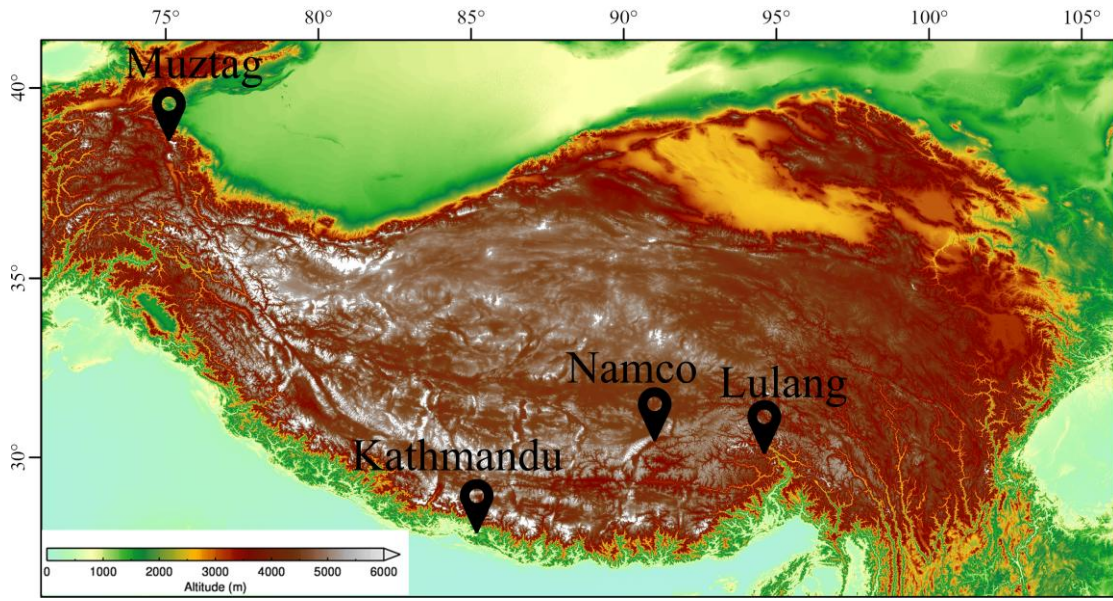


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31 **Figure S1. Map of locations for four high-altitude monitoring stations.**

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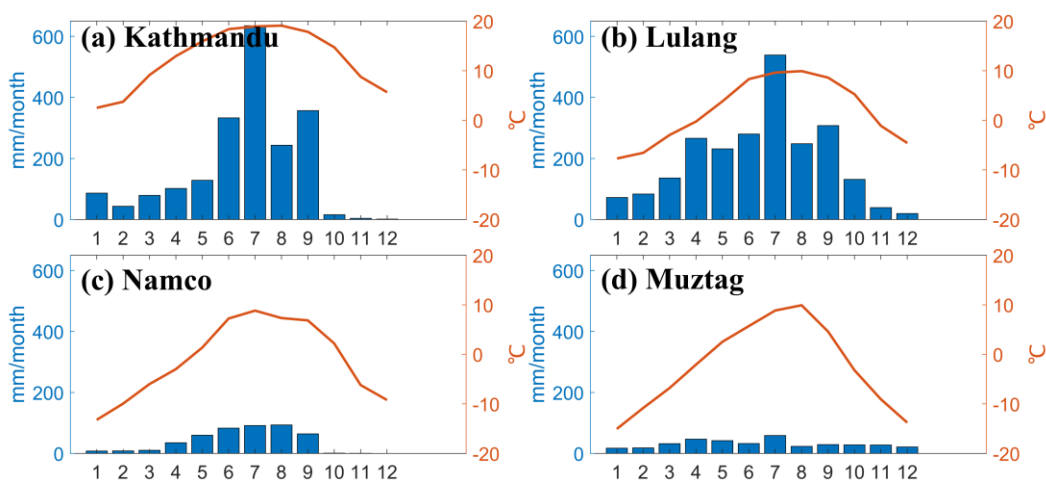
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50 **Seasonal Cycles of Temperature and Precipitation**

51 Seasonal cycles of temperature and precipitation at four monitoring stations are shown
52 in Supplementary Fig. 1. At Kathmandu site, the maximum precipitation occurred in
53 July that reaching 634.6 mm per month, while in December was the least, to only 1.4
54 mm/month. The maximum 2 m air temperature occurred in August (19.1 °C) and
55 reached lowest in January (2.5 °C). At Lulang site, the maximum precipitation occurred
56 in July (538.6 mm/month), and the minimum precipitation occurred in December (19.4
57 mm/month). Compared to Kathmandu, precipitation at Lulang shows a more gradual
58 change. The maximum 2 m air temperature occurred in August (9.9 °C) and reached
59 lowest in January (-7.7 °C). At Namco site, the station closer to the TP interior,
60 precipitation has sharply decreased. The maximum precipitation occurred in August
61 (93.6 mm/month) and in December was minimum (0.1 mm/month). The maximum 2
62 m air temperature occurred in July (8.8 °C) and reached lowest in January (-13.2 °C).
63 At Muztag site, the only station located in northern TP, presenting the driest
64 characteristics from four monitoring stations. The maximum precipitation occurred in
65 July (58.5 mm/month), and the minimum precipitation occurred in January (17.3
66 mm/month). The maximum 2 m air temperature occurred in August (9.9 °C) and
67 reached lowest in January (-15.1 °C).



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69 **Figure S2. Seasonal cycles of observed 2 m air temperature [°C] and precipitation**
70 **intensity [mm/month] at (a) Kathmandu, (b) Lulang, (c) Namco, and (d) Muztag.**

71 Results were averaged from year 2020-2021.

72 **Calibration and Quality Control**

73 The observation conditions at four monitoring stations are slightly different. At
74 Kathmandu, Picarro L2130-i analyzer was installed at the Kathmandu Centre for
75 Research Education (KCRE) and the sampling inlet was mounted 7 m above the ground
76 surface with a 10 L min⁻¹ pump that deliver air from inlet to the analyzer. Desiccant was
77 used to drying air. At Lulang, ambient air was collected at 2 m above the ground surface,
78 and dry air comes from the external dry air cylinder that is connected. At Namco, the
79 sampling inlets were installed on the flux tower with four different heights (1 m, 4 m,
80 11 m, 40 m) and switched automatically every 15 minutes. Dry air comes from the
81 external dry air cylinder. At Muztag, the sampling inlet was mounted 2 m above the
82 ground surface, and air was dried through desiccant.

83 The measured water vapor isotopic ratios from Picarro L2130-i is affected by factors
84 such as humidity (called humidity dependency), and instrument properties (called
85 instrumental drift). Therefore, calibration is necessary to minimize measurement errors
86 as much as possible. Referring Steen-Larsen et al. (2013) and Bastrikov et al. (2014),
87 the calibration protocols are similar across four monitoring stations but slightly
88 different for Namco. Except Namco, standard deliver module (SDM) was used to
89 perform calibration. The SDM controls flow rate of standard to generates standard at
90 different humidity level that covering full range of atmospheric humidity. The
91 calibration protocols including following steps:

- 92 1) Humidity dependency calibration: Isotopic values were measured at a constant flow
93 rate of dry air for 25 min at each humidity level and then change gradually. Using a
94 isotopic value that humidity of close to 20,000 ppmv as a true value to calculate
95 differences of measured isotopic value at different humidity levels. Constructing
96 function between different humidity levels and differences to calibrate isotopic
97 observations of the current month. To remove a memory effect, the first 15 min of
98 data from the calculations were excluded.
- 99 2) Instrumental drift calibration: two water isotopic standards (S1: $\delta^{18}\text{O}=-10.009\text{‰}$,

100 $\delta D = -69.476\text{‰}$; S2: $\delta^{18}\text{O} = -29.806\text{‰}$, $\delta D = -227.225\text{‰}$) were measured at each day
101 with six different humidity levels. Averaging over the last 15 min at each humidity
102 level to obtain a calibrating function by applying regression function to the
103 standards and averaged values.

104 At Namco, calibration system was replaced with Dew Point Generator (DPG, Steen-
105 Larsen et al., 2014). At each day, the DPG generates two different humidity levels
106 instead of six compared to other stations.

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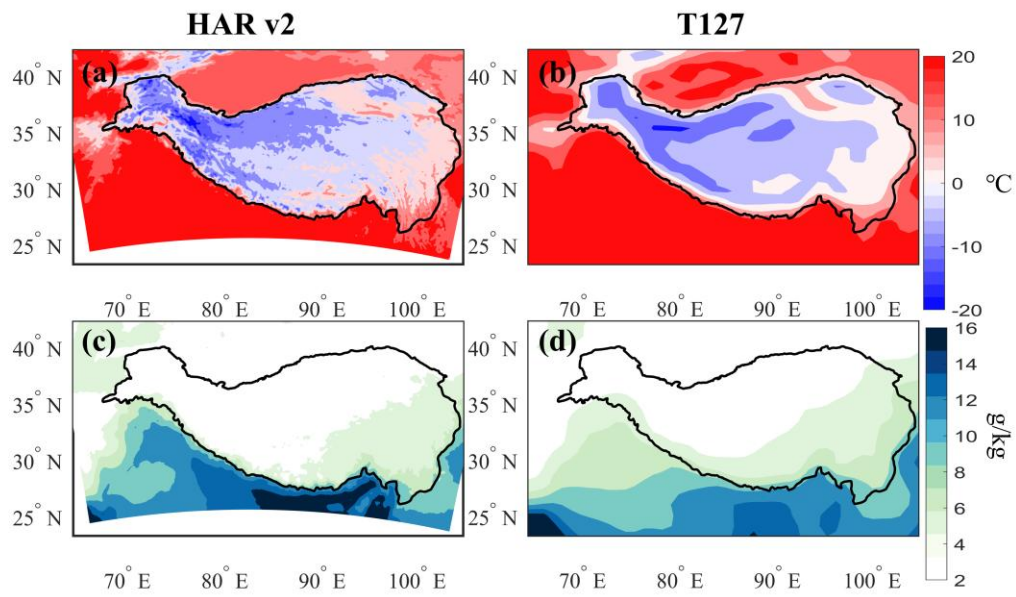
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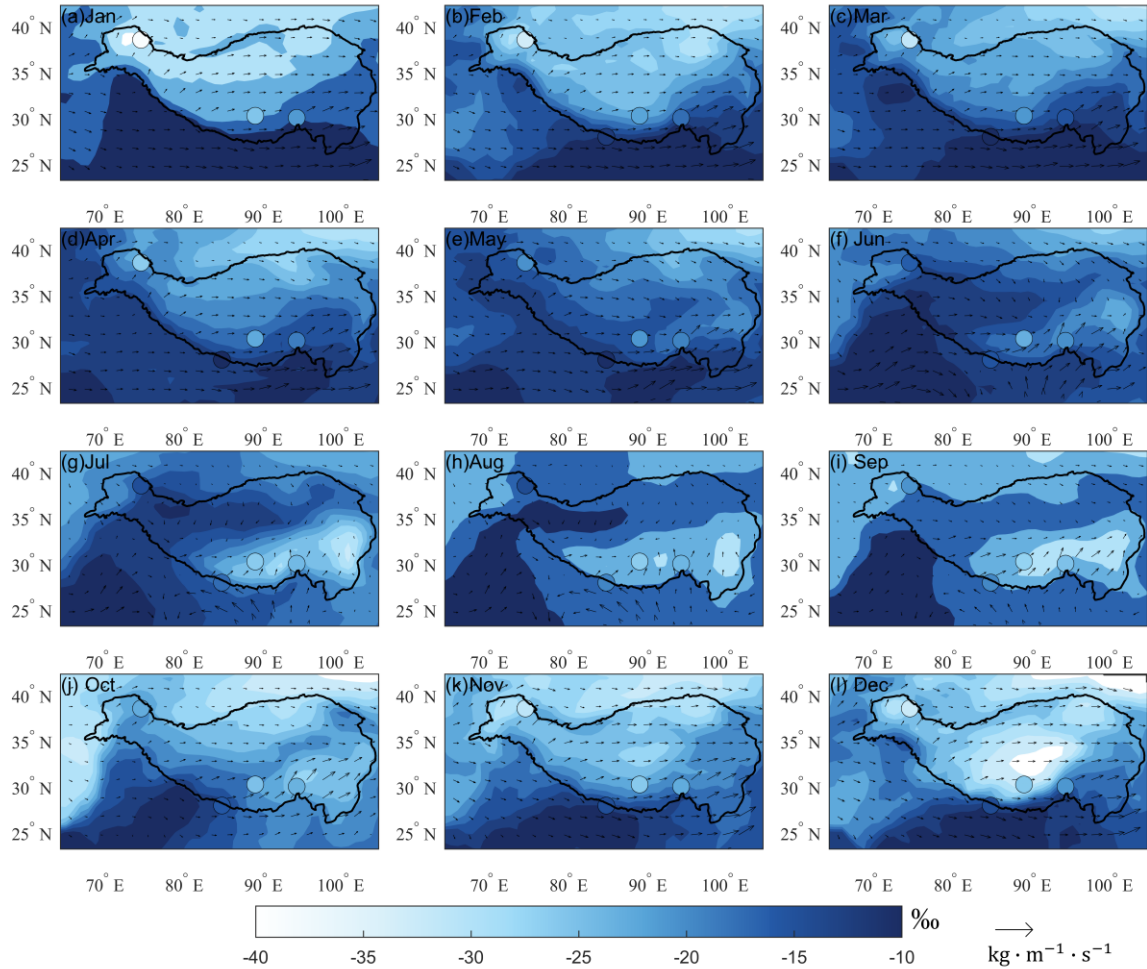


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122 **Figure S3. Distributions of referenced (HARv2) and simulated (a), (b) 2m air**
 123 **temperature [°C] and (c) (d) specific humidity [g/kg], averaged of year 2020-2021.**

124 Black polygon outlines the TP border.

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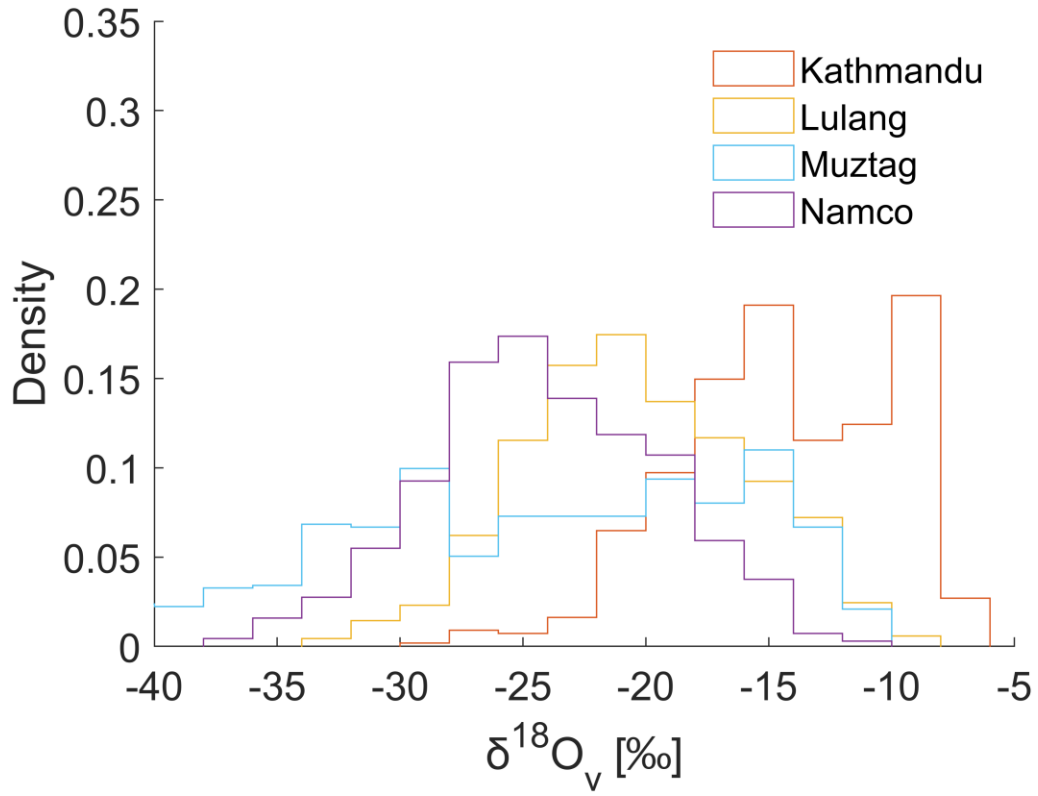
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127 **Figure S4. Distributions of simulated (colored contours) and observed (colored**
 128 **dots) monthly mean near-surface $\delta^{18}\text{O}_v$ values [%], averaged of period 2020-2021.**

129 Black arrows denote the simulated vertically integrated water vapor flux [$\text{kg} \cdot \text{m}^{-1} \cdot$
 130 s^{-1}], while the black polygon outlines the TP border. Note: Panel (a) is missing the

131 observational data from Kathmandu.

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134 **Figure S5. PDFs of observed daily $\delta^{18}\text{O}_v$ at Kathmandu (orange), Lulang (yellow),**

135 **Namco (purple), and Muztag (light blue).**

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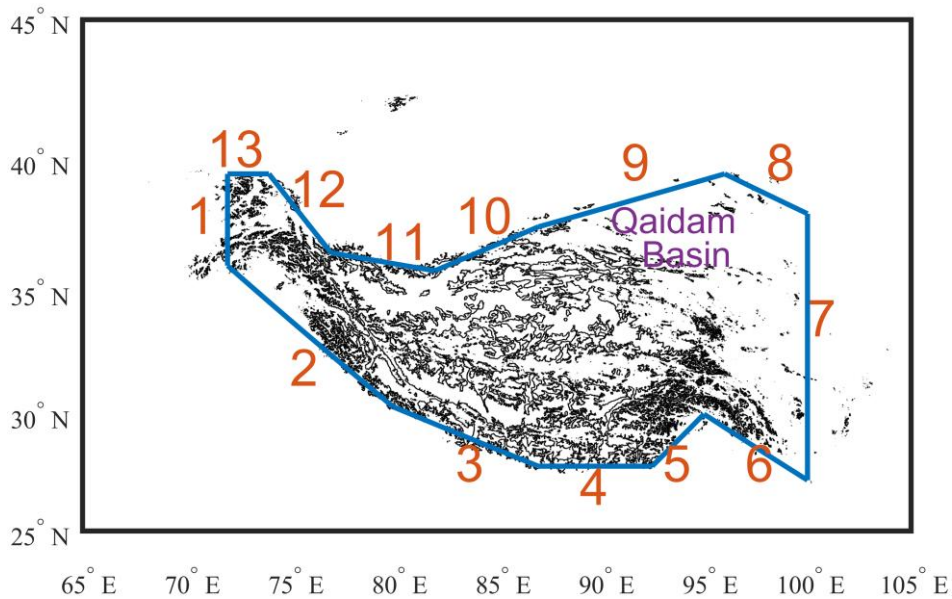
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150 **Division for 13 transects over the TP**

151 Given the extremely complex boundaries and variable winds around the TP, it will
152 introduce great uncertainty if only focusing atmospheric moisture transport in four
153 directions. Therefore, it's imperative to demarcate the TP border based on the potential
154 pathways for atmospheric moisture transport. We defined 13 transects attempting to
155 follow the 4000 m a. s. l. in the mountain range and to cut cross the mountain valleys.



156 **Figure S6. Distribution of the 13 transects (blue lines).** Black contours are the
157 elevation of 4000 m a. s. l. over the TP. Length of each transect: transect 1: 389.18 km;
158 transect 2: 1092.30 km; transect 3: 826.52 km; transect 4: 611.57 km; transect 5: 370.30
159 km; transect 6: 637.22 km; transect 7: 1200.90 km; transect 8: 475.02 km; transect 9:
160 1025.20 km; transect 10: 587.23 km; transect 11: 561.40 km; transect 12: 471.76 km;
161 transect 13: 222.39 km.

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171 **Atmospheric moisture transport**

172 Atmospheric moisture transport is commonly expressed by the water vapor flux in an
173 atmospheric column, which can be calculated as:

$$174 \quad q_{\text{flux}} = \rho \cdot q \cdot v, \quad (1)$$

175 ρ is the air density (kg m^{-3}), q denotes the specific humidity (kg kg^{-1}), and v is the
176 horizontal wind vector (m s^{-1}).

177 Total air column water vapor flux is calculated by integrating water vapor fluxes over
178 the whole air column:

$$179 \quad Q = \int_{p_{\text{surf}}}^{p_{\text{top}}} \frac{1}{g} \cdot q_{\text{flux}} dp, \quad (2)$$

180 where Q is the vertically integrated water vapor flux ($\text{kg} \cdot \text{m}^{-1} \cdot \text{s}^{-1}$), p_{top} and p_{surf}
181 represent the pressure at the top atmosphere and surface, respectively, while g is
182 acceleration by gravity ($9.8 \text{ Pa} \cdot \text{m}^2 \cdot \text{kg}^{-1}$).

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200 **Inflow profile**

201 We calculate perpendicular vector values of atmospheric moisture transport relative to
202 the transect as the inflow. Thus:

203 $q_{\text{flux,input}} = q_{\text{flux}} \cdot \sin \theta, (3)$

204 where $q_{\text{flux,input}}$ is the inflow and θ is the angle between the atmospheric moisture
205 transport and the transect.

206 inflow profiles can be obtained by calculating the inflow at each atmosphere level along
207 a transect. Ideally, this involves identifying the grid cells that intersect with the transect
208 to derive the inflow profile. However, due to the mismatches between the grid cells and
209 the transect locations, we first identify grid cells within 30 km of the transect. The
210 transect is then discretized into n equally spaced points. For each point, the nearest grid
211 cells are used to calculate the mean inflow. At the junction of the two transects, the
212 overlapping grid cells are used only for the subsequent transect to prevent double
213 counting. This procedure is repeated for each atmosphere level to obtain the inflow
214 profiles.

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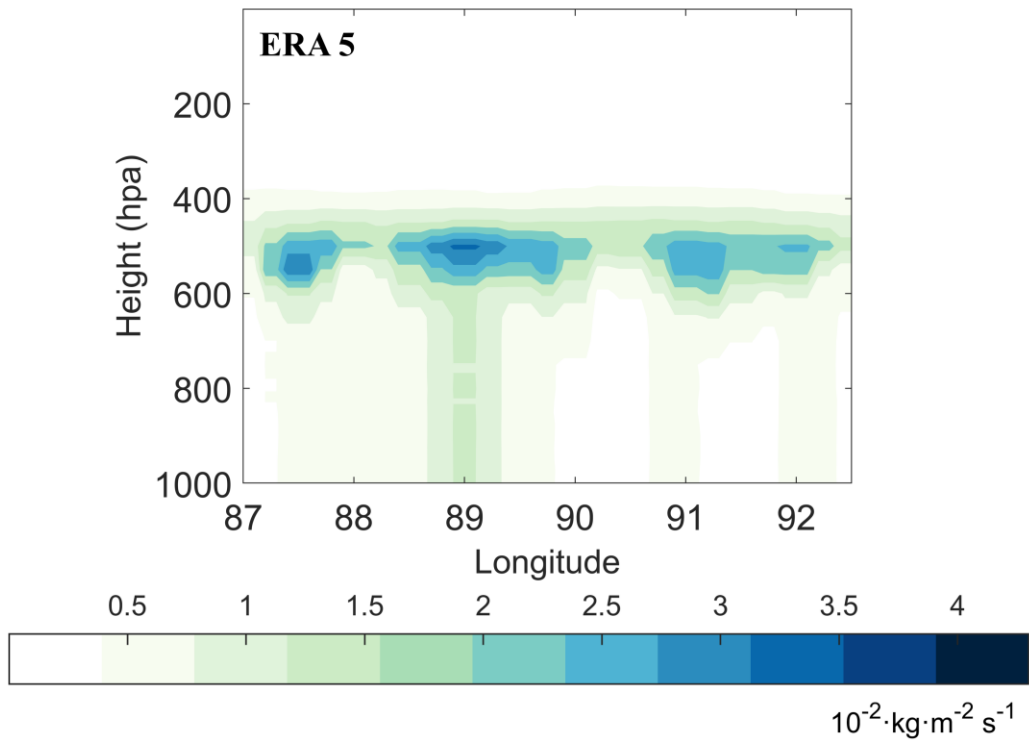
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230 **Figure S7. Inflow profile [$10^{-2} \text{ kg m}^{-2} \text{ s}^{-1}$] on transect 4 derived from ERA5.**