



# Evaluating Different Roughness Approaches and Infiltration Parameters for Vegetation-Influenced Overland Flow in Hydrological Model

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**Abstract.** Accurately simulating overland flow in vegetated landscapes remains a challenge in hydrological modeling due to the complex interactions between vegetation, surface roughness, and soil infiltration. This study evaluates multiple methods for estimating Manning's roughness coefficient and explores the influence of vegetation on infiltration processes using the OpenLISEM model. Based on 132 artificial rainfall experiments across 22 sites in southwest Germany, the model was calibrated and validated against observed runoff data, incorporating both depth-independent and depth-dependent roughness formulations. Incorporating water depth-dependent roughness into the model can improve its performance in simulating overland flow. Beyond roughness effects, vegetation was shown to significantly alter soil hydraulic properties, particularly saturated hydraulic conductivity ( $K_{sat}$ ). Paired site comparisons revealed that increased vegetation cover corresponded with higher infiltration capacities, emphasizing vegetation's role not only in surface resistance but also in enhancing subsurface water fluxes. The findings demonstrate that models must account for both surface and subsurface impacts of vegetation to improve runoff predictions.

## 1 Introduction

Overland flow is a critical component of the hydrological cycle, playing a significant role in flood generation, soil erosion, and pollutant transport. Accurate overland flow modelling is essential for effective water resource management, flood prediction, and environmental protection. Accurately representing the effects of vegetated areas remains one of the primary challenges in overland flow modelling, as these areas play a critical role in the hydrological cycle (Peel, 2009). Vegetation significantly influences flow dynamics by increasing surface roughness, modifying flow patterns, and providing additional drag (Zhang et al., 2018). Beyond these hydrodynamic effects, vegetation also changes the infiltration regime, thereby the partitioning between infiltration and overland flow (Ajayi et al., 2021).

The hydrodynamic effects of vegetation on flow vary significantly between emergent and submergent plant communities, with distinct hydrodynamic impacts based on their structural characteristics and interaction with water depth (D'Ippolito et al., 2021). As vegetation density increases, it slows flow velocity and can reduce the erosive power of surface runoff (Mu et al., 2019). The interaction between vegetation and overland flow is often quantified through roughness coefficients, with Manning's coefficient being one of the most widely used parameters in hydrological modelling. At present, roughness parameters for overland flow are derived mainly from field measurements and laboratory experiments (Oberle et al., 2024).

Recent studies have shown that roughness coefficients are not constant but vary with factors such as water depth, vegetation density, and flow velocity (Ruiz Rodriguez, 2017; Fu et al., 2019; Hinsberger et al., 2022). Hinsberger et al. (2022) performed laboratory experiments to investigate roughness variations in submerged and emergent vegetation, demonstrating that increased submergence reduces roughness, whereas for emergent vegetation, greater submergence leads to heightened roughness. Their findings suggested that roughness-water depth relationships for intermediate zones can be approximated using a linear approach. Feldmann et al. (2023) proposed a framework to estimate Manning roughness dependent on shallow water depth. First, the partitioning of overland flow and infiltration was calculated during the descending limb of the hydrograph to determine the minimum infiltration rate. Then, they reduced the solution space by comparing experiments



conducted at one site and by comparing sites with similar properties. The framework's robustness was tested using three different depth-dependent roughness equations and a constant Manning coefficient.

Utilizing flow resistance models in vegetated areas holds immense value in evaluating the potential for flooding and formulating flood mitigation strategies grounded in scientific principles (Green, 2005). However, evaluating these equations

45 to calculate overland flows continues to be a staple area of research within hydrology. The uncertainty associated with roughness coefficients can significantly impact surface runoff accumulation. For example, Dalledonne et al. (2019) introduced an approach to evaluate uncertainty in floodplain hydrodynamic models influenced by vegetation, testing four resistance formulas. Oberle et al. (2021), carried out a review on flow resistance in overland flow. Based on some previous laboratory experiments concerning artificial grass, they demonstrated that the roughness function varies with water depth in the presence  
50 of vegetation. They noted that uncertainties emerge as the cross-sectional impact of vegetation elements is usually not considered in the calculation of resistance coefficients. In contrast, Luhar and Nepf (2013) investigated the effect of vegetation distribution on channel velocity, presenting physically based models that link drag generated by vegetation at the blade and patch scale to hydraulic resistance. This resistance depends on the blockage factor, which represents the fraction of the channel cross-section occupied by vegetation. However, the applicability of their approach to overland flow is examined in this study.  
55 These findings highlight the need for further evaluation of roughness estimation methods under varying hydrological conditions.

On the other hand, vegetation and root systems influences soil structure, creates preferential flow paths, which promote infiltration and reduce overland flow (Ajayi et al., 2021; Jarvis et al., 2013). Gao et al. (2023) stated that the most established hydrological theories, such as those presented by Drewniak (2019) and Lu et al. (2019), predominantly parameterize water  
60 fluxes based on soil properties, including texture, porosity, moisture retention capacity, wilting point, and plant-available water. These approaches are grounded in the assumption that soil properties govern key hydrological processes such as infiltration, drainage, and evapotranspiration. In traditional modelling approaches, infiltration parameters are often estimated using soil texture-based pedotransfer functions as a primary input when direct measurements are unavailable. Gao et al. (2023) challenge this perspective, suggesting instead that this causality is misrepresented: soil properties should be viewed as  
65 outcomes rather than drivers of water movement, which is fundamentally regulated by the dynamics of the surrounding terrestrial ecosystem. Neglecting key site factors, such as land use, in parameter estimation routines can introduce significant errors in the partitioning of infiltration and runoff in hydrological modelling (Jarvis et al., 2013). The impact of vegetation cover on infiltration properties such as saturated hydraulic conductivity remains insufficiently implemented in surface runoff models. Understanding the vegetation effects on soil parameters is crucial for improving the accuracy of hydrological models.  
70 In surface runoff models, saturated hydraulic conductivity is often calibrated to align with observed data, indirectly capturing the influence of vegetation on soil properties. This study explores whether such calibrated values can implicitly reflect the influence of vegetation on soil hydraulic properties. The scope of our research encompasses the following objectives:

- Modelling the overland flow to compare and validate different approaches for Manning's coefficient estimation.
- Evaluation of overland flow model performance in estimating infiltration in the presence of vegetation

By addressing these objectives, our research contributes to improving the accuracy of hydrological models and enhancing our understanding of overland flow dynamics in vegetated areas. By utilizing the experimental dataset and hydrodynamic simulation, this study assesses the accuracy of roughness coefficient estimations in a hydrological model in a realistic  
80 environment. This assessment covers a variety of scenarios involving different levels of vegetation coverage and vegetation height and varying rainfall intensities. By providing insights into the most effective approaches for estimating surface roughness and understanding the interactions of vegetation and infiltration, this research aims to enhance the reliability of



overland flow predictions and support more informed decision-making in hydrological engineering and environmental planning.

## 85 2 Materials and methods

### 2.1 Study site and experimental setup

To develop and evaluate overland flow models in the absence of real measurement, artificial sprinkling studies present an opportunity to investigate vegetation effects on overland flow. Ries et al. (2020) conducted 132 sprinkling experiments on natural hillslopes at 23 sites with different soil types and land use in Baden-Württemberg (Germany), one of the most extensive  
90 datasets accessible in southwest Germany. Table 1 provides information about land use, vegetation properties, and soil characteristics for each site. The experimental area was a 10 by 10-meter square, with slopes ranging from 9% to 32%. These experiments aimed to simulate a 100-year or locally observed maximum rainfall intensity event with different durations. Rainfall experiments started with Run 1 on the first day. Subsequently, Run2 – Run5 were conducted on the following day and Run 6 was carried out on the third day (Table 2).

95

**Table 1: Properties of experimental sites and the values of constant Manning's roughness coefficient.**

Site*	Slope* %	Vegetation*	Veg_height* (m)	Plant coverage* %	soil type	n (Chow)	n (Feldmann)
1	12	Pasture	0.15	100	Clay	0.05	0.58
2	18	Pasture	0.1	100	Silty loam	0.05	0.60
3	16	Pasture	0.1	90	Loam	0.05	0.70
4	16	Mustard	0.15	40	Clay loam	0.04	0.45
5	14	Triticale (seeded)	0	0	Silty loam	0.03	0.18
6	21	Pasture	0.05	100	Silty loam	0.04	0.65
7	14	Winter Barley	0.3	80	Silty loam	0.05	0.38
8	16	Corn (seeded)	0.05	15	Sandy loam	0.035	0.13
9	21	Pasture	0.1	100	Sandy loam	0.05	0.58
10	32	Pasture	0.15	100	Sandy clay loam	-	-
11	18	Pasture	0.1	80	Silty clay	0.045	0.68
12	19	Pasture	0.15	100	Silty clay	0.05	0.65
13	11	Alfalfa	0.2	40	Silty clay	0.04	0.28
14	27	Pasture	0.15	100	Silty clay	0.05	0.70
15	14	Winter Barley	0.05	0	Clay loam	0.03	0.50
16	12	Pasture	0.1	100	Clay loam	0.05	0.40
17	14	Pasture	0.05	100	Silty loam	0.05	0.48
18	12	Alfalfa and Clover	0.2	60	Clay	0.045	0.38
19	21	Pasture	0.15	100	Sandy clay loam	0.05	0.98
20	9	Corn (harvested)	0	0	Clay loam	0.03	0.05
21	14	Green Manure	0.15	50	Silty clay loam	0.04	0.35
22	12	Pasture	0.2	100	Silty clay	0.05	0.38
23	14	Corn (harvested)	0	0	Clay	0.03	0.08

\* Data from Ries et al. (2020)

Pair sites

The experiments conducted at Site 10 did not produce any runoff and were not used in this study. Discharge at the outlet, rainfall intensity, and initial soil moisture were measured at a temporal resolution of 1 minute. Out of the 23 sites surveyed, 12



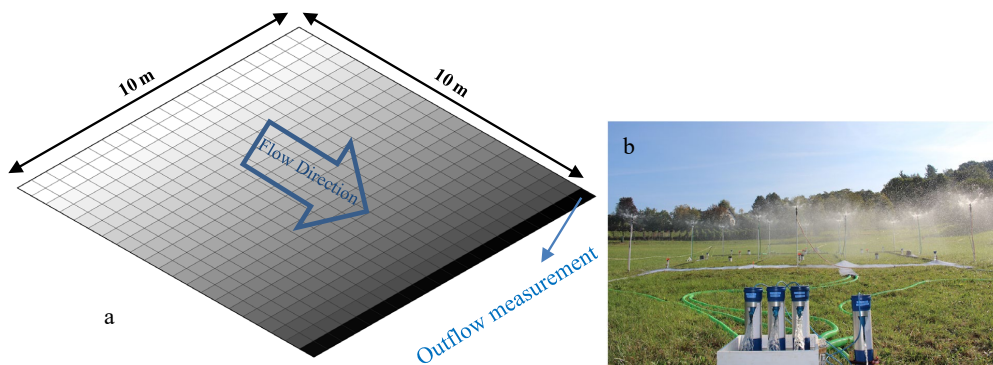
locations are paired sites, highlighted in bold in Table 1. This arrangement facilitates a direct comparison between the effects of two different land uses on runoff and infiltration. The deliberate choice of these paired sites is underscored by their proximity, with distances maintained within the threshold of less than 100 meters. For more comprehensive details of these experiments, refer to Ries et al. (2020).

**Table 2: Characteristics of rainfall for experimental sites (Ries et al. 2020).**

Run no.	Duration (min)	Return period (yr)	Intensity (mm hr <sup>-1</sup> )	Cumulative Runoff: min, max, mean (mm)
Run 1	60	100	42-76	0.0, 44.3, 13.0
Run 2	60	100	42-76	0.0, 58.6, 26.9
Run 3	30	100	82-130	0.0, 50.9, 31.7
Run 4	15	100	110-172	1.4, 30.4, 22.2
Run 5	180	worst case	44-53	0.1, 145.1, 100.6
Run 6	60	worst case	99-126	32.0, 100.1, 71.0

## 2.1 Model

To explore the impact of roughness on overland flow simulations, it is crucial to integrate the relationship between roughness and water depth into the model. For this purpose, OpenLISEM (Open Limburg Soil Erosion Model), which was developed based on the original LISEM (Jetten, 2002), was chosen for its modular structure, physics-based approach and accessibility of the source code, published under a free licence (GNU Public Licence v3, <https://github.com/vjetten/openlisem/>). It is an event-based and spatial hydrological model suitable for different sizes of catchments. It focuses on simulating runoff, sediment dynamics, and infiltration during heavy rainstorms, allowing for detailed assessments of land use changes and conservation measures (Baartman et al., 2012). The elevation model is generated with a cell size of 0.5×0.5 meter, providing information about the gradient of each specific location in the database (Table 1). Since the surface of the experimental plots is homogeneous, the generated DEM does not include micro-depressions. So, all surface parameters that may influence overland flow are represented within Manning's coefficient. This simplification does not affect our evaluation of different roughness approaches, as the conditions are consistent across all roughness methods. The last row of the DEM, colored black in Figure 1-a, represents the trench designed to collect runoff, positioned 40 cm below the surface as in constructed experiments. Figure 1-b illustrates the field setup from Ries et al. (2020), which measured flow at three points within the trench. In our model, discharge data is recorded at the outlet, located at the corner end of the trench. Since the trench length to the outlet in the experiments is one-third of that in our model, we compensated by tripling the water velocity in the trench through a reduction in Manning's coefficient for the trench surface.



**Figure 1: a) 0.5 × 0.5-meter digital elevation model applied for simulations, incorporating the specific slope of each site. b) Setup of field experiments by Ries et al. (2020).**



125 Time resolution for simulation is 1second and the total simulation time is chosen based on observation runoff data.  
For the distributed routing of overland flow, a four-point finite-difference solution of the kinematic wave is together with  
Manning's equation (Jetten, 2002). Infiltration was estimated using the Green-Ampt method (Rawls et al., 1983), which  
incorporates field-measured variables such as porosity and initial soil moisture content. Two additional parameters, saturated  
hydraulic conductivity (Ksat) and average soil suction at the wetting front (Psi), are not typically measured in the field. Prior  
130 studies, including those by Jetten (2002), Hessel et al. (2003) and Starkloff and Stolte (2014), have highlighted the primary  
sensitivity of OpenLISEM to Ksat and Psi parameters. Therefore, reasonable ranges for Ksat and Psi were adopted from Rawls  
et al. (1983), and the values were subsequently calibrated to best match observed runoff data. It should be considered that,  
infiltration in model depends on both soil properties and surface water depth, increased vegetation cover or a higher Manning's  
roughness coefficient reduces flow velocity, leading to greater surface water depth and, consequently, an enhanced infiltration  
135 rate.  
OpenLISEM version 6.873 has been utilized which employs Manning's approach to calculate the runoff velocity. While the  
original software employed a constant Manning's coefficient as a raster map for roughness, a new feature called the dynamic  
Manning's n function has been introduced into the software to implement different Manning's coefficient estimation methods  
in simulations. This feature enables users to select from various methods of roughness estimation, including not only a constant  
140 value but also methods dependent on the depth of runoff. Detailed information about these extensions can be found in the  
'Code availability.' section.

## 2.2 Surface roughness functions

Surface roughness functions are foundational components in the simulating of overland flow, affecting the accuracy of  
hydrological models. Roughness estimation approaches represent the resistance of the surface in the model that affects the  
145 momentum and energy dissipation of overland flow. In this study, two depth-independent Manning's roughness coefficients  
and five depth-dependent roughness functions were introduced into OpenLISEM to assess the impact of different Manning's  
roughness functions on vegetation modeling.

### 2.2.1 Constant Manning's coefficient

The initial approach assumes a constant value for Manning's roughness coefficient (n) based on Chow (1959), representing the  
150 range of flow resistance for floodplains covered by vegetations. The values of Manning's roughness coefficient using Chow's  
method for each site of the artificial rainfall experiments are given in Table 1. In this method, values are typically selected  
based on established literature or site-specific calibration. This is suitable for homogeneous surfaces and it does not consider  
the effect of water depth in presence of vegetation.

### 2.2.2 Robust Manning's coefficient

155 In the study conducted by Feldmann et al. (2023), the n values were directly iterated within the framework they established.  
The authors reported that the most robust results, characterized by high Nash-Sutcliffe Efficiency (NSE) values, were achieved  
with constant Manning values, as presented in Table 1. They estimate surface roughness by analyzing the shape of the  
hydrograph, fitting the Hortonian equation to the difference between rainfall input and observed discharge for the falling limb  
of the hydrograph. To achieve this goal, they assumed that the infiltration rate in the descending limb of the hydrograph is  
160 constant. For more details, see Feldmann et al. (2023).

### 2.2.3 Linear method

Drawing on previous literature on artificial grass, including Ruiz Rodriguez (2017), Oberle et al. (2021) concluded that a flow-  
depth-dependent roughness spectrum can be derived for overland flow, despite inherent variability in the data. Similarly,



Hinsberger et al. (2022) found Strickler coefficient,  $k_{Str}$ , values varied with different water depths in the presence of  
165 vegetation. Based on their results, there are three zones to specify roughness within the data range, categorized according to  
the submergence ratio: for emergent and fully submergent zones they emphasize the roughness is constant.  
A linear function of relative submergence can be described for the roughness coefficient between emergent and fully  
submergence zones ( $1 < \frac{h}{h_{veg}} < 5$  to 7) (Hinsberger et al. 2022).

These relationships are summarized in equation 1:

$$1/n_{Manning} = \begin{cases} \frac{k_{Str}}{5} & \text{for } 0 < h < h_{veg} \\ \frac{k_{Str}}{5} + k_{Str} \frac{h - h_{veg}}{5} & \text{for } h_{veg} < h < 5 \cdot h_{veg} \\ k_{Str} & \text{for } h > 5 \cdot h_{veg} \end{cases} \quad (1)$$

170 In this study, the parameter  $k_{Str}$  is Strickler's coefficient which is estimated based on the inverse of the roughness coefficient  
above the vegetation using Chow (1959). Then Manning's coefficient is calculated from Eq.1, depending on the submergence  
ratio.

#### 2.2.4 Luhar and Nepf's method

Another method to investigate vegetation effect on roughness was proposed by Luhar and Nepf (2013) for open channel. They  
175 suggested the following relationships between the Manning roughness caused by vegetation and blockage factor,  $B_x$ , for both  
submerged and emergent vegetation.

$$n_{Manning-veg} = \begin{cases} \frac{K h^{\frac{1}{6}}}{g^{\frac{1}{2}}} \left( \frac{C_f}{2} \right)^{\frac{1}{2}} (1 - B_x)^{-\frac{3}{2}} & \text{for } h \leq h_{veg} \text{ and } B_x < 0.8 \\ \frac{K h^{\frac{1}{6}}}{g^{\frac{1}{2}}} \left( \frac{C_d a h}{2} \right)^{\frac{1}{2}} & \text{for } h \leq h_{veg} \text{ and } B_x \geq 0.8 \\ \frac{K h^{\frac{1}{6}}}{g^{\frac{1}{2}}} \frac{1}{\left( \frac{2}{C_f} \right)^{\frac{1}{2}} \left( 1 - \frac{h_{veg}}{h} \right)^{\frac{3}{2}} + \left( \frac{2}{C_d a h_{veg}} \right)^{\frac{1}{2}} \left( \frac{h_{veg}}{h} \right)} & \text{for } h > h_{veg} \end{cases} \quad (2)$$

where  $n_{Manning-veg}$  is the vegetation component of Manning's  $n$ ,  $a$  is the frontal area per unit volume parameter, and  $C_d$  is  
180 drag coefficient. We assumed that the stem of vegetation is cylindrical in shape, and therefore a  $C_d$  value of 1 was used.  $C_f$  (= 0.015 - 0.19) is a coefficient to parameterize the shear stress at the interface between vegetated and unvegetated regions and  
the constant  $K = 1 \frac{m^{\frac{1}{3}}}{s}$  is required to make the equation dimensionally correct. The other parameters will still be the same.  
Although the equation was originally proposed for channel flow, this study examines its applicability to overland flow.

#### 2.2.5 Exponential method

185 The exponential equation describes the relationship between  $n$  and  $h$  in terms of the variables  $c$  and  $d$  (Eq. 3).

$$n = \frac{1}{c + e^{dh}} \quad (3)$$

The optimum values of the  $c$  and  $d$  parameters for each location were derived from the study by Feldmann et al. (2023), whose  
proposed approach is explained in section 2.2.2.

#### 2.2.6 Kadlec's method

190 Based on experimental studies on overland flow, Kadlec's power law was simplified by Jain et al. (2004) (Eq. 4).



$$n = n_0 \left( \frac{h}{h_0} \right)^{-\varepsilon} \quad (4)$$

where  $h_0$  establishes the minimum flow depth, beyond which the roughness coefficient  $n_0$  is assumed to remain constant.  $\varepsilon$  represents the influence of vegetation drag. Our study utilized the optimal values for the parameters  $n_0$  and  $\varepsilon$  as outlined in Feldmann et al. (2023). As they did not provide information on the  $h_0$  value, we assumed  $h_0$  to be five times the plant height to apply the Kadlec's method in our study. This assumption is confirmed by previous studies (Hinsberger et al., 2022; Oberle et al., 2021).

### 2.2.7 Fu's equation

Fu et al., (2019) developed an equation to calculate Manning's  $n$  based on plant basal cover and flow depth (Eq. 5).

$$n = (a + b(1 - e^{-0.061C_v})^{1.668})h^{0.604-0.710e^{-0.219C_v}} \quad (5)$$

Where variable  $C_v$  is the ratio between the area covered by stems and the flume bed. It is considered as plant coverage in Ries et al. (2020). The plant basal cover varied between 1.25% and 30%. However, uncertainties arise in the calculation of resistance coefficients. This is because the basal elements of the vegetation may cover a smaller area than the canopy, which can result in an incomplete representation of flow resistance. The parameters  $a$  and  $b$  vary with vegetation type. In this study, the values of  $a$  and  $b$  parameters obtained by Feldmann et al., (2023) are used.

All of these equations were incorporated into the source code of OpenLISEM in order to assess the impact of various roughness methodologies on overland flow modeling.

## 2.3 Parameter calibration and validation

To compare the different roughness equations, we calibrate the unknown sensitive parameters of the model using one of the six rainfall experiments (Run) per site and validate the parameters using the remaining rainfall experiments. The most sensitive parameters saturated conductivity (Ksat) and average soil suction at the wetting front (Psi) are calibrated for 23 sites and 7 different roughness approaches (154 models). The parameters for the roughness functions are selected as described above and Manning's  $n$  is selected from the well-known Chow-Table (Chow, 1959). To assess the effect of these preselected values, we added Manning's  $n$  as an additional parameter, adding one model per location with 3 calibrated parameters (total 176 models). The calibration was performed with 5,000 simulations per model (880,000 models) with a distribution of the 2 or 3 parameters using the latin hypercube sampling (LHS) method using the implementation in SPOTPY (Statistical Parameter Optimization Tool) (Houska et al., 2015). The saturated hydraulic conductivity (Ksat) varies between 5 and 100 mm/hr, and the wetting front suction head (Psi) from 0 to 50 cm water column, as suggest by Gowdiah and Muñoz-Carpena, (2009) for different soil types. For most locations, run 2 (100-year return period event, prewetted soil) was selected as the calibration event. Runs 1, 3, 4, 5, and 6 were selected as validation experiments. The reason for choosing Run 2 for calibration was that the soil moisture conditions during this test were neither excessively dry nor fully saturated. Since Run 2 in site 14 does not have any runoff, Run 6 is selected for calibration. Site 1 has a different order of experiments, so we are using Run 4 as the calibration run.

The best calibrated parameters are selected by ranking the model runs by their Nash-Sutcliffe efficiency. After calibrating the Ksat and Psi, models were developed for the rest experiments. The validation performance is reported as Nash-Sutcliffe efficiency (NSE) and relative bias in percent (pBias) (Table 3). High positive NSE values (close to 1) indicate that the model's predictions are in excellent agreement with the observed data. pBias with values closer to zero indicating better model performance.

Figure 2 displays a framework illustrating the calibration and simulation process of models. The simulations were iteratively repeated, considering all methods of roughness estimation. A total of 104 runs were simulated, each representing different sites or rainfall events, and repeated for various roughness methods, resulting in 832 simulations. However, models associated with Run 2 and 3 at Site 14, as well as Run 1 at Sites 12 and 16, were excluded from NSE assessment due to the absence of

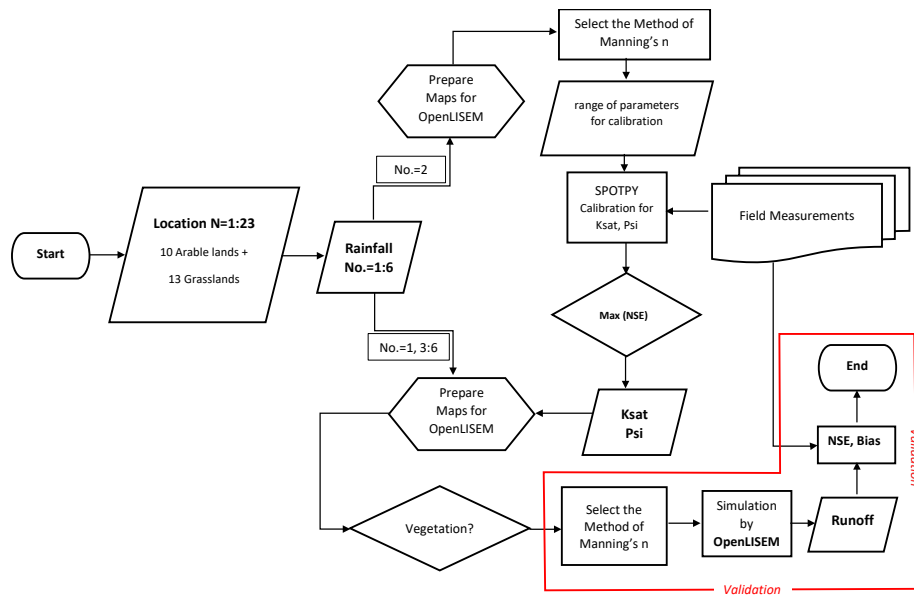


runoff in these experimental runs. Since the observed data were zero, the NSE could not be calculated. Nevertheless, based on a comparison between the simulated hydrographs and the corresponding MSE values, the differences between the simulations and observations indicate that the model performance is acceptable.

**Table 3: Criteria of NSE value (Motovilov et al., 1999) and pBias.**

NSE value	pBias value	Interpretation
$0.75 < \text{NSE}$	$-10\% < \text{pBias} < 10\%$	Good
$0.36 < \text{NSE} < 0.75$	$-50\% < \text{pBias} < -10\%$ or $10\% < \text{pBias} < 50\%$	Qualified
$\text{NSE} < 0.36$	$\text{pBias} < -50\%$ or $50\% < \text{pBias}$	Not-Qualified

235



**Figure 2: Framework for calibration and validation of the models.**

## 2.4 Initial soil moisture

240 Initial soil moisture plays a critical role in hydrological modeling, as it directly influences the partitioning between infiltration and surface runoff. Soil moisture measured at two points at each site was used in the runoff modeling.

In addition, the sequence of six rainfall-runoff experiments (Runs 1–6, as shown in Table 2) was considered, which involved varied antecedent moisture conditions, ranging from dry to saturated. This experimental design provides a general representation of initial soil moisture states.

245 Therefore, in addition to point-based measurements, considering the antecedent moisture conditions of each run enhances the interpretation of simulation results and improves understanding of the hydrological model's response.

## 4 Result

### 4.1 Calibration of different roughness methods

250 During the calibration process using various roughness estimation methods, the simulated hydrographs generally aligned well with observed hydrographs across most sites. For instance, Figure 3 compares the calibrated hydrographs at site 6, where



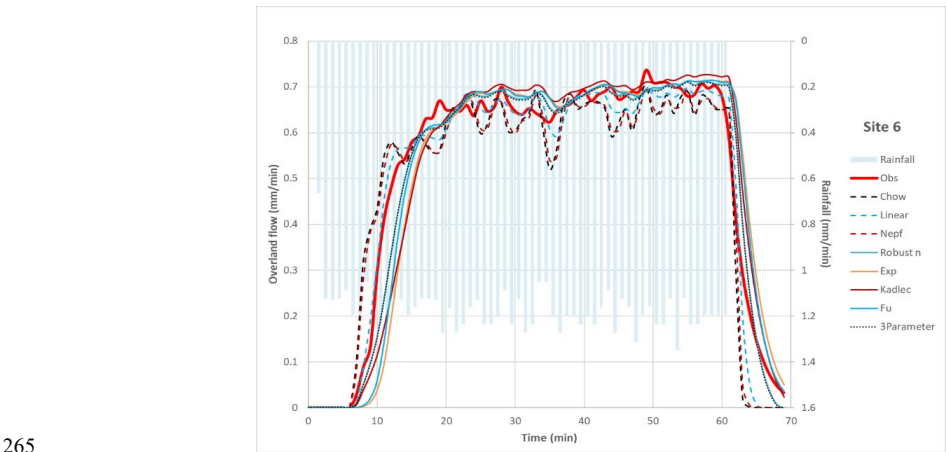


simulated results successfully capture the temporal pattern of measured discharge for other sites; the results are presented in supplementary data. The NSE values for all sites are summarized in Figure 4. Additionally, the pBias values, computed using the calibrated Ksat and Psi parameters, are presented in Figure 5. A larger deviation of pBias from zero typically indicates a less accurate calibration.

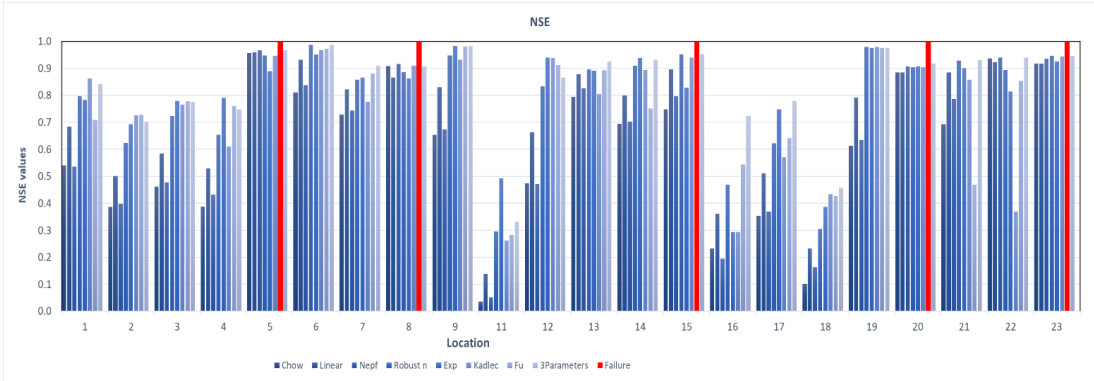
255 Overall, the NSE values obtained from different roughness estimation methods showed limited variation at each site. However, Fu's method yielded poor calibration performance at Sites 5, 8, 15, 20, and 23, shown by negative NSE values and a pBias of -100. These results indicate a complete failure of the Fu method to simulate runoff at these locations, with the modeled hydrographs resulting in zero discharge.

Unfavorable calibration performance was also observed at Sites 11 and 16, where all roughness estimation methods produced

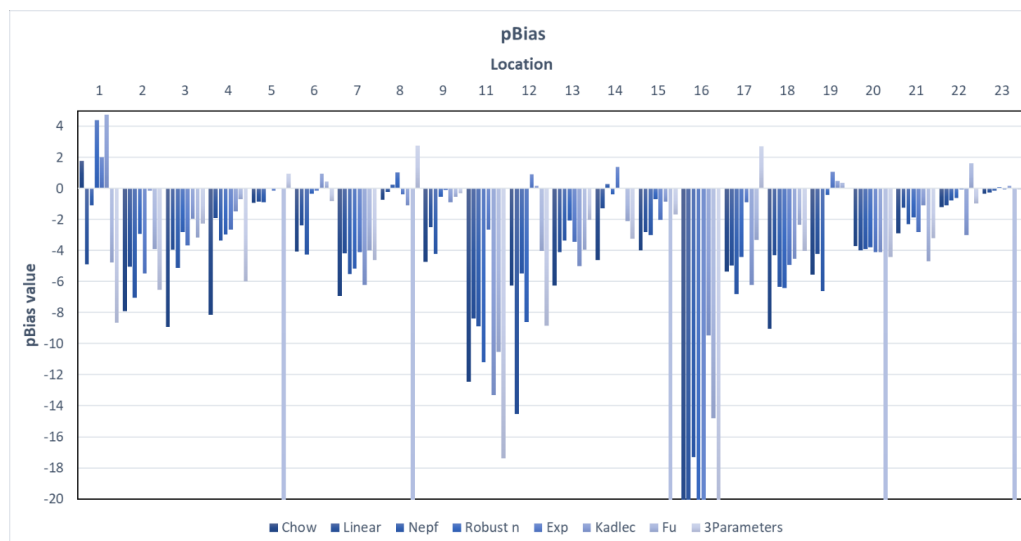
260 relatively low NSE and pBias values. It indicates a significant discrepancy between the observed and simulated hydrographs. In contrast, the remaining sites showed satisfactory calibration results using all methods except Fu's. Excluding Sites 11 and 16, the NSE values across other locations, except Fu's method, generally ranged between 0.65 and 0.87, reflecting an acceptable level of model performance.



265 **Figure 3: Comparison of the hydrograph computed using OpenLISEM with various roughness coefficient methodologies against the observed discharge.**



270 **Figure 4: Maximum model performance (Nash-Sutcliffe-Efficiency) for the calibration runs of the different roughness models, separated for each site. The red bars show model failure.**



**Figure 5: pBias values for parameters calibration of the different roughness models, separated for each site. Rainfall simulation Run 2 has been used for calibration, except for sites 1 and 14 (see section 3).**

Runoff is generally underestimated by the model, only 13% of the runs show a slight overestimation ( $< 5\%$  bias). 59% of the model runs underestimate the measured runoff by less than 5%, while 21% of the runs are underestimated by 5 – 15% of the runoff. Massive underestimation of runoff ( $>15\%$ ) happens outside at 5 runs using Fu's equation for surface roughness, while the runoff at site 16 is underestimated by most model runs, which is connected to the low total runoff at this site.

Table 4 presents a summary of the calibrated values of saturated hydraulic conductivity and average soil suction at the wetting front, calculated using different methods across all sites. In the case of Fu's method, the Ksat values for sites 5, 8, 15, 20, and 23 differ significantly from those obtained using other methods. These discrepancies suggest that Fu's method does not perform well in calibrating Ksat at these specific sites. The highly negative NSE values of the Fu method at these sites further support this observation. Additional results are presented in detail in the supplementary data.

A comparison of Ksat values shows that the differences between roughness methods are generally not significant, P-value=0.94, across sites. However, the values of Psi for different roughness methods show differences, P-value=0.038. By considering the soil type at each location and comparing the calibrated Ksat and Psi values with the estimates provided by Rawls et al. (1982), it becomes evident that the calibrated values are consistently higher across all sites. The only exceptions are Sites 8 and 9, which have sandy loam soils; in these cases, the calibrated values closely match those estimated by Rawls et al. (1983).

Since this discrepancy occurs across all roughness function methods, it suggests that the difference is not related to the choice of roughness method. Rather, it highlights a potential limitation of applying simplified, texture-based infiltration parameters to complex field conditions. Factors such as macropores or root development may influence soil hydraulic behavior and lead to higher infiltration rates than those predicted using generalized soil texture classifications.

Table 4: Statistical summary of calibrated parameters, Ksat (mm/hr) and Psi (cm), by site for different roughness methods.

Site No.	1	2	3	4	5	6	7	8	9	11	12
Range- Ksat	49.8- 53.9	35.5- 41.6	32.3- 37.5	30.4- 34.7	5.7- 13.2	26.0- 29.7	30.4- 33.4	7.4- 11.4	5.0- 8.6	35.8- 39.8	45.6- 47.9
Avg- Ksat	52.6	38.6	34.2	31.9	11.9	27.7	32.0	8.7	6.4	38.2	46.9
Range- Psi	1.5- 50.0	18.8- 49.9	19.5- 50.0	19.6- 49.7	0.1- 50	0.0- 48.0	16.5-49.7	0.1-19.0	11.1- 49.7	18.6- 49.9	16.0- 49.9



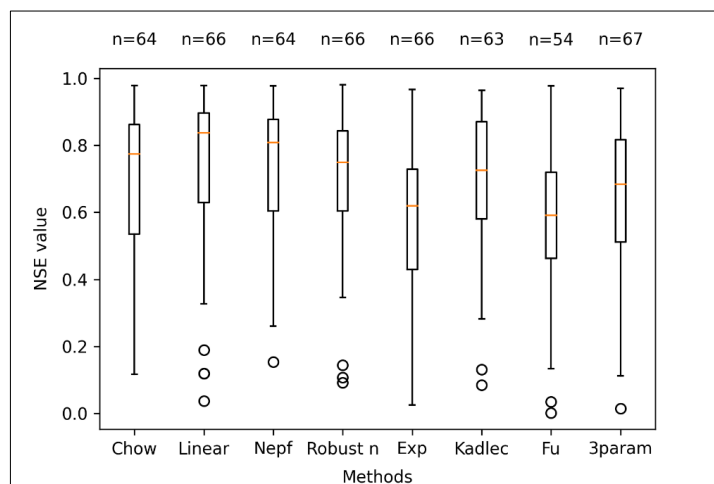
Avg- Psi	37.7	45.6	45.5	45.2	23.1	15.0	40.1	4.0	30.5	45.5	43.9
Site No.	13	14	15	16	17	18	19	20	21	22	23
Range- Ksat	38.2- 40.3	56.8- 63.7	36.4- 85.9	68.9- 70.3	24.6- 30.5	37.7- 41.2	9.0- 14.6	5.0- 94.7	5.0- 6.9	11.2- 15.5	7.2- 18.3
Avg- Ksat	39.1	60.2	43.3	69.6	28.2	39.1	11.0	16.3	5.5	14.4	8.7
Range- Psi	19.4- 49.7	18.4- 49.9	0.9- 49.7	19.9- 49.0	19.7- 49.9	19.2- 49.9	0.4- 49.9	2.4- 49.4	3.8- 47.6	0.1- 48.8	1.7- 45.4
Avg- Psi	41.8	45.5	27.0	41.5	45.8	45.2	30.8	36.8	23.3	12.7	19.4

#### 4.2 Validation of different roughness methods

The outcomes of validation reveal that the maximum NSE range is 0.96-0.98 for different methods. Depending on the type of method, the number of models with negative NSE varies between 29 and 46, of which most of them are Run 1 and Run 5.

300 Given that greater NSE values indicate more efficiency of the model in simulating runoff, we focused our investigation on the distribution of positive NSE values by excluding these underperforming models. Figure 6 illustrates the distribution of NSE for values greater than zero. The results indicate that the Linear and Nepf methods perform better in estimating runoff compared to the other methods; however, the differences are not statistically significant. ANOVA analysis on NSE values reveals significant differences between all group means, including Fu and Exp (P-value =  $1.3 \times 10^{-11}$ ). In contrast, when excluding Fu and Exp from the analysis, no significant differences are observed among the remaining roughness methods (P-value = 0.4).

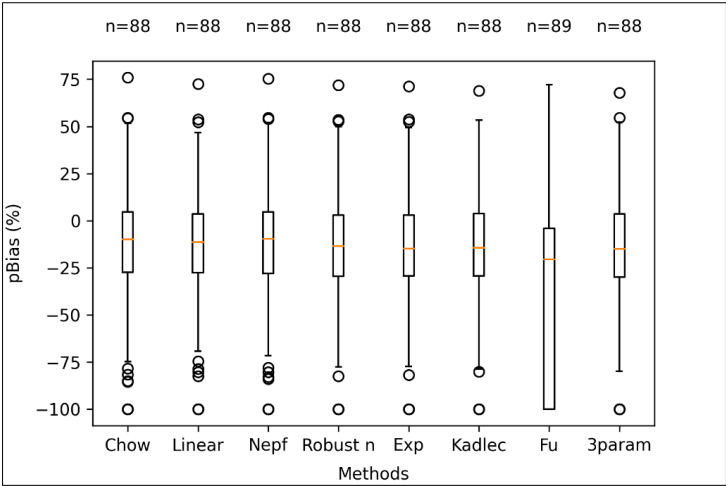
305



**Figure 6: Distribution of the absolute values of NSE for each method of roughness for the validation runs.**

The pBias results for the simulated hydrograph compared to the measured hydrograph exhibit a broad range from -100% to 100% in Figure 7. It is evident that all the methods exhibit almost a consistent trend, with the majority showcasing model bias consistently below zero. This suggests an underestimation across various roughness estimation methods. However, ANOVA analysis of the pBias values for all methods excluding Fu indicates no statistically significant difference between group means (p-value = 0.99).

310



**Figure 7: Distribution of the pBias for each method of roughness for the validation runs.**

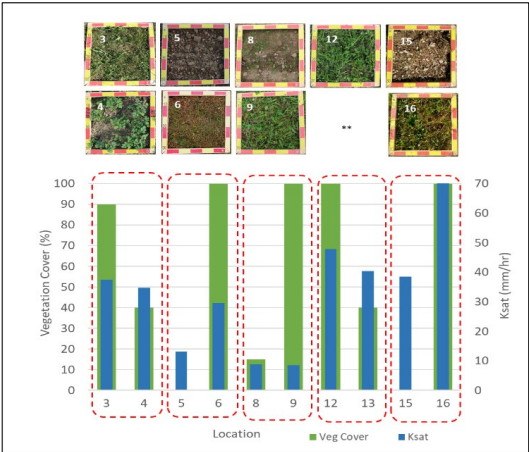
315 The analysis reveals that the Nepf, Linear, and Chow methods exhibit the most favorable performance, with 39, 38, and 34 models falling into the "Good" category based on NSE values. Conversely, for Robust n, Kadlec, 3-parameter, exponential, and Fu methods, 33, 29, 25, 15, and 9 models respectively meet the "Good" NSE criteria. Interestingly, pBias values across different methods are relatively comparable. Nepf, Chow, Linear, and 3-parameter demonstrate particularly robust performance, each with 27, 27, 26, and 26 models falling within the -10% to 10% bias range. This consistency in bias values  
320 suggests a commendable performance by these models based on pBias criteria.

**4.3 Effect of initial condition and pre-event soil moisture**

The validation outcomes of the roughness methods revealed Run 1 (dry conditions) and Run 5 (saturated conditions) generally shows poor model performance, with most of the methods. From the 36 model runs with negative NSE using the Nepf method, 30 are from Runs 1 and 5, as an example. Run 1 tends to overestimate runoff (positive pBias), while Run 5 underestimates it  
325 (negative pBias). The extremely low observed runoff in Run 1 makes NSE highly sensitive and often unreliable. On the other hand, these weak performance for Run1 and Run5 in comparison others may because of the different on the initial condition of models with Run 2 which was selected for calibration.

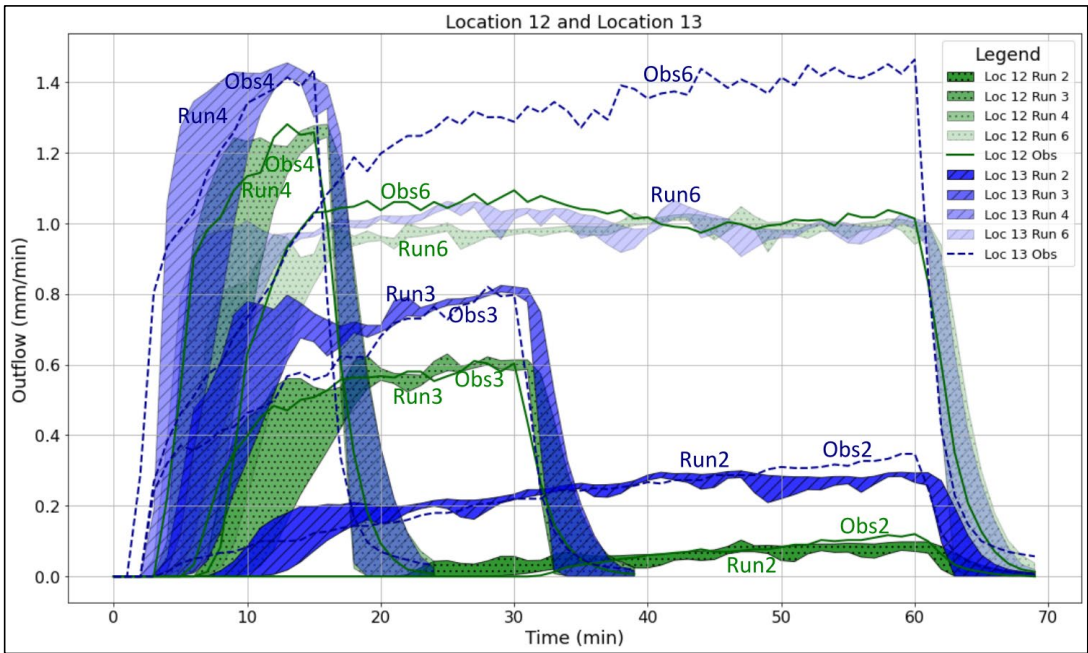
**4.4 Result of different vegetation coverage**

The spatial proximity between the paired experimental sites offers a unique advantage in the research, providing an environment where variations in soil characteristics can be minimized, enhancing the validity of the comparative analysis.  
330 In Figure 8, a comparative analysis between vegetation cover and Ksat, as determined by the Chow method, is presented. Comparing the pair sites reveal an increase in Ksat corresponding to more vegetation coverage. Notably, the contrast in Ksat is particularly pronounced between sites 15 and 16. Site 15, characterized as devoid of vegetation cover, displays a stark difference from site 16, boasting 100% vegetation coverage. The calibration results underscore this disparity, indicating a  
335 substantial Ksat difference of approximately 30 mm/hr. Conversely, for sites 8 and 9, this difference in Ksat is minimal. It's noteworthy that, although Ksat values may show only slight differences, another critical parameter influencing infiltration, Psi, exhibits a substantial contrast between sites 8 and 9. As presented in Table 4, the average of Psi value in site 9 is 30.5 cm; however, this value for site 8 is 4 cm. Specifically, Psi is higher for site 9 than site 8, resulting in an enhancement in infiltration. This highlights the relationship between various parameters and their  
340 combined impact on the overall dynamics of infiltration.



**Figure 8: Saturated hydraulic conductivity values for various land uses in paired sites. \*\* The vegetation cover images are from Ries et al. (2020). There is no picture for Site 13.**

As an example, the result for pair sites 12, 13 are shown in Figure 9. Site 12 with 100% vegetation cover and site 13 with 40%  
345 show different hydrographs both in observation and simulation. The results for Runs 2, 3, 4, and 6 are presented in this figure.  
For these runs, the model performs well, and the differences between observed and simulated values are not significant, the  
result for the other paired locations are shown in the supplementary material (Masoodi and Kraft, 2025). In these figures solid  
lines show the observed hydrographs and the shaded areas show the spread of results from different roughness methods. The  
green shaded area shows the results for the location with more vegetation cover. The spread of simulations is much larger for  
350 location 13, with less vegetation. It means in the presence of vegetation; the infiltration rate is higher than in places with less  
vegetation cover.



**Figure 9: Comparison of observed, solid lines, and simulated hydrographs, shaded areas, at sites 12 and 13 using different roughness methods for Run2, 3, 4, and 6.**



355 An example illustrating the model results with weak performance in Runs 1 and 5 is presented in Figure 10, which shows the  
outcomes for Sites 12 and 13. As discussed previously, the most models perform poorly for these two runs. A comparison  
between Figures 9 and 10 indicates that the weak performance in Runs 1 and 5 is not related to either the infiltration modeling  
or the roughness approach. This conclusion is supported by the fact that the infiltration modeling in the other runs (2, 3, 4, and  
6) shows acceptable agreement between observed and simulated values. The different roughness methods cannot account for  
360 the large discrepancies observed. This substantial variation may instead be attributed to the initial soil moisture conditions,  
which are discussed in Section 5.2.

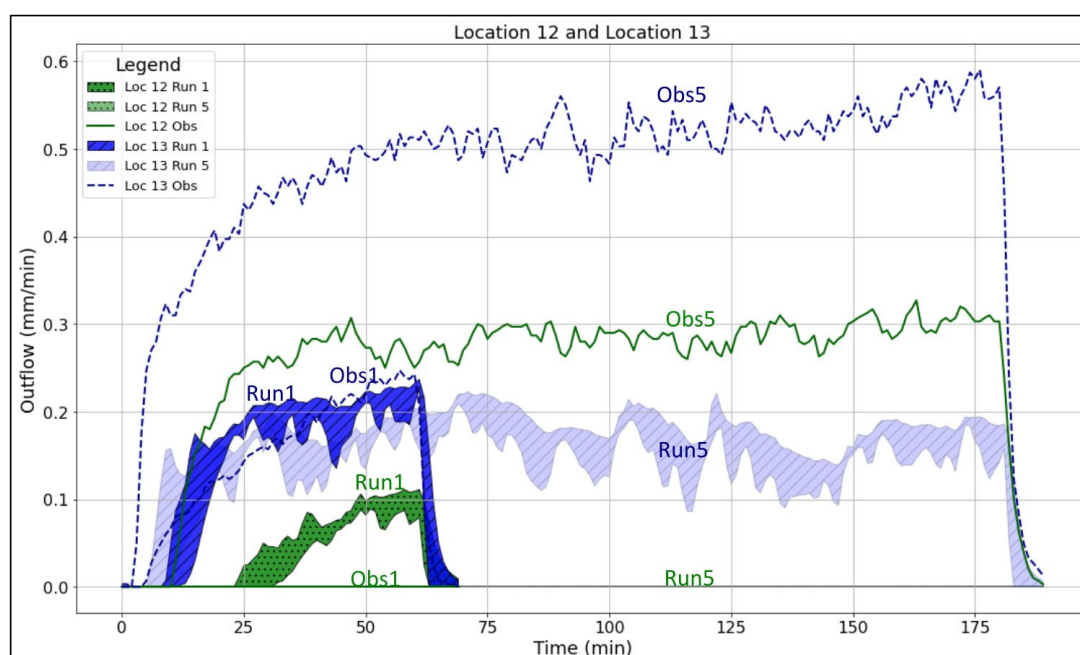


Figure 10: Comparison of observed, solid lines, and simulated hydrographs, shaded areas, at sites 12 and 13 using different roughness methods for Run1 and Run5.

365

## 5 Discussion

### 5.1 Validation of different roughness methods

Our study on the validation of various roughness estimation methods revealed that models using Fu's function yielded comparatively weaker simulation results compared to experimental data. This finding is consistent with Feldmann et al. (2023),  
370 who reported that Fu's equation typically produces lower NSE values, attributed primarily to the formula's limited adaptability. This limitation may stem from the fact that the function was developed based on laboratory experiments and is most applicable under similar controlled conditions where plant basal cover varied between 1.25% and 30%. Among the five sites where Fu's method completely failed during calibration, four lack vegetation cover, which may partially explain the poor model performance. An analysis of Fu's equation shows that when the value of vegetation cover,  $C_v$ , is less than 0.74, the parameter Manning's  $n$  decreases with increasing  $h$ , whereas for  $C_v$  values greater than 0.74,  $n$  increases with increasing  $h$ .  
375 This shift in behaviour may explain why Fu's method performs less effectively in runs without vegetation cover. In contrast, models based on Nepf, Linear, Chow, and Robust  $n$  methods, ranked in that order, demonstrated a closer match between the simulated and observed hydrographs. Although the differences in NSE values among these latter methods are not substantial,



their use in roughness estimation leads to simulated hydrographs that more closely represent those derived from physical  
380 observations. One notable strength of the Nepf and Linear methods is their incorporation of water-depth-dependent  
relationships in estimating roughness coefficients. This is in agreement with Hinsberger et al. (2022), who emphasized the  
critical role of water depth in influencing hydraulic roughness and highlighted the importance of integrating this factor into  
catchment-scale modeling. It should be noted that in our simulations, water depth remained below vegetation height, placing  
the system in an emerged flow regime. Under this condition, the performance of the applied methods is considered valid;  
385 however, further investigation is required to assess their accuracy under submerged flow conditions. Additionally, the  
improved performance of the Nepf method may also be attributed to its inclusion of the blockage factor, which effectively  
represents vegetation cover and enhances the simulation of overland flow. Although originally developed for channel flow,  
the Nepf method demonstrates strong alignment with physically measured hydrographs in overland flow scenarios as well.  
Therefore, further research is warranted to assess and refine its applicability in such contexts.

390 Our results using the 3-parameter method indicate that increasing the number of parameters during calibration can lead to  
greater model complexity, which may hinder the ability to efficiently identify optimal solutions. This increase in complexity  
can also negatively impact overall model performance. Similar findings have been reported in previous studies involving  
conceptual rainfall-runoff models. For instance, Zhu et al. (2024) concluded that increasing model complexity by adding more  
parameters often leads to challenges in calibration, including difficulty in parameter estimation and reduced calibration  
395 efficiency. Likewise, García-Romero et al. (2019) calibrated three hydrological models with varying levels of complexity,  
comprising 4, 10, and 16 parameters, across nine catchments. Their results demonstrated that simpler models required fewer  
iterations to reach convergence, whereas more complex models demanded significantly more computational effort.

The results of methods in which roughness values are derived using the approach of Feldmann et al.'s (2023) concept, including  
Kadlec, Robust n, Fu, and exponential, tend to exhibit greater deviation from experimental data. Figure 11 illustrates a  
400 comparison of the simulated hydrographs using different roughness estimation methods for all experiments conducted at site  
9. Site 9 is specifically chosen because its hydrographs were featured in Feldmann et al.'s (2023) study, and the calibration for  
the four methods employed therein is superior to that of the Linear and Nepf methods, as depicted in Figure 4. Figure 11  
demonstrates that Kadlec, Robust n, Exponential, and Fu methods approximate the falling limb of the hydrograph more closely  
to the observed hydrograph compared to the Linear, Nepf, and Chow methods. It's essential to note that the base of optimization  
405 in Feldmann et al. (2023) study is on the falling limb of the hydrograph, where it shows superior performance. However, the  
NSE results for the entire hydrograph are better for Nepf, Linear, and Chow.



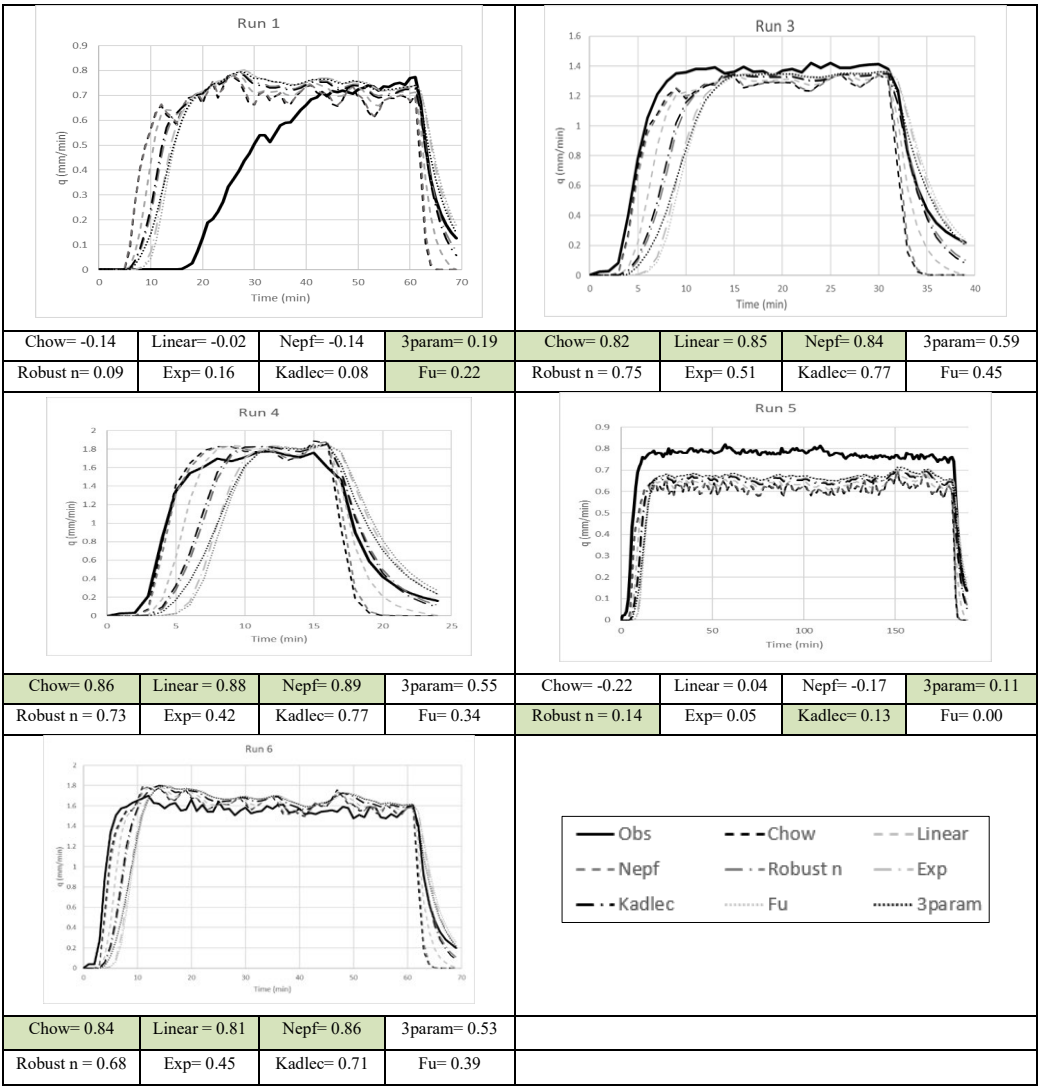


Figure 11: Comparison of validated and observed hydrographs at site 9. NSE values are calculated for the entire hydrograph, with green cells indicating methods that have higher NSE values.

This discrepancy may stem from the approach's omission of vegetation effects on infiltration parameters. Feldmann et al. (2023) proposed a more constrained roughness estimation method by identifying overlapping solution spaces and reducing the overall solution space to enhance reliability. Their methodology focuses on the falling limb of the hydrograph, where infiltration is assumed to remain relatively constant. They fitted an infiltration function to this segment of the hydrograph and derived infiltration rates without explicitly considering vegetation's role in modifying these rates. However, our findings suggest that vegetation significantly influences not only roughness coefficients but also key infiltration parameters, such as  $K_{sat}$ , thereby affecting overall infiltration dynamics. These results are consistent with the conclusions of Gao et al. (2023), who emphasized that soil hydraulic properties are influenced by both water movement and ecosystem activity. They highlighted the root zone as a critical component with substantial storage capacity, playing a key role in regulating how precipitation is partitioned into streamflow. According to their framework, vegetation actively alters soil characteristics to





optimize water availability, which underscores the importance of incorporating ecosystem and soil interactions into hydrological modeling.

## 5.2 Effect of initial condition and pre-event soil moisture

425 Our results highlight the significant influence of antecedent soil moisture conditions on runoff modeling accuracy, particularly in Runs 1 and 5 (Figure 10). Run 1 began with unusually dry soil, while Run 5 followed a sequence of moderate rainfall events (Runs 2, 3, and 4), leading to substantially wetter initial conditions. Both exhibited significant deviations between simulated and observed runoff, suggesting that the model struggled to replicate hydrological responses under extreme antecedent moisture states.

430 These findings are in agreement with Brocca et al. (2008), who demonstrated that pre-event soil moisture is a key determinant of runoff depth and peak discharge. Their conceptual soil water balance model incorporates Green–Ampt infiltration and non-linear drainage mechanism. In our study, models calibrated under a specific initial moisture condition (e.g., Run 2) yielded more reliable results when validated against runs with comparable antecedent states (e.g., Runs 3, 4, and 6). However, performance declined when these models were applied to scenarios with contrasting initial soil moisture (e.g., Runs 1 and 5), emphasizing the model’s sensitivity to calibration context. Feldmann et al. (2023) observed a decrease in median deviation from the roughness mean in Run 5 during prolonged rainfall events and attributed this to the formation of flow paths influencing roughness values. However, we suggest that this reduction may be linked to the effects of antecedent rainfall on runoff response, and not to rainfall intensity or flow path development. This is supported by the behavior in Run 6, where the deviation from the roughness mean increased again despite continued rainfall, indicating that the changes are not solely due to flow path formation.

440 Zehe and Blöschl (2004) investigated how uncertainty in initial soil moisture affects hydrologic responses at the plot and catchment scales, using a physical model that accounts for transitions between matrix and preferential flow. Their simulation results showed that model predictability is lowest near the soil moisture threshold separating these flow regimes in the soil. In the present study, Runs 1 and 5 represent transitional soil moisture conditions similar to those reported by Zehe and Blöschl (2004). Comparing the results of these runs highlight the difficulty of accurately predicting hydrological responses under uncertain initial soil moisture conditions. These findings are consistent with Zehe and Blöschl (2004).

We found that the response of our model under different soil moisture condition has uncertainty, particularly when soil approaches saturation. This discrepancy may stem from limitations in infiltration modeling under these conditions. For example, the Green–Ampt approach assumes an initially dry soil profile, which can result in unrealistic infiltration estimates during high-intensity storms on already wet soils. This limitation highlights the need for improved infiltration models that better accommodate a range of antecedent soil moisture conditions.

## 5.3 Result of different vegetation coverage

The findings presented in our study validate previous research, which has emphasized the differences in near-surface Ksat across various land covers (Zwartendijk et al., 2023). These differences result in different shaping perched water table dynamics and overland flow responses (Ghimire et al., 2020; van Meerveld et al., 2021; Zwartendijk et al., 2020, 2023). The study conducted by Wu et al. (2024) on the temporal variability of Ksat throughout the growing season revealed the significant influence of root growth. They explained that root development improves soil pore connectivity, thereby increasing Ksat. Consequently, top-soil infiltration rates typically experience improvement, resulting in reduced overland flow and a decrease or delayed runoff response to rainfall events (van Meerveld et al., 2019). Jarvis et al. (2013) identified land use as one of the top three most significant predictors for Ksat. They concluded that intensive cultivation of arable land significantly diminishes topsoil hydraulic conductivity compared to perennial agriculture, natural vegetation, and forests, by approximately 2–3 times. They attributed this reduction to the disruptive effects of tillage on macropores, including faunal and root bio pores.



Our research indicates that in the presence of vegetation, not only is surface roughness important in hydrological processes, but the increase in Ksat also significantly influences the response of hydrological models to runoff. This highlights the critical importance of incorporating vegetation-induced changes in hydraulic conductivity when modeling runoff responses. A great difference from the related studies by Feldmann et al. (2023) and Hinsberger et al. (2022) is the use of a model with an integrated infiltration model. Classical engineering models for surface runoff and most commercial models deal with infiltration as a process that can be determined a priori and subtracted directly from the rainfall. The ability of the soil to absorb water is dynamic in nature but is often oversimplified which led to inaccuracies (Beven, 2021). We used the dynamic Green-Ampt Infiltration model from OpenLISEM, and which captured the infiltration process in the majority of cases. Thus, the result is both a validation of expected trends and a contribution to understanding the importance of incorporating Ksat variability in hydrological models. While we observe the strong effect of vegetation on infiltration capacity, our data set is not sufficient to come up with a robust estimate to quantify this effect.

## 6 Conclusion

Our study evaluates of various roughness estimation methods and their impact on hydrological modeling using OpenLISEM. Through model calibration and validation, we have gained valuable insights into the performance of each roughness method. Our findings reveal that certain methods, such as Linear, constant Manning's n proposed by Chow, and the physical base method proposed by Luhar and Nepf (2013), demonstrate favorable performance in reproducing observed hydrological data, as evidenced by high NSE values and minimal bias. Methods like Fu's equation exhibit weaker simulation results, attributed to its limited adaptability and lower NSE values. The methods have been developed for submerged vegetation, but in our study, as for sheet flow events on vegetated surfaces in general, the runoff depth observed in this study did not exceed the height of the vegetation.

We observed notable differences in near-surface saturated hydraulic conductivity across various vegetation covers. The differences observed in model outcomes between various runs in one site highlight the need for improved models that accurately account for infiltration for varying antecedent conditions. Surface runoff models use vegetation solely as a parameter of surface roughness and rainfall runoff models as a transpiration parameter. For the effect of storm events in developed landscapes, vegetation is an important regulator of infiltration, yet this effect is not well represented in current models. Future studies should investigate which rainfall events yield better results when included in the calibration process. Selecting the most representative rainfall event should consider both dry and saturated soil moisture conditions, enhancing the accuracy of hydrological modeling. It is important to acknowledge the inherent limitations of hydrological models, which may influence our results. For instance, this model does not explicitly consider the effects of increased water pressure at higher water levels, which could also impact infiltration dynamics.

## Supplementary and Code availability.

Data are published in the zenodo.org repository under <https://doi.org/10.5281/zenodo.17572291>

Code is available on [https://github.com/philippkraft/openlisem/tree/modified\\_manning\\_console](https://github.com/philippkraft/openlisem/tree/modified_manning_console)

**Author contributions.** AM: Programming, Simulation, Data analysis, Manuscript draft writing.

PK: Conceptualization, Funding acquisition, Software development, Manuscript review and editing.

**Competing interests.** The authors declare that they have no conflict of interest.

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