



1 Brief Communication: Rise of the Guadalupe River- A Multifaceted Post Event

2 Analysis of the July 4, 2025, Flood in Central Texas

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9 Abstract

10 The flash flooding across Central Texas on July 4th, 2025, caused more than 130 fatalities and
11 property losses exceeding 20 billion dollars. The objective of this study is to diagnose the drivers
12 of this catastrophic event and to analyze the temporal variability in forecasting flood inundation
13 dynamics in the hours leading up to and during the event. Using the Operational National Water
14 Model short-range streamflow forecast product, we generated 306 forecasted flood inundation
15 maps between July 3rd and July 4th, 2025. For evaluation, we constructed an inundation extent
16 benchmark derived from USGS high water marks. Both impact-based and pixel-based assessments
17 are presented.

18 1. Introduction

19 On July 4th at dawn , a catastrophic flash flood hit Kerr and Kendall Counties in Texas, claiming
20 at least 135 lives, making it one of the deadliest inland flooding events in United States history
21 (<https://psl.noaa.gov/news/2025/texasfloods.html>). The event was triggered by intense rainfall up
22 to 3-4 inches per hour in some of the impacted areas, causing flash flooding with exceptionally
23 high peaks throughout the Guadalupe River basin. The Texas Hill Country, including Kerr and
24 Kendall County, is prone to flash flooding, known as “Flash Flood Alley” (Saharia et al., 2017),
25 partly due to the geomorphology of the area, having steep slopes and clay-rich soils, which result
26 in high runoff rates (Sharif et al., 2010). Based on United States Geological Survey (USGS)
27 streamflow observations, extreme flows were recorded downstream of the confluence of the South
28 Fork Guadalupe River and the North Fork River (Figure 1d). At Hunt (Gage ID: 08615500), the
29 streamflow reached 8,260.8 m³/s at 5:05 AM, far exceeding the 500-year return period flow of
30 4,160.8 m³/s. A significant portion of this peak was contributed by the ungauged South Fork



31 Guadalupe River, which caused numerous fatalities near Camp Mystic (Nevitt 2025). Further
32 downstream, at Kerrville, the streamflow peaked at 8,316.0 m³/s at 6:45 AM, crossing the 500-
33 year return period flow of 7,937.6 m³/s. Apart from the peak values, the hydrographs at both
34 upstream gauge stations exhibited exceptionally short times to peak, reaching the 500-year return
35 period level within just 1–1.5 hours. This rapid rise of flow is indicative of extremely high runoff
36 response, amplifying the severity of the event.

37 The main motivation of this study was to utilize multiple operational forecast Flood Inundation
38 Maps (FIM) and conduct an extensive impact-based and categorical assessment of the event across
39 different forecast hours against high water mark derived benchmark FIM. We employed the
40 National Weather Service (NWS) National Water Model (NWM) short-range forecast and the
41 FIMserv tool (Baruah et al., 2025) to generate 306 FIMs at the Hydrologic Unit Code (HUC)-8
42 scale. Additionally, we developed a methodology to use post-event USGS observed high-water
43 marks to create a spatially continuous FIM benchmark for evaluating the forecast FIMs. Our
44 objective is to investigate the trade-off between NWM forecast range and the reliability of flood
45 impact predictions. Specifically, we examined how FIM forecast skill, including building-level
46 impacts, varied with respect to different forecast hours at five different locations (four streamflow
47 gauges and near Camp Mystic).

48 2. Hydrometeorological Assessment

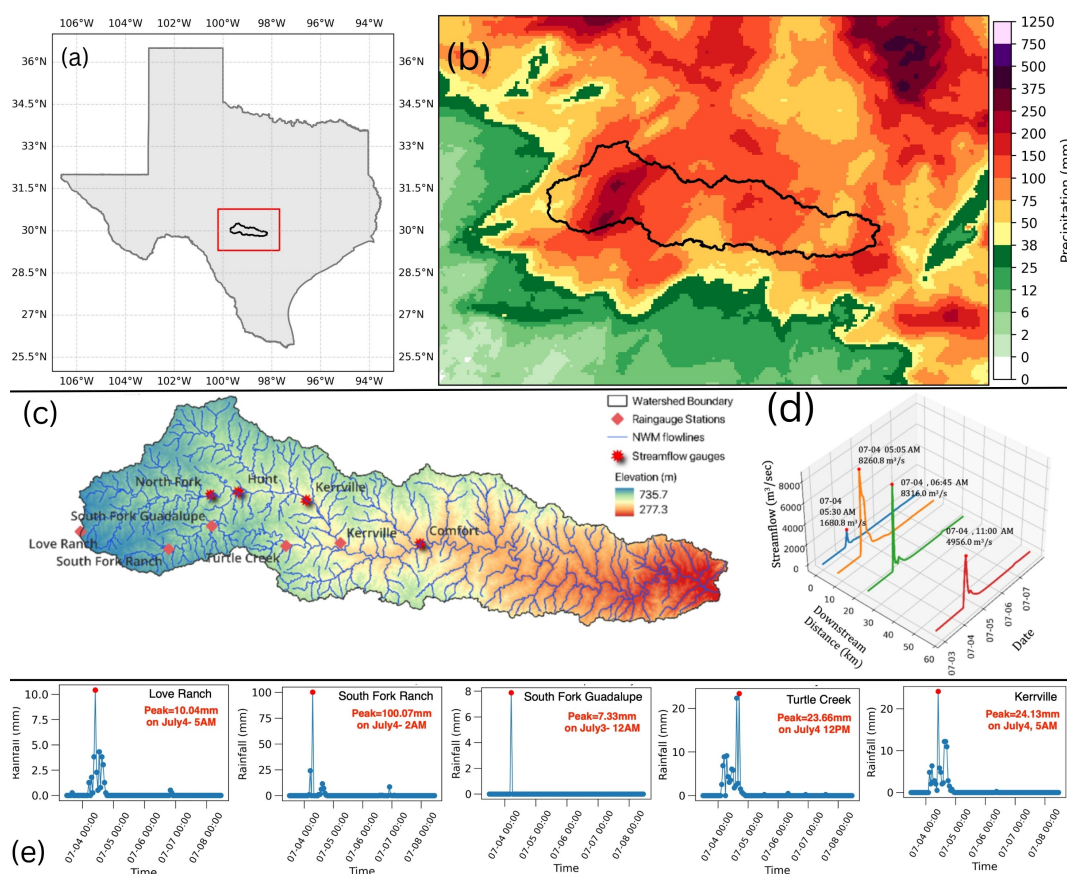
49 Between July 3rd and 6th, 2025, the Texas Hill County region experienced an extraordinary rainfall
50 amounts that produced catastrophic flash flooding along the Guadalupe River (Figure 1a-1c). The
51 event was initiated by remnant moisture from Tropical Storm Barry, which had made landfall in
52 Mexico days earlier, and was further intensified by a mesoscale convective vortex embedded
53 within a persistent mid-level trough. These factors, combined with a strengthening low-level jet to
54 sustain widespread convection, favor back-building successive thunderstorms across the Hill
55 County (WPC, 2025). Hourly precipitation amounts from the Multi-Radar Multi-Sensor (MRMS)
56 gauge-corrected quantitative precipitation estimation (QPE) dataset (Zhang et al., 2016),
57 supplemented with rain gauge observations, reveal accumulations exceeding 500 mm (20 inch) in
58 parts of the upper Guadalupe basin between July 3 to July 6 (Figure 1b). Rainfall intensities
59 surpassed 100-year return period thresholds for durations ranging from 3 to 24 hours at the rainfall



60 gauges when compared against NOAA Atlas 14 precipitation frequency curves (Perica et al., 2018;
61 NSSL, 2025). One of the most severe bursts occurred between 2 AM and 5 AM on July 4, when
62 localized rainfall rates reached 100 mm/h (Figure 1e, Figure S2). The persistence of convective
63 regeneration amplified accumulations and produced rainfall totals approaching 460 mm in some
64 localized areas on July 4. Gauge records showed peaks at stations in the western part of the basin
65 that aligned with MRMS QPE observations, where total precipitation indicated higher
66 accumulations (Figure 1b, e, Figure S2).

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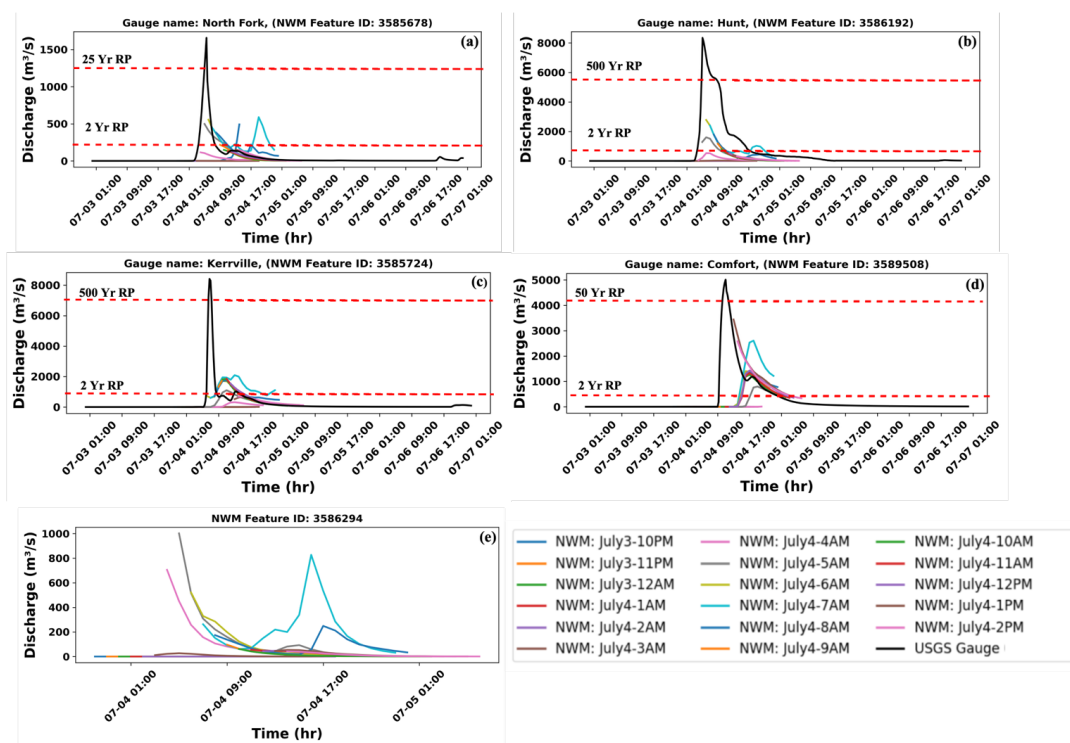


69



70 Figure 1. (a) Geographical location of the study area, (b) MRMS-derived total precipitation
71 between 4–6 July 2025, (c) locations of USGS streamflow and rainfall gauges, (d) Gauge
72 streamflow records along the reach, and (e) hourly rainfall time series.

73 The NWM short-range forecasts (SRF) provide hourly streamflow predictions extending to 18
74 hours forecast range (<https://water.noaa.gov/about/nwm>). We identified the NWM flowlines
75 (feature_id) that intersect with the USGS gages and downloaded the SRF generated (Figure 2)
76 from 10 PM, July 3rd till 2 PM, July 4th using FIMserv. At North Fork (peak at 5.30 AM), earlier
77 SRFs show no flooding conditions, but there is a sudden jump on the forecast generated on July 4
78 , between 4 AM to 7AM (120 m³/sec to 600 m³/sec). At Hunt (peak at 5:05 AM), the forecast
79 generated for 4 AM indicates a possibility that flow will cross 500 m³/sec (above 2 Year RP flow
80 of 266.08 m³/sec) in the next two hours, while the forecast generated for 5 AM, reaches the 10-
81 year RP (1276.52 m³/sec). Further downstream, at Kerrville (peak at 6:45 AM), there was no
82 indication of a high flow event; however, the forecast generated for 6 AM shows that flow will
83 exceed the 2-year return period flow (284.22 m³/sec). At Comfort (peak at 11:00 AM), the initial
84 forecast shows low flows, while the forecast generated after 10 AM indicates that flow will exceed
85 the 10-year RP flow (1842.73 m³/sec), and the subsequent forecast follows the same trend. Near
86 Camp Mystic, for which we do not have a USGS gage, the forecast for 4 AM in South Fork
87 Guadalupe River predicted a peak of 750 m³/sec. A Zoom-in view of the generated forecast closer
88 to the event is shown in Figure-S1 of the supplementary material.



89

90 Figure 2. NWM short-range forecast at different lead times at (a) North Fork (b) Hunt (c) Kerrville
 91 (d) Comfort and (e) Camp Mystic. The red dash line indicates the return period flow exceeded by
 92 the gage readings.

93 Overall, the NWM SRF deviated substantially from the USGS observations in this case (Figure
 94 2). These underpredictions in NWM SRF during the flood event were strongly affected by two
 95 primary sources of uncertainty: 1) Inconsistency in the location and magnitude of precipitation
 96 rates in the precipitation forcing from the High-Resolution Rapid Refresh (HRRR) model leading
 97 up to the event, and ii) the failure of USGS stream gauges used for data assimilation. The NWM
 98 short-range configuration relies on HRRR Quantitative Precipitation Forecast (QPF) at 3-km
 99 resolution to drive runoff generation (Dowel et al., 2022). A rainfall-to-rainfall comparison
 100 between the HRRR-QPF and MRMS Quantitative Precipitation Estimate (QPE) indicated a
 101 notable underestimation in the HRRR rainfall forecasts (Figure S3 in the supplementary material).
 102 When QPF underestimates or spatially misplaces convective rainfall cells, the resulting simulated
 103 discharge and flood peaks are either lower in magnitude or displaced in time relative to
 104 observations (Krajewski et al., 2025; Vergara et al., 2023). This bias has a pronounced effect on



105 streamflow forecasts, especially for basins smaller than 1,000 km² that are prone to flash flooding
106 (Krajewski et al., 2025). The combination of the spatially misplaced QPF, smaller basin sizes, and
107 flash flood prone geomorphology caused the NWM to signal intense flooding potential in the
108 basins surrounding the Guadalupe River in the hours leading up to the event. However, the
109 changing signal location in each timestep resulted in underprediction for the Guadalupe basin. The
110 underestimation in the NWM during the event was exacerbated by the failure of the USGS gauge
111 08165500 near Hunt on the Guadalupe River during the fast-rising streamflow, as seen from the
112 outage of data on the USGS water data gauge page from July 4th to the 5th
113 (<https://wik.ly/3Wjb6hk>). This outage disrupted the NWM's data assimilation process (Seo et al.,
114 2021) from performing streamflow “nudging” to correct model states toward observed discharge.
115 These errors were extrapolated with downstream flow propagation, resulting in systematic
116 underprediction of streamflow.

117 3. Forecast FIM Generation and Evaluation

118 We used FIMserv to generate 306 flood inundation maps using the above described NWM
119 forecasted flows. FIMserv assigns each forecast as an inflow to the OWP HAND-FIM model,
120 which uses reach-averaged synthetic rating curves to generate binary FIMs, based on the Height
121 Above Nearest Drainage (HAND) approach (Aristizabal et al., 2023; Chen et al., 2025).

122 3.1 Derivation of Maximum Forecasted Inundation

123 The maximum extents from the forecast FIMs at a given reference time are estimated by combining
124 multiple short-range forecast FIMs (Figure S4 in the supplementary material). For example, to
125 assess flooding on July 4th, 5:00 am (reference time), we used the maximum inundation extent
126 from a total of 7 forecasts from earlier timestamps (10 pm July 3 through 4:00 am July 4) that
127 predict conditions at 5:00 am. Each raster (i.e., each of the 7 forecasts) was stacked, and for each
128 pixel, if it was marked as flooded in any raster, it was considered flooded in the final composite.
129 This approach produces a temporally integrated, conservative estimate of potential flooding (i.e.,
130 the largest possible forecasted extent for that hour), capturing uncertainty and variability in
131 subsequent short-range forecasts.

132 3.2 Flood benchmark map creation using High Water Marks (HWMs)



133 We used the USGS High-water marks (HWMs) as the primary reference data for the creation of
134 the benchmark FIM. HWM observations were obtained from the USGS Short-Term Network
135 (STN) database (<https://stn.wim.usgs.gov/STNDataPortal/#>) and subjected to multi-stage
136 preprocessing. First HWMs were filtered based on data quality (“Good” or “Excellent” quality
137 were retained). Surveyed elevations (elev_ft) were converted to metric units (elev_m) relative to
138 mean sea level. Next, global outlier removal was performed using the interquartile range (IQR)
139 method (Tukey, 1977) to eliminate extreme data points. Subsequently, spatial outliers were
140 identified using Local Moran’s I, which evaluates each HWM in the context of its neighboring
141 points rather than the dataset as a whole. The spatial relationships are defined using a weights
142 matrix, with the neighborhood distance empirically determined through semivariogram analysis.
143 This approach ensures that the detection of local outliers reflects the natural decay of spatial
144 autocorrelation across the floodplain, improving the reliability of the interpolated water surface
145 elevation. The filtered HWM dataset was then interpolated into a continuous Water Surface
146 Elevation (WSE) raster using the Topo to Raster algorithm in ArcGIS Pro 3.4.0, a hydrologically
147 conditioned interpolation approach that enforces drainage continuity (Feaster and Koeing.,2017;
148 Koeing et al., 2016). The interpolated WSE surface was subtracted from a 10 m Digital Elevation
149 Model (DEM), yielding flood depth estimates. Cells with positive residuals ($DEM \leq WSE$) were
150 classified as inundated, while negative residuals were assigned as non-flooded. This procedure
151 yielded a benchmark flood inundation map derived solely from empirical HWM data that was used
152 in FIM forecast evaluations in subsequent sections.

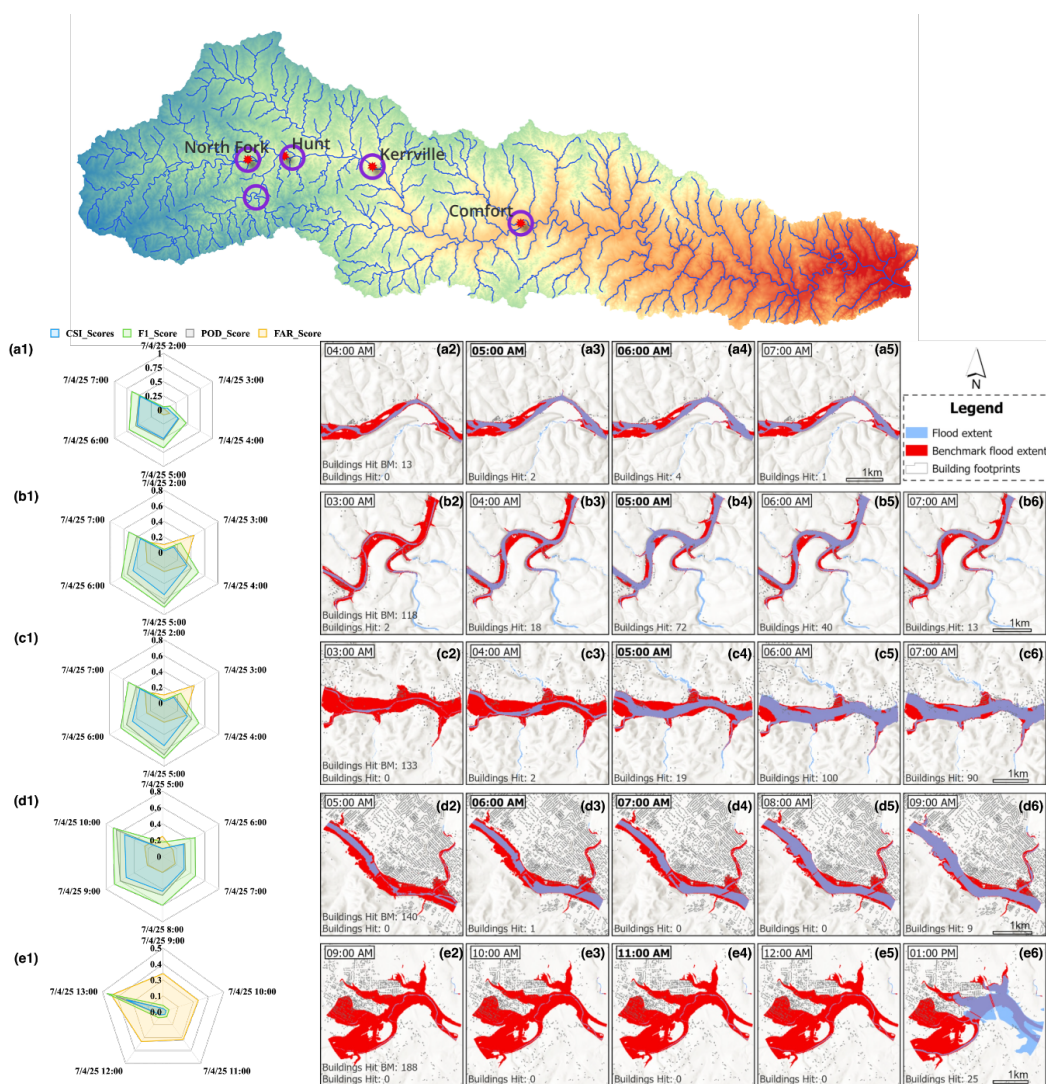
153 3.3 Evaluation of the forecasted FIM against the benchmark FIM

154 We used FIMeval (Devi et al., 2025) to evaluate the forecasted FIMs at five locations (Figure 3)
155 across different forecast times against the benchmark FIM. Since the HWM-derived benchmark is
156 static (maximum inundation) and the exact time at which the HWMs were attained during the flood
157 event is unknown, the gage-recorded peak time was used as the reference, and forecasted FIMs
158 were evaluated within a ± 2 -hour window around this reference hour. This introduces an additional
159 source of temporal uncertainty into the overall evaluation process. For pixel-based assessment, we
160 used Critical Success Index (CSI), F1-Score, Probability of Detection (POD), and False Alarm
161 Rate (FAR) as the evaluation matrix (Figure 3), and for impact assessment, we compared the
162 number of predicted and observed flooded buildings at different forecast times.



163 At North Fork, the flood peak occurred at 5:30 AM. Compared to earlier forecasts, the FIM
164 forecasts for 4 AM to 6 AM show gradual improvements in CSI, F1, and POD scores, although the
165 4 AM forecast also exhibits a higher FAR (Figure 3a1). The impact assessment (Figures 3a2–a5)
166 indicates that 4 AM forecast FIM predicts no building flooded, 5 AM forecast predicts two flooded
167 buildings, whereas the benchmark FIM shows 13 flooded buildings. Near Camp Mystic, the
168 evaluation scores for the 4 and 5 AM forecasts improved substantially compared to earlier forecasts
169 (Figure 3b1). In terms of impacts, the benchmark FIM shows 118 buildings affected, while the 4
170 AM and 5 AM forecasts predict only 18 and 72 flooded buildings, respectively (Figures 3b2–b6).
171 At Hunt, the flood peak was recorded at 5:05 AM. Here, the evaluation scores also improved, with
172 CSI values increasing from 0.34 for the 4 AM forecast to 0.52 for the 5 AM forecast, while earlier
173 forecasts yielded much lower scores (<0.25) (Figure 3c1). The impact assessment (Figures 3c2–
174 c6) indicates that the benchmark FIM estimates 133 buildings impacted, compared to only 19 for
175 the 5 AM forecast and only 2 for the 4 AM forecast. At Kerr, the peak was recorded at 6:45 AM.
176 Here, we found higher evaluation scores in the post-event forecast. For instance, the CSI scores
177 are below 0.30 for 6 AM, but the scores are increasing at 10 AM, at 0.53. A similar trend was
178 observed in POD and F1 score. From the impact assessment, we found that the benchmark FIM
179 shows 140 flooded buildings, while the forecast FIMs have only one building flooded at 6 AM.
180 We also observed notable underprediction in forecast FIM extents downstream of hydraulic
181 structures (Figure 3d2-d4). Such discrepancies likely stem from artifacts in the HAND raster and
182 insufficient representation of dam release flows in the NWM streamflow forecasts (Aristizabal et
183 al., 2023; Kim et al., 2020). At Comfort, the flood peak occurred at 11:00 AM. Early forecasts
184 showed very low scores (<0.1), but the scores improved at 1 PM (Figure 3e1). Eventually, we
185 found no buildings hit from the predicted FIMs until 1 PM, while the benchmark indicates 188
186 flooded buildings (Figure 3 e2-e6).

187



188

189 Figure 3. Top panel shows the FIM evaluation extent. (a) North Fork (b) Camp Mystic (c) Hunt
 190 (d) Kerr and (e) Comfort. The bottom left panel (a1-e1) shows the accuracy metrics of FIM
 191 evaluation and the right panel (a2-e6) shows the forecast flood extent, benchmark flood extent,
 192 and number of building hits at different forecast hours. Each subpanel lists the forecast hour in the
 193 upper-left box; times that coincide with, or cover, the USGS-observed peak discharge are
 194 highlighted in bold.

195



196 4. Closing Remarks

197 In this brief communication, we highlight the hydroclimatic drivers and impacts of the Texas flash
198 flood event on July 4, 2025. Using USGS gauge observations, we analyzed the NWM short-range
199 streamflow forecasts. Across all four-gauge locations, the NWM short-range forecasts
200 considerably underpredicted the peak flow, with a pronounced lag between observed and
201 forecasted flows at downstream sites. We found that underprediction and lag in short range
202 forecasts are mainly due to the errors in rainfall estimation and the failure of data assimilation
203 (“nudging”) caused by malfunctioning USGS gauges during the peak flow. These streamflow
204 underpredictions seem to have propagated, resulting in substantially underestimated flood extents
205 in forecasted FIMs at different lead times. Using the gauge-recorded peak time as a reference, we
206 evaluated forecast FIMs at different hours. against a benchmark flood inundation extent generated
207 using ground-sampled high-water marks from USGS. At upstream gages, forecast skill improved
208 as the forecast time approached the reference peak, whereas at downstream locations (Kerr and
209 Comfort), evaluation scores were very poor at the reference time but improved after the observed
210 peak flow. It is also clear from the impact assessment that forecast FIM was unable to capture the
211 majority of flooded buildings compared to the benchmark. This case study points to the need for
212 communicating the uncertainty and error bounds in operational forecast FIMs for early response
213 and decision-making. One promising approach is probabilistic FIM which can effectively
214 represent and leverage uncertainty in streamflow forecasts, providing more informative and
215 actionable guidance for emergency responders.

216 **Code and data availability**

217 Code for downloading the NWM short-range forecast and for producing the flood inundation maps
218 is available at <https://github.com/sdmlua/FIMserv>. The benchmark high water flood inundation
219 map for the Texas Flood event is available in <https://github.com/sdmlua/fimbench>

220 **Author contributions**

221 Conceptualization: Anupal Baruah, Dinuke Munasinghe, Sagy Cohen. Formal analysis and
222 methodology: Anupal Baruah, Dinuke Munasinghe, Mohamed Abdelkader, Dipsikha Devi,
223 Yixian Chen, Derek Supervision: Sagy Cohen. Writing (original draft preparation): Anupal



224 Baruah, Mohamed Abdelkader, Dinuke Munasinghe, Dipsikha Devi, Riley McDermott, Derek
225 Giardino, Humberto Vergara. All authors reviewed the final paper.

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230 **Conflict of Interest**

231 None of the authors has any conflict of interests

232 **Disclaimer**

233 The scientific results and conclusions, as well as any views or opinions expressed herein, are those
234 of the authors and do not necessarily reflect the views of NOAA.

235

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