

# Revision of ‘Modeling the Coupled and Decoupled states of Polar Boundary-Layer Mixed-Phase Clouds ’

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This document contains the response to the first review of ‘Modeling the Coupled and Decoupled states of Polar Boundary-Layer Mixed-Phase Clouds’ submitted to EGUSPHERE for possible publication in Atmospheric Chemistry and Physics. Comments from the Reviewer are in black and responses are in blue. Paragraphs that have been added or modified during the revision process are copied in purple.

## Reviewer #1

This paper evaluates two new microphysical parameterizations in simulations of well-tested M-PACE and ISDAC mixed-phase stratocumulus cases in the LMDZ (global atmospheric component of the IPSL-CM Earth System Model) single column model. In this model, boundary layer turbulent fluxes are parameterized with an Eddy Diffusivity-Mass Flux scheme, where the mass-flux scheme is only active when surface convective instability occurs. Therefore, turbulence in decoupled cloud cases (i.e., the ISDAC case) is only parameterized with local counter-gradient diffusion.

In the current version of the model, phase-partitioning in boundary layer clouds is a function of temperature. A parameterization developed in Raillard et al. (2025) for mid-level clouds that replaces a temperature dependent formulation for one that is a function of subgrid turbulent activity and ice crystal properties is added to the convective boundary layer scheme. The second new parameterization adds a “homogenization” term to the equation for the evolution of supersaturation of ice. This parameterization accounts for air parcels mixing between clouds in the environment and air in the surface-forced thermal plumes. This parameterization was included in Furtado et al. (2016) but not in Raillard et al. (2025). This second parameterization is only active when surface convective instability occurs. Simulations without these new parameterizations is referred to as CNTL. Simulations with the new phase-partitioning scheme is referred to as R25. Simulations with both new parameterizations is referred to as TEST.

Perturbed parameters ensemble experiments are performed for the two case studies to test the sensitivity to parameters that control turbulence and ice crystal properties within acceptable ranges.

We sincerely thank the Reviewer for the thorough and insightful review of our manuscript. We truly appreciated all the comments, which have substantially helped us improve the study. Please find below our detailed responses to each comment.

## Comments

For the M-PACE case, only the TEST simulation can produce a mixed-phase stratocumulus with cloud liquid and ice similar to the observations. Even though the R25 simulation has a more realistic potential temperature profile, it produces almost no liquid and too much cloud ice. The fixed Naero5 for the M-PACE case should be much lower than for the ISDAC case. 0.16/L is the value typically used for these cases studies. How does R25 perform with lower values of INP?

Thank you for raising this point. In fact, changing the INP concentration to 0.16/L does not substantially change the results except that slightly higher ice precipitation occurs due to the overall lower ice number concentration (see figure below). Additional sensitivity tests exploring a wider range of INP values and varying the value of other tuning parameters does not change the overall conclusion (not shown). In fact, neglecting the supersaturation source from the plumes' detrainment (i.e. shifting from R25 to TEST) is paramount to capture the liquid-dominated cloud structure and more reasonable ice concentration. Note that the sensitivity to the INP concentration is thoroughly assessed through the inclusion of the  $N_{aero5}$  parameter in the PPE exercise. We have added the following paragraph in Sect. 3.1:

Additional sensitivity tests to the value of free parameters – in particular  $N_{aero5}$  – show that those biases cannot be attributed to calibration issues (not shown).

TEST produces relative humidity with respect to liquid in the liquid layer that is greater than 100%. How is this possible?

First, we would like to emphasize that the relative humidity is a diagnostic variable of the model. By construction, the cloud scheme condenses all the water in excess to saturation with respect to liquid. What is happening in the plot is a very subtle issue related to output variables only. In presence of shallow convection, the cloud scheme computes a subgrid distribution of the saturation deficit  $s$ , and condenses all the water corresponding to  $s$  values higher than the  $s_{liq}$  threshold, which corresponds to liquid saturation. By construction, this adjustment method makes the saturation deficit never exceed 0 and the relative humidity with respect to liquid never exceed 1 (as  $s = q_{sl}(RH - 1)$ ). This has been double-checked with systematic prints at the end of the condensation routine (not shown). However, the quantity that is shown in the plot in the paper is not strictly speaking the mean relative humidity in the mesh  $RH_1$ , but

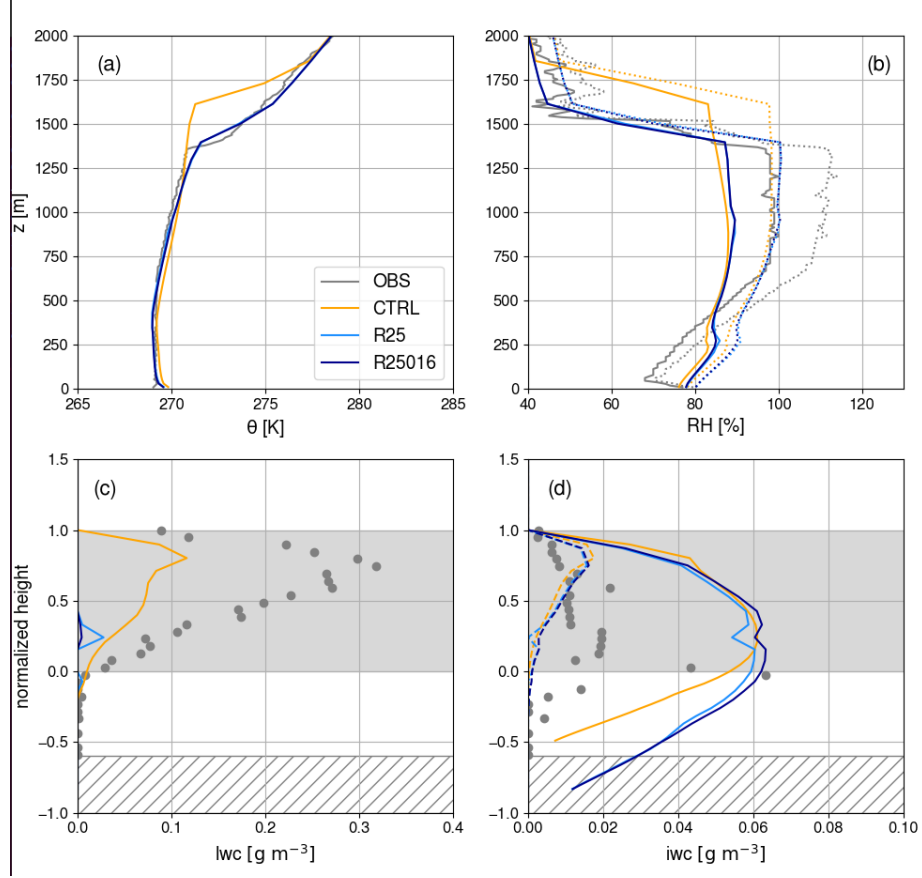


Figure 1: Same as Figure 2 in the main manuscript but the dark blue curve corresponds to a R25 simulation with a INP concentration of 0.16/L.

a diagnostic variable computed at the end of the parameterizations' sequence that can differ by a few % from  $\overline{\text{RH}}_1$ :  $[\text{RH}_1] = \bar{q}/q_{sl}(\bar{T})$ . Here,  $\bar{q}$  and  $\bar{T}$  refer to the mean specific humidity and temperature in the mesh (which are state variables of the model), and  $q_{sl}$  is the saturation specific humidity with respect to the liquid phase. In order to avoid any confusion, the vertical profiles of RHl have been removed from the figure and specifications on how the RHl variable is calculated in the model are now given in the caption.

TEST has near surface layer RH that is much lower than obs and the other runs, indicating too much mixing of sub-cloud air into the liquid layer? This is an interesting point indeed. The investigation of humidity tendencies at the first model level indeed reveals that the shallow convection scheme is more efficient in transporting water upward in the TEST simulation than in

the two other simulations. The exact reason behind this is not completely clear but the weaker ice precipitation flux – that tends to overall dry the system out and which has an associated stabilisation effect due to the sublimation below the cloud – is at least one part of the explanation. Note however that the observed RH profile corresponds to the initial profile of the simulation (see figure below), and that the boundary layer deepens during the run. We do not have any observational reference for the RH vertical profile near the end of the run and thus it is difficult to assess whether this near-surface drying is realistic or not. We have added the following paragraph in the manuscript to clarify this aspect in addition to additional clarification on the difference in timing between the profiles shown in the simulation and that from the observations:

It also exhibits a dryer atmospheric surface layer due to an enhanced upward transport of moisture by shallow convection that coincides with a weaker ice precipitation flux and sublimation below the cloud layer (Figure 2d).

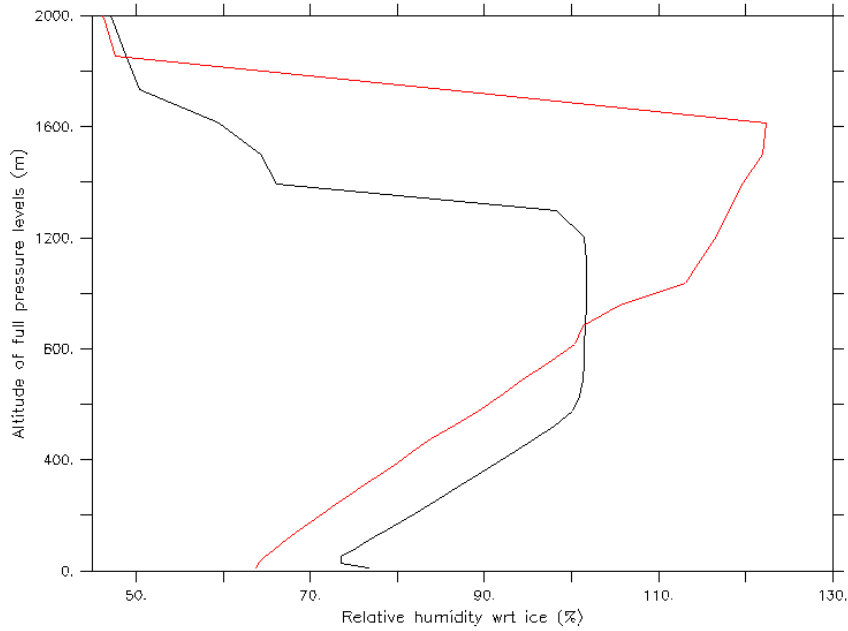


Figure 2: Vertical profile of simulated relative humidity with respect to ice at the beginning of the M-PACE run (black) and 12 hours later (red). Note that the black profile is very close to the radiosounding that served to initialize the profiles in the simulation.

M-PACE has large surface fluxes (cold air outbreak) but is there no representation of cloud-driven top-down turbulence in the model? How does this change the balance between turbulence and microphysics at cloud top in the model?

Although non-local mixing through large eddies — that is, eddies whose size exceeds the typical thickness of model layers — is not taken into account in LMDZ (we elaborate on this aspect in more detail in subsequent responses), local cloud-top turbulence is parameterized through eddy diffusivity using a TKE-1 scheme. The combination of a mass-flux representation of boundary-layer convective structures with an eddy-diffusivity scheme — the so-called thermal plume model — has proven successful in representing the structure of stratocumulus clouds in LMDZ, and in particular, the cloud-top dynamics [Hourdin’2019]. Wu’2020 further showed that adding a parameterization of non-local downdrafts only marginally improves the overall simulation of surface-coupled warm stratocumulus clouds. Overall, we are therefore confident in LMDZ’s ability to represent turbulent transport in the surface-coupled stratocumulus case during M-PACE, and that the absence of parameterized downdrafts is not detrimental to capturing the cloud-top dynamics (again, for surface-based MPCs). Consequently, the main conclusions regarding the interactions between microphysics and turbulence remain robust: the TKE-1 diffusion scheme in LMDZ captures the local generation of turbulence at cloud top associated with local convective instability, and supercooled liquid water (SLW) is then produced through the new phase-partitioning scheme, which explicitly relates TKE to SLW production. We have added a paragraph in Sect. 2.1.1 to emphasize the ability of the thermal plume model to capture the dynamics of stratocumulus clouds:

The combination of the LMDZ eddy-diffusivity and mass-flux schemes has proven successful in representing the structure of stratocumulus clouds, and in particular, the cloud-top dynamics [Hourdin’2019].

TEST produces large TKE above the liquid layer in the inversion (Figure 3c). How is TKE calculated?

This is a good point indeed. TKE is calculated based on a typical prognostic equation (see details in Vignon’2024). The mean vertical profiles of TKE production and loss terms during the same period as that shown in Figure 3c are plotted below. In the TEST simulation, the fact that supercooled liquid water is captured near cloud top strongly enhances the cloud-top radiative cooling. Subsequently, convective instability develops near cloud top and TKE is generated through buoyancy production and is transported – by diffusion – above the liquid layer. Note however the logarithmic x-scale for TKE in Figure 3c. In fact despite the diffusion, the TKE strongly decreases above the inversion. The corresponding paragraph in Section 3.1 has been rephrased as follows:

The subsequent production of SLW in the upper part of the cloud enhances the cloud-top radiative cooling and indirectly the buoyancy production of TKE. This production enhances the TKE near cloud top (Figure 3c), within the cloud layer and even above through TKE diffusion. Note however the logarithmic x-axis for TKE in Figure 3c and therefore the quite sharp decrease of TKE above the cloud.

Lines 341-345: How is turbulence due to cloud-top radiative cooling represented in the model? By local diffusion? Or is it in the microphysical scheme,

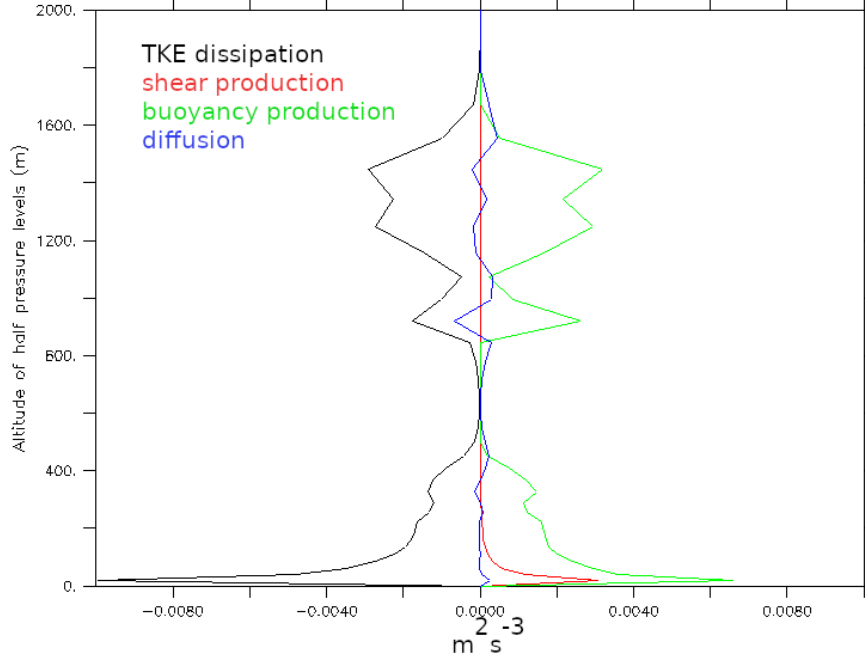


Figure 3: Mean vertical profiles of TKE production and loss terms on the MPACE in the TEST simulation (the same period as that of Figure 3c in the main manuscript is considered).

determined by the Lagrangian turbulent decorrelation time-scale? Is it assumed that local diffusion estimated from TKE is a representation of non-local mixing by cloud-top cooling? Is so, why is TKE limited to cloud top in the ISDAC simulation?

Turbulence due to cloud-top radiative cooling is represented by local turbulent diffusion, that is by the local TKE-l turbulence scheme, the non-local component being missing (see further explanation in our answer to your last comment on the ISDAC simulations). In this scheme, the TKE production terms – in the TKE evolution equation – are closed with local closure formulations. Similarly to traditional TKE-l schemes, the buoyancy production term is expressed with a K-gradient approach (see Vignon et al. 2024). Therefore, the simulated TKE buoyancy production is located near cloud-top and coincides with the occurrence of strong temperature gradients. In the TKE-l diffusion scheme, the vertical transport of TKE is only ensured by local diffusion, which is a relatively slow process, hence the TKE confined near cloud top in our ISDAC simulations. In the microphysical scheme, the SLW production by local turbulence (2nd term in Eq. 15) is related to the TKE calculated in the TKE-l scheme and is therefore a local production. The text of Sect. 3.2 in the main manuscript has been modified to clarify how the turbulence due to cloud-top radiative cooling is rep-

resented in the model:

Subsequently, TKE is locally enhanced through buoyancy production (Figure 6c,d), the latter being parameterized with local K-diffusion formulation [Vignon’2024] which captures only the local component of the cloud-top mixing.

For the ISDAC case, since this is a decoupled case where the surface convective scheme is inactive, R25 and TEST are the same. This simulation tests the impact of the two different phase-partitioning schemes. It is no surprise that the temperature dependent phase-partitioning scheme produces too much cloud ice and causes the liquid layer to collapse.

We agree that it is not that surprising that the temperature dependent phase partitioning produces too much cloud ice which results in an overall too short cloud lifetime. Nonetheless, this phase partitioning is that used in the CMIP6 version of LMDZ. Moreover, many climate models still use a simple temperature function to determine the cloud phase. We therefore deem important to show – even briefly – the effect of such phase partitioning on a simple case of decoupled Arctic boundary-layer cloud. Note that not only the phase-partitioning methodology but also the fact that the cloud water content is estimated through saturation adjustment with respect to the ice phase explain the biases in the CTRL simulations. To emphasize that this result is kind of expected, we have reformulated the corresponding paragraph as follows:

Cloud formation through saturation adjustment with respect to ice results in high in-cloud condensed water contents. In turn, this leads to substantial autoconversion of ice crystals into snowfall and of supercooled liquid droplet into supercooled drizzle, which immediately freezes. Moreover, an excessive ice water content near cloud top - whose temperature ranges between 258 and 260 K - is also expected due to the temperature-based phase partitioning that predicts a cloud ice mass fraction of about 30% [Madeleine’2020]. As a result, high  $q_i$  values and intense ice precipitation are present from cloud top down to the surface.

Lines 367-369: Again top-down vertical diffusion of TKE by subgrid turbulence is discussed but isn’t this just local diffusion in the model?

Yes it is ‘just’ local diffusion (see our answer to your first comment on the ISDAC case and the more general discussion in response to your general comment below). This is now specified in the main text:

Moreover, the top-down vertical transport of TKE by local subgrid turbulent diffusion [Vignon’2024] leads to a net upward turbulent flux of water vapour from the moist lower levels, up to cloud altitude, which favours cloud persistence and deepening.

Figure 6c shows TKE buoyancy term and TKE essentially only at cloud top but Ovchinnikov et al. (2014) shows maximum TKE near the liquid cloud base. Even though the R25/TEST simulations maintain a liquid layer, this result indicates fundamental error in turbulence that will also produce fundamental

errors in microphysics.

We address this comment jointly with the last one. Please see our response below.

Minor comments:

Line 98: Change “ofrid” to “of”.  
Corrected.

Figure 2 and 3: Include “M-PACE” in figure caption.  
Added.

Line 343: “...loop, that...”  
Corrected.

I have major questions about the parameterizations used in this climate model. Is it assumed that local diffusion estimated from TKE is a representation of non-local mixing by cloud-top cooling? If so, why is TKE limited to cloud top in the ISDAC simulation? Also, There are many ways to modify turbulence/microphysics in order to maintain cloud liquid. My concern is that this simulation is getting the right answer for the wrong reason. This is extremely important for climate simulations since it will produce unrealistic sensitivity to changes in environmental conditions, surface conditions, and aerosols. Thank you for this general comment that clearly raises the need for additional information in the paper. First, we would like to emphasize that we totally acknowledge that our model misses the non-local component of the cloud-top driven mixing. As explained above, TKE is limited to cloud-top as the buoyancy-production term is expressed with a local closure and because the model does not have a subgrid mass-flux – i.e. convective – parameterization that represents the non-local transport by cloud-top driven convective cells. As explained in the paper, the shallow-convection scheme only activates when convective instability occurs at the surface. To our knowledge, only a few large-scale atmospheric models account for an explicit parameterization of convective downdrafts triggered at cloud top (e.g., **Wu’2020**). This is an important shortcoming and limitation of our study that should be stated more explicitly at different places of the manuscript and that should appear more clearly as a development priority. However, we do believe that our new parameterization captures the production of SLW for the good reasons, at least qualitatively. Even if it occurs only locally near cloud top, the positive feedback loop involving cloud-top radiative cooling induced by supercooled liquid droplets, subsequent buoyancy production of turbulence as well as the supercooled liquid water production associated with local turbulence is reproduced. Of course, the next step will be to capture this feedback loop with more realistic vertical structure of turbulence considering the non-local mixing by non-local convection triggered at cloud top. This is definitely



in the abstract:

‘most of the turbulence is confined near the cloud-top which is probably due to a missing parameterization for convective downdrafts in the model.’

In section 3.1.2:

‘Qualitatively, the TEST simulation thus captures the positive feedback loop involving cloud-top radiative cooling induced by supercooled liquid droplets, subsequent buoyancy production of turbulence as well as the supercooled liquid water production associated with local turbulence near cloud-top. However, ISDAC LES show that vigorous turbulence is not confined to cloud-top, and that intense turbulent vertical velocity variance extends several hundred meters below the SLW layer **Ovchinnikov’2014**. In fact, the mixed-layer forming below the cloud during ISDAC mostly consists in non-local convective cells triggered by radiative cooling at cloud top. In the absence of surface convective instability, LMDZ does not account for the contribution of non-local vertical turbulent transport by organized convective cells in addition to the local mixing parameterized by K-diffusion. The non-local component of turbulent mixing is thus missed by our model here.’

and:

‘The absence of a dedicated parameterization for non-local convective mixing from cloud-top is likely responsible for an underestimation of the net upward water flux from the underlying moist layers. Parameterizing the cloud-top driven convection such as the convective downdrafts scheme of **Wu’2020** is likely a parameterization development priority to further advance the representation of clouds with an intense cloud-top driven mixing layer. Such a parameterization may also help reduce the TKE at cloud-top and the time-step dependency of our ISDAC simulations (see Appendix A).’

and in the conclusion:

”However, vigorous turbulence remains unrealistically confined close to cloud top and the liquid and ice water contents are underestimated with respect to the LES simulations analyzed in **Ovchinnikov’2014**. Those shortcomings are likely due to the absence of a parameterisation of non-local convection triggered at cloud-top in LMDZ, leading to an overly weak upward turbulent flux of water vapour below and within the cloud.”

”The remaining limits of LMDZ to capture the vertical structure of the turbulence and the cloud water amounts on the ISDAC case also suggest revisiting the LMDZ shallow convection scheme to account for downward non-local mixing triggered by convective instability at the top of surface-decoupled clouds. ”