



# Sensitivity of time-lapse magnetic resonance sounding to vadose zone hydrodynamic parameters: monitoring of an intense meteorological event

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**Abstract.** Magnetic Resonance Sounding (MRS) is a geophysical method that provides direct information on subsurface water content and can complement traditional hydrological observations for model calibration. We develop a coupled hydrogeophysical framework by linking one-dimensional unsaturated flow with an MRS forward model to simulate a time-lapse MRS experiment during an infiltration event in the Strengbach headwater catchment in northeastern France. The geometry of the model is conditioned using insights on the porous medium thickness provided by seismic refraction tomography, in order to reduce model uncertainties related to the thickness of subsurface layers. We apply a Global Sensitivity Analysis (GSA) to quantify how uncertainty in hydrodynamic parameters affects MRS signals and their temporal evolution. The GSA combines variance-based Sobol indices with two other moment-based metrics (AMAE and AMAV) to characterize the sensitivity of both the mean and the variance of the MRS signal distributions. Using these complementary metrics provides a more robust assessment of parameter influence than Sobol indices alone. Our results identify the parameters which exert the strongest control on time-lapse MRS signals and reveal how their influence changes during the infiltration event. We also identify parameters whose uncertainties have insignificant contribution to MRS signals. These insensitive parameters are not expected to be precisely estimated with inverse modeling techniques based on MRS data. These insights clarify the potential and limitations of MRS data for constraining hydrological parameters in shallow mountain aquifers and demonstrate how the temporal evolution of MRS sensitivity can be exploited to optimize monitoring strategies during transient hydrological events.

## 1 Introduction

Water resources in mountainous regions are of primary importance because they supply freshwater to both local and downstream population (Viviroli et al., 2011, 2020). These regions also provide key ecosystem services that depend on water availability, including food and timber production and carbon sequestration (Grêt-Regamey and Weibel, 2020). Mountain environments are especially vulnerable to climatic and socio-economic changes (Immerzeel et al., 2019). Hydrological modeling is a fundamental tool for predicting the effects of climate change on the water resource in these sensitive systems and for supporting sustainable resource management (Haro-Montegudo et al., 2020; Moraga et al., 2021).



Accurate model parameterization is essential to reduce uncertainty in hydrological predictions. Calibrating hydrological models based on stream discharge solely introduces equifinality issues: several model parametrization resulting in a good fit of the observed data (Ebel and Loague, 2006). Additional constraints can be brought by point-scale observations such as piezometric data. However, in mountainous regions, access difficulties and steep slopes make borehole drilling challenging or impossible. Furthermore, headwater catchments exhibit strong heterogeneities in subsurface hydraulic properties and layer geometry (Benton et al., 2022; Lesparre et al., 2020), which limit the spatial representativity of point-scale measurements. Near surface geophysical methods are valuable in this context because they provide relatively low-cost, non-destructive and distributed additional information on subsurface properties and flow processes (Binley et al., 2015). A wide range of techniques are used to characterize subsurface heterogeneity, including Electrical Resistivity Tomography (ERT, Pleasants et al. (2022)), Seismic Refraction Tomography (SRT, Pasquet et al. (2022)), Ground Penetrating Radar (GPR, Zhang et al. (2022)), microgravimetry (Chaffaut et al., 2022), Magnetic Resonance Sounding (MRS, Legchenko et al. (2020)).

This study focuses on MRS. One of the major advantages of this geophysical method is its direct sensitivity to the water content distribution in the subsurface (Legchenko and Valla, 2002). Most geophysical methods (e.g. ERT and GPR) rely on petrophysical laws to infer the hydrologic properties from measured geophysical variables. MRS data are not burdened by the modeling errors related to these petrophysical models, and they can be directly interpreted in terms of hydrological behavior of the studied object. The vertical measurement footprint of MRS data reaches depths several tens of meters, compared to a few meters for GPR (Legchenko et al., 2018). Time-lapse MRS has been successfully applied to study the dynamics of the subsurface water content (Legchenko et al., 2020, 2022; Mazzilli et al., 2020). Geophysical data can be used in a coupled hydrogeophysical approach to infer the subsurface hydrodynamic parameters (Costabel and Günther, 2014; Lesparre et al., 2020; Moua et al., 2023). While Costabel and Günther (2014) inferred hydrologic parameters from static MRS observations of the capillary fringe in homogeneous sands, recent studies have expanded MRS applications to dynamic or layered systems. For instance, Legchenko et al. (2020) utilized time-lapse MRS measurements for parameter estimation, and Lesparre et al. (2020) characterized aquifer layer thickness and porosity from spatially distributed MRS data. Because a comprehensive analysis and discussion of how MRS signals respond to hydrodynamic parameters is still lacking in these approaches, this study provides a Global Sensitivity Analysis (GSA) of time-lapse MRS signals to bridge this gap and advance hydrogeophysical modeling.

One of the crucial steps in the calibration process of a numerical model is sensitivity analysis. GSA quantifies the effects of the uncertainties in the model parameters, considered as random variables, on the outputs of the model (Saltelli et al., 2007). For the purpose of conciseness and readability, we will describe the effects of the uncertainties in the parameters as the effects of the parameters in the following. GSA is a crucial step in the calibration process because it allows a deep understanding of the studied model (Ferretti et al., 2016; Razavi et al., 2021) and the identification of parameters with little to no influence on the outputs of interest. Those parameters are not expected to be identifiable by observations of the outputs (Wu et al., 2019). Thus, the non-sensitive parameters can be set to experimentally measured or literature-based reference values in order to reduce the parameter space dimension for the parameter estimation procedure (Dell'Oca et al., 2025). GSA is also well suited for dynamic systems, such as those analyzed through time-lapse experiments, where the influence of parameters may vary over time (Maina and Guadagnini, 2018; Younes et al., 2018). It has been widely applied to hydrological models (Song et al., 2015). It was



notably applied to hydrogeophysical models, coupling subsurface flow models and near surface geophysical methods such as GPR (Moua et al., 2023) or gravimetry (Maina and Guadagnini, 2018). Recent studies outlined the limitations of using solely variance-based GSA such as the classical analysis of Sobol indices (Dell’Oca et al., 2017). It is therefore interesting to base the GSA on complementary features of the model outputs probability density function (pdf) such as the mean or higher order statistical moments (Dell’Oca et al., 2025; Maina and Guadagnini, 2018).

We developed a hydrogeophysical model based on Richards 1D water flow equation (Richards, 1931) and the fundamental equations of MRS (Legchenko and Valla, 2002). We define a numerical time-lapse MRS experiment based on real meteorological and hydrological data collected during a meteorological event in the Strengbach headwater catchment (Pierret et al., 2018). This numerical experiment allows us to simulate several acquisition parametrization at a single moment and high acquisition frequencies which are unreachable in realistic field conditions. We address two main questions: (1) Which parameters exert the greatest influence and how does this influence evolve during a significant meteorological event ? (2) Which hydrodynamic parameters have a negligible influence on the MRS signals ? The information gathered by answering these questions is useful for a better use of MRS signals in hydrogeophysical inverse problems and for future experimental design. Taking into account the limitations of variance-based only GSA exposed by the authors of Dell’Oca et al. (2017), we conduct the GSA of our model through Sobol indices (Sobol, 2001), and also through the AMAE and AMAV indices (Dell’Oca et al., 2017): sensitivity indices based on the mean and the variance of the outputs of the model, respectively. Section 2 describes the studied site. Section 3 presents the methodological background, including the subsurface flow model and the MRS method. Section 4 details the GSA methodology. Results are presented in Sect. 5 and discussed in Sect. 6. Finally, Sect. 7 summarizes the main conclusions of this study.

## 2 Studied site

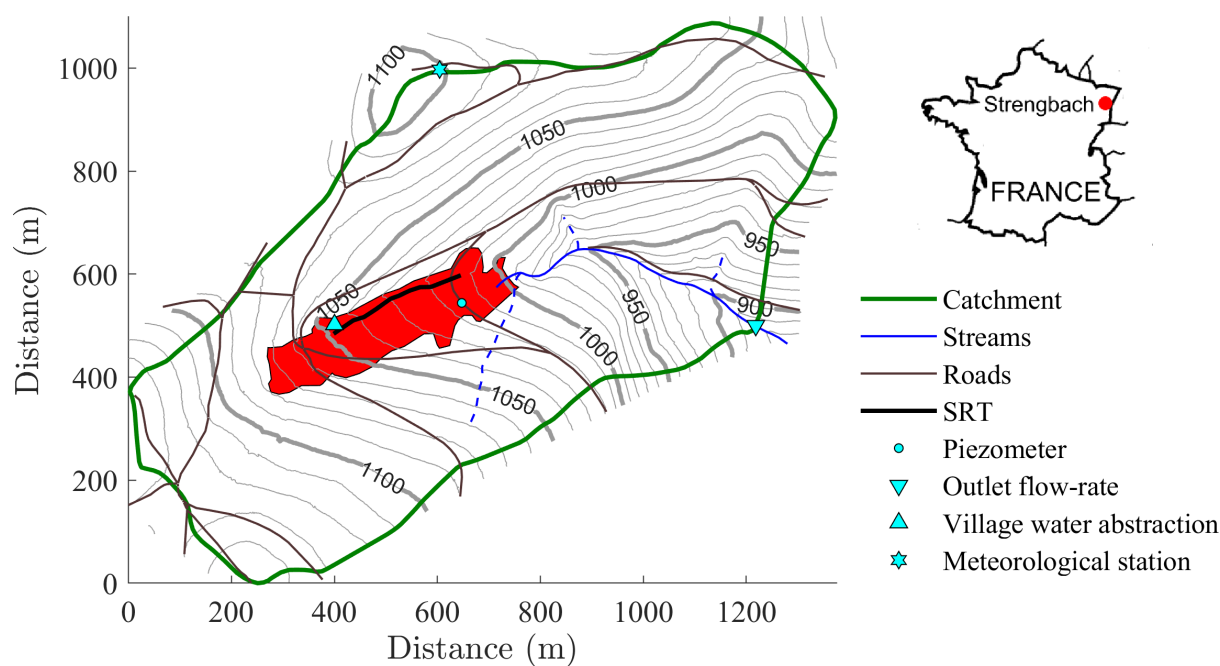
The numerical experiment we present in this study was designed using data collected on the Strengbach headwater catchment in order to base the test case on realistic mountainous watershed conditions. The Strengbach catchment is located in the Vosges mountains in northeastern France (Fig. 1). It is the experimental site of the Observatoire Hydro-Géochimique de l’Environnement (OHGE, <https://ohge.unistra.fr/>) which is part of the French critical zone observatories network (OZCAR, <https://www.ozcar-ri.org>). The OHGE has been collecting hydrological, geochemical and meteorological data on the catchment since 1986 to explore several environmental questions such as the impact of acid rains on forests or the water resources in a mid-mountainous context (Pierret et al., 2018). Such long term observations allowed the assessment of the effects of local climate change on the hydrological cycle of the catchment (Strohmeinger et al., 2022) and the projection of future effects of climate change on both the water cycle and the vegetation cover (Beaulieu et al., 2016).

The Strengbach is a small forested catchment covering an area of 0.8 km<sup>2</sup>, with an altitude ranging between 880 and 1150 m a.s.l. The bedrock is mainly composed of fractured granite. The lithology of the catchment also shows outcrops of microgranite and gneiss bodies along the southern and northern slopes (Pierret et al., 2018). We describe the subsurface compartments as follows: above the bedrock is a granitic saprolite above which lies a soil layer. Soils are very coarsely grained,



sandy and rich in gravel (Fichter et al., 1998). The layers' thicknesses show strong heterogeneities at the catchment scale. A recent study used SRT to infer the depths of the boundaries between soil, saprolite, and bedrock layers from compression P-wave velocities (Lesparre et al., 2024). Saprolite thickness varies from  $4 \pm 1$  m to  $12 \pm 1.4$  m and soil thickness from  $1.4 \pm 0.5$  m to  $3.4 \pm 1.1$  m. Local climatic conditions are temperate oceanic mountainous, with a mean precipitation of  $1380 \text{ mm.yr}^{-1}$ , and a mean annual temperature of  $6^\circ\text{C}$  in the period 1986 to 2015. During that same period, mean potential evapotranspiration was of  $571 \text{ mm.yr}^{-1}$ , with values ranging between 516 and  $729 \text{ mm.yr}^{-1}$ , and the mean discharge at the stream outlet was about  $750 \text{ mm.yr}^{-1}$ , with variations ranging from 494 to  $1132 \text{ mm.yr}^{-1}$  (Pierret et al., 2018).

We focus on a relatively flat zone above the main spring of the Strengbach catchment (Fig. 1), where the subsurface below the soil consists of colluvium (Pierret et al., 2018). This area features the catchment's thickest saprolite ( $\approx 13$  m, Lesparre et al. (2024)), forming a thick weathered zone that hosts a shallow unconfined aquifer well-suited for 1D hydrological modeling. Indeed, the moderate slope, the relatively high soil permeability, the water-table depth, and the observed dynamics are all consistent with the vertical infiltration assumed in such 1-D models. Previous research underscores the hydrological significance of this zone. For instance, MRS mapping identified it as having the highest subsurface water content in the entire catchment (Boucher et al., 2015), while time-lapse micro-gravimetry revealed intense localized water dynamics (Chaffaut et al., 2022). Furthermore, numerical experiments by Lesparre et al. (2020) showed that this zone is particularly well-suited for time-lapse MRS monitoring due to the high expected magnitude of signal variations.



**Figure 1.** Map of the Strengbach headwater catchment, northeastern France. The studied area is highlighted in red.



### 3 Background

#### 3.1 1D subsurface flow model

We model the one-dimensional subsurface flow using the so-called "mixed" form of Richards' equation (Gilding, 1991):

$$110 \quad \frac{\partial \theta}{\partial t} - \frac{\partial}{\partial z} \left[ K(h) \left( \frac{\partial h}{\partial z} - 1 \right) \right] = f, \quad (1)$$

where  $\theta$  ( $\text{m}^3 \cdot \text{m}^{-3}$ ) is the water content,  $t$  (s) is the time,  $z$  (m) is the depth, positive downwards,  $K$  ( $\text{m} \cdot \text{s}^{-1}$ ) is the hydraulic conductivity of the medium,  $h$  (m) is the pressure head, and  $f$  ( $\text{m}^3 \cdot \text{m}^{-3} \cdot \text{s}^{-1}$ ) is a source/sink term. Along with Richards' equation, the hydrologic model uses Van Genuchten's (VG) model to define the pressure-water content relationship (Van Genuchten, 1980) and Mualem's model for the pressure-hydraulic conductivity relationship (Mualem, 1976). Those models write:

$$115 \quad \theta(h) = \begin{cases} \theta_r + (\theta_s - \theta_r)(1 + |\alpha h|^n)^{-m} & \text{if } h < 0, \\ \theta_s & \text{if } h \geq 0, \end{cases} \quad (2)$$

$$K(S_e(h)) = \begin{cases} K_s S_e(h)^L \left[ 1 - \left( 1 - S_e(h)^{\frac{1}{m}} \right)^m \right]^2 & \text{if } h < 0, \\ K_s & \text{if } h \geq 0, \end{cases} \quad (3)$$

where  $\theta_r$  ( $\text{m}^3 \cdot \text{m}^{-3}$ ) is the residual water content,  $\theta_s$  ( $\text{m}^3 \cdot \text{m}^{-3}$ ) is the saturated water content,  $\alpha$  ( $\text{m}^{-1}$ ) is a parameter related to the mean pore size,  $n$  (-) is the pore distribution index,  $m$  is a parameter defined as  $m = 1 - 1/n$ ,  $K_s$  ( $\text{m} \cdot \text{s}^{-1}$ ) is the saturated hydraulic conductivity,  $S_e$  (-) is the effective saturation:

$$120 \quad S_e(h) = \frac{\theta(h) - \theta_r}{\theta_s - \theta_r}, \quad (4)$$

and  $L$  (-) is a parameter related to the tortuosity, set here to 0.5.

In order to solve the temporal evolution of the water content with this model, one needs to define the initial state of the system (the pressure head distribution  $h(z, t = 0 \text{ s})$ ) and boundary conditions. We use two types of boundary conditions: Dirichlet (imposed pressure head) at the bottom of the subsurface column and Neumann (imposed flux) at the surface. The numerical  
125 solution of Richard's equation is computed with Phydus (Collenteur et al., 2020), a python library based on HYDRUS-1D finite element flow equation solver (Šimůnek et al., 2008).

The hydrologic model boundary conditions (BCs) are constrained by meteorological and hydrological data measured on the Strengbach catchment. The lower BC is a time-variable pressure condition. The water table depth  $z_{table}$  (m) is measured hourly in a piezometer within the studied area (Fig. 2d). The water table depth value is always under 7 m. Therefore, we set  
130 the maximum depth of the zone where unsaturated water flow equations are solved to  $z_{max} = 7 \text{ m}$ . Piezometric measurements give local information and we are studying a relatively large area (Fig. 1). Therefore, we introduce the parameter  $\Delta h_{piezo}$  (m)



in the GSA to take into account uncertainties on  $z_{table}$ . This parameter is considered as a random variable and we analyze its effects on MRS output signals along with hydrodynamic parameters. The pressure at the bottom of the soil column is  $h(z = z_{max}, t) = z_{max} - z_{table}(t) + \Delta h_{piezo}$ . The upper BC is modeled from precipitations and meteorological data measured at the summit weather station of the catchment. The time variable upper flux BC  $Q_{top}(t)$  ( $\text{mm}\cdot\text{s}^{-1}$ , cumulated to a daily time-step in Fig. 2c) is obtained by taking into account several surface processes:

$$Q_{top}(t) = R(t) + Q_s(t) - E(t) - Tr(t) - R_s(t), \quad (5)$$

where  $R$  is the flux due to rain infiltration,  $Q_s$  is the snowmelt infiltration flux,  $E$  is the soil evaporative flux,  $Tr$  is the transpiration flux, and  $R_s$  is the surface runoff, all fluxes in  $\text{mm}\cdot\text{s}^{-1}$ . The Strengbach catchment exhibits a strong drainage capacity and surface runoff is negligible. Thus, within the scope of this study, we set  $R_s(t) = 0 \text{ mm}\cdot\text{s}^{-1}$ , for all  $t$ .

The first two terms (i.e.  $R$  and  $Q_s$ ) depend on effective precipitation: the portion of precipitations that reaches the ground. They require to model precipitations interception by the vegetation cover and to subtract it from measured precipitations. The evapotranspiration components (i.e.,  $E$  and  $Tr$ ), which correspond to Actual Evapotranspiration (AET) in Eq. (5), are in fact estimated based on the Potential Evapotranspiration (PET), the available water content and the vegetation state. The computation of PET is based on the Penman model. For details on the PET computation procedure, see Belfort et al. (2025) and references therein. Whereas PET is computed only from meteorological variables, AET takes into account the availability of water in the root system zone and vegetation parameters. AET and interception are computed using a reservoir based model which takes into account several ecophysiological processes in order to compute AET from PET (for details on the computation of interception and AET, see Granier et al. (1999) and references therein). Interception and AET are computed with a daily time step (Fig. 2a) and interpolated to the hourly time step (based on the timing of the precipitations and the length of the day respectively) for hydrological simulation. Interception is deducted from raw precipitation in order to get effective precipitation (Fig. 2b). A temperature-based snowpack model is used to implement the precipitation infiltration delay due to the accumulation of a snow layer on the ground surface. The snowpack model was adapted from the Hydrologiska Byråns Vattenbalansavdelning (HBV - Hydrological Bureau Water Balance Department) hydrological model (Lindström et al., 1997). The effective precipitation phase (snow, rain or mixed phases) depends on the measured temperature. We define two threshold temperatures for this purpose:  $T_{min}$  ( $^{\circ}\text{C}$ ) the temperature below which all precipitations are in solid phase, and  $T_{max}$  ( $^{\circ}\text{C}$ ) the temperature above which all precipitations are in liquid phase. For temperatures between  $T_{min}$  and  $T_{max}$ , the fraction of solid precipitations varies linearly between 1 and 0. We consider  $T_{min} = -3^{\circ}\text{C}$  and  $T_{max} = 1^{\circ}\text{C}$ . The liquid precipitations directly infiltrate the soil and the solid precipitations accumulate in a snowpack and melt generating the snowmelt infiltration flux  $Q_s$ .

The mean temperature of the snowpack  $T_s$  ( $^{\circ}\text{C}$ ) is computed as follows:

$$T_s(t) = k_1 T_s(t - \Delta t) + (1 - k_1) T(t), \quad (6)$$

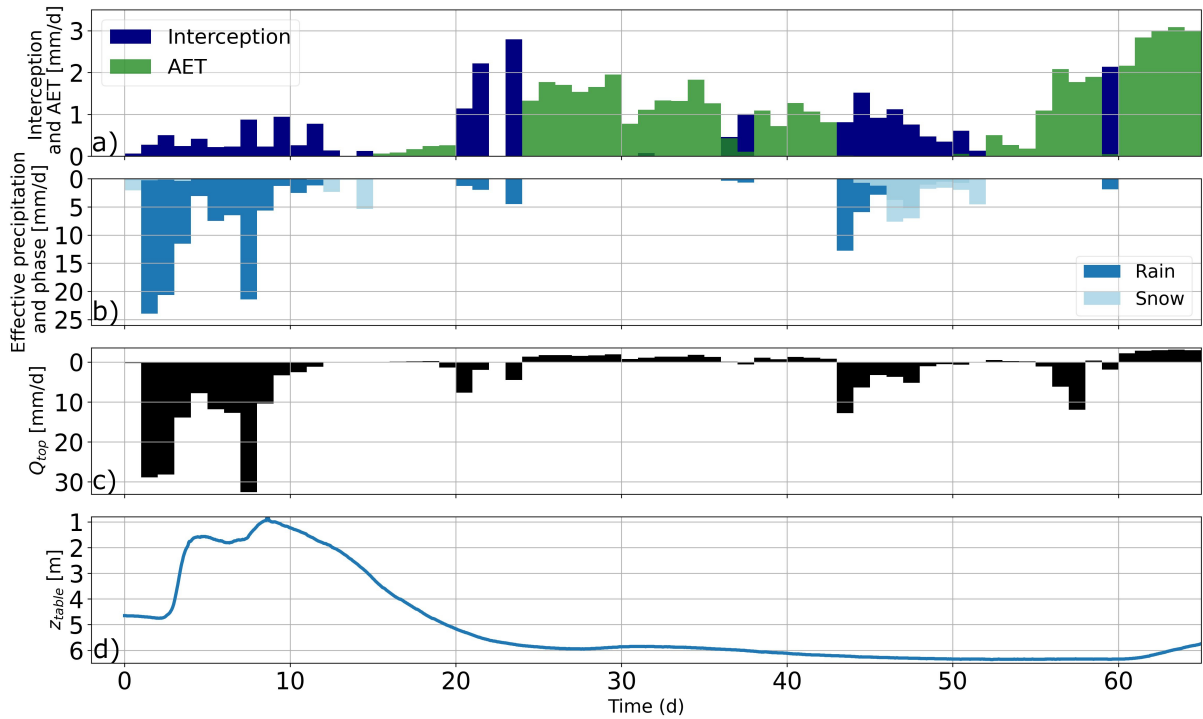
where  $k_1$  (-) is a user defined weighting factor,  $\Delta t$  (s) is the time step and  $T$  ( $^{\circ}\text{C}$ ) is the air temperature. We set  $k_1 = 0.3$  (Lindström et al., 1997) and the time step  $\Delta t$  corresponds to the weather variables measurement time step: 3600 s. The



165 accumulated snowpack melts under two conditions: (1) the air temperature is higher than 0°C, and (2)  $T_s = 0$  °C. If these two conditions are met, the snowmelt flux is computed as follows:

$$Q_s(t) = k_2 T(t), \tag{7}$$

where  $k_2$  ( $\text{mm}\cdot\text{s}^{-1}\cdot\text{°C}^{-1}$ ) is the degree-day factor parameter, set to  $0.1 \text{ mm}\cdot\text{s}^{-1}\cdot\text{°C}^{-1}$  in this study (Lindström et al., 1997).



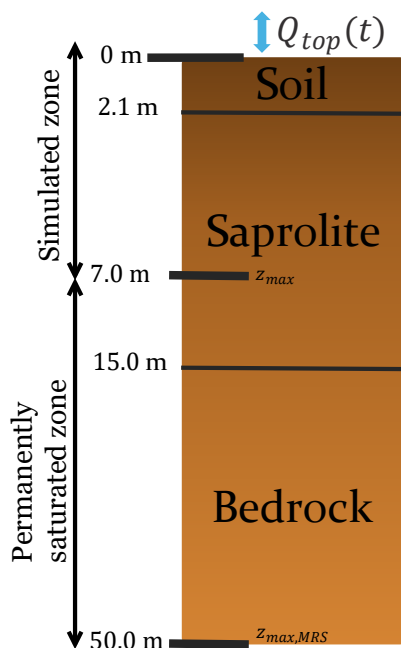
**Figure 2.** Time series of the hydrological and meteorological data constraining the model boundary conditions: a) interception and AET, b) effective precipitation, c) surface flux  $Q_{top}$ , and d) water table depth  $z_{table}$  measured in a piezometer within the studied area.

We set our study in winter 2021, since an intense meteorological event occurred this year. We observed an intense rise in the water table level measured in the piezometer at the end of January and early February (Fig. 2d). Such a fast and important saturation of the medium can be particularly interesting to understand the saturation/unsaturation behavior of the shallow aquifer we study. This extreme hydrological event is due to two main drivers. Firstly, a strong and long-lasting rain event: effective precipitations were higher than  $20 \text{ mm}\cdot\text{d}^{-1}$  at most and reached 107 mm cumulated over a period of 12 days. Secondly, it is due to the accumulation of a snow cover before the rain event: the measured snowpack height reached 0.8 m. A rise in the temperature and the rain event triggered the melt of this snow cover. We notice this coupled effect by comparing Fig. 2b and Fig. 2c: during the period from day one to day 12 (day zero is set to the 26<sup>th</sup> of January 2021), the modeled infiltration flux is larger than the effective precipitation. Prior to the accumulation of this snow cover, the weather was dry. In this context, we simulated MRS measurements every 24 hours during a time period of 66 days in order to analyze both the short term



and mid-term effects of the meteorological event on the sensitivity of MRS signals to hydrodynamic parameters. We consider a model warm-up period starting on the first of November 2020 in order not to define arbitrarily the initial condition of the simulation.

We set the boundaries between underground compartments (soil, saprolite, bedrock) using prior information obtained by SRT. The whole catchment was investigated in 2018 and 2019 with SRT (Lesparre et al., 2024). One of the SRT profiles is located within the area we examine in this study (Fig. 1). We use the boundaries' depths inferred in Lesparre et al. (2024) for this SRT profile:  $z_{Soil/Sapro} = 2.1 \text{ m}$ ,  $z_{Sapro/Bedrock} = 15 \text{ m}$  (Fig. 3). Subsurface material is expected to be highly altered close to the surface and less and less altered towards the bedrock. Still, there might be a non-negligible water content in the saturated zone below  $z_{max}$ . Thus, we introduce a permanently saturated zone where the water content is constant:  $\forall z > z_{max} \theta(z) = \theta_s(z)$ . This zone ranges from depth  $z_{max} = 7 \text{ m}$  to  $z_{max,MRS} = 50 \text{ m}$ . We set the maximum depth of the subsurface column to 50 m as the granitic bedrock is altered and fractured down to depths of several tens of meters (Lajaunie et al., 2023) and to consider fully the region investigated by MRS measurements.



**Figure 3.** Schematic representation of the subsurface model. The underground porous medium is divided in three layers, from surface to depth: the soil, the saprolite and the bedrock. The hydrogeophysical model considers two compartments: a simulated zone where the unsaturated water flow equations are solved numerically and a permanently saturated zone where  $\theta(z) = \theta_s(z)$ .

### 190 3.2 MRS method and modeling

MRS uses the magnetic properties of the protons in hydrogen atoms composing the subsurface water molecules. Under natural conditions, the macroscopic magnetization vectors of the protons align with Earth's magnetic field (Legchenko and Valla,



2002). The generation of an alternating electrical current in a wire loop placed on the ground induces a perturbing electromagnetic field that tilts the protons' magnetization vectors away from their equilibrium state. The product of the injected current intensity and the emission duration is defined as the electromagnetic pulse  $q$  (A.ms). Both the pulse and the geometry of the loop control the investigated depth of the MRS sounding: larger loops and stronger electromagnetic pulses result in deeper investigation. The frequency of the electromagnetic field is set to Larmor frequency, which is the precessional frequency of hydrogen protons. The perturbing electromagnetic field is then shut down, and the protons relax back to their equilibrium state. The oscillations of the magnetization vectors around Earth's magnetic field at Larmor frequency during relaxation generates an electromagnetic field. This field induces in turn an electrical current in the wire loop. The voltage measured in the loop is proportional to the subsurface water content (Legchenko and Valla, 2002).

The envelope of the signal measured in the loop is multi-exponentially decaying (Hertrich et al., 2005):

$$E(t, q) = \int_z \int_{T_2^*} \kappa(q, z) \theta_{MRS}(z, T_2^*) e^{-\frac{t}{T_2^*(z)}} dT_2^* dz, \quad (8)$$

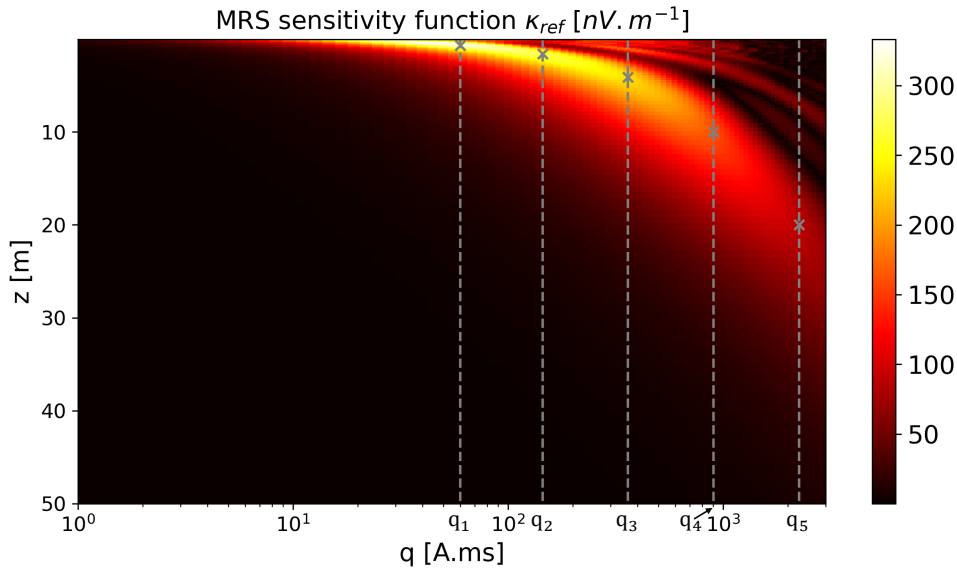
where  $\kappa(q, z)$  ( $\text{nV} \cdot \text{m}^{-1}$ ) is the sensitivity function,  $\theta_{MRS}(-)$  is the water content which can be detected by MRS,  $T_2^*$  (s) is the exponential relaxation characteristic time. Assuming a mono-exponential behavior and evaluating Eq. (8) at time  $t = 0$  s leads to the following equation:

$$E_0(q) = \int_z \kappa(q, z) \theta_{MRS}(z) dz. \quad (9)$$

This study focuses on the sensitivity of  $E_0(q)$  to hydrodynamic parameters. The sensitivity function  $\kappa$  depends on several parameters: the geometry of the loop, the electrical resistivity of the subsurface, and the local geomagnetic field. We consider an eight-shaped loop made of two squares meeting at a common corner, each with a side length of 40 m. This loop layout was used on previous MRS investigations of the catchment (Boucher et al., 2015). The considered loop is located on a single pedological unit (the colluvium zone, highlighted in red in Fig. 1). Therefore, we assume that the scale of lateral heterogeneities in subsurface properties is larger than the MRS measurement footprint. Thus, the coupled 1D hydrogeophysical model is consistent with the studied field properties. For the purpose of this study, a reference sensitivity function  $\kappa_{ref}$  (Fig. 4) is computed with the software Samovar (Legchenko and Shushakov, 1998) using the above-mentioned parameters, as well as a maximum depth (i.e.  $z_{max, MRS}$ ), and boundaries for the pulse interval. Then, the reference sensitivity function  $\kappa_{ref}$  is interpolated to correspond to the spatial discretization of the hydrologic model and the experimental pulse values. The water content profiles  $\theta(z)$  computed with the hydrological model described in Sect. 3.1 are used to compute MRS signals with a numerical integration of the integral in Eq. (9). The numerical experiment introduced in this work aims to analyze the sensitivity of the system's response to variations in hydrodynamic parameters across five distinct pulse values. This representative subset was selected to ensure a thorough GSA while maintaining computational efficiency. The electromagnetic pulse values are spaced evenly on a logarithmic scale on the interval  $[60, 2260]$  A.ms:  $(q_1, q_2, q_3, q_4, q_5) = (60, 145, 362, 904, 2260)$  A.ms. This



logarithmic pulse moment spacing is typical for MRS acquisition sequences. The pulse values control the depth of investigation through the MRS sensitivity function  $\kappa$  (Fig. 4). The depths of maximum sensitivity  $z_{s,max}(q_i)$  ( $i \in \{1, \dots, 5\}$ ) are  $z_{s,max}(q_1) =$   
 225  $0.7 \text{ m}$ ,  $z_{s,max}(q_2) = 1.6 \text{ m}$ ,  $z_{s,max}(q_3) = 4.1 \text{ m}$ ,  $z_{s,max}(q_4) = 10.0 \text{ m}$ ,  $z_{s,max}(q_5) = 20.0 \text{ m}$ . These depths are represented with crosses in Fig. 4.



**Figure 4.** Reference MRS sensitivity function  $\kappa_{ref}(q, z)$  computed with Samovar (Legchenko and Shushakov, 1998). Vertical dashed lines represent the simulated pulse moments, crosses are placed at the depths of maximal sensitivity for each pulse.

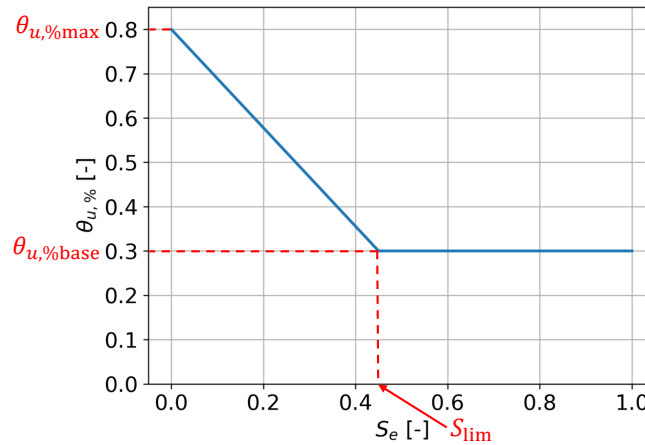
The subscript *MRS* is added to the water content variable in Eq. (8) and Eq. (9) because the MRS method is not sensitive to the entire water content in the subsurface (Lubczynski and Roy, 2003; Boucher et al., 2011). The MRS measurement devices have an instrumental dead time: the time needed to switch the device from emitting to receiving mode. This instrumental dead time is fixed at  $3.10^{-2} \text{ s}$  for the device considered in this study: NUMISplus (IRIS instruments). The water with a relaxation time  $T_2^*$  shorter than - or very close to - the instrumental dead time cannot be detected by this MRS equipment. Several physical and hydrological properties have an influence on the relaxation time. Boucher et al. (2011) carried out a laboratory experiment in order to quantify the effects of (1) grain size distribution, (2) clay content, and (3) saturation degree on the fraction of MRS undetectable water content (denoted as  $\theta_{u\%}$ , i.e.  $\theta_{MRS} = \theta \times (1 - \theta_{u\%})$ ). They showed that  $\theta_{u\%}$  is firstly sensitive to saturation: in the driest samples,  $\theta_{u\%} \approx 50 - 60\%$ , depending on grain size distributions. When the saturation increases,  $\theta_{u\%}$  decreases. Then a saturation threshold around 40% is reached, and the value of  $\theta_{u\%}$  is minimal ( $\approx 10 - 20\%$ ). For saturations above this threshold,  $\theta_{u\%}$  remains almost constant. This behavior is reproduced in Fig. 5. The strong control of saturation over the relaxation time, and thus on MRS undetectable water content, is due to increased interactions between water molecules and the solid grains under low saturation. The effects of grain size distributions and clay contents were measured on saturated samples.  $\theta_{u\%}$  is the smallest for the largest grain size; it increases as the median grain size decreases. It reaches a maximum of 16%  
 230  
 240



for a median grain size around 0.1 mm and decreases for smaller grains. Concerning the effects of clay content, we consider the results for the samples with a clay content below 20% as it corresponds to measured soil granulometry in the Strengbach catchment (Belfort et al., 2018; Oursin et al., 2023; Belfort et al., 2025). In these samples, the higher the clay content is, the higher  $\theta_{u\%}$  is. This increase is stronger for coarser grains. Considering the combined effects of grain size distribution, clay content, and saturation degree in our hydrogeophysical model, we implement MRS water content as follows:

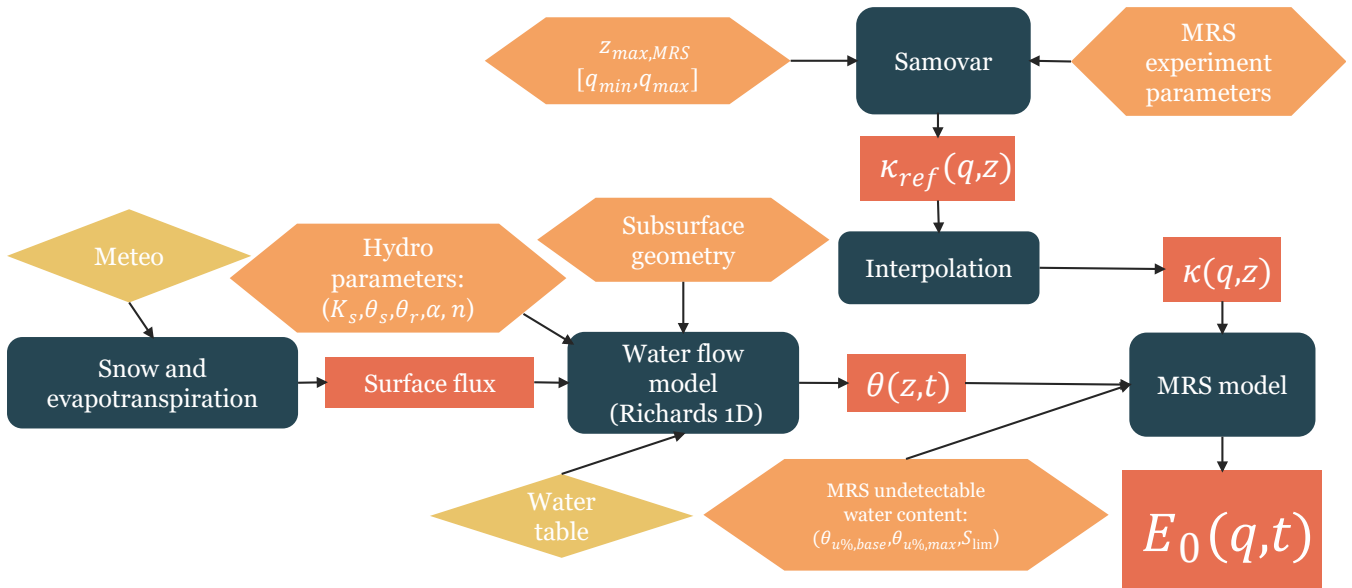
$$\theta_{MRS}(z) = \theta(z) \times (1 - \theta_{u\%}(S_e(z), \theta_{u\%,base}, \theta_{u\%,max}, S_{lim})), \quad (10)$$

with  $\theta_{u\%} \in [0, 1]$ . We implement  $\theta_{u\%}$  as a function of effective saturation  $S_e(z)$ . The properties of this function are characterized by 3 parameters:  $\theta_{u\%,max}$  the limit MRS undetectable water content (when  $S_e \rightarrow 0$ ),  $S_{lim}$  the threshold saturation above which MRS undetectable water content is constant, and  $\theta_{u\%,base}$  the constant MRS undetectable water fraction for saturations higher than  $S_{lim}$  (Fig. 5).



**Figure 5.** MRS undetectable water content:  $\theta_{u\%}(S_e(z), \theta_{u\%,max}, S_{lim}, \theta_{u\%,base})$ .

In this model, the effects of clay contents are taken into account by shifting the  $\theta_{u\%,base}$  value (higher clay contents yield higher  $\theta_{u\%,base}$ ). The effects of grain size distributions are modeled through both  $S_{lim}$  and  $\theta_{u\%,base}$  (finer grains lead to lower  $S_{lim}$  values and the effects of the clay content are increased for coarse grains). To sum up the information presented in this section, we designed a flowchart of the hydrogeophysical model (Fig. 6).



**Figure 6.** Flowchart of Phydus-MRS hydrogeophysical modeling framework. Yellow diamond shaped boxes represent field data. Orange hexagons represent user defined parameters. Models and mathematical processings are shown as blue rectangles with rounded corners. Red rectangles represent the results of numerical models.

## 255 4 Global sensitivity analysis

### 4.1 Moment-based sensitivity indices

To perform a GSA of the MRS signals  $E_0$  to variations of the hydrodynamic parameters, we used the moment-based sensitivity indices defined by Dell’Oca et al. (2017), for the first two statistical moments: AMAE and AMAV. We also used the classical variance-based sensitivity indices: Sobol indices (Sobol, 2001).

#### 260 4.1.1 AMAE and AMAV indices

Let  $y = f(\xi)$  be a mathematical model which input is a set of  $M$  independent random variables:  $\xi = \{\xi_1, \xi_2, \dots, \xi_M\}$ . The AMA index associated with the first statistical moment (i.e. the mean), AMAE, quantifies the expected relative variation of the mean of  $y$  due to variations in  $\xi_i$  (Dell’Oca et al., 2017). For the second statistical moment (i.e. the variance), the AMAV index



quantifies the expected relative discrepancy between unconditional and conditional variance. The former is defined as:

$$265 \quad AMAE_{\xi_i} = \begin{cases} \frac{E[|y_0 - E[y|\xi_i]|]}{|y_0|} & y_0 \neq 0, \\ E[|E[y|\xi_i]|] & y_0 = 0, \end{cases} \quad (11)$$

where  $E[\cdot|\cdot]$  is the conditional expectation operator and  $y_0$  is the unconditional expected value of  $y$ , and the latter is defined as:

$$AMAV_{\xi_i} = \frac{E[|V[y] - V[y|\xi_i]|]}{V[y]}, \quad (12)$$

where  $V[\cdot|\cdot]$  is the conditional variance operator. These indices provide information that complements classical variance-  
 270 based sensitivity measures. Using multiple sensitivity metrics makes our GSA approach more robust, as it does not rely on  
 the assumption that the total influence of the hydrodynamic parameters can be fully captured through output variance alone.  
 Furthermore, Dell’Oca et al. (2017) demonstrated that a given parameter may have a negligible Sobol index and still have  
 an impact on the model output variance, quantified by the AMAV index. AMA-based GSA has been applied across diverse  
 contexts, including hydrogeophysics (gravimetry, Maina and Guadagnini (2018)), risk assessment related to pesticide pollution  
 275 (Tang et al., 2021), and land-surface modeling (Dell’Oca et al., 2025).

#### 4.1.2 Sobol indices

Sobol (2001) shows that under the assumption that  $f$  is square-integrable, it can be uniquely decomposed in the following  
 manner:

$$f(\xi) = y_0 + \sum_{i=1}^M f_i(\xi_i) + \sum_{j>i}^M f_{i,j}(\xi_i, \xi_j) + \dots + f_{1\dots M}(\xi_1, \dots, \xi_M), \quad (13)$$

280 where  $f_{i_1, \dots, i_s}$  are centered orthogonal functions ( $i_1, \dots, i_s \subseteq \{1, \dots, M\}$ ). This decomposition is called ANOVA, for ANalysis  
 Of VAriance (Archer et al., 1997), because by squaring it and taking the mathematical expectation, one obtains a decomposition  
 of the variance of  $f(\xi)$ :

$$V = \sum_{i=1}^M V_i + \sum_{j>i}^M V_{i,j} + \dots + V_{1\dots M}, \quad (14)$$

where  $V = \text{var}[f(\xi)]$  is the total variance of  $f$ , and  $V_{i_1, \dots, i_s} = \text{var}[f_{i_1, \dots, i_s}]$  are the partial variances. Thanks to this decompo-  
 285 sition, Sobol (2001) defines sensitivity indices, which measure the contribution of a model parameter to the output variance.  
 The first Sobol index associated with the parameter  $\xi_i$  is:

$$S_{1,i} = \frac{\text{var}\{E[f(\xi)|\xi_i]\}}{\text{var}[f(\xi)]} = \frac{V_i}{V}. \quad (15)$$



Higher-order Sobol indices quantify the variance contributions of interactions among parameters:

$$S_{i_1, \dots, i_s} = \frac{V_{i_1, \dots, i_s}}{V}. \quad (16)$$

290 In this study, we compute and analyze the first and second order Sobol indices for the hydrodynamic parameters. Along with the AMA indices, these indices provide insights on the identifiability of  $\xi$  with observations of  $f$ . If a given parameter  $\xi_i$  has a negligible impact on the statistical moments of the function  $f$ , then observations of  $f$  will not help estimating the value of  $\xi_i$  (Wu et al., 2019). Sobol indices can be estimated with a Monte Carlo approach (Sobol, 2001). They can also be estimated with an approach based on Polynomial Chaos Expansion (PCE) (Sudret, 2008). The latter reduces the Sobol indices estimation  
295 problem to the estimation of the PCE coefficients, which is less expensive in terms of computing time than the original Monte Carlo approach.

## 4.2 Polynomial Chaos Expansion

PCE theory was originally developed by Wiener (1938). PCE is a class of surrogate models, widely used to replace process-based models in frameworks which require large numbers of model evaluations, such as GSA or Bayesian parameter inference  
300 (Sudret, 2008; Dell’Oca et al., 2017; Younes et al., 2018; Maina and Guadagnini, 2018; Rouzies et al., 2023). Under the assumption that the model function  $f$  is square integrable, it admits the following expansion (Soize and Ghanem, 2004):

$$f(\xi) = s_0 \Psi_0 + \sum_{i=1}^M s_i \Psi_1(\xi_i) + \sum_{i<j}^M s_{i,j} \Psi_2(\xi_i, \xi_j) + \sum_{i<j<k}^M s_{i,j,k} \Psi_3(\xi_i, \xi_j, \xi_k) + \dots \quad (17)$$

Let us consider the  $p^{th}$  order truncation of the series described in Eq. (17):

$$f(\xi) \approx \sum_{|\alpha| \leq p} s_\alpha \Psi_\alpha(\xi), \quad (18)$$

305 where  $|\alpha| = \sum_{i=1}^N \alpha_i$ ,  $s_\alpha$  are the polynomial coefficients, and  $\Psi_\alpha$  are the  $\alpha$ -degree polynomials of the orthogonal basis. The number of coefficients in this decomposition is

$$P + 1 = \frac{(M + p)!}{M! p!}. \quad (19)$$

The orthogonal polynomials corresponding to uniformly distributed random input parameters are Legendre polynomials (Sudret, 2008). Equation (18) is an ANOVA decomposition of  $f$ , as  $\Psi_\alpha$  are orthogonal polynomials. Therefore, once the  
310 polynomial coefficients are estimated, one has direct access to Sobol indices through the definitions introduced in the previous section. We used the UQ[py]Lab python library to build the PCE and compute Sobol indices (Lataniotis et al., 2021).



In order to train the PCE surrogate models, we sampled 3000 realizations of the random vector containing the hydrogeophysical model parameters. We used the "Leave-One-Out" Cross-Validation (LOOCV) error  $\epsilon_{LOO}$  to assess the quality of the PCE (Yates et al., 2023). LOOCV error is designed to avoid overfitting.  $N$  surrogate models  $f^{PC/i}$  are created and trained on a  
315 reduced training set  $X/x^i = \{x^j, j = 1, \dots, N, j \neq i\}$ . The cross-validation error is then computed by comparing the prediction of the model for the excluded sample  $f^{PC/i}(x_i)$  with the real value  $f(x_i)$ . LOOCV error is defined as:

$$\epsilon_{LOO} = \frac{\sum_{i=1}^N (f(x_i) - f^{PC/i}(x_i))^2}{\sum_{i=1}^N (f(x_i) - \hat{\mu}_Y)^2}, \quad (20)$$

where  $\hat{\mu}_Y = \frac{1}{N} \sum_{i=1}^N f(x_i)$  is the empirical mean of the random samples model evaluation. PCE surrogate models reproduce with high accuracy the behavior of the forward model with a global maximum cross-validation error of  $\epsilon_{LOO,max} = 1.1 \cdot 10^{-2}$ .  
320 This error reaches its maximum value for the second pulse  $q_2 = 145$  A.ms. For pulses higher than  $q_2$  the cross-validation error decreases as the pulse value increases.

### 4.3 Experimental design

We consider a total number of 18 parameters in our GSA: the hydrodynamic parameters for the two subsurface layers ( $\theta_{r,L}, \theta_{s,L}, \alpha_L, n_L, \log_{10}(K_{s,L})$ ) as well as the MRS undetectable water content function parameters  $\theta_{u\%,base,L}, S_{lim,L}$ , and  
325  $\theta_{u\%,max,L}$  ( $L \in \{\text{soil, saprolite}\}$ ), the bedrock MRS water content  $\theta_{MRS,bedrock}$ , and  $\Delta h_{piezo}$  are considered as random variables following uniform distributions. The description of the parameters, and their variability ranges are summarized in Table 1. The ranges of Mualem-Van Genuchten parameters were chosen based on plausible estimates related to the Strengbach catchment (Hammecker et al., 2004). We chose  $\log_{10}(K_s)$  (–) as the random parameter (rather than  $K_s$  (m.s<sup>-1</sup>) itself) because  $K_s$  varies by several orders of magnitude across soil types. We base the computation of Sobol indices on the coefficients of the  
330 PCE, and we produced 7000 additional simulations to compute AMAE and AMAV indices using Eq. (11) and Eq. (12).



Parameter	Description	Unit	Soil	Saprolite
$\log_{10}(K_s)$	$\log_{10}$ of saturated hydraulic conductivity	–	[–6.56, –3.38]	[–6.56, –5.38]
$\theta_r$	residual water content	–	[0.00, 0.10]	[0.00, 0.04]
$\theta_s$	saturated water content	–	[0.30, 0.50]	[0.08, 0.20]
$n$	VG parameter	–	[1.1, 3.0]	[1.1, 3.0]
$\alpha$	VG parameter	$\text{m}^{-1}$	[1.0, 15.0]	[1.0, 15.0]
$\theta_{u\%,base}$	base $\theta_{u\%}$ value	–	[0.20, 0.45]	[0.20, 0.45]
$S_{lim}$	limit saturation threshold	–	[0.40, 0.50]	[0.40, 0.50]
$\theta_{u\%,max}$	maximum $\theta_{u\%}$ value	–	[0.50, 0.70]	[0.50, 0.70]
Other Parameters				
$\Delta h_{piezo}$	piezometric uncertainty	m	[–0.20, 0.20]	
$\theta_{MRS,bedrock}$	bedrock MRS water content	–	[0.01, 0.05]	

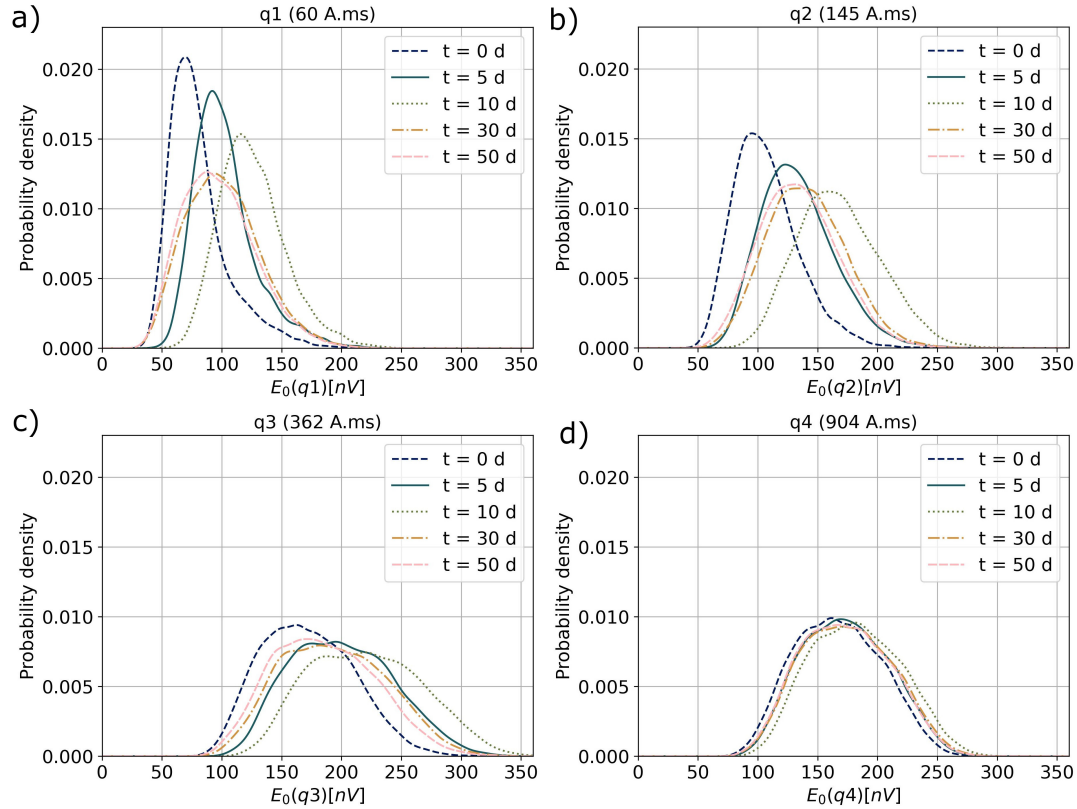
**Table 1.** Ranges of variability of the hydrogeophysical model parameters. All parameters follow uniform distributions on the intervals  $[min, max]$ .

A straightforward and global approach to assess the dataset we produced by sampling the parameter space detailed in Table 1 is to estimate and visualize the pdfs of the MRS signals  $E_0$  simulated from these samples. The pdfs are estimated with the gaussian kernel density estimator tool of the Scipy python library (Virtanen et al., 2020). We estimated these pdfs at five key moments of the period considered in the numerical experiment: the initial state ( $t = 0$  d), during the rain event and the rising phase of the water table ( $t = 5$  d), at the end of this phase ( $t = 10$  d), and at two later times ( $t = 30$  d and  $t = 50$  d) after the water table returned to its initial depth.

## 5 Results

### 5.1 $E_0$ probability density functions

We estimated the pdfs of the MRS signals at simulation times  $t \in \{0, 5, 10, 30, 50\}$  days for the five pulse values ( $E_0(q_i), i \in \{1, \dots, 5\}$ ). The signal pdfs for the fifth pulse behave similarly to those of the fourth pulse. Therefore, we only present here the results concerning the first four pulse values (Fig. 7). We show the corresponding results for  $q_5$  on Fig. S1 in the Supplement.



**Figure 7.** MRS signal  $E_0(q_i)$  probability density functions at times  $t \in \{0, 5, 10, 30, 50\}$  days for increasing pulse values: a)  $q_1 = 60$  A.ms, b)  $q_2 = 145$  A.ms, c)  $q_3 = 362$  A.ms, d)  $q_4 = 904$  A.ms.

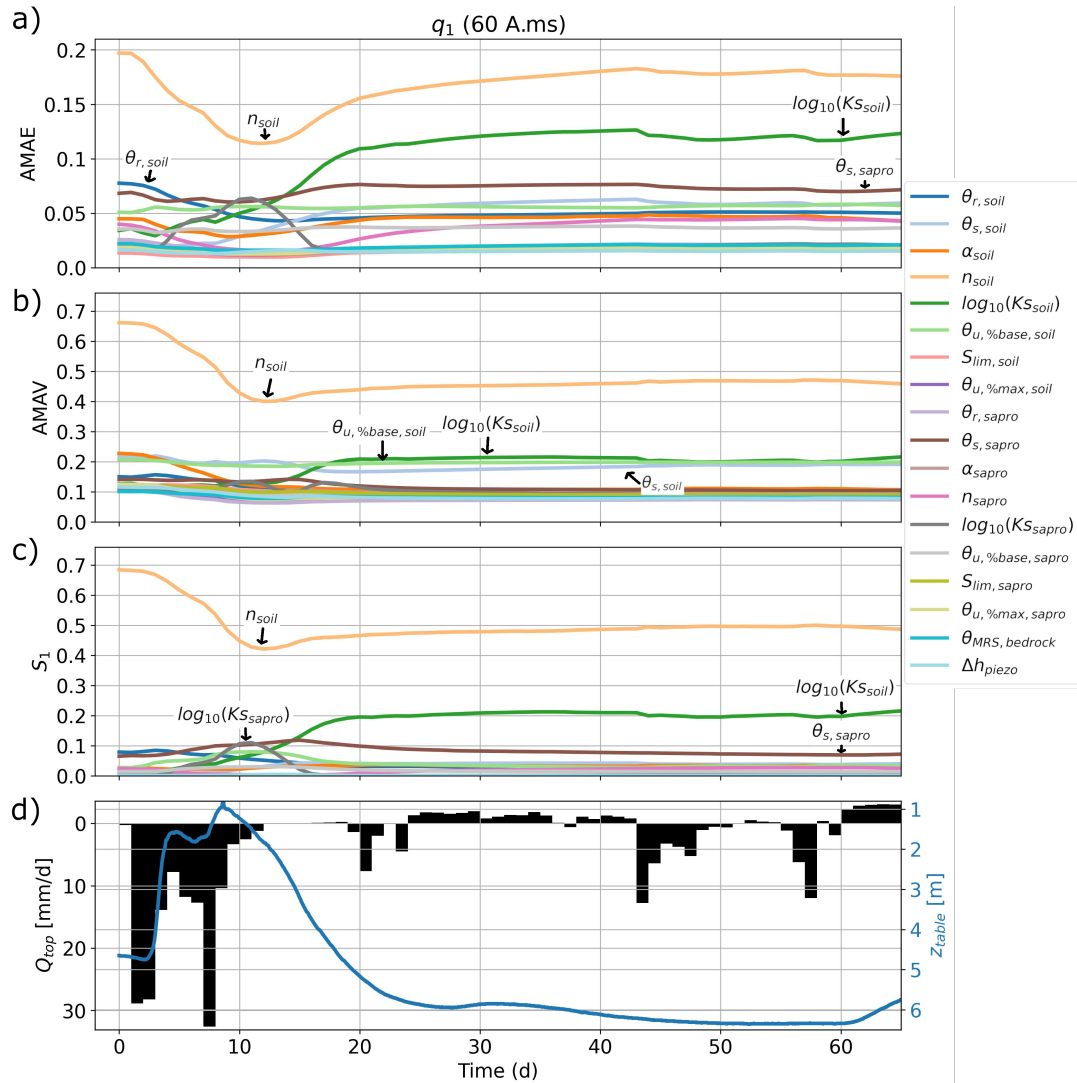
We observe a shift in the pdfs of the MRS signals towards higher values between day zero and day ten (Fig. 7a to d). This indicates that during the first ten days of the simulation period, the mean value of MRS signals increases. For the five pulse values at times  $t = 30$  d and  $t = 50$  d, the pdfs exhibit similar shapes. The distributions widen (i.e. show higher variance) as the pulse value increases from  $q_1$  (Fig. 7a) to  $q_3$  (Fig. 7c). The distributions for  $q_4$  (Fig. 7d) are slightly narrower than those for  $q_3$ . They also show the weakest temporal variations: the pdf curves are almost superimposed at all examined times. We make the same observations for  $q_5$ , which also displays narrower distributions centered on lower signal values (Fig. S1 in the Supplement). The pdfs also display an asymmetry, with a higher probability for stronger MRS signals. This asymmetry is more important for the lower pulse values and at earlier simulation times.

## 5.2 Global sensitivity indices: $q_1$

The global sensitivity indices presented in Sect. 4 exhibit their strongest temporal variability and the largest contrasts between AMAE, AMAV, and  $S_1$  for the first pulse moment ( $q_1 = 60$  A.ms; Fig. 8). Over the entire simulated period,  $n_{soil}$  exerts the dominant control on both the mean and variance of the MRS signals. After approximately 12-17 days, depending on the sen-



sitivity index considered,  $K_{s,soil}$  emerges as the second most influential parameter. During the early stage of the numerical  
355 experiment,  $\theta_{r,soil}$  significantly affects both the mean and variance of the MRS signals (Fig. 8a,c), but its influence decreases  
rapidly thereafter. The most pronounced differences among sensitivity indices are observed for the AMAV metric: AMAV val-  
ues associated with  $\theta_{s,soil}$  and  $\theta_{u\%,base,soil}$  remain high (approximately 0.20) throughout the simulation, indicating a persistent  
contribution of these parameters to the variance of the MRS signals. In contrast, AMAE and  $S_1$  identify  $\theta_{s,sapro}$  as the third  
360 most influential parameter. Despite these differences, all three sensitivity indices show similar temporal patterns for  $n_{soil}$ , with  
a sharp decline during the first 13 days followed by a renewed increase, more pronounced for the mean response (AMAE;  
Fig. 8a) than for the variance (AMAV and  $S_1$ ; Fig. 8b,c). Sensitivity indices associated with  $K_{s,soil}$  increase rapidly during  
the first 20 days before stabilizing, whereas those related to  $\theta_{r,soil}$  display an opposite trend over the same period. Finally,  
sensitivity indices for the remaining influential parameters ( $\theta_{s,sapro}$  for AMAE and  $S_1$ ;  $\theta_{s,soil}$  and  $\theta_{u\%,base,soil}$  for AMAV)  
exhibit weaker temporal variability and remain close to their initial values throughout the experiment.

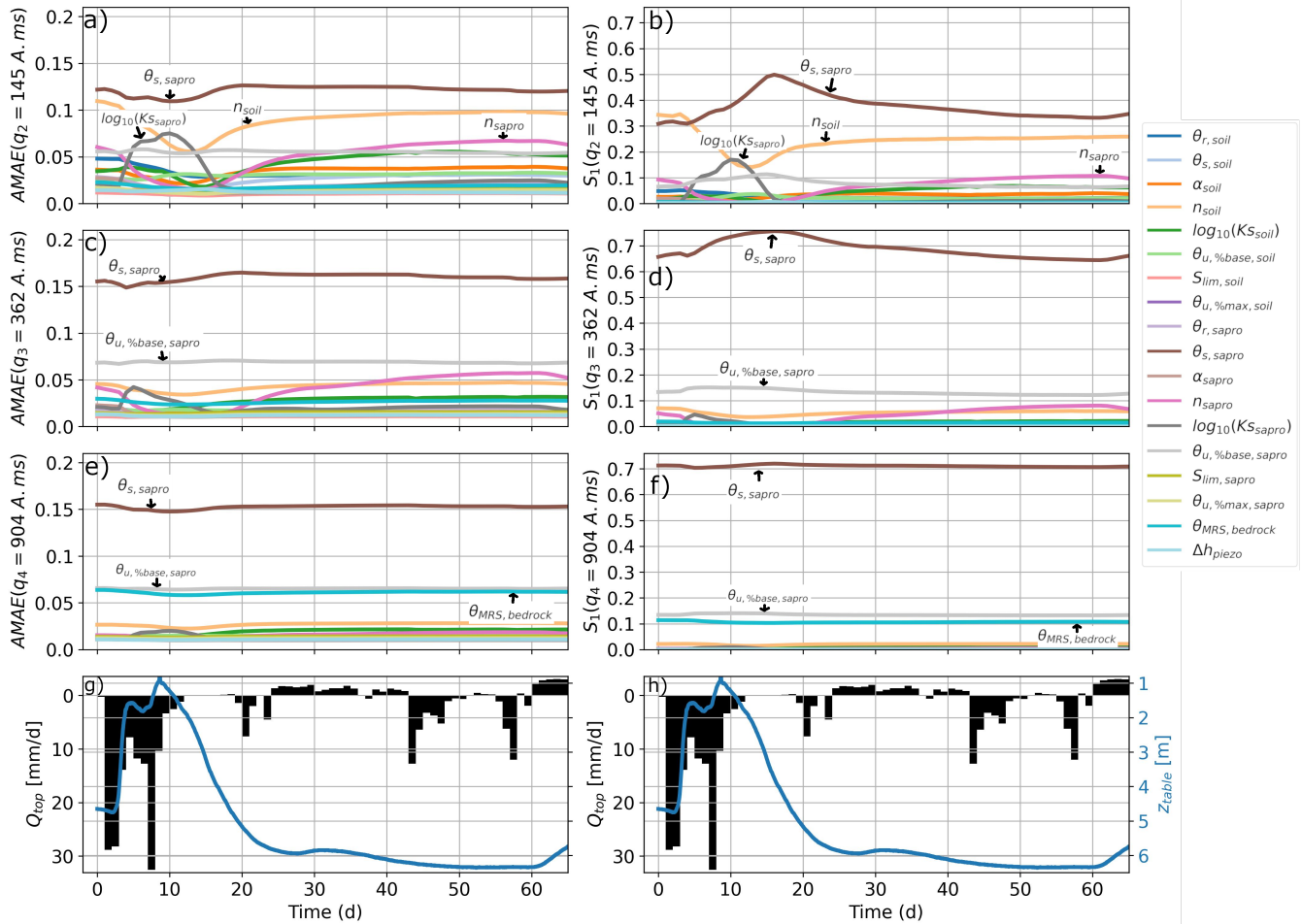


**Figure 8.** Time series of a) AMAE, b) AMAV and c)  $S_1$  sensitivity indices of MRS signals for the first pulse value:  $q_1 = 60.0$  A.ms, and d) time-series of the data constraining the model BC: upper BC (black) and bottom BC (blue).

### 365 5.3 Global sensitivity indices: $q_2$ to $q_5$

For higher pulse values ( $q_2 = 145$  A.ms to  $q_4 = 904$  A.ms), the sensitivity indices related to the variance of the MRS signals (AMAV and  $S_1$ ) exhibit similar behaviors. Therefore, we describe and analyze only the AMAE and  $S_1$  indices and their temporal dynamics for these pulse values (Fig. 9). The time series of AMAV indices for pulses  $q_1$  to  $q_5$  are provided in Fig. S2 in the Supplement. For the fifth pulse, the mean and variance of the MRS signals are largely controlled by a single parameter,  $\theta_{MRS, bedrock}$ , and the corresponding sensitivity indices remain constant throughout the simulated period (Fig. S3 in the Supplement).

370



**Figure 9.** Time series of AMAE (left column: a, c, e) and  $S_1$  (right column: b, d, f) for  $q_2$ ,  $q_3$  and  $q_4$ , and time-series of the data constraining the model BC: upper BC (black) and bottom BC (blue) (g, h).

$\theta_{s, sapro}$  exerts the strongest influence on both the mean and variance of the MRS signals for pulses  $q_2$  to  $q_4$ . For the second pulse,  $n_{soil}$  also remains influential (Fig. 9a,b): it is the second most influential parameter for most of the simulated period and the main driver of variance during the first days. Sensitivity to  $K_{s, sapro}$  shows pronounced temporal variability between days three and 17 (Fig. 9a,b). It increases markedly until day ten, when it reaches a maximum and  $K_{s, sapro}$  temporarily becomes the second most influential parameter. After day ten, sensitivity to  $K_{s, sapro}$  decreases back to its initial level. Sensitivity indices associated with  $n_{sapro}$  display opposite dynamics: they are initially significant, decrease between days three and 17, and then return close to their initial values for  $q_2$  (Fig. 9a,b), while continuing to increase for  $q_3$  (Fig. 9c,d).  $\theta_{u, \%base, sapro}$  also has a major contribution to both the mean and variance of the MRS signals for pulses  $q_3$  and  $q_4$ . The variability of  $\theta_{MRS, bedrock}$  is significant only for the higher pulse values ( $q_4$  and  $q_5$ ). In contrast, the VG parameters  $\alpha$  and  $\theta_r$  in the saprolite zone have a negligible effect on the mean and variance of the MRS signals at all times and for all pulse values. The same conclusion applies



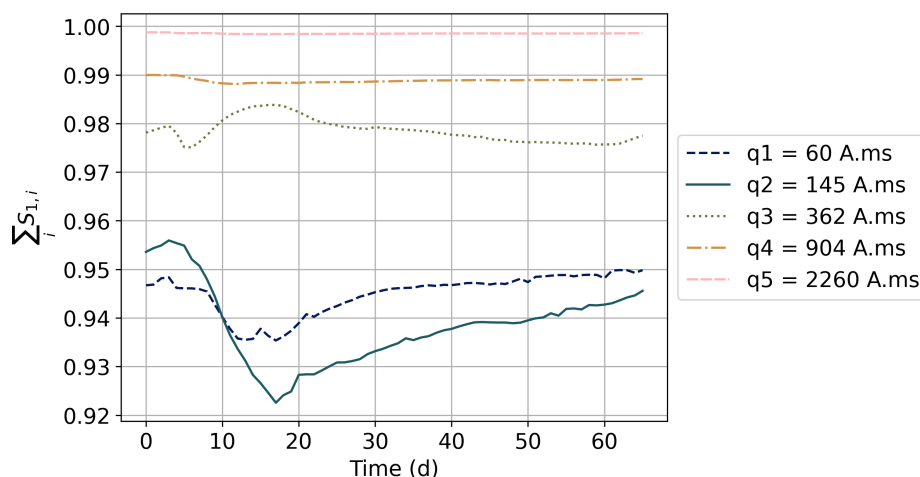
to two parameters related to the MRS-undetectable water content,  $S_{lim}$  and  $\theta_{u\%,max}$ , in both the soil and saprolite zones, and to  $\Delta h_{piezo}$ . Table 2 summarizes the sensitivity of the MRS signals to hydrodynamic parameters for all pulse values and for the three sensitivity indices considered.

Parameter	q1			q2			q3			q4			q5		
	AMAE	AMAV	$S_1$	AMAE	AMAV	$S_1$	AMAE	AMAV	$S_1$	AMAE	AMAV	$S_1$	AMAE	AMAV	$S_1$
$\theta_{r,soil}$	+~	-	+~	+~	-	-	-	-	-	-	-	-	-	-	-
$\theta_{s,soil}$	-	+~	-	-	-	-	-	-	-	-	-	-	-	-	-
$\alpha_{soil}$	-	+~	-	-	-	-	-	-	-	-	-	-	-	-	-
$n_{soil}$	+++~	+++~	+++~	+++~	+++~	+++~	+~	-	+~	-	-	-	-	-	-
$\log_{10}(K_{s,soil})$	+++~	+~	+++~	+~	-	-	-	-	-	-	-	-	-	-	-
$\theta_{u\%,base,soil}$	-	+~	+~	-	-	-	-	-	-	-	-	-	-	-	-
$S_{lim,soil}$	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
$\theta_{u\%,max,soil}$	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
$\theta_{r,sapro}$	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
$\theta_{s,sapro}$	+~	-	+~	+++~	+++~	+++~	+++~	+++~	+++~	+++~	+++~	+++~	+~	-	-
$\alpha_{sapro}$	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
$n_{sapro}$	-	-	-	+~	-	+~	+~	+~	+~	-	-	-	-	-	-
$\log_{10}(K_{s,sapro})$	+~	-	-	+++~	-	+++~	+~	-	-	-	-	-	-	-	-
$\theta_{u\%,base,sapro}$	-	-	-	+~	-	+~	+++~	+++~	+++~	+~	+~	+~	-	-	-
$S_{lim,sapro}$	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
$\theta_{u\%,max,sapro}$	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
$\theta_{MRS,bedrock}$	-	-	-	-	-	-	-	-	-	+++~	+++~	+++~	+++~	+++~	+++~
$\Delta h_{piezo}$	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-

**Table 2.** Summary of the sensitivity of the MRS signals to the hydrodynamic parameters. The symbol “+” denotes significant sensitivity, whereas “-” indicates negligible sensitivity. For parameters exhibiting significant sensitivity, we further indicate whether sensitivity varies over time (denoted by “~”) or remains stable throughout the numerical experiment (denoted by “\_”).

### 385 5.4 Parameters interactions

The presented sensitivity indices account for the independent effects of the hydrodynamic parameters. Higher-order indices should be computed in order to take into account the interactions between parameters. The magnitude of these interactions can be estimated by summing the first-order Sobol indices of all the parameters (Fig. 10). The greater the difference between this sum and unity is, the stronger the interactions between the parameters are.



**Figure 10.** Time series of the sum of all the first order Sobol indices  $\sum_i S_{1,i}$  for the five pulse values.

390 For the highest pulse values, nearly all of the variance can be explained by independent effects of the model parameters (Fig. 10). The interactions are stronger for  $q_1$  and  $q_2$ : up to more than 6% and 7% of the variance can be attributed to the interaction between parameters for  $q_1$  and  $q_2$ , respectively. Investigation of the second-order Sobol indices shows that the couples of parameters all have a second order index smaller than 0.02, indicating that the difference between the sum of first order Sobol indices and unity is composed of multiple weak interactions.

## 395 6 Discussions

### 6.1 $E_0$ probability density functions

The increase in the mean amplitude of the MRS signals for all pulses during the first ten days of the numerical experiment (observed in Fig. 7) is a direct consequence of the meteorological event. Indeed, surface infiltration and the rise in the water table level lead to stronger MRS signals. On the other hand, the evolution of variance with increasing pulses reflects the investigation depths associated with the different pulses. From  $q_1$  to  $q_3$ , the variance increases as the signals become progressively sensitive to deeper regions (Fig. 4) which exhibit a higher degree of saturation (see Fig. S4 in the Supplement). Pulses  $q_4$  and  $q_5$  are primarily sensitive to the portion of the subsurface column that is always saturated. However, the variance is slightly lower for  $q_4$  due to lower values of the sensitivity function  $\kappa$  (Fig. 4). It is smaller for  $q_5$ , because of both lower values of the sensitivity function and the narrower variation range for the water content in the bedrock layer (Sect. 4.3). The MRS signals pdfs indicate a satisfactory sampling of the parameter space. The superposition of the pdfs corresponding to similar hydric states at  $t = 30$  and  $t = 50$  d (see Fig. S4 in the Supplement for the mean saturation distributions) confirms that the parameter space was explored with a sufficient number of Monte Carlo realizations. For all considered pulses and at all simulation times,



the pdfs of MRS signals do not display multimodality. Furthermore, the observed asymmetry is low to moderate. This ensures the relevance of variance-based sensitivity analysis (Saltelli et al., 2002).

## 410 6.2 GSA for $q_1$

For the first pulse value, the parameter which has the strongest influence on both the mean and variance of the MRS signals is  $n_{soil}$ . This dominant effect arises from the strong influence of  $n$  on the relationship between pressure  $h$  and water content  $\theta$  (Eq. 2), especially in the low saturation domain ( $h < 0$  with high absolute value). The parameter  $\alpha$  also affects this relationship, but to a lesser extent, which explains the difference in how these two parameters impact the MRS signals (see Fig. S5 in the  
415 Supplement, showing retention curves  $\theta(h)$  for several values of  $n$  and  $\alpha$ ). During the meteorological event (rainfall infiltration and water table rise), sensitivity to  $n_{soil}$  decreases, whereas sensitivity to  $K_{s,soil}$  increases (Fig. 8). Sensitivity to  $n_{soil}$  stops decreasing once the rain event ends (after day 12), indicating that the primary driver of this sensitivity is the surface infiltration flux  $Q_{top}$ , and that this flux negatively affects the influence of  $n_{soil}$ . In contrast, sensitivity to  $K_{s,soil}$  stabilizes a few days after the end of the infiltration event. This delay may result from the presence of an infiltration front, whose propagation speed is  
420 controlled by  $K_{s,soil}$  through its effect on the (unsaturated) hydraulic conductivity (Eq. 3).

The values of the AMAV index for the parameters  $\theta_{u\%,base,soil}$  and  $\theta_{s,soil}$  (Fig. 8b) imply that these two parameters have a non-negligible impact on the variance of the MRS signals. This observation highlights the relevance of using multiple sensitivity measures. Indeed, basing our GSA approach on  $S_1$  solely would have led us to the wrong conclusion that the two  
425 aforementioned parameters do not have an impact on the variance of MRS signals. This is consistent with the results by Dell'Oca et al. (2017), who showed for an analytical benchmark function that the Sobol indices can miss the effects of some parameters on the outputs of a model.

We also observe a different baseline value for the indices AMAE, AMAV and  $S_1$ . This baseline value provides information on the precision of the estimation of the sensitivity indices. Only the parameters with sensitivity indices above this baseline can be discussed with confidence. The baseline value for the AMAE indices is around 0.025, that for the AMAV indices is close to  
430 0.10. Despite this fact, the sensitivities discussed so far lie above this baseline. The Sobol indices are estimated with a better precision as their baseline is close to zero. This may be due to the high accuracy of the PCE used to compute the Sobol indices.

## 6.3 GSA for $q_2$ to $q_4$

The consistently strong influence of  $\theta_{s,sapro}$  on both the variance and the mean of the MRS signals for pulses  $q_2$  to  $q_4$  can be explained by the fact that a non-negligible fraction of the saprolite zone remains permanently saturated. Under saturated  
435 conditions, the water content  $\theta$  (and, consequently, the MRS signals) is solely controlled by the parameter  $\theta_s$  (Eq. 2). For pulses  $q_3$  and  $q_4$ , the parameter  $\theta_{u\%,base,sapro}$  has a strong and constant influence on both the mean and the variance of the MRS signals. This results from the high degree of saturation in the regions of sensitivity of these two pulses. These saturation values are consistently above the saturation threshold  $S_{lim}$ , making  $\theta_{u\%,base,sapro}$  the only parameter influencing the MRS undetectable water content (Fig. 5).



440 Whereas the second pulse remains sensitive to some of the soil hydrodynamic parameters, higher pulse values are primarily  
sensitive to the saprolite zone parameters. The variability of the parameter  $n_{sapro}$  is significant for pulses  $q_2$  and  $q_3$  during  
periods when the water table level is low. The temporal dynamics of the sensitivity indices for pulse  $q_2$  are largely governed by  
the bottom boundary condition. For instance, the sensitivity indices associated with  $K_{s,sapro}$  exhibit the same temporal trend  
as the water table level during the meteorological event. Sensitivity to  $\theta_{s,sapro}$  is correlated with the rise of the water table, but  
445 displays a temporal delay. This delay arises from the two dynamics driving the system: (1) the propagation of the precipitation  
infiltration front, and (2) the rise of the water table. Analysis of water content distributions from individual simulations (see  
Fig. S6 in the Supplement) shows that, depending on the parameter set, the infiltration front reaches the saturated zone at  
different times. In some simulations, this introduces a delay in when the top of the saturated zone reaches its lowest depth.  
Finally, the sensitivity dynamics become less pronounced as the pulse value increases, consistent with the analysis of the pdfs  
450 of the MRS signals.

#### 6.4 Parameters with insignificant contribution

Some parameters have a negligible impact on both the mean and variance of MRS signals for all pulse values and at all times.  
Among these parameters are two of VG parameters related to the saprolite layer:  $\theta_{r,sapro}$  and  $\alpha_{sapro}$ . These parameters have a  
negligible impact on the MRS signals because they do not affect the water content in the saturated part of the subsurface column.  
455 Concerning the MRS undetectable water content fraction, two of the three parameters governing this quantity always exhibit a  
negligible impact:  $\theta_{u\%,max}$  and  $S_{lim}$ .  $\theta_{u\%,max}$  is the limit fraction of undetectable water content when the saturation tends to  
zero (Fig. 5). Although the fraction of undetectable water increases with decreasing saturation, the value of  $\theta_{u\%,max}$  does not  
appear to influence the MRS signals. This is likely because it primarily affects the lowest saturation values, which contribute  
only weakly to the MRS signals. Furthermore, the water content distributions show very sharp transitions in saturation (Fig. S6  
460 in the Supplement). As a result, the position of the threshold  $S_{lim}$  along the saturation axis is of minor importance, since  
saturation rapidly transitions from values above the threshold to values that are negligible for the MRS response over very short  
depth intervals. Regarding parameter identifiability, our results indicate that under the investigated experimental conditions,  
these six parameters - namely  $\theta_{r,sapro}$ ,  $\alpha_{sapro}$ ,  $S_{lim}$ , and  $\theta_{u\%,max}$  in both the soil and saprolite zones - are unlikely to be  
accurately estimated through an inverse problem based solely on time-lapse MRS data (Wu et al., 2019). This limitation could  
465 be mitigated by incorporating complementary data into the inversion framework. Useful constraints include direct water content  
measurements (Belfort et al., 2018) or supplementary geophysical datasets, such as seismic and gravimetric data (Fores et al.,  
2018) or ERT and self-potential data (Li et al., 2024). Additionally, integrating GPR with time-lapse MRS data holds significant  
potential; the shallow depth of investigation characteristic of GPR would effectively complement the deeper sensitivity of MRS  
measurements (Legchenko et al., 2018).

470 To maintain a focused GSA, the framework excludes the effects of environmental electromagnetic noise on MRS data.  
Because such noise introduces a random bias independent of subsurface hydrodynamic processes, it is expected to globally  
attenuate parameter identifiability rather than alter the relative sensitivity of individual parameters.



The parameter  $\Delta h_{piezo}$ , introduced to account for the uncertainty in the representativity of the piezometric data for the studied area, also has a negligible impact on both the variance and the mean of MRS signals for all pulse values. This result suggests that, assuming the uncertainty in the representativity of the piezometric measurements varies within the range  $[-0.20, 0.20]$  m, it does not have a measurable impact on the MRS signal statistical moments. Finally, the sum of first-order Sobol indices is always close to unity, indicating that parameter interactions have a negligible contribution to the variance of the MRS signals.

## 7 Conclusions

We present a hydrogeophysical model, coupling the one-dimensional Richards equation for subsurface unsaturated water flow with the geophysical method of MRS. We analyze the sensitivity of MRS signals to hydrodynamic parameters and uncertainties in the lower BC in the context of a meteorological event which occurred in winter 2021 in the Strengbach headwater catchment. During this intense meteorological event, a fast saturation of the underground porous medium was observed due to the combined effect of snowmelt (0.8 m of snow accumulated before the event) and a strong and long lasting rain event (107 mm cumulated over a period of 12 days). To conduct the GSA, we designed a numerical experiment based on real hydrological and meteorological data collected at the Strengbach catchment. This numerical experiment allows us to simulate signal acquisition for several pulse moments as if they could be acquired simultaneously and to explore acquisitions repeated through time every 24 hours. The domain geometry, parameters and boundary conditions are representative of the studied site. Following the conclusions of Dell’Oca et al. (2017), we used several sensitivity indices to quantify the effects of uncertainty in hydrodynamic parameters on the MRS signals. We conducted the sensitivity analysis with the classical variance-based Sobol indices, together with the AMAE and AMAV indices. Thus, we present a robust GSA of the hydrogeophysical model, free from the assumption that the totality of the effects of hydrodynamic parameters can be captured solely through their impact on the model output variance. To the best of our knowledge, the model we developed for this study is the first one to account for the fraction of MRS-undetectable water content within the modeling framework thereby enabling simulation of MRS signals of the same order of magnitude as typical experimental observations using realistic hydrodynamic parameters for the soil and saprolite zones. The results of the numerical experiment lead to the following conclusions:

1. The parameters which exert the strongest influence on the mean and variance of the MRS signals depend on the pulse value. For the lowest pulse value (i.e., the shallowest depth of investigation), the dominant parameter controlling both the mean and variance of MRS signals is the VG parameter  $n$  in the soil layer, followed by  $K_{s,soil}$ . For pulses  $q_2$  to  $q_4$ , the most influential parameter is  $\theta_s$  in the saprolite zone.  $n_{soil}$ ,  $K_{s,sapro}$  and  $n_{sapro}$  have significant contributions to the MRS signals mean and variance of the second pulse. For the third and fourth pulse, the second most influential parameters are  $\theta_{u\%,base,sapro}$  and  $\theta_{MRS,bedrock}$  respectively. Finally, the dominant parameter associated with the fifth pulse (i.e. the deepest region of investigation) is the MRS water content in the bedrock zone.
2. Some parameters have a negligible impact on both the mean and variance of the MRS signals across all times and pulse values. Among the subsurface flow parameters, the non-sensitive ones are  $\theta_{r,sapro}$  and  $\alpha_{sapro}$ . For the parameters related



505 to the MRS-undetectable water content fraction, the parameters with negligible influence on MRS signals are  $\theta_{u\%,max}$  and  $S_{lim}$  (in both the soil and saprolite zone). Consequently, these six parameters are unlikely to be accurately estimated from an inverse problem relying solely on time-lapse MRS data.

3. The use of multiple sensitivity indices provides valuable information beyond that obtained from a Sobol-indices-only GSA. Indeed, it prevents the erroneous conclusion that the parameters  $\theta_{s,soil}$  and  $\theta_{u\%,base,soil}$  have a negligible impact  
510 on the MRS signals for the first pulse value.

4. The temporal dynamics of the sensitivity indices of MRS signals are stronger for lower pulse values. We conclude that these pulse values are the most relevant to repeat in a time-lapse experiment. In this context, energy can be saved by avoiding repetition of the highest pulse values which are also the most energy-intensive, and by focusing on lower pulse values for investigating the shallow subsurface. However, this conclusion is site dependent and a dedicated sensitivity  
515 analysis can help defining the most appropriate MRS acquisition sequence in other settings.

The results of this study provide valuable insights for estimating hydrodynamic parameters from time-lapse MRS data and for guiding the design of future experimental developments. While this study leverages site-specific geological data and a distinct meteorological event, the integrated GSA framework provides a transferable methodology applicable to geophysical monitoring experiments across diverse hydrogeological contexts. The GSA results constitute a solid comprehension basis of  
520 the model's behavior, which is a crucial information before attempting subsurface flow model calibration with time-lapse MRS data.

*Code and data availability.* The meteorological data and the water table depth measured in the piezometer pz5b used to compute the boundary conditions were obtained from the OHGE database (<https://bd-ohge.unistra.fr/OHGE/>). This database is accessible upon creation of an account and request of access. The transformed data (computed boundary conditions), the hydrodynamic parameters samples, the simulated  
525 MRS signals and the codes implementing the Phyrus-MRS forward model, the GSA of the model and the visualization routines are available on Zenodo (Gru et al., 2026) (<https://doi.org/10.5281/zenodo.20558903>). The routines used to define the PCE metamodels and compute the Sobol sensitivity indices are available in the UQ[py]Lab python library (Lataniotis et al., 2021). The Phyrus python library used for unsaturated water flow simulation (Collenteur et al., 2020) is publicly available.

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