



# Thermohydraulic Experiments on Water Infiltration in Frozen Slopes: The Role of Macropores and Initial Water Content

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**Abstract.** Infiltration of rainwater or snowmelt into frozen soil is strongly constrained by ice-blocked pore spaces, depending on the thermal and hydrological state. The resulting reduction in permeability promotes surface runoff, which can trigger erosion or debris flows. Preferential pathways such as macropores can locally bypass this barrier, yet their quantitative role has remained poorly constrained by experiments. Here, we present nine large-scale rainfall experiments in a tiltable soil box inside a controlled climate chamber, systematically varying initial water content and the presence or absence of an interconnected macropore network. The coarse textured soil was instrumented with a dense three-dimensional grid of temperature and volumetric water content sensors, complemented by continuous outflow monitoring of drainage and surface runoff. Frost depth was governed primarily by the antecedent thermal state and only weakly by the macropore network or initial water content. In contrast, infiltration/runoff partitioning depended strongly on initial water content and secondarily on the macropore network. Under low initial water content conditions, infiltration was dominated by matrix flow, whereas at high initial water content the frozen matrix became effectively impermeable and the macropore network enabled rapid bypass infiltration. Progressive refreezing and particle-assisted clogging reduced macropore functionality over time, shifting flow towards surface runoff. These results reveal the transient, non-linear role of macropore networks in frozen soils and provide a benchmark for testing dual-domain and non-equilibrium models relevant to process representation in alpine hydrology and slope stability.

## 1 Introduction

According to the Copernicus Climate Change Service, 2024 was the warmest year on record globally, with mean surface temperatures exceeding pre-industrial levels by more than 1.5 °C (Copernicus Climate Change Service (C3S), 2025). Especially amplified is the warming in high latitude and alpine regions, consistent with elevation-dependent warming observed in many mountain ranges (Wang et al., 2013; Gobiet et al., 2022; Bliss et al., 2024). Frost days have already declined markedly, alongside reductions in snow cover, permafrost extent, and seasonal snowpack (Bednar-Friedl et al., 2022). These changes lead to more frequent freeze-thaw cycles and intermittent snow-free periods. Recent work highlights that climate impacts in mountain regions can occur not only gradually but also through sudden, non-linear shifts, where small additional warming can trigger pronounced responses in soil processes (Zeng et al., 2025). Total winter precipitation is projected to remain stable or increase



in many regions, with a larger fraction falling as rain rather than snow (Ranasinghe et al., 2021; Beniston et al., 2022; Fuentes-Franco et al., 2023). In mountain catchments with seasonally frozen ground, this implies more frequent exposure of frozen soils to liquid precipitation or intense snowmelt during winter and spring (Ala-Aho et al., 2021). While snow modulates winter hydrology in natural systems, we focus here on rainfall onto snow-free but frozen soils to isolate subsurface thermo-hydraulic responses.

Rainfall on frozen ground can produce contrasting hydrological responses. Liquid precipitation may infiltrate and percolate downward, contributing to groundwater recharge, and may locally induce thawing or refreezing along its pathway. However, in frozen soils, matrix infiltration is strongly impeded by ice blocked pores that drastically reduce hydraulic conductivity (Dingman et al., 1975; Burt and Williams, 1976; Kane and Stein, 1983). This limits vertical percolation and promotes water accumulation at the surface. On slopes, this can lead to surface runoff or lateral flow along the soil-air interface, accelerating event runoff and potentially reducing groundwater recharge (Dunne and Black, 1971; Covino, 2017). Each pathway may have implications for slope stability. Infiltration and associated thawing can elevate pore water pressures and reduce effective stress, increasing failure potential, whereas surface runoff can mobilise sediment and initiate erosion, potentially triggering landslides or debris flows (Iverson, 1997; Baselt and Heinze, 2021; Li et al., 2024). The dominant response reflects an interplay between soil structure (grain size distribution, porosity, packing density, macroporosity) and thermo-hydraulic states and forcings (soil temperature, freezing state, rain water temperature, initial water content) (Baselt and Heinze, 2021). The vertical distribution of liquid water, the associated hydraulic conductivity, and the potential for ice occurrence are key controls on infiltration under seasonally frozen conditions (Demand et al., 2019; Stuurup et al., 2021).

Pore architecture is especially important under frozen conditions because ice formation differs between micro- and macropores (Mohammed et al., 2018; Baselt and Heinze, 2021). In micropores (packing voids), ice grows from the pore centre toward the solid boundary. Within macropores (equivalent pore diameters typically  $> 0.05$  mm, formed by cracks, root channels, or fauna) (Hartge et al., 2014), freezing initiates at the walls and advances inward, lining conduits and altering both flow and heat transfer (Watanabe and Kugisaki, 2017). This asymmetry controls the temporal evolution of infiltration pathways during sub-zero events. Preferential flow through a macropore network can bypass the frozen micropore matrix and enable rapid, gravity-driven infiltration (Johnsson and Lundin, 1991; Stähli et al., 1996; Beven and Germann, 2013). A macropore network also affects the thermal regime by enhancing advective heat transport and promoting localised thawing (Watanabe and Kugisaki, 2017; Mohammed et al., 2018). Preferential pathways can, however, be interrupted when conduits within the macropore network refreeze from the walls inward, rapidly reducing hydraulic capacity. On inclined terrain, such transitions strongly affect the partitioning between infiltration and surface runoff and thus geohazard potential.

Although the significance of coupled thermo-hydraulic processes and macropore networks is recognised, several widely used hydrological and slope stability models (e.g. GEOtop (Endrizzi et al., 2014), SWAT (Arnold et al., 1998), TRIGRS (Baum et al., 2008), r.slope.stability (Mergili et al., 2014)) still treat the subsurface as a single continuum under local thermal equilibrium, neglecting preferential flow. Other frameworks (HYDRUS (Šimůnek et al., 2016), WaSiM (Schulla, 2012)) include macropore network or dual-domain representations. HYDRUS offers a freezing/thawing module that couples water, vapour,



and heat transport (Hansson et al., 2004). GEOtop and WaSiM include physically based (GEOtop) or parameterised (WaSiM) freeze/thaw modules. Nevertheless, the combined representation of preferential flow and freeze/thaw in seasonally frozen soils remains poorly developed and rarely constrained by experiments (Mohammed et al., 2018; Larsbo et al., 2019; Heinze, 2021). Traditional Richards-based approaches further assume matrix dominated flow and local thermal equilibrium, which may be inaccurate under strong thermal gradients or pronounced preferential flow (Hansson et al., 2004; Kurylyk et al., 2014; Grenier et al., 2018; Heinze, 2021). Recent developments, including dual permeability approaches (Larsbo et al., 2019) and multiphase local thermal non equilibrium (LTNE) frameworks (Heinze and Blöcher, 2019), provide more realistic process representations, but their predictive skill still hinges on validation against empirical data.

At the field scale, macropore network-driven infiltration under frozen conditions has been observed (Stähli et al., 1999, 2004; Webb et al., 2018; Fang et al., 2024), but boundary conditions such as volumetric water content, frost depth, and rainfall intensity are difficult to constrain, and heterogeneity complicates attribution. Consequently, deriving process resolved insights into macropore network controls under natural conditions remains challenging. Laboratory studies have largely focused on small soil columns, which yielded valuable insights into water redistribution, freezing behaviour, and preferential flow in partially frozen soils (Stadler et al., 2000; Weigert and Schmidt, 2005; Watanabe and Kugisaki, 2017; Pittman et al., 2020). The influential study by Watanabe and Kugisaki (2017) showed that introducing artificial macropores (implemented there as single vertical conduits) can delay freezing and promote infiltration, but may refreeze rapidly from the walls inward and block flow. Those experiments, however, used highly idealised configurations: vertical columns with homogeneous fine-textured material, constant thermal gradients, continuous vertical macropores, and ponded infiltration at constant head via a Mariotte bottle. Lateral flow, surface runoff, and geomorphic feedbacks were not represented. In particular, the role of interconnected macropore networks and their dynamic switch between infiltration and blockage remains insufficiently constrained. To our knowledge, no prior experimental study has systematically investigated these coupled thermo-hydraulic processes in a three-dimensional soil body under seasonally frozen conditions while accounting for slope angle, soil structure, and event-scale precipitation characteristics.

Here, we present large-scale laboratory experiments designed to test how an artificial, reproducible, and interconnected macropore network influences thermo-hydraulic processes in seasonally frozen soils across different initial water content states. We evaluate how initial water content and the macropore network influence frost depth and freezing dynamics prior to rainfall, and how they subsequently affect the thermal response and the partitioning between infiltration, drainage, and surface runoff once rainfall begins. We further examine how ongoing refreezing during infiltration modifies macropore network functionality, including flow path continuity and the capacity to bypass frozen pore space.

By systematically controlling slope, initial water content, and thermal boundary conditions in a three-dimensional soil body, we provide new insights into cold region infiltration dynamics under conditions representative of alpine environments.



## 90 2 Methods

### 2.1 Experimental setup and instrumentation

The large-scale experiments were conducted in the laboratory for Hydromechanics and Hydraulic Engineering at the Universität der Bundeswehr München. To replicate rainfall on frozen alpine slopes under controlled conditions, two existing water basins in the institute's experimental hall were converted into a fully integrated large-scale experimental facility. The infras-  
 95 tructure allows the use of substantial soil volumes under precisely controlled hydraulic and thermal boundaries, combining structural flexibility with realistic environmental conditions (Fig. 1). Key components of the experimental setup include:

- A walk-in climate chamber (exterior dimensions: 4.1 m × 3.4 m × 2.4 m). The sidewalls are constructed with a double layer of extruded polystyrene foam insulation enclosed between plywood panels and a wooden frame. The floor and ceiling are insulated with a single layer of extruded polystyrene foam. The chamber is equipped with a 2.5 kW cooling unit (Viessmann Tecto RF WMC3), enabling stable air temperature control in the range of  $-5^{\circ}\text{C}$  to  $+15^{\circ}\text{C}$  (Fig. 1a).  
 100
- A PVC soil box (exterior dimensions: 160 cm × 90 cm × 60 cm), which can be filled with approximately 0.87 m<sup>3</sup> of soil (about 1500 kg). The box is thermally insulated along the bottom and side walls to minimise heat exchange with the surrounding environment and to ensure that freezing initiates exclusively at the air-soil interface, akin to natural conditions. It can be tilted from 0° to 20° to simulate natural slope conditions (Figs. 1b and 2a). The bottom is filled with  
 105 honeycomb-structured plates acting as a drainage layer, overlaid with geotextile to prevent sedimentation and blockage of the drainage layer.
- A rainfall simulator equipped with a dual-fluid nozzle is positioned 50 cm above the soil surface (Fig. 1b). This setup produces a fine, evenly distributed spray with droplet sizes that are characteristic of laboratory rainfall simulators. The setup ensures homogeneous surface wetting and controlled rainfall flux while avoiding splash or soil sealing effects. The  
 110 nozzle is moved by a motor, reversing directions automatically to ensure even water distribution over the area. Each complete cycle (returning to the starting position) lasts about 20 s. It is enclosed in an acrylic glass housing to minimize overspray. The system allows rainfall intensities ranging from 2 to 20 L h<sup>-1</sup>.
- A macropore pattern plate (Fig. 1c) made of 3 cm thick PVC with 60 guided boreholes (plus 60 individual steel rods). The boreholes were drilled at various inclinations in the horizontal and vertical directions, leaving two principal angles. The boreholes were drilled at various inclinations in the horizontal and vertical directions, leaving two principal angles.  
 115 practical manufacturing constraints limited the second angle. About 28 % of the boreholes were fully vertical, while the remaining boreholes were at least slightly tilted. The steel rods varied in length, with about 20 % not reaching the soil bottom (dead ends). Each borehole was assigned an individual rod, which was inserted to create the macropore pattern. The angles and rod lengths were selected such that about 15 % of the rods were in contact with each other. After insertion, the rods were removed, leaving open cylindrical pores within the soil body, including interconnections and  
 120 dead ends. The artificially created macropore network comprised both interconnected and dead-end pores, representing a simplified analogue of natural macropore systems (e.g. Jarvis, 2007; Beven and Germann, 2013).





(a)



(b)



(c)



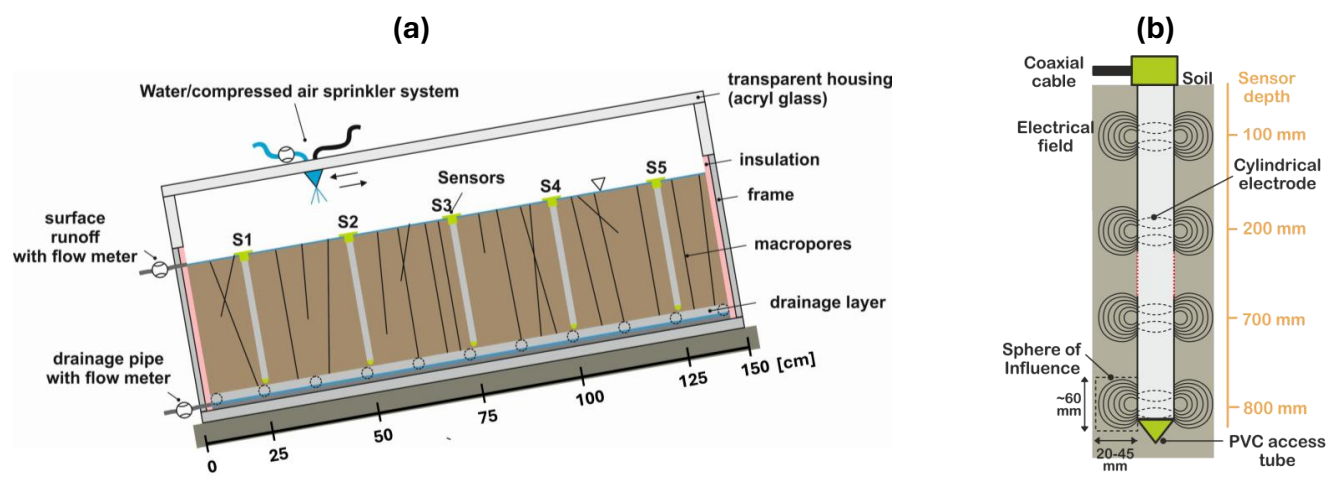
(d)



**Figure 1.** Photographic overview of the large-scale experimental facility. (a) Climate chamber, (b) soil box tilted to  $10^\circ$  with rainfall simulator mounted, (c) macropore pattern plate with rods inserted to visualise the artificial pore network, (d) AquaCheck probes for soil moisture and temperature sensing (as seen in a field application).



Despite the straight geometry of the pores, this configuration enables reproducible studies of connectivity effects on infiltration into frozen soil (Watanabe and Kugisaki, 2017). The rods had a diameter of 10 mm, resulting in a total macropore volume of approximately  $4 \times 10^{-3} \text{ m}^3$ , corresponding to a volume fraction of 0.5 %. This value lies within the lower bound of typical macropore fractions reported for soils (Hartge et al., 2014), although the pore diameter is at the coarse end of the natural range.



**Figure 2.** Schematic representation of the experimental system. (a) Side view of the soil box with rainfall simulator (not to scale), drainage and surface runoff outlets (with flow meters), and vertically installed probes. Macropore configuration is only shown schematically. (b) AquaCheck probe schematic (not to scale), indicating eight capacitance-based water content sensors and integrated thermocouples. Shaded areas represent approximate measurement influence zones.

Reverse osmosis treated water was supplied from a cooled reservoir (1 °C, 130 L) to ensure controlled irrigation temperatures and was pumped into the climate chamber. An addition of 3 g NaCl per 130 L was used, which is negligible for freezing behaviour but sufficient to provide electrical conductivity for the flow meter measurements.

- 130 To monitor the thermo-hydraulic conditions inside the soil body, ten AquaCheck profile probes were vertically installed (Figs. 1d and 2b). Each probe is a cylindrical rod (3 cm diameter) equipped with eight measurement pairs (capacitance sensor for measuring soil moisture and a thermocouple sensor for measuring temperature) spaced at 10 cm intervals vertically. Figure 2b schematically illustrates one probe. The probes were arranged in two parallel lines across the box width, with five probes per line (S1–S5) and 25 cm spacing in the longitudinal direction (the detailed sensor layout is shown in Appendix B).
- 135 To improve vertical resolution and avoid interference, one line was offset vertically by 5 cm. This configuration provided a total of 80 distinct measurement locations.

Hydrological fluxes (irrigation inflow, surface runoff, and drainage outflow) were recorded using three inductive flow meters (type SM4000, ifm electronic). The devices detect flow rates as low as  $0.005 \text{ L min}^{-1}$ , ensuring accurate measurements even under low flow conditions.



## 140 2.2 Soil characteristics

The soil used in the experiments was an artificial mixture designed to reproduce the texture and hydraulic behaviour of coarse alpine soils. It was blended from individual grain size fractions to achieve a realistic structure while ensuring reproducibility across all experiments. The final mixture consisted of approximately 25 % gravel, 60 % sand, and 15 % silt, based on reference samples from the Reiteralpe region in the German Alps (Fig. D1). Coarse particles larger than 8 mm and fine particles smaller  
 145 than 0.02 mm were deliberately excluded. This constraint prevented preferential flow along large gravel contacts within the limited soil box volume and avoided clogging of the drainage layer by fine material. The resulting soil exhibited a homogeneous packing structure and stable hydraulic properties across all runs. The dry bulk density of the mixture was approximately  $1755 \text{ kg m}^{-3}$ , characteristic of coarse-textured, clay-poor soils with low organic content (Poesen and Lavee, 1998; Aşkin and Özdemir, 2008). The effective porosity was estimated at about 0.16, which aligns with dense, sand-rich sediments (Hölting and  
 150 Coldewey, 2019). The median grain diameter ( $d_{50}$ ) was roughly 1.2 mm. These properties ensured that the matrix remained dominated by primary pores while still allowing measurable interaction with the macropore network. The saturated hydraulic conductivity ( $K_{\text{sat}}$ ) was estimated as  $6.5 \times 10^{-7} \text{ m s}^{-1}$  using the HYDRUS 1D model and measured input parameters. This value is consistent with well-packed sandy materials of comparable grain size. Because the main purpose of the experiments was to isolate thermo-hydraulic processes rather than to simulate specific field sites, the simplified grain composition provided  
 155 both hydraulic representativeness and experimental repeatability. The detailed grain size distribution of the artificial soil is provided in Appendix D.

## 2.3 Experimental scenarios and procedure

A total of nine experiments were conducted under different combinations of freezing conditions, macropore network presence, and initial water content (Table 1). Seven experiments were performed under frozen conditions, covering roughly three initial  
 160 saturation levels (approximately 60 %, 75 %, and 95 %). Each saturation level included one run with and one without a macropore network. The high volumetric water content (VWC) macropore network case was repeated to confirm the reproducibility of key outcomes. Two additional reference experiments were carried out under non-frozen conditions.

Before each experiment, the soil and the required amount of water were homogeneously mixed using a pug mill mixer to achieve the target initial water content. The soil was then filled into the PVC box in five successive layers. For each layer, the  
 165 volumetric water content was verified using the oven drying method. After filling, a macropore network was created in half of the experiments by inserting steel rods through the macropore pattern plate (see Fig. 1c). The rods were subsequently removed, leaving an open macropore network with interconnected conduits and dead ends. The prepared soil box was then placed inside the climate chamber and subjected to freezing at  $-5^\circ\text{C}$  for 105-120 h. After the freezing phase, the box was tilted to  $10^\circ$ , and rainfall was applied using the dual-fluid nozzle. During irrigation, the air temperature in the climate chamber was increased  
 170 to  $+1^\circ\text{C}$  to prevent equipment freezing and to simulate mild winter rainfall. Irrigation rates averaged approximately  $5 \text{ L h}^{-1}$  and were maintained for up to 20 h (see Table 1). The irrigation water temperature differed slightly from that of the reservoir because the water passed through the inductive flow meter, which caused minor heating, followed by slight cooling when



mixed with decompressing air in the nozzle. To account for these variations, the water temperature was monitored manually. As shown in Table 1, the average water temperature varied between experiments ( $\Delta T \approx 1.6^\circ\text{C}$ ) due to these combined effects and measurement uncertainty. Control measurements were taken every few hours by transferring small samples into a secondary container and measuring them with a handheld thermometer.

VWC and temperature within the soil were recorded by the AquaCheck probes at one minute intervals starting from the onset of freezing. Flow meters continuously logged irrigation inflow, drainage, and surface runoff at 10 Hz. The data were subsequently averaged to one minute intervals to synchronise with the soil sensor measurements. Although the rainfall simulator produced consistent droplet characteristics and reproducible intensities, minor variations in total inflow rate ( $4.1\text{--}5.6\text{ L h}^{-1}$ , see Table 1) occurred. These differences can affect the precise timing of drainage onset and cumulative discharge. Consequently, flow responses are interpreted relative to inflow volumes and initial soil conditions rather than in absolute terms. This approach ensures that any observed differences attributed to the macropore network or initial water content are not confounded by minor inflow variability.

**Table 1.** Overview of the parameter combinations used in the experiments. All experiments were performed at a slope angle of  $10^\circ$ . Acronyms were defined to enable a quick and unambiguous identification of each experiment: the first letter indicates frozen (F) or non-frozen (N) conditions, the second letter denotes the presence (M) or absence (N) of a macropore network, and the final number represents the rounded initial volumetric water content [%].

No.	Acronym	Scenario	Macropore diameter [mm]	Irrigation intensity [ $\text{L h}^{-1}$ ]	Precipitation temperature [ $^\circ\text{C}$ ]	Volumetric water content (saturation) [%]
1	NN10	non-frozen	-	5.5	5.7	10.1 (63)
2	NM10	non-frozen	10	5.0	5.0	10.1 (63)
3	FN10	frozen	-	5.5	4.3	10.0 (63)
4	FM10	frozen	10	5.6	4.5	10.1 (63)
5	FN12	frozen	-	4.1	4.7	11.8 (74)
6	FM13	frozen	10	5.3	5.9	12.7 (79)
7	FN15	frozen	-	5.6	4.8	14.8 (93)
8	FM15	frozen	10	5.1	5.0	15.0 (94)
9	FM16	frozen	10	5.3	5.1	15.9 (100)

## 2.4 Sensor calibration and measurement

AquaCheck probes were selected as the primary sensors for this study because of their robustness and reliability. Although originally developed for field applications in agriculture and hydrogeology, they provided the robustness and durability required for large-scale laboratory experiments and thus offered a suitable basis for precise measurements. However, their use under controlled laboratory conditions necessitated careful calibration of both the thermocouples and, in particular, the capacitance sensors. The manufacturer does not recommend relying solely on the standard calibration curves provided for different soil





types when high accuracy is required. Instead, the sensors, especially those measuring (liquid) volumetric water content (VWC) were calibrated to the specific soil structure and grain size distribution used in this study. Each AquaCheck probe integrates a thermocouple for temperature measurement and a capacitance sensor for VWC at each of eight measurement points (see Fig. 2b). The thermocouples exhibited small systematic offsets, which were corrected by comparison with high-precision PT1000 sensors (accuracy 0.01 °C).

Unlike many capacitance-based sensors, AquaCheck probes do not output relative permittivity directly. Instead, they provide a factory calibrated scaled frequency unit (SFU) ranging from 0 in air to 100 in water. While this metric is sufficient for operational field use, it is inadequate for quantitative analysis of freeze and thaw dynamics. To derive physically meaningful dielectric properties, the SFU values were converted to effective relative permittivity ( $\epsilon_c$ ) using a soil-specific calibration. Capacitance sensing relies on the strong dielectric contrast between liquid water ( $\epsilon_w \approx 80$ ), air ( $\epsilon_a \approx 1$ ), and soil minerals ( $\epsilon_s \approx 3.9$ ). Conventional calibration curves are valid for unfrozen soil conditions (e.g. Topp et al., 1980), but they fail once ice forms, since the relative permittivity of ice ( $\epsilon_i \approx 3.27$ ) is much lower than that of liquid water (Seyfried and Murdock, 1996). To properly account for both aggregate states of water, we followed previous frozen soil studies (Roth and Boike, 2001; Marco Bittelli and Evett, 2003; Watanabe et al., 2009; Demand et al., 2019) and applied a three-phase dielectric mixing model for unfrozen conditions (Roth et al., 1990) and a four-phase model for frozen conditions (Roth and Boike, 2001; Watanabe et al., 2009). Under unfrozen conditions ( $T > 0$  °C), the three-phase model considers soil, air, and liquid water. According to Roth et al. (1990), the volumetric water content  $\theta$  is given by:

$$\theta = \frac{\epsilon_c^m - (1-n)\epsilon_s^m - n\epsilon_a^m}{\epsilon_w^m(T) - \epsilon_a^m} \quad (1)$$

where  $0 \leq \theta \leq n$ ,  $n$  is porosity, and  $m$  is a pore-geometry factor ( $m = 0.5$ , represents isotropic, random pore structures typical of coarse-textured mineral soils).  $\epsilon_c$  denotes the effective relative permittivity obtained from calibration, while  $\epsilon_s$ ,  $\epsilon_a$ , and  $\epsilon_w$  represent the relative permittivities of soil minerals, air, and liquid water, respectively. The temperature dependence of  $\epsilon_w$  is expressed by the empirical polynomial of Roth et al. (1990):

$$\epsilon_w(T) = 78.54 \left[ 1 - 4.579 \times 10^{-3}(T - 25) + 1.19 \times 10^{-5}(T - 25)^2 - 2.8 \times 10^{-8}(T - 25)^3 \right], \quad (2)$$

which accounts for the variation of liquid water permittivity with temperature. Under frozen conditions ( $T < 0$  °C), the influence of ice within the pore space is considered using the four-phase model (Roth and Boike, 2001; Watanabe et al., 2009):

$$\theta_u = \frac{\epsilon_c^m - (1-n)\epsilon_s^m - (n - \theta_{\text{tot}})\epsilon_a^m - \theta_{\text{tot}}\epsilon_i^m}{\epsilon_w^m(T) - \epsilon_i^m}, \quad 0 \leq \theta_u \leq \theta_{\text{tot}}, \quad (3)$$

where the unfrozen water content  $\theta_u$  is separated from the total water content  $\theta_{\text{tot}}$ .

The combination of the three-phase and four-phase mixing models provides a consistent framework for analysing the measurement data. For every measurement time step, the appropriate model was applied depending on the recorded temperature: the three-phase model for  $T > 0$  °C and the four-phase model for  $T < 0$  °C. To avoid spurious switching at the freezing point, a hysteresis of  $\pm 0.2$  °C was applied, following freeze-hold/thaw-update strategies commonly used in frozen soil hydrology



(Watanabe and Kugisaki, 2017; Demand et al., 2019). This approach enabled consistent evaluation of thermo-hydraulic processes in the soil.

225 At each of the 80 measurement points, the total volumetric water content ( $\theta_{\text{tot}}$ ) was determined as  $\theta$  (from the three-phase model) at the moment when local temperature exceeded 1 °C, after which this value was fixed for all subsequent times at lower temperatures. The threshold of 1 °C ensured that the reference was derived under unambiguously unfrozen conditions. While this procedure is valid when  $\theta_{\text{tot}}$  is known (during the freezing phase), absolute changes in  $\theta_{\text{tot}}$  cannot be resolved from dielectric measurements once irrigation begins. Absolute water balances were derived independently of the inductive flow meter data  
 230 (inflow, drainage, and surface runoff), while relative changes in unfrozen water content ( $\theta_u$ ) were obtained from the dielectric measurements. The magnetic-inductive flow meters were operated according to the manufacturer's specifications without additional calibration. The stated measurement accuracy is  $\pm(2\%$  of reading  $+0.5\%$  of full scale), and the sensors exhibited stable and repeatable readings throughout all experiments without noticeable drift. For the AquaCheck probes, temperature measurements have an uncertainty of  $\pm 0.02$  °C. For VWC, the combined uncertainty is estimated at  $\pm 1\%$ , accounting for both sensor  
 235 repeatability and the soil-specific calibration (details are provided in Appendix C). Accordingly, the temporal analysis of the VWC data, especially after the onset of irrigation, focuses on relative rather than absolute changes.

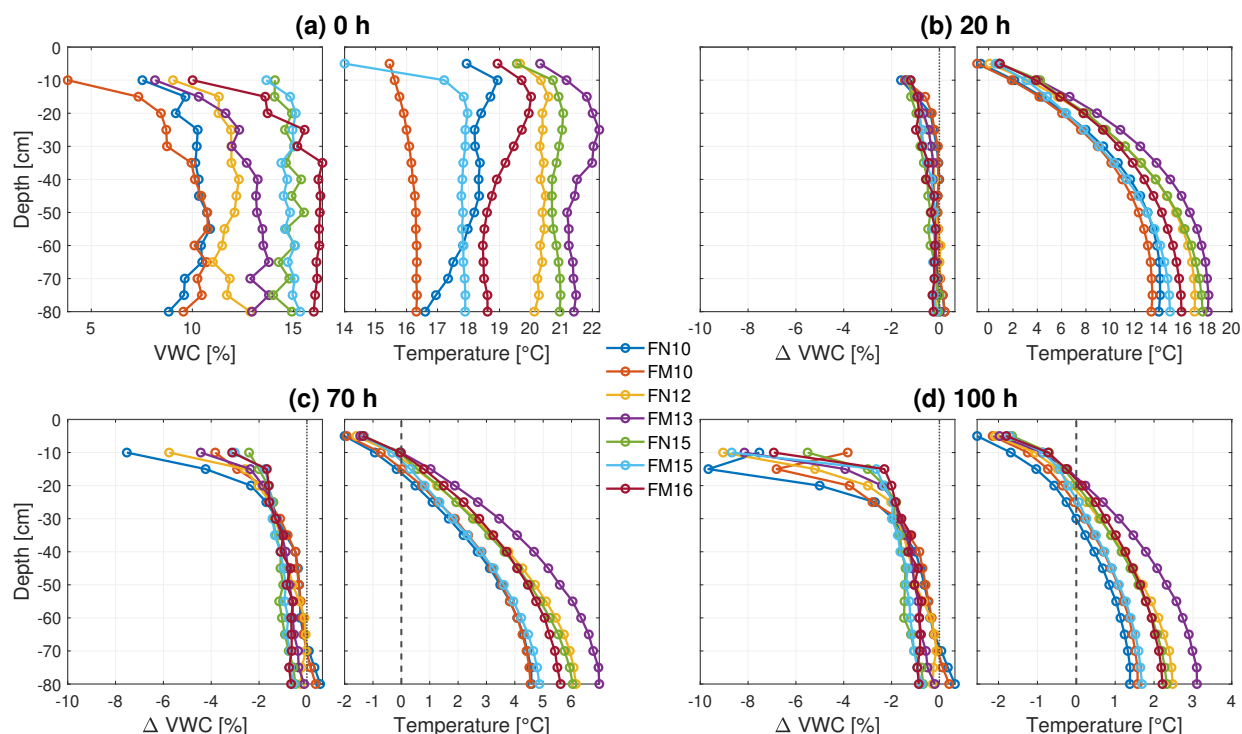
### 3 Results

This section presents the results of the freezing and infiltration experiments. First, we analyse the freezing process as a function of time between the onset of cooling and the initiation of precipitation, with emphasis on the effects of initial water content  
 240 and the presence of the macropore network. Second, we describe the infiltration behaviour and surface runoff generation during precipitation under partially frozen conditions. Finally, we examine the spatio-temporal evolution of soil temperature and (liquid) volumetric water content (VWC) during irrigation to link observed flow responses to internal thermo-hydraulic dynamics.

#### 3.1 Freezing process

245 During the initial phase, the soil was frozen while the box remained in a horizontal position and was exposed to sub-zero air temperatures ( $-5$  °C) inside the climate chamber. The temperature and VWC distributions were found to be largely uniform across the soil body, with only minor spatial variations and weak boundary influences near the walls and bottom. Therefore, probe readings were averaged to derive representative vertical profiles of temperature and VWC (Fig. 3). These results provide insight into the freezing behaviour of the soil and allow assessment of the influence of initial water content and the macropore  
 250 network. One experiment (FN10) represents an exception, as an adjustment to the climate chamber control was required before this run. The modified regulation increased cooling efficiency, resulting in faster and deeper freezing of the soil. Consequently, FN10 is excluded from detailed interpretation regarding the temporal evolution freezing process.

At the beginning of the experiment (Fig. 3a), soil temperatures ranged between 14 and 22 °C, reflecting seasonal variability in laboratory conditions between mid-May and late August. VWC profiles agreed well with the target VWC levels defined during



**Figure 3.** Vertical profiles of volumetric water content (VWC, left) and temperature (right) at four stages during the freezing process: (a) immediately after soil filling (initial state), (b) after 20 h of cooling, (c) after 70 h, and (d) after 100 h. In (a), VWC represents absolute values, while in (b–d), VWC is shown as the change relative to the initial state. Dashed vertical lines in the temperature plots mark the 0 °C isotherm. The uppermost sensor is partly influenced by ambient air conditions and is excluded from the VWC plots.

filling (e.g. 10 % for FM10). Vertical heterogeneities in VWC resulted from the layer-wise filling process, which was necessary due to the large soil volume and limited capacity of the mixing device. These variations represent slight differences between mixing batches and do not indicate systematic bias. A comparison of sensor-based VWC with reference measurements from the oven drying method (Appendix C) confirmed the accuracy of the VWC data.

After 20 h of freezing at an air temperature of -5 °C, pronounced thermal gradients developed (Fig. 3b). The surface layer (-5 cm) exhibited the highest cooling rates, with a maximum of -0.55 °C h<sup>-1</sup> (FM13) and a median of -0.5 °C h<sup>-1</sup> across all experiments. In contrast, deeper layers (40-60 cm) cooled more slowly (approximately -0.25 °C h<sup>-1</sup>), reflecting the insulating properties of the soil and box structure, which led to a gradual top-down progression of the cooling front. Concurrent VWC decreases in the upper 10-20 cm (> 0.5 %) indicate early redistribution of unfrozen water. In high initial VWC scenarios (FN15, FM15, FM16), water displacement occurred throughout the entire profile, consistent with gravitational drainage prior to freezing (estimated at 2-3 L). In drier cases (e.g. FN10, FM10), the VWC reduction near the surface was accompanied by slight increases at depth (≈ 0.3 %), suggesting downward redistribution.



By 70 h (Fig. 3c), most upper layers (10-20 cm) had reached the freezing point (0 °C). Initial temperature differences between the experimental runs of up to 6 °C (10 cm) decreased to below 1 °C due to latent heat buffering. Correspondingly, VWC reductions at 15 cm depth ranged from -1.1 % (FM16) to -4.3 % (FN10). Drier soils showed larger decreases, reflecting faster freezing because of lower latent heat demand.

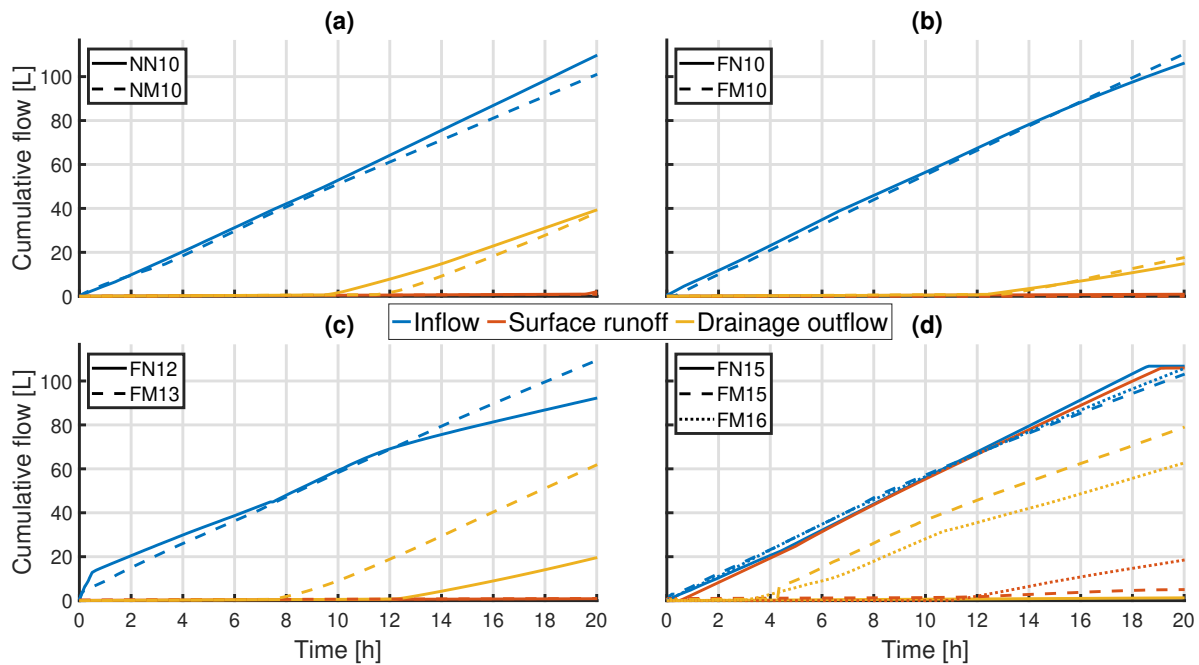
After 100 h (Fig. 3d), all profiles exhibited sub-zero temperatures in the upper soil column. The freezing front extended to depths of 15-30 cm and was primarily governed by the initial soil temperature. The uppermost 10 cm froze between 52 and 82 h, depending on the initial thermal state. Temperatures at 15 cm across all experiments converged to a narrow range (-1.2 to -0.4 °C), again illustrating the stabilising effect of latent heat. In all experiments, the final VWC within the 20-30 cm range decreased, averaging  $-4.2 \pm 0.5$  %. Between 30 and 50 cm, mean losses were about 0.5-2 %, and at depths below 50 cm, the differences from the 70h snapshot were negligible. These patterns are consistent with progressive freezing from the surface downward, reducing the measurable liquid water fraction. In wetter soils, pre-freezing drainage contributed to additional VWC loss at depth. Minor late-stage reductions (> 70 h) in unfrozen lower layers likely reflect upward migration of liquid water toward the freezing front under matric potential gradients.

Overall, wetter soils cooled slightly more effectively due to higher thermal conductivity but exhibited slower advancement of the freezing front because of increased latent heat demand. This effect was masked by initial temperature differences of up to 4 °C. With this setup and under the applied conditions, the presence of the macropore network (macropore volume fraction of 0.5 %) had no visible effect on the thermal or hydraulic behaviour during the freezing phase.

### 3.2 Water balance during the irrigation

The second part of the results focuses on the infiltration phase. After completion of the freezing process, the soil box was inclined at an angle of 10°, and the rainfall simulator was mounted above the surface. Irrigation commenced, and flow meter data were recorded continuously. This section presents the temporal evolution of irrigation inflow, surface runoff, and subsurface drainage outflow throughout each experiment, covering the full duration from the onset of irrigation to the termination of the water supply. Figure 4 summarises the cumulative flow measurements for all experimental scenarios. Each panel displays three cumulative flow curves - blue for inflow from irrigation, orange for surface runoff, and yellow for drainage - plotted against time. Comparative experiments with similar initial water content, conducted with and without a macropore network, are displayed together for direct comparison. The upper left panel shows the unfrozen reference experiments, the upper right panel the frozen low VWC experiments, the lower left the intermediate VWC experiments, and the lower right the high VWC experiments.

In the unfrozen (NN10, NM10) and frozen (FN10, FM10) low VWC scenarios, total inflow volumes ranged between 100 and 112 L over 20 h. Drainage began after 9.5-13.5 h and reached 20 L (FN10, FM10) to 40 L (NN10, NM10) by the end of the experiments, whereas surface runoff remained negligible (< 5 L). These results indicate that under initially low VWC conditions, nearly all applied water infiltrated until saturation, after which excess input was discharged as drainage. Under these conditions, the macropore network did not act as a dominant preferential pathway, as the soil matrix absorbed most of the precipitation, allowing only minimal bypass flow. Within the unfrozen experiments, small differences between soils with and



**Figure 4.** Cumulative discharge dynamics from large-scale infiltration experiments into partially frozen soils with and without a macropore network. Each panel compares experiments under similar boundary conditions, showing cumulative inflow (blue), surface runoff (orange), and drainage flow (yellow) over time. Solid lines denote experiments without a macropore network; dashed and dotted lines represent experiments with a macropore network. Panels illustrate (a) unfrozen, low initial water content; (b) frozen, low initial water content; (c) frozen, intermediate initial water content; and (d) frozen, high initial water content scenarios (three experiments).

without macropores were observed. Drainage onset in the macropore network case (NM10) was delayed by about 2 h, likely reflecting a combination of slightly lower inflow and soil structural heterogeneities such as shrinkage or minor cracking.

In contrast, the hydrological differences between the two low VWC frozen scenarios (FN10, FM10) were very small. Although the freezing front was more strongly developed in FN10 (see Figs. 3d and 5), both experiments exhibited slower infiltration dynamics compared to the unfrozen reference. Drainage began after approximately 13.6 h, consistent with the reduced permeability under freezing conditions. Overall, the low VWC experiments demonstrate that both frozen and unfrozen soils maintained high infiltration capacities, as sufficient air-filled pore space remained and the matrix potential was strong enough to induce suction of the applied precipitation. Under these conditions, the frozen matrix remained permeable, and no refreezing occurred, allowing continuous infiltration throughout the experiment. Thus, the macropore network exerted no systematic influence on the infiltration/runoff partitioning, and observed variability primarily reflected freezing conditions and soil heterogeneity.

At intermediate initial VWC (FN12, FM13), differences between the macropore network and non macropore setups became more distinct. Inflow volumes were slightly higher in FM13 (110 L) than in FN12 (90 L), but the first 12 h of irrigation showed





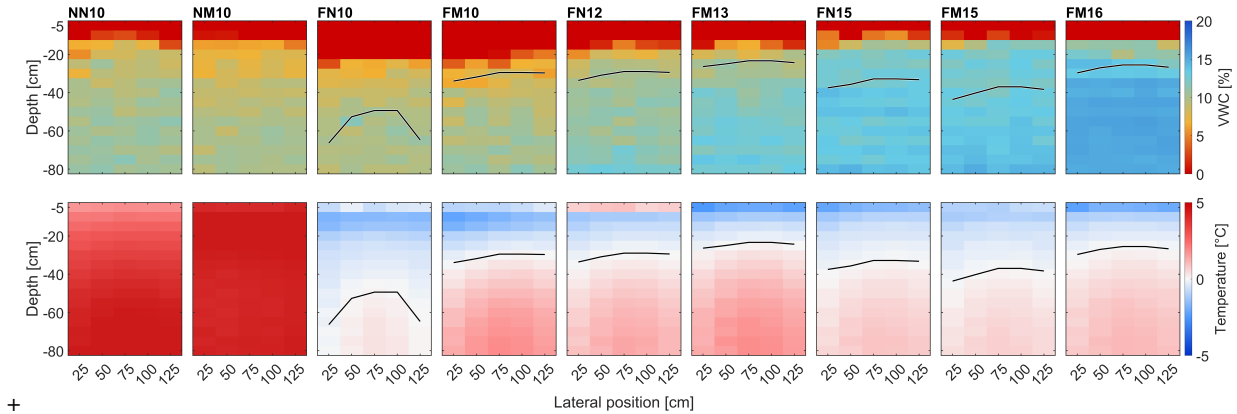
nearly identical inflow behaviour (about 70 L), enabling a direct comparison of drainage response. The experiment with a  
 315 macropore network (FM13) exhibited an earlier drainage onset (8 h) compared to the non-macropore case (FN12, 12 h), and  
 the total drainage volume was substantially larger. Although total inflow differed slightly (110 L vs. 90 L), the similar early  
 inflow phase supports interpretation of the earlier drainage in FM13 as evidence of preferential bypass flow instead of just  
 being a result of variations in inflow. Surface runoff was absent in both experiments. These findings suggest that under inter-  
 mediate initial water content, the macropore network facilitated preferential pathways that allowed early bypass flow through  
 320 the partially frozen profile, accelerating infiltration and advancing drainage onset.

The strongest contrasts were observed under high initial VWC conditions (FN15, FM15, FM16). Visual inspection at the onset  
 of irrigation revealed that the soil surface was fully frozen and exhibited a mechanically rigid structure. This condition resem-  
 bles what is often described as a nearly impermeable, concrete-like frost layer, typically formed when a saturated upper soil  
 layer refreezes after mid-winter snowmelt (Ala-Aho et al., 2021). In FN15, without a macropore network, almost the entire  
 325 inflow ( $\approx 104$  L) was diverted into surface runoff, with negligible drainage ( $< 2$  L), indicating that the frozen soil matrix  
 entirely prevented infiltration. In sharp contrast, the macropore network experiments (FM15, FM16) showed substantial early  
 drainage after only about 4 h, reaching 61–80 L in total. After approximately 12 h, however, drainage rates declined while  
 surface runoff increased (up to 20 L in FM16), likely due to progressive refreezing of preferential flow paths within the soil and  
 partial blockage of some macropores (discussed in Sect. 4.3). This temporal pattern occurred consistently in both macropore  
 330 network experiments (FM15, FM16), though the magnitude of the effect varied.

Taken together, these results demonstrate that the influence of the macropore network on infiltration and runoff dynamics  
 increases with higher initial VWC. Under initial low VWC conditions, the network exerted only a minor influence on precipi-  
 tation partitioning. In contrast, at higher initial VWC, partial ice blocking reduced infiltration into the soil matrix. However, this  
 335 effect was partly offset by flow through the macropore network, which enabled water to bypass frozen regions and resulted in  
 earlier and more pronounced drainage. As infiltration continued, drainage rates in the high initial VWC experiments gradually  
 decreased while surface runoff increased, reflecting progressive blockage of some macropores. These findings highlight the  
 importance of macropore network connectivity and the pre-freezing saturation state in controlling infiltration behaviour under  
 frozen conditions.

### 340 **3.3 Temperature and water content evolution within the inclined soil body**

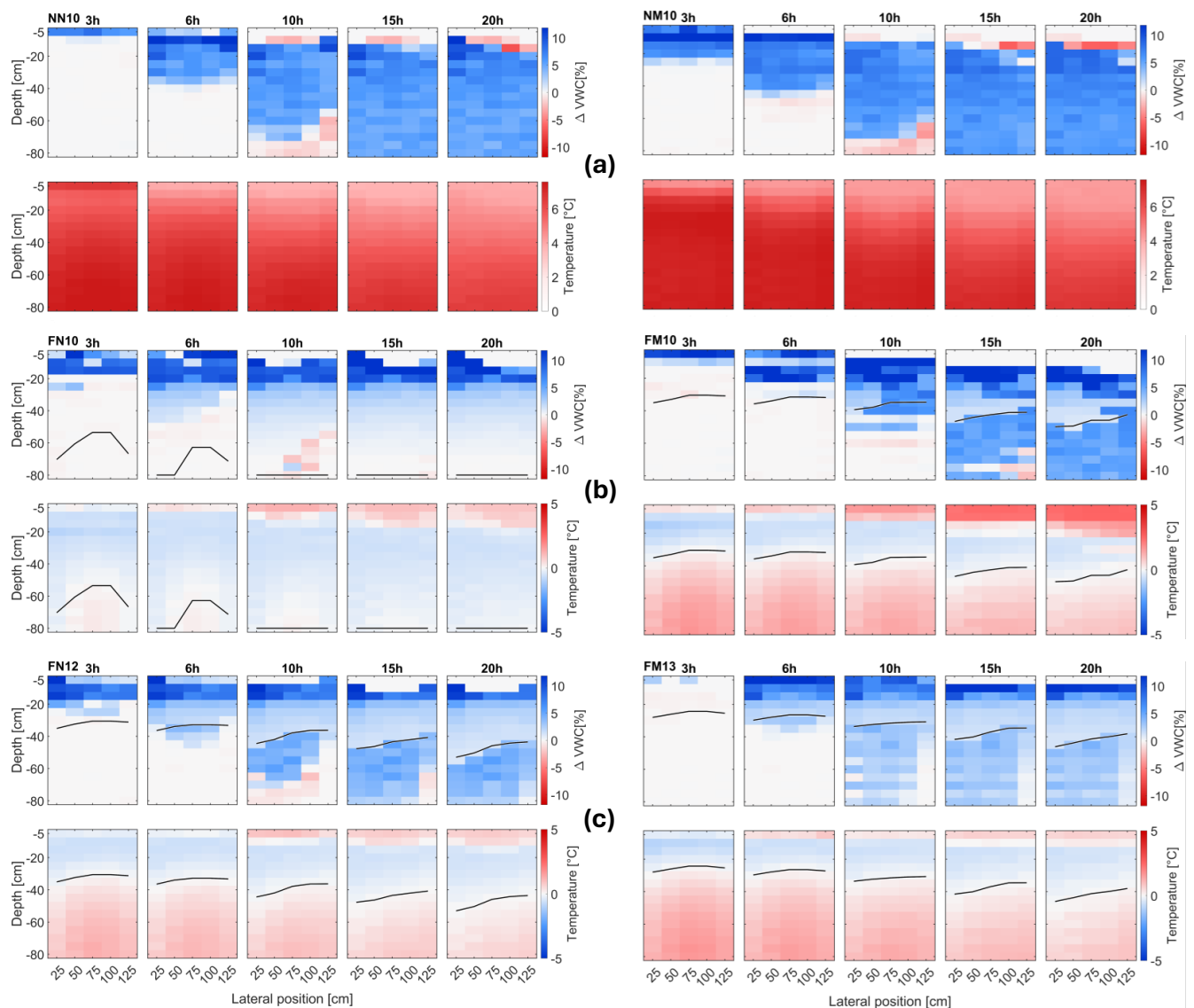
This subsection presents the spatially distributed sensor data during infiltration into the  $10^\circ$  inclined soil body. The results  
 should be interpreted in conjunction with the cumulative flow shown in Fig. 4. The initial conditions (Fig. 5) and subsequent  
 evolution of VWC and temperature (Figs. 6 and 7) are displayed as two-dimensional cross-sections (side views of the inclined  
 face of the soil box) with soil depth on the vertical axis and lateral sensor position on the horizontal axis. The upper panels show  
 345 VWC, while the lower panels show temperature. Colours indicate sensor readings, and the black line in the frozen experiments  
 marks the  $0^\circ\text{C}$  isotherm. The analysis begins with the post-freezing initial state for all nine experiments (Fig. 5), providing a  
 baseline for evaluating the effects of irrigation. In contrast to Fig. 3d, which shows a uniform 100-hour snapshot, these profiles



**Figure 5.** Profiles of volumetric water content (VWC) and temperature for all nine experiments directly after the freezing period and before the start of precipitation ( $t = 0$  h). The first row shows the total VWC, while the second row depicts the corresponding temperature distribution. The first two profiles represent the unfrozen reference experiments. The black line denotes the  $0\text{ }^{\circ}\text{C}$  isotherm. The slope extends from 0 cm at the lower end to 150 cm at the upper end.

represent the final freezing state for each experiment. The duration required to reach this state varied among experiments, as comparable frost depths were targeted between macropore network and non-macropore network pairs (e.g. 102 h for FM13 and 122 h for FN15). In the unfrozen scenarios (NN10, NM10), the temperature remained above  $0\text{ }^{\circ}\text{C}$  throughout the soil profile, while in frozen soils, the  $0\text{ }^{\circ}\text{C}$  isotherm ranged from 25 cm (FM16) to 55 cm (FN10), primarily depending on initial soil temperature and freezing duration. As discussed in Sect. 3.1, no strong systematic effect of the macropore network or initial VWC was observed.

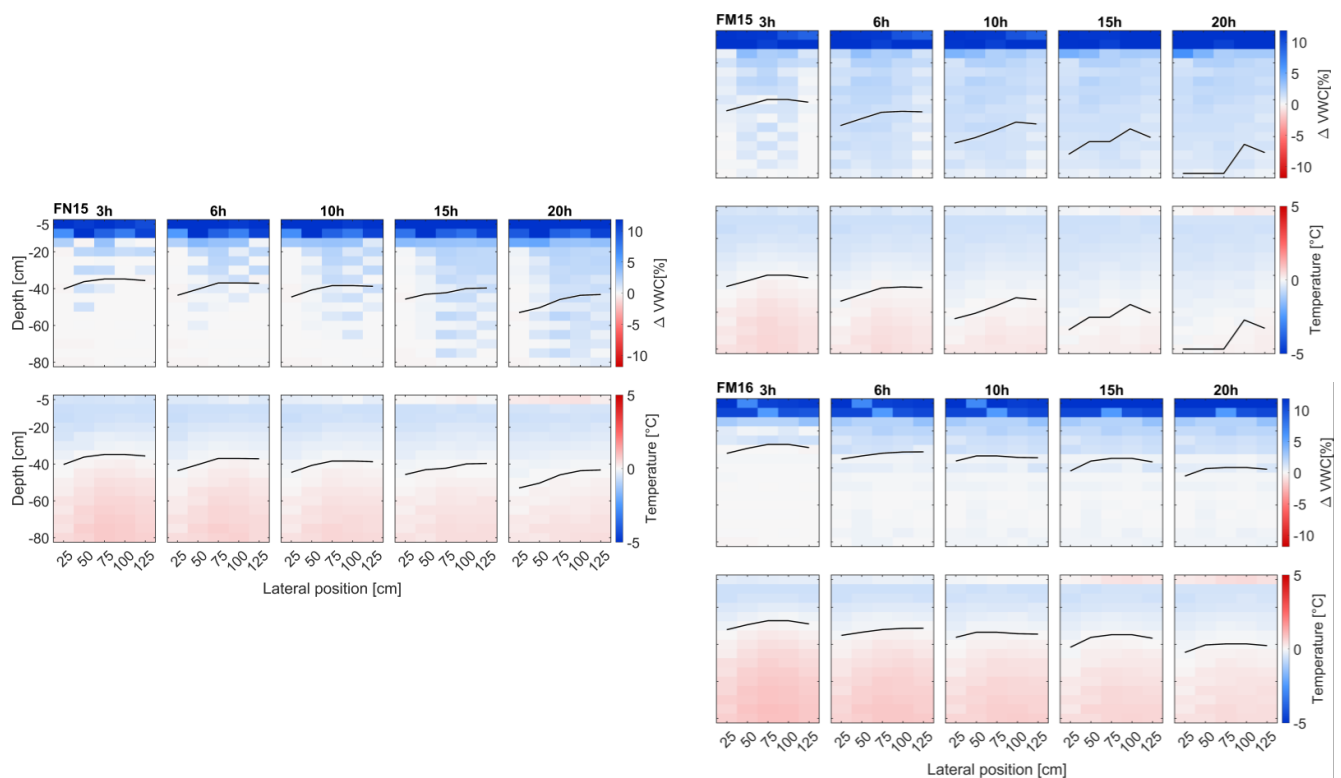
The temporal evolution of VWC and temperature during irrigation is shown in Figs. 6-7. Significantly, the upper panels exclusively show changes in VWC compared to the state immediately after freezing. (Fig. 5). For non-frozen experiments, NN10 and NM10 (Fig. 6a), infiltration progressed steadily with an advancing wetting front along the down slope direction. In NN10, a temperature decrease of 1.6 K at 55 cm depth within the first 20 h indicates advective cooling by the infiltrating water. Net VWC changes reflect unhindered infiltration due to the absence of frozen barriers. Differences between the macropore network and non-macropore setups were negligible. In FN10, a deeply developed freezing front (50-70 cm) was present at the onset of irrigation, the freezing front progressed downwards and at 10h the entire soil body was at sub-zero temperatures. Only small (1-2 %) VWC changes in the lower soil layers (40-80 cm) were found, as most of the initial liquid water had turned into ice. FM10 exhibited a weaker frozen layer at 25-30 cm depth. Infiltration into the matrix was visibly delayed, with the wetting front lagging by approximately 20 cm after 10 h (compared to the unfrozen NM10). Once the wetting front intersected the  $0\text{ }^{\circ}\text{C}$  isotherm, advective heat transport by infiltrating water and latent heat release during freezing caused the freezing front to migrate downward, from 35 cm at 3 h to 45-55 cm at 20 h. Full infiltration occurred in both experiments. In FM10, total VWC increases of 5-7 % were observed below the freezing front, whereas FN10 showed much smaller increases because the entire soil body was already frozen. No clear macropore network effect was observed under these relatively low initial water content



**Figure 6.** Temporal evolution of the change of soil volumetric water content ( $\Delta$  VWC) and temperature for the low and intermediate water content experiments after the onset of irrigation. The time labels above the plots indicate elapsed time since irrigation began. The first row shows VWC changes relative to  $t = 0$  h (in percent), while the second row shows temperature evolution in the frozen soil during irrigation. The black line represents the 0 °C isotherm, marking the position of the freezing front.



conditions. In all low VWC experiments (Figs. 6a and 6b), the sensor readings of the upper 10-20 cm are misleading, since soil shrinkage during irrigation occurred, which exposed sensors to air. These near-surface measurements are therefore considered  
 370 artefacts and excluded from quantitative interpretation, though retained in the plots for transparency.  
 In the intermediate VWC experiments FN12 and FM13 (Fig. 6c), a pronounced frozen layer initially extended between 0 and 30-35 cm depth. FM13 showed earlier deep wetting, with the 80 cm sensor recording VWC increases of 1–2 % after 10 h, compared to no detectable change in FN12. Together with the earlier drainage response (Sect. 3.2), these observations strongly  
 375 suggest preferential bypass flow through the macropore network, even though direct visualisation of flow paths was not possible. The freezing front advanced during irrigation, reaching 50 cm in FN12 and 45 cm in FM13, with deeper penetration down slope due to advective heat transport. Both scenarios showed a much stronger increase of VWC below the freezing front, comparable to FM10.



**Figure 7.** Temporal evolution of the change of soil volumetric water content ( $\Delta$  VWC) and temperature for the high water content experiments after the onset of irrigation. Time labels above the plots indicate the elapsed time since irrigation began. The first row shows VWC changes relative to  $t = 0$  h (in percent), while the second row shows the temperature evolution in the frozen soil during irrigation. The black line marks the 0 °C isotherm, indicating the freezing front position.



380 In the high VWC scenarios FN15, FM15, and FM16 (Fig. 7), all experiments began with frost depths of approximately 30-45 cm. In FN15, infiltration was almost completely suppressed: VWC changes remained below 1 % throughout the profile, and most inflow was diverted into surface runoff (see Fig. 4d). In FM15, small but measurable VWC increases throughout the whole soil body occurred in the first 6 h. In contrast, FM16 showed no detectable changes in VWC below the freezing front. This behaviour is consistent with infiltration through macropore network pathways bypassing the impermeable matrix. Currently, the downward progression of the freezing front indicates enhanced advective heat transport. These patterns provide evidence that the macropore network can transiently promote both infiltration and heat transfer even under fully frozen surface conditions, although the exact flow paths could not be resolved within the current setup. Between 0 and 20 h, the freezing front advanced approximately 10 cm in FN15, 10-15 cm in FM16, and 25-35 cm in FM15. In FM15, the 0 °C isotherm reached depths beyond 75 cm, indicating that most of the soil profile had frozen by the end of the experiment. The strong downward progression of the freezing front in FM15 reflects enhanced advective heat transport, likely driven by infiltration through the macropore network. Notably, FM15 also exhibited the greatest initial frost depth (Fig. 3). These observations confirm that the macropore network can facilitate infiltration and heat transfer even under fully frozen conditions, provided sufficient connectivity exists.

395 Overall, the distributed sensor data confirm that the macropore network substantially enhances infiltration and advective heat transport in frozen soils, but only under sufficiently high initial VWC. These effects are absent under low VWC conditions, where matrix dominated infiltration prevails regardless of soil structure.

## 4 Discussion

### 4.1 Soil freezing behaviour

400 The freezing dynamics observed in our experiments were governed primarily by the antecedent soil temperature, whereas variations in initial water content and the presence of the macropore network played only minor roles within the tested parameter range (an exception marks the FN10 run, where the cooling procedure was modified). Differences of up to 4-6 K in the initial thermal state largely determined frost depth, consistent with the importance of sensible heat storage reported by Kurylyk and Hayashi (2016). In wetter soils, higher thermal conductivity facilitated slightly more efficient heat loss from the surface, yet the advance of the freezing front was delayed because the increased water content raised the latent heat requirement. Consequently, cooling and freezing progressed in opposite directions: temperatures decreased more rapidly, but the phase change advanced more slowly. This highlights the dual role of water content in frozen soils, acting both as a thermal conductor and a latent heat buffer.

In fine-textured or organic-rich soils, these effects are further complicated by cryosuction and water redistribution (Nagare et al., 2012), but in our coarse sandy matrix such processes were much smaller. Throughout the experiments, a slight reduction in water content at deeper soil layers during freezing suggested a small upward migration toward the freezing front. However, these effects were minimal within the coarse, low capillarity matrix used here. The absence of a macropore network effects on





freezing contrasts with the findings of Watanabe and Kugisaki (2017), who reported pronounced retardation of freezing around macropores in fine-textured soil columns. Their experiments used narrow, vertically oriented pores (5 mm diameter) and a  
 415 macropore volume fraction of about 1.6 %, whereas our large-scale setup contained coarser (10 mm) pores with a smaller total volume fraction ( $\approx 0.5$  %). Under these conditions, the coarse texture, low porosity, and limited cumulative heat exchange area likely restricted significant thermal buffering along macropore walls. A similar dependence on macropore network fraction was also reported by Demand et al. (2019), who found moderate freezing delays at higher macropore volumes, suggesting that macropore-related thermal effects may scale with their overall abundance. Overall, our findings emphasise the dominant role of  
 420 thermal preconditioning in controlling frost penetration, while underscoring that such controls are strongly soil-specific. These preconditioning effects set the foundation for the infiltration and runoff dynamics discussed below.

## 4.2 Infiltration and runoff dynamics

Initial water content emerged as the principal control on infiltration/runoff partitioning in frozen slopes. At low volumetric water content (VWC), infiltration proceeded primarily through the soil matrix, and the macropore network had little influence. At  
 425 intermediate VWC, however, the macropore network enhanced infiltration and drainage by providing preferential flow paths, supporting the threshold-type behaviour described by Demand et al. (2019) and consistent with the column experiments of Watanabe and Kugisaki (2017). Distributed sensor data demonstrate that such preferential infiltration not only bypassed the frozen matrix but also enhanced advective heat transport, advancing the freezing front and altering the internal thermal regime, consistent with previous modelling studies of coupled water and heat flow in frozen soils (Hansson et al., 2004; Grenier et al.,  
 430 2018).

The strongest contrasts were observed at high VWC (near saturation), where the frozen matrix became nearly impermeable. Without a macropore network, almost all inflow was converted to surface runoff, whereas soils containing a macropore network exhibited rapid initial drainage that bypassed the frozen layer, followed by partial blockage of preferential flow paths due to refreezing. At first glance, these results might appear to contradict the findings of Pittman et al. (2020), who observed reduced  
 435 infiltration at high VWC because their natural macropore network froze and became blocked. On closer inspection, however, the two outcomes are complementary. In our experiments, infiltration remained high as long as macropores were open and unfrozen. Once parts of the network refroze and lost hydraulic connectivity, both drainage and infiltration rates declined markedly, illustrating that infiltration efficiency decreases sharply when most macropores become blocked. At the start of irrigation, by contrast, the macropore network was deliberately kept open and unfrozen, allowing preferential pathways to function even  
 440 under fully frozen surface conditions. In our coarse sandy soil, with an effective porosity of approximately 0.16, macropores became hydraulically effective only when the initial VWC exceeded 12-13 %. Below this threshold, sufficient air-filled pore space remained for matrix infiltration to dominate. While the exact threshold is soil-specific, the underlying mechanism, a shift from matrix dominated to bypass dominated infiltration as micropores fill and freeze, likely applies more broadly. This threshold behaviour highlights the non-linear sensitivity of infiltration to pre-freezing conditions (Stähli et al., 1996, 2004; Mo-  
 445 hammed et al., 2018). Small differences in the initial VWC can determine whether a macropore network effectively contributes to the partitioning of precipitation, and whether a precipitation event results in efficient infiltration and drainage or, instead, in



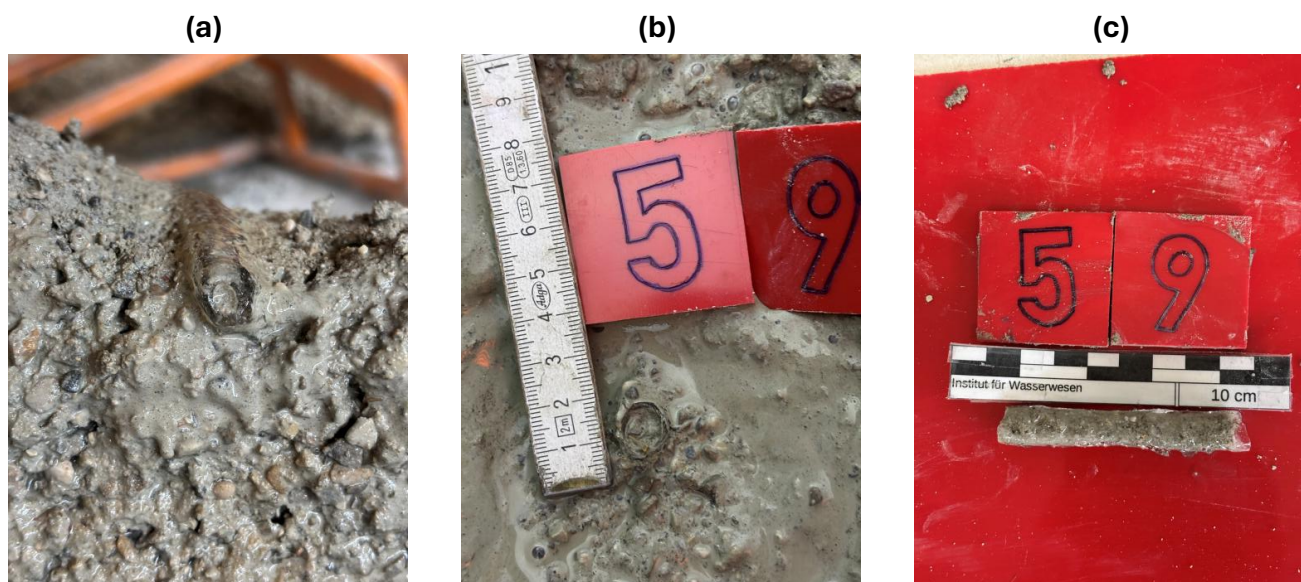
rapid and nearly complete surface runoff. Importantly, the sloping experimental setup ( $10^\circ$ ) promoted efficient lateral runoff, preventing ponding and realistically reproducing natural hill slope conditions often absent in column studies. These findings show that even modest variations in pre-event conditions can shift hill slope response between infiltration dominated and runoff dominated regimes, with implications for both groundwater recharge and debris flow initiation.

### 4.3 Macropore refreezing

A novel aspect of this study is the direct observation of macropore network refreezing on an inclined soil slope under continuous wetting with a fine, naturalistic spray cone. In analysing Fig. 4d, the observed decrease in drainage and the concurrent increase in surface runoff in FM15 and FM16 were initially attributed to refreezing of individual macropores during irrigation. This interpretation was first based on flow meter data and corroborating signals from the AquaCheck probes. After the experiments were terminated and the soil was excavated, this interpretation was confirmed through the direct identification of frozen macropores (Fig. 8). Some macropores remained largely unfrozen (mainly in the upper slope) while others exhibited thin ice linings along the pore walls (Fig. 8a, 8b), particularly in the mid-slope region. In contrast, macropores located on the lower slope were constricted by up to 50 % of their diameter. Macropore refreezing occurred exclusively in the high VWC experiments, and the processes leading to pore blockage differed between runs. In FM15, the soil profile experienced deep and persistent freezing, resulting in thermal refreezing of macropores throughout the column (Fig. 8c). In FM16, by contrast, the frozen layer was shallower, but sediment deposition from the surface promoted pore blockage, as indicated by macropores partially filled with grains (Fig. 8b, 8c). These observations suggest two distinct mechanisms that reduced the functionality of the macropore network: (i) thermal blockage due to the growth of pure ice along pore walls, and (ii) particle-assisted clogging, where fine particles were flushed into the macropores and subsequently promoted refreezing onto these particles.

The dual role of the macropore network, acting first as conduits for infiltration and later as barriers through refreezing, emerges as a key feature of frozen soil hydrology. Refreezing substantially reduced the effective diameter of macropores, strongly diminishing their hydraulic conductivity and their interaction with the surrounding matrix. Even thin ice linings were sufficient to restrict flow and decouple macropores from the unfrozen pore space, leading to a rapid shift from infiltration to surface runoff once the discharge capacity was exceeded. The estimated 50 % narrowing observed in the high initial water content experiments (FM15, FM16) plausibly explains the concurrent decline in drainage and rise in surface runoff. Because natural macropores are irregular, partially filled, and rough-walled, these effects likely represent a lower bound for the hydraulic impact of partial refreezing.

Our findings that macropores freeze progressively from the pore walls inward are consistent with previous observations under idealised laboratory conditions (Watanabe and Kugisaki, 2017). The present study demonstrates that this process also occurs in a large-scale, realistic experimental setup representative of alpine slopes subjected to natural rainfall, providing a novel experimental confirmation of this phenomenon. Additionally, evidence of particle-assisted clogging was observed, particularly in terminating macropores. Fine particles transported with surface runoff appeared to enter macropores and accumulate at their lower ends, enhancing partial blockage.



**Figure 8.** Partially frozen macropores observed in the excavated soil. (a) shows a macropore with an approximately 50 % reduction in diameter, coinciding with the sudden increase in surface runoff (observed in FM15). (b) and (c) show a macropore (macropore 59 see Appendix A) at an early stage of ice formation, with a thin ice rim initiating at the pore wall and advancing inward (observed in FM16). All macropores initially had an open diameter of 10 mm. Photographs were taken post-experiment during systematic soil excavation. Residual sand and fines are visible in some macropores, likely introduced by surface runoff during the experiment or inadvertently during excavation.

480 This process likely acted in conjunction with refreezing, further reducing infiltration capacity. However, the overall extent of clogging remains uncertain, as some deposits may have been introduced during excavation.

#### 4.4 Limitations

The following limitations outline the scope and constraints of our experimental design, which deliberately simplified natural soil complexity to isolate the thermo-hydraulic effects of macropore networks under controlled conditions. The choice of relatively large macropore diameters was intentional to (i) ensure structural stability of the pores during freezing, (ii) facilitate reproducibility across experiments, and (iii) enable clear monitoring of macropore network effects in the presence of a dense sensor grid. In natural alpine soils, macropore networks are more heterogeneous in form and size, with diameters often below 5 mm and influenced by roots, cracks, and biogenic activity. Thus, while the implemented design accentuates preferential flow processes, it represents an upper-end scenario of macropore influence and should be interpreted accordingly.

490 The absence of fine particles and organic matter also suppresses cryosuction and reduces the potential for capillary water redistribution during freezing. Consequently, while the soil mixture reproduces the coarse end of alpine soil textures, it does not capture the full spectrum of cryogenic processes typical of finer structured or organic-rich mountain soils. This simplification was deliberate to isolate the role of the macropore network and initial water content, but it limits the transferability of the



results to natural soils with higher silt or clay fractions.

495 The experimental design intentionally held several influential factors constant to isolate and visualise the role of the macro-  
 pore network under different initial water contents. While this reduction in degrees of freedom improved interpretability, it  
 also reduced generality. A single coarse-textured artificial soil with standardised packing and no organic content was used.  
 Natural heterogeneity, such as layering, root channels, or biogenic roughness, was not represented and may influence capil-  
 larity, cryosuction, and refreezing dynamics. The macropore network in our experiments was artificial and reproducible, with  
 500 fixed connectivity and orientation. Most macropores were vertical or only slightly inclined, resulting in predominantly vertical  
 flow paths with limited tortuosity and little lateral preferential flow. This differs from natural soils, where macropore networks  
 formed by roots, cracks, and fauna are highly tortuous and interconnected, facilitating both vertical and lateral preferential  
 flow (Hartge et al., 2014). Furthermore, the artificial macropores used here had a uniform diameter of 10 mm, whereas natural  
 systems typically contain a broader distribution of pore sizes. A shift toward smaller, more realistic pore diameters would likely  
 505 alter refreezing dynamics and the hydraulic response. The parameter space was also restricted: only one macropore volume  
 fraction ( $\approx 0.5\%$ ), one pore diameter (10 mm), and one slope inclination ( $10^\circ$ ) were tested.

Hydraulic and thermal boundary conditions introduce additional limitations. In seasonally frozen soils, increasingly dynamic  
 temperature fluctuations lead to more frequent freeze-thaw cycles, which can either strengthen or weaken frost fronts depend-  
 ing on air temperature and precipitation regime (Lundberg et al., 2016). Rainfall in the laboratory was applied under controlled  
 510 conditions with predefined intensity and temperature, which cannot fully reproduce the natural variability of precipitation such  
 as bursts, intermittency, or wind effects. In nature, winter precipitation events often occur over much shorter timescales and  
 at lower intensities, yet with highly variable dynamics (Bardou and Delaloye, 2004). Overall, rain on frozen soil events in the  
 field are typically far more transient and complex than those achieved in controlled experiments.

Furthermore, snowpack processes and meltwater inputs were not considered, and the climate chamber conditions approximate  
 515 but do not fully reproduce outdoor exchanges such as radiation, wind-driven convection, or diurnal cycling. Sensor-related  
 uncertainties provide an additional source of limitation. AquaCheck probes required soil-specific calibration, and conversion  
 from scaled frequency to effective permittivity and subsequently to volumetric water content introduces uncertainty, particu-  
 larly when ice is present. Local shrinkage occasionally exposed near-surface sensors to air, producing artefacts such as apparent  
 VWC deficits. Although temperature offsets were corrected, small residual biases cannot be excluded. Evidence for refreezing  
 520 processes such as particle-assisted clogging relies partly on post-excavation inspection, which may disturb fragile ice linings  
 or redistribute fine particles.

These limitations delineate the range of validity of our findings and motivate future research across a broader range of soil  
 types, macropore fractions and diameters, slope angles, and compound snow-rain freeze-thaw sequences under more natural  
 boundary conditions. Two aspects of the experimental design warrant particular caution when transferring these results to natu-  
 525 ral alpine soils. First, the artificial soil mixture was deliberately coarse and lacked organic material, suppressing cryosuction and  
 limiting water redistribution during freezing. This simplification ensured homogeneous packing and reproducible conditions,  
 but likely underestimates the role of capillary retention and ice segregation that occur in finer textured mountain soils. Second,  
 the artificial macropores had a uniform diameter of 10 mm, representing the coarse end of natural variability. While this en-



hanced structural stability and reproducibility, it represents an upper-end scenario of macropore influence. Natural macropore  
 530 networks are more heterogeneous in size, orientation, and connectivity, and their hydraulic behaviour may therefore differ from  
 the controlled structures tested here.

#### 4.5 Implications for modelling and field conditions

Despite the outlined limitations, our results bridge the gap between small-scale column experiments and uncontrolled field  
 observations. The combination of a large soil volume, inclined slope, naturalistic rainfall, and a three-dimensional macropore  
 535 network enabled reproduction of key hydrological processes such as lateral flow and surface runoff phenomena typically ab-  
 sent in column experiments. Field studies have reported both rapid runoff and infiltration under frozen conditions (Stähli et al.,  
 2004; Webb et al., 2018), yet attributing these behaviours to macropore activity remains challenging due to heterogeneity. Our  
 controlled experiments provide rare process-level evidence that even a small macropore volume fraction (0.5 %) can substan-  
 tially alter infiltration/runoff partitioning under wet preconditions.

540 From a modelling perspective, these findings underline the limitations of Richards-based local thermal equilibrium (LTE) for-  
 mulations, which cannot capture the transient role of preferential pathways or the abrupt transition from infiltration to blockage.  
 The observed switch from active infiltration to macropore refreezing highlights the need for dual-domain and local thermal  
 non-equilibrium (LTNE) frameworks (Larsbo et al., 2019; Heinze and Blöcher, 2019). The experimental dataset presented here  
 provides an opportunity to test such models under controlled yet realistic slope-scale conditions. For instance, the paired macro-  
 545 pore and non-macropore network experiments can inform the parameterisation of dual-permeability modules in HYDRUS or  
 WaSiM, while the measured thermal dynamics and freeze/thaw transitions offer valuable benchmarks for LTNE implemen-  
 tations such as GEOTop. By confronting these models with experimental evidence, their ability to predict runoff generation,  
 pore-pressure evolution, and slope instability under variable winter conditions can be systematically assessed and improved.  
 Taken together, our results demonstrate that macropore networks in frozen soils play a highly dynamic role governed by initial  
 550 water content, thermal state, and refreezing. Soils with few macropores tend to promote immediate runoff and debris flow initia-  
 tion, whereas macroporous soils initially enhance infiltration and pore-pressure build-up before later producing delayed runoff  
 surges. Both pathways are highly relevant for slope stability in mountain environments. With projected increases in winter  
 rainfall and freeze/thaw variability (Ranasinghe et al., 2021; Beniston et al., 2022), preferential flow and transient macropore  
 blockage are likely to become increasingly important for alpine hydrology and hazard prediction.





## 555 5 Conclusions

This study presents nine large-scale laboratory experiments examining rainfall infiltration into frozen slopes under controlled but near-natural boundary conditions. The results reveal the transient and non-linear role of macropore networks in controlling thermo-hydraulic processes in frozen soils:

1. **Freezing dynamics.** Frost penetration was primarily governed by the antecedent thermal state. The presence of an open  
 560 macropore network (volume fraction  $\approx 0.5\%$ ) had negligible influence on frost depth or propagation under the tested conditions.
2. **Infiltration-runoff partitioning.** Partitioning depended strongly on the initial volumetric water content (VWC). At low initial VWC, the matrix remained partly permeable and infiltration was matrix-dominated. At high initial VWC, extensive ice blocking rendered the matrix nearly impermeable and infiltration occurred mainly through the macropore  
 565 network.
3. **Temporal switching of pathways.** At high initial VWC conditions, macropore flow initially enhanced infiltration and drainage, but progressive refreezing and particle-assisted clogging reduced macropore capacity over time, diverting rainfall toward surface runoff.
4. **Hazard-relevant implications.** These contrasting responses imply different event trajectories on slopes: in macropore-  
 570 poor soils, frozen matrices favour rapid conversion of rainfall to surface runoff, consistent with immediate overland-flow pulses and potential debris-flow initiation when sediment supply is available. In macroporous soils, early bypass infiltration can transiently elevate subsurface drainage and pore-water pressures below a frozen surface layer before partial refreezing reduces connectivity and shifts fluxes back to the surface. The timing and magnitude of this switch depend on pre-event VWC, macropore connectivity, and refreezing rates (cf. cumulative flows in Fig. 4d), underscoring  
 575 a threshold-like behaviour rather than a single deterministic outcome.

The dataset provides a benchmark for validating dual-domain and local thermal non-equilibrium (LTNE) formulations, including the transient functionality and blockage of preferential pathways. Future work should extend the parameter space toward compound rain-snow events, repeated freeze-thaw cycles, and finer textures with stronger capillarity. With winter rainfall projected to intensify, representing preferential flow and its dynamic refreezing will be increasingly critical for predicting  
 580 alpine slope stability and subsurface recharge.

*Data availability.* All experimental data used in this study are available at the Open Data repository of the Universität der Bundeswehr München. The dataset is published under the following DOI: <https://doi.org/10.60776/MSLOMM>.

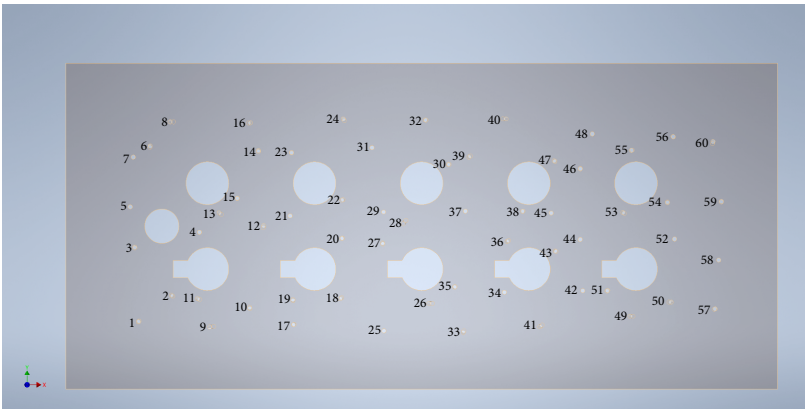
The dataset includes all raw and processed measurements of temperature, volumetric water content, inflow, drainage, and surface runoff, as well as sensor calibration files and experiment metadata. If additional information or derived data are required, please contact the corresponding author.  
 585

**Appendix A: Macropore network geometry**

The macropore network consisted of 60 boreholes ( $\varnothing$  10 mm) with varying lengths and inclinations. About 28 % were vertical, the remaining ones were inclined between  $1^\circ$  and  $20^\circ$  in both longitudinal and transverse directions. Approximately 20 % ended within the soil body, and 15 % were hydraulically connected through intersecting pathways. A representative subset of borehole parameters is listed in Table A1. Figure A1 shows the pattern plate with all 60 boreholes and their respective IDs.

**Table A1.** Representative subset of borehole geometry parameters used in the macropore pattern plate. Here only one angle is shown, the full geometry can be found in the dataset. The full dataset and the full geometry with the 3D CAD technical drawing can be found in the dataset provided. Available in the Open Data repository (DOI: 10.60776/MSLOMM).

Borehole ID	Length [cm]	Inclination [°]	Type
M01	50	4	dead end
M05	90	0	vertical
M30	90	3	interconnected
M45	41	0	dead end
M59	90	0	vertical

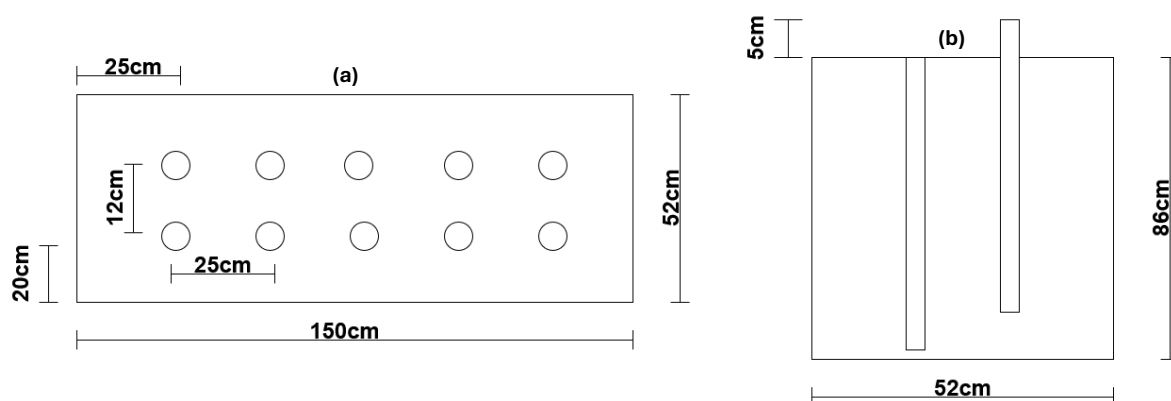


**Figure A1.** Schematic of the macropore pattern plate with 60 numbered boreholes. Large circular openings were left blank to avoid contact with AquaCheck probe heads. The left side corresponds to the upper part of the soil box.



## Appendix B: Sensor positioning and layout

The positions of all AquaCheck probes and individual sensor levels within the soil box are shown in Figure B1. This schematic illustrates the top and rear views of the complete measurement grid used for temperature and volumetric water content monitoring.

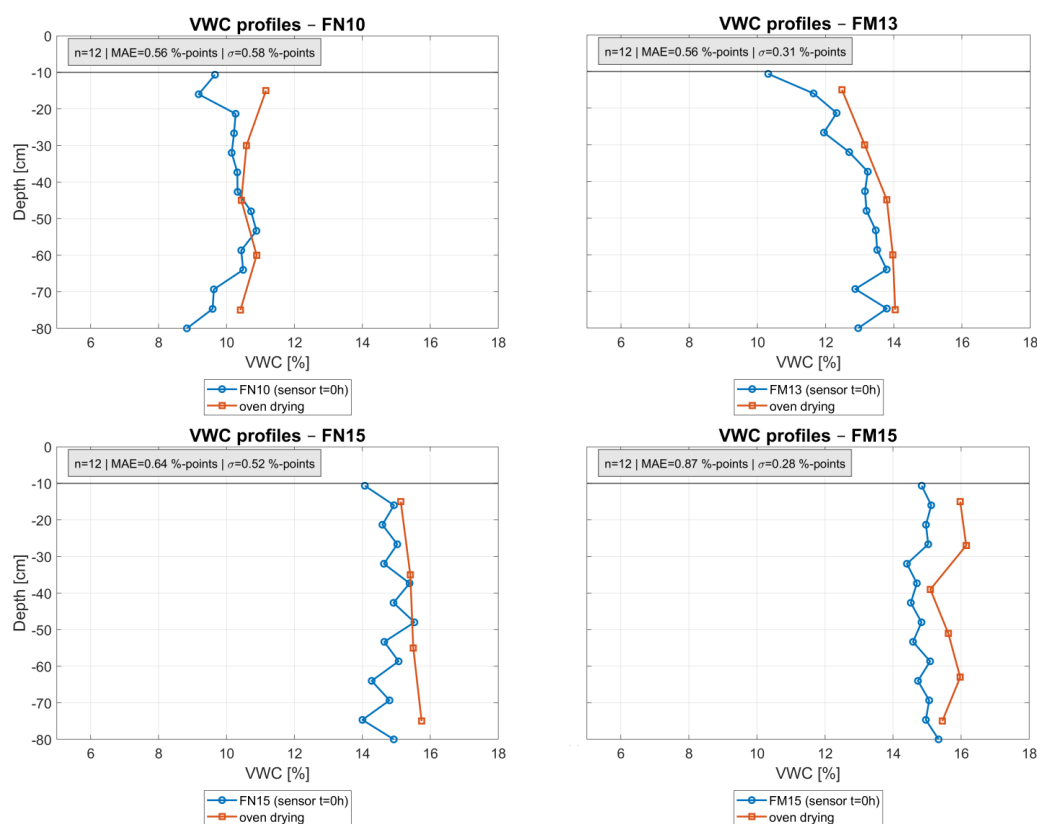


**Figure B1.** Schematic representation of the probe arrangement showing (a) top view and (b) rear view of the soil box with all AquaCheck probe positions (S1–S5 in two parallel rows). Each probe contains eight combined sensors for temperature and volumetric water content.



## 595 Appendix C: Sensor calibration and validation

All AquaCheck capacitance sensors were calibrated against oven-dried soil samples to obtain dielectric values. Calibration was performed over 20 moisture levels covering the full range from air-dry to saturated conditions. For validation of each experiment, additional soil samples were collected and analysed by oven drying to verify the reliability of the calibrated AquaCheck readings under experimental conditions (Fig. C1). The mean absolute deviation between calibrated volumetric  
 600 water contents and oven drying reference values remained below  $\pm 1.0$  percentage points. Temperature readings were validated against PT1000 sensors, and a systematic offset correction of every single sensor was applied. All calibration and comparison data are available in detail in the open data repository (DOI: <https://doi.org/10.60776/MSLOMM>).



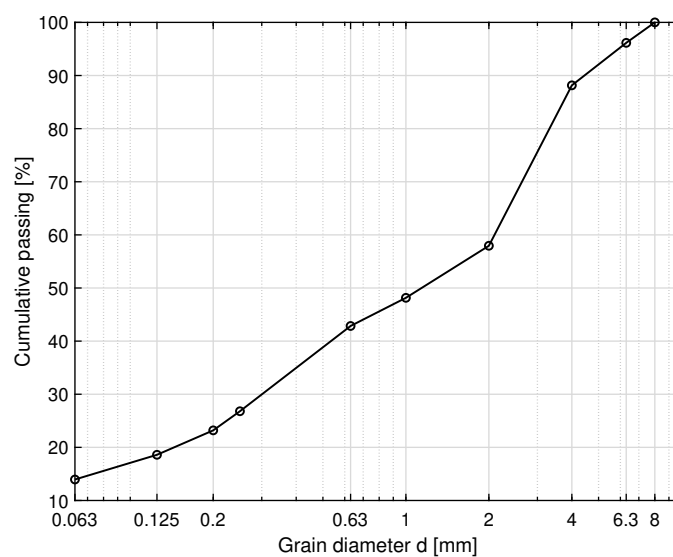
**Figure C1.** Comparison between AquaCheck sensor readings ( $t = 0$  h) and oven-dried volumetric water contents for the four experiments with the largest deviations. Each panel shows the vertical water content profile derived from AquaCheck sensors and corresponding oven-drying samples. Reported values include the mean absolute error (MAE) and standard deviation between both measurement methods, expressed in percentage points.



## Appendix D: Soil specifics

**Table D1.** Grain-size distribution of the artificial soil sample

Grain diameter [mm]	Passing [%] Sample 1
10.0	100.0
8.0	100.0
6.3	96.0
4.0	88.5
2.0	59.2
1.0	49.1
0.63	43.5
0.25	27.2
0.20	23.6
0.125	18.9
0.063	14.2



**Figure D1.** Grain-size distribution of the artificial soil sample





605 *Author contributions.* JB - Conceptualization, Methodology, Investigation, Data curation, Formal analysis, Visualization, Writing - original  
draft preparation;  
SM - Methodology, Technical design, Writing - review and editing;  
IB - Conceptualization, Methodology, Supervision, Project administration, Technical design, Writing - review and editing;  
TH - Conceptualization, Methodology, Writing - review and editing;  
HKB - Writing - review and editing.

610 *Competing interests.* The authors declare they have no competing interests

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