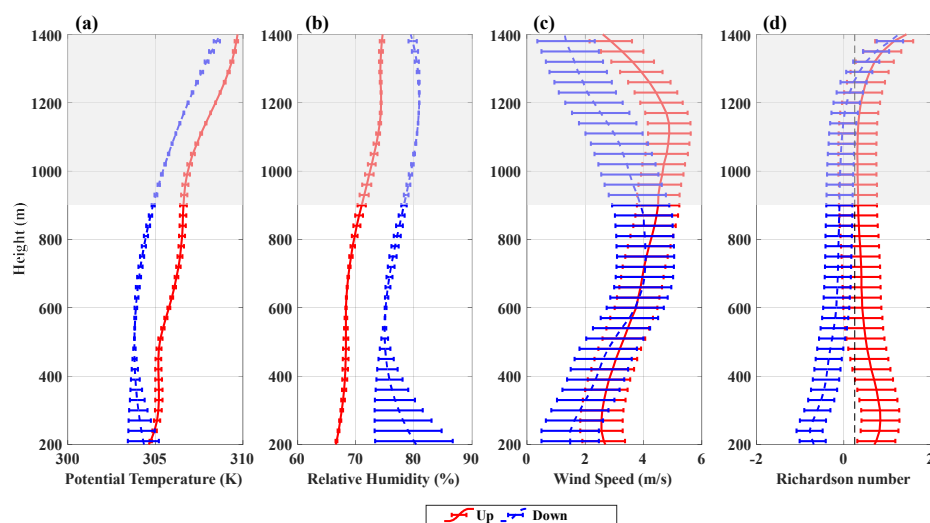


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677 **Figure 5.** (a) Spatial distributions of the 500 hPa geopotential height (blue contours, units: gpm),
678 925 hPa temperature (red contours, units: °C), 925 hPa relative humidity (black contours,
679 units: %), and horizontal wind field (wind barbs) at 14:00 BJT on July 31, 2025. (b) Vertical
680 profiles derived from UAV hovering observations at Qianxian Township on July 31, 2025. (c)
681 Time-height cross section of the wind field from 17:00 to 20:00 BJT on July 31, 2025. The shaded
682 contours represent the magnitude of vertical wind shear of horizontal winds; positive values
683 indicate normal shear (wind speed increases with height), while negative values denote reverse
684 shear (wind speed decreases with height, units: s^{-1}). The solid and dashed black, red, and blue
685 lines represent the ascent and descent trajectories of the three UAV sounding flights, respectively:
686 black for 18:24~18:43 BJT, red for 18:55~19:22 BJT, and blue for 19:43~19:55 BJT.



687

688 **Figure 6.** Vertical profiles of atmospheric background field during 18:24–18:43 BJT on July 31,

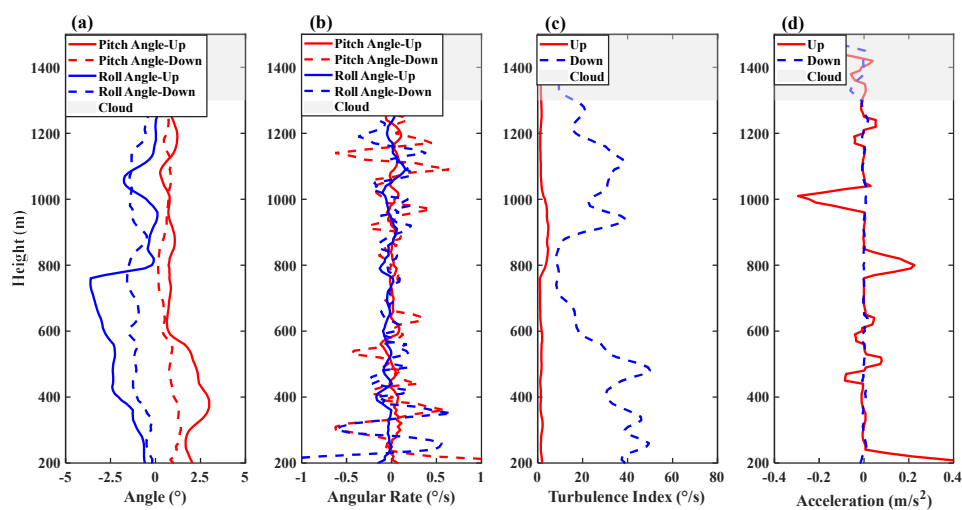
689 2025: (a) potential temperature, (b) relative humidity, (c) wind speed, (d) gradient Richardson

690 number

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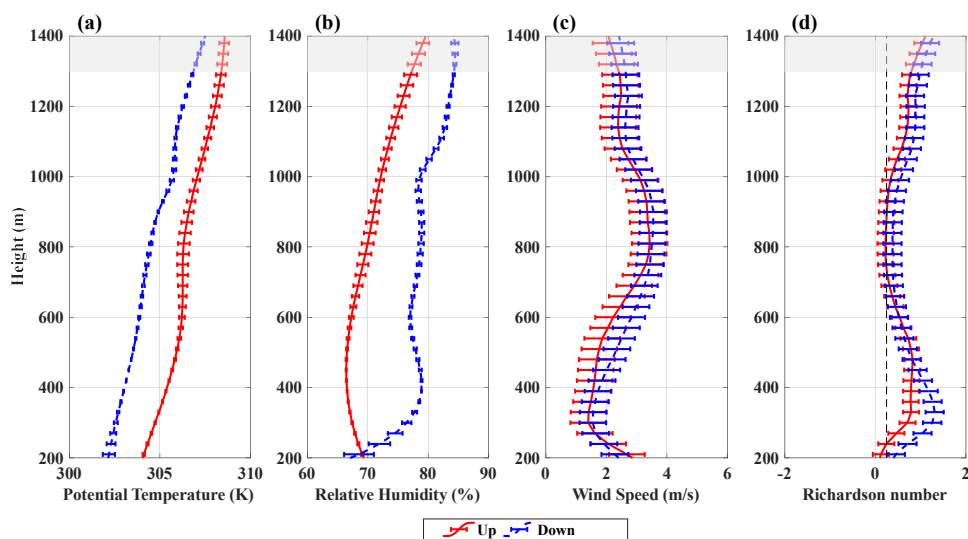


693

694 **Figure 7.** Vertical response profiles of UAV flight attitude parameters during 18:24–18:43 on
 695 July 31, 2025: (a) attitude angles profile, (b) angular rate profile, (c) turbulence index profile, (d)
 696 vertical acceleration profile
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700 **Figure 8.** Same as Figure 6, but for the period of 18:55–19:22 BJT on July 31, 2025.

701

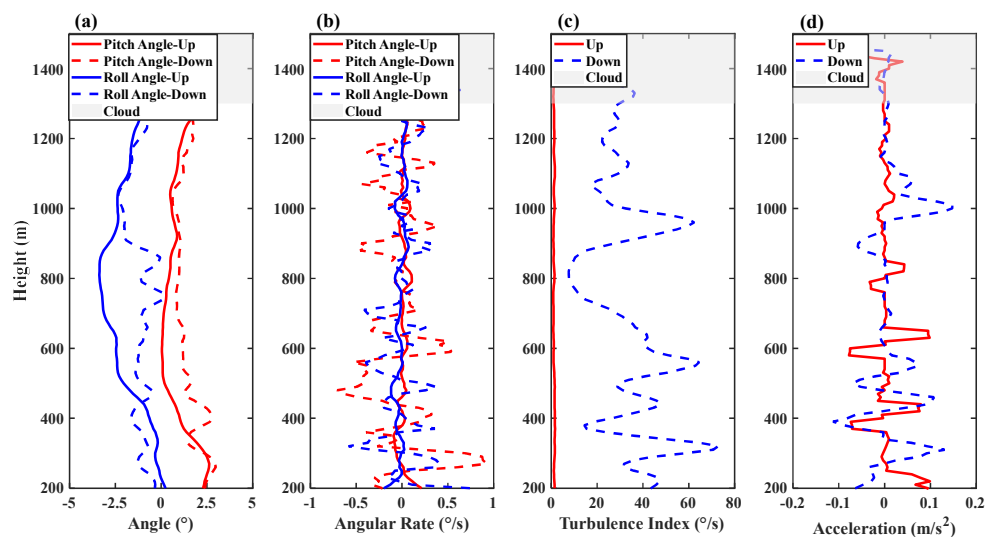
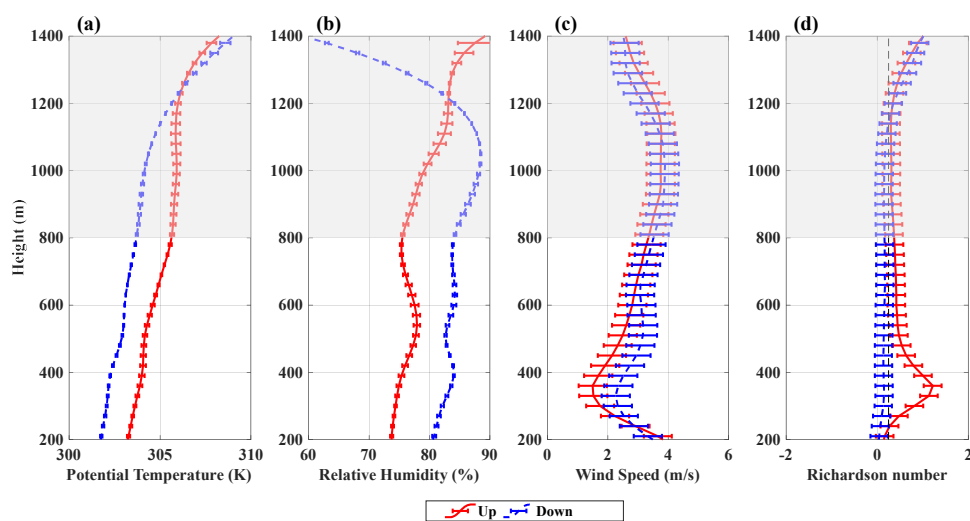


Figure 9. Same as Figure 7, but for the period of 18:55–19:22 BJT on July 31, 2025.



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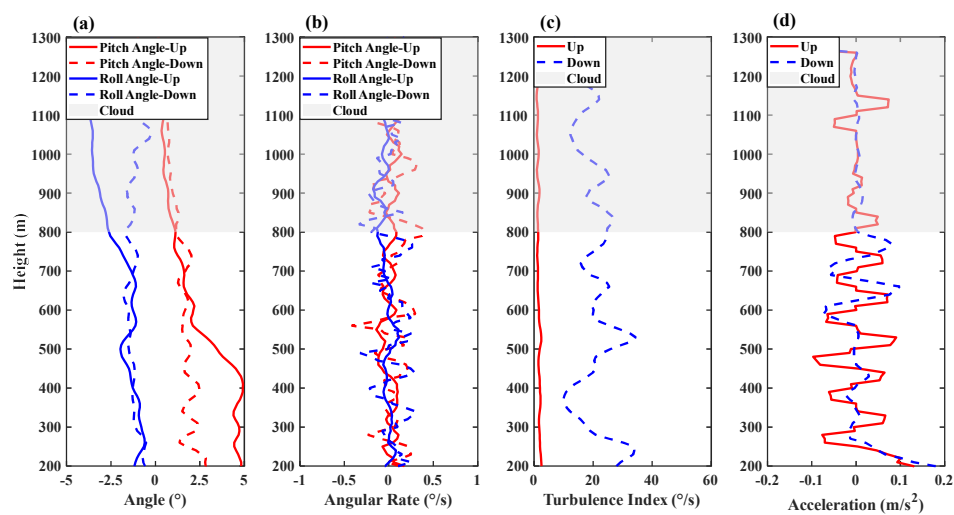
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707 **Figure 10.** Same as Figure 8, but for the period of 19:43–19:55 BJT on July 31, 2025.

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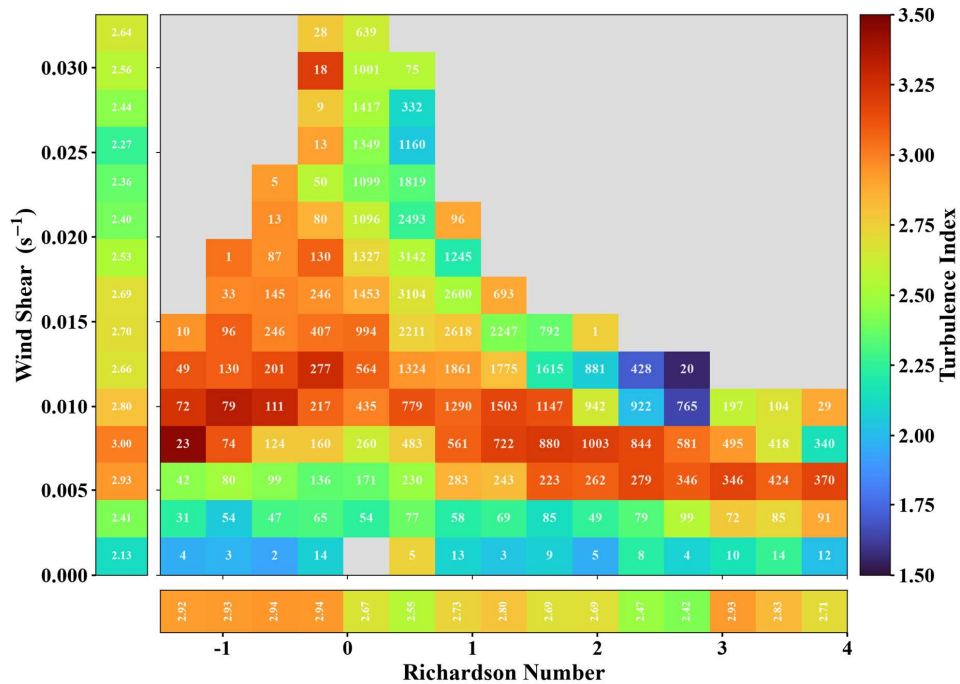
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711 **Figure 11.** Same as Figure 9, but for the period of 19:43–19:55 BJT on July 31, 2025.

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714

715 **Figure 12.** Joint distribution of the gradient Richardson number (Ri) and vertical wind shear. The
716 horizontal axis denotes Ri ; the vertical axis represents vertical wind shear with units of s^{-1} . The
717 color bar on the right indicates the UAV-derived turbulence index (unit: $^{\circ}/s$), where higher values
718 indicating stronger atmospheric turbulent disturbances and more intensive UAV flight
719 perturbations, while lower value corresponding to quiescent atmospheric conditions with
720 negligible turbulent interference.

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