



Airborne performance assessment of the DLR MIRO MGA³ quantum cascade laser spectrometer for fast N₂O measurements

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Abstract.

Nitrous oxide (N₂O) is the most dominant precursor of ozone-depleting substances and the third most important anthropogenic greenhouse gas, with agriculture contributing the largest share of emissions (56%). Over the past two decades, airborne in-situ measurements have become increasingly important for studying emission and transport of N₂O in the atmosphere, also driven by the development of more precise and simultaneously faster Quantum Cascade Laser (QCL)-based spectrometers.

However, many QCL-based spectrometers exhibit sensitivities to environmental and flight-related parameters that can vary rapidly (≤ 1 s), such as static or cabin pressure and aircraft roll and pitch angles. The impact of changing ambient water vapor is particularly critical due to both dilution and quantum-mechanical effects. Because the variability of N₂O in the lower troposphere is often very small (<1 ppb) relative to its high background (~ 338 ppb), even minor variations in these parameters can significantly affect data quality and must be corrected. Although many instruments can resolve such small concentration changes, their typical temporal resolution of 1 Hz may limit the application of advanced measurement techniques such as eddy covariance on fast-moving aircraft.

Here, we present and evaluate a new instrument setup for precise (< 0.2 ppb) and high-frequency (10 Hz) airborne in-situ N₂O measurements in altitudes up to 4500 m based on a MIRO MGA³ QCL spectrometer (MIRO Analytical AG). The instrument was successfully deployed during two airborne science missions, namely onboard the unpressurized DLR Cessna during the Greenhouse Gas Monitoring (GHGMon) campaign in 2023 in the Netherlands, as well as onboard the NASA



DC8 during the Satellite Investigation of the Asian Air Quality (ASIA-AQ) campaign in 2024. Specifically, we evaluate and compare different water vapor correction approaches using ASIA-AQ data sampled within the tropical boundary layer over South Korea, the Philippines, Thailand and Taiwan, which partly were characterized by specifically high ambient humidity (up to 30000 ppm H₂O). The water vapor correction methods include an empirical approach that relies on both native and corrected MIRO in-flight water vapor measurements, as well as an approach by an updated version of the MIRO specific fitting software. Comparison with N₂O measurements from a well-established instrument onboard the NASA DC8 shows agreement within combined measurement uncertainties for all tested water vapor correction approaches, albeit special caution is needed for humidities larger than 15000 ppm. The new water vapor corrected data shows a 42% better precision than with original default settings of the instrument. We further show that the instrument setup is insensitive to flight parameter changes such as roll and pitch angle of the aircraft, and allows for stable measurements even under challenging conditions such as in the turbulent boundary layer.

This instrument setup enables improved characterization of N₂O emissions and sources from the agricultural sector which is, in particular, relevant for tropical regions with strong agricultural activity and high humidity, where observational data remain scarce.

1 Introduction

Nitrous Oxide (N₂O) is, after carbon dioxide (CO₂) and methane (CH₄), the third most important anthropogenic greenhouse gas (GHG) (Myhre et al., 2013) and the dominant precursor of ozone (O₃)-depleting substances in the stratosphere (Ravishankara et al., 2009). It has an atmospheric lifetime exceeding 100 years (Prather and Wilson, 2026; Prather et al., 2023, 2015; Myhre et al., 2013). Since the preindustrial era, its atmospheric mole fraction has increased from approximately 270 ppb in 1750 to 336 ppb in 2022 (Tian et al., 2024; MacFarling Meure et al., 2006) corresponding to a sustained rise with a mean annual growth rate of 0.96 ppby⁻¹ during the decade from 2010 to 2019 (Tian et al., 2024).

N₂O is emitted to the atmosphere from both natural (65% of total net emissions) and anthropogenic (35%) sources (Tian et al., 2024). Among anthropogenic sources, agriculture dominates, accounting for 56% of total net emissions. These emissions primarily arise from the microbial processes of nitrification and denitrification, through which organic and synthetic fertilizers are partially converted to N₂O, as well as from direct nitrogen (N) inputs to soils (Tian et al., 2024; Smith, 2017). Additional significant anthropogenic contributions originate from other direct emissions (32%), including industry, fossil fuel use, and biomass burning (Tian et al., 2024). The growth rate is expected to increase even further in the future due to the growing demand for food, energy and industrial processes associated with continued population growth (Tian et al., 2024; Smith, 2017; Reay et al., 2012).

This makes N₂O a key target for future mitigation policy (Kanter et al., 2020). To meet the goals of the Paris Agreement (UN-FCCC, 2018), limiting global warming to 2°C requires a reduction in N₂O emissions of 11% by 2050 and as much as 22% to achieve the 1.5°C limit (Rogelj and Lamboll, 2024; Tian et al., 2024). However, alarmingly, even the worst case Representative Concentration Pathways (RCPs) and Shared Socioeconomic Pathways (SSPs) underestimate the global mean N₂O mole



50 fractions observed in the atmosphere by roughly 2-3 ppb in 2020 (Tian et al., 2024). Current models sometimes lack adequate representation for N₂O emission factors, for example, for the amount of N soil input or freeze-thaw cycles, which results from a lack of data and measurements for specific regions (Del Grosso et al., 2022; Thompson et al., 2019).

Developing efficient mitigation strategies requires precise quantification of emissions from dominant source sectors and a robust understanding of the underlying processes. N₂O emissions can be estimated using a range of approaches, commonly
55 classified as Bottom Up (BU) and Top Down (TD) methods (Tian et al., 2024; Saboya et al., 2024; CCAC, 2024; Davidson and Kanter, 2014). TD approaches include satellite observations, which offer global coverage but are not yet operational for N₂O (Kiemle et al., 2024). At smaller scales, chamber and tower measurements provide insights at spatial extents of 1 m² and up to 10 km², respectively, but are inherently limited to fixed locations (Chadwick et al., 2014; Rapson and Dacres, 2014; Pattey et al., 2007). In contrast, airborne measurements can cover regional scales on the order of 1-100 km and help bridge
60 spatial gaps in the data from chamber and tall tower measurements (Dacic et al., 2024; Pattey et al., 2007). Additionally, in combination with eddy covariance techniques, they further enable improved quantification of emissions from specific sources, which is particularly valuable for the complex and heterogeneous agricultural sector (Waldmann et al., 2026; Smith, 2017).

In the case of N₂O, previously used instruments for high precision N₂O measurements, such as the well established Gas Chromatographs (GCs) or Fourier transform infrared (FTIR) spectrometers with temporal resolutions in the order of 1 min,
65 are being replaced due to the improvement of laser-based measurement techniques and the growing commercial availability of laser spectrometers, allowing for precise (< 1 ppb) and simultaneously faster measurements (~ 1 Hz) (CCAC, 2024; Lebeque et al., 2016; Rapson and Dacres, 2014; Lopez et al., 2012). Particularly, the development of Continuous Wave (CW) Quantum Cascade Lasers (QCLs) working at room temperature opened new possibilities for fast, continuous, more sensitive and more feasible mid-Infrared (IR) absorption spectroscopy (Li et al., 2013; Capasso, 2010) making overly complicated and expensive
70 cooling systems on an aircraft redundant.

Several airborne N₂O in-situ studies using QCLs or other laser-based techniques have already been successfully conducted over the last two decades (Dacic et al., 2024; Eckl et al., 2021; Gvakharia et al., 2020; Kostinek et al., 2019; Gvakharia et al., 2018; Pitt et al., 2016; Xiang et al., 2013; Schiller et al., 2008). However, many of these studies report a temporal resolution of 1 Hz or less, which can be too slow for N₂O eddy covariance measurements on a fast aircraft. Furthermore, airborne measure-
75 ments still bear more challenges than ground based measurements. During a flight, several parameters may vary considerably, thereby affecting measurement performance. Pitt et al. (2016), Gvakharia et al. (2018) and Kostinek et al. (2019), for example, report dependencies on changes in cabin pressure, roll and pitch angles of the aircraft, and also water vapor (H₂O), which resulted in deviations of some ppb in N₂O. This can be difficult for the precise measurement of small N₂O variability (< 1 ppb) and could be particularly problematic for flights in highly humid regions. Therefore, possible dependencies must be known
80 and addressed by empirical corrections and specific calibration procedures. Furthermore, the space for the instrument setup onboard the aircraft is usually limited, resulting, e.g., in fewer possibilities to carry calibration gases which can impact the calibration procedure and, consequently, data quality.

Here, we present the performance assessment and evaluation of the DLR-MIRO system, a fast (10 Hz sampling frequency) airborne measurement setup specifically tuned for N₂O measurements with an in-flight precision of ~ 0.18 ppb enabling air-



85 borne eddy covariance measurements for N₂O (Waldmann et al., 2026). The core instrument of the setup is a commercially available Quantum Cascade Laser Absorption Spectrometer (QCLAS), namely a Multicomponent Gas Analyzer (MGA³), from the Swiss company MIRO Analytical AG. We assess the performance of the instrument during in-flight operation onboard two different research aircraft, a Cessna 208-B Grand Caravan operated by the German Aerospace Center (DLR) with an unpressurized cabin and NASA's Douglas DC-8 with a pressurized cabin. The Cessna was deployed on the Greenhouse Gas Monitoring (GHGMon) campaign in the Netherlands in June 2023. The DC-8 was deployed on the NASA Airborne and Satellite Investigation of the Asian Air Quality (ASIA-AQ) campaign in February and March 2024 over the Philippines, South Korea, Taiwan and Thailand. Flights were conducted in humid regions using repeated country-specific flight patterns and vertical profiles. Due to the high variability of H₂O (0-3%) in tropical environments, we focus on its impact on retrieved N₂O mole fractions. This is particularly important because the original fitting software version v1 did not account for H₂O effects, including both dilution and quantum-mechanical processes such as line broadening. To address this, we derive an empirical water vapor correction based on dedicated laboratory experiments. The results obtained with this correction are compared with those from an updated MIRO fitting software v2, which incorporates a water vapor correction derived from the same experimental dataset from the laboratory. We evaluate and discuss the advantages and limitations of both approaches, including an assessment of the MGA³ H₂O measurements themselves and the importance for their overall accuracy.

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100 This study is structured as follows: In section 2, we present the specifications of our MGA³ instrument and the airborne setup, which was identical for both the NASA DC-8 and the DLR Cessna Grand Caravan. We describe the calibration procedure, the basics of the retrieval software v1 of the MGA³ and elaborate on the relevant parameters for fitting the measured spectra, such as the width of absorption line (β). In Section 3, we first provide an overview of the different water vapor correction approaches applied in this study and describe the laboratory experiment used to derive corresponding parameters for the correction equation. In the next step, we compare the MGA³ H₂O-measurements to NASA's established Diode Laser Hygrometer (DLH) H₂O-measurements to derive an even more precise water vapor correction. We compare our empirical water vapor correction approaches with a new software version v2 that already implements a water vapor correction based on the same conducted laboratory experiment. We also compare our H₂O-corrected N₂O-measurements with N₂O-measurements conducted by NASA's established Differential Absorption Carbon monoxide Measurements (DACOM) spectrometer (Sachse et al., 1987), a Tunable Diode Laser Absorption Spectrometer (TDLAS) which was also onboard the DC-8 during the ASIA-AQ campaign. In Section 4, we assess the stability of the MGA³ under ground conditions by calculating its Allan precision and investigate potential dependencies of N₂O-measurements on cabin pressure and roll and pitch angles of the aircraft during flights. In section 5, we present selected flight data from the ASIA-AQ campaign corrected using the different water vapor correction approaches. Finally, we show examples of ambient N₂O measurements from GHGMon and ASIA-AQ to demonstrate the capabilities of the MGA³ airborne setup under in-flight conditions.

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Table 1. Wavenumbers and HITRAN isotopologue numbers of the absorption lines of the target species of laser 1 and laser 2 of the MGA³.

	wavenumber cm^{-1}	isotopologue number	laser
N ₂ O	2190.35	446	laser 1
CO	2190.02	26	laser 1
CH ₄	1281.61	211	laser 2
H ₂ O	1281.53	162	laser 2

2 Operational Design

At both the GHGMon and the ASIA-AQ campaign, we operated the same DLR-MIRO setup with a commercially available QCLAS, namely the Multicomponent Gas Analyzer (MGA³) by the MIRO Analytical AG from Switzerland, as its core instrument. The setup is specifically optimized for N₂O measurements with the capability for the eddy covariance method and up to altitudes of approximately 5.5 km. In the following sections we first describe the specifications of the MGA³, its integration into the airborne instrument setup, and the data calibration procedure. To provide a better context for our water vapor correction approach, Section 3 outlines the basic theory of spectral fitting and introduces the most important parameters for the water vapor correction as well as the method used by the MGA³ mole fraction retrieval software.

2.1 Instrument specifications of the MIRO MGA³

The MGA³ is a two-laser (Alpes Lasers; St. Blaise, Switzerland) QCLAS and is able to measure three species at once - N₂O, CH₄, and CO - in addition to H₂O, all within one Herriot measurement cell with a volume of 0.44 L and an optical path length of 76 m. The wavenumbers scanned by the first laser (laser 1) are 2191.38 cm^{-1} -2189.85 cm^{-1} and the wavenumbers of the second laser (laser 2) are 1282.50 cm^{-1} -1281.01 cm^{-1} (see Table 1). The MGA³ is specifically optimized for N₂O measurements by the selection of the spectral absorption lines and the settings defined by the manufacturer. The maximum time resolution of the data retrieval of the instrument is 10 Hz.

The QCLs are driven by an intermittent Continuous Wave (iCW) driving scheme with pulse durations of 10-100 ns and an overall period of about 0.5-1 ms. The temperatures of the lasers are held constant at around 32 °C (laser 1) and -2 °C (laser 2) by ThermoElectric Coolers (TECs). For further general information on the MGAs by MIRO Analytical, please find the paper of Hundt et al. (2018).

2.2 Airborne setup

For the complete functional airborne setup, the MGA³ requires additional structural components and peripheral devices. First, a liquid chiller (Thermorack401, Solid State Cooling Systems, Wappingers Falls, USA) provides the heat reservoir for the optical compartment of the MGA³ and the TECs cooling the lasers within the compartment (see section 2.1) as can be seen in Figure 1. The MGA³ has two inlets, one sample air inlet and one calibration gas inlet. When measuring sample air from outside

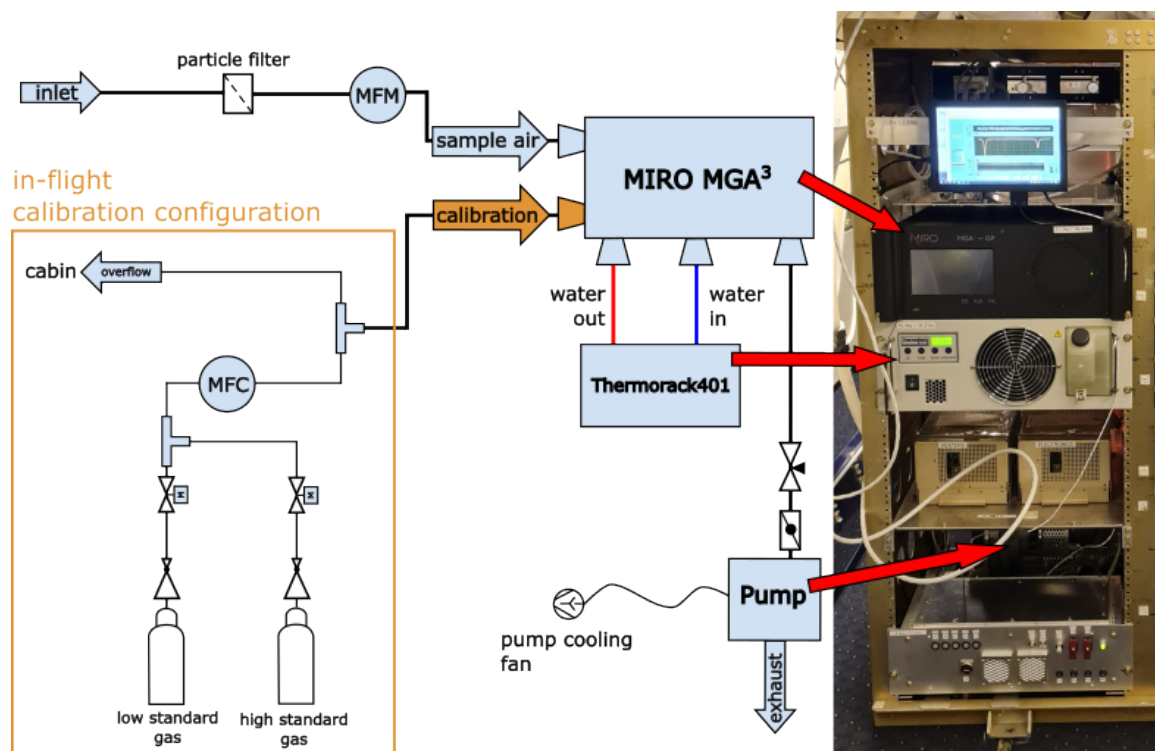


Figure 1. Setup of the instrumentation for both the 2023 GHGmon campaign and the 2024 ASIA-AQ campaign. The left side shows a scheme of the setup including the calibration setup within the orange box. The right side contains a photo of the setup onboard NASA’s DC-8 during ASIA-AQ.

140 the DC-8 aircraft, the air is first drawn through a rear-facing 62 degree trapezoid inlet at the hull of the aircraft and then directed through an about 6.5m long PTFE tube with a diameter of 1/2in to a 2 μ m PTFE-membrane particle filter (filter membrane: R2PJ047 Pall, filter holder: PA1235 Pall). For the Cessna, the PTFE tube was approximately 5.5 m long and installed through the wing of the aircraft and through its attached wingpod. After filtering the sample air passes a Mass Flow Meter (MFM) (F-102E, Bronkhorst) before it enters the MGA³ through its sample air inlet. A scroll pump (IS500C, Anest Iwata) connected to the outlet of the MGA³ is used for creating a vacuum which draws the sample air in. The pump was specifically selected to generate the highest possible mass flow without exceeding the Cessna’s power constraints. In this instrument setup with the long inlet tubing, the pump generated a mass flow of 12.5slpm-13.8slpm. The pump motor is additionally cooled with a standard external fan to prevent overheating. Given the MGA³ cell volume of 0.44L and a cell pressure of 70 hPa this corresponds to an effective sampling frequency of 6.85-7.57 Hz, assuming plug flow. To achieve higher mass flows, and therefore higher effective

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150 sampling frequencies, we recommend minimizing the distance between the aircraft inlet and the instrument.

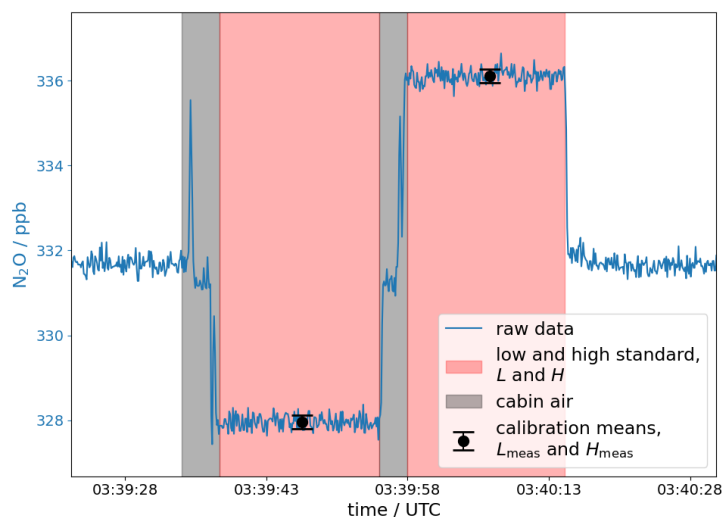


Figure 2. Example of an in-flight two-point calibration from the ASIA-AQ campaign. When a calibration sequence is activated first an internal valve of the MGA³ switches from the sample air inlet to the calibration gas inlet. Then, during the first time span (gray area), cabin air is drawn in via the overflow of the calibration system. Shortly after the solenoid valve for the low standard calibration gas L is activated for about 20s allowing the gas to be drawn in by the MGA³ (first red area). Then the solenoid valve closes and cabin air is shortly drawn again (second gray area) until the second solenoid valve activates for the high standard calibration gas H (second red area). In total the calibration process lasts for about 40s. The black dots are the mean values L_{meas} and H_{meas} of L and H with their respective errors, which are then used for the calibration to relate to the known reference values of the calibration gases.

2.3 Calibration of data and response time

In this section, we describe the calibration procedure applied to our data to account for drifts and potential changes in the sensitivity of the MGA³ and determine the response time of the system. To avoid drift and sensitivity effects of GHG measurements and to improve the accuracy of the retrieved mole fractions, the instrument needs to be regularly calibrated in-flight using a two-point calibration. For this, the MGA³ switches an internal valve and then draws air not from the sample air inlet but from the calibration gas inlet which is connected to an in-flight calibration system (see Figure 1, orange box). As can be seen from the measurements in Figure 2, as an example from ASIA-AQ, every 10min two calibration gases are drawn, a low-standard calibration gas L and a high-standard calibration gas H , each for 20s in sequence. Two solenoid valves are operated directly from the MGA³ software and they control which of the two gases is currently being used. The red areas show the L and H standards, and the grey areas show when cabin air is sampled through the overflow while switching the main MGA³ valve from the sample air inlet to the calibration gas inlet. When the main valve of the MGA³ switches to cabin air in the first grey area or when the solenoid valves switch to the calibration gases, the initial high pressure coming from the cabin or the cylinders results in a feedback behavior leading to a time of 1-2s for the cell to be completely flooded by the cabin air or the calibration gases. When switching the valves back to the cabin air in the second grey area in Figure 2 or back to ambient sampling air after the



Table 2. Mole fraction values of each high and low standard gas pair for the GHGMon and ASIA-AQ campaign.

	N ₂ O low standard / ppb	N ₂ O high standard / ppb
GHGMon 1	344.85	347.35
GHGMon 2	344.63	346.65
ASIA-AQ 1	333.99	342.23
ASIA-AQ 2	330.47	340.65
ASIA-AQ 3	331.32	339.03

165 second red area, this effect does not occur. With these two cases we determine our response time of 0.1-0.2s which confirms
our effective sampling frequency of approximately 7Hz determined with the mass flow through the cell in Section 2.2. More
details on the calibration times will be shown in Section 4.1. The Mass Flow Controller (MFC) (F-201CV, Bronkhorst) behind
the solenoid valves is set to a higher flow than the instrument consumes (15slpm) and any excess flow of the calibration gases
in front of the MGA³ inlet is released to the cabin via an overflow. All in-flight calibration gas standards for N₂O are chosen to
170 be close to the atmospheric background mole fractions and were themselves calibrated on the ground against NOAA-standards
(traceable to the NOAA-N2O_X2006A reference scale). In Table 2, the N₂O mole fractions of the two different high and low
standards used during the GHGMon campaign and the three different high and low standards used during the ASIA-AQ cam-
paign are shown. High and low standards were chosen to have a difference of 10-20ppb to be able to cover the small variability
in N₂O caused by agricultural emissions.

175 To calculate the calibrated time series $X_{\text{cal}}(t)$ out of a measured raw data time series $X_{\text{raw}}(t)$ that is provided by the MGA³,
we first calculate a scale factor m_n and an offset d_n for each calibration cycle $n = 1, \dots, N$ for all $N \in \mathbb{N}$ cycles, according
to Pitt et al. (2016) with:

$$m_n = \frac{H_{\text{true}} - L_{\text{true}}}{H_{\text{meas},n} - L_{\text{meas},n}}, \quad n = 1, \dots, N; N \in \mathbb{N} \quad (1)$$

$$d_n = H_{\text{true}} - m_n \cdot H_{\text{meas}}. \quad (2)$$

180 Here $H_{\text{meas},n}$ and $L_{\text{meas},n}$ are the means of the measured values for the high and low standards H and L as shown for one
calibration cycle n in Figure 2. H_{true} and L_{true} represent their known true mole fractions in Table 2. We interpolate the scale
factors m_n and offsets d_n between every calibration cycle for every time point t in the measured time series $X_{\text{raw}}(t)$ and get
the continuous scale factor $m(t)$ and offset $d(t)$ which lead us to the calibrated values $X_{\text{cal}}(t)$:

$$X_{\text{cal}}(t) = m(t) \cdot X_{\text{raw}}(t) + d(t). \quad (3)$$

185 For our H₂O measurements, we only use a one-point-calibration, since both L and H standards are dry and should not contain
any H₂O. Here, we calculate the difference d_n between the mean $V_{\text{meas},n}$ of a measured calibration cycle of only one of the



two cylinders and its known actual value V_{true} . We obtain the calibrated value $X_{\text{cal}}(t)$ by interpolating d_n for every t to $d(t)$:

$$d_n = V_{\text{true}} - V_{\text{meas},n} \quad n = 1, \dots, N; N \in \mathbb{N} \quad (4)$$

$$X_{\text{cal}}(t) = X_{\text{raw}}(t) + d(t). \quad (5)$$

190 For the uncertainty of our cylinders we use the standard error for every mean calculated from the L and H standards in the calibration cycles resulting in uncertainties below 1 ppb. Experience from GHGMon showed that the respective differences between the standards of about 3 ppb in N_2O were too small causing issues while calibrating the data, especially with the error calculation for the calibration procedure. Based on this and the later experience from ASIA-AQ flights, we recommend that the differences between the high and low standards including the errors of the cylinder values should be at least two orders of
195 magnitude higher than the precision of the MGA³.

2.4 MGA³ mole fraction retrieval software and versions

In this section, we explain how the MGA³ software retrieves the mole fraction values C from its measurements. The lasers of the MGA³ emit light in a wavenumber range close to the absorption lines of the target species such as N_2O . The laser beam is directed into the measurement cell where the target sample air is located. There, the intensity I_0 of the laser beam
200 weakens through absorption by the sample air. After the laser beam exits the cell, it illuminates a detector which measures the intensity I along the wavelengths, i.e. the absorption spectrum and therefore the absorption line profile of the N_2O . Each measured spectrum is then provided as the transmittance $\tau(\nu)$ by the MGA³. The measured absorption line profile can either be fitted online while measuring or later on at any time with the MGA-ReFit software. The lines are fitted by minimizing the sum of least-squares using the Beer-Lambert law, which in this case is based on a Voigt profile:

$$205 \quad \tau(\nu) = \frac{I(\nu)}{I_0(\nu)} = \exp(-\alpha(\nu, p, T) \cdot N_0(p, T) \cdot L \cdot C). \quad (6)$$

Here N_0 is the Loschmidt constant and ν represents the wavenumber. By knowing the pressure p , the temperature T and the optical path length L of the measurement cell, the software can calculate the absorption coefficient α and the mole fraction C of the measured species (Hundt et al., 2018). The absorption coefficient α represents the shape of the Voigt profile for a specific molecule including the Half-Width-Half-Maximum (HWHM) of its absorption line profile if only one such molecule
210 is observed (see Appendix A). The mole fraction C then scales α for more than one molecule.

In this paper we use two different versions of the MGA³ fitting software. The original software of our MGA³ model, which we denote as version 1 (v1) (V30.0.171.0), does not correct for water vapor dependencies. That means that it fits each measured absorption line applying Equation 6 and calculates the mole fraction C , but does not account for dilution and it cannot account sufficiently enough for all quantum-mechanical effects, such as water vapor line broadening, on the data, since not all processes
215 are known or can be determined. To correct for these water vapor dependencies we conducted a water vapor experiment in the laboratory which we use to determine an empirical water vapor correction as shown in Section 3. This correction is then applied during the data post-processing to the already retrieved C time series. In parallel, an updated version of the fitting software was developed by MIRO Analytical. The new version is based on the same laboratory experiment and now includes a correction



for water vapor dilution and broadening effects already implemented in the fitting process of the spectra. The software version
220 (V30.1.59.0) is in the following referred to as version 2 (v2). The resulting v2 time series of the retrieved mole fractions C
does not longer require the postfit corrections as in v1.

2.5 Fitting with constant HWHM - the β option

For the software version v1, the MGA³ has the option to activate or deactivate the β , which is, within the MIRO software, an
internal measure for the HWHM of each absorption line and therefore for the absorption coefficient α (see Appendix A). If
225 the β is deactivated, the MGA³ freezes the HWHM of the respective absorption line for all upcoming spectra and uses the last
used value when the β was still active. This means, however, that consequently the mole fraction C in the fitting function 6
has to account for any changes that would occur in α . This leads to deviations from the actual values in C . However, with high
water vapor contents in the sample air, as we show in Appendix A, the HWHM solely depends on water vapor for our N₂O
spectral line. Based on this, the mole fraction C time series with a frozen β can subsequently be corrected by an empirical
230 water vapor correction. In the following, we denote this water vapor corrected data as v1- β -off. To enforce the same behavior
for all v1- β -off refit-processes as much as possible, we deactivate the β always when dry gas is measured and therefore no
water vapor should be present.

At this point, the mole fractions retrieved by v1- β -off should not differ compared to water vapor corrected data retrieved
with v1 and an activated β - from here on denoted as v1- β -on. However, due to the α being kept constant in v1- β -off the fitting
235 software has one parameter less to account for in the fitting process which results in less numerical noise in C compared to
v1- β -on. Software version v2 does not have a β option an already corrects for water, and therefore will be simply denoted
as v2. These correction approaches will now be discussed in more detail in the next Section 3.

3 Water vapor correction approaches of N₂O in this study

Water vapor is highly variable in the atmosphere with 1-10ppm in the Upper Troposphere - Lower Stratosphere (UTLS)
240 (Kaufmann et al., 2016) and even up to 30000ppm within the tropical boundary layer as shown in Figure 5 from the ASIA-AQ
measurements. Due to this high variability of water vapor in different regions of the world and its volatility, GHG measurements
are usually reported in dry mole fractions for better comparability, which requires precise water vapor measurements at all
times. The first step is to eliminate the dilution from the gas due to the present H₂O by using the following equation:

$$C_{\text{dry}} = \frac{C_{\text{wet}}}{1 - C_{\text{H}_2\text{O}}}. \quad (7)$$

245 Here, C_{wet} denotes the mole fraction of N₂O diluted by H₂O. $C_{\text{H}_2\text{O}}$ is the mole fraction of the H₂O and C_{dry} represents the
mole fraction of N₂O in the gas mixture after the removal of H₂O. However, additional spectroscopic effects, such as water
vapor line broadening, or instrument-specific behaviors in the measurements can have an impact on the data if not accounted
for correctly or not at all. Those effects then often have to be corrected by using an empirical water vapor correction, also
specific to each instrument (e.g. Pitt et al. (2016) and Gvakharia et al. (2018)).



250 Since the original MGA³ software v1 does not provide a water vapor correction, neither for dilution nor completely for spectroscopic effects, we first derive an empirical water vapor correction from a laboratory experiment, further described in Section 3.1. With the parameters a_0 and b_0 determined from a quadratic function in the laboratory, we apply the following water vapor correction equation also used by Rella et al. (2013) to account for all potential H₂O dependencies:

$$C_{\text{dry}} = \frac{C_{\text{wet}}}{a_0 \cdot C_{\text{H}_2\text{O}}^2 + b_0 \cdot C_{\text{H}_2\text{O}} + 1}, \quad (8)$$

255 which we will explain more thoroughly in Section 3.2. In the following, we shortly introduce how we attain four water vapor corrected mole fraction data sets, retrieved from a single measured spectral data set, by different approaches.

v1- β -on

The wet mole fractions C_{wet} for N₂O and $C_{\text{H}_2\text{O}}$ for H₂O are retrieved by the software version v1 and with an activated β . The time series C_{wet} is then water vapor corrected to obtain C_{dry} by using Equation (8). The data for the lab experiment from
260 which we derive our correction is also fitted with the software version v1 with an active- β (see Section 3.1).

v1- β -off

This approach is identical to v1- β -on except that the β is deactivated during all fitting and retrieval processes by the MGA³ software.

v1- β -off-DLH

265 A precise water vapor correction approach requires precise water vapor measurements. Hence, for this specific approach, we first retrieve the wet mole fractions C_{wet} for N₂O and $C_{\text{H}_2\text{O}}$ for H₂O with a deactivated β , as for v1- β -off, and then compare our MGA³-H₂O measurements to the H₂O measurements made by NASA's well established Diode-Laser-Hygrometer (DLH) at the ASIA-AQ campaign (Diskin et al., 2002). Thereby, we checked the stability of the MGA³ water vapor measurements over multiple flights and adjusted the MGA³-H₂O measurements accordingly to the DLH-H₂O measurements to achieve the
270 same standard for the MGA³-H₂O measurements over all the flights (see Section 3.3 for more details). The mean behavior of the MGA³-H₂O measurements of all flights compared to the DLH-H₂O measurements is also used to calibrate the the MGA³-H₂O measurements from the laboratory experiment from which the water vapor correction is derived. Then the DLH-adjusted $C_{\text{H}_2\text{O}}$ and the DLH-adjusted correction function from the laboratory experiment are used for correcting C_{wet} to C_{dry} using the correction function (8).

v2

In this approach, we use the newly implemented MGA³ retrieval software v2 which already includes a water vapor correction based on the same laboratory experiment as used for the previous approaches. The water vapor correction, however, is applied already while fitting the spectra and not after the N₂O mole fraction C_{wet} is retrieved. Here, the H₂O spectra are directly used to

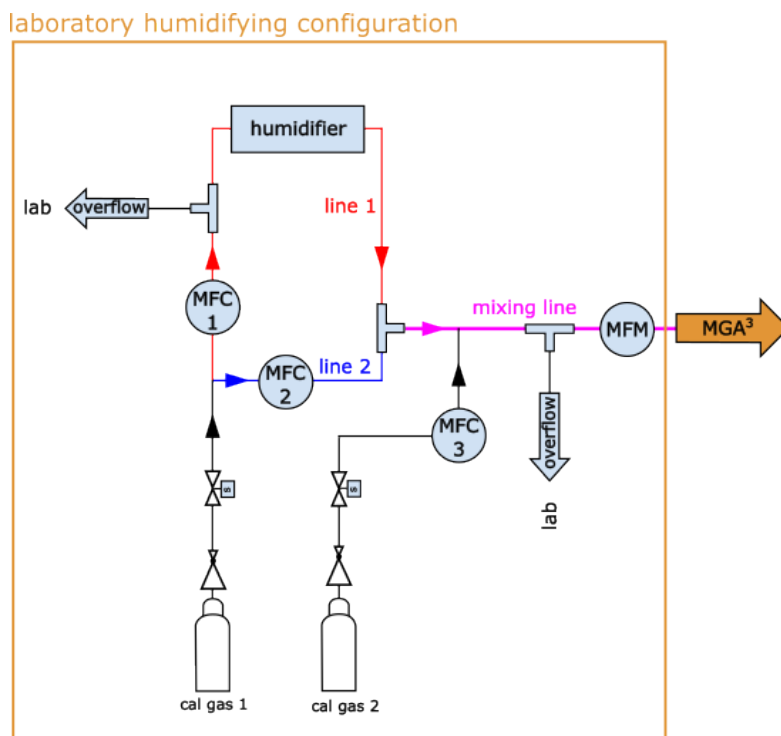


Figure 3. Scheme of the setup of the water vapor laboratory experiment. To fully function the orange box gets exchanged with the orange box of the in-flight calibration configuration in Figure 1.

correct the N_2O spectra and directly report corrected C_{dry} mole fractions. The H_2O spectra or measurements are not adjusted
 280 to the DLH measurements beforehand as for v1- β -off-DLH.

3.1 Laboratory Experiment

In this chapter, we explain the setup of the laboratory experiment for the water vapor correction, how we conducted it and how we prepared the data retrieved from this experiment for the water vapor correction equation. For the laboratory experiment, we change the calibration system in Figure 1 from the "in-flight calibration" configuration to the "laboratory humidifying"
 285 configuration in Figure 3 and only use the calibration gas inlet of the MGA³ throughout the whole experiment. The sample gas is provided by a gas cylinder (cal gas 1) and is first divided into two sub-lines, which are controlled by a mass flow controller each. One sub-line (line 1) is provided only 3slpm by its mass flow controller (MFC 1), since the humidifier (Dew Point Generator LI-610, LICOR) only operates with mass flows up to 2.5slpm. The excess gas in line 1 is then released through the overflow behind the MFC 1 to protect the humidifier. The output of the humidifier is controlled in a range of 0slpm-2.5slpm
 290 with a valve on the humidifier itself. The second sub-line (line 2) is provided with 0slpm-5slpm by the MFC 2 which directly merges with the humidified output from line 1. The length of the mixing line is 1.5m to allow for optimal mixing of dry gas

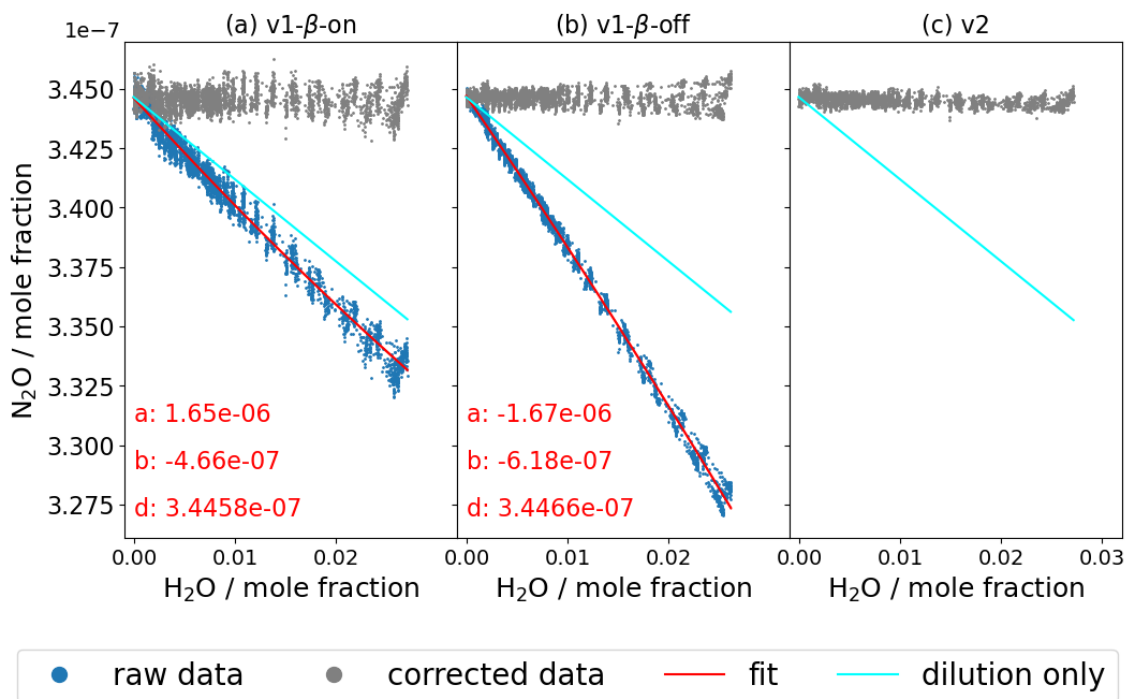


Figure 4. In (a) and (b) we can see the behavior of the raw N_2O with increasing H_2O mole fractions (blue dots) during laboratory water vapor experiment for $v1-\beta\text{-on}$ and $v1-\beta\text{-on}$. The red lines are fitting functions giving us the parameters for our water vapor correction function in section 3.2. The cyan line shows the expected behavior of the raw mole fractions if only dilution was having an effect on the measurements. The grey dots are the blue dots corrected by the water vapor correction function (17) in section 3.2. In (c) the grey dots represent the raw mole fraction output of the experiment when reprocessed with version v2 of the MGA-ReFit software. The data were already corrected for water vapor influences based on the same data in (a) and (b) while they were being reprocessed.

and humidified gas. The merged gas then directly flows into the MGA^3 , which is set to operate with a mass flow of 1.9slpm for this experiment. The excess gas in the mixing line is released through an overflow in front of the MGA^3 . The second gas, cal gas 2, is used only for calibration purposes. The settings are the same as in the airborne setup at the GHGMon and the ASIA-AQ campaigns (see Section 2.2) with a cell pressure of 70 hPa and a cell temperature T of 25 °C.

For the experiment, the MFC 2 is first set to 5slpm and the humidifier output to 0slpm, allowing only for the dry gas from cylinder 1 to be sampled. Then, the output of the humidifier is increased stepwise from 0slpm to 2.5slpm, increasing the mole fraction of water vapor in the mixing line. Once the maximum mass flow for the humidifier output is reached, the mass flow of MFC 2 is incrementally decreased from 5slpm to 0slpm, further increasing the humidity in the merged gas until only the output from the humidifier is sampled. Thereby, a range of water vapor mole fractions of 0-3% is covered. This process of humidifying is repeated four times. Before and after each repetition, the gas from cylinder 2 is sampled for calibration purposes.



The recorded spectral data are then refitted with three different water correction approaches. Twice with the original software version v1 (once with an activated β and once with a deactivated β) and once with the updated version v2. Figure 4 shows the retrieved N_2O mole fractions from all those three approaches versus the retrieved H_2O mole fractions after calibrating the time series to the dry cylinder gases. As obvious from Figure 3 (a) and (b) for v1, the uncorrected N_2O (blue dots) mole fraction varies by more than 10-18 ppb in humid versus dry conditions. The cyan line gives the expected impact of the dilution effect only compared to dry conditions. In (a) and (b) the measured raw data deviate from the expected behavior due to spectroscopic effects, which not all can be accounted for by the software in general. Furthermore, we only use an one-point calibration for the H_2O measurement, which could be a reason for the deviations from the cyan line. Since we use dry calibration gas in both cylinders, we cannot account for changes in sensitivity of the H_2O measurements for values above 0. With the deactivated, frozen β in v1 the deviation is larger than with the activated β -on since the water vapor line broadening is not accounted for in this setting (see Section 2.5). Figure 4(c) shows the mole fractions retrieved with the updated software version v2, in which the N_2O mole fractions are already corrected for water vapor during the fitting process of the measured spectra (grey dots). For the raw data in Figure 4(a) and (b) we first have to derive a correction which leads us to the corrected data sets v1- β -on and v1- β -off (grey dots). This, we show in the next Section 3.2.

3.2 Water Correction Function

In the next step, we correct the raw N_2O data in Figure 4(a) and (b) and derive a water vapor correction function. For this, the wet raw data $C_{\text{lab,wet}}$ given in Figure 4(a) and (b) are fitted with a quadratic function (red line), giving us the parameters a , b , d :

$$\text{fit}(C_{\text{H}_2\text{O}}) = a \cdot C_{\text{H}_2\text{O}}^2 + b \cdot C_{\text{H}_2\text{O}} + d. \quad (9)$$

Here, $C_{\text{H}_2\text{O}}$ is the H_2O mole fraction. In an ideal fit, the parameter d represents the actual value of the dry cylinder mole fraction for $C_{\text{H}_2\text{O}} = 0$ and therefore simultaneously the dry target value after the water vapor correction is applied for all $C_{\text{H}_2\text{O}}$. To obtain the water vapor corrected mole fraction $C_{\text{lab,dry}} = d$ for N_2O in this laboratory experiment, the value of the correction function 9 is subtracted without the parameter d from $C_{\text{lab,wet}}$:

$$C_{\text{lab,dry}} = C_{\text{lab,wet}} - (a \cdot C_{\text{H}_2\text{O}}^2 + b \cdot C_{\text{H}_2\text{O}}). \quad (10)$$

However, the parameters of this fit function apply only for the specific mole fraction d of the used cylinder and not necessarily for cylinders with random mole fractions C_{dry} . If a humidified air sample containing no N_2O were sampled, these specifically determined parameters would still produce a correction value for the corresponding $C_{\text{H}_2\text{O}}$, despite the absence of the N_2O . To account for any other values C_{dry} in the cylinder, we use following boundary condition:

$$C_{\text{dry}} = 0 \Leftrightarrow \text{fit}_x(C_{\text{H}_2\text{O}}) = 0 \quad \forall C_{\text{H}_2\text{O}} > 0 \quad (11)$$

$$\Rightarrow a, b, d = 0 \quad (12)$$



and assume that the parameters a , b and c - consequently the fit Equation 9 - approach 0 proportionally with decreasing mole fractions C_{dry} , giving:

$$a = \frac{a-0}{d-0} \cdot C_{\text{dry}} = \frac{a}{d} \cdot C_{\text{dry}} = a_0 \cdot C_{\text{dry}}, \quad (13)$$

$$335 \quad b = \frac{b}{d} \cdot C_{\text{dry}} = b_0 \cdot C_{\text{dry}}, \quad (14)$$

$$d = \frac{d}{d} \cdot C_{\text{dry}} = d_0 \cdot C_{\text{dry}} = C_{\text{dry}}, \quad (15)$$

$$C_{\text{dry}} = C_{\text{wet}} - (a_0 \cdot C_{\text{dry}} \cdot C_{\text{H}_2\text{O}}^2 + b_0 \cdot C_{\text{dry}} \cdot C_{\text{H}_2\text{O}}). \quad (16)$$

C_{wet} is the measured wet mole fraction of N_2O using the new cylinder with C_{dry} . The fit parameters in (13)-(15) are now dependent on the mole fractions C_{dry} in the cylinder and from equation (16) we get:

$$340 \quad C_{\text{dry}} = \frac{C_{\text{wet}}}{a_0 \cdot C_{\text{H}_2\text{O}}^2 + b_0 \cdot C_{\text{H}_2\text{O}} + 1}, \quad (17)$$

which can finally be used for any random measurement C_{wet} with a simultaneously measured $C_{\text{H}_2\text{O}}$. Equation 17 is the same as the one used by Rella et al. (2013), also with the assumption that the water vapor correction is proportional to the mole fraction of our observed species.

The correction Equation (17) is then applied to the raw data in Figure 4(a) and (b) and results in the grey corrected data
 345 v1- β -on and v1- β -off. With this, our retrieved data is corrected for water vapor and influences and should be independent of water vapor changes either by dilution or spectral effects like line broadening. The main difference between the β -on and β -off retrieved data is that the noise in the data for the β -off data is smaller (see Section 2.5) by roughly 70% compared to its respective β -on retrieved data, which will be discussed in Section 3.5 in more detail.

3.3 H₂O calibration against DLH absolute ambient measurements

350 The quality of the water vapor measurement is decisive for a precise water vapor correction. While the absolute accuracy is not of main importance, the stability of the water vapor measurement is, hence, the replicability of the H₂O measurements over time. To analyze the stability of the MGA³-H₂O measurements in our setup, we compare data from 14 flights from the ASIA-AQ campaign with absolute ambient H₂O vapor measurements measured by the established DLH. We use the DLH because it reliably reports stable water vapor measurements which can be used to effectively correct the MGA³ water vapor
 355 measurements. In our airborne measurement setup the MGA³ is only calibrated by an one-point calibration using our dry cylinder gases (see Section 3.1), leading to differences in the data between the two instruments. In Figure 5(a) the DLH-H₂O for each of the 14 flights is plotted against the respective MGA³-H₂O data for the β -off setting. The flights were conducted over a time span of roughly two months. The lines are polynomial fits (second order) of the measurements, calculated by applying orthogonal distance regressions. The dashed red line shows a slope of 1. The dashed black line shows the mean of all curves,
 360 which is also a quadratic function described with $f(x) = ax^2 + bx + d$. The difference in the length of every curve is due to the differences in the maximum measured humidity during each flight.

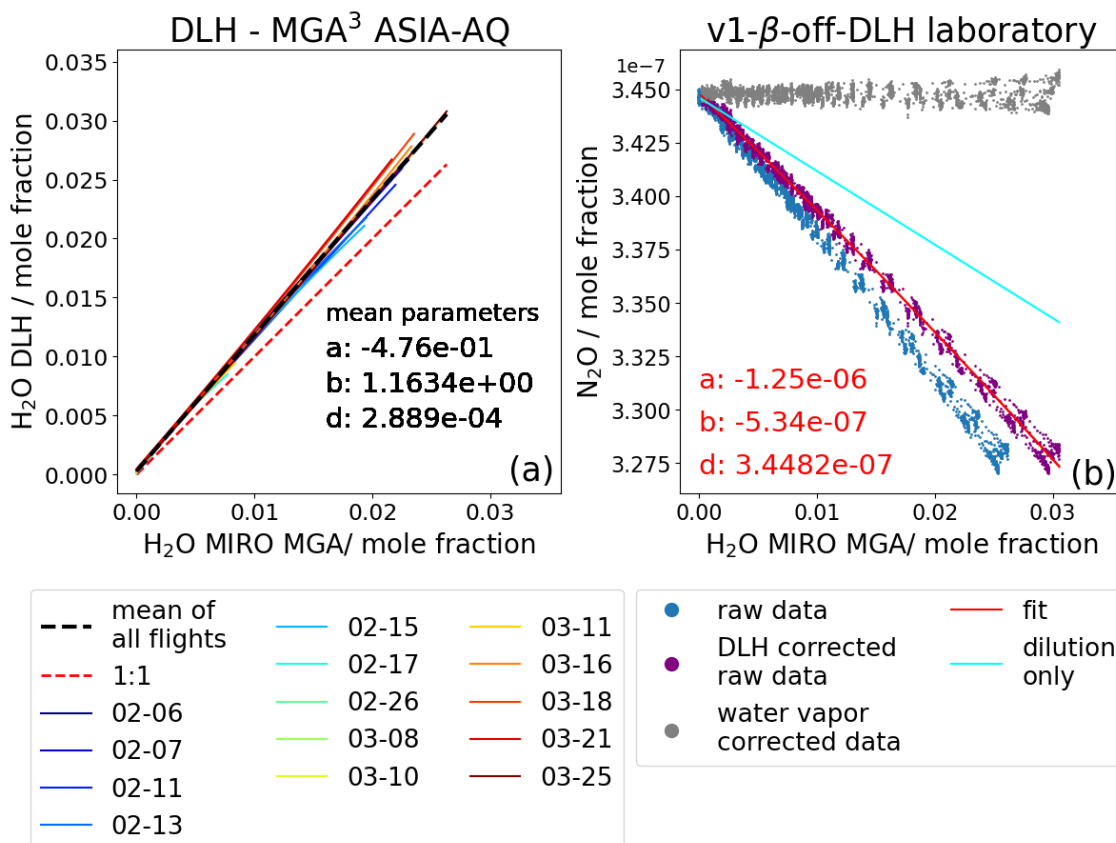


Figure 5. In (a) we plotted the DLH-H₂O measurements against the MGA³-H₂O measurements for the mole fractions retrieved with v1 with a deactivated β for 14 ASIA-AQ flights from February 6th to March 25th. In general, our instrumental setup measured less H₂O than DLH. With increasing H₂O the MGA₃ measurements seem to deviate more from each other indicating changes in sensitivity of the instrument. The black dashed lines show the mean for all flights. Figure 5(b) shows again the same as Figure 4 (b) but now the blue raw data is first corrected by the respective dashed black line in Figure 5(b) resulting in the "DLH-corrected" purple dots. The red lines are now the fitting lines for the purple data, which parameters now can be used to derive the new correction v1- β -off-DLH.

In general, the DLH measures about $b = 1.16$ times higher H₂O values than the MGA₃ with our instrumental setup, which is mainly due to not being able to conduct a two-point-calibration as mentioned. Other minor reasons could be, for example, water vapor tube dampening effects through the long 6.5 m PTFE inlet tubing in our setup. At the instrument flow rate of approx. 13 slpm, it takes about 2 s at 1 atm until the sample air reaches the measuring cell, during which water vapor could attach and slowly unstick from the inner tubing walls. Still, the results show that the correlation of both H₂O measurements for the flights diverge for higher H₂O values, indicating changes in the sensitivity. In principle, this can only be accounted for by a sufficient two-point-calibration as explained in Section 3.2. The changing behavior over the flights, however, means that



Table 3. Percentage of how many data points of the DACOM measurements overlap with MGA³ data with different water vapor correction approaches applied within the combined uncertainties at 5 Hz.

flight	v1- β -off / %	v1- β -off-DLH / %	v2 / %
2024-03-25	74.5	74.4	60.8
2024-03-21	53.1	79.4	55.9
2024-03-18	70.1	82.3	62.1

the once attained correction equation in the laboratory will behave slightly differently for every flight unless the MGA³-H₂O is not standardized to a norm.

To account for this variability in behavior of the MGA³-H₂O from flight to flight, we constructed a new correction specifically for all the ASIA-AQ flights in addition to the already existing v1- β -off approach in chapter 3.2, called v1- β -off-DLH, which can be seen in 5 (b) (grey dots). First, since the H₂O measurement in the laboratory water vapor experiment cannot be calibrated against absolute reference values - due to our used humidifying configuration setup not being able to provide such an accurate value - we assume that the H₂O behavior in the experiment is similar to the mean behavior of all flights (dashed black line in Figure 5(a)). Thus, we correct our laboratory experiment H₂O values with this mean (see Section 3.4 for explanation). This results in the purple DLH corrected data in Figure 5(b). We can see that the DLH adjusted N₂O raw data is closer to the cyan line which represents the ideal behavior if only dilution existed. Now, the fit (red line) is used for deriving the parameters of our water vapor correction in the same way as for v1- β -off. However, before the correction function is applied to the flight data, we first correct the H₂O flight measurements with their respective line in Figure 5(a) to assure, that all flight measurements and the laboratory H₂O measurements are "calibrated" to the same standard, which in this case are the DLH measurements. Now, the water vapor correction function can be applied to the flight data giving the water vapor corrected mole fraction data. This approach is denoted as v1- β -off-DLH.

In the next section, we compare the results from the different correction approaches v1- β -off, v1- β -off-DLH and v2.

3.4 Comparison of the different water correction approaches

In this chapter, we compare the data retrieved by the different MGA³ software versions and water correction approaches v1- β -off, v1- β -off-DLH and v2 with the data measured by NASA's established DACOM spectrometer. The DACOM is a TDLAS designed for CO measurements but it also measures CH₄ and N₂O. It has a temporal resolution of 5 Hz and dries the sample air via a Nafion tube before sampling, negating water vapor interference and dilution effects. Our calibration cylinders for the MGA³ were cross calibrated against the NOAA calibration cylinders of DACOM. This makes the DACOM measurements ideal for the validation of our water vapor correction approaches for the MGA³-N₂O measurements. For a better comparison, the MGA³ data was resampled to 5 Hz to match the DACOM data. We chose to compare three flights in Thailand for which data from both instruments are available, well calibrated and, most importantly, high H₂O variability was measured.

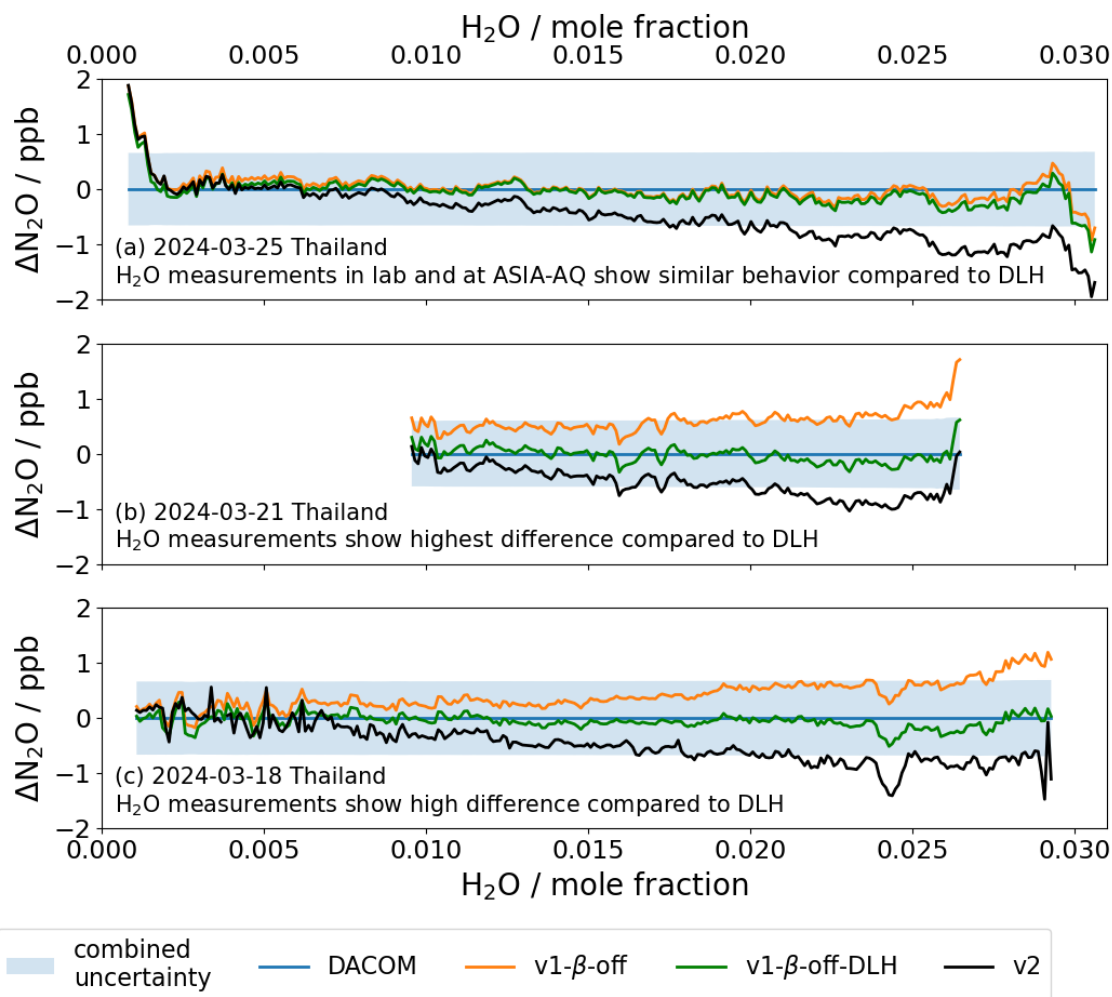


Figure 6. Differences between N_2O data measured by DACOM and the MGA^3 for the different water vapor correction approaches $v1-\beta$ -off, $v1-\beta$ -off-DLH and $v2$ for three ASIA-AQ flights on the 2024-03-25 (a), 2024-03-21 (b) and 2024-03-18 (c). The colored lines show the mean values of the differences between DACOM and the MGA^3 corrected data in 0.01 % or 100 ppm H_2O bins. The shaded blue areas represent the combined uncertainties of DACOM and the MGA^3 with $v1-\beta$ -off-DLH but at full resolution and not with the 0.01 % bin resolution.

Figure 6(a), (b) and (c) illustrates the difference between the DACOM- N_2O data and the MGA^3 - N_2O for three selected ASIA-AQ flights (2024-03-25, 2024-03-21 and 2024-03-18). Different colors represent data retrieved using the different MGA^3 approaches ($v1-\beta$ -off in orange, $v1-\beta$ -off-DLH in green and $v2$ in black). The lines represent the mean values for 0.01 % (100 ppm) H_2O bins. The blue shaded areas show the combined uncertainties of the DACOM measurements and the $v1-\beta$ -off-DLH data. However, for the combined uncertainties, we do not use the 0.01 % H_2O bins resolution, but uncertainties of the full 5 Hz resolution to capture the variability of the instruments more accurately. Since our MGA^3 calibration cylinders were calibrated against the DACOM NOAA cylinders, the accuracy determined from the uncertainty in the NOAA cylinders should have the



same effect on the accuracy of our calibration cylinders. Therefore, for the combined uncertainty we only include the precision of DACOM and the total uncertainty of the MGA³, which includes the precision of each data point and the uncertainty of our own cylinders an.

To quantify the agreement between the MGA³ measurements and DACOM, we calculate the fraction of data points that overlap within the combined uncertainty of both instruments which is summarized in Table 3. In Figure 6(a) for the 2024-03-25, the difference between DACOM and $v1-\beta$ -off (orange line) is already very small with 74.5% of data overlapping between the two instruments. This indicates that the behavior of H₂O of the water laboratory experiment is actually close to the mean behavior for all ASIA-AQ flights (dashed black line, Figure 5) and therefore to the behavior during this flight. This is indicated by the differences for $v1-\beta$ -off-DLH (green line) which show only smaller deviations compared to $v1-\beta$ -off due to the application of the DLH-correction (74.4% overlap with DACOM). The differences for $v2$, however show a drift with increasing H₂O mole fractions with 60.8% of data overlapping DACOM. In particular, for H₂O values above 1.5% or 15000 ppm the differences between DACOM and $v2$ are larger than the combined uncertainties. A reason for the drift can be water dependencies found in the pressure regulator used in the MGA₃ which is replaced by an updated regulator in the newer models (personal communication with Oleg Aseev). In Figure 6(b) and (c), the differences for $v1-\beta$ -off show deviations greater than 1 ppb compared to DACOM. The overlap of the data is 53.1% and 70.1%, respectively. This can be explained by the indicated changes in the sensitivity of the MGA³-H₂O measurements as discussed in Chapter 3.3. When corrected with DLH, however, the resulting $v1-\beta$ -off-DLH corrected data overlaps within 79.4% and 82.3% with DACOM data and the deviations for larger H₂O values decrease. For the 2024-03-21 and 2024-03-18 in $v2$ the same trends are found in Figure 6(b) and (c) as for the 2024-03-25 shown in Figure 6(a).

There are several possible reasons that the percentages of overlapping data with DACOM do not reach higher values than 82%. First, of course, the two instruments are not identical and react inherently different to changes in the measured species especially due to the different setups (Nafion-drier, pump, mass flow, etc.). Second, DACOM used one additional calibration cylinder and calibrates every 4 min while our setup uses only two cylinders for calibrations every 10 min, making our instrument potentially more prone to changes in sensitivity compared to DACOM. Third, it could be that the distance of the inlets for the two instruments of about 20m leads to the sampled air by both instruments not being identical. In the case of $v1-\beta$ -off-DLH, a last reason could be that the mean behavior of H₂O for all flights in Figure 5(a) (dashed black line) correcting the laboratory experiment does not represent the actual true behavior. This could also explain the slight negative trend in N₂O from lower to higher H₂O values.

We conclude that the $v1-\beta$ -off approach could be improved by the additional DLH correction resulting in the $v1-\beta$ -off-DLH approach. The newer $v2$ version shows a significant drift for growing H₂O mole fractions but matches DACOM until 1.5% or 15000 ppm H₂O within the uncertainties. However, it does not need an additional adjustment with DLH data or data from other instruments as $v1-\beta$ -off-DLH.



Table 4. Contribution of the N₂O-precision, H₂O-precision, calibration and water vapor correction procedure to the total squared uncertainty for the v1- β -off N₂O data in percentages.

	mean / %	min-max / %
precision N ₂ O	93.25	88.05 – 97.27
precision H ₂ O	4.49	1.55 – 7.53
calibration	0.04	0.01 – 0.1
water vapor correction	2.22	0.9 – 4.8

3.5 N₂O precision, noise and uncertainty

In Section 2.5, we explained the possibility of changing the- β setting and how it influences the fitting process. An advantage
 435 from the deactivation of the β is, that the fitting software has one less parameter that has to be accounted for in the fitting
 process, leading to less noise in the retrieved mole fractions.

Therefore, we compare the precision of 14 ASIA-AQ flights refitted with the approaches v1- β -off, v1- β -off-DLH and v2.
 We determine the in-flight precision by calculating the mean of the precision values for each flight, obtained by propagating
 the standard deviations of all calibration time windows within the given flight, such as the one in Figure 2. The mean N₂O
 440 precision for both the v1- β -off-DLH version and the v2 version is about 42% \pm 4% lower than for the v1- β -off version. The
 lowest determined in-flight precision for a flight at ASIA-AQ with the v1- β -off-DLH version was approximately 0.17 ppb.

Further uncertainties arise from the calibration and the water vapor correction of the data. We summarize the uncertainty
 budget in Table 4 in percentages according to the contribution to the total uncertainty. After propagating the precision of
 the N₂O measurements through the calibration Equation (3) and the water vapor correction Equation (17) we find, that in the
 445 mean across flights the precision of N₂O contributes about 93% to the squared total uncertainty. The H₂O-precision, usually
 in the range of approximately 0.01 vol%, contributes approximately 4.5%, the calibration procedure about 0.05% and the
 water vapor correction procedure about 2.2% to the total squared uncertainty. However, in this calculation, we assume that the
 uncertainties of the NOAA-cylinders used for cross calibrating our own calibration cylinders are 0 and therefore only apply
 the uncertainties of our calibration cylinders which are < 0.1 ppb using standard errors. The squared uncertainty of the H₂O
 450 measurements itself also increases by roughly 40% after applying the DLH-correction to the ASIA-AQ data.

The precision depends crucially on the optics alignment. Usually, we recognize a misalignment by a drop in the detected laser
 intensity, by worsened residuals when fitting the spectra or by worsened precision values compared to previous measurements
 which all can be corrected again by realigning the mirrors. The mirrors directing the laser beams into the measuring cell can
 misalign when the instrument experiences heavy shocks. We also experienced a misalignment after transporting the instrument
 455 with a van over several hours on the highway. Onboard the Cessna at the GHGMon campaign we did not experience any clear
 misalignment over the course of roughly 50 flight hours (including transfer flights). Onboard the DC-8 at ASIA-AQ, we did
 not experience any clear changes in the alignment either for about 90 flight hours. In South Korea, even after warming up

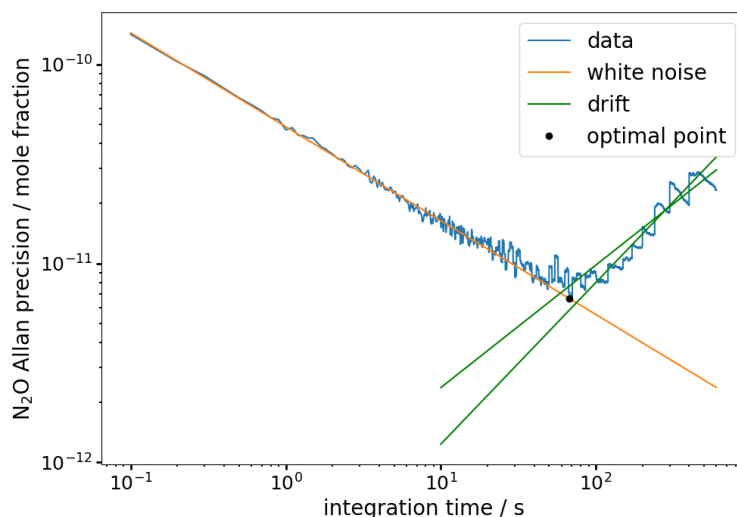


Figure 7. Allan Precision for N₂O. Values along the orange line are considered white noise. The green lines show the minimum and maximum range for drift behavior. The optimal integration time τ after which the drift sets in is shown with the black dot at $\tau = 67\text{ s} \pm 8\text{ s}$.

the device for 1-3 hours from temperatures slightly above the freezing point over night to 25 °C in the optics compartment of the instrument we could not see any significant changes to the alignment and precision. However, after the transfer flight from South Korea to Thailand, a clear misalignment in the optics worsening the precision of the instrument by about 50-100% for the last four campaign flights. The optics could be realigned again in the laboratory after the campaign. The source of the misalignment could have multiple reasons, e.g, heavier shocks than usual while landing, but we could not identify any specific cause. In general, we realign the optics before every campaign for optimal data quality. Because of a possible misalignment, we recommend to built in the MGA³ in the top of a rack to have easier access to the mirrors while doing flight tests.

We conclude that the v1- β -off-DLH and v2 versions give a better precision for the data than the v1- β -on version. However, for the v1- β -off-DLH version to work, we have to determine an empirical water correction as described in Chapter 3 whereas version v2 works with no additional data refinement after the mole fraction retrieval. The instrument is stable in regards of its optical alignment over whole campaigns with about 50 flight hours and longer. Nonetheless, we recommend a realignment of the optics before every campaign for optimal data quality.

4 Stability of the DLR airborne MGA³ system

4.1 Allan Precision and calibration frequencies

In this section, we determine the stability of the MGA³-N₂O via its Allan precision according to Werle et al. (1993), as can be seen in Figure 7. We calculate the Allan precision from a 20min time series of a measured calibration gas in the laboratory on ground and discuss the optimal calibration times and frequencies for the in-situ measurement. The range of white noise can



Table 5. Allan Precision for different integration times τ in Figure 7. The optimal integration time is at 67 s. The values for $\tau = 1$ s, 200 s are slightly higher than the values given by the manufacturer.

integration time τ	calculated (ppb)	manufacturer values (ppb)
@0.1 s	0.15	
@1 s	0.05	0.03
@10 s	0.017	
@67 s	0.007	
@100 s	0.009	
@200 s	0.015	0.01

475 be found along the orange line. The two green lines show the maximum and the minimum slope where the behavior of the instrument shows a drift. Based on this, the optimum integration time $\tau = 67\text{ s} \pm 8\text{ s}$ was determined by calculating the mean of the times between the intersects of the green and orange lines. In Table 5, the result for a set of integration times τ can be seen, including two values that were given by the manufacturer. Our self-determined values are comparable to the manufacturer values but are slightly higher. Therefore, the data should be calibrated about every 67 s to avoid any drift in the data. However, 480 this would lead to a duty cycle of about 63% leading to a high and expensive calibration gas consumption. As a trade-off between data quality, gas consumption, and data acquisition, we chose to calibrate for 40 s in total every 10 min leading to a duty cycle of about 94%, as we already saw in Figure 2 in an example from the ASIA-AQ campaign. The calibration time windows show stable behavior within their respective 20 s and, in combination with the high cell exchange rate and after our experience at the GHGMon and ASIA-AQ campaigns, we suggest even shorter periods than 20 s for the high and low standards 485 in future flights, further improving the duty cycle of our our system.

4.2 Dependency on cabin pressure

As previously noted, the DC-8 aircraft has a pressurized cabin while the DLR Cessna aircraft is unpressurized. In the DC-8 the cabin pressure data are provided by the DC-8 Meteorological and Navigation Facility Instrumentation (MetNav). As a proxy for the cabin pressure in the Cessna, we use the static pressure measurement provided by the meteorological sensor 490 package (METPOD). Previously, Pitt et al. (2016) have shown cabin pressure dependencies in their data resulting in deviations of several ppb for pressures ranging from about 1000 hPa down to 800 hPa, which were corrected by a pressure differentiated calibration procedure. However, with this procedure the data is filtered by a condition where the influence of pressure is small, leading to high losses in the amount of data. Gvakharia et al. (2018) also showed deviations in N_2O within a similar pressure range. These deviations were accounted for by frequent calibrations.

495 To study the potential effect of cabin pressure on the measurement quality, we measured calibration gas during a specific descent of the DLR Cessna for about 8 min covering a pressure change from 820 hPa to 880 hPa. To study the effect onboard the NASA DC8, we specifically asked to actively lower the cabin pressure between 840 hPa and 760 hPa within 8 min. Figure 8

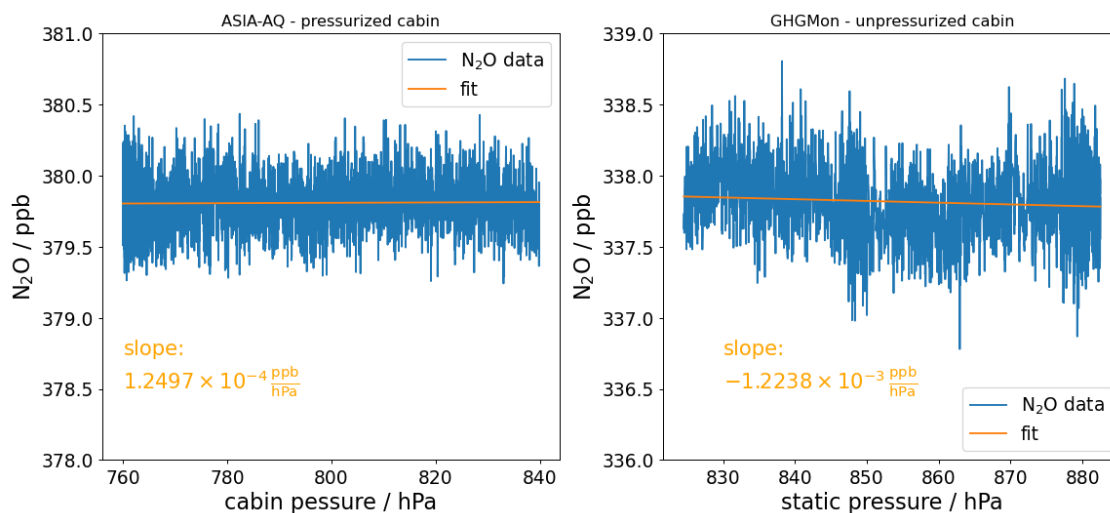


Figure 8. On the left, N₂O calibration gas measurements are plotted against the cabin pressure of the NASA DC8. The pressure of the pressurized cabin was actively reduced from 840 hPa to 760 hPa within 8 min. The slope of the fit function shows no significant drift in N₂O. On the right we see the N₂O calibration gas measurements plotted against the static pressure as a proxy for the cabin pressure, because the cabin of the DLR Cessna is not pressurized. During a descent within 8 min the static pressure increased from 820 hPa to 880 hPa. The slope shows a significant drift for pressure changes of more than roughly 150 hPa, which would be higher than the precision of the instrument 0.17 ppb. However, the behavior seems to be less stable so that the drift does not seem to be connected to changes in cabin pressure alone.

shows the retrieved mole fractions of the sampled calibration gas, once plotted against the cabin pressure of the DC8 and once against the static pressure for the DLR Cessna during the descent. For the ASIA-AQ data no obvious dependencies on the cabin pressure can be identified. The data seems to be stable, as can be seen from the fit of the data with a slope of $1.2497 \times 10^{-4} \frac{\text{ppb}}{\text{hPa}}$. For a pressure change in the range of 1000 hPa, the resulting drift would still almost be within the uncertainty/precision of 0.19 ppb of the instrument for these 8 min. However, for the GHGMon flight with the unpressurized cabin a less stable behavior with a standard deviation of 0.24 ppb can be seen, which is higher than the determined precision for this flight with 0.17 ppb. The fit function shows a slope of $-1.2238 \times 10^{-3} \frac{\text{ppb}}{\text{hPa}}$, but it does not show a clear linear behavior which would indicate a clear dependency on the cabin pressure alone.

We conclude that the measurements from the unpressurized cabin are less stable but are probably not solely linked to cabin pressure changes alone. Nonetheless, we recommend for both a pressurized and unpressurized cabin to sample calibration gas before and after each relevant ascent or descent in a profile to minimize any drift.

4.3 Dependency on roll and pitch angle

In this section, we analyze if changes in the roll and pitch angle of the aircraft influence the measurements of the MGA³. For example, Pitt et al. (2016) introduced a quality flag for their data for roll angles over 10°, which caused deviations in the

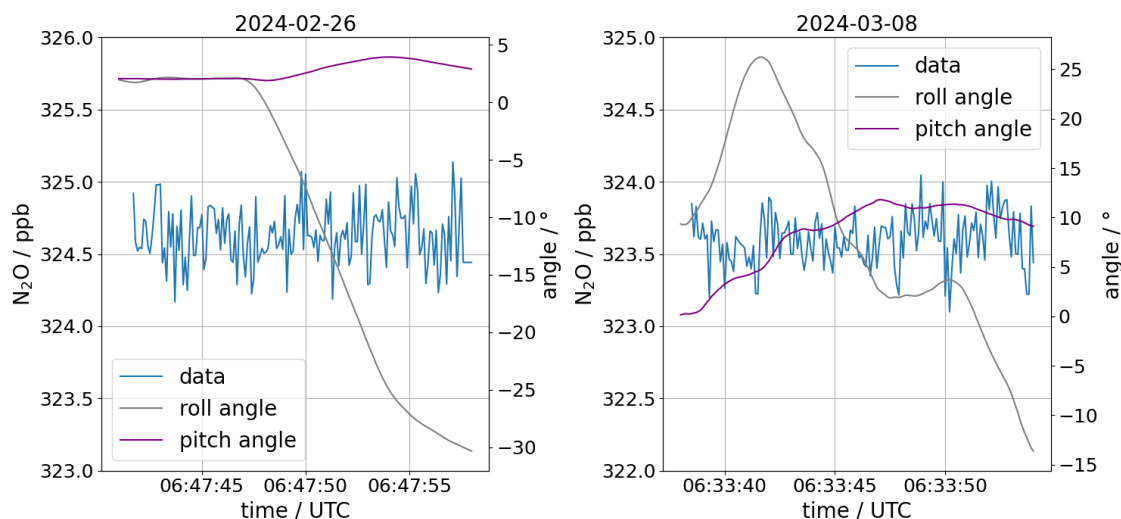


Figure 9. Calibration gas measured in-flight at the ASIA-AQ campaign during changing roll and pitch angles on the 2024-02-26 and the 2024-03-08 in South Korea. On the 2024-02-26 we flew a left turn with a roll angle up to -30° while the pitch angle was almost constant. On the 2024-03-08 we were ascending with a pitch angle of up to 12° while changing from a right turn to a left turn with roll angles from 25° to -15° . In both flights no dependencies that are larger than the respective noise of the measurements could be found.

measurements due to the centrifugal force acting on the alignments in the laser setup. The roll angle describes the rotation of the aircraft around its longitudinal axis (nose to tail) respective to its initial horizontal position of the wings (positive values: clockwise rotation looking forward) and the pitch angle describes the the rotation of the aircraft around its lateral axis (wing tip to wing tip) respective to its initial horizontal position (positive values: nose up). The roll and pitch angle data were provided by the DC-8 MetNav. The minium and maximum reached values for the roll angle during all flights at the ASIA-AQ campaign were $-36^\circ \pm 4^\circ$ to $36^\circ \pm 4^\circ$ and for the pitch angle $-8^\circ \pm 2^\circ$ to $15^\circ \pm 2^\circ$.

In Figure 9, we plotted data of 15s from two calibration time windows from the flights on the 2024-02-26 and 2024-03-08 against the roll and the pitch angle of the aircraft. In (a) and (b) we cannot see any clear dependency of the measurements on the angles that are larger than the noise or precision of our measurements.

5 Case Studies and example measurements

In this section, we present calibrated and water vapor ($v1-\beta$ -off-DLH) corrected N_2O measurements from the ASIA-AQ campaign. The goal of the campaign is to better understand the air quality in Southeast and East Asia through airborne in-situ measurements that later on can be used for validating models and satellite data (Crawford et al., 2025). The general approach was to fly the same pattern specifically designed for each country repeatedly for multiple flights to acquire data for large horizontal ranges within the PBL. The flight patterns were repeated two to three times per flight with frequent profiles to scan the whole PBL at different day times. Within a pattern, the profiles were flown at the same locations, as far as possible. With

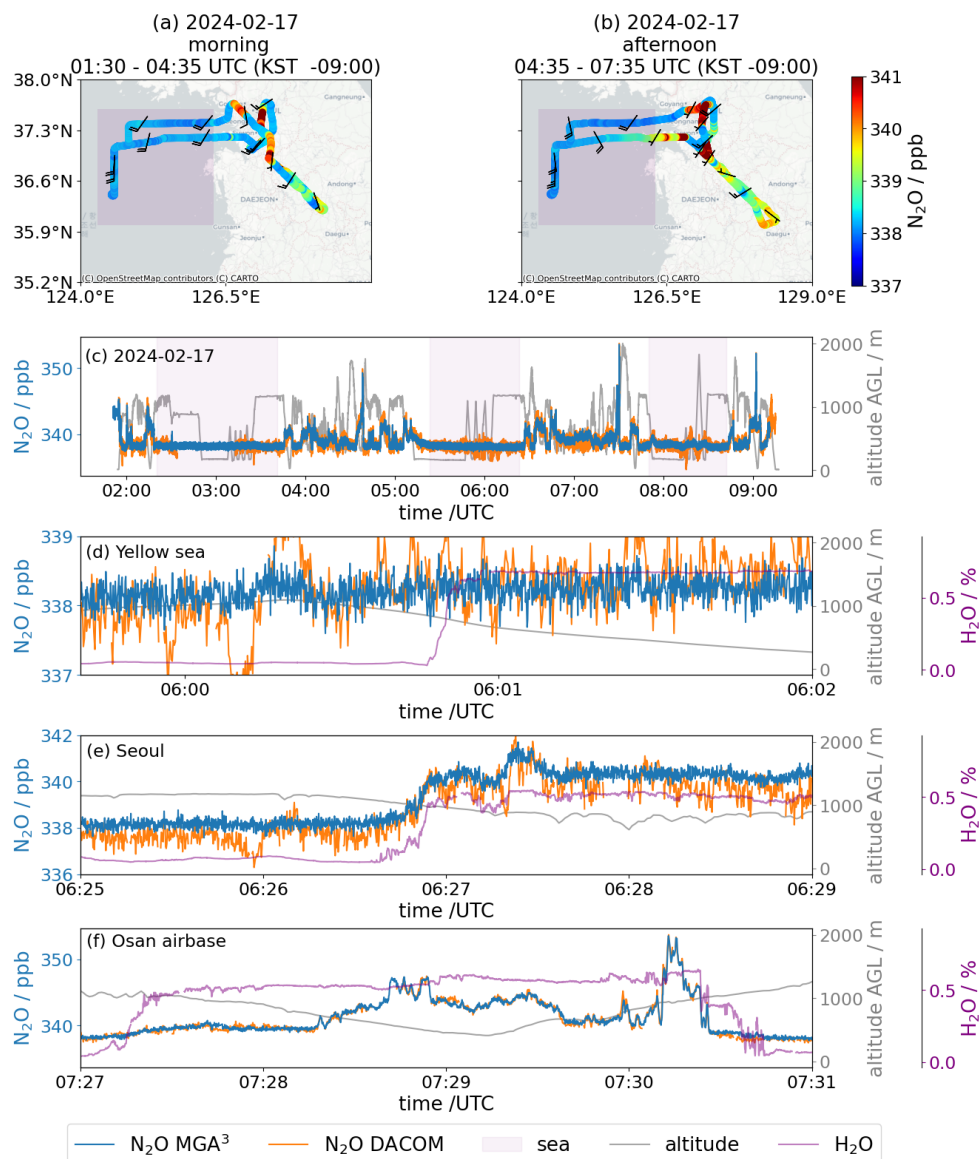


Figure 10. Comparison of color coded N₂O data measured by the MGA³ in the morning in Figure (a) and in the afternoon in Figure (b) of the same flight in South Korea on the 2024-02-17. Panel (c) depicts the time series for the whole flight measured by the MGA³ (10Hz, precision: 0.18ppb) and DACOM (5Hz, precision: 0.3ppb) and the altitude above ground level showing the frequent ascents and descents. The purple shaded areas show the flight paths over the yellow sea in (a) and (b), where we measured background concentrations of about 338 ppb in N₂O. Figure (d) shows data from the afternoon over the Yellow sea where we entered the PBL. The change in water vapor mole fraction while entering does not show any effect on the water vapor corrected v1-β-off-DLH data and the air seems to be clean enough to show no changes in N₂O compared to the background measurements outside the PBL. Figure (e) shows data while entering the PBL over Seoul where enhancements in N₂O can be seen. Figure (f) shows enhancements of up to 16 ppb in N₂O between Pyeongtaek and Anseong approaching Osan Airbase which are in good comparison with the DACOM measurements.



this, we acquired a N₂O data set with about 100h of combined data measured at 10Hz for the regions of Luzon (Northern Philippines), Taiwan, South Korea and Thailand in the winter of 2024. GPS-data and altitude above ground level (AGL) were provided or deduced from the measurements of the DC-8 MetNav. The wind measurements at flight altitude were provided in 20Hz by the Meteorological Measurement System (MMS) (Scott et al., 1990) which is used on multiple NASA aircraft.

Figure 10 presents an example flight from the campaign in South Korea on the 2024-02-17 and shows the variability of N₂O data as observed on large horizontal scales. Figure 10(a) and (b) show the flight tracks for the morning and afternoon flights, respectively, color coded by measured N₂O. The wind barbs indicate southerly to southwesterly winds over the whole flight. In the afternoon (Figure 10(b)), slightly higher enhancements can be found than in the morning (Figure 10(a)). Especially, the southerly flight path leading west from the land to the sea shows higher enhancements in the afternoon than in the morning. Those enhancements could be caused by the coal fired KOEN Yeonheung Power Plant on Yeonheung island but also by transport from land due to the mainly southerly winds in the afternoon. The correct source attribution is beyond the scope of this work and will be part of an upcoming study. Figure 10 (c) shows the time series of the whole flight with a duration of about 7h as measured by the MGA³ (10Hz, precision: 0.17 ppb) and by DACOM (5Hz, precision: 0.3%). The grey lines represent the flight altitude above ground level (AGL), showing the frequent level changes and vertical profiles between 0m and 2000m. Over the Yellow Sea west of South Korea, indicated by the purple shaded areas, the N₂O background mole fraction is relatively constant at about 338ppb. Here, no significant differences within and outside the PBL are observed for N₂O, as shown in more detail in Figure 10(d). A change in H₂O of about 0.7% is observed when entering the PBL at ~ 900m during a descent, while the water vapor corrected N₂O values remain at the same level. The figure also illustrates the better precision and stability of the DLR-MGA3 in comparison to the DACOM instrument. In contrast, much higher mole fractions with enhancements of about 3ppb compared to the background were measured when entering into the PBL over Seoul (Figure 10(e)). Finally, Figure 10(f) illustrates the general good comparison between the MGA³ data and the DACOM data over larger ranges in N₂O mole fractions, with enhancements of up to 16ppb as measured during a vertical profile taken close to the Osan Airbase.

Using the frequent profiles, we can compare the vertical distribution of N₂O for different regions and also compare it to other species. In the following example, we use NH₃ for comparison, since the agricultural sector is the main anthropogenic source for both species (Behera et al., 2013). The NH₃ was measured by the Los Gatos Research Ammonia Analyzer - Trace (LGR-AAT) (1σ,0.1s: 0.7ppb) operated by the Hankuk University of Foreign Studies (HUFS) and the National Institute of Environmental Research (NIER) in South Korea. In Figure 11(a), (b) and (c), by using the data from all flights for South Korea and Thailand respectively and a single flight for Taiwan, we calculate the 50th and 90th percentile for N₂O (blue and cyan) and NH₃ (red and orange) for 100, m bins with. Each bin has about >1000 values except for Taiwan with >100. Due to the warmer temperatures in Thailand and Taiwan compared to South Korea, we generally had to fly higher to scan the PBL completely. For the 50th percentile of N₂O, slightly higher values of 1-2ppb in Thailand and in Taiwan than in South Korea can be seen for AGL flight altitudes below 1500m and 1000m, respectively. For the 90th percentile below 1000m in Thailand, higher values of up to 4ppb in N₂O compared to South Korea and up to 2ppb higher than in Taiwan can be seen. One reason for the higher N₂O values in Thailand compared to South Korea could be the impact of lower temperatures on agriculture in South Korea during February. In general, a reason for the high N₂O measured over Thailand could be, that we flew over Central Thailand over

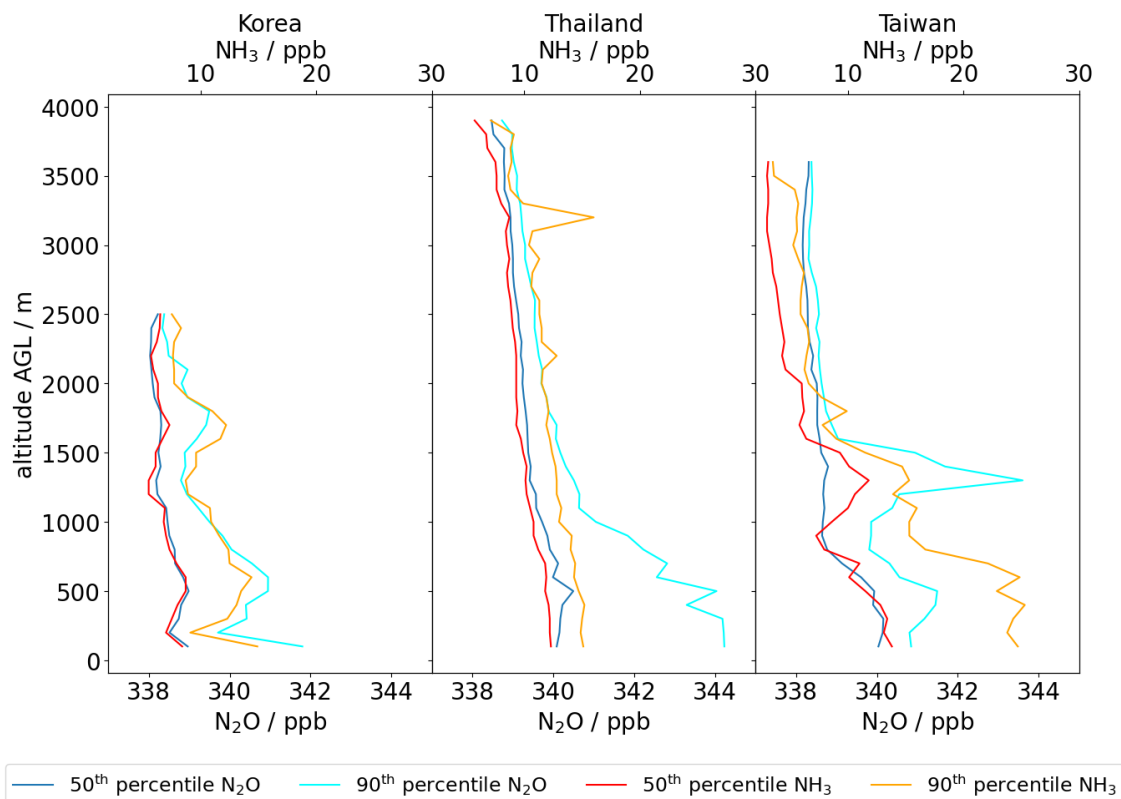


Figure 11. The 50th and 90th percentile of N₂O and NH₃ for South Korea, Thailand and Taiwan. For each country data from all flights are taken to calculate the percentile, except for Taiwan, where we have data from one flight only. In Thailand and Taiwan had to fly higher than in Korea to get out of the PBL due to higher ambient temperatures. In Korea N₂O and NH₃ show similar behavior. In Thailand the N₂O shows an increase for altitudes below 1500m due to a rain event in one flight, after which the N₂O emissions were higher over agricultural areas. In general Thailand shows higher enhancements in the PBL for N₂O due to the higher agricultural activities in this region. In Taiwan an increase in N₂O around 1500m altitude can be seen, which was measured at a technology park at Tainan with manufacturing plants by TSMC.

a plain stretching from Bangkok to Northern Thailand where agriculture is very prominent and concentrated over thousands of square kilometers. Additionally, on the flight of the 2024-03-21, there was a rain event after which N₂O emission rose in general with enhancements of up to 14ppb in that area dominating the higher N₂O values for the 90th percentile in Thailand. Those enhancements were measured mainly in agricultural areas. In Taiwan, in the 90 percentile a high enhancement of up to 6ppb can be seen compared to the background around an altitude of 1000-1700m. These enhancements with maximum values of 15ppb originate mainly from the overflights over a technology park divided between the Anding, Shanhua and Xinshi Districts of Tainan where several plants of semiconductor and chip manufacturers like TSMC are located. Additionally, the technology park is surrounded by agricultural fields and contains a waste water treatment facility making this area complex

for source attribution. For NH_3 , we can see that the 90th percentile in South Korea shows structures similar to those of N_2O . In Taiwan, first, the 50th percentile of NH_3 and the 90th percentile of N_2O seem to match at the altitudes around 1500m, but then the 90th percentile NH_3 seems to diverge more to higher values for altitudes below 1500m. For Thailand, NH_3 does not seem to correlate with the N_2O percentiles, especially not with the 90th percentile, although these enhancements in N_2O originate
575 mainly from agricultural regions.

In an already conducted study by Waldmann et al. (2026) at the GHGMon campaign 2023 in the Netherlands, our MGA³ was used for a N_2O eddy covariance study, calculating N_2O fluxes. For a comparison, we applied the same method for specific, representative flux legs across one research flight, once with the $v1-\beta$ -off water correction and once with the $v2$ correction. In the comparison, we could find that the relative difference between the results was around 3% which is an order of magnitude
580 smaller than the typical relative flux errors reported by Waldmann et al. (2026). Hence, for this instrument setup, we cannot find any significant difference in the influence of the water vapor correction approaches on the calculated eddy covariance fluxes.

6 Summary and Conclusions

In this paper, we evaluate a measurement system for fast (10Hz) airborne N_2O measurements. The core of the system consists of a commercial QCLAS, the Multicomponent Gas Analyzer (MGA) from MIRO Analytical AG (Switzerland). The system
585 was successfully deployed twice: during the 2023 GHGMon campaign aboard the DLR Cessna with an unpressurized cabin in the Netherlands, and during the 2024 ASIA-AQ campaign aboard NASA's DC8 with a pressurized cabin over South Korea, Thailand, the Philippines, and Taiwan. The system is calibrated using a two-point calibration every 10 min, with a high and low standard gas for approximately 40s in total, resulting in a duty cycle of about 94%. Under this setup, the measuring cell is fully flushed with calibration gas in under 1s, indicating that the duty cycle could be further increased by reducing the calibration
590 duration.

We operate the instrument in the β -deactivated mode, in which the fitting software freezes the last value used for the width of the spectral profile. By reducing the number of adjustable parameters, this mode decreases the data noise by about 42% compared to the default β -activated setting. However, because the spectral profile widths are strongly influenced by the highly variable H_2O in the PBL, cross-dependencies on H_2O remain observable in the data.

To correct H_2O dependencies in both the β -deactivated and the β -activated mode, arising from dilution, line broadening, and other spectroscopic effects, we derived an empirical water vapor correction from laboratory experiments. We further observed that, from flight to flight, the H_2O measurements show differences relative to NASA's DLH measurements. This is likely due to the inability to perform a two-point calibration of the MGA³ H_2O measurements, as our calibration gases are dry standards. To improve the H_2O correction, we therefore calibrate the MGA³ H_2O measurements against the DLH data leading to the
600 water vapor corrected version of the MGA data, namely the $v1\beta$ -off-DLH. Also, we tested a new version of the MGA³ fitting software, namely $v2$, that includes a water vapor correction based on the same laboratory experiments. For H_2O values up to 15000ppm, $v2$ performs comparably to the $v1\beta$ -off-DLH, showing similar precision (approximately 0.17ppb. The $v1\beta$ -off-DLH data compares well with N_2O measurements from NASA's DACOM measured simultaneously with our system at



the ASIA-AQ campaign even up to 30000 ppm H₂O. In example data from ASIA-AQ we show that clear differences within
605 large horizontal and vertical scales can be distinguished between different regions with high humidity. We also compare the
two approaches using GHGMon campaign data (Waldmann et al., 2026) to calculate eddy covariance fluxes, but found no
significant difference in the resulting fluxes.

We did not observe clear dependencies of the measurements on the aircraft's roll and pitch angles, nor cabin pressure, while
610 sampling calibration gas. However, on the DLR Cessna with its unpressurized cabin, the measurements were generally slightly
less stable.

We conclude that the presented instrumental setup enables fast and precise airborne N₂O measurements, suitable for eddy
covariance flux estimates and for deployment in highly humid tropical regions.

Data availability. The data are available from the author upon request. All of the ASIA-AQ campaign data is available on the archive:
615 <https://www-air.larc.nasa.gov/cgi-bin/ArcView/asiasaq> (<https://doi.org/10.5067/SUBORBITAL/ASIA-AQ/DATA001>, ASIA-AQ Science Team,
2024)

Appendix A: Dependency of absorption coefficient α on water vapor H₂O

The absorption coefficient α is retrieved from the HITRAN Database 2016 (Gordon et al., 2017). According to the official
HITRAN website at <https://hitran.org/docs/definitions-and-units/> (Gordon et al., 2022) α is defined as:

$$\alpha(\nu, T, p) = S_{ij}(T) f(\nu, \nu_{ij}, T, p), \quad (\text{A1})$$

620 where S_{ij} is the intensity of a spectral line for a single molecule for the transition between two states i and j , f the Voigt profile
and ν_{ij} the wavenumber of the spectral line transition in vacuum. The Voigt profile further consists partially of a normalized
Lorentz profile f_L defined as:

$$f_L(\nu, \nu_{ij}, T, p) = \frac{1}{\pi} \frac{\gamma(p, T)}{\gamma(p, T)^2 + [\nu - \nu_{ij}^*(p)]^2}. \quad (\text{A2})$$

Here ν_{ij}^* is the pressure shift corrected wavenumber ν_{ij} and γ is the Lorentzian Half-Width-Half-Maximum (HWHM) width
625 of the line shape. In the case of pressure broadening on the observed species induced by air, water vapor and the species itself,
the resulting width γ is defined as (Kostinck et al. (2019), <https://hitran.org/docs/definitions-and-units/>):

$$\gamma(p, T) = \left(\frac{T_{\text{ref}}}{T} \right)^{n_{\text{air}}} (\gamma_{\text{air}}(p_{\text{ref}}, T_{\text{ref}}) (p - p_{\text{self}} - p_{\text{H}_2\text{O}}) + \gamma_{\text{self}}(p_{\text{ref}}, T_{\text{ref}}) p_{\text{self}} + \gamma_{\text{H}_2\text{O}}(p_{\text{ref}}, T_{\text{ref}}) p_{\text{H}_2\text{O}}). \quad (\text{A3})$$

Here γ_{air} , γ_{self} and $\gamma_{\text{H}_2\text{O}}$ are the HWHM induced by the partial pressures p_{air} , $p_{\text{H}_2\text{O}}$ and p_{self} of air, water vapor and the
species itself at a reference temperature $T_{\text{ref}} = 296$ K and pressure $p_{\text{ref}} = 1$ atm.

630 Specifically for the N₂O absorption line used in our MGA³, the HITRAN data base shows that H₂O has a higher broadening
effect than air (=nitrogen (N₂), oxygen (O₂)) and N₂O itself with $\gamma_{\text{H}_2\text{O}} = 0.1308$, $\gamma_{\text{air}} = 0.0701$ and $\gamma_{\text{self}} = 0.085$ (Gordon



et al., 2022). The difference between γ_{self} and $\gamma_{\text{N}_2\text{O}}$ has important implications on the spectral line width. While the global background concentration of N_2O in the troposphere is in the range of about 338 ppb, H_2O mole fractions lie between 1 ppm to 10 ppm even in the dry stratosphere, but can get specifically high in regions such as the tropical boundary layer (up to
635 30000 ppm, which is 4 to 5 orders of magnitudes higher than for N_2O). With this, we can simplify equation (A3) for measurements in the troposphere to:

$$\gamma(p, T) = \left(\frac{T_{\text{ref}}}{T}\right)^{n_{\text{air}}} (\gamma_{\text{air}}(p_{\text{ref}}, T_{\text{ref}})(p - p_{\text{H}_2\text{O}}) + \gamma_{\text{H}_2\text{O}}(p_{\text{ref}}, T_{\text{ref}})p_{\text{H}_2\text{O}}). \quad (\text{A4})$$

Therefore, we assume the width γ of our measured line spectra to be mainly dependent on water vapor for atmospheric measurements in the troposphere, assuming that T and p are constant in the cell.

640 Appendix B: N_2O Eddy Covariance GHGMon

Waldmann et al. (2026) used the same MGA³ as presented in our study to conduct airborne eddy covariance flux measurements in the course of the GHGMon (Greenhouse Gas Monitoring) campaign 2023 in the Netherlands. Precise high-frequency GHG measurements without interference from water vapor related effects are a prerequisite for robust flux measurements, as water vapor mole fractions are often quite distinct between turbulent updrafts and downdrafts, potentially falsifying GHG
645 measurements if not properly corrected. In order to investigate the extent to which different water vapor correction approaches affect flux measurements, we applied both, the v1- β -off water correction and the v2 correction to specific, representative flux legs across one research flight of the study of Waldmann et al. (2026).

In Figure B1(a) and (b), we can see the vertical wind measurements and the H_2O measurements of the METPOD system on the DLR Cessna from a flight in Friesland on 21 June 2023. Both show high-frequency fluctuations, typical during fair-weather
650 turbulent conditions, which in turn are fundamental for applying the eddy covariance methodology. In Figure B1(c), we see the MGA³- N_2O measurements for the v1- β -off and v2 water correction approaches, similarly showing high-frequency variability expected in the turbulent PBL. In Figure B1(d), the calculated eddy covariance fluxes are shown as time series for the two retrieved mole fractions from (c), calculated according to the procedure presented in ?. The mean value for the fluxes over the given time frame is slightly higher for the fluxes with the v2 water correction ($0.36 \text{ gm}^{-2}\text{s}^{-1}$) compared to the fluxes with the
655 v1- β -off water correction ($0.33 \text{ gm}^{-2}\text{s}^{-1}$), which translates to a relative difference of 9%. This difference is expected, given the drift in N_2O corrected according to v2, with increasing H_2O (see Section 3.4). However, the relative difference (9%) is approximately 1 order of magnitude smaller than typical relative flux errors reported in ?, which range between 30-100%, which are superimposed as error bars for the v1- β -off fluxes in Figure B1(d). For both corrections, we computed the limit of detection of N_2O fluxes, which was found to be slightly higher for the v2 water correction ($0.028 \text{ gm}^{-2}\text{s}^{-1}$) compared
660 to $0.017 \text{ gm}^{-2}\text{s}^{-1}$ for v1- β -off. Given that the differences in fluxes derived with both water vapor corrections is one order of magnitude smaller than typical flux errors, we conclude that the choice of water correction approaches is not a limiting factor for the quality of such flux measurements, but have to be considered when corresponding systems should be improved or small fluxes close to the detection limits are to be measured. We note explicitly that these conclusions are only valid for

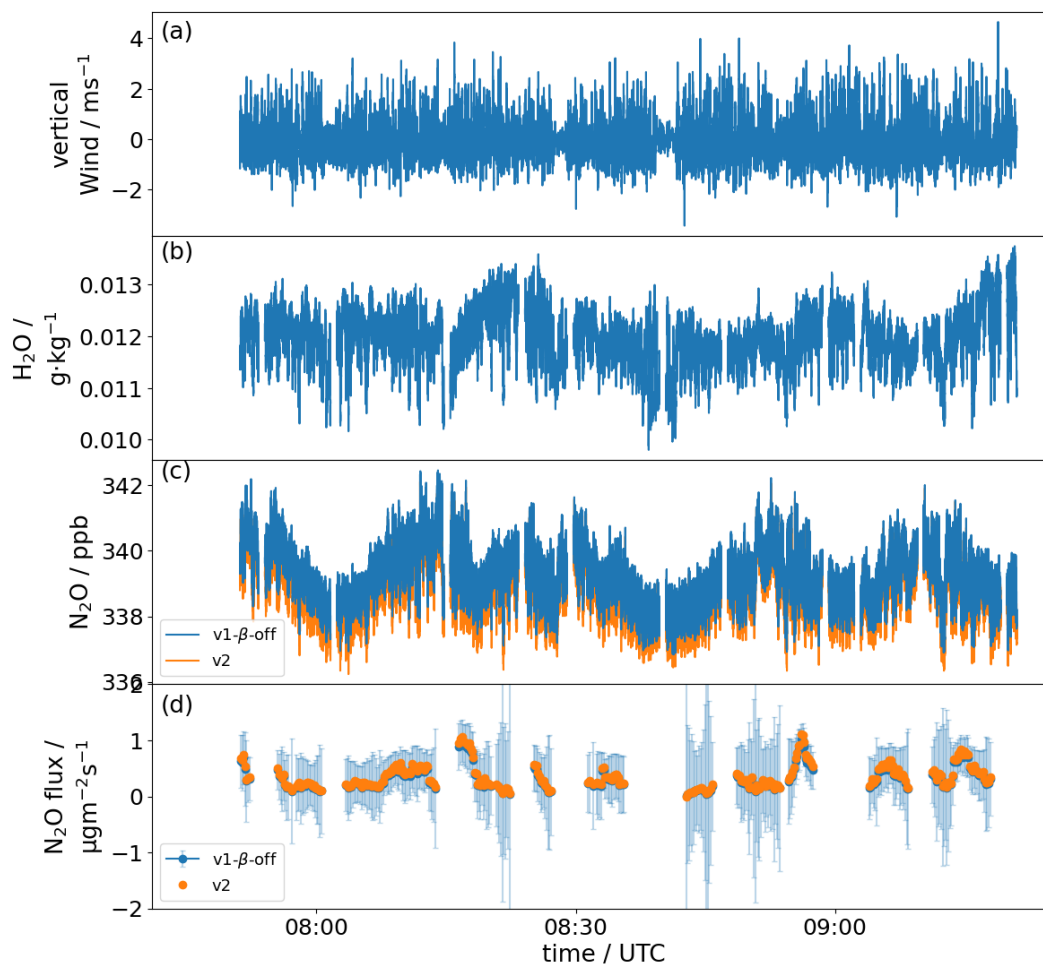


Figure B1. Panel (a) presents vertical wind measurements from a flight on 21 June 2023 in the Netherlands. Panel (b) shows corresponding H₂O measurements. Panel (c) shows the water vapor corrected N₂O measurements, once retrieved with v1- β -off and once with v2. Subplot (d) shows the calculated eddy covariance fluxes from the respective time series in Figure (c), error bars depicting the uncertainty associated with the flux computation.

665 the comparison of the water vapor corrections presented within this work, and do not represent differences in fluxes calculated with mole fraction measurements with and without water vapor correction.

Author contributions. LK wrote the paper, did the analysis and prepared the figures. LK and ME prepared the MGA³ instrument for ASIA-AQ. LK, ME, PW and AR operated the instrument at GHGMon and ASIA-AQ and conducted the measurements. AF and MP contributed to the manuscript and discussion. OA provided the new v2 software for the MGA³. GD, JD, YH and JM operated the DACOM and DLH instruments at ASIA-AQ and provided the respective data and also provided altitude above ground level data for the DC-8 at ASIA-AQ.

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670 RB, CG, JDD and RP provided GPS-data, wind measurements, static pressure measurements, cabin pressure measurements and roll and pitch angle data from the DC-8 at ASIA-AQ. GL and JK provided the LGR-NH₃ measurements at ASIA-AQ. All authors contributed to the manuscript and the discussion.

Competing interests. The authors have no competing interests.



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