

Version 3.0.2 of the Crocus snowpack model

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Abstract. This article presents a comprehensive description of the 3.0.2 stable release of the Crocus snowpack model in the SURFEX modelling platform. It synthesizes and harmonizes a number of equations disseminated in various previous publications, introduces a number of unpublished parameterizations and includes new developments implemented since 2012. Among the novelties, an explicit representation of the evolution of impurity mass in snow (e.g. black carbon, mineral dust) allows representing their impact on solar radiation absorption in the snowpack at different wavelengths and their feedback on all snowpack properties. The model also allows the formation of surface ice layers due to freezing rain. In addition, Crocus is coupled to the MEB "big-leaf" vegetation scheme and can therefore be applied in forested areas. A module for snow management can also be optionally activated to simulate the snowpack on ski slopes in ski resorts. The model can be coupled with various blowing snow schemes. The MEPRA expert system which analyses the mechanical stability of the simulated snowpack has been implemented directly within SURFEX. For each physical process represented by empirical parameterizations, several new parameterizations from the literature were implemented. The different combinations of these parameterizations constitute the ESCROC multiphysics ensemble model. It allows the quantification of simulations uncertainty for various applications. Finally, a technical solution was proposed for externalized applications allowing the use of the scheme in other Land Surface Models. The paper also reviews the available scientific evaluations and applications of the model. It describes its numerical efficiency and the main scientific and technical challenges providing guidance for the future of snow modelling.

1 Introduction

A large variety of snowpack modelling systems (e.g. Krinner et al., 2018) have been developed for several decades for various applications (Larger et al., 2020): the computation of energy fluxes at the atmosphere-cryosphere interface in climate modelling and numerical weather prediction; hydrological simulations for discharge forecasting, water resources and hydropower

20 management; physical process studies in the snowpack; avalanche hazard forecasting; glacier mass balance assessment; sea ice modelling; etc. The most detailed snowpack models include a detailed representation of the snowpack stratigraphy as well as an explicit representation of some microstructural properties of the snow layers through the implementation of empirical parameterization of snow metamorphism. There is a relatively limited number of snowpack models with such a level of detail: mainly the "Swiss" SNOWPACK model (Lehning et al., 1999), the "American" SNTherm model (Jordan, 1991), the
25 "Japanese" SMAP model (Niwano et al., 2012) and the "French" Crocus model. The latter has been initially developed by Brun et al. (1989, 1992) and was implemented in the early 2010s in the SURFEX platform of surface modelling (Masson et al., 2013) to facilitate coupling with atmospheric models and the other components of surface modelling, especially soil and vegetation schemes of the ISBA Land Surface Model. The last description of the model was published by Vionnet et al. (2012) after this major evolution.

30 However, numerous evolutions of the model have been implemented after Vionnet et al. (2012). Some of them are only partly described in dedicated scientific publications (Carmagnola et al., 2014; Spandre et al., 2016; Lafaysse et al., 2017; Tuzet et al., 2017; Vionnet et al., 2018; Quéno et al., 2018). These articles were generally published before the merging of all new developments in a unique and stable code version. A comprehensive and accurate description of the state of the last official model release is therefore missing. This lack of documentation has been identified by Menard et al. (2021) as one of the main
35 factors of human errors in numerical simulations. The purpose of this paper is to provide an updated reference with all the functionalities available in the latest stable release of the model. To help the users to find any information they may need to understand the model implementation, all the equations disseminated in the various papers are reported here either in the main text or in Appendices, including the equations already published in previous references of Brun et al. (1992) and Vionnet et al. (2012) in order to provide a self-sufficient reference describing the whole model. Following the recommendations of
40 Menard et al. (2021), a major effort has been dedicated to check the consistency and comprehensiveness between the code and the equations. The scope of this paper is limited to the snowpack on the ground. The coupled modules representing soil, vegetation and blowing snow remain beyond the scope of this paper and only the terms involved in the coupling are mentioned. More details can be found in the reference publications of the coupled models: Decharme et al. (2016); Boone et al. (2017) for soil and vegetation; Vionnet et al. (2014, 2018) and Baron et al. (2024) for blowing snow, cf. Section 2.4.2. Note that the
45 standalone Crocus model was last designated as version 2.4. This versioning was discontinued by Vionnet et al. (2012) in favor of the SURFEX versioning system. However, due to the impossibility to synchronize Crocus and SURFEX main stable releases and the integration of Crocus in other Land Surface Models, a dedicated versioning is necessary for Crocus. This paper thus describes version 3.0.2 of Crocus. Section 2 presents all scientific equations necessary to evolve the state variables of the model. Section 3 presents complementary diagnoses computed as output of the model. Section 4 presents technical features
50 associated with running the model (simulation geometries, numerical efficiency, and associated tools to facilitate running and visualization). Finally, Section 5 reviews the available scientific evaluations of the model and provides an overview of its applications. In light of these elements, we discuss the confidence that can be placed in the simulation results and the main remaining challenges for the future, including perspectives in terms of data assimilation.

Table 1. Available physical options in Crocus. Default options appear in bold. The last column shows options which are not available in the externalized release but only within the SURFEX implementation of Crocus. Although the combination of all options is possible in theory, the options for snow management in ski resorts were only tested with the default options of the other processes and the blowing snow schemes were never tested together with the MEB vegetation scheme.

Process	Namelist key	Options	Requirements	Only in SURFEX
Snowfall	SNOWFALL	V12 , S14, A76		
Metamorphism	SNOWMETAMO	B21 , F06, S-B, S-F		
Compaction	SNOWCOMP	B92 , T11, S14		
Drifting snow (subgrid effect)	SNOWDRIFT	NONE, DFLT, VI13 , GA01		
Mobility index	SNOWMOB	GM98 , VI12		
Absorption of solar radiation	SNOWRAD	B92 , T17	T17 requires LAP forcing	
Thermal conductivity	SNOWCOND	Y81 , C11, I02		
Percolation	SNOWLIQ	B92 , SPK, B02		
Snow-vegetation interactions	MEB	True, False		X
Blowing snow (transport)	SNOWPAPPUS	True, False	2-D grids	X
Blowing snow (transport)	SNOWSYTRON	True, False	4 or 8 slope aspects	X
Machine-made snow	SNOWMAK_ BOOL	True, False		X
Production strategy	SELF_ PROD	True, False	Water use target	X
Grooming	SNOWCOMPACT	True, False		X
Tilling	SNOWTILLER	True, False		X

2 Physical model

55 Compared to Vionnet et al. (2012), the model has become highly modular with the extension of applications and the development of the ESCROC multiphysics framework by Lafaysse et al. (2017). The common modelling structure includes the discretization procedure and the solving of the heat diffusion equation which is the core of the model. Figure 1 presents an overview of the sequence of routines and summarizes the main changes (new routines and updated routines) which are detailed in this Section. Table 1 summarizes the different available options for each process and associated requirements. The details
60 of each option are described in the subsection dedicated to the corresponding process. The ESCROC multiphysics ensemble system consists in the combination of these differents physical options and different values of some key parameters such as τ_a (Section 2.4.9), R_i (Section 2.4.11).

2.1 Forcing variables

The model has to be forced with subdaily time series of air temperature T_a (K) and specific humidity q_a (kg kg^{-1}) at a
65 known level z_a (m), wind speed U (m s^{-1}) at a known level z_u (m), incoming longwave radiation $\text{LW}\downarrow$ (W m^{-2}), incoming shortwave direct and diffuse radiation $\text{SW}_{\text{DIR}}\downarrow$ and $\text{SW}_{\text{DIF}}\downarrow$ (W m^{-2}), rainfall $\mathcal{P}_r$ and snowfall $\mathcal{P}_s$ ($\text{kg m}^{-2} \text{s}^{-1}$) and surface

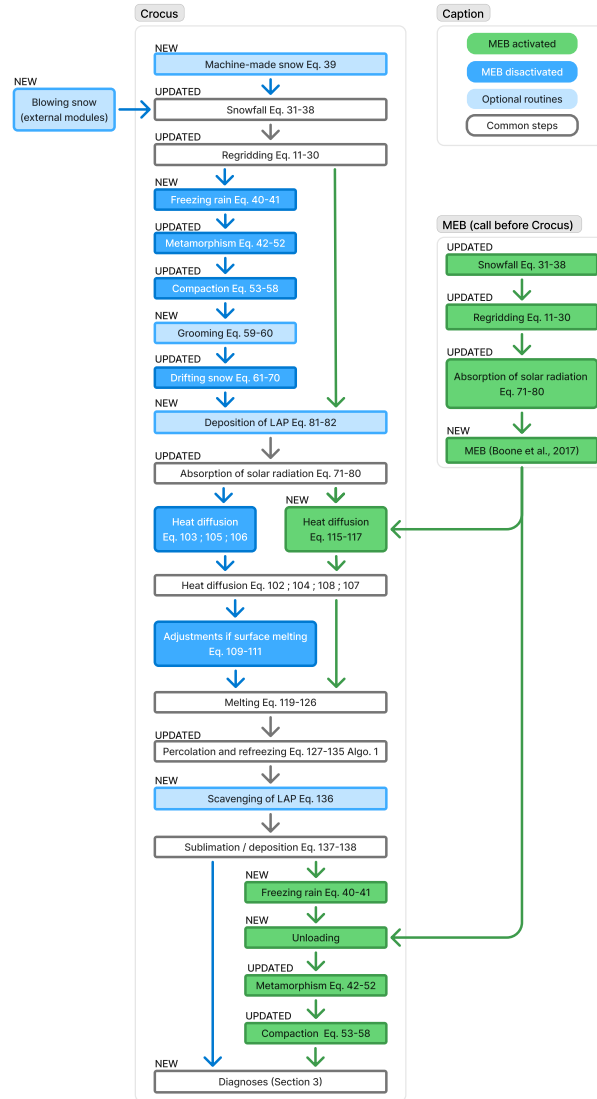


Figure 1. Sequence of Crocus subroutines for each time step without (blue) or with (green) coupling with MEB. Optional subroutines in light blue. Compared to the version of Vionnet et al. (2012), new subroutines are labelled "NEW". The label "UPDATED" refers to subroutines in which changes were applied due to the new state variables for microstructure and where new physical options were implemented. The heat diffusion, melting and sublimation routines were only concerned by minor changes or technical optimizations.

pressure P_s (Pa). The very low sensitivity of model results to P_s allows the user to provide constant P_s values when a time series is not available. The split of global shortwave radiation $SW_{\downarrow}$ between direct and diffuse components is only used with specific model options (coupling with TARTES optical scheme, Section 2.4.9, and/or coupling with MEB big-leaf vegetation scheme, Section 2.4.14). When none of these options are activated, the split between both components is not necessary as only their sum is considered. When TARTES or MEB are activated, an accurate forcing of $SW_{DIR\downarrow}$ and $SW_{DIF\downarrow}$ should always be preferred. Nevertheless, for users interested in these options without available data to separate both components, the following parameterization as a function of the cosine of the solar zenithal angle μ and derived from SBDART clear-sky modelling (Ricchiazzi et al., 1998) at Col de Porte is available for mid-latitude areas. Following Gardner and Sharp (2010), the estimated error in cloudy conditions for the simulated broadband albedo is lower than 0.1. The parameterization is applied by default in the code if the diffuse component is set to zero:

$$\frac{SW_{DIF}}{SW_{DIR} + SW_{DIF}} = \min \left(\exp \left(-1.549919\mu^3 + 3.735357\mu^2 - 3.524211\mu + 0.029911 \right), 1. \right) \quad (1)$$

Optionally, dry and wet deposition fluxes of Light-Absorbing Particles (LAP) $\mathcal{W}_{d,j}$ and $\mathcal{W}_{w,j}$ ($\text{kg m}^{-2} \text{s}^{-1}$) can be included for each type j depending on the physical option selected for radiative transfer (Section 2.4.9).

80 2.2 State variables

The prognostic variables (i.e. transmitted from a given time step to the next one) describing each snow layer i are its mass m_i (kg m^{-2}), density ρ_i (kg m^{-3}), enthalpy H_i (J m^{-2}) defined as the energy required to melt the snow layer i (Boone and Etchevers, 2001), age A_i (days since snowfall), and complementary variables for snow microstructure. The state variables initially used for snow microstructure as described in Vionnet et al. (2012) (dendricity, sphericity, grain size) were replaced by optical diameter d_i (m) and sphericity $S_i \in [0, 1]$ (Carmagnola et al., 2014). After several years of coexistence, the formulation from Brun et al. (1992) was removed from the code in order to improve its readability but also its efficiency as numerous expensive conditional statements could be removed. This change of state variables does not only affect metamorphism evolution laws but also various equations based on microstructure properties in other simulated processes. All modified equations are provided in the following section or in an appendix. In addition, a historical tracker h_i is used as a last state variable with its meaning summarized in Table 2.

Light Absorbing Particles (LAP) are organic or mineral substances able to increase radiation absorption in snow. Tuzet et al. (2017) added LAP mass contents $\mathcal{M}_{i,j}$ (kg m^{-2}) as new optional state variables for each layer i and LAP type j . Although the code is designed to deal with any number of LAP types, only the parameters corresponding to black carbon and mineral dust are implemented in version 3.0.2. LAP interact with the other variable states of the model through absorption of solar radiation when the TARTES optical scheme is activated (Section 2.4.9).

Table 2. Possible values of the historical tracker h_i

	Liquid water at any time before t	Faceted crystals at any time before t	More than one freezing-melting cycle before t .
0	No	No	No
1	No	Yes	No
2	Yes	No	No
3	Yes	Yes	No
4	Yes	No	Yes
5	Yes	Yes	Yes

Note that the layer thickness z_i (m), the layer temperature T_i (K) and the layer mass of liquid water l_i (kg m^{-2}) can be directly derived from the state variables and are used in many parts of the model.

$$z_i = \frac{m_i}{\rho_i} \quad (2)$$

$$T_i = \min(T_0, T_i^*) \quad (3)$$

$$l_i = \max(0, T_i^* - T_0) \frac{m_i c_I}{L_m} \quad (4)$$

$$\text{where } T_i^* = T_0 + \frac{H_i}{m_i c_I} + \frac{L_m}{c_I} \quad (5)$$

T_0 (K) is the water melting point temperature which in SURFEX is assumed to be equal to the triple point value. L_m (J kg^{-1}) is the latent heat of fusion, and c_I ($\text{J kg}^{-1} \text{K}^{-1}$) the ice thermal capacity. Note also that the temperature θ_i in $^\circ\text{C}$ is also used in some parameterizations:

$$\theta_i = T_i - T_0 \quad (6)$$

2.3 Layering

2.3.1 Vertical discretization

One of the main original feature of Crocus compared to the majority of snowpack schemes available in the literature is its Lagrangian vertical discretization based on a dynamical evolution of the number and thicknesses of the numerical snow layers. The number of active layers N varies between $N_{\min} = 3$ and a user-defined maximum $N_{\max}$ (the default value is 50). Each layer is referenced by the index i which varies from 1 for the surface layer to N for the deepest layer. The main discretization principles described in Vionnet et al. (2012) are still valid in the current version but they have been a bit complexified to solve numerical issues in specific applications. The current article provides the first comprehensive formulation of the algorithm.

115 First, a similarity criterion $D(i, i+1)$ between adjacent layers i and $i+1$ is defined. The initial formulation was a Manhattan distance of weighted values of dendricity, sphericity and grain size but it has never been published. The strict variable transformation of Carmagnola et al. (2014) led to a unjustified complexity in the formulation of this distance. Therefore, this distance was simplified in the same spirit by:

$$\begin{cases} D(i, i+1) = 50(|S_{i+1} - S_i| + 2000|d_{i+1} - d_i| + \delta_h(i, i+1)) & \text{if } (A_i - A_{i+1}) < 300 \\ D(i, i+1) = 200 & \text{otherwise} \end{cases} \quad (7)$$

120 where

$$\begin{cases} \delta_h(i, i+1) = 1 & \text{if } (h_i > 1 \text{ and } h_{i+1} \leq 1) \text{ or } (h_i \leq 1 \text{ and } h_{i+1} > 1) \\ \delta_h(i, i+1) = 0 & \text{otherwise} \end{cases} \quad (8)$$

The 2000 coefficient is chosen for normalization considering the typical range of 5.10^{-4} m between highest and lowest values of d_i (Carmagnola et al., 2014) and the range of 1 between highest and lowest values of S_i . The δ_h function avoids the aggregation between cold snow and wet/refrozen snow. The specific case of significant age difference was introduced to avoid
125 the aggregation of a recent snow layer with layers describing permanent snow or glacier. This distance is noted $D(n, 1)$ when it is applied between a new snowfall and the surface layer.

When it is necessary to choose two layers to aggregate, a penalty criteria $P(i, i+1)$ is defined by:

$$P(i, i+1) = D(i, i+1) + 25 \left(\frac{z_i}{z_i^*} + \frac{z_{i+1}}{z_{i+1}^*} \right) \quad (9)$$

where z_i^* (m) is the layer thickness of the optimal attractor profile defined in Appendix A.

130 Layers l_{sup} and l_{inf} are the adjacent layers which satisfy:

$$P(l_{\text{sup}}, l_{\text{inf}}) = \min_{i \in [1, N-1]} (P(i, i+1)) \quad (10)$$

The algorithm modifies the thicknesses at the previous time step $z_i^{t-\Delta t}$ for $i \in [1, N^{t-\Delta t}]$ towards a new profile z_i^t for $i \in [1, N^t]$ following Eq. 11 by a succession of exclusive conditional statements depending on the total initial depth $Z^{t-\Delta t} = \sum_{i=1}^N z_i^{t-\Delta t}$, the initial thickness of the first layer $z_1^{t-\Delta t}$, the thickness of new snowfall to add $z_n = \frac{m_n}{\rho_n}$ (m), and the initial
135 number of layers $N^{t-\Delta t}$. The computations of the mass m_n (kg m^{-2}) and density of new snowfall ρ_n (kg m^{-3}) are described later in Section 2.4.1.

$$\left\{ \begin{array}{l} \text{If } z_n > 0 \\ \text{else} \\ \text{else} \end{array} \right\} \left\{ \begin{array}{l} \left[\begin{array}{l} \text{If } Z^{t-\Delta t} < Z_{\min} \\ \text{or } N^{t-\Delta t} < N_{\min} \end{array} \right] \left\{ \begin{array}{l} N^t = \max[N_{\min}, \min(N_{\max}, \lfloor 100z_n \rfloor)] \\ z_i^t = \frac{z_n}{N^t} \forall i \in [1, N^t] \end{array} \right\} \\ \left[\begin{array}{l} \text{If } z_1^{t-\Delta t} < z_1^* \text{ and } D(n, 1) < 0.2 \\ \text{or } \frac{m_n}{\Delta t} < 3 \times 10^{-5} \text{ kg m}^{-2} \text{ s}^{-1} \text{ and } z_1 < 2z_1^* \\ \text{or } z_1^{t-\Delta t} < 10^{-4} \end{array} \right] \left\{ \begin{array}{l} N^t = N^{t-\Delta t} \\ z_1^t = z_1^{t-\Delta t} + z_n \\ z_i^t = z_i^{t-\Delta t} \forall i \in [2, N^t] \end{array} \right\} \\ \left[\begin{array}{l} \text{If } N^{t-\Delta t} < N_{\max} \\ \text{else} \end{array} \right] \left\{ \begin{array}{l} N^t = N^{t-\Delta t} + 1 \\ z_1^t = z_n \\ z_i^t = z_{i-1}^{t-\Delta t} \forall i \in [2, N^t] \end{array} \right\} \\ \left[\begin{array}{l} \text{else} \\ \text{else} \end{array} \right] \left\{ \begin{array}{l} N^t = N_{\max} \\ z_1^t = z_n \\ z_i^t = z_{i-1}^{t-\Delta t} \forall i \in [2, l_{\sup}] \\ z_{l_{\inf}}^t = z_{l_{\sup}} + z_{l_{\inf}} \\ z_i^t = z_i^{t-\Delta t} \forall i \in [l_{\inf} + 1, N_{\max}] \end{array} \right\} \end{array} \right\} \quad (11)$$

$$\left\{ \begin{array}{l} \text{If } z_1^{t-\Delta t} < 5.10^{-3} \\ \text{else} \\ \text{else} \end{array} \right\} \left\{ \begin{array}{l} \left[\begin{array}{l} \text{If } z_1^{t-\Delta t} < 5.10^{-3} \\ \text{If } z_{N^{t-\Delta t}}^{t-\Delta t} < 10^{-2} \end{array} \right] \left\{ \begin{array}{l} N^t = N^{t-\Delta t} - 1 \\ z_1^t = z_1^{t-\Delta t} + z_2^{t-\Delta t} \\ z_i^t = z_{i+1}^{t-\Delta t} \forall i \in [2, N^t] \end{array} \right\} \\ \left[\begin{array}{l} \text{If } \exists j \in [1, \min(N^t - 1, N_{\max} - 4)] | z_j^{t-\Delta t} > \left(8 - \frac{N_{\max} - N^{t-\Delta t}}{N^{t-\Delta t} - N_{\min}} \right) z_j^* \\ \text{else} \end{array} \right] \left\{ \begin{array}{l} N^t = N^{t-\Delta t} + 1 \\ z_i^t = z_i^{t-\Delta t} \forall i \in [1, j-1] \\ z_j^t = \frac{z_j^{t-\Delta t}}{2} \forall i \in [j, j+1] \\ z_i^t = z_{i-1}^{t-\Delta t} \forall i \in [j+2, N^t] \end{array} \right\} \\ \left[\begin{array}{l} \text{If } \exists j \in [2, N^t - 1] | \left[\begin{array}{l} z_j^{t-\Delta t} < \frac{5z_j^*}{D(i, i+1)} \\ \text{and } (z_j^{t-\Delta t} + z_{j+1}^{t-\Delta t}) < 4.5 \max(z_j^*, z_{j+1}^*) \end{array} \right] \\ \text{else} \end{array} \right] \left\{ \begin{array}{l} N^t = N^{t-\Delta t} - 1 \\ z_i^t = z_i^{t-\Delta t} \forall i \in [1, j-1] \\ z_j^t = z_j^{t-\Delta t} + z_{j+1}^{t-\Delta t} \\ z_i^t = z_{i+1}^{t-\Delta t} \forall i \in [j+1, N^t] \end{array} \right\} \\ \text{else} \left\{ \begin{array}{l} N^t = N^{t-\Delta t} \\ z_i^t = z_i^{t-\Delta t} \forall i \in [1, N^t] \end{array} \right\} \end{array} \right\}$$

In the definition of the initial number of layers (first line of Eq. 11), $\lfloor \cdot \rfloor$ designates the floor operator. The literal translation of Eq. 11 is as follows. A uniform layering is applied for new snowfall on the ground while the total snow depth does not reach $Z_{\min} = 0.03$ m. In other cases, snowfall is aggregated to the surface layer when it is similar to a sufficiently thin surface layer or when it is very low. When new snowfall is too thick or too different from the surface layer, a new layer is created. However, if $N_{\max}$ was already reached, this layer creation is done after the preliminary aggregation of the two closest layers of the profile $l_{\sup}$ and $l_{\inf}$ (as defined by Eq. 10). When there is no snowfall, the algorithm applies only one of the following modification by order of priority: aggregation of surface layer or bottom layer when too thin, split of internal layer when too thick, aggregation of internal layer when too thin, relative to the optimal attractor profile. Note than only one modification by point is allowed at each time step. Thus, when the conditions for an internal split or aggregation are obtained for several layers (i.e. several values of j) at the same time, it is only applied for the uppermost layer $\min(j)$. For glacier applications, aggregation is strictly

forbidden between snow and ice layers (i.e. when $\rho_i < \rho_G$ and $\rho_{i+1} > \rho_G$ where the threshold density for glacier ρ_G can be adjusted by the user (default 850 kg m^{-3}).

150 This algorithm is applied independently at each simulation point. Therefore, the vertical layering differs between points in terms of number and thickness of snow layers. This raises a number of vectorization issues in the management of loops which were the topic of recent investigations detailed in Appendix J.

2.3.2 Aggregation of layers

When two layers i and $i+1$ are aggregated ($z_i^t = z_i^{t-\Delta t} + z_{i+1}^{t-\Delta t}$ from Eq. 11) the state variables are modified in order to
 155 conserve mass and enthalpy. The optical diameter is updated in order to obtain a mass-weighted average of the corresponding albedo. A mass-weighted average is also applied for sphericity and age.

$$m_i^t = m_i^{t-\Delta t} + m_{i+1}^{t-\Delta t} \quad (12)$$

$$\rho_i^t = \frac{m_i^t}{z_i^t} \quad (13)$$

$$H_i^t = H_i^{t-\Delta t} + H_{i+1}^{t-\Delta t} \quad (14)$$

$$160 \quad d_i^t = \left[\frac{0.9 - \frac{m_i^{t-\Delta t} (0.9 - 15.4 \sqrt{d_i^{t-\Delta t}}) + m_{i+1}^{t-\Delta t} (0.9 - 15.4 \sqrt{d_{i+1}^{t-\Delta t}})}{m_i + m_{i+1}}}{15.4} \right]^2 \quad (15)$$

$$S_i^t = \frac{m_i^{t-\Delta t} S_i^{t-\Delta t} + m_{i+1}^{t-\Delta t} S_{i+1}^{t-\Delta t}}{m_i + m_{i+1}} \quad (16)$$

$$A_i^t = \frac{m_i^{t-\Delta t} A_i^{t-\Delta t} + m_{i+1}^{t-\Delta t} A_{i+1}^{t-\Delta t}}{m_i + m_{i+1}} \quad (17)$$

$$h_i^t = \begin{cases} h_i^{t-\Delta t} & \text{if } m_i^{t-\Delta t} \geq m_{i+1}^{t-\Delta t} \\ h_{i+1}^{t-\Delta t} & \text{otherwise} \end{cases} \quad (18)$$

$$\mathcal{W}_{d,i}^t = \mathcal{W}_{d,i}^{t-\Delta t} + \mathcal{W}_{d,i+1}^{t-\Delta t} \quad (19)$$

$$165 \quad \mathcal{W}_{w,i}^t = \mathcal{W}_{w,i}^{t-\Delta t} + \mathcal{W}_{w,i+1}^{t-\Delta t} \quad (20)$$

The same equations apply to aggregate falling snow with the surface layer replacing x_i^t , $x_i^{t-\Delta t}$ and $x_{i+1}^{t-\Delta t}$ by respectively x_1^t , $x_1^{t-\Delta t}$ and x_n for each x representing all state variables m , ρ , H , d , S , A , h , $\mathcal{W}_d$ and $\mathcal{W}_w$ in Eq. 12-20.

2.3.3 Splitting of layers

When a layer i is split into two layers i and $i + 1$ ($z_i^t = z_{i+1}^t = \frac{z_i^{t-\Delta t}}{2}$ from Eq. 11), mass and enthalpy are divided into equal parts and microstructure properties are not modified:

$$m_i^t = m_{i+1}^t = \frac{m_i^{t-\Delta t}}{2} \quad (21)$$

$$\rho_i^t = \frac{m_i^t}{z_i^t} \quad (22)$$

$$H_i^t = H_{i+1}^t = \frac{H_i^{t-\Delta t}}{2} \quad (23)$$

$$d_i^t = d_{i+1}^t = d_i^{t-\Delta t} \quad (24)$$

$$S_i^t = S_{i+1}^t = S_i^{t-\Delta t} \quad (25)$$

$$A_i^t = A_{i+1}^t = A_i^{t-\Delta t} \quad (26)$$

$$h_i^t = h_{i+1}^t = h_i^{t-\Delta t} \quad (27)$$

$$\mathcal{W}_{d,i}^t = \mathcal{W}_{d,i+1}^t = \frac{\mathcal{W}_{w,i}^{t-\Delta t}}{2} \quad (28)$$

$$\mathcal{W}_{w,i}^t = \mathcal{W}_{w,i+1}^t = \frac{\mathcal{W}_{w,i}^{t-\Delta t}}{2} \quad (29)$$

$$180 \quad (30)$$

2.4 Evolution equations

2.4.1 Snowfall

The new snow amount is the result of solid precipitation, but also deposition of blowing snow and snowmaking, when the corresponding modules are activated. These three mass sources are respectively referred by the subscripts SP, BS and SM in the following. In case of simultaneous occurrence, only one additional layer is created with weighted physical properties. Thus, the mass of the new layer is defined by:

$$m_n = m_{SP} + m_{BS} + m_{SM} \quad (31)$$

The density of new snow ρ_n , optical diameter d_n , and sphericity S_n are expressed by:

$$\rho_n = \frac{\rho_{SP}m_{SP} + \rho_{BS}m_{BS} + \rho_{SM}m_{SM}}{m_n} \quad (32)$$

$$190 \quad d_n = \frac{d_{SP}m_{SP} + d_{BS}m_{BS} + d_{SM}m_{SM}}{m_n} \quad (33)$$

$$S_n = \frac{S_{SP}m_{SP} + S_{BS}m_{BS} + S_{SM}m_{SM}}{m_n} \quad (34)$$

The mass of solid precipitation during the time step Δt is directly provided by the forcing:

$$m_{SP} = \mathcal{P}_s \Delta t \quad (35)$$

Several empirical expressions of the density of natural falling snow ρ_{SP} are implemented (Vionnet et al., 2012; Schmucki et al., 2014; Anderson, 1976), as a function of 2-m air temperature $T_a^* (^{\circ}C) = T_a - T_0$ and 10-m wind speed U_{10} ($m s^{-1}$). They can be activated through the SNOWFALL physical option following Eq. 36. An illustration comparing these formulations is provided in Lafaysse et al. (2017), Figure 1 in the corrigendum. The parameters are listed in Appendix K3. When the forcing wind speed is not available at a 10 m height, a logarithmic adjustment is applied following Appendix B.

$$\left\{ \begin{array}{ll} \text{If SNOWFALL = V12:} & \rho_{SP} = \max(\rho_{\min}, a_{\rho} + b_{\rho}T_a^* + c_{\rho}\sqrt{U_{10}}) \\ \text{If SNOWFALL = S14:} & \begin{cases} \log_{10}(\rho_{SP}) = e_{\rho} + f_{\rho}T_a^* + g_{\rho} + h_{\rho}\sin^{-1}(\sqrt{i_{\rho}}) + j_{\rho}\log_{10}(\max[U_{10}, 2]) & \text{if } T_a^* \geq -14^{\circ}C \\ \log_{10}(\rho_{SP}) = e_{\rho} + f_{\rho}T_a^* + h_{\rho}\sin^{-1}(\sqrt{i_{\rho}}) + j_{\rho}\log_{10}(\max[U_{10}, 2]) & \text{otherwise} \end{cases} \\ \text{If SNOWFALL = A76:} & \rho_{SP} = \rho_{\min} + \max(k_{\rho}(T_a^* + l_{\rho})^{1.5}, 0) \end{array} \right. \quad (36)$$

Adjustments of parameter c_{ρ} were proposed by Woolley et al. (2024) to account for the uncertainties associated with the impact of wind speed on Arctic snowfall density. Although hard-coded in version 3.0.2, this parameter will be tunable in a future version.

Several formulations of microstructure properties of new snow were implemented by Vionnet et al. (2018) depending on SNOWDRIFT option. Again, Appendix B is used to assess the 5-m wind speed U_5 from the forcing wind speed U at height z_u . SNOWDRIFT options are reformulated here with the new microstructure variables now used in the model:

$$\left\{ \begin{array}{ll} \text{If SNOWDRIFT=NONE} & \begin{cases} S_{SP} = \min(\max(0.0795U_5 + 0.38, 0.5), 0.9) \\ d_{SP} = 10^{-4}(\delta_{NONE} + (1 - \delta_{NONE})(4 - S_{SP})) \\ \text{where } \delta_{NONE} = \min(\max(1.29 - 0.173U_5, 0.2), 1) \end{cases} \\ \text{If SNOWDRIFT=DFLT} & \begin{cases} S_{SP} = 0.5 \\ d_{SP} = 10^{-4} \end{cases} \\ \text{If SNOWDRIFT=VI13} & \begin{cases} S_{SP} = \min(\max(0.035U_5 + 0.43, 0.5), 0.9) \\ d_{SP} = 10^{-4}(\delta_{VI13} + (1 - \delta_{VI13})(4 - S_{SP})) \\ \text{where } \delta_{VI13} = \min(\max(1.14 - 0.07U_5, 0.2), 1) \end{cases} \\ \text{If SNOWDRIFT=GA01} & \begin{cases} S_{SP} = 1 - 0.49\delta_{GA01} \\ d_{SP} = 10^{-4}(\delta_{GA01} + (1 - \delta_{GA01})(4 - S_{SP})) \\ \text{where } \delta_{GA01} = \min(\max(2.868\exp(-0.085U_5) - 1, 0), 1) \end{cases} \end{array} \right. \quad (37)$$

VI13 refers to the approach of Vionnet et al. (2013) and GA01 refers to the approach of Gallée et al. (2001). The initial value of the historical tracker is $h_n = 0$ and the initial value of snow age is $A_n = 0$. At each following time step, this variable

remembers the duration from the snowfall event by the simple evolution:

$$210 \quad A_i^{t+\Delta t} = A_i^t + \frac{\Delta t}{86400} \quad (38)$$

2.4.2 Blowing snow

The mass, density, optical diameter and sphericity of blowing snow (m_{BS} , ρ_{BS} , d_{BS} , S_{BS}) can be provided by an external snow transport module. Within SURFEX, three different snow transport modules can be coupled to Crocus. The SYTRON module (Durand et al., 2001; Vionnet et al., 2018) is designed to simulate erosion and accumulation from the windward to
 215 the leeward side of the crests in French operational simulations based on an idealized topography. The SnowPappus module comprehensively described by Baron et al. (2024) is designed for gridded simulations at horizontal resolutions between 30 and 250 m (Haddjeri et al., 2024). Finally, snow transport can be solved by an explicit coupling with the MESO-NH Large Eddy Simulation model for process studies on small study domains and at the event scale (Vionnet et al., 2014, 2017).

2.4.3 Machine-made snow

220 A representation of machine-made snow can optionally be provided by a dedicated module activated by the logical option SNOWMAK_BOOL. This enables the model to compute the mass, density, optical diameter and sphericity of machine-made snow (snowmaking) (m_{SM} , ρ_{SM} , d_{SM} , S_{SM}) and its interaction with the rest of the snowpack. First, the wet bulb temperature T_w (expressed in K) is computed following Eq. F20 in Appendix F. The machine-made production is allowed if both the wet bulb temperature and the wind speed are lower than the respective user-defined thresholds T_{lim} and U_{lim} . When the meteorological
 225 conditions are satisfied, snowmaking is activated only during two periods over the winter season: the "base-layer generation" production period and the "reinforcement" production period (Spandre et al., 2016; Hanzer et al., 2020). The dates of beginning and end of each period and the times allowed in the day are defined by the user from parameters day_1 to day_3 and t_1 to t_4 described in Appendix K3. Two different strategies can be adopted depending on the SELF_PROD logical option. When it is set to True, the production follows a pre-defined set of rules. In this case, during the base-layer generation period the production
 230 is allowed until a given amount of water p_{lim} (kg m^{-2}) is used. During the reinforcement period, instead, the production is allowed if the total snow depth Z is lower than a threshold Z_{lim} . If SELF_PROD is False, the production is forced to match a water use target (kg m^{-2}) defined by the user for each simulated point, regardless of any meteorological or timing condition.

The mass of machine-made snow is then obtained by:

$$m_{SM} = (1 - \mathcal{L}_{SM}) \frac{\mathcal{I}_{SM}}{\mathcal{A}_{SM}} (a_{SM}(T_w - T_0) + b_{SM}) \Delta t \quad (39)$$

235 where $\mathcal{I}_{SM} = 1$ when production is allowed, and 0 otherwise, $\mathcal{A}_{SM}$ is the surface area covered by a snow gun set to 3300 m^2 , and $\mathcal{L}_{SM}$ the loss factor set to 0.4 by Spandre et al. (2016). a_{SM} ($\text{kg K}^{-1} \text{s}^{-1}$) and b_{SM} (kg s^{-1}) are regression coefficients of the parameterization of the potential mass produced by a snowgun. They can be adjusted by the user or derivated from Olefs et al. (2010).

The density ρ_{SM} of machine-made snow can be adjusted by the user whereas the snow microstructure properties d_{SM} and
 240 S_{SM} are fixed following Spandre et al. (2016).

For more information about the implementation of the snowmaking practices in Crocus, please refer to Spandre et al. (2016) and Hanzer et al. (2020).

2.4.4 Freezing rain

When liquid precipitation occurs at negative temperatures, the model can simulate the formation of an ice layer at the top of the surface following the work of Quéno et al. (2018). In a first step, the whole precipitation mass is assumed to form a new ice layer at T_0 , only aggregated to the previous surface layer if a thin ice layer is already present (Eq. 40)

$$\text{If } \mathcal{P}_r > 0 \text{ and } T_a < T_0 : \left\{ \begin{array}{l} m_n = \mathcal{P}_r \Delta t \\ \rho_n = \rho_I \\ H_n = -L_m \mathcal{P}_r \Delta t \\ A_n = 0 \\ d_n = 2 \times 10^{-3} \text{m} \\ S_n = 1 \\ h_n = 2 \end{array} \right. \quad (40)$$

$$\text{If } (D(n, 1) < 20 \text{ and } z_1^- < 0.01) \text{ or } N^- = N_{\max} : \left\{ \begin{array}{l} N^+ = N^- \\ \text{Eq. 12 - 20 applied to } (x_n, x_1^-) \\ \forall x \in [m, \rho, H, A, d, S, h] \end{array} \right.$$

$$\text{else : } \left\{ \begin{array}{l} N^+ = N^- + 1 \\ x_1^+ = x_n \forall x \in [m, \rho, H, A, d, S, h] \\ x_i^+ = x_{i-1}^- \forall x \in [m, \rho, H, A, d, S, h] \text{ and } \forall i \in [2, N^+] \end{array} \right.$$

The energy associated with the phase change E_{FRZ} (W m^{-2}) is computed by Eq. 41 and accounted for further as an additional energy source in the surface energy balance (Eq. 94), able to partly melt this new ice layer:

$$\left\{ \begin{array}{l} \text{If } \mathcal{P}_r > 0 \text{ and } T_a < T_0 : E_{\text{FRZ}} = (1 - \phi_{\text{FRZ}}) L_m \mathcal{P}_r \Delta t \text{ where } \phi_{\text{FRZ}} = \frac{c_w}{L_m} (T_0 - T_a) \\ \text{else : } E_{\text{FRZ}} = 0 \end{array} \right. \quad (41)$$

The assumption behind Eq.41 is that a fraction ϕ_{FRZ} of the latent heat release due to refreezing is consumed by the increase of temperature from T_a to T_0 and the remaining part is fully stored by the surface layer and can either be available for melting or be partly dissipated through diffusion or heat exchanges with the atmosphere, as solved later in Sections 2.4.12 and 2.4.13.

Note that some other implementations of this process in other models consider than while all the precipitation eventually freezes and contributes to the formation of an ice layer at the surface, only a fraction of the associated latent heat is kept in

the ice layer, while the remaining latent heat is transferred to the atmosphere at a shorter time scale than the model time step (Lackmann et al., 2002; Basnet and Thériault, 2025).

2.4.5 Metamorphism

The prognostic equations of microstructure variables d_i and S_i are still fully empirical in the absence of physical evolution laws. They depend on conditions of the vertical temperature gradient $\mathcal{G}_i$ estimated by:

$$\begin{cases} \mathcal{G}_1 = \frac{2|T_2 - T_1|}{z_1 + z_2} \\ \mathcal{G}_i = \frac{2|T_{i+1} - T_{i-1}|}{z_{i-1} + 2z_i + z_{i+1}} \forall i \in [2, N-1] \\ \mathcal{G}_N = \frac{2|T_N - T_{N-1}|}{z_{N-1} + z_N} \end{cases} \quad (42)$$

Following Brun et al. (1992) and Vionnet et al. (2012), the evolution of sphericity ΔS_i during a time step Δt is defined by Eq. 43 (dry metamorphism) and 44 (wet metamorphism):

$$\text{If } l_i = 0 : \begin{cases} \text{If } \mathcal{G}_i < 5 \text{ K m}^{-1} \begin{cases} \text{If } S_i < 1 & \Delta S_i = \text{sph}_1 e^{-6000/T_i} f_{\text{corr}}(d_i, S_i, h_i) \Delta t \\ \text{else} & \Delta S_i = 0 \end{cases} \\ \text{else} \begin{cases} \text{If } S_i > 0 & \Delta S_i = -\text{sph}_2 e^{-6000/T_i} \mathcal{G}_i^{0.4} \Delta t \\ \text{else} & \Delta S_i = 0 \end{cases} \end{cases} \quad (43)$$

$$\text{265 If } l_i > 0 : \begin{cases} \text{If } S_i < 1 : \Delta S_i = \max \left(\text{sph}_3 \left(100 \frac{l_i}{\rho_i z_i} \right)^3, \text{sph}_2 e^{-6000/T_0} \right) \Delta t \\ \text{If } S_i = 1 : \Delta S_i = 0 \end{cases} \quad (44)$$

Parameters sph_1 , sph_2 and sph_3 are provided in Appendix K3. $f_{\text{corr}}(d_i, S_i, h_i)$ is an unpublished parameterization in the original code of Vionnet et al. (2012) which modifies the general behaviour of Eq. 43 by reducing the sphericity increase of snow layers with microstructure properties typical of depth hoar or large faceted crystals and submitted to low thermal gradients. This prevents the formation of rounded grains from depth hoar or large faceted crystals. Indeed, the persistence of anisotropy in this case was obtained with a phase-field numerical model applied to snow microstructure (Bouvet et al., 2022) and recently confirmed by unpublished tomography observations.

$$\begin{cases} \text{If } S_i \geq 0.5 ; h_i = 1 \text{ and } g_{s_i}(d_i, S_i) > 5 \times 10^{-4} \text{ m} & f_{\text{corr}}(d_i, S_i, h_i) = 0 \\ \text{If } S_i < 0.5 ; h_i = 1 \text{ and } g_{s_i}(d_i, S_i) > 5 \times 10^{-4} \text{ m} & f_{\text{corr}}(d_i, S_i, h_i) = \exp\left(\frac{3 \times 10^{-4} - g_{s_i}(d_i, S_i)}{10^{-4}}\right) \\ \text{otherwise} & f_{\text{corr}}(d_i, S_i, h_i) = 1 \end{cases} \quad (45)$$

h_i is a tracker of the snow layer history (Table 2) for which odd values (1, 3, 5) corresponds to the occurrence of depth hoar at any time since the layer creation. $g_{s_i}(d_i, S_i)$ is a variable originally used to describe snow microstructure by Brun et al. (1992) (grain size). Its retrieval from the current state variables d_i and S_i is described in Appendix D. It must be noticed that

this parameterization was forgotten by Carmagnola et al. (2014) because it was unpublished and was only recently restored in the code.

Several prognostic evolutions of d_i during dry metamorphism were implemented by Carmagnola et al. (2014) and Lafayse et al. (2017), following the works from Brun et al. (1992), Flanner and Zender (2006) and Schleef et al. (2014). Furthermore, several issues were found by Baron (2023) in the translation of the Brun et al. (1992) formalism (using dendricity and grain size) in terms of optical diameter evolution by Carmagnola et al. (2014) (details in Appendix D). A new parameterization (B21) was therefore recently implemented to solve the associated issues and now replaces the original implementation of Carmagnola et al. (2014) now removed from the code. The resulting available evolution laws of d_i during dry metamorphism are given by Eq. 46-49.

$$285 \quad \left[\begin{array}{l} \text{If SNOWMETAMO=B21} \\ \text{and } l_i = 0 : \end{array} \right] \left\{ \begin{array}{l} \text{If } d_i \geq 10^{-4}(4 - S_i) : \left\{ \begin{array}{l} \text{If } \mathcal{G}_i > 15 \text{ K m}^{-1} \text{ and } S_i = 0 : \Delta d_i = \frac{1}{2} f(\theta_i) h(\rho_i) g(\mathcal{G}_i) \Phi \Delta t \\ \text{else:} \quad \Delta d_i = \frac{d_i - 4 \times 10^{-4}}{1 + S_i} \Delta S_i \end{array} \right. \\ \text{else :} \quad \Delta d_i = 10^{-4} \left[-\text{sph}_2 e^{-6000/T_i} \mathcal{J}_i (S_i - 3) + \frac{\Delta S_i}{\Delta t} \frac{10^4 d_i - 1}{S_i - 3} \right] \Delta t \\ \text{where } \left\{ \begin{array}{l} \mathcal{J}_i = \mathcal{G}_i^{0.4} \quad \text{if } \mathcal{G}_i \geq 5 \\ \mathcal{J}_i = 1 \quad \text{if } \mathcal{G}_i < 5 \end{array} \right. \end{array} \right. \quad (46)$$

$$\left[\begin{array}{l} \text{If SNOWMETAMO=F06} \\ \text{and } l_i = 0 : \end{array} \right] \Delta d_i = 2\dot{r}_0(\rho_i, T_i, \mathcal{G}_i) \left[\frac{\tau(\rho_i, T_i, \mathcal{G}_i)}{\frac{d_i}{2} - r_0 + \tau(\rho_i, T_i, \mathcal{G}_i)} \right]^{\frac{1}{\kappa(\rho_i, T_i, \mathcal{G}_i)}} \Delta t \quad (47)$$

$$\left[\begin{array}{l} \text{If SNOWMETAMO=S-B} \\ \text{and } l_i = 0 : \end{array} \right] \left\{ \begin{array}{l} \text{If } A_i \leq 2 \text{ days} \quad \Delta d_i = \frac{a_s \rho_i d_i^2}{6} + \frac{b_s T_i \left(\frac{6}{\rho_i} \right)^{m_s - 1}}{d_i^{m_s - 2}} \\ \text{else:} \quad \text{Eq. 46} \end{array} \right. \quad (48)$$

$$\left[\begin{array}{l} \text{If SNOWMETAMO=S-F} \\ \text{and } l_i = 0 : \end{array} \right] \left\{ \begin{array}{l} \text{If } A_i \leq 2 \text{ days} \quad \text{Eq. 48} \\ \text{else:} \quad \text{Eq. 47} \end{array} \right. \quad (49)$$

(50)

290 Functions $f(\theta_i)$, $h(\rho_i)$, $g(\mathcal{G}_i)$ and parameter Φ used in Eq. 46 for the growth of faceted crystals in the case of high gradient metamorphism follow Marbouty (1980) and are defined in Appendix C. In Eq. 47 from Flanner and Zender (2006), coefficients $\dot{r}_0(\rho_i, T_i, \mathcal{G}_i)$, $\tau(\rho_i, T_i, \mathcal{G}_i)$ and $\kappa(\rho_i, T_i, \mathcal{G}_i)$ are retrieved from look-up tables provided in a parameters file (cf. section on Data and Code availability) and $r_o = 5 \times 10^{-5}$ m. Experimental parameters a_s , b_s , m_s in Eq. 49 are defined in Appendix K3 from Schleef et al. (2014).

295 Regardless of the SNOWMETAMO option, wet metamorphism is always parameterized with the laws published by Vionnet et al. (2012), rewritten here with the new microstructure prognostic variables and the methodology described in Appendix D:

$$\text{If } l_i > 0 \left\{ \begin{array}{l} \text{If } d_i < 10^{-4}(4 - S_i) : \left\{ \begin{array}{l} \text{If } S_i < 1 : \Delta d_i = 10^{-4} \left(\frac{10^4 d_i - 1}{S_i - 3} - (S_i - 3) \right) \Delta S_i \\ \text{If } S_i = 1 : \Delta d_i = 2 \cdot 10^{-4} \max \left(\text{sph}_3 \left(100 \frac{l_i}{\rho_i z_i} \right)^3, \text{sph}_2 e^{-6000/T_0} \right) \Delta t \end{array} \right. \\ \text{else :} \left\{ \begin{array}{l} \text{If } S_i < 1 : \Delta d_i = \frac{d_i - 4 \cdot 10^{-4}}{S_i + 1} \Delta S_i \\ \text{If } S_i = 1 : \Delta d_i = \frac{2}{\pi} \frac{\left[v_0 + v_1 \left(100 \frac{l_i}{\rho_i z_i} \right)^3 \right]}{d_i^2} \Delta t \end{array} \right. \end{array} \right. \quad (51)$$

To follow its definition in Table 2, the historical tracker h_i is updated at the end of this subroutine by:

$$\left\{ \begin{array}{l} \text{If } d_i \geq 10^{-4}(4 - S_i) : \\ \quad \left\{ \begin{array}{l} \text{If } S_i = 0 \text{ and } h_i^t = 0 : h_i^{t+\Delta t} = 1 \\ \text{else : } \left\{ \begin{array}{l} \text{If } S_i = 1 \text{ and } \frac{l_i}{\rho_i z_i} > 0.005 : \left\{ \begin{array}{l} \text{If } h_i^t = 0 : h_i^{t+\Delta t} = 2 \\ \text{If } h_i^t = 1 : h_i^{t+\Delta t} = 3 \\ \text{else : } h_i^{t+\Delta t} = h_i^t \end{array} \right. \\ \text{else : } \left\{ \begin{array}{l} \text{If } T_i < T_0 : \left\{ \begin{array}{l} \text{If } h_i^t = 2 : h_i^{t+\Delta t} = 4 \\ \text{If } h_i^t = 3 : h_i^{t+\Delta t} = 5 \\ \text{else : } h_i^{t+\Delta t} = h_i^t \end{array} \right. \\ \text{else : } h_i^{t+\Delta t} = h_i^t \end{array} \right. \end{array} \right. \\ \text{else } h_i^{t+\Delta t} = h_i^t \end{array} \right. \quad (52)$$

300 2.4.6 Natural compaction

For a given layer of density ρ_i the mechanical settling under the over burden σ_i (Pa) is expressed with a visco-elastic model (Anderson, 1976; Navarre, 1975):

$$\text{If } \text{SNOWCOMP} \in [\text{B92}, \text{T11}] : \Delta\rho_i = \frac{\rho_i \sigma_i}{\eta_i} \Delta t \quad (53)$$

where

$$\left\{ \begin{array}{l} \sigma_i = g \cos \Theta \sum_{j=1}^{i-1} \rho_j z_j \forall i \in [2, N] \\ \sigma_1 = g \cos \Theta \times 0.5 \rho_1 z_1 \end{array} \right. \quad (54)$$

g is the gravitational acceleration and Θ the slope angle from horizontal.

The viscosity η_i is a function of density ρ_i and temperature θ_i ($^{\circ}\text{C}$) depending on the SNOWCOMP option (Lafaysse et al., 2017; Teufelsbauer, 2011):

$$\left\{ \begin{array}{l} \text{If } \text{SNOWCOMP} = \text{B92}: \quad \eta_i = f_1(w_i) f_2(d_i, S_i) \eta_0 \frac{\rho_i}{c_\eta} e^{a_\eta(-\theta_i) + b_\eta \rho_i} \\ \text{If } \text{SNOWCOMP} = \text{T11}: \quad \eta_i = f_1(w_i) f_2(d_i, S_i) * 0.05 \rho_i^{-0.0371\theta_i + 4.4} (10^{-4} e^{0.018\rho_i} + 1) \end{array} \right. \quad (55)$$

310 The parameters for case B92 are defined in Appendix K3. The multiplicative function f_1 accelerates the settlement of wet snow as a function of the volumetric liquid water content w_i . The multiplicative function f_2 reduces the settlement of layers consisting of faceted snow types as a function of microstructure properties d_i and S_i (translation of the formula from Vionnet et al. (2012) in the new formalism).

$$f_1(w_i) = \frac{1}{1 + 60 \frac{w_i}{\rho_w}} \quad (56)$$

$$f_2(d_i, S_i) = \begin{cases} \min(4, \exp(\min(4, g_{s_i}(d_i, S_i) \times 10^4 - 2))) & \text{if } d_i > (4 - S_i) \times 10^{-4} \text{ and } S_i \leq 0.5 \\ 1 & \text{otherwise} \end{cases} \quad (57)$$

where $g_{s_i}(d_i, S_i)$ is defined by Eq. D6. The compaction rate however has a complex dependence on snow microstructure (Lehning et al., 2002) which cannot be described by the representation of snow microstructure in Crocus. Alternatively to Eq. 53, it is possible to use a parameterization from Schleef et al. (2014) derived from tomographic observations and representing a non-linear relationship between settlement, the stress σ_i (Pa) and the optical diameter increase for the first 48 hours after snowfall:

$$\text{If SNOWCOMP} = \text{S14:} \begin{cases} \Delta\rho_i = B_S \frac{\Delta d_i}{d_i^2} \sigma_i^{k_S} & \text{if } A_i \leq 2 \text{ days} \\ \text{Eq. 53} & \text{if } A_i > 2 \text{ days} \end{cases} \quad (58)$$

with $B_S = 3.96 \times 10^{-2}$ and $k_S = 0.18$. The current Crocus parameterization is applied when the snow layer age exceeds 2 days.

Alternative parameterizations reducing compaction in the presence of low vegetation were proposed by Woolley et al. (2024) combining earlier works from Domine et al. (2016) and Royer et al. (2021). Although not available in version 3.0.2, they will be implemented in a future version.

2.4.7 Grooming

The effects of grooming machines (snowcats) on the snow physical properties include the compaction induced by their overburden weight and the mixing of surface layers produced by the tiller. Both these effects can optionally be simulated in Crocus (Spandre et al., 2016).

The compaction effect is activated using the logical switch SNOWCOMPACT and only applies if the total mass $M = \sum_{i=1}^N m_i$ is higher than 20 kg m^{-2} (a minimum value required by the grooming machines) and between 8pm and 9pm (and also 6am-9am in case of snowfall during the night). Grooming starts on November 1st and continues until the date day_{END} chosen by the user. Its frequency f_{GRO} (number of grooming sessions per day) is also user-defined. It is worth noticing that it is possible to activate grooming without activating snowmaking, but the opposite would not be realistic. The static stress due to the weight of the snowcat itself σ_{GRO_i} (Pa) is expressed for layer i by:

$$\text{If SNOWCOMPACT} \begin{cases} \text{If } \sum_{j=1}^i m_j < 50 \text{ kg m}^{-2} : \sigma_{\text{GRO}_i} = g \cos \Theta \times 500 \\ \text{If } 50 \text{ kg m}^{-2} \leq \sum_{j=1}^i m_j < 150 \text{ kg m}^{-2} : \sigma_{\text{GRO}_i} = g \cos \Theta \times (150 - \sum_{j=1}^i m_j) * 5 \\ \text{If } \sum_{j=1}^i m_j \geq 150 \text{ kg m}^{-2} : \sigma_{\text{GRO}_i} = 0 \end{cases} \quad (59)$$

and the corresponding density change is obtained by replacing σ_i by σ_{GRO_i} in Eq. 53.

The tilling effect is activated using the logical switch SNOWTILLER, applies down to 35 kg m^{-2} below the surface and only if SNOWCOMPACT = True. The tiller mounted at the rear of snowcats produces two main effects: it further increases the density of the snow by loading the snowpack with extra pressure and it modifies the snow microstructure by creating smaller, rounded grains. As a result, all impacted layers are mixed together, their properties are homogenized and some of them are modified (Spandre et al., 2016). These effects are simulated in Crocus by directly modifying the density, optical diameter and sphericity of the impacted layers. The density reached by the snowpack after grooming is parameterized as:

$$\text{345 If SNOWTILLER: } \rho_i = \max\left(\bar{\rho}, \frac{2\bar{\rho} + 3\rho_{\text{GRO}}}{5}\right) \forall i \in [1, k] \mid \sum_{i=1}^k m_i \leq 35 \text{ kg m}^{-2} \quad (60)$$

where $\bar{\rho} = \frac{\sum_{i=1}^k \rho_i m_i}{\sum_{i=1}^k m_i}$ is the weighted average density of the k impacted layers and ρ_{GRO} is the target density that should eventually be reached by the grooming process (Spandre et al., 2016; Hanzer et al., 2020). The optical diameter and sphericity of snow are altered analogously, using the respective target values d_{GRO} and S_{GRO} (Appendix K3, Spandre et al., 2016; Hanzer et al., 2020).

350 2.4.8 Drifting snow

Even if the Crocus model is not coupled with a dedicated module able to transport snow from one simulation point to another, it is possible to activate a parameterization from Vionnet et al. (2012) simulating the impact of drifting snow on compaction and metamorphism, but with mass conservation. This parameterization relies on two possible definitions of a mobility index MOB_i (Guyomarc'h and Merindol, 1998; Vionnet et al., 2012):

$$\text{355 } \left\{ \begin{array}{l} \text{If SNOWMOB=GM98} \\ \text{If SNOWMOB=VI12} \end{array} \right\} \left\{ \begin{array}{l} \text{If } d_i < 10^{-4}(4 - S_i): \text{ MOB}_i = 0.5(1 - S_i) + 0.75\delta_i \\ \text{else:} \\ \text{If } d_i < 10^{-4}(4 - S_i): \text{ MOB}_i = 0.34 \times (0.5(1 - S_i) + 0.75\delta_i) + 0.66F(\rho_i) \\ \text{else:} \end{array} \right. \text{ MOB}_i = 0.833(1 - S_i) - 0.583g_{s_i} \quad (61)$$

$$\text{where } F(\rho) = [1.25 - 0.0042(\max(\rho_{\min}, \rho) - \rho_{\min})] \text{ and } \rho_{\min} = 50 \text{ kg m}^{-3}. \quad (62)$$

In addition, a threshold is applied on the mobility index in case liquid water had been present at any time in the snow layer:

$$\text{If } h_i \geq 2 : \text{ MOB}_i = \min(-0.0583, \text{MOB}_i \text{ from Eq.61}) \quad (63)$$

The mobility index was expressed with the original formalism of metamorphism. The conversion functions $\delta_i(d_i, S_i)$ and $g_{s_i}(d_i, S_i)$ are defined in Appendix D by Eq. D2 and D6. Redefining this index as a function of the current state variables (d_i

and S_i) would be more consistent and flexible but it would require a significant new effort of evaluation. It highlights the issues involved by changes in the variable states in a model which have been underestimated in the work of Carmagnola et al. (2014).

A driftability index $\mathcal{D}_i$ is then obtained by combining the mobility index and the 5 m wind speed U_5 :

$$\mathcal{D}_i = \max(\text{MOB}_i - (2.868 * \exp(-0.085 \times U_5) - 1.), 0) \quad (64)$$

365 We then introduce:

$$\mathcal{D}_{\text{EFF}_i} = \mathcal{D}_i \times \exp\left(-10 \times \left(\sum_{j=1}^{i-1} z_j (3.25 - \mathcal{D}_j) + \frac{z_i}{2} (3.25 - \mathcal{D}_i)\right)\right) \quad (65)$$

to formulate the variation of density due to snow drift by:

$$\Delta\rho_i = \mathcal{D}_{\text{EFF}_i} \max(\rho_{\text{MAX}} - \rho_i, 0) \frac{\Delta t}{\tau_{\text{DRIFT}}} \quad (66)$$

370 with $\rho_{\text{MAX}} = 350 \text{ kg m}^{-3}$ and $\tau_{\text{DRIFT}} = 172800 \text{ s}$ (2 days). Adjustments of parameters ρ_{MAX} and τ_{DRIFT} were proposed by several authors for Arctic snow as summarized by Woolley et al. (2024). Although hard-coded in version 3.0.2, they will be adjustable by the user in a future version. Then, the variation of microstructure properties due to fragmentation during snow transport are obtained by Eq. 67. The origin of this expression is provided in Appendix E.

$$\begin{cases} \text{If } d_i < 10^{-4}(4 - S_i) : & \Delta d_i = \mathcal{D}_{\text{EFF}_i} \times 10^{-4} [(2.5 - 1.5S_i)\delta_i - 1 + S_i] \frac{\Delta t}{\tau_{\text{DRIFT}}} \\ \text{else} & \Delta d_i = \mathcal{D}_{\text{EFF}_i} \left(-5 \times 10^{-4} \frac{1+S_i}{2} + (d_i - 4 \times 10^{-4}) \frac{1-S_i}{1+S_i} \right) \frac{\Delta t}{\tau_{\text{DRIFT}}} \end{cases} \quad (67)$$

$$375 \quad \Delta S_i = \mathcal{D}_{\text{EFF}_i} (1 - S_i) \frac{\Delta t}{\tau_{\text{DRIFT}}} \quad (68)$$

Optionally, a mass loss due to blowing snow sublimation can be estimated and removed from the surface layer. The parameterization is inspired from Gordon et al. (2006) with a modification of a threshold wind speed U_t to account for the microstructure-related mobility index. This option is not activated by default due to the large associated uncertainties and lack of evaluation but is considered to be necessary in polar environments (Brun et al., 2013; Woolley et al., 2024). The mass
380 reduction of the surface layer due to sublimation Δm_1 is obtained by:

$$\Delta m_1 = \min\left(0.5m_1, a_{\text{SUBL}} \left(\frac{T_0}{T_a}\right)^{\gamma_{\text{SUBL}}} U_t \rho_a q_{\text{sat}}(T_a, P_s) \left(1 - \frac{q_a}{q_{\text{sat}}(T_a, P_s)}\right) \left(\frac{U_5}{U_t}\right)^{b_{\text{SUBL}}} \Delta t\right) \quad (69)$$

$$\text{where } U_t = \frac{-\log(\frac{\text{MOB}_1+1}{c_{\text{SUBL}}})}{d_{\text{SUBL}}} \quad (70)$$

The air density ρ_a (kg m^{-3}) and the saturation specific humidity $q_{\text{sat}}(T_a, P_s)$ (kg kg^{-1}) are computed following Appendix F. a_{SUBL} , b_{SUBL} , γ_{SUBL} , c_{SUBL} , d_{SUBL} are dimensionless parameters defined in Appendix K3

385 2.4.9 Absorption of solar radiation

Two schemes of different complexities are currently implemented and can be activated through the SNOWRAD option. When SNOWRAD=B92, the initial 3-band scheme of Brun et al. (1992) is applied, inspired from Warren (1982). The incoming solar radiation at the interface between layers i and $i + 1$ is defined by:

$$R_i = \sum_{k=1}^3 (1 - \alpha_k) \gamma_k \text{SW}\downarrow \exp \left(- \sum_{j=1}^i \beta_{k_j} z_j \right) \forall i \in [0, N] \quad \text{if SNOWRAD=B92} \quad (71)$$

390 The spectral partitioning of incoming radiation is fixed by parameters γ_k (Appendix K3, with $\sum_{k=1}^3 \gamma_k = 1$).

Spectral albedo values α_k are parameterized by:

$$\alpha_k = \chi \alpha_{k_1} + (1 - \chi) \alpha_{k_2} \forall k \in [1, 3] \quad (72)$$

$$\text{where } \chi = 0.8 \min \left(1, \frac{z_1}{0.02} \right) + 0.2 \min \left[1, \max \left(0, \frac{z_1 - 0.02}{0.01} \right) \right] \quad (73)$$

$$395 \quad \begin{cases} \alpha_{1_i} = \max \left[0.6, \min \left(0.92, 0.96 - 1.58 \sqrt{d_i} \right) - 0.2 \frac{A_i}{\tau_a} \times \min \left(\max \left(0.5, \frac{P_s}{P_{\text{CDP}}} \right), 1.5 \right) \right] \text{ if } \rho_i < \rho_G \\ \alpha_{1_i} = \alpha_{1_G} \text{ if } \rho_i \geq \rho_G \end{cases} \quad \text{for } i \in [1, 2] \quad (74)$$

$$\begin{cases} \alpha_{2_i} = \max \left(0.3, 0.9 - 15.4 \sqrt{d_i} \right) \text{ if } \rho_i < \rho_G \\ \alpha_{2_i} = \alpha_{2_G} \text{ if } \rho_i \geq \rho_G \end{cases} \quad \text{for } i \in [1, 2] \quad (75)$$

$$\begin{cases} \alpha_{3_i} = 346.3 d_i' - 32.31 \sqrt{d_i'} + 0.88 \text{ if } \rho_i < \rho_G \quad \text{where } d_i' = \min(d_i, 0.0023) \\ \alpha_{3_i} = \alpha_{3_G} \text{ if } \rho_i \geq \rho_G \end{cases} \quad \text{for } i \in [1, 2] \quad (76)$$

Note that compared to Vionnet et al. (2012), the consideration of optical diameters of the first two layers, already in the code but not documented, is now made explicit in Eq. 72. The time constant τ_a in Eq. 74 is the main control of the parameterization
 400 reducing snow albedo in the visible band as a function of the age of the layer A_i in order to mimic the effect of Light-Absorbing Particles (LAP). Its default value is set to 60 days with an elevation-dependent multiplicative correction factor (function of P_s) assuming that LAP deposition decreases with elevation. However, it is recommended to adjust this parameter depending on the expected amount of LAP in the target region (Gaillard et al., 2025), to consider calibration against observed albedo time series when possible, or to apply several values of this parameter in multiphysics applications (Lafaysse et al., 2017). The last
 405 modification about absorption of solar radiation consists in applying constant glacier spectral albedo values α_{k_G} on snow-free glacier surfaces. Default values (Appendix K5) are taken from Lejeune (2009) but must be adjusted to each specific glacier (e.g. Réveillet et al., 2018)

Absorption coefficients β_{k_i} (m^{-1}) for band k and layer i are parameterized by:

$$\beta_{1_i} = \max\left(40, 0.00192 \frac{\rho_i}{\sqrt{d_i}}\right) \forall i \in [1, N] \quad (77)$$

$$410 \quad \beta_{2_i} = \max\left(100, 0.01098 \frac{\rho_i}{\sqrt{d_i}}\right) \forall i \in [1, N] \quad (78)$$

$$\beta_{3_1} = +\infty \quad (79)$$

Alternatively to Eq. 71, an option is available for solar radiative transfer calculation in the snowpack (SNOWRAD=T17) combining the TARTES radiative scheme (Two-streAm Radiative TransfER in Snow model, Picard and Libois, 2024) and an explicit modelling of LAP (Tuzet et al., 2017). TARTES is a two-stream radiative transfer scheme based on an analytical
415 formulation of radiative transfer in snow (Kokhanovsky and Zege, 2004). The scheme is applied separately for the direct (DIR) and diffuse (DIF) components of solar radiation. For both components, TARTES computes spectral solar absorption within each layer E_{k_i} (Eq. 59-63 in the comprehensive scientific documentation of TARTES, Picard and Libois, 2024) and the spectral albedo α_k (Eq. 63 in Picard and Libois, 2024). Eq. 80 is used to come back to the profile of R_i used in Crocus:

$$R_i = \sum_{k=1}^{N_k} \left((1 - \alpha_{k \text{ DIR}}) \gamma_{k \text{ DIR}} \text{SW}_{\text{DIR}} \downarrow - \sum_{j=1}^i E_{k_j \text{ DIR}} + (1 - \alpha_{k \text{ DIF}}) \gamma_{k \text{ DIF}} \text{SW}_{\text{DIF}} \downarrow - \sum_{j=1}^i E_{k_j \text{ DIF}} \right) \forall i \in [0, N] \quad \text{if SNOWRAD=T17} \quad (80)$$

420 The default spectral resolution is 20 nm for $N_k = 111$ spectral bands in the interval [300 nm - 2500 nm]. Coefficients $\gamma_{k \text{ DIR}}$ and $\gamma_{k \text{ DIF}}$ to split input direct and diffuse broadband radiation in spectral solar irradiance are currently provided as fixed parameters derived from SBDART (Ricchiazzi et al., 1998) under the conditions encountered at Col de Porte.

To compute E_{k_i} , TARTES accounts for the effect of snow physical properties (SSA and density) and Light-Absorbing Particles using the mass absorption efficiency of each LAP type and its mass content vertical profile. For dust, the mass
425 absorption efficiency is defined following Eq. 83 of Picard and Libois (2024) with parameters $\lambda_0 = 400$ nm, $\text{MAE}(\lambda_0) = 110 \text{ m}^2 \text{kg}^{-1}$ and $\text{AAE} = 4.1$ (values for dust PM2.5 from Libya in Table 4 of Caponi et al., 2017). For black carbon, the mass absorption efficiency is defined following Eq. 82 of Picard and Libois (2024) with a constant density $\rho_{\text{BC}} = 1270 \text{ kg m}^{-3}$ (Flanner et al., 2012) and a constant refractive index ($m_{\text{BC}} = 1.95 - 0.79i$ from Bond and Bergstrom, 2006). The MAE is then scaled with a multiplicative factor $f_{\text{BC}} = 1.638$ to obtain an MAE value at 550 nm of $1.125 \times 10^4 \text{ m}^2 \text{kg}^{-1}$ consistently
430 with measurements of Hadley and Kirchstetter (2012). The scaling makes it possible to implicitly account for the potential absorption enhancement due to internal particle mixing or particle coating. The implementation of new types of LAP would require the implementation of the description of their associated mass absorption efficiency. The vertical profile of LAP mass content is obtained following Section 2.4.10.

2.4.10 Light-Absorbing Particles

435 From Tuzet et al. (2017), the evolution law of the mass $\mathcal{M}_{i,j}$ of LAP j in layer i is expressed as follows:

$$\mathcal{M}_{1,j}^+ = \mathcal{M}_{1,j}^- + \mathcal{W}_{w,j} \Delta t + \frac{\mathcal{W}_{d,j} \Delta t \exp\left(\frac{-z_1}{h}\right)}{\sum_{k=1}^N \exp\left(\frac{-Z_k}{h}\right)} \quad (81)$$

$$\mathcal{M}_{i,j}^+ = \mathcal{M}_{i,j}^- + \frac{\mathcal{W}_{d,j} \Delta t \exp\left(\frac{-Z_i}{h}\right)}{\sum_{k=1}^N \exp\left(\frac{-Z_k}{h}\right)} \forall i \in [2, N] \quad (82)$$

where Z_i represents the depth of layer i from the surface ($Z_i = \sum_{j=1}^i z_j$) and h the e-folding depth characterizing the decrease rate with depth of the impact of the dry deposition flux $\mathcal{W}_{d,j}$. The wet deposition flux $\mathcal{W}_{w,j}$ only affects the uppermost
440 layer.

However, in case of thin layers at the surface, a homogeneous repartition is applied on the uppermost N_{10} layers gathering the first 10 kg m^{-2} of snow. This limits artificial albedo variations due to vertical regridding (Dumont et al., 2020):

$$\mathcal{M}_{i,j}^+ = \frac{m_i}{\sum_{k=1}^{N_{10}} m_k} \times \sum_{k=1}^{N_{10}} \mathcal{M}_{k,j}^+ \forall i \in [1, N_{10}] \text{ where } N_{10} \text{ is the highest integer such that } \sum_{k=1}^{N_{10}-1} m_k < 10 \text{ kg m}^{-2} \quad (83)$$

Note than the wet deposition flux should be consistent with the occurrence of precipitation in the model input data. If not,
445 any positive wet deposition flux without precipitation is not incorporated in the snowpack LAP mass content (Reveillet et al., 2022).

2.4.11 Turbulent fluxes

The sensible and latent turbulent heat fluxes are expressed by:

$$H = \rho_a c_P C_H U_{>1} \left(\frac{T_1}{\Pi_s} - \frac{T_a}{\Pi_a} \right) \quad (84)$$

$$450 \quad LE = \rho_a L_s C_H U_{>1} (q_{sat}(T_1, P_s) - q_a) \quad (85)$$

ρ_a is the air volumetric mass (kg m^{-3}), Π_s and Π_a the Exner functions at the surface and at the level of the atmospheric forcing and $q_{sat}(T_1, P_s)$ the saturation specific humidity at surface temperature T_1 (kg kg^{-1}), cf. Appendix F for their computations. A minimum value of 1 m s^{-1} is applied to wind speed ($U_{>1} = \max(U, 1 \text{ m s}^{-1})$) to maintain minimal fluxes even with very low wind speeds. Note that a simplification has been introduced compared to Vionnet et al. (2012) by considering only surface
455 sublimation and not evaporation of liquid water. The exchange coefficient C_H depends on the stability of the atmosphere through the Richardson Number Ri (Appendix F) following Noilhan and Mahfouf (1996):

$$\begin{cases} C_H = \frac{\kappa_{VK}^2}{\ln\left(\frac{z_u}{z_0}\right) \ln\left(\frac{z_a}{z_{0h}}\right)} \left(1 - \frac{15Ri}{1 + C_h \sqrt{|Ri|}}\right) & \text{if } Ri \leq 0 \\ C_H = \frac{\kappa_{VK}^2}{\ln\left(\frac{z_u}{z_0}\right) \ln\left(\frac{z_a}{z_{0h}}\right)} \times \frac{1}{1 + 15Ri^* \sqrt{1 + 5Ri^*}} & \text{if } Ri > 0 \text{ where } Ri^* = \min(Ri, Ri_l) \end{cases} \quad (86)$$

where κ_{VK} is the Von Karman constant. Coefficient C_h in the unstable case is defined by:

$$C_h = 15 \left(3.2165 + 4.3431 \ln \left(\frac{z_0}{z_{0h}} \right) + 0.5360 \left(\ln \left(\frac{z_0}{z_{0h}} \right) \right)^2 - 0.0781 \left(\ln \left(\frac{z_0}{z_{0h}} \right) \right)^3 \right) \frac{k^2}{\ln \left(\frac{z_u}{z_0} \right) \ln \left(\frac{z_a}{z_{0h}} \right)} \left(\frac{z_a}{z_{0h}} \right)^p \quad (87)$$

$$460 \quad \text{where } p = 0.5802 - 0.1571 \ln \left(\frac{z_0}{z_{0h}} \right) + 0.0327 \left(\ln \left(\frac{z_0}{z_{0h}} \right) \right)^2 - 0.0026 \left(\ln \left(\frac{z_0}{z_{0h}} \right) \right)^3 \quad (88)$$

In the stable case, an adjustable threshold Ri_l is applied on the Richardson number (Martin and Lejeune, 1998). Considering the high uncertainty of these parameterizations of turbulent processes, sensitivity analyses to momentum and thermodynamic roughness lengths z_0 and z_{0h} (m) and to parameter Ri_l are recommended for robust applications of the model (Lafaysse et al., 2017).

465 **2.4.12 Heat diffusion and energy balance**

The formalism of this section is largely inspired by the documentation of the ISBA-ES (Explicit Snow) snowpack scheme from Boone (2002). The model solves the heat diffusion in the stratified snowpack using an implicit time integration scheme:

$$c_I \rho_i z_i \frac{T_i^+ - T_i^-}{\Delta t} + E_i = G_{i-1}^+ - G_i^+ \quad \forall i \in [1, N] \quad (89)$$

where G_i^+ (Wm^{-2}) represents the heat flux between layers i and $i+1 \forall i \in [1, N-1]$ at the end of the time step. G_0^+ and G_N^+ are the heat fluxes at the interfaces with atmosphere and soil at the end of the time step and E_i (Wm^{-2}) the energy of phase change for layer i . The main assumption of the model is that it is possible to separate heat diffusion and phase changes. Thus, the diffusion is solved assuming $E_i = 0 \forall i \in [1, N]$.

The heat flux between two snow layers i and $i+1$ is the sum between the radiative flux R_i and the heat conduction K_i^+ (Wm^{-2}) between these layers:

$$475 \quad G_i^+ = K_i^+ + R_i \quad \forall i \in [1, N-1] \quad (90)$$

The conduction flux K_i is expressed at the end of the time step by:

$$K_i^+ = 2 \overline{\lambda}_i \frac{T_i^+ - T_{i+1}^+}{z_i + z_{i+1}} \quad \forall i \in [1, N-1] \quad (91)$$

where $\overline{\lambda}_i$ is the harmonic weighted mean of the thermal conductivities of layers i and $i+1$:

$$\overline{\lambda}_i = \frac{z_i + z_{i+1}}{\frac{z_i}{\lambda_i} + \frac{z_{i+1}}{\lambda_{i+1}}} \quad (92)$$

480 Eq. 92 replaces the arithmetic mean used in previous versions of Crocus (Lafaysse et al., 2025). Although there is not a clear agreement in the literature that harmonic means outperform the modelling of heat diffusion (Kadioglu et al., 2008), this solution is more consistent with the other components of SURFEX and more commonly used today in snow models (Fourteau et al., 2024).

The thermal conductivity λ_i of layer i is parameterized as a function of density ρ_i following parameterizations of Yen (1981),
 485 Calonne et al. (2011) or Boone and Etchevers (2001):

$$\begin{cases} \text{If SNOWCOND=Y81:} & \lambda_i = \max \left[a_\lambda \left(\frac{\rho_i}{\rho_w} \right)^{1.88}; \lambda_{\min} \right] \\ \text{If SNOWCOND=C11:} & \lambda_i = b_\lambda \rho_i^2 + c_\lambda \rho_i + d_\lambda \\ \text{If SNOWCOND=I02:} & \lambda_i = e_\lambda + f_\lambda \rho_i^2 + \left(g_\lambda + \frac{h_\lambda}{T_i^- + i_\lambda} \right) \frac{P_0}{P} \end{cases} \quad (93)$$

All empirical parameters are provided in Appendix K3. Alternatives to Eq. 93 were proposed by Woolley et al. (2024) for Arctic snow. Although not available in version 3.0.2, they will be implemented in a future version.

The heat flux between the atmosphere and the surface is the sum of all energy fluxes at the surface:

$$490 \quad G_0 = R_0 + \epsilon(\text{LW}\downarrow - \sigma T_1^4) - H - LE + \mathcal{P}_r \Delta t \times c_W(T_a - T_0) + E_{\text{FRZ}} \quad (94)$$

All fluxes in Eq. 94 are expressed at time $t + \Delta t$ with the following approximation:

$$F^+ = F^- + \frac{\partial F}{\partial T_1}(T_1^+ - T_1^-) \quad (95)$$

Thus,

$$\begin{aligned} G_0^+ = & R_0 + \epsilon(\text{LW}\downarrow - \sigma(T_1^-)^3(4T_1^+ - 3T_1^-)) - \rho_a c_P C_H U_{>1} \left(\frac{T_1^+}{\Pi_s} - \frac{T_a}{\Pi_a} \right) \\ & - \rho_a L_s C_H U_{>1} \left(q_{\text{sat}}(T_1^-, P_s) - q_a + \frac{\partial q_{\text{sat}}}{\partial T_1}(T_1^+ - T_1^-) \right) + \mathcal{P}_r \Delta t \times c_W(T_a - T_0) + E_{\text{FRZ}} \end{aligned} \quad (96)$$

495 The computation of $\frac{\partial q_{\text{sat}}}{\partial T_1}$ is detailed in Appendix F. The heat flux between the bottom layer and the ground G_N^+ is expressed with a semi-implicit coupling (i.e. considering the ground surface temperature $T_{G_1}^-$ at time step t) in order to solve separately the thermal diffusion in the soil, outside the snowpack model:

$$G_N^+ = 2\overline{\lambda_N} \frac{T_N^+ - T_{G_1}^-}{z_N + z_{G_1}} + R_N \quad (97)$$

500 where $\overline{\lambda_N}$ is the harmonic mean between the thermal conductivity of the bottom snow layer λ_N and the thermal conductivity of the first soil layer λ_{G_1} :

$$\overline{\lambda_N} = \frac{z_N + z_{G_1}}{\frac{z_N}{\lambda_N} + \frac{z_{G_1}}{\lambda_{G_1}}} \quad (98)$$

Combining and rearranging Eq. 89-91, 96 and 97 the system to solve becomes:

$$\begin{cases} \left(\left(\frac{c_I \rho_1 z_1}{\Delta t} + \frac{2\overline{\lambda_1}}{z_1 + z_2} + 4\epsilon\sigma(T_1^-)^3 + \rho_a C_H U_{>1} \left(\frac{c_P}{\Pi_s} + L_s \frac{\partial q_{\text{sat}}}{\partial T_1} \right) \right) T_1^+ - \frac{2\overline{\lambda_1}}{z_1 + z_2} T_2^+ = \right. \\ \left. \frac{c_I \rho_1 z_1}{\Delta t} T_1^- + R_0 - R_1 + \epsilon(\text{LW}\downarrow + 3\sigma(T_1^-)^4) + \rho_a C_H U_{>1} \left(c_P \frac{T_a}{\Pi_a} + L_s \left(q_a - q_{\text{sat}}(T_1^-, P_s) + \frac{\partial q_{\text{sat}}}{\partial T_1} T_1^- \right) \right) \right. \\ \left. + \mathcal{P}_r \Delta t \times c_W(T_a - T_0) + E_{\text{FRZ}} \right. \\ \left. - \frac{2\overline{\lambda_{i-1}}}{z_{i-1} + z_i} T_{i-1}^+ + \left(\frac{c_I \rho_i z_i}{\Delta t} + \frac{2\overline{\lambda_i}}{z_i + z_{i+1}} + \frac{2\overline{\lambda_{i-1}}}{z_{i-1} + z_i} \right) T_i^+ - \frac{2\overline{\lambda_i}}{z_i + z_{i+1}} T_{i+1}^+ = \frac{c_I \rho_i z_i}{\Delta t} T_i^- + R_{i-1} - R_i \forall i \in [2, N-1] \right. \\ \left. - \frac{2\overline{\lambda_{N-1}}}{z_{N-1} + z_N} T_{N-1}^+ + \left(\frac{c_I \rho_N z_N}{\Delta t} + \frac{2\overline{\lambda_N}}{z_N + z_{G_1}} + \frac{2\overline{\lambda_{N-1}}}{z_{N-1} + z_N} \right) T_N^+ = \frac{2\overline{\lambda_N}}{z_N + z_{G_1}} T_{G_1}^- + \frac{c_I \rho_N z_N}{\Delta t} T_N^- + R_{N-1} - R_N \right. \end{cases} \quad (99)$$

The first line of Eq. 99 is rewritten in the form:

$$505 \quad \frac{1}{C_T \Delta t} T_1^+ - \frac{\zeta_2}{C_T \Delta t} T_2^+ = \frac{\zeta_1}{C_T \Delta t} \quad (100)$$

$$\text{where } C_T = \frac{1}{c_I \rho_1 z_1} \quad (101)$$

$$\zeta_2 = \frac{2C_T \bar{\lambda}_1}{\mathcal{A}(z_1 + z_2)} \quad (102)$$

$$\mathcal{A} = \frac{1}{\Delta t} + C_T \left[\frac{2\bar{\lambda}_1}{z_1 + z_2} + 4\epsilon\sigma(T_1^-)^3 + \rho_a C_H U_{>1} \left(\frac{c_P}{\Pi_s} + L_s \frac{\partial q_{sat}}{\partial T_1} \right) \right] \quad (103)$$

$$\zeta_1 = \frac{\mathcal{B}T_1^- + \mathcal{C}}{\mathcal{A}} \quad (104)$$

$$510 \quad \mathcal{B} = \frac{1}{\Delta t} + C_T \left[3\epsilon\sigma(T_1^-)^3 + \rho_a C_H U_{>1} \frac{\partial q_{sat}}{\partial T_1} \right] \quad (105)$$

$$\mathcal{C} = C_T \left[R_0 - R_1 + \epsilon \text{LW}\downarrow + \rho_a C_H U_{>1} \left(c_P \frac{T_a}{\Pi_a} + L_s (q_a - q_{sat}(T_1^-, P_s)) \right) + \mathcal{P}_r \Delta t \times c_W (T_a - T_0) + E_{\text{FRZ}} \right] \quad (106)$$

Therefore, the temperature profile at time $t + \Delta t$ is obtained by:

$$\begin{bmatrix} T_1^+ \\ T_2^+ \\ \dots \\ T_i^+ \\ \dots \\ \dots \\ T_N^+ \end{bmatrix} = \begin{bmatrix} B_1 & C_1 & 0 & 0 & \dots & \dots & 0 \\ A_2 & B_2 & C_2 & 0 & \dots & \dots & 0 \\ 0 & A_3 & \dots & \dots & \dots & \dots & \dots \\ 0 & 0 & \dots & B_i & C_i & \dots & 0 \\ \dots & \dots & \dots & A_i & \dots & \dots & 0 \\ \dots & \dots & \dots & \dots & \dots & \dots & C_{N-1} \\ 0 & 0 & \dots & 0 & 0 & A_N & B_N \end{bmatrix}^{-1} \begin{bmatrix} Y_1 \\ Y_2 \\ \dots \\ Y_i \\ \dots \\ \dots \\ Y_N \end{bmatrix} \quad (107)$$

where vectors $A = (A_2, \dots, A_i, \dots, A_N)$, $B = (B_1, \dots, B_i, \dots, B_N)$, $C = (C_1, \dots, C_i, \dots, C_{N-1})$, $Y = (Y_1, \dots, Y_i, \dots, Y_N)$ are defined by:

$$\begin{cases} A_i = -\frac{2\overline{\lambda_{i-1}}}{z_{i-1} + z_i} \forall i \in [2, N] \\ B_1 = \frac{1}{C_T \Delta t} \\ B_i = \left(\frac{c_I \rho_i z_i}{\Delta t} + \frac{2\overline{\lambda_i}}{z_i + z_{i+1}} + \frac{2\overline{\lambda_{i-1}}}{z_{i-1} + z_i} \right) \forall i \in [2, N-1] \\ B_N = \left(\frac{c_I \rho_N z_N}{\Delta t} + \frac{2\overline{\lambda_N}}{z_N + z_{G_1}} + \frac{2\overline{\lambda_{N-1}}}{z_{N-1} + z_N} \right) \\ C_1 = -\frac{\zeta_2}{C_T \Delta t} \\ C_i = -\frac{2\overline{\lambda_i}}{z_i + z_{i+1}} \forall i \in [2, N-1] \\ Y_1 = \frac{\zeta_1}{C_T \Delta t} \\ Y_i = \frac{c_I \rho_i z_i}{\Delta t} T_i^- + R_{i-1} - R_i \forall i \in [2, N-1] \\ Y_N = \frac{2\overline{\lambda_N}}{z_N + z_{G_1}} T_{G_1}^- + \frac{c_I \rho_N z_N}{\Delta t} T_N^- + R_{N-1} - R_N \end{cases} \quad (108)$$

2.4.13 Adjustments in case of surface melting

The possibility for T_1^+ to exceed the freezing point in the solving of Eq. 107 can lead to overestimate the surface energy fluxes that depend on T_1^+ and to overestimate the heat conduction K_1 below surface. To avoid this numerical artefact, Crocus distinguishes the case of first melting ($T_1^- < T_0$ and $T_1^+ > T_0$), and ongoing melting ($T_1^- \geq T_0$ and $T_1^+ > T_0$).

In the case of a first melting ($T_1^- < T_0$ and $T_1^+ > T_0$), the temperature profile for layers $i \in [2, N]$ is not updated, so only the surface fluxes are adjusted replacing T_1^+ by T_0 in Eq. 84, 85, 96. The new temporary surface temperature (before melting) is obtained by converting the difference in both consecutive estimates of the surface energy flux G_0 in terms of temperature change:

$$\text{525 If } T_1^- < T_0 \text{ and } T_1^+ > T_0 : \begin{cases} G_0^+ = R_0 + \epsilon(LW\downarrow - \sigma(T_1^-)^3(4T_0 - 3T_1^-)) - \rho_a c_P C_H U_{>1}(T_0 - T_a) \\ \quad - \rho_a L_s C_H U_{>1} \left(q_{sat}(T_1^-, P_s) - q_a + \frac{\partial q_{sat}}{\partial T_0}(T_0 - T_1^-) \right) + \mathcal{P}_r \Delta t \times c_W(T_a - T_0) \\ T_1^+ = T_1^{\text{first}} + \frac{\Delta t}{c_I \rho_i z_i} (G_0^+ - G_0^{\text{first}}) \end{cases} \quad (109)$$

where T_1^{first} is the solution of Eq. 107, and G_0^{first} is the flux obtained applying Eq. 96 with T_1^{first} . This ensures that the energy budget over the snowpack is closed.

In the case of an ongoing melting (i.e. the solution of Eq. 107 provides a temperature above freezing point for the surface layer at two consecutive time steps: $T_1^- \geq T_0$ and $T_1^+ > T_0$), the system is solved a second time for layers $i \in [2, N]$ by

530 constraining $T_1^+ = T_0$:

$$\begin{bmatrix} T_2^+ \\ \dots \\ T_i^+ \\ \dots \\ T_N^+ \end{bmatrix} = \begin{bmatrix} B_2 & C_2 & 0 & \dots & \dots & 0 \\ A_3 & \dots & \dots & \dots & \dots & \dots \\ 0 & \dots & B_i & C_i & \dots & 0 \\ \dots & \dots & A_i & \dots & \dots & 0 \\ \dots & \dots & \dots & \dots & \dots & C_{N-1} \\ 0 & \dots & 0 & 0 & A_N & B_N \end{bmatrix}^{-1} \begin{bmatrix} Y_2 + \frac{2\bar{\lambda}_1}{z_1+z_2} T_0 \\ \dots \\ Y_i \\ \dots \\ Y_N \end{bmatrix} \quad (110)$$

Then, the surface energy fluxes are updated replacing T_1^+ and T_1^- by T_0 in Eq. 84, 85, 96 and the conduction flux between the two first layers is updated with the solution of Eq. 110. A new estimate of the surface layer T_1^+ is temporarily obtained from Eq. 89 ($i = 1$) consistently with these updated fluxes, before the transfer of exceeding energy in phase change (E_1 , see
535 Section 2.4.16):

$$\text{If } T_1^- \geq T_0 \text{ and } T_1^+ > T_0 : \begin{cases} G_0^+ = R_0 + \epsilon(\text{LW}\downarrow - \sigma T_0^4) - \rho_a c_P C_H U_{>1} (T_0 - T_a) \\ \quad - \rho_a L_s C_H U_{>1} (q_{sat}(T_0, P_s) - q_a) + \mathcal{P}_r \Delta t \times c_W (T_a - T_0) \\ K_1^+ = \frac{2\bar{\lambda}_i}{z_i + z_{i+1}} \frac{T_0 - T_2^+}{\Delta t} \\ T_1^+ = T_0 + \frac{\Delta t}{c_I \rho_i z_i} (G_0^+ - K_1^+ - R_1) \end{cases} \quad (111)$$

This also guarantees the closure of the energy budget in that case. Note that Fourteau et al. (2024) recently proposed alternative model formulations to compute a more stable surface energy balance with a better coupling between surface melting and heat transfers. This should be explored in the future to avoid the need of such numerical adjustments.

540 2.4.14 Coupling with MEB

MEB (Multiple Energy Balance, Boone et al., 2017) is a variant of the ISBA land surface scheme in which the soil-vegetation system is no longer described by a composite approach but by an explicit representation of vegetation with a big-leaf approach. This allows representation of the main physical processes involved in forest-snow interactions including snowfall interception and radiative impacts of the trees. An extensive description of this implementation is beyond the scope of this paper but
545 available in Boone et al. (2017). However, as coupled processes require a coupled solving of snow surface and vegetation temperatures T_1 and T_v , the solving of heat diffusion is modified when Crocus is coupled to the MEB scheme. In that case, the values of the surface energy fluxes are no longer obtained through the implicit solving of Eq. 99-107 but are imposed as a boundary condition to conserve energy. Eq. 89 is modified for the surface layer to maintain the fluxes obtained from MEB:

$$c_I \rho_i z_i \frac{T_1^+ - T_1^-}{\Delta t} + E_1 = G_{0\text{MEB}} - R_1 - K_1^+ \quad (112)$$

$$\text{550 where } G_{0\text{MEB}} = R_0 + \epsilon(\text{LW}\downarrow - \sigma T_{1\text{MEB}}^4) - H_{\text{MEB}} - LE_{\text{MEB}} + \mathcal{P}_r \Delta t \times c_W (T_a - T_0) \quad (113)$$

$G_{0_{\text{MEB}}}$ represents the total surface energy flux in agreement with the first estimate of surface temperature from MEB $T_{1_{\text{MEB}}}$ and the associated turbulent fluxes H_{MEB} and LE_{MEB} . $LW\downarrow$ accounts for vegetation radiation and is therefore linked to the solution obtained for vegetation temperature $T_{v_{\text{MEB}}}$. It must be noted that as R_0 and R_1 are already needed in MEB, they are computed with the same routine as described in Section 2.4.9 but earlier in the time step (before the MEB solving) to guarantee identical values at both steps (MEB and Crocus), and accounting for shading by trees in $SW\downarrow$.

Consistently with Eq. 112, the first line of Eq. 99 is replaced by:

$$\left(\frac{c_I \rho_1 z_1}{\Delta t} + \frac{2\overline{\lambda_1}}{z_1 + z_2} \right) T_1^+ - \frac{2\overline{\lambda_1}}{z_1 + z_2} T_2^+ = \frac{c_I \rho_1 z_1}{\Delta t} T_1^- + G_{0_{\text{MEB}}} - R_1 \quad (114)$$

Rewriting Eq. 114 with the same form as Eq. 100 is equivalent to replacing Eq.103, 105, 106 by Eq. 115, 116, 117 and solving the linear system of Eq. 107 with coefficients C_1 and Y_1 of Eq. 108 modified according to the new values of ζ_2 and ζ_1 from Eq. 102 and Eq. 104.

$$\mathcal{A} = \frac{1}{\Delta t} + C_T \left[\frac{2\overline{\lambda_1}}{z_1 + z_2} \right] \quad (115)$$

$$\mathcal{B} = \frac{1}{\Delta t} \quad (116)$$

$$\mathcal{C} = C_T [G_{0_{\text{MEB}}} - R_1] \quad (117)$$

The adjustments of Section 2.4.13 are no longer required as G_0 is imposed by MEB and phase change was already accounted for to compute this flux.

The validity of Eq. 114 would require that no modification of the state variables of the snowpack has occurred between the computation of $G_{0_{\text{MEB}}}$ and the solving of Eq. 107 because $G_{0_{\text{MEB}}}$ depends on snow properties through Eq. 48 and 49 in Boone et al. (2017) and the associated Appendix I4. In practice, the SURFEX code structure makes this constraint especially challenging. The violation of this assumption can generate numerical instabilities especially with thin surface layers due to the violation of the second principle of thermodynamics (Fourteau et al., 2026). To reduce as much as possible the occurrence of this problem, the sequence of routines is modified following Figure 1. However, there is currently no solution to avoid modifications due to snow interception by vegetation because this term cannot be computed before solving MEB (the mass balance depends on latent heat terms known only after the solving). Numerical instabilities are therefore still possible and further investigations are in progress to safely allow large scale applications of MEB-Crocus. This issue is more challenging than in the case of the coupling of MEB with ES snow scheme (Boone et al., 2017; Napoly et al., 2020) which has already been successfully applied in large scale simulations. This is probably due to the possible occurrence of thinner surface snow layers with Crocus.

2.4.15 Total melting or sublimation

The snowpack is assumed to totally disappear when

$$G_0^+ - G_N^+ \geq \frac{-\sum_{i=1}^{N^t} H_i^+ + H_{\text{subl}}}{\Delta t} \text{ or } \frac{\max(0, LE^+) \Delta t}{L_s} \geq \sum_{i=1}^{N^t} m_i \quad (118)$$

The first condition corresponds to a total melt of the snowpack (energy gain during the time step exceeds available internal energy for melting). It requires to remove the enthalpy of surface snow potentially sublimated H_{subl} from the total enthalpy. The second condition corresponds to a total sublimation of the snowpack, which is a very unusual case of snow disappearance but can appear especially when a snow transport module provide a very low amount of snow on bare ground in cold and windy conditions.

In both cases, for mass conservation, the runoff at the bottom of the snowpack is set to the total snow mass and the energy associated with LE^+ is transmitted to the soil scheme as a correction term. If Eq. 118 is not verified, the procedure follows Sect. 2.4.16 to Sect. 2.4.20.

2.4.16 Melting

Let's define the mass of solid and liquid fractions of the snow before any phase change s_i^- and l_i^- (kg m^{-2}):

$$s_i^- = m_i - l_i^- \quad (119)$$

When the heat diffusion solving provides a temperature T_i^+ above the melting point T_0 for layer i , the model simulates melting. The energy available for fusion E_{f_i} (J m^{-2}) on layer i can be constrained either by the available heating energy or by the available mass of the solid fraction of snow before melting s_i^- . Thus, the energy and mass f_i (kg m^{-2}) of melting during the time step are computed by:

$$E_{f_i} = \min(c_I \rho_i (T_i^+ - T_0), L_m s_i^-) \quad (120)$$

$$f_i = \frac{E_{f_i}}{L_m} \quad (121)$$

The mass of solid and liquid fractions after melting are:

$$s_i^+ = s_i^- - f_i \quad (122)$$

$$l_i^+ = l_i^- + f_i \quad (123)$$

The corresponding updates of depth and total density can be expressed by:

$$z_i^+ = z_i^- \times \frac{m_i - l_i^+}{m_i - l_i^-} \quad (124)$$

$$\rho_i^+ = \frac{m_i}{z_i^+} \quad (125)$$

In case of melting, the melting point temperature is attributed to the layer temperature:

$$T_i^{++} = \min(T_0, T_i^+) \quad (126)$$

In practice, a first evaluation of Eq.120-121 is computed for all layers to identify cases where a numerical layer fully melts out ($c_I \rho_i (T_i^+ - T_0) \geq L_m s_i^-$). In such a case, the numerical layer i is aggregated with the numerical layer $i+1$ for $i \in [1, N-1]$,

following Equations 12-20. If the bottom layer N is concerned, it is aggregated with the above layer $N - 1$. Several iterations can be done in case of melting of multiple consecutive layers. Then, the melting is computed again with this updated discretization
610 with the guarantee that all numerical layers remain defined.

2.4.17 Refreezing

When the heat diffusion solving provides a temperature T_i^+ below the melting point T_0 whereas liquid water is present, the model simulates refreezing. The energy available for refreezing E_{r_i} (J m⁻²) can be constrained either by the layer cooling after diffusion or by the maximum available liquid water content before refreezing l_i^- . Thus, the energy and mass r_i (kg m⁻²)
615 of refreezing during the time step are computed by:

$$E_{r_i} = \min(c_I \rho_i (T_0 - T_i^+), L_m l_i^-) \quad (127)$$

$$r_i = \frac{E_{r_i}}{L_m} \quad (128)$$

The mass of solid and liquid fractions after refreezing are:

$$s_i^+ = s_i^- + r_i \quad (129)$$

$$620 \quad l_i^+ = l_i^- - r_i \quad (130)$$

The energy conservation during the refreezing process is expressed by:

$$c_I \rho_i (T_i^+ - T_i^{++}) s_i^+ + E_{r_i} + c_I \rho_i (T_0 - T_i^+) r_i = 0 \quad (131)$$

where T_i^+ and T_i^{++} (K) are the layer temperature of the solid fraction before and after refreezing. In Eq. 131, the first term corresponds to the heating of the solid fraction after refreezing, the second term to the latent heat release due to refreezing and
625 the third term to the cooling of the refrozen part necessary for the thermal equilibrium of the solid phase.

By combining Eq. 131 and 130, the evolution of the layer temperature due to refreezing is computed by:

$$T_i^{++} = T_0 + (T_i^+ - T_0) \frac{s_i^-}{s_i^+} + \frac{E_{r_i}}{c_I \rho_i s_i^+} \quad (132)$$

Equations 127-132 are not applied independently but jointly with liquid water percolation as described in Section 2.4.18 within Algorithm 1

630 2.4.18 Liquid water percolation

Let's define the volumetric liquid water content w_i (kg m⁻³):

$$w_i = \frac{l_i}{z_i} \quad (133)$$

and the snow porosity:

$$\phi_i = 1 - \frac{\rho_i^- - w_i}{\rho_I} \quad (134)$$

635 where ρ_I is the volumetric mass of pure ice. The liquid water flow $\mathcal{F}_i$ (kg m^{-2}) between layers i and $i + 1$ is computed by a simple and conceptual bucket approach where the layers are seen as superposed water reservoirs with a maximum liquid water holding capacity $w_{i \text{ max}}$. The excess water drains to the underlying layer when w_i exceeds $w_{i \text{ max}}$ following Algorithm 1. Snow layer densities ρ_i are updated with the resulting net mass flux $\mathcal{F}_i - \mathcal{F}_{i-1}$. However, in the limit case of ice layers ($\rho = \rho_I$) and refreezing ($r_i > 0$), the excess liquid water mass increases the ice layer depth at constant density. Note that another choice
640 would be possible (Fourteau et al., 2024) by considering ice layers impermeable (i.e. computing $\mathcal{F}_i$ before any refreezing and r_i after percolation) with potential impacts on glaciers simulations.

Algorithm 1 Buckets algorithm for liquid water percolation

```

 $\mathcal{F}_0 = \mathcal{P}_r \Delta t$ 
for  $i \in [1, N]$  do
  Compute  $r_i, s_i, w_i$  with Eq. 127-133
   $w_i^* = w_i + \frac{\mathcal{F}_{i-1} + f_i - r_i}{z_i}$ 
   $\mathcal{F}_i = \max(0, w_i^* - w_{i \text{ max}}) z_i$ 
   $w_i = w_i^* - \frac{\mathcal{F}_i}{z_i}$ 
   $\rho_i^+ = \rho_i^- (\mathcal{F}_i - \mathcal{F}_{i-1}) \frac{\rho_w}{z_i}$ 
  if  $\rho_i^+ > \rho_I$  then
     $z_i = \frac{\rho_i^+}{\rho_I} z_i$ 
     $\rho_i^+ = \rho_I$ 
  end if
end for

```

Several formulations of $w_{i \text{ max}}$ were implemented by Lafaysse et al. (2017):

$$\left\{ \begin{array}{ll} \text{If SNOWLIQ} = \text{B92:} & w_{i \text{ max}} = 0.05 \rho_w \phi_i \\ \text{If SNOWLIQ} = \text{SPK:} & \begin{cases} w_{i \text{ max}} = \rho_w (0.08 - 0.1023(0.97 - \phi_i)) & \text{if } \phi_i \geq 0.77 \\ w_{i \text{ max}} = \rho_w \left(0.0264 + 0.0099 \frac{\phi_i}{1 - \phi_i} \right) & \text{otherwise} \end{cases} \\ \text{If SNOWLIQ} = \text{B02:} & w_{i \text{ max}} = \rho_i \left(r_{\min} + (r_{\max} - r_{\min}) \max \left(0, \frac{\rho_r - \rho_i}{\rho_r} \right) \right) \end{array} \right. \quad (135)$$

Parameters $r_{\min}, r_{\max}, \rho_r$ are defined in Appendix K3.

645 The resolution of Richards equations might help improve the realism of this process in a detailed snowpack model (Wever et al., 2014, 2015, 2016a, b, 2017). However, the developments of D’Amboise et al. (2017) are not sufficiently robust to be available in this official release. More stable and numerically efficient alternatives are emerging and might be preferred in the future following the recommendations of Fourteau et al. (2025).

2.4.19 Scavenging of LAP

650 When LAP are activated (Section 2.4.10), liquid water percolation may carry a fraction of LAP mass (Tuzet et al., 2017):

$$\mathcal{M}_{i,j}^+ = \mathcal{M}_{i,j}^- - \mathcal{F}_i \times C_{\text{scav},j} \times \frac{\mathcal{M}_{i,j}^-}{m_i} \quad (136)$$

The scavenging coefficient $C_{\text{scav},j}$ can be adjusted by the user for each LAP j (default values are set to $C_{\text{scav},j} = 0$ i.e. no scavenging).

2.4.20 Sublimation and deposition

655 Sublimation and deposition are accounted for by adding or removing mass to the surface layer accordingly with the surface latent heat flux (Eq. 85 where T_1 is the solution of Eq. 107, 109 or 111 depending on the occurrence of melting). The corresponding evolution of the surface layer properties is described by Eq. 137-138.

$$z_1^+ = \max\left(z_1 + LE \frac{\Delta t}{L_s(\rho_1^- - \frac{l_1}{z_1^-})}, 0\right) \quad (137)$$

$$\rho_1^+ = \rho_1^- + \frac{l_1}{z_1^+} \quad (138)$$

660 Microstructure properties are not modified. Therefore, in case of deposition, the current Crocus snow model only increases the mass of the surface snow layer but it does not allow the formation of a dedicated layer with microstructure properties typical of surface hoar. As a result, it is neither possible to track the burying of surface hoar in the snowpack. In the very unusual cases when the mass of the surface layer is insufficient for sublimation ($-LE \frac{\Delta t}{L_s} > z_i(\rho_i^- - \frac{l_i}{z_i^-})$ which only occurs for extremely thin snowpacks), the quantity $-LE \frac{\Delta t}{L_s} - z_i(\rho_i^- - \frac{l_i}{z_i^-})$ is later extracted from the first soil layer in the ISBA-DIF soil scheme to
 665 conserve energy, and the remaining liquid water, if any, is transferred to the next layer. A homogeneous regridding is applied before the next time step.

2.4.21 Unloading from vegetation

In case of unloading from vegetation, the initial implementation of MEB consisted in adding the unloaded mass to the mass of solid precipitation m_{SP} , following Eq. 36 and 37 for snow density and microstructure. This could lead to unrealistic surface
 670 density when unloading occurred in cold conditions. A recent new parameterization instead attributes a fixed density ρ_{UN} and microstructure properties d_{UN} and S_{UN} to unloaded snow. The associated snow mass is either aggregated to the surface snow layer following Eq. 12-20 or associated to a new snow layer depending on the properties of the surface snow layer.

3 Diagnoses

This section describes the complementary diagnoses of a Crocus simulation provided in addition to the state variables of the
 675 model. These diagnoses can be useful for model evaluation or interpretation in research or operational applications.

3.1 Diagnoses of recent, wet or refrozen snow

We define n_X as the number of snow layers more recent than X days, i.e. satisfying the following condition:

$$A_i < X \quad \forall i \in [1, n_X] \quad (139)$$

Thus, thickness Z_X and mass M_X of snow more recent than X days are defined by:

$$Z_X = \sum_{i=1}^{n_X} z_i \quad (140)$$

$$M_X = \sum_{i=1}^{n_X} m_i \quad (141)$$

These diagnoses are provided for $X \in [0.5, 1, 3, 5, 7]$. Similarly, the number of wet and refrozen snow layers from the surface n_w and n_r are defined by:

$$l_i > 0 \quad \forall i \in [1, n_w] \quad (142)$$

$$l_i < 0 \quad \forall i \in [1, n_r] \quad (143)$$

The thickness of wet and refrozen snow Z_w and Z_r are diagnosed by:

$$Z_w = \sum_{i=1}^{n_w} z_i \quad (144)$$

$$Z_r = \sum_{i=1}^{n_r} z_i \quad (145)$$

3.2 Grain type classification

For each snow layer, a diagnosis of grain type Ψ_i is derived from values of optical diameter and sphericity through the following classification (Eq. 146) in which $\delta_i(d_i, S_i)$ and $g_{s_i}(d_i, S_i)$ are defined respectively by Eq. D2 and D6. The values taken by Ψ_i are taken from the International Snow Classification (Fierz et al., 2009) and include PP (Precipitation Particles), DF (Decomposited Fragments), RG (Rounded Grains), FC (Faceted Crystals), DH (Depth Hoars), MF (Melt Forms) and combinations of these types.

$$\begin{aligned}
& \left\{ \begin{array}{l} \text{If } d_i < 10^{-4}(4 - S_i) \\ \text{else} \end{array} \right. \left\{ \begin{array}{l} \text{If } \delta_i \in [0; 0.3[\quad \left\{ \begin{array}{l} \text{If } S_i < 0.55 \quad \Psi_i = \text{DF+FC} \\ \text{else} \quad \Psi_i = \text{DF+RG} \end{array} \right. \\ \text{If } \delta_i \in [0.3; 0.6[\quad \Psi_i = \text{DF} \\ \text{If } \delta_i \in [0.6; 0.8[\quad \Psi_i = \text{PP+DF} \\ \text{If } \delta_i \in [0.8; 1.0] \quad \Psi_i = \text{PP} \\ \text{If } h_i = 0 \quad \left\{ \begin{array}{l} \text{If } S_i \in [0; 0.2[\quad \Psi_i = \text{FC} \\ \text{If } S_i \in [0.2; 0.8[\quad \Psi_i = \text{RG+FC} \\ \text{If } S_i \in [0.8; 1.0] \quad \Psi_i = \text{RG} \end{array} \right. \\ \text{If } h_i = 1 \quad \left\{ \begin{array}{l} \text{If } g_{s_i} \in [0, 0.55[\quad \left\{ \begin{array}{l} \text{If } S_i \in [0; 0.2[\quad \Psi_i = \text{FC} \\ \text{If } S_i \in [0.2; 0.8[\quad \Psi_i = \text{RG+FC} \\ \text{If } S_i \in [0.8; 1.0] \quad \Psi_i = \text{RG} \end{array} \right. \\ \text{If } g_{s_i} \in [0.55, 1.05[\quad \left\{ \begin{array}{l} \text{If } S_i < 0.55 \quad \Psi_i = \text{FC+DH} \\ \text{else} \quad \Psi_i = \text{MF+DH} \end{array} \right. \\ \text{If } g_{s_i} \geq 1.05 \quad \left\{ \begin{array}{l} \text{If } S_i < 0.55 \quad \Psi_i = \text{DH} \\ \text{else} \quad \Psi_i = \text{MF+DH} \end{array} \right. \end{array} \right. \\ \text{If } h_i \in (2; 4) \quad \left\{ \begin{array}{l} \text{If } g_{s_i} \in [0, 0.55[\quad \left\{ \begin{array}{l} \text{If } S_i < 0.55 \quad \Psi_i = \text{MF+FC} \\ \text{else} \quad \Psi_i = \text{RG+MF} \end{array} \right. \\ \text{If } g_{s_i} \geq 0.55 \quad \left\{ \begin{array}{l} \text{If } S_i < 0.55 \quad \Psi_i = \text{MF+FC} \\ \text{else} \quad \Psi_i = \text{MF} \end{array} \right. \end{array} \right. \\ \text{If } h_i \in (3; 5) \quad \left\{ \begin{array}{l} \text{If } S_i < 0.55 \quad \Psi_i = \text{MF+FC} \\ \text{else} \quad \Psi_i = \text{MF+DH} \end{array} \right. \end{array} \right.
\end{aligned} \tag{146}$$

3.3 Snowmaking diagnoses

The water use for snowmaking is obtained by:

$$\mathcal{V}_{\text{SM}} = \frac{m_{\text{SM}} \mathcal{A}_{\text{SM}}}{(1 - \mathcal{L}_{\text{SM}}) \rho_w} \tag{147}$$

It is cumulated since the beginning of the season in the model diagnoses.

700 3.4 Optical diagnoses

The specific surface area SSA_i (m^2kg^{-1}) of each snow layer i is directly diagnosed from the optical diameter by:

$$SSA_i = \frac{6}{d_i \rho_I} \quad (148)$$

When CSNOWRAD=T17, spectral albedo values are also provided from an integration of incoming and absorbed radiations over user-defined spectral bands.

705 3.5 Mechanical diagnoses

3.5.1 Penetration resistance

A penetration resistance is computed for each layer. It is designed to represent the measurement obtained by the rammsonde commonly used in field snowpack observations (Giraud et al., 2002). The value of penetration resistance $\mathcal{R}_{p_i}$ is inferred for each layer $i \in [1, N]$ by Eq. 149 from microstructure properties (d_i , S_i and the transformation $g_{s_i}(d_i, S_i)$ following Eq. D6),
710 density ρ_i , liquid water content w_i (kg m^{-3}) and temperature θ_i ($^\circ\text{C}$). The result is expressed in kgf ($1 \text{ kgf} \simeq 9.81 \text{ N}$).

$$\left\{ \begin{array}{l} \text{If } d_i < 10^{-4}(4 - S_i) : \mathcal{R}_{p_i} = \frac{d_i \times 10^4 - 4 + S_i}{S_i - 3} \times \max(1, 0.018\rho_i - 1.363) + \frac{1 - d_i \times 10^4}{S_i - 3} \times \max[2, S_i(0.17\rho_i - 31) + (1 - S_i)(0.085\rho_i - 14.9)] \\ \text{else:} \left\{ \begin{array}{l} \text{If } \Psi_i = \text{RG} : \left\{ \begin{array}{l} \text{If } \rho_i < 200 : \mathcal{R}_{p_i} = 3 \\ \text{else: } \mathcal{R}_{p_i} = 0.17\rho_i - 31 \end{array} \right. \\ \text{If } \Psi_i = \text{RG+FC} : \left\{ \begin{array}{l} \text{If } \rho_i < 200 : \mathcal{R}_{p_i} = 2 \\ \text{else: } \mathcal{R}_{p_i} = S_i \times (0.17\rho_i - 31) + (1 - S_i) \times (0.17\rho_i - 31) \cdot (0.8 - g_{s_i}(d_i, S_i)) + 2 \times g_{s_i}(d_i, S_i) \end{array} \right. \\ \text{If } \Psi_i \in \left[\begin{array}{c} \text{FC} \\ \text{FC+DH} \end{array} \right] : \left\{ \begin{array}{l} \text{If } d_i > 4 \times 10^{-4}(S_i + 1), \mathcal{R}_{p_i} = 2 \\ \text{else} \left\{ \begin{array}{l} \text{If } \rho_i < 200 : \mathcal{R}_{p_i} = 3 \cdot (0.8 - g_{s_i}(d_i, S_i)) + 2 \cdot g_{s_i}(d_i, S_i) \\ \text{else: } \mathcal{R}_{p_i} = 0.17\rho_i - 31 \end{array} \right. \\ \text{If } \Psi_i \in \left[\begin{array}{c} \text{MF} \\ \text{MF+RG} \\ \text{MF+FC} \\ \text{MF+DH} \end{array} \right] : \left\{ \begin{array}{l} \text{If } (\theta_i < -0.2 \text{ or } w_i < 5) : \mathcal{R}_{p_i} = \max(10, 0.103\rho_i - 19.666) \\ \rho_i < 250, \mathcal{R}_{p_i} = 1 \\ \text{else} \left\{ \begin{array}{l} 250 \leq \rho_i < 350, \mathcal{R}_{p_i} = 2 \\ \rho_i \geq 350, \mathcal{R}_{p_i} = 0.16\rho_i - 54 \end{array} \right. \end{array} \right. \\ \text{If } \Psi_i = \text{DH} : \mathcal{R}_{p_i} = 2 \end{array} \right. \end{array} \right. \quad (149)$$

3.5.2 Shear strength

To be able to compute stability indexes of the snowpack, a shear resistance $\mathcal{R}_{s_i}$ is diagnosed for each layer i . It is also computed from microstructure properties, density, liquid water content and temperature through Eq. 150. $\mathcal{R}_{s_i}$ is expressed in kgf dm^{-2}

715 $(1 \text{ kgf dm}^{-2} \simeq 0.981 \text{ kPa})$.

$$\left\{ \begin{array}{l} \left[\begin{array}{l} \text{If } w_i \geq 5 \\ \text{and } \Psi_i \in \left\{ \begin{array}{l} \text{RG, MF, RG+FC,} \\ \text{RG+MF, DF+RG,} \\ \text{MF+FC, MF+DH} \end{array} \right\} \end{array} \right] \left\{ \begin{array}{l} \text{If } \rho_i < 200 : \quad \mathcal{R}_{s_i} = 0.1 \\ \text{If } 200 \leq \rho_i < 320 : \quad \mathcal{R}_{s_i} = 0.02\rho_i - 3.9 \\ \text{If } \rho_i \geq 320 : \quad \mathcal{R}_{s_i} = 0.068\rho_i - 18.64 \end{array} \right. \\ \text{else:} \quad \mathcal{R}_{s_i} = \max(0.05, \mathcal{C}_1(S_i, h_i) \times \mathcal{C}_2(d_i, S_i) \times \mathcal{C}_3(d_i, S_i, h_i) \times \mathcal{C}_4(w_i, \rho_i) \\ \times \mathcal{C}_5(d_i, S_i, h_i, w_i, \rho_i) \times (\rho_i^2 \cdot 10^{-4} - 0.6) + 0.12) \end{array} \right. \quad (150)$$

$\mathcal{C}_1, \mathcal{C}_2, \mathcal{C}_3, \mathcal{C}_4$ and $\mathcal{C}_5$ multiplicative functions are defined in Appendix G.

3.6 MEPRA

MEPRA was a standalone module designed to estimate the avalanche hazard from the snowpack stratigraphy simulated by
 720 Crocus, from mechanical diagnosis and expert rules (Giraud et al., 2002). It has been fully implemented in the SURFEX
 platform, and its output are now available with the other diagnostic variables. The general idea is to compare the shear strength
 $\mathcal{R}_{s_i}$ as defined previously, to the shear stress in the layer. For natural release, only the weight of overlying layers is taken into
 account while the load related to the presence of a skier at the snowpack surface is added to represent the accidental triggering.
 Expert rules are then defined to determine a hazard index from these mechanical stability indicators, both for natural release and
 725 accidental triggering. These expert rules were initially implemented by Giraud et al. (2002) but remained largely unpublished
 and have evolved to answer to feedbacks of operational avalanche forecasters, without detailed documentation. Equations
 implemented in the current version of SURFEX are described below. They are only valid for slope angle $\Theta = 40^\circ$.

3.6.1 Mechanical stability of snowpack layers

A simple mechanical diagnosis for stability is computed by dividing the shear resistance $\mathcal{R}_{s_i}$ by the shear in the layer. Two
 730 values are computed, to discriminate between natural avalanche activity and human triggering.

Natural release

The stability index $\mathcal{S}_{\text{nat}_i}$ for natural release is defined in each layer i as follows:

$$\mathcal{S}_{\text{nat}_i} = \frac{\mathcal{R}_{s_i}}{\sigma_{i+1}} \quad (151)$$

where σ_{i+1} is the weight of overlying layers (including considered layers), projected on the slope-parallel axis, as defined by
 735 Eq. 54.

Accidental triggering

The stability index for accidental triggering $\mathcal{S}_{\text{acc}_i}$ is similar to equation 151, with a supplementary term for shear stress to
 represent the additional load on the snowpack:

$$\mathcal{S}_{\text{acc}_i} = \frac{\mathcal{R}_{s_i}}{\sigma_{i+1} + \Xi_i \sigma_{\text{acc}_i}} \quad (152)$$

740 where σ_{acc_i} is designed to represent the shear load induced by a skier, defined as a piecewise linear decreasing function of depth $Z_i = \sum_{j=1}^i z_j$:

$$\sigma_{\text{acc}_i} = \begin{cases} 4 - 15Z_i & \text{if } Z_i < 0.1 \\ 2.5 - 10(Z_i - 0.1) & \text{if } 0.1 \leq Z_i < 0.15 \\ 2 - 8(Z_i - 0.15) & \text{if } 0.15 \leq Z_i < 0.2 \\ 1.6 - 4(Z_i - 0.2) & \text{if } 0.2 \leq Z_i < 0.35 \\ 1 - 2(Z_i - 0.35) & \text{if } 0.35 \leq Z_i < 0.5 \\ 0.7 - 1.5(Z_i - 0.5) & \text{if } 0.5 \leq Z_i < 0.8 \\ 0 & \text{if } 0.8 \leq Z_i \end{cases} \quad (153)$$

and Ξ_i is designed to represent the bonding effect reducing the shear stress in the layers, defined by:

$$\Xi_i = \frac{\sum_{j=1}^i m_j \xi_j}{\sum_{j=1}^i m_j} \text{ where } \xi_i : \begin{cases} \text{If } \Psi_i \in \left\{ \begin{array}{l} \text{MF, RG+MF,} \\ \text{MF+FC, MF+DF} \end{array} \right\} & \begin{cases} \text{If } \theta_i < -0.2, \xi_i = 0.5 \\ \text{else: } \xi_i = 1.1 \end{cases} \\ \text{else:} & \begin{cases} \text{If } \mathcal{R}_{s_i} > 1.5 : \xi_i = 1.0 \\ \text{else: } \xi_i = 1.2 \end{cases} \end{cases} \quad (154)$$

745 3.6.2 Hazard indexes

MEPRA analyses the profiles of $\mathcal{S}_{\text{nat}_i}$ and $\mathcal{S}_{\text{acc}_i}$ mechanical indexes with other parameters (mainly grain type, temperature and liquid water content and snow heights), to assess a natural avalanche hazard index $\mathcal{H}_{\text{nat}}$, on a scale of 0-5 and accidental hazard index $\mathcal{H}_{\text{acc}}$ on a scale 0-3, with a set of expert rules presented below. These hazard indexes are associated with levels of instability (one for high instability, Z_h , and one for moderate instability, Z_m , at most). For natural release, a classification

750 between 5 avalanche types is also provided.

Natural release

The natural release analysis relies on a classification of the upper layers of the snowpack (referred as "superior profile") in 4 classes : NEW (new snow), WET (wet snowpack), FRO (refrozen snowpack) or NAN (when it could not be classified in other class), based on the conditions listed in Table H1. A height of this superior profile Z_{SUP} is also defined below which the snowpack is significantly different, and called inferior profile. The latter is also classified into three classes : SOF (soft), HAR (hard) and NAN (undefined) as a function of the maximum penetration resistance, following Table H2.

755 Levels of high and moderate instabilities are looked for in the superior profile, as the uppermost buried layer where $\mathcal{S}_{\text{nat}_i}$ is below a threshold $\mathcal{S}_h = 2$ or $\mathcal{S}_m = 3$ respectively (or $\mathcal{S}_m = 3.05$ for a NEW type of superior profile):

$$\text{If } \exists j | Z_j > 0.1 \text{ and } Z_j \leq Z_{\text{SUP}} \text{ and } \mathcal{S}_{\text{nat}_j} \leq \mathcal{S}_h : Z_h = Z_j - \frac{z_j}{2} \quad (155)$$

$$760 \quad \text{If } \exists k | Z_k > 0.1 \text{ and } Z_j \leq Z_{\text{SUP}} \text{ and } \mathcal{S}_{\text{nat}_j} \leq \mathcal{S}_m \text{ and } j \neq k : Z_m = Z_k - \frac{z_k}{2} \quad (156)$$

A first natural avalanche hazard index $\mathcal{H}_{\text{nat}}$ is defined depending on depths of instability level Z_h and Z_m , superior profile height Z_{SUP} and superior profile type with the following expert rules:

$$\begin{aligned} \mathcal{H}_{\text{nat}_1} = & \begin{cases} Z_h > 0.8 \begin{cases} \text{NEW} \rightarrow 5 \\ \text{WET} \rightarrow 5 \\ \text{FRO} \rightarrow 3 \end{cases} \\ Z_h > 0.4 \begin{cases} \text{NEW} \rightarrow 4 \\ \text{WET} \rightarrow 4 \\ \text{FRO} \rightarrow 3 \end{cases} \\ Z_h > 0.2 \begin{cases} \text{NEW} \rightarrow 2 \\ \text{WET} \rightarrow 2 \\ \text{FRO} \rightarrow 3 \end{cases} \\ Z_h > 0 \begin{cases} \text{NEW} \rightarrow 1 \\ \text{WET} \rightarrow 1 \\ \text{FRO} \rightarrow 1 \end{cases} \\ Z_h \text{ not defined} \rightarrow 0 \end{cases} & \mathcal{H}_{\text{nat}_2} = \begin{cases} Z_m > 0.8 \begin{cases} \text{NEW} \rightarrow 3 \\ \text{WET} \rightarrow 3 \\ \text{FRO} \rightarrow 1 \end{cases} \\ Z_m > 0.4 \begin{cases} \text{NEW} \rightarrow 3 \\ \text{WET} \rightarrow 3 \\ \text{FRO} \rightarrow 1 \end{cases} \\ Z_m > 0.2 \begin{cases} \text{NEW} \rightarrow 3 \\ \text{WET} \rightarrow 3 \\ \text{FRO} \rightarrow 1 \end{cases} \\ Z_m > 0 \begin{cases} \text{NEW} \rightarrow 1 \\ \text{WET} \rightarrow 1 \\ \text{FRO} \rightarrow 1 \end{cases} \\ Z_m \text{ not defined} \rightarrow 0 \end{cases} & \mathcal{H}_{\text{nat}_3} = \begin{cases} Z_{\text{SUP}} > 0.8 \begin{cases} \text{NEW} \rightarrow 1 \\ \text{WET} \rightarrow 1 \\ \text{FRO} \rightarrow 0 \end{cases} \\ Z_{\text{SUP}} > 0.4 \begin{cases} \text{NEW} \rightarrow 1 \\ \text{WET} \rightarrow 1 \\ \text{FRO} \rightarrow 0 \end{cases} \\ Z_{\text{SUP}} > 0.2 \begin{cases} \text{NEW} \rightarrow 1 \\ \text{WET} \rightarrow 1 \\ \text{FRO} \rightarrow 0 \end{cases} \\ Z_{\text{SUP}} > 0 \begin{cases} \text{NEW} \rightarrow 0 \\ \text{WET} \rightarrow 1 \\ \text{FRO} \rightarrow 0 \end{cases} \\ Z_{\text{SUP}} \text{ not defined} \rightarrow 0 \end{cases} \end{aligned} \quad (157)$$

$$\text{NEW, WET, or FRO} \rightarrow \mathcal{H}_{\text{nat}} = \begin{cases} 2 & \text{if } \mathcal{H}_{\text{nat}_1} = 2 \\ \max(\mathcal{H}_{\text{nat}_1}, \mathcal{H}_{\text{nat}_2}, \mathcal{H}_{\text{nat}_3}) & \text{otherwise} \end{cases}$$

$$\text{NAN} \rightarrow \mathcal{H}_{\text{nat}} = 0$$

The avalanche situation is then classified in 6 classes following Appendix H2. Finally, $\mathcal{H}_{\text{nat}}$ is updated by expert rules accounting from the temporal evolution between times $t - \Delta t_M$ and t following Appendix H3. Note that these rules are sensitive to the MEPRA time step Δt_M , set to 3 hours by Giraud et al. (2002).

Accidental triggering

$\mathcal{H}_{\text{acc}}$ is based on the identification of a slab structure in the snowpack including a slab (layer i and possibly layers above) over a weak layer (layer $i + 1$). This structure is identified through the following conditions:

$$770 \quad \begin{cases} \text{MF} \notin \Psi_{i-1} \\ \mathcal{R}_{s_i} > 1.3 \\ \Psi_i \in [\text{DF+RG}, \text{RG}, \text{RG+FC}, \text{DF}] \\ 0.01m \leq Z_i < 1m \\ \Psi_{i+1} \in [\text{FC}, \text{DH}, \text{FC+DH}, \text{PP}, \text{PP+DF}, \text{DF}] \end{cases} \quad (158)$$

Similarly to the natural instability levels (Eq. 155 and 156), levels of high accidental instability and moderate accidental instability are looked for among the identified weak layers satisfying Eq. 158:

$$\text{If } \exists i | \Psi_{i+1} \in [\text{FC}, \text{DH}, \text{FC+DH}] \text{ and } \mathcal{S}_{\text{acc}_{i+1}} < 1.5 : Z_h = Z_{i+1} - \frac{z_{i+1}}{2} \quad (159)$$

$$\text{If } \exists i | \Psi_{i+1} \in [\text{PP}, \text{PP+DF}, \text{DF}] \text{ or } (\Psi_{i+1} \in [\text{FC}, \text{DH}, \text{FC+DH}] \text{ and } 1.5 \leq \mathcal{S}_{\text{acc}_{i+1}} < 2.5) : Z_m = Z_{i+1} - \frac{z_{i+1}}{2} \quad (160)$$

775 The accidental hazard index is finally defined with the following expert rules:

$$\left\{ \begin{array}{l} \text{If } \exists i | \text{Eq. 159} : \begin{cases} \text{If } Z_c < 0.01 : \mathcal{H}_{\text{acc}} = \max(3, \mathcal{H}_{\text{eq}}) \\ \text{else: } \mathcal{H}_{\text{acc}} = \max(1, \mathcal{H}_{\text{eq}}) \end{cases} \\ \text{If } \exists i | \text{Eq. 160} : \begin{cases} \text{If } Z_c < 0.01 : \mathcal{H}_{\text{acc}} = \max(2, \mathcal{H}_{\text{eq}}) \\ \text{else: } \mathcal{H}_{\text{acc}} = \max(1, \mathcal{H}_{\text{eq}}) \end{cases} \\ \text{If } \nexists i | \text{Eq. 159 or Eq. 160} : \mathcal{H}_{\text{acc}} = \max(0, \mathcal{H}_{\text{eq}}) \end{array} \right. \quad (161)$$

where $\mathcal{H}_{\text{eq}}$ is a function of the natural index $\mathcal{H}_{\text{nat}}$ following Appendix H4 and Z_c is the cumulated depth of crusts above a layer:

$$Z_{c_h} = \sum_i z_i \text{ for } i | \theta_i < 0.2 \text{ and } \text{MF} \in \Psi_i \text{ and } Z_i < Z_h \text{ and } (\text{PP} \notin \Psi_j \text{ and } \text{DF} \notin \Psi_j \forall j \in [1, i-1]) \quad (162)$$

$$780 \quad Z_{c_m} = \sum_i z_i \text{ for } i | \theta_i < 0.2 \text{ and } \text{MF} \in \Psi_i \text{ and } Z_i < Z_m \text{ and } (\text{PP} \notin \Psi_j \text{ and } \text{DF} \notin \Psi_j \forall j \in [1, i-1]) \quad (163)$$

Note that only one value for Z_h and Z_m is provided in the diagnoses output file. If $\mathcal{H}_{\text{acc}} = \mathcal{H}_{\text{eq}}$ in Eq. 161, they correspond to Eq. 155 and 156, otherwise they correspond to Eq. 159 and 160.

4 Technical features

4.1 Implemented simulation geometries

785 All variables in the code are defined as vectors including at least a spatial dimension, and when necessary the snow layers as second dimension. The implication in terms of numerical efficiency of loops in the code is described in detail in Appendix J. This 1D spatial dimension allows to use either discontinuous collections of points or regular grids for simulations. A typical example of a collection of points is the semi-distributed geometry based on homogeneous massifs and topographic classes which has been used for more than 30 years for operational simulations in French mountains and in the associated 66-year
790 reanalysis (Vernay et al., 2022). Gridded experiments can also be easily defined through the standard SURFEX tools which include regular latitude-longitude coordinates or various conformal projections. Over the French territory, the Lambert 93 projection is recommended as a national standard for gridded simulations (i.e. Deschamps-Berger et al., 2022; Haddjeri et al., 2024).

4.2 Parallelization and numerical efficiency

795 In the general case where Crocus is not coupled with a snow transport model, the processes currently represented by the model do not involve any mass or energy exchange between the snowpacks of the different spatial units. Therefore, parallelization can be very efficiently applied without any need of communication between processors in the physical model. A distributed memory parallelism has been chosen for that purpose in the offline driver of the SURFEX platform based on MPI libraries. However, the standard SURFEX Input-Output routines are not currently parallelized. Therefore, all input and output data are
800 forwarded to a single processor. As a result, over large domains, the efficiency of parallel computing is currently limited by the saturation of the IO processor, in all cases but especially when the user chooses to output a large number of diagnoses at high temporal resolution. The XIOS library (Yepes-Arbós et al., 2022) implemented in SURFEX is designed to deal with this issue but the implementation of its compatibility with Crocus variables is still in progress. The numerical cost of the model itself depends on the number of layers created by the model. Therefore, it can vary significantly from one domain to another
805 and from a season to another, depending on the number of layers of each simulated snowpack which highly depends on total snow depth.

To give the magnitude of the numerical cost, Table 3 presents the computing time of a 1-year simulation over 4471 simulation points in the French Alps. It must be noticed that the numerical cost of Crocus is very low compared to the cost of IO, providing a clear guidance for priorities in future optimizations. Crocus also only represents 26% of the computation time of the ISBA
810 land surface model itself. Even in an alpine region, the variability of snow cover in time and space makes the snow component relatively cheap with a similar level of complexity compared to the 20-layer soil model running all year over all points. As a result, the numerical cost of Crocus ($0.3 \text{ cores} \times \text{s}$ per year and simulation point for this example) can not be considered as a valid argument to prefer simpler models in large scale applications of Land Surface Models or coupled applications.

Considering the partitioning of numerical costs between the different subroutines within Crocus, it appears clearly that the
815 complexity of the discretization rules emphasized by Eq. 11 has a significant impact as this routine represents 33% of the whole model cost. The metamorphism routine is the second most contributing routine although its cost has been considerably reduced compared to previous versions (Carmagnola et al., 2014). The numerical core of the model solving heat diffusion and energy balance is very efficient contributing to less than 6% of the cost. Numerical optimizations are still possible in some routines representing an unjustified contribution compared to their low complexity (e.g. thermal conductivity). Possible optimizations
820 may concern the management of loops (cf. Appendix J) or some iterative calls to scalar functions in external modules.

The memory consumption of the model is relatively low with the standard physical options. In the experiment described above, the maximum Resident Set Size (RSS) is lower than 17 GB. However, the high spectral resolution of the TARTES optical scheme slightly increases the memory consumption (25 GB) and highly increases the total numerical cost when this option is activated ($28588 \text{ cores} \times \text{s}$ for the TARTES module in an experiment identical to Table 3 but with SNOWRAD=T17,
825 i.e. about 20 times the reference numerical cost of Crocus).

Table 3. Numerical cost of a 1-year simulation from 1 Aug 2023 to 1 Aug 2024 over 4471 simulation points corresponding to the French Alps domain described in Vernay et al. (2022) and the default physical options as in Lafayssse et al. (2017). The code was compiled with Intel®MPI library version 2018.5.274 and O2 optimization level. Output are minimized (reduced to daily snow depth), otherwise the total execution time would be highly increased. The simulation is performed using 80 MPI threads on 80 physical cores on one 2.2 GHz AMD®Rome computing node constituted by 2 sockets of 64 cores. Results are presented in cores $\times$ s. The real elapsed time for this simulation in this architecture is 449 s.

	Time (cores $\times$ s)	Ratio with Crocus time (%)
SURFEX run	35964	2480
IO reading and communications	29390	2026
ISBA land surface model	5513	380
Crocus snow model	1450	100
Snowfall and vertical discretization	491	33.4
Metamorphism	173	11.9
Absorption of solar radiation	162	11.2
Compaction	95	6.6
Regridding (aggregation / dissociation)	77	5.3
Heat diffusion (Eq. 107-108)	64	4.4
Thermal conductivity	61	4.2
Percolation and refreezing	58	4.0
Melting	30	2.1
Aggregation of vanishing layers	27	1.9
Drift	25	1.7
Diagnostic of energy fluxes	23	1.6
Energy balance (Eq. 102-106)	20	1.4

4.3 Running environment and visualization

Beyond the FORTRAN code itself, most offline applications of the model have to deal with the management of input and output files to perform various experiments with different forcing files, namelists, or binaries, different setting of initial and final simulation dates, standard initialization procedures (soil spinup, etc.). Therefore, a common running environment of the
830 model in Python is provided in an independent package called snowtools with full user documentation and an interface for technical support (cf. Code availability section).

Crocus scalar diagnoses can be easily processed by any scientific plotting software supporting netcdf format as input. However, the irregular vertical discretization of the snowpack model complexifies the visualization of the simulated profiles. A simple software provided in the snowtools package is able to combine the variables to plot with the depth of each layer to

835 produce detailed instantaneous stratigraphies or temporal evolution of a given stratified variable (as in Appendix I). For spatial simulations, plotting the spatial variability of the vertical structure of the snowpack is still a challenge.

4.4 Externalization

Although the reference implementation of Crocus is within the SURFEX land surface modelling platform (Masson et al., 2013), there is an increasing need of being able to couple Crocus with other land surface schemes. For that purpose, an externalized
840 version of the source codes is now available as an independent Fortran library that can be compiled alone and called by other land surface models (cf. Code availability section). It includes all the processes described in this paper except the coupling with external components (snow transport modules and MEB vegetation module). Thus, Crocus is also now fully integrated within the SVS2 land surface system (Vionnet et al., 2025). It was also recently implemented within the Flexible Snow Model (FSM2, Essery et al., 2025) allowing the coupling with its more detailed vegetation model (Mazzotti et al., 2024). SURFEX, SVS2 and
845 FSM2 rely on a unique code repository of Crocus that guarantees the long-term maintenance and convergence of the code and therefore facilitates the contributions of different research groups to the model developments. For instance, as mentioned for several processes in Section 2, various new parameterizations better suited for Arctic snow were recently proposed within the SVS2 implementation (Woolley et al., 2024; Vionnet et al., 2025). Thanks to this method, these developments will integrate soon a future release and be beneficial for SURFEX and FSM2 applications. Therefore, we strongly encourage other groups
850 that have copied the code within their specific applications to try to converge towards this unique code version. This includes the implementation of Crocus within WRF-Hydro (Eidhammer et al., 2021), the coupling of Crocus with Noah Land Surface Model (Navari et al., 2024), the MAR regional climate model largely used for polar regions (Fettweis et al., 2017; Agosta et al., 2019) and from which the Crocus version has diverged for a long time (Gallée et al., 2001), and even applications which have only extracted specific routines such as the CryoGrid permafrost model (Zweigle et al., 2021).

855 5 Review of evaluations and scientific applications

5.1 With a local scale meteorological forcing

The most direct evaluations of the model are performed on well-instrumented sites allowing to minimize errors in the meteorological forcing and in the observations used for evaluation. Model skills have been documented in detail at the Col de Porte experimental site (Morin et al., 2012; Lejeune et al., 2019), a mid-elevation meadow in French Alps. The very first evaluations
860 of Brun et al. (1989) present qualitative evaluations of surface and internal temperature, snow depth, and basal runoff during short periods of the winter 1986-1987. Brun et al. (1992) extended the evaluations to the whole winter 1988-1989 on the same variables as well as a subjective comparison between the simulated stratigraphies and weekly observed profiles. Extensions of the evaluation period were successively published by Essery et al. (1999); Boone and Etchevers (2001); Strasser et al. (2002); Etchevers et al. (2004); Avanzi et al. (2016) in the context of model intercomparisons, and also by Vionnet et al. (2012). These
865 papers also included evaluations of albedo and Snow Water Equivalent. Lafaysse et al. (2017) extended these evaluations to

all multiphysics options and accounted for observation uncertainties usually ignored in previous papers. The accuracy of the model on these variables has not significantly changed since the first years of development. Complementary evaluations of density and microstructure profiles are provided by Morin et al. (2013) and Carmagnola et al. (2014). However, quantitative evaluation of internal snow properties is still a methodological challenge due to frequent discrepancies between numerical and
870 observed snow layers that can easily lead to double penalty issues. This can only be partly solved with vertical adjustments algorithms (Viallon-Galinier et al., 2020; Herla et al., 2021) or with an expert layer tracking (Calonne et al., 2020).

More challenging evaluations include a variety of environmental and climate conditions. Evaluations driven by local meteorological observations were performed in Svalbard (Bruland et al., 2001; Sauter and Obleitner, 2015), at the high elevation site of Weissflujoch, Switzerland (Etchevers et al., 2004), over tropical glaciers and moraines in Bolivia (Lejeune et al., 2007)
875 and Ecuador (Wagon et al., 2009), at Sherbrooke University, Quebec (Langlois. et al., 2009), at Torgnon, Italy (Di Mauro et al., 2019). The most comprehensive evaluations in terms of number of sites and years were performed on 10 contrasted sites through the Earth System Model-Snow Model Intercomparison Project (ESM-SnowMIP, Krinner et al., 2018; Menard et al., 2021) and with a few more sites for albedo evaluations by Gaillard et al. (2025). Typical errors on snow depth, SWE, albedo, surface temperature and ground temperature were in the range of state-of-the art snow models as illustrated with up-
880 to-date simulations with this model version in Appendix I. A similar overall skill can be obtained by simpler models on these variables. The cold bias in surface temperature identified by Menard et al. (2021) may be attributed to the parameterization of turbulent fluxes which are suspected to be underestimated with the previously standard configuration ($Ri_t = 0.2$) but this bias is removed with the new default value ($Ri_t = 0.026$, Martin and Lejeune, 1998; Lafaysse et al., 2017). This assumption was also recently supported by more detailed evaluations of all components of the energy balance including eddy-covariance
885 observations of turbulent fluxes in Québec (Lackner et al., 2022) and in Finnish peatlands (Nousu et al., 2024). However, it is especially important to be aware of the equifinality between the different empirical parameterizations (i.e. different model configurations providing similar model results) and to be cautious with the complex compromises in multivariate evaluations (the optimal model configuration can change depending on the evaluated variable, Essery et al., 2013; Lafaysse et al., 2017). These difficulties should encourage future attempts to improve processes representations to be tested robustly with ensemble
890 multiphysics simulations and multivariate evaluations (e.g. Woolley et al., 2024).

5.2 With a regional scale meteorological forcing

In many other applications, the model was forced by meteorological reanalyses (e.g. Durand et al., 2009; Brun et al., 2013; Vernay et al., 2022) or short-term forecasts (e.g. Vionnet et al., 2016; Skaugen et al., 2018) or a combination of both (Vionnet et al., 2022). Although these studies often include snow depth evaluations on a large range of stations, in this case the resulting
895 modelling errors of any snow model are dominated by errors in the meteorological forcing (Raleigh et al., 2015; Günther et al., 2019) and Crocus does not make an exception (Quéno et al., 2017; Réveillet et al., 2018; Vionnet et al., 2019; Gouttevin et al., 2022). Thus, the attribution of some limitations of the simulation results to the snowpack model itself is difficult. However, this is sometimes the only possible method for the assessment of some specific processes. For instance, the simulated concentrations of Light-Absorbing Particles (Tuzet et al., 2017), the spectral reflectances from the TARTES optical scheme (Cluzet et al.,

2020), the blowing snow fluxes (Vionnet et al., 2018; Baron et al., 2024) were only evaluated in such context. The same applies to the ability of the model to reproduce the properties of polar snow (e.g. Dang et al., 1997; Libois et al., 2015; Barrere et al., 2017; Vionnet et al., 2025), the spatial distribution of snow conditions depending on topography (Revuelto et al., 2018; Skaugen et al., 2018; Haddjeri et al., 2024), or complex remote sensing signals (Veyssière et al., 2019). Similar simulation frameworks are used to investigate the suitability of the model for hydrological diagnoses (e.g. Strasser and Etchevers, 2005), glacier mass balance (e.g. Réveillet et al., 2018; Roussel et al., 2025) or avalanche activity (Eckert et al., 2010; Viallon-Galinier et al., 2022).

Based on the confidence provided by these available evaluations, the model is used for various purposes including the understanding of internal physical processes (e.g. Domine et al., 2013; Dick et al., 2023; Roussel et al., 2024), the quantification of contributions to the energy balance (e.g. Tuzet et al., 2020; Dumont et al., 2020; Reveillet et al., 2022, for light-absorbing particles), the monitoring of the long-term climatology of extreme snow loads (Le Roux et al., 2022) or avalanche activity (Reuter et al., 2022, 2025), the investigation of the links between snow cover and alpine ecosystems evolutions (Nicoud et al., 2025), and climate projections of natural snow conditions (Rousselot et al., 2012; Verfaillie et al., 2018), avalanche hazard (Castebrunet et al., 2014) and ski resorts operating conditions (Spandre et al., 2019; Morin et al., 2021; François et al., 2023). The development efforts were originally dedicated to operational avalanche hazard forecasting (Durand et al., 1999). However, after about 30 years of operation, the model did not become the main tool of the forecasters because this application is especially sensitive to uncertainties (Vernay et al., 2015) among numerous other challenges as reviewed by Morin et al. (2020). The statistical post-processing of simulations through various techniques of artificial intelligence (Nousu et al., 2019; Evin et al., 2021; Viallon-Galinier et al., 2023) might provide guidance to improve the practical interest of such simulations for operational applications including avalanche forecasting.

5.3 Towards data assimilation

The long memory of the snowpack on the past meteorological conditions and past snow processes imply that all sources of modelling errors tend to cumulate all along the season. Therefore, there is a large avenue for data assimilation algorithms in order to improve the initial states of the simulations (Largerou et al., 2020). However, the variable dimension size of the Crocus state vector (due to the variable number of layers) and the high non-linearities in the simulated processes make the application of a number of data assimilation algorithms to this model challenging. Therefore, most recent efforts intended to apply different variants of the Particle Filter to weight the members of an ensemble of simulations according to their distance to some observations (Charrois et al., 2016; Cluzet et al., 2021, 2022; Deschamps-Berger et al., 2022). The different options of the algorithm are described in Cluzet et al. (2021) and the implemented variables are snow depth and optical reflectance, for which the observation operator is simply the identity function as these variables are direct diagnoses of the model. The assimilation of optical reflectance is however constrained by the retrieval errors of this variable in complex terrain (Cluzet et al., 2020) that still exceed the requirements for an efficient data assimilation (Revuelto et al., 2021). Large efforts are planned in a near future to extend these possibilities. For some common satellite observations (e.g. snow cover fraction, wet snow fraction), this will require the development of appropriate observation operators from the simulated state variables.

6 Conclusion

935 This article provides a comprehensive description of all equations implemented in version 3.0.2 of the Crocus snow model. It gathers the recent developments of the last 13 years in a unique publication: (i) modelling of Light-Absorbing Particles, (ii) coupling with the TARTES optical scheme, (iii) modelling of ice layers due to freezing rain, (iv) coupling with the MEB big-leaf vegetation scheme, (v) snow management practices on ski slopes, (vi) coupling with blowing snow schemes, (vii) multiphysics parameterizations for most processes and (viii) diagnosis of the snowpack mechanical stability. In addition, this
 940 article documents a number of equations implemented in previous code versions but never published in the literature. It must be mentioned that during the preparation of this publication, a considerable number of errors or discrepancies between the code and previous publications were identified and corrected. This is in full agreement with the main conclusions of Menard et al. (2021) suggesting that insufficient model documentation is a key factor for the difficulty to improve snow modelling in the last decades. This comprehensive documentation is expected to help snow scientists to better interpret results based on this
 945 model. This is especially important in the context of an in-progress extension of Crocus applications in several land surface schemes. This documentation effort is also expected to help the snow modelling community improve numerical models in the future thanks to an accurate knowledge of the existing parameterizations and numerical difficulties. Despite our best efforts to minimize errors, previous literature and experience suggest that some errors may still remain in this publication. In such a case, corrigenda will be associated to this publication in due course.

950 Appendix A: Attractor profile in layering

The attractor profile z_i^* used in Eq. 11 depends only on the total snow depth Z and number of layers N . Let's define N^* and Z^* by:

$$\left\{ \begin{array}{l} \text{if } Z > 20 \text{ and } N > \frac{N_{\max}}{3} + 2 \\ \text{else} \end{array} \right\} \left\{ \begin{array}{l} N^* = N - \frac{N + N_{\max}}{6} \\ Z^* = 3 \end{array} \right. \quad \left\{ \begin{array}{l} N^* = N \\ Z^* = Z \end{array} \right. \quad (\text{A1})$$

Then, the attractor profile is defined by:

$$\begin{aligned}
 & \left\{ \begin{aligned}
 & z_1^* = \min(0.01, \frac{Z^*}{N^*}) \\
 & z_2^* = \min(0.0125, \frac{Z^*}{N^*}) \\
 & z_3^* = \min(0.03, \frac{Z^*}{N^*}) \text{ if } N^* > 3 \\
 & z_4^* = \min(0.04, \frac{Z^*}{N^*}) \text{ if } N^* > 4 \\
 & z_5^* = \min(0.05, \frac{Z^*}{N^*}) \text{ if } N^* > 5 \\
 & z_6^* = \max(0.07, \min(\frac{Z^*}{N^*}, 0.5)) \text{ if } N^* > 6 \\
 & z_7^* = \max(0.07, \min(\frac{Z^*}{N^*}, 1.)) \text{ if } N^* > 7 \\
 & z_8^* = \max(0.07, \min(\frac{Z^*}{N^*}, 2.)) \text{ if } N^* > 8 \\
 & z_9^* = \max(0.07, \min(\frac{Z^*}{N^*}, 4.)) \text{ if } N^* > 9 \\
 & z_{10}^* = \max(0.07, \min(\frac{Z^*}{N^*}, 10.)) \text{ if } N^* > 10 \\
 & z_i^* = \max(0.07, \min(\frac{Z^*}{N^*},)) \forall i \in [11, N^*] \text{ if } N^* > 11 \\
 & z_i^* = (i - N^*) \frac{2(Z-3)}{(N-N^*)(N-N^*+1)} \forall i \in [N^* + 1, N] \text{ if } Z > 20 \\
 & z_N^* = \min(0.02, \frac{Z}{N^*}) \\
 & \text{if } Z > 3 \text{ and } N^* > 10 \left\{ \begin{aligned}
 & z_{N-1}^* = 0.66z_N^* + 0.34z_{N-3}^* \\
 & z_{N-2}^* = 0.34z_N^* + 0.66z_{N-3}^*
 \end{aligned} \right. \quad \text{instead of previous definitions}
 \end{aligned} \right. \tag{A2}
 \end{aligned}$$

It extends the definition of Vionnet et al. (2012) in order to converge towards a profile allowing a numerically stable resolution of heat diffusion for thick snowpacks and glacier applications.

Appendix B: Adjustment of wind speed

Several parameterizations of the model are formulated with a wind speed at a specific height corresponding to the experimental conditions but might not correspond to the reference height of the forcing variable. In these cases, the wind speed U_z (ms^{-1}) at height z (m) is adjusted assuming a logarithmic profile in the surface boundary layer based following:

$$U_z = U \frac{\ln\left(\frac{z}{z_0}\right)}{\ln\left(\frac{z_u}{z_0}\right)} \tag{B1}$$

where z_0 is the surface roughness length (m).

Appendix C: Growth of faceted crystals in B21 metamorphism parameterizations

965 The growth of faceted crystals in B21 parameterization (Eq. 46) is based on cold room experiments from Marbouty (1980). These functions already published by Vionnet et al. (2012) are repeated here for the comprehensiveness of this paper. f , g , h and Φ are dimensionless functions from 0 to 1 given by:

$$f(\theta_i) = \begin{cases} 0 & \text{if } \theta_i < -40 \text{ }^\circ\text{C} \\ 0.011 \times (\theta_i + 40) & \text{if } -40 \leq \theta_i < -22 \text{ }^\circ\text{C} \\ 0.2 + 0.05 \times (\theta_i + 22) & \text{if } -22 \leq \theta_i < -6 \text{ }^\circ\text{C} \\ 0.7 - 0.05\theta_i & \text{otherwise} \end{cases} \quad (\text{C1})$$

$$970 \quad h(\rho_i) = \begin{cases} 1. & \text{if } \rho_i < 150 \text{ kg m}^{-3} \\ 1 - 0.004 \times (\rho_i - 150) & \text{if } 150 < \rho_i < 400 \text{ kg m}^{-3} \\ 0. & \text{otherwise} \end{cases} \quad (\text{C2})$$

$$g(\mathcal{G}_i) = \begin{cases} 0. & \text{if } \mathcal{G}_i < 15 \text{ K m}^{-1} \\ 0.01 \times (\mathcal{G}_i - 15) & \text{if } 15 \leq \mathcal{G}_i < 25 \text{ K m}^{-1} \\ 0.1 + 0.037 \times (\mathcal{G}_i - 25) & \text{if } 25 \leq \mathcal{G}_i < 40 \text{ K m}^{-1} \\ 0.65 + 0.02 \times (\mathcal{G}_i - 40) & \text{if } 40 \leq \mathcal{G}_i < 50 \text{ K m}^{-1} \\ 0.85 + 0.0075 \times (\mathcal{G}_i - 50) & \text{if } 50 \leq \mathcal{G}_i < 70 \text{ K m}^{-1} \\ 1. & \text{otherwise} \end{cases} \quad (\text{C3})$$

$$\Phi = 1.0417 \cdot 10^{-9} \text{ m s}^{-1} \quad (\text{C4})$$

Appendix D: New formalism of metamorphism

The translation of the original metamorphism parameterizations in terms of dendricity, sphericity and size from Brun et al. 975 (1992) to the new formalism of Carmagnola et al. (2014) in terms of optical diameter and sphericity, was based on the original expression of the optical diameter d_i as a function of dendricity δ_i , sphericity S_i and grain size g_{s_i} (as already published in Eq. 13 of Vionnet et al. (2012)):

$$d_i = \begin{cases} 10^{-4} [\delta_i + (1 - \delta_i)(4 - S_i)] & \text{if } \delta_i > 0 \text{ (dendritic case)} \\ g_{s_i} \times S_i + (1 - S_i) \times \max(4 \cdot 10^{-4}, \frac{g_{s_i}}{2}) & \text{if } \delta_i = 0 \text{ (non-dendritic case)} \end{cases} \quad (\text{D1})$$

This relationship has always been required to compute the absorption of solar radiation from the equations of Section 2.4.9.

980 In the dendritic case, the transformation $(S_i, \delta_i) \Rightarrow (S_i, d_i)$ is bijective. The inversion of this relationship lead to:

$$\delta_i = \frac{10^4 \times d_i - 4 + S_i}{S_i - 3} \text{ if } d_i < 10^{-4}(4 - S_i) \quad (\text{D2})$$

and the new evolution law of d_i was obtained by Carmagnola et al. (2014) using

$$\frac{dd_i}{dt} = \frac{\partial d_i}{\partial \delta_i} \frac{d\delta_i}{dt} + \frac{\partial d_i}{\partial S_i} \frac{dS_i}{dt} \quad (\text{D3})$$

Thus, the combination of Eq. D3 with the equations from Table 1 of Vionnet et al. (2012) provides the second line of Eq. 46
 985 in this paper (which is close to the right column of Table 2 in Carmagnola et al. (2014) after typo corrections).

In the non-dendritic case, the transformation $(S_i, g_{s_i}) \Rightarrow (S_i, d_i)$ is not bijective. When $S_i = 0$, Eq. D1 gives $d_i = 4 \times 10^{-4} \forall g_{s_i} \in [3 \times 10^{-4}, 8 \times 10^{-4}]$. As a result, the metamorphism functions from Table 1 of Vionnet et al. (2012) cannot be reproduced in the space (S_i, d_i) when $S_i = 0$ (e.g. depth hoar). Then, Eq. D1 is discontinuous at the limit between dendritic and non-dendritic cases. Indeed, the limit of the dendritic case gives $\lim_{\delta_i \rightarrow 0} d_i = 10^{-4}(4 - S_i)$. When combined with the non
 990 dendritic case, this would result in $g_{s_i} = 3 \times 10^{-4}$ while the initial value of g_{s_i} was actually higher for non-spheric particles in Brun et al. (1992): $g_{s_i} = 10^{-4}(4 - s_i)$. In the other cases, the inversion of Eq. D1 can provide a relationship for g_{s_i} as a function of d_i and S_i :

$$g_{s_i} = \begin{cases} \frac{2d_i}{S_i+1} & \text{if } d_i \geq 4 \times 10^{-4}(S_i + 1) \\ \frac{d_i - 4 \times 10^{-4}(1 - S_i)}{S_i} & \text{if } d_i < 4 \times 10^{-4}(S_i + 1) \end{cases} \quad (\text{D4})$$

Eq. D4 is actually more complex than Eq. 3 of Carmagnola et al. (2014) which was an incorrect simplification corresponding
 995 only to the initialization of grain size at the dendritic - non-dendritic transition. It is also not defined when $S_i = 0$ and $d_i < 4 \times 10^{-4}(S_i + 1)$. Last, the derivation of an evolution law for optical diameter was obtained by Carmagnola et al. (2014) in the non-dendritic case (left column of their Table 2) by considering only $\frac{dd_i}{dt} = \frac{\partial d_i}{\partial S_i} \frac{dS_i}{dt}$. This is actually inconsistent with the original formalism in the non-dendritic case as it ignores the term $\frac{\partial d_i}{\partial g_{s_i}} \frac{dg_{s_i}}{dt}$. Ignoring this term may be convenient to avoid the problems mentioned above but it affects the metamorphism of faceted crystals and depth hoar without any scientific justification
 1000 whereas they are the most critical snow types for further analyses in terms of mechanical stability. Furthermore, a number of parameterizations of other processes and diagnoses in the code were also affected by the incorrect simplification of Eq. D4. The original difficulty of this translation of formalisms comes from the fact that Eq. D1 is neither bijective nor continuous. However, we considered that it is better to adapt this unpublished formula and preserve as much as possible the metamorphism laws, the parameterizations of other processes and the diagnoses relying on microstructure properties. A new metamorphism
 1005 option (B21) has therefore been defined, replacing the expression from Carmagnola et al. (2014) by:

$$d_i = g_{s_i} \times S_i + (1 - S_i) \frac{4 \times 10^{-4} + g_{s_i}}{2} \text{ if } \delta_i = 0 \text{ (non-dendritic case)} \quad (\text{D5})$$

This allows to replace Eq. D4 by:

$$g_{s_i} = 2 \frac{d_i - 2 \times 10^{-4}(1 - S_i)}{1 + S_i} \quad (\text{D6})$$

This way, the evolution of optical diameter in the non dendritic case can be obtained by:

$$1010 \quad \frac{dd_i}{dt} = \frac{\partial d_i}{\partial g_{s_i}} \frac{dg_{s_i}}{dt} + \frac{\partial d_i}{\partial S_i} \frac{dS_i}{dt} \quad (\text{D7})$$

$$= \frac{1 + S_i}{2} \frac{dg_{s_i}}{dt} + \left(\frac{g_{s_i}}{2} - 2 \times 10^{-4} \right) \frac{dS_i}{dt} \quad (\text{D8})$$

$$= \frac{1 + S_i}{2} \frac{dg_{s_i}}{dt} + \frac{d_i - 4 \times 10^{-4}}{1 + S_i} \frac{dS_i}{dt} \quad (\text{D9})$$

The main advantage of this new formalism is that it respects the original evolution law of $\frac{dg_{s_i}}{dt}$ as published by Vionnet et al. (2012). As a result, all parameterizations and diagnostics calibrated in the original formalism can still considered to be valid in this new formalism. Finally, the first line of Eq. 46 corresponds to the combination of Eq. D9 and Table 1 of Vionnet et al. (2012). Complementary analyses by Baron (2023) have shown that the obtained microstructure properties of B21 option are closer to the original formalism of Vionnet et al. (2012) than the implementation of Carmagnola et al. (2014) (also referred as C13 in Lafaysse et al. (2017)). This is especially true when this parameterization is combined with the snow drift options. More details are available in Baron (2023).

1020 Similarly for wet metamorphism, the combination of Eq. D9 and Table 2 of Vionnet et al. (2012) provides Eq. 51 of this paper. The transformation of wet metamorphism laws in this new formalism were neither provided in Carmagnola et al. (2014) nor correctly implemented.

Appendix E: Evolution of optical diameter during snow drift

The evolution of microstructure properties was parameterized in terms of dendricity δ_i , sphericity S_i and grain size g_{s_i} from simple evolution laws provided in Table 3 of Vionnet et al. (2012) in which sign errors must be accounted for in the evolution of δ_i and g_{s_i} :

$$\frac{d\delta_i}{dt} = \frac{-\delta_i}{2\tau_{\text{DRIFT}}} \text{ if } \delta_i > 0 \text{ (dendritic case)} \quad (\text{E1})$$

$$\frac{dg_{s_i}}{dt} = \frac{-5 \times 10^{-4}}{\tau_{\text{DRIFT}}} \text{ if } \delta_i = 0 \text{ (non-dendritic case)} \quad (\text{E2})$$

$$\frac{dS_i}{dt} = \frac{1 - S_i}{\tau_{\text{DRIFT}}} \quad (\text{E3})$$

1030 In the dendritic case, the evolution of the optical diameter d_i is obtained by the introduction of Eq. E1 and E3 in Eq. D3 and computing $\frac{\partial d_i}{\partial \delta_i}$ and $\frac{\partial d_i}{\partial S_i}$ from the first line of Eq. D1. In the non-dendritic case, the evolution of the optical diameter d_i is

obtained by the introduction of Eq. E2 and E3 in Eq. D7 and computing $\frac{\partial d_i}{\partial g_{s_i}}$ and $\frac{\partial d_i}{\partial S_i}$ from Eq. D5. Finally:

$$\begin{cases} \frac{dd_i}{dt} = 10^{-4}(S_i - 3) \times \left(\frac{-\delta_i}{2\tau_{\text{DRIFT}}} \right) + 10^{-4}(\delta_i - 1) \times \frac{1 - S_i}{\tau_{\text{DRIFT}}} & \text{if } d_i < 10^{-4}(4 - S_i) \\ \frac{dd_i}{dt} = \frac{S_i + 1}{2} \times \frac{-5 \times 10^{-4}}{\tau_{\text{DRIFT}}} + \frac{g_{s_i} - 4 \times 10^{-4}}{2} \times \frac{1 - S_i}{\tau_{\text{DRIFT}}} & \text{if } d_i \geq 10^{-4}(4 - S_i) \end{cases} \quad (\text{E4})$$

The first line can be slightly simplified and Eq. D6 introduced in the second line to finally obtain the equivalent discrete
1035 formulation of Eq. 67.

Appendix F: Thermodynamical functions

The air volumetric mass ρ_a is obtained by:

$$\rho_a = \frac{P_s}{R_a T_a \left(1 + \left(\frac{R_v}{R_a} - 1 \right) q_a \right) + g \times z_a} \quad (\text{F1})$$

The Exner functions at surface and at the forcing level are defined by:

$$1040 \quad \Pi_a = \left(\frac{P_a}{P_0} \right)^{\frac{R_a}{c_p}} \quad (\text{F2})$$

$$\Pi_s = \left(\frac{P_s}{P_0} \right)^{\frac{R_a}{c_p}} \quad (\text{F3})$$

where $P_0 = 10^5 \text{ Pa}$ and the atmospheric pressure at forcing level P_a is obtained from hydrostatism:

$$P_a = P_s - \rho_a g z_a \quad (\text{F4})$$

The saturation specific humidity at temperature T is obtained by:

$$1045 \quad q_{sat}(T, P_s) = \frac{\frac{R_a}{R_v} \times \frac{e_{sat}(T)}{P_s}}{1 + \left(\frac{R_a}{R_v} - 1 \right) \frac{e_{sat}(T)}{P_s}} \quad (\text{F5})$$

where the water vapor partial pressure at saturation $e_{sat}(T)$ is obtained from Eq. F6 which is an approximate integral of the Clausius-Clapeyron formula:

$$\begin{cases} \text{If } T \geq T_0 & e_{sat}(T) = \exp \left(\alpha_w - \frac{\beta_w}{T} - \gamma_w \ln(T) \right) \\ \text{If } T < T_0 & e_{sat}(T) = \exp \left(\alpha_I - \frac{\beta_I}{T} - \gamma_I \ln(T) \right) \end{cases} \quad (\text{F6})$$

$$1050 \quad \text{where} \quad \gamma_w = \frac{c_W - c_{P_v}}{R_v} \quad (\text{F7})$$

$$\beta_w = \frac{L_v}{R_v} + \gamma_w T_0 \quad (\text{F8})$$

$$\alpha_w = \ln(e_{sat}(T_0)) + \frac{\beta_w}{T_0} + \gamma_w \ln(T_0) \quad (\text{F9})$$

$$\gamma_I = \frac{c_I - c_{P_v}}{R_v} \quad (\text{F10})$$

$$\beta_I = \frac{L_s}{R_v} + \gamma_I T_0 \quad (\text{F11})$$

$$1055 \quad \alpha_I = \ln(e_{sat}(T_0)) + \frac{\beta_I}{T_0} + \gamma_I \ln(T_0) \quad (\text{F12})$$

$$e_{sat}(T_0) = 611.14 \text{ Pa} \quad (\text{F13})$$

The derivative $\frac{\partial q_{sat}(T, P_s)}{\partial T}$ is obtained by:

$$\frac{\partial q_{sat}(T, P_s)}{\partial T} = \frac{\partial e_{sat}(T)}{\partial T} q_{sat}(T, P_s) \times \frac{1}{1 + \frac{\frac{R_a}{R_v} - 1}{1 + \frac{R_a}{R_v} \left(\frac{1}{q_{sat}(T, P_s)} - 1 \right)}} \quad (\text{F14})$$

$$\text{where} \quad \frac{\partial e_{sat}(T)}{\partial T} = \frac{\beta_w}{T^2} - \frac{\gamma_w}{T} \quad (\text{F15})$$

1060 The Richardson number is computed by:

$$\text{Ri} = g \cos \Theta z_u^2 \frac{\theta_{v_a} - \theta_{v_s}}{0.5 (\theta_{v_a} + \theta_{v_s}) \max(U, U_{th})^2 z_a} \quad (\text{F16})$$

$$\text{where} \quad \theta_{v_a} = \frac{T_a}{\Pi_a} \left(1 + \left(\frac{R_v}{R_a} - 1 \right) q_a \right) \quad (\text{F17})$$

$$\theta_{v_s} = \frac{T_1}{\Pi_s} \left(1 + \left(\frac{R_v}{R_a} - 1 \right) q_{sat}(T_1, P_s) \right) \quad (\text{F18})$$

$$(\text{F19})$$

1065 The wet bulb temperature T_w^* (°C) is computed by Eq. F20:

$$T_w^* = \frac{\gamma \cdot T_a^* + \frac{\partial e_{sat}(T)}{\partial T} \cdot T_d^*}{\gamma + \frac{\partial e_{sat}(T)}{\partial T}} \quad (\text{F20})$$

where the slope of the saturation vapor pressure curve $\frac{\partial e_{sat}(T)}{\partial T}$ is given by Eq. F15 ; the dew point temperature T_d^* (°C) is parameterized by

$$T_d^* = [116.9 + 237.3 \ln(e)] / [16.78 - \ln(e)] \quad (\text{F21})$$

1070 and the psychrometric constant γ (in kPa K⁻¹) is obtained by:

$$\gamma = \frac{c_{P_m} \cdot P_s}{0.622 \cdot L_v} \quad (\text{F22})$$

where c_{P_m} is the specific heat capacity of moist air at constant pressure (in kJ kg⁻¹ °C⁻¹).

Appendix G: Functions in the parameterization of shear resistance

$$\left\{ \begin{array}{l} \text{If } S_i > 0.8 \text{ and } h_i \in [3, 5] : \quad C_1(d_i, S_i) = 1.05 \\ \text{else:} \end{array} \right. \quad C_1(d_i, S_i) = \begin{cases} 0.45 + 0.7S_i & \text{if } S_i < 0.25 \\ 0.625 + 1.0 \cdot (S_i - 0.25) & \text{if } 0.25 \leq S_i < 0.5 \\ 0.875 + 0.6 \cdot (S_i - 0.5) & \text{if } 0.5 \leq S_i < 0.75 \\ 1.025 + 0.5 \cdot (S_i - 0.75) & \text{if } 0.75 \leq S_i \end{cases} \quad (\text{G1})$$

$$1075 \quad C_2(d_i, S_i) = \begin{cases} 1 - 0.4\delta_i & \text{if } \delta_i < 0.25 \\ 0.9 - 0.4 \cdot (\delta_i - 0.25) & \text{if } 0.25 \leq \delta_i < 0.5 \\ 0.8 - 0.8 \cdot (\delta_i - 0.5) & \text{if } 0.5 \leq \delta_i < 0.75 \\ 0.6 - 0.6 \cdot (\delta_i - 0.75) & \text{if } 0.75 \leq \delta_i \end{cases} \quad \text{where } \delta_i = \frac{d_i \times 10^4 - 4 + S_i}{S_i - 3} \quad (\text{G2})$$

$$\left\{ \begin{array}{l} \text{If } d_i \leq (4 - S_i) \times 10^{-4} : \quad C_3(d_i, S_i) = 1 \\ \text{else:} \end{array} \right. \quad \begin{cases} \text{If } g_{s_i}(d_i, S_i)(d_i, S_i) \leq 4 \times 10^{-4} - 10^{-4}S_i : \quad C_3(d_i, S_i) = 1 \\ \text{else:} \end{cases} \quad C_3(d_i, S_i) = 1 - 530 \cdot (0.8 - 0.2s) \cdot (-4 \times 10^{-4} + g_{s_i}(d_i, S_i) + 10^{-4}S_i) \quad (\text{G3})$$

where $g_{s_i}(d_i, S_i)$ is defined by Eq. D6.

$$\left\{ \begin{array}{l} \text{If } \frac{w_i}{w_{i \max}} < 0.9 : \quad C_4(w_i, \rho_i) = \begin{cases} 1 + \frac{w_i}{w_{i \max}} & \text{if } \frac{w_i}{w_{i \max}} < 0.1 \\ 1.1 - 2.35(\frac{w_i}{w_{i \max}} - 0.1) & \text{if } 0.1 \leq \frac{w_i}{w_{i \max}} < 0.3 \\ 0.63 - 0.4(\frac{w_i}{w_{i \max}} - 0.3) & \text{if } 0.3 \leq \frac{w_i}{w_{i \max}} < 0.9 \end{cases} \\ \text{else:} \end{array} \right. \quad C_4(w_i, \rho_i) = \max(0.15, \min[0.35, (\rho_i - w_i) \times 10^{-4}]) \quad (\text{G4})$$

where $w_{i \max}(\rho_i, w_i)$ is defined by Eq. 135.

$$1080 \quad \left\{ \begin{array}{l} \text{If } h_i \in [0, 1] \text{ or } \frac{w_i}{w_{i \max}} > 0.5 : \quad C_5 = 1 \\ \text{else:} \end{array} \right. \quad \begin{cases} \text{If } w_i = 0 : \quad C_5 = 1.5 \cdot \left(\frac{1.15 + 0.2(1 - S_i)}{1.15} \right) \cdot \left(1 + \frac{0.2}{C_3(d_i, S_i)} \right) \\ \text{else:} \end{cases} \quad \begin{cases} \text{If } h_i \in [2, 3], C_5 = 1 \\ \text{else:} \end{cases} \quad C_5 = \begin{cases} 1.5 - 2 \frac{w_i}{w_{i \max}} & \text{if } \frac{w_i}{w_{i \max}} < 0.1 \\ 1.3 - 0.75(\frac{w_i}{w_{i \max}} - 0.1) & \text{if } \frac{w_i}{w_{i \max}} \geq 0.1 \end{cases} \quad (\text{G5})$$

Appendix H: MEPRA expert rules

H1 Classification of profiles

Table H1. MEPRA classification of superior profile

Condition	Type	Z_{SUP}
$\exists i : \text{PP} \in \Psi_i \text{ or } \text{DF} \in \Psi_i$	NEW	$\sum_{i=1}^j z_i + \sum_{i=j}^k z_i$ where $\begin{cases} j : \text{PP} \in \Psi_j \text{ or } \text{DF} \in \Psi_j \text{ and } (\text{PP} \notin \Psi_i \text{ and } \text{DF} \notin \Psi_i) \forall i \in [j, N] \\ k : w_i \geq 5 \forall i \in [j, k] \\ \text{and } \sum_l z_l < 0.01 \forall l \in [1, k] (w_l < 5 \text{ and } \text{MF} \in \Psi_l) \end{cases}$
$\begin{cases} \exists i : \text{MF} \in \Psi_i \text{ and } Z_i < 0.03 \\ \text{For the uppermost layer } j \text{ satisfying above condition:} \\ \theta_j < -0.2 \text{ or } w_j < 5 \end{cases}$	FRO	$\sum_{i=j}^k z_i$ where $k : \text{MF} \in \Psi_i \forall i \in [j, k]$
$\begin{cases} \exists i : \text{MF} \in \Psi_i \text{ and } Z_i < 0.03 \\ \text{For the uppermost layer } j \text{ satisfying above condition:} \\ w_j \geq 5 \end{cases}$	WET	$\sum_{i=j}^k z_i$ where $k : \text{MF} \in \Psi_i \forall i \in [j, k]$
Other cases	NAN	Undefined

Table H2. MEPRA classification of inferior profile

Condition	Type
$\mathcal{R}_{p_i} \leq 8 \forall i \in [k, l] \text{ where } l : \sum_{i=k}^l z_i \leq \frac{Z_{\text{SUP}}}{4} < \sum_{i=k}^{l+1} z_i$	SOF
$\exists i \in [k, l] : \mathcal{R}_{p_i} > 8 \text{ and } \sum_{i=k}^l z_i \leq \frac{Z_{\text{SUP}}}{4} < \sum_{i=k}^{l+1} z_i$	HAR
$Z < 1.25 Z_{\text{SUP}}$	NAN

H2 Classification of avalanche situations

The avalanche situation is classified in 6 typical classes: NEW_DRY (new snow, dry), NEW_WET (new snow, wet), NEW_MIX (new snow, mixed type), MEL_SUR (melting at surface), MEL_GRO (melting, not mainly at surface) and AVA_NAN if could not identify to an other type. The expert rules determining avalanche type from superior profile, inferior profile, temperature

and liquid water content of layers of superior profile are described in following equation:

$$\left\{ \begin{array}{l} \text{NEW} \left\{ \begin{array}{l} \text{If } w_i < 5 \forall i | Z_i \leq Z_{\text{SUP}} \rightarrow \text{NEW_DRY} \\ \text{If } w_i \geq 5 \forall i | Z_i \leq Z_{\text{SUP}} \rightarrow \text{NEW_WET} \\ \text{else} \rightarrow \text{NEW_MIX} \end{array} \right. \\ \text{WET} \left\{ \begin{array}{l} \text{HAR} \rightarrow \text{MEL_SUR} \\ \text{SOF} \rightarrow \text{MEL_GRO} \\ \text{else} \left\{ \begin{array}{l} \text{If } w_i \geq 5 \forall i | 0.1 < Z_i \leq Z_{\text{SUP}} \rightarrow \text{MEL_GRO} \\ \text{else} \rightarrow \text{MEL_SUR} \end{array} \right. \end{array} \right. \\ \text{FRO} \left\{ \begin{array}{l} \text{If } \mathcal{H}_{\text{nat}} = 0 \rightarrow \text{AVA_NAN} \\ \text{HAR} \rightarrow \text{MEL_SUR} \\ \text{SOF} \rightarrow \text{MEL_GRO} \\ \text{else} \left\{ \begin{array}{l} \left[\begin{array}{l} \text{If } w_k \geq 5 \text{ for } k | Z_k = Z_{\text{SUP}} \\ \text{and } \sum_{i=j}^k z_i > \frac{Z_{\text{SUP}}}{3} \text{ where } j | Z_{j-1} < 0.1 < Z_j \end{array} \right] \rightarrow \text{MEL_GRO} \\ \text{else} \rightarrow \text{MEL_SUR} \end{array} \right. \end{array} \right. \\ \text{NAN} \rightarrow \text{AVA_NAN} \end{array} \right. \quad (\text{H1})$$

H3 Accounting for the temporal evolution in natural hazard index

- 1090 – If at time t , superior profile is NEW but avalanche type is not NEW_MIX and if between $t - \Delta t_M$ and t , avalanche type has remained unchanged and Z and Z_{SUP} have decreased, then $\mathcal{H}_{\text{nat}}$ is updated from Table H3. The same rule is applied if avalanche type is NEW_MIX but only if the continuous wet thickness $Z_W = \sum_{i=0}^{n_W} z_i$ where $n_W | w_i > 5 \forall i \in [1, n_W]$ has decreased or remained constant since $t - \Delta t_M$.
- 1095 – If superior profile is WET or FRO at t and at $t - \Delta t_M$ and $Z - Z_{\text{SUP}}$ has not reduced by more than 0.05 m between $t - \Delta t_M$ and t :
- If $\mathcal{H}_{\text{nat}} = 3$ then it is reduced to 2
 - If superior profile is WET and $\mathcal{H}_{\text{nat}}(t) \in [4, 5]$ then:
 - If $\mathcal{H}_{\text{nat}}(t - \Delta t_M) \in [3, 4, 5]$, then $\mathcal{H}_{\text{nat}}(t) = 3$
 - If $\mathcal{H}_{\text{nat}}(t - \Delta t_M) = 1$, then $\mathcal{H}_{\text{nat}}(t) = 1$

Table H3. Update of $\mathcal{H}_{\text{nat}}$ depending on $\mathcal{H}_{\text{nat}}(t)$ as assessed from Eq. 157 and from its value at previous output time step $\mathcal{H}_{\text{nat}}(t - \Delta t_M)$. - represents an undefined value.

$\mathcal{H}_{\text{nat}}(t - \Delta t_M)$	$\mathcal{H}_{\text{nat}}(t)$						
	0	1	2	3	4	5	-
0	0	1	2	3	4	5	-
1	0	1	1	1	4	5	-
2	0	1	1	1	4	5	-
3	0	1	1	1	3	4	-
4	0	1	2	3	3	4	-
5	0	1	2	3	3	4	-
-	0	1	2	3	4	5	-

1100 H4 Equivalent natural hazard index

In Eq. 161, $\mathcal{H}_{\text{eq}}$ is designed to account for natural hazards in the assessment of the accidental hazard index. It is defined by:

$$\left\{ \begin{array}{l} \text{if } Z \geq 0.2\text{m} \left\{ \begin{array}{ll} \text{If } \mathcal{H}_{\text{nat}} \geq 4 : & \mathcal{H}_{\text{eq}} = 3 \\ \text{If } 2 \leq \mathcal{H}_{\text{nat}} < 4 : & \mathcal{H}_{\text{eq}} = 2 \\ \text{If } \mathcal{H}_{\text{nat}} = 1 : & \mathcal{H}_{\text{eq}} = 1 \end{array} \right. \\ \text{else :} & \mathcal{H}_{\text{eq}} = 1 \end{array} \right. \quad (\text{H2})$$

Appendix I: Overview of simulation results with the ESM-SnowMIP dataset

This appendix illustrates the application of Crocus 3.0.2 at the 10 ESM-SnowMIP reference sites. In-situ meteorological forcing and evaluation dataset are available from (Ménard et al., 2019). Simulations are performed with default physical options as defined in Table 1 except for the 3 BERMS forest sites (Saskatchewan, Canada) where the coupling with MEB is activated. Default values are used for all adjustable parameters as defined in Appendix K5 except for z_a and z_u which are adjusted following the site-specific metadata (Ménard et al., 2019). Simulations are compared with observations of snow depth, snow water equivalent, albedo and surface temperature at two alpine sites where all observations are available (Col de Porte, 1325 m, France, Fig. I1, and Weissfluhjoch, 2540 m, Switzerland, Fig. I2) and only with snow depth for the 8 other sites (Fig. I3-I10). The illustrations show the ability of the model to simulate contrasted stratigraphies between wet sites dominated by Melt Forms (Fig. I1, I7), cold sites dominated by Faceted Crystals or Depth Hoar (Fig. I3-I5, I9), and high-elevation sites with thick and often dry snowpacks dominated by Rounded Grains with only thin layers of Faceted Crystals (Fig. I2, I8, I10). Table I1 summarizes the model skill with scores computed following Lafaysse et al. (2017) on the 7-year periods selected for illustration. They do not exhibit any systematic bias on the evaluated variables and errors in the magnitude of other snow

Table I1. Scores of Crocus 3.0.2 simulations forced and evaluated by the ESM-SnowMIP dataset. Missing cells correspond to unavailable observations in the dataset. *N* is the number of available data considered to compute the scores. 7-year evaluation periods for all sites: 2007-2014 for Col de Porte (cdp), Weissfluhjoch (wfj), Sapporo (sap), Senator Beck (snb), Sodankyla (sod), Swamp Angel (swa) ; 2003-2010 for BERMS old aspen (oas), old black spruce (obs) and old jack pine (ojp) ; 2001-2008 for Reynolds Mountain East (rme), as in the associated illustrations (Figures I1-I10).

Site	Snow depth (cm)			Snow water equivalent (kg m ⁻²)			Albedo			Surface Temperature (K)		
	Bias	RMSE	N	Bias	RMSE	N	Bias	RMSE	N	Bias	RMSE	N
cdp	0.6	10.2	1773	-30.3	48.3	1663	0.05	0.08	768	0.6	1.7	640
wfj	-1.7	35.3	43753	-49.2	146.1	124	-0.04	0.06	1526	-0.1	2.2	3122
oas	2.3	11.2	29225	-13.6	28.4	28						
obs	2.8	6.7	42005	4.7	22.2	31						
ojp	5.5	8.9	41854	16.4	22.6	43						
rme	-7.1	16.8	45912	-33.9	66.5	45912						
sap	-5.3	10.2	30449	-50.8	66.3	192	-0.01	0.06	537	-0.6	1.4	1110
snb	39.4	47.9	1703	83.1	141.0	63	0.00	0.05	1256			
sod	-5.4	12.2	36510	-18.2	32.6	249						
swa	-23.2	29.3	1694	-118.9	141.2	96	0.03	0.07	809			

models (Menard et al., 2021). These results can be considered as a benchmark of the model skill in various environment and climate conditions. This benchmark can be useful to assess the impact of future model developments.

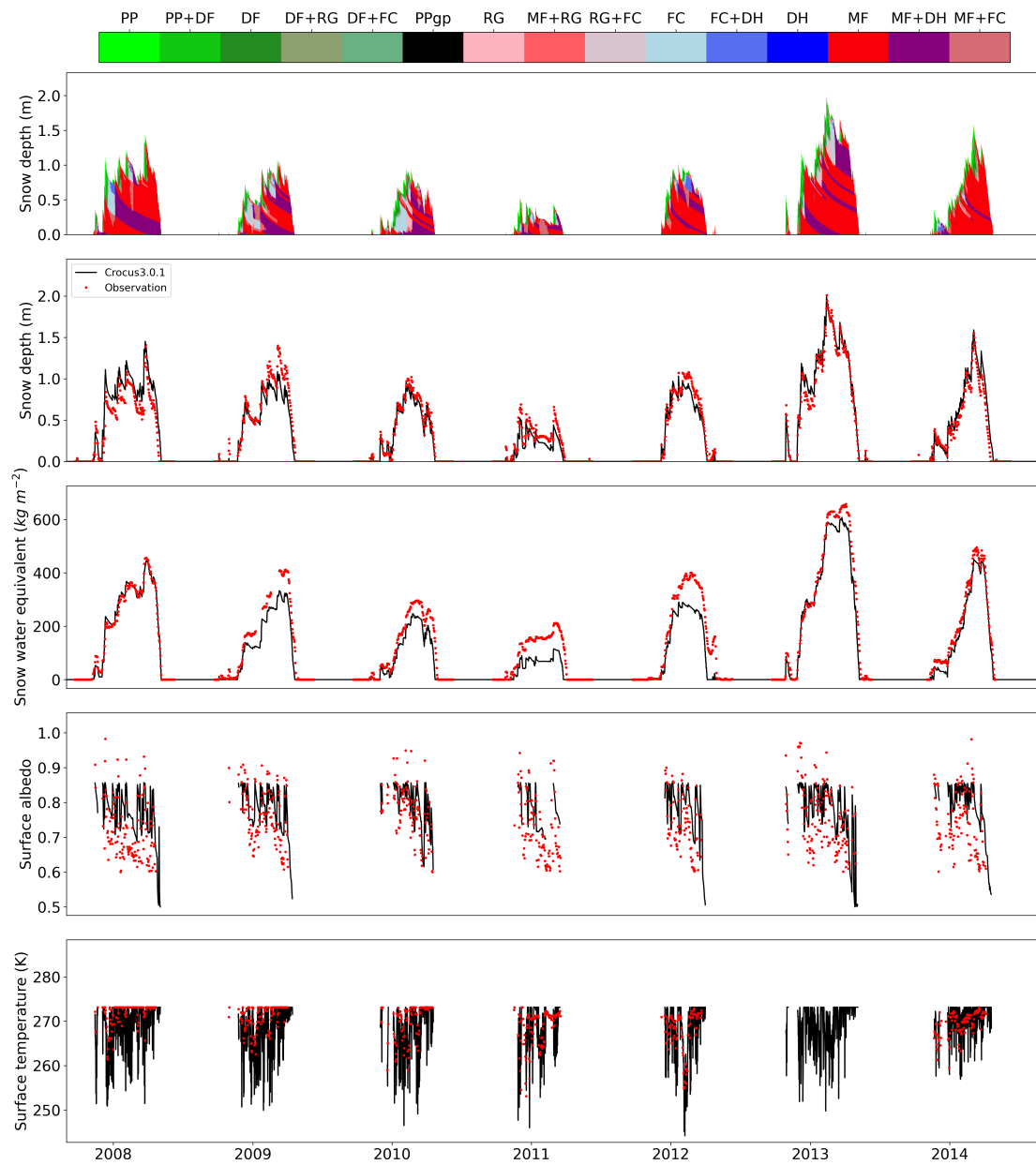


Figure 11. Illustration of Crocus simulation with ESM-SnowMIP dataset. Snow grain type, snow depth, snow water equivalent, snow surface albedo, snow surface temperature. Col de Porte, France, 2007-2014.

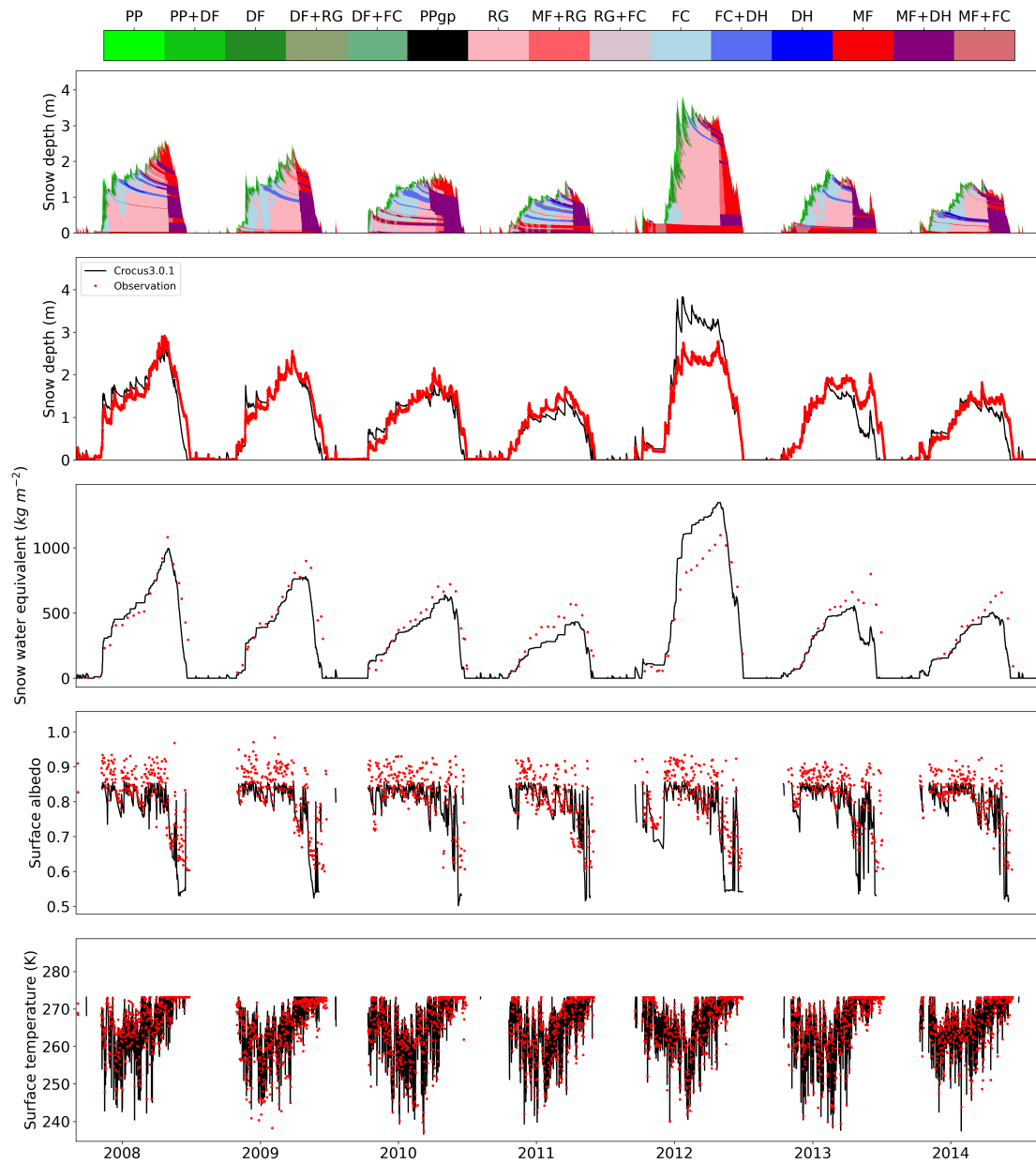


Figure I2. Illustration of Crocus simulation with ESM-SnowMIP dataset. Snow grain type, snow depth, snow water equivalent, snow surface albedo, snow surface temperature. Weissfluhjoch, Switzerland, 2007-2014.

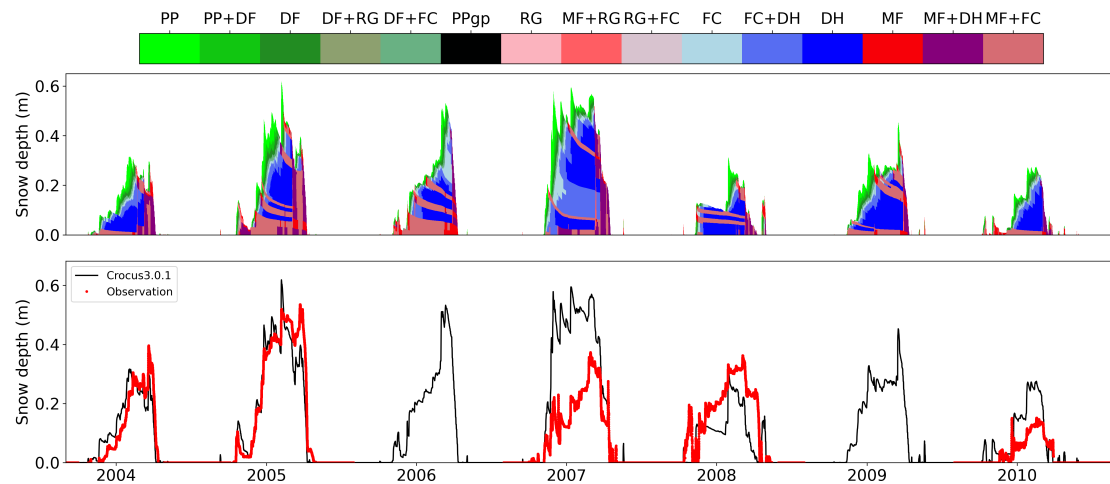


Figure I3. Illustration of Crocus simulation with ESM-SnowMIP dataset. Snow grain type, snow depth. BERMS Old Aspen, Saskatchewan, Canada, 2007-2014.

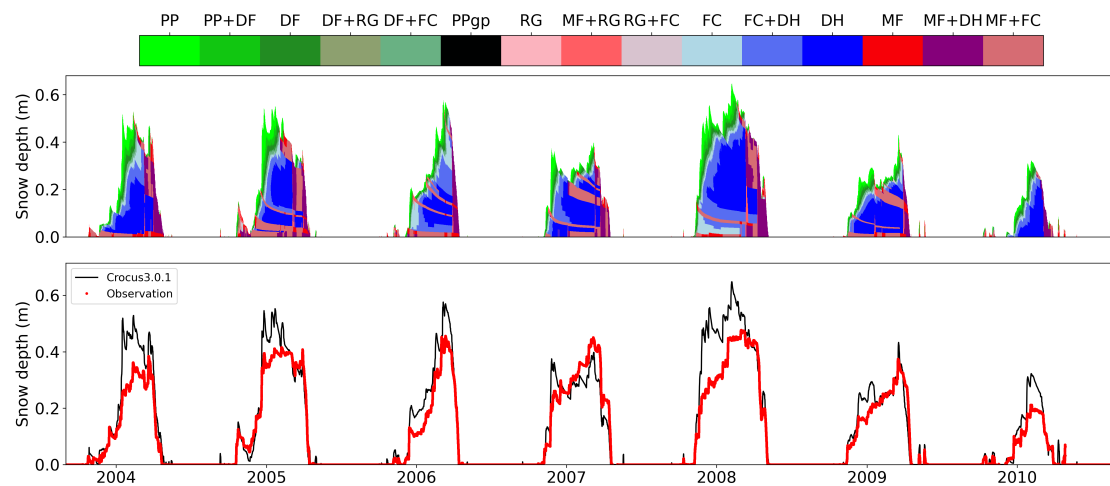


Figure I4. Illustration of Crocus simulation with ESM-SnowMIP dataset. Snow grain type, snow depth. BERMS Old Black Spruce, Saskatchewan, Canada, 2007-2014.

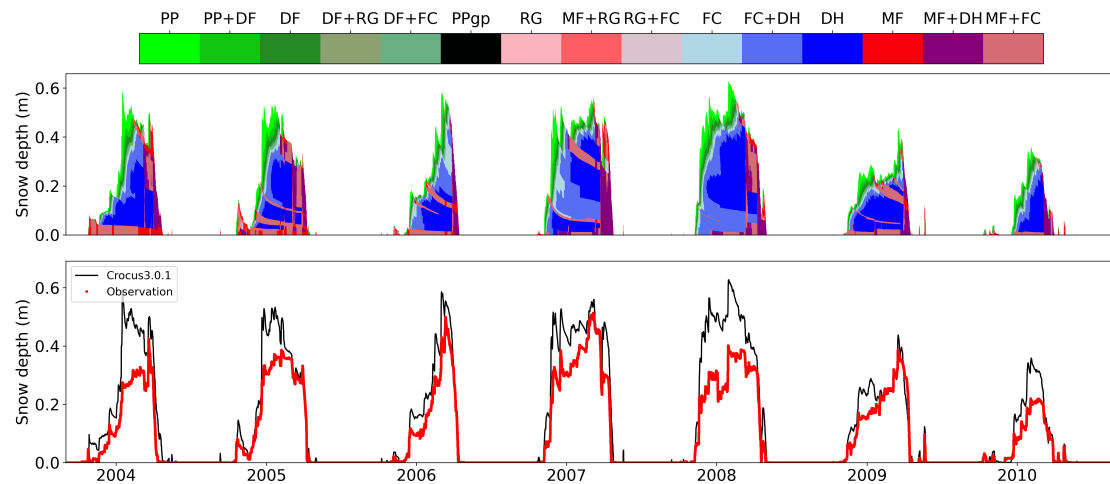


Figure 15. Illustration of Crocus simulation with ESM-SnowMIP dataset. Snow grain type, snow depth. BERMS Old Jack Pine, Saskatchewan, Canada, 2007-2014.

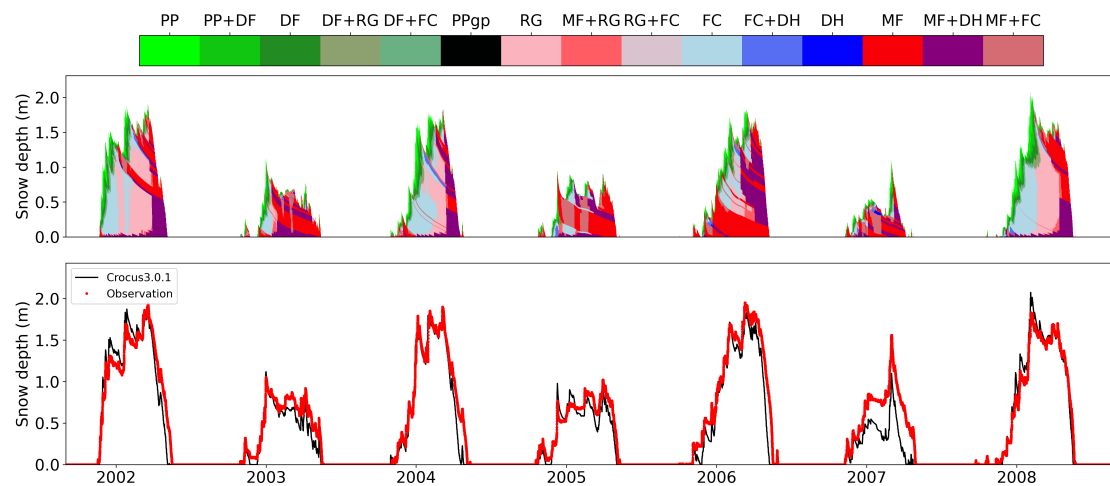


Figure 16. Illustration of Crocus simulation with ESM-SnowMIP dataset. Snow grain type, snow depth. Reynolds Mountain East, Idaho, USA, 2007-2014.

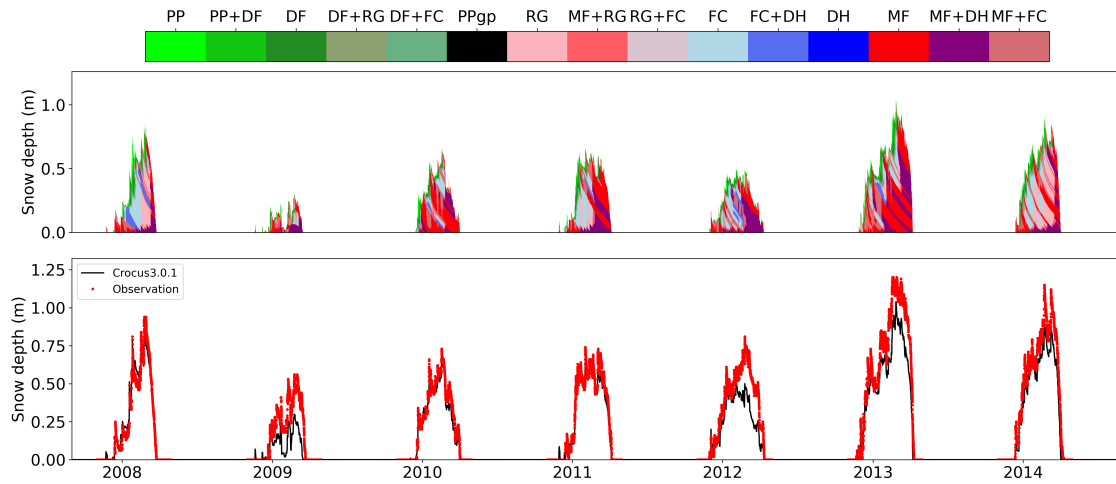


Figure 17. Illustration of Crocus simulation with ESM-SnowMIP dataset. Snow grain type, snow depth. Sapporo, Japan, 2007-2014.

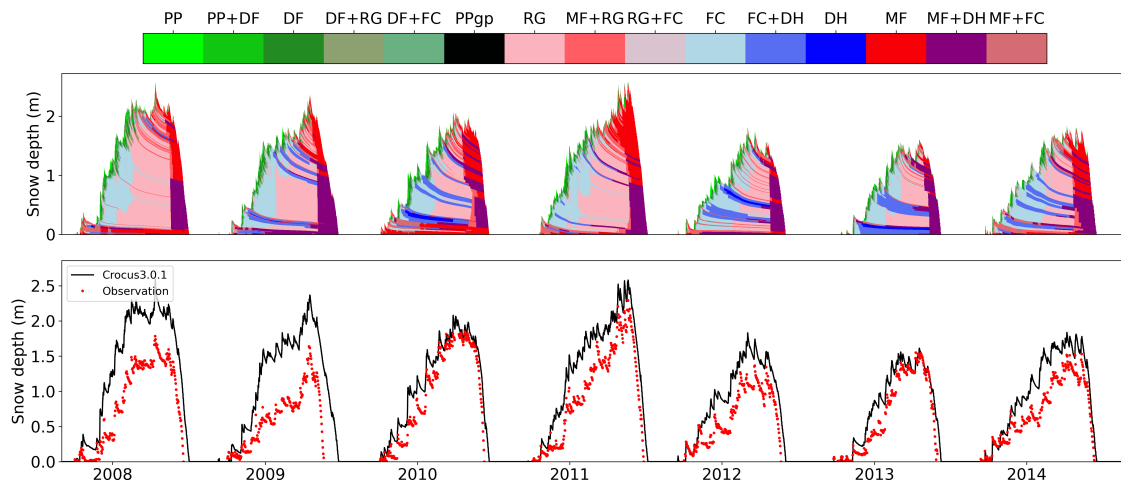


Figure 18. Illustration of Crocus simulation with ESM-SnowMIP dataset. Snow grain type, snow depth. Senator Beck, Colorado, USA, 2007-2014.

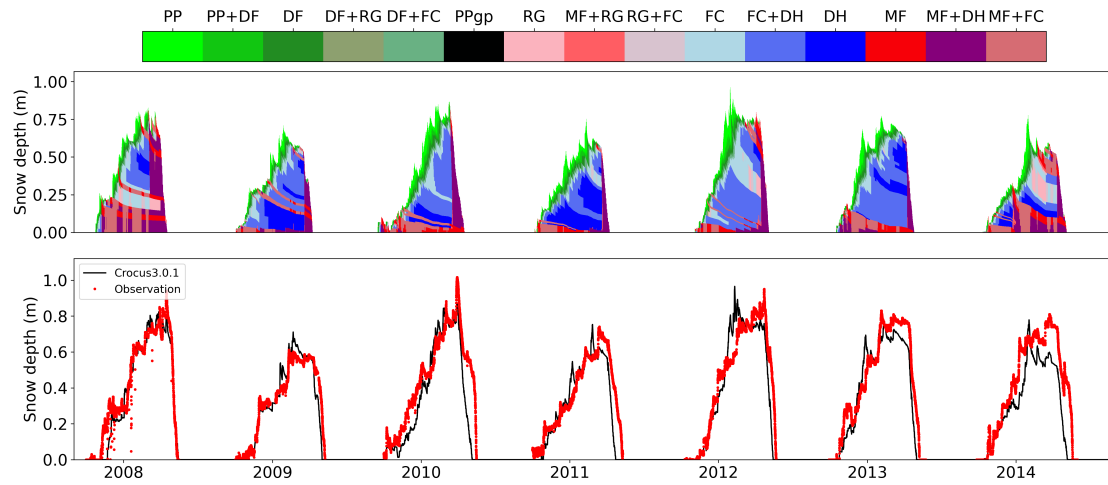


Figure 19. Illustration of Crocus simulation with ESM-SnowMIP dataset. Snow grain type, snow depth. Sodankylä, Finland, 2007-2014.

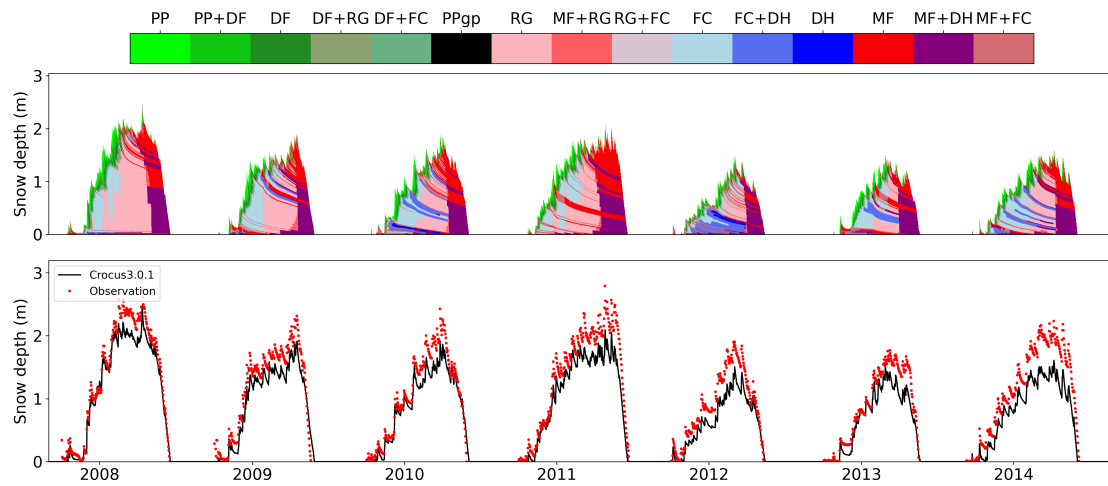


Figure 110. Illustration of Crocus simulation with ESM-SnowMIP dataset. Snow grain type, snow depth. Swamp Angel, Colorado, USA, 2007-2014.

Appendix J: Numerical efficiency of loops

All equations of this paper must be applied iteratively over all simulation points and often over all snow layers. The variable number of active snow layers N between points introduces a spatial dependence of the boundary of the loop iterator operating on snow layers. Furthermore, the maximum number of snow layers also depends on time. Several options are possible to implement these specificities, in the context where in SURFEX the leftmost dimension of arrays represent the spatial dimension, which is also the fastest varying dimension in Fortran with continuous memory storage. Without extended analyses of their numerical impact, two options were implemented in previous versions of the code. A compressed-index form (CINDX, Algorithm J1) where the loop over snow layers is inside the loop over points had been chosen by Vionnet et al. (2012) in most parts of the code. This option minimizes the number of iterations and operations as the boundary of the snow layer iterator can vary between points and dates. However, the successive accesses to the values of the arrays are not performed continuously relatively to the memory storage involving more expensive memory accesses and preventing the vectorization of computations. A full iteration with condition (FCOND, Algorithm J2) had been chosen in other parts including the heat diffusion and the TARTES optical scheme. This option does not minimize the number of iterations but still minimizes the number of operations and allows continuous memory accesses. However, it adds a potentially expensive conditional statement which still prevents vectorization. Other options could be considered. For instance, a full iteration with a predefined mask (FMASK, Algorithm J3) allows continuous memory access and vectorization. However, it adds operations on empty layers so that the interest of this approach is expected to increase with the matrices density. Note also that some operations such as divisions must be secured with this approach to avoid floating point exceptions on empty layers.

Algorithm J1 Loops with compressed index (CINDX): illustration for the computation of vertical gradient

```
for  $p \in [1, N_p]$  do
  for  $i \in [1, N(p) - 1]$  do
     $\mathcal{G}(p, i) = 2 \frac{T(p, i) - T(p, i+1)}{z(p, i) + z(p, i+1)}$ 
  end for
end for
```

Algorithm J2 Loops with full iteration with condition (FCOND): illustration for the computation of vertical gradient

```
for  $i \in [1, N_{\max} - 1]$  do
  for  $p \in [1, N_p]$  do
    if  $i \leq N(p) - 1$  then
       $\mathcal{G}(p, i) = 2 \frac{T(p, i) - T(p, i+1)}{z(p, i) + z(p, i+1)}$ 
    end if
  end for
end for
```

Algorithm J3 Loops with full iteration with mask (FMASK): illustration for the computation of vertical gradient. MASK is a precomputed array with 1 values for defined snow layers ($i \leq N$) and 0 for undefined layers ($i > N$)

```

for  $i \in [1, N_{\max} - 1]$  do
  for  $p \in [1, N_p]$  do
     $\mathcal{G}(p, i) = 2 \frac{T(p, i) - T(p, i+1)}{z(p, i) + z(p, i+1)} \times \text{MASK}(p, i)$ 
  end for
end for

```

Comparing the numerical efficiency of the whole model with these different options would represent a considerable amount of work because it would need to code all the model loops with these options. Therefore, the efficiency of these different options were only compared on simple test cases with random initialization values: the sum of a quantity over the vertical dimension (i.e. computation of total snow depth Z), the computation of the vertical gradient of a quantity (i.e. Eq. 42), the solving of a linear system with a tridiagonal matrix (i.e. Eq. 107), and finally the series of Equations to represent metamorphism (Section 2.4.5). The obtained results are presented in Table J1 and exhibit a large variability depending on the operations and matrix filling. Although, the initially implemented compressed-index method was found to be more efficient for all operations in the case of sparse matrices ($N = 12$ layers), the efficiency is highly deteriorated in case of dense matrices (N closer to 50) probably due to the discontinuous accesses to memory. The full iteration with condition has the best efficiency for simple operations.

The full iteration with mask improves the efficiency of the inversion of tridiagonal matrix compared to other methods but deteriorates the efficiency of the complex metamorphism routine with numerous conditional statements. Finally, the whole code was homogenized using a full iteration with condition (FCOND) allowing continuous memory accesses and presenting more stable computing times in the most common cases. We recommend that future developments follow the same approach, unless a dedicated efficiency performance test is able to demonstrate that an added value is obtained with another method for a specific and expensive algorithm.

Table J1. Comparison of computing time of loops based on compress-index form (CINDEX), a full iteration with condition (FCOND), and a full iteration with mask (FMASK), for 4 types of operations : Sum over the layer dimension ; Computation of vertical gradients ; Solving of a linear system with tridiagonal matrix (Eq. 107) ; and the whole metamorphism routine (Sect. 2.4.5). Tests were applied with 3 different densities of matrices (12 layers / 50 ; 50 layers / 50 ; or random values between 12 and 50 layers / 50) and with two lengths of the spatial dimension (100 points and 4000 points, adjusting the number of iterations to have the same number of computations). Tests are performed with Intel®Fortran Compiler 18.0.5 and O2 optimization level on one physical core of a 2.2 GHz AMD®Rome computing node.

Points	Layers	Iterations	Operation	CINDEX	FCOND	FMASK
100	12	4000000	Sum	2.2	4.5	6.1
100	12	4000000	Gradient	9.8	14.5	14.5
100	12	400000	Eq. 107	2.7	3.6	4.1
100	12	40000	Metamorphism	9.6	9.9	13.8
4000	12	100000	Sum	1.4	4.6	6.0
4000	12	100000	Gradient	10.2	14.6	14.7
4000	12	10000	Eq. 107	2.8	3.3	4.1
4000	12	1000	Metamorphism	9.0	10.1	13.9
100	50	4000000	Sum	9.3	4.5	6.0
100	50	4000000	Gradient	29.5	14.4	14.5
100	50	400000	Eq. 107	17.8	7.4	4.1
100	50	40000	Metamorphism	35.8	34.9	34.3
4000	50	100000	Sum	9.9	4.6	6.1
4000	50	100000	Gradient	37.4	14.5	14.7
4000	50	10000	Eq. 107	22.2	7.3	4.0
4000	50	1000	Metamorphism	34.9	35.3	35.1
100	[12-50]	4000000	Sum	5.0	4.6	6.0
100	[12-50]	4000000	Gradient	20.4	14.5	14.5
100	[12-50]	400000	Eq. 107	11.2	5.9	4.1
100	[12-50]	40000	Metamorphism	23.5	23.9	26.2
4000	[12-50]	100000	Sum	7.5	4.6	6.1
4000	[12-50]	100000	Gradient	29.6	14.6	14.7
4000	[12-50]	10000	Eq. 107	13.8	10.0	4.8
4000	[12-50]	1000	Metamorphism	23.0	24.2	28.1

Appendix K: Symbols and units

K1 Indexes

<i>Symbol</i>	<i>Description</i>
i	snow layer, $i = 1$ refers to the surface layer, increasing indexes going down
j	type of Light-Absorbing Particles
k	spectral band for solar radiation
p	simulation point (spatial dimension)

K2 Variables

<i>Symbol</i>	<i>Units</i>	<i>Description</i>
A_i	days	Age of snow layer i
C_H	-	Exchange coefficient for turbulent fluxes
d_i	m	Optical diameter of layer i
d_n	m	Optical diameter of new snow
d_{SP}	m	Optical diameter of solid precipitation
d_{BS}	m	Optical diameter of blowing snow
$D(i, i + 1)$	-	Similarity criteria between layers i and $i + 1$
$\mathcal{D}_i$	-	Driftability index of layer i
f_i	kg m^{-2}	Mass of melting for layer i during a time step
E_{FRZ}	W m^{-2}	Energy released at the surface by freezing of supercooled rain
E_i	W m^{-2}	Energy of phase change for layer i
E_{f_i}	W m^{-2}	Energy available for fusion in layer i
E_{r_i}	W m^{-2}	Energy available for refreezing in layer i
E_{k_i}	W m^{-2}	Absorbed solar radiation by layer i for spectral band k
$\mathcal{F}_i$	kg m^{-2}	Liquid water flow between layer i and $i + 1$ during a time step
$\mathcal{G}_i$	K m^{-1}	Vertical temperature gradient in layer i
G_i	W m^{-2}	Global heat flux between layers i and $i - 1$
h_i	-	Historical tracker of layer i
H	W m^{-2}	Surface turbulent sensible heat flux
H_i	J m^{-2}	Enthalpy of layer i
$\mathcal{H}_{\text{nat}}$	0-5	Natural avalanche hazard index of the simulated snow profile
$\mathcal{H}_{\text{acc}}$	0-3	Accidental avalanche hazard index of the simulated snow profile
l_i	kg m^{-2}	Mass of liquid water of layer i
K_i	W m^{-2}	Conduction heat flux between layers i and $i - 1$
LE	W m^{-2}	Surface turbulent latent heat flux
$l_{\text{inf}}, l_{\text{sup}}$	-	Adjacent layers minimizing the penalty criteria
$\text{LW}\downarrow$	W m^{-2}	Incoming atmospheric longwave radiation
m_i	kg m^{-2}	Total mass of layer i
m_n	kg m^{-2}	Mass of new snow
m_{SP}	kg m^{-2}	Mass of new solid precipitation
m_{BS}	kg m^{-2}	Mass of new blowing snow
m_{SM}	kg m^{-2}	Mass of new machine-made snow
M_X	kg m^{-2}	Mass of snow more recent than X days
$\mathcal{M}_{i,j}$	kg m^{-2}	Mass of Light-Absorbing Particles of type j in layer i
MOB_i	-	Mobility index of layer i
N	-	Number of active layers

N_p	-	Number of simulation points
n_X	-	Number of layers more recent than X days
n_r	-	Number of refrozen layers at the surface
n_w	-	Number of wet layers at the surface
$\mathcal{P}_r$	$\text{kg m}^{-2} \text{s}^{-1}$	Rainfall flux
$\mathcal{P}_s$	$\text{kg m}^{-2} \text{s}^{-1}$	Snowfall flux
P_s	Pa	Atmospheric pressure at surface
$P(i, i + 1)$	-	Penalty criteria for aggregation between layers i and $i + 1$
q_a	kg kg^{-1}	Air specific humidity at reference height z_a
$q_{sat}(T, P_s)$	kg kg^{-1}	Saturation specific humidity for temperature T and pressure P_s
r_i	kg m^{-2}	Mass of refrozen water for layer i during a time step
R_i	W m^{-2}	Shortwave radiative flux between at the interface between layers i and $i + 1$
Ri		Richardson number
$\mathcal{R}_{p_i}$	kgf	Penetration resistance of layer i
$\mathcal{R}_{s_i}$	kgf dm^{-2}	Shear resistance of layer i
s_i	kg m^{-2}	Mass of solid phase of layer i
S_i	-	Sphericity of layer i
S_n	-	Sphericity of new snow
S_{SP}	-	Sphericity of solid precipitation
S_{SP}	-	Sphericity of blowing snow
S_{nat_i}	-	Stability index of layer i for natural avalanche release
S_{acc_i}	-	Stability index of layer i for accidental avalanche release
SSA_i	$\text{m}^2 \text{kg}^{-1}$	Specific Surface Area of snow layer i
$SW_{DIR\downarrow}$	W m^{-2}	Incoming direct solar shortwave radiation
$SW_{DIF\downarrow}$	W m^{-2}	Incoming diffuse solar shortwave radiation
$SW_{\downarrow}$	W m^{-2}	Incoming total solar shortwave radiation
$SW_{k\downarrow}$	W m^{-2}	Incoming spectral shortwave radiation for band k
T_a	K	Air temperature at reference height z_a
T_a^*	$^{\circ}\text{C}$	Air temperature at reference height z_a
T_w^*	$^{\circ}\text{C}$	Wet bulb air temperature
T_d^*	$^{\circ}\text{C}$	Dew point air temperature
T_i	K	Temperature of layer i
T_{G_1}	K	Temperature of surface soil layer
U	m s^{-1}	Wind speed at reference height z_u
$U_{>1}$	m s^{-1}	Wind speed at reference height z_u with a minimum threshold of 1 m s^{-1} for the computation of turbulent fluxes
U_z	m s^{-1}	Wind speed at height z
$\mathcal{V}_{SM}$	$\text{kg m}^{-2} \text{s}^{-1}$	Water consumption for snow making
w_i	kg m^{-3}	Volumetric liquid water content of layer i
$w_{i \text{ max}}$	kg m^{-3}	Maximum liquid water holding capacity of layer i
$\mathcal{W}_{d,j}$	$\text{kg m}^{-2} \text{s}^{-1}$	Dry deposition flux for Light-Absorbing Particles of type j
$\mathcal{W}_{w,j}$	$\text{kg m}^{-2} \text{s}^{-1}$	Wet deposition flux for Light-Absorbing Particles of type j
z_i	m	Thickness of layer i
z_n	m	Thickness of new snowfall
Z_i	m	Depth of the bottom of layer i from the surface
Z_X	m	Thickness of snow more recent than X days
Z_r	m	Thickness of refrozen snow at the surface
Z_w	m	Thickness of wet snow at the surface
α_k		Spectral surface albedo for band k
β_{k_i}	m^{-1}	Absorption coefficient of solar radiation for band k and layer i
η_i	$\text{kg s}^{-1} \text{m}^{-1}$	Viscosity of layer i
θ_i	$^{\circ}\text{C}$	Temperature of layer i
Ψ_i	-	Grain type of layer i in the International Snow Classification

λ_i	$\text{W m}^{-1} \text{K}^{-1}$	Thermal conductivity of layer i
λ_{G1}	$\text{W m}^{-1} \text{K}^{-1}$	Thermal conductivity of surface soil layer
$\overline{\lambda_i}$	$\text{W m}^{-1} \text{K}^{-1}$	Integrated thermal conductivity for layers i and $i + 1$
μ	-	Cosine of solar zenithal angle
Π_a	-	Exner function at height z_a
Π_s	-	Exner function at the surface
ρ_a	kg m^{-3}	air volumetric mass
ρ_i	kg m^{-3}	Density of layer i
ρ_n	kg m^{-3}	Density of new snow
ρ_{SP}	kg m^{-3}	Density of natural snowfall
ρ_{BS}	kg m^{-3}	Density of blowing snow
σ_i	Pa	Pressure of over burden snow for layer i
σ_{GRO_i}	Pa	Static stress due to snowcat for layer i
ϕ_i	-	Porosity of snow layer i
ϕ_{FRZ}	-	Fraction of latent heat release due to the freezing of supercooled rain consumed by the heating up to T_0

1155 K3 Fixed parameters

<i>Symbol</i>	<i>Values and units</i>	<i>Description</i>
Thermodynamical and physical parameters		
c_I	$2.106 \times 10^3 \text{ J kg}^{-1} \text{ K}^{-1}$	Ice specific heat capacity
c_W	$4.218 \times 10^3 \text{ J kg}^{-1} \text{ K}^{-1}$	Liquid water specific heat capacity
c_P	$1.0047 \times 10^3 \text{ J kg}^{-1} \text{ K}^{-1}$	Dry air specific heat capacity
c_{P_v}	$1.8461 \times 10^3 \text{ J kg}^{-1} \text{ K}^{-1}$	Vapor specific heat capacity
c_{P_m}	$1.013 \times 10^3 \text{ J kg}^{-1} \text{ K}^{-1}$	Typical moist air specific heat capacity
κ_{VK}	0.4	Von Karman constant
L_m	$3.337 \times 10^5 \text{ J kg}^{-1}$	Latent heat of ice fusion
L_v	$2.5008 \times 10^6 \text{ J kg}^{-1}$	Latent heat of vaporization of liquid water
L_s	$2.8345 \times 10^6 \text{ J kg}^{-1}$	Latent heat of ice sublimation
ρ_I	917 kg m^{-3}	Volumetric mass of pure ice
ρ_w	1000 kg m^{-3}	Volumetric mass of liquid water
R_a	$287.05967 \text{ J kg}^{-1} \text{ K}^{-1}$	Specific gas constant for dry air
R_v	$461.52499 \text{ J kg}^{-1} \text{ K}^{-1}$	Specific gas constant for water vapor
T_0	273.16 K	water melting point temperature assumed to be equal to the triple point value
σ	$5.6705 \times 10^{-8} \text{ W m}^{-2} \text{ K}^{-4}$	Stefan-Boltzmann parameter
g	9.80665 m s^{-2}	Gravitational acceleration
Layering parameters		
N_{min}	3	Minimum number of snow layers
Z_{min}	0.03 m	Threshold for uniform layering
Parameters for density of new snow when SNOWFALL=V12		
ρ_{min}	50 kg m^{-3}	Minimum threshold
a_ρ	109 kg m^{-3}	Regression coefficient
b_ρ	$6 \text{ kg m}^{-3} \text{ K}^{-1}$	Regression coefficient
c_ρ	$26 \text{ kg m}^{-7/2} \text{ s}^{+1/2}$	Regression coefficient
Parameters for density of new snow when SNOWFALL=S14		
e_ρ	3.28	Empirical parameter
f_ρ	0.03	Empirical parameter

g_{ρ}	-0.36	Empirical parameter
h_{ρ}	-0.75	Empirical parameter
i_{ρ}	0.8	Empirical parameter
j_{ρ}	0.3	Empirical parameter
Parameters for density of new snow when SNOWFALL=A76		
k_{ρ}	$1.7 \text{ kg m}^{-3} \text{ K}^{-1.5}$	Regression coefficient
l_{ρ}	15 K	Regression coefficient
Parameters for metamorphism		
sph_1	11574.07 s^{-1}	Empirical parameter
sph_2	2314.81 s^{-1}	Empirical parameter
sph_3	$7.2337 \times 10^{-7} \text{ s}^{-1}$	Empirical parameter
a_s	$1.1 \times 10^{-6} \text{ m}^2 \text{ kg}^{-1} \text{ s}^{-1}$	Empirical parameter
b_s	3.1×10^{-8}	Empirical parameter
m_s	3.1	Empirical parameter
Parameters for thermal conductivity when SNOWCOND=Y81		
a_{λ}	$2.22 \text{ W m}^{-1} \text{ K}^{-1}$	Empirical parameter
$\lambda_{\min}$	$4 \times 10^{-2} \text{ W m}^{-1} \text{ K}^{-1}$	Empirical parameter
Parameters for thermal conductivity when SNOWCOND=C11		
b_{λ}	$2.5 \times 10^{-6} \text{ W m}^5 \text{ K}^{-1} \text{ kg}^{-2}$	Empirical parameter
c_{λ}	$-1.23 \times 10^{-4} \text{ W m}^2 \text{ K}^{-1} \text{ kg}^{-1}$	Empirical parameter
d_{λ}	$2.4 \times 10^{-2} \text{ W m}^{-1} \text{ K}^{-1}$	Empirical parameter
Parameters for thermal conductivity when SNOWCOND=I02		
e_{λ}	$2.0 \times 10^{-2} \text{ W m}^{-1} \text{ K}^{-1}$	Empirical parameter
f_{λ}	$2.5 \times 10^{-6} \text{ W m}^5 \text{ K}^{-1} \text{ kg}^{-2}$	Empirical parameter
g_{λ}	$-6.023 \times 10^{-2} \text{ W m}^{-1} \text{ K}^{-1}$	Empirical parameter
h_{λ}	-2.5425 W m^{-1}	Empirical parameter
i_{λ}	-289.99K	Empirical parameter
P_0	10^5 Pa	Empirical parameter
Parameters for solar radiation absorption when SNOWRAD=B92		
γ_1	0.71	Fraction of shortwave radiation in band [0.3-0.8 μm]
γ_2	0.21	Fraction of shortwave radiation in band [0.8-1.5 μm]
γ_3	0.08	Fraction of shortwave radiation in band [1.5-2.8 μm]
P_{CDP}	$8.7 \times 10^5 \text{ Pa}$	Reference atmospheric pressure at Col de Porte
Parameters for solar radiation absorption when SNOWRAD=T17		
λ_0	400 nm	Reference wavelength for dust MAE
$\text{MAE}(\lambda_0)$	$110 \text{ m}^2 \text{ kg}^{-1}$	Mass Absorption Efficiency of dust at wavelength λ_0
AAE	4.1	Angström absorption exponent for dust
ρ_{BC}	1270 kg m^{-3}	Density of black carbon
m_{BC}	1.95-0.79 i	Refractive index of black carbon
f_{BC}	1.638	Multiplicative factor to compute black carbon MAE
Parameters for Light-Absorbing Particles		
h	0.005 m	E-folding depth of the exponential decay rate for dry deposition
Parameters for compaction when SNOWCOMP=B92		
η_0	$7.62237 \times 10^6 \text{ kg s}^{-1} \text{ m}^{-1}$	Empirical parameter
a_{η}	0.1 K^{-1}	Empirical parameter
b_{η}	$0.023 \text{ m}^3 \text{ kg}^{-1}$	Empirical parameter
c_{η}	250 kg m^{-3}	Empirical parameter

Parameters for compaction when SNOWCOMP=S14		
B_S	3.96×10^{-2}	Empirical parameter
k_S	0.18	Empirical parameter
Parameters for snow drift		
a_{SUBL}	1.8×10^{-3}	Empirical parameter
b_{SUBL}	4	Empirical parameter
c_{SUBL}	2.868	Empirical parameter
d_{SUBL}	0.085	Empirical parameter
γ_{SUBL}	3.6	Empirical parameter
Parameters for percolation when SNOWLIQ=B02		
r_{min}	0.03	Mass of liquid fraction parameter in B02 parameterization
r_{max}	0.1	Mass of liquid fraction parameter in B02 parameterization
ρ_r	200 kg m^{-3}	Density parameter in B02 parameterization
Parameters for snowmaking and grooming		
$\mathcal{A}_{\text{SM}}$	3300 m^2	Surface area covered by a snowgun
$\mathcal{L}_{\text{SM}}$	0.4	Loss factor during snowmaking
d_{SM}	$2.8 \times 10^{-4} \text{ m}$	Optical diameter of machine-made snow
S_{SM}	0.9	Sphericity of machine-made snow
ρ_{GRO}	450 kg m^{-3}	Target density of groomed snow
d_{GRO}	$2.6 \times 10^{-4} \text{ m}$	Optical diameter of groomed snow
S_{GRO}	0.9	Sphericity of groomed snow
Parameters for unloading		
ρ_{UN}	200 kg m^{-3}	Density of unloaded snow
d_{UN}	$6 \times 10^{-4} \text{ m}$	Optical diameter of unloaded snow
S_{UN}	0.9	Sphericity of unloaded snow

K4 Physiographic parameters

<i>Symbol</i>	<i>units</i>	<i>Description</i>
z_{G_j}	m	Depth of soil layer j
Θ	rad	Slope angle

K5 Parameters adjustable in namelist

<i>Symbol</i>	<i>Default values and units</i>	<i>Description</i>
N_{max}	50	Maximum number of layers
Δt	900 s	model time step
ϵ	0.99	snow emissivity
Ri_l	0.026	Threshold on the Richardson number for the exchange coefficient parameterization
z_0	10^{-3} m	snow roughness for momentum
z_{0_h}	10^{-4} m	snow roughness for heat
z_a	2 m	Reference height for air temperature
z_u	10 m	Reference height for wind speed
α_{1G}	0.38	Glacier albedo in band [0.3-0.8 μm]
α_{2G}	0.23	Glacier albedo in band [0.8-1.5 μm]
α_{3G}	0.08	Glacier albedo in band [1.5-2.8 μm]

ρ_G	850 kg m ⁻³	Density threshold to separate snow and ice on glaciers
τ_a	60 days	Time constant in visible albedo parameterization
$C_{\text{scav},j}$	0	Scavenging coefficient for Light-Absorbing Particles of type j
T_{lim}	269.15 K	Snowmaking: wet but temperature threshold
U_{lim}	4.2 m s ⁻¹	Snowmaking: wind speed threshold
day ₁	November 1st	Snowmaking: day of beginning of the base-layer generation production period
day ₂	December 15th	Snowmaking: day of end of the base-layer generation production period
day ₃	March 31st	Snowmaking: day of end of the reinforcement production period
t_1	0 s (= 0am)	Snowmaking: time of beginning of the base-layer generation production period
t_2	86400 s (= 12pm)	Snowmaking: time of end of the base-layer generation production period
t_3	64800 s (= 6pm)	Snowmaking: time of beginning of the reinforcement production period
t_4	28800 s (= 8am)	Snowmaking: time of end of the reinforcement production period
p_{lim}	150 kg m ⁻²	Snowmaking: water use allowance for the base-layer generation production period
Z_{lim}	0.6 m	Snowmaking: total (natural + machine-made) snow depth threshold for the reinforcement production period
ρ_{SM}	500 kg m ⁻³	Snowmaking: machine-made snow density
a_{SM}	-0.4377 kg K ⁻¹ s ⁻¹	Snowmaking: coefficient to compute the production potential mass of lance guns
b_{SM}	-0.47 kg s ⁻¹	Snowmaking: coefficient to compute the production potential mass of lance guns
day _{END}	4, 30, 4, 30	Grooming: month and day at which grooming is stopped (without and with snowmaking, respectively)
f_{GRO}	1 day ⁻¹	Grooming: daily frequency of grooming

Code and data availability. The Crocus snowpack model is developed within the opensource SURFEX project within CeCILL-C 1.0 license (https://cecill.info/licences/Licence_CeCILL-C_V1-en.html, last access 30 March 2026). The source code of the version referred in this work can be accessed freely on https://doi.org/10.5281/zenodo.20493693 (Lafaysse et al., 2026). Obviously, the code will evolve after submission and publication. The most up-to-date stable version of Crocus can be accessed through the branch *cen* of the SURFEX_CEN git repository, currently hosted on https://github.com/UMR-CNRM/ (last access 30 March 2026). All informations to access to this repository are available on https://umr-cnrm.github.io/snowtools-doc/surfex/surfex-index.html (last access 30 March 2026). Latest developments not yet stabilized are in branch *cen_dev*. For reproductibility of results, providing a git tag is recommended in any publication based on Crocus simulations with any modification of the source code compared to the version associated with this paper. The version described in this work is tagged as *crocus3.0.2*.

The SURFEX Land Surface Model comes with a comprehensive documentation including user's guide, technical and scientific documentation available at https://www.umr-cnrm.fr/surfex, last access 30 March 2026. Nevertheless, we recommend to combine the use of SURFEX-Crocus with the snowtools_git Python3 package (Section 4.3) which includes pre and post-processing tools. Version 2.0.3 of the snowtools package was fully tested with Crocus3.0.2 and archived on https://doi.org/10.5281/zenodo.17122726 (Viallon-Galinier et al., 2025). The installation of the most up-to-date version and execution procedures are described in https://umr-cnrm.github.io/snowtools-doc/, last access 30 March 2026. It also includes informations to request technical support on registration. This documentation also includes a summarized documentation to install SURFEX-Crocus and run a first test case (https://umr-cnrm.github.io/snowtools-doc/surfex/surfex-index.html, last access 30 March 2026).

The externalized version of Crocus is also available on https://doi.org/10.5281/zenodo.20493693 (Lafaysse et al., 2026). However, model developers who intent to couple their Land Surface Model with Crocus are encouraged to access the code through the SURFEX git repository following the procedure described at https://umr-cnrm.github.io/snowtools-doc/surfex/surfex-extern.html (last access 30 March 2026). This will highly facilitate future updates of the code coming from the SURFEX implementation and allow to provide new contributions potentially useful for the whole Crocus community.

Author contributions. ML wrote the paper with contribution of all authors and has led the Crocus model development since 2012 with support of MD and SM. BDF (with major contribution), JB, KF, MB and LR read and help to fix typos in the equations and their consistency with the code. LVG wrote the description of the mechanical diagnoses and MEPRA. We only mention here the contributions to the code from the previous reference paper (2012). RN and MF undertook various technical improvements, merging and optimizations. BC and
1185 ML implemented the different multiphysics options. ML implemented TARTES within Crocus, the management of glacier configurations, and model diagnoses. ML coupled Crocus with MEB with the help of ABoo. ABoo implemented unloading from vegetation with the scientific supervision of ABoo. FT implemented light-absorbing particles with the scientific supervision of MD. PS and CC implemented machine made snow and snow grooming with the scientific supervision of SM. CC initiated the implementation of the new formalism of metamorphism with the scientific supervision of SM. MB fixed this implementation of metamorphism as described in this paper. MB and
1190 AH coupled Crocus with Snowpappus and adjusted the drift parameterizations. LQ implemented the management of ice layers after freezing rain with the scientific supervision of VV. PH implemented the MEPRA module within SURFEX. VV coupled Crocus with the SYTRON blowing snow module within SURFEX. VV coupled the externalized version of Crocus with the SVS2 platform and has frequently provided contributions to the code. GM coupled Crocus with the FSM2 platform. MM has supervised the different updates of Crocus within SURFEX. SM, MD and ML led the snow modelling team of CNRM/CEN respectively from 2009 to 2015, 2015 to 2020, and 2021 to today.

1195 *Competing interests.* The authors declare that they have no conflict of interest.

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