1 Supplement of

- 2 Surfactants Regulate the Mixing State of Organic-Inorganic Mixed
- 3 Aerosols Undergoing Liquid-Liquid Phase Separation
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- 13 Numbers of Figures: 18

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15 **Table of Contents**

- Section S1. Influence of SDS on the Mixing State of OIR = 1:4 and 4:1 Particles
- 17 **Section S2.** Surface Tension Predictions for Aqueous Systems with Decreasing RH
- 18 Section S3. Changes in SRH and ERH with Varying Initial Surfactant Concentrations
- 19 Supplementary Figures
- Figure S1. Hygroscopic growth curves for the OIR = 1:1 system without SDS (a) and
- 21 the org:sulf:SDS = 1:1:0.001 system (b). The panels display optical images
- 22 corresponding to area ratios at specific RH values. The SRH, ERH and DRH values are
- 23 indicated in red.
- 24 Figure S2. Optical images and corresponding illustrations of mixed
- 25 1,2,6-hexanetriol/AS/SDS particles with org:sulf:SDS ratios of 1:1:0.0005 (a),
- 26 1:1:0.00075 (b), 1:1:0.00125 (c), and 1:1:0.0015 (d) during LLPS, efflorescence, and
- 27 deliquescence. The RH percentage is indicated in each frame, with specific values
- 28 highlighted in red to signify the occurrence of phase transitions.
- 29 Figure S3. Optical images and corresponding illustrations of mixed
- 30 1,2,6-hexanetriol/AS particles with an OIR of 1:4 without SDS (a), and with
- org:sulf:SDS ratios of 1:4:0.007 (b) and 1:4:0.0075 (c), during LLPS, efflorescence,
- 32 and deliquescence. The RH percentage is indicated in each frame, with specific values
- highlighted in red to signify the occurrence of phase transitions.
- 34 Figure S4. Optical images and corresponding illustrations of mixed
- 35 1,2,6-hexanetriol/AS/SDS particles with org:sulf:SDS ratios of 1:4:0.008 (a) and
- 36 1:4:0.01 (b) during LLPS, efflorescence, and deliquescence. The RH percentage is
- 37 indicated in each frame, with specific values highlighted in red to signify the
- 38 occurrence of phase transitions.
- 39 Figure S5. Optical images and corresponding illustrations of mixed
- 40 1,2,6-hexanetriol/AS/SDS particles with org:sulf:SDS ratios of 4:1:0.004 (a),
- 4:1:0.0045 (b), and 4:1:0.005 (c) during LLPS, efflorescence, and deliquescence. The
- 42 RH percentage is indicated in each frame, with specific values highlighted in red to
- signify the occurrence of phase transitions.

- 44 **Figure S6.** SDS concentration evolutions predicted by the EAIM model (a) and surface
- 45 tension measurements from simulated SDS/AS mixed solutions (b) as a function of
- ambient RH for particles with org:sulf:SDS ratios of 1:1:0.001, 1:4:0.0075, and
- 47 4:1:0.0045. AS and SDS concentrations in the simulated SDS/AS solutions are derived
- 48 from EAIM predictions. Each surface tension measurement represents the average of
- 49 three replicates.
- 50 Figure S7. Optical images and corresponding illustrations of mixed
- 51 1,2,6-hexanetriol/AS/SDS particles with org:sulf:SDS ratios of 1:1:0.005 and 1:1:0.01
- 52 after LLPS and efflorescence. The RH percentage is indicated in each frame.
- 53 Figure S8. Optical images and corresponding illustrations of mixed
- 54 1,2,6-hexanetriol/AS/SDS particles with org:sulf:SDS ratios of 1:1:0.1 (a) and 1:1:1 (b)
- during LLPS, efflorescence, and deliquescence. The RH percentage is indicated in each
- frame, with specific values highlighted in red to signify the occurrence of phase
- 57 transitions.
- 58 Figure S9. Optical images and corresponding illustrations of mixed
- 59 1,2,6-hexanetriol/AS/SDS particles with org:sulf:SDS ratios of 1:1:0.001 (a), 1:1:0.005
- 60 (b), 1:1:0.2 (c), and 1:1:0.5 (d) after LLPS and efflorescence. The corresponding RH
- values during dehumidification are indicated in each frame. Note that the illustrations
- depict only the biphasic particles with identifiable mixing states.
- 63 Figure S10. Optical images and corresponding illustrations of mixed
- 64 1,2,6-hexanetriol/AS/SDS particles with an org:sulf:SDS ratio of 1:1:0.01, obtained
- from mixture solutions at pH 1.5, during LLPS, efflorescence, and deliquescence. The
- RH percentage is indicated in each frame, with specific values highlighted in red to
- signify the occurrence of phase transitions.
- 68 Figure S11. Optical images and corresponding illustrations of mixed organic/AS/SDS
- 69 particles with an org:sulf:SDS ratio of 1:1:0.01 after LLPS.
- 70 Figure S12. Optical images and corresponding illustrations of mixed
- 71 1,2,6-hexanetriol/AS/CTAC particles with org:sulf:CTAC ratios of 1:1:0.00001 (a) and
- 72 1:1:0.005 (b) during LLPS, efflorescence, and deliquescence. The RH percentage is
- 73 indicated in each frame, with specific values highlighted in red to signify the

- occurrence of phase transitions. (c) Equilibrium particle morphologies after LLPS for
- 75 1,2,6-hexanetriol/AS/CTAC particles at different initial CTAC concentrations.
- 76 Figure S13. Surface tension measurements at varying concentrations of CTAC and
- 77 SDS for simulated CTAC/AS and SDS/AS mixed solutions, with a fixed AS
- 78 concentration of 2.71 mol L⁻¹. Hollow symbols indicate estimated approximate surface
- 79 tension values.
- 80 Figure S14. Optical images and corresponding illustrations of mixed
- 81 1,2,6-hexanetriol/AS/Triton X-100 particles with varying org:sulf:Triton X-100 ratios
- after LLPS.
- 83 Figure S15. Optical images and corresponding illustrations of mixed
- 84 1,2,6-hexanetriol/AS/PFOA particles with the molar ratio of 1:1:0.1 during LLPS,
- 85 efflorescence, and deliquescence. The RH percentage is indicated in each frame, with
- specific values highlighted in red to signify the occurrence of phase transitions.
- Figure S16. Calculated spreading coefficients, S_1 and S_2 , as a function of surfactant
- 88 concentration for model systems of octane/AS (a) and octanol/AS (b) with the addition
- 89 of SDS, CTAC, or Triton X-100.
- 90 Figure S17. SRH (a) and ERH (b) values for OIR = 1:4, 1:1, and 4:1 particles with
- 91 varying initial concentrations of SDS, CTAC, and Triton X-100. The dotted lines
- 92 indicate the original SRH and ERH values for 1,2,6-hexanetriol/AS mixed particles
- 93 without surfactants.
- 94 Figure S18. Optical images of pure SDS system during an RH cycle. The RH
- 95 percentage is indicated in each frame.

S1. Influence of SDS on the Mixing State of OIR = 1:4 and 4:1

Particles

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For the particle with OIR = 1:4 without SDS, LLPS occurs via the growth of a second phase from the particle surface at RH values between 74.3% and 70.9% (Figure S3a). Following efflorescence, the organic phase becomes trapped within the cavity of the AS crystal. These scenarios are consistent with our previous observations (Ma et al., 2021a). Upon adding SDS, the LLPS mechanism changes to spinodal decomposition, as depicted in Figure S3b and S3c. During this process, schlieren patterns appear over the aqueous droplet, followed by the growth and coalescence of separated AS inclusions (Ma et al., 2021a; Ciobanu et al., 2009). Notably, as the SDS fraction increases, such as in the org:sulf:SDS = 1:4:0.0075 mixture, a core-shell morphology is no longer observed; instead, a partial engulfing structure forms (Figure S3c). Further increases in SDS concentration, seen in the 1:4:0.008 and 1:4:0.01 mixtures (Figure S4a and S4b), still result in the persistence of partial organic-phase engulfing. Figure illustrates phase transition S5 the behaviors of mixed 1,2,6-hexanetriol/AS/SDS particles with org:sulf:SDS ratios of 4:1:0.004, 4:1:0.0045, and 4:1:0.005. For the 4:1:0.004 mixture, LLPS occurs at 77.9% RH through a nucleation and growth mechanism (Ma et al., 2021a; Ciobanu et al., 2009), resulting in a core-shell particle morphology. In contrast, for the 4:1:0.0045 and 4:1:0.005 mixtures, LLPS occurs via spinodal decomposition, leading to the formation of numerous dispersed AS inclusions. Coupled with the particle morphologies observed after efflorescence, we can infer that these AS inclusions tend to reside on the particle surface, indicative of a partial engulfing structure.

It is evident that the SDS concentration threshold regulating the dominance of core-shell versus partial engulfing morphologies differs between the OIR = 1:4 and 4:1 systems compared to the OIR = 1:1 particles. To further explore this, we compare the changes in SDS concentration and surface tension with decreasing RH for the org:sulf:SDS = 1:1:0.001, 1:4:0.0075, and 4:1:0.0045 systems, as shown in Figure S6. At the SRH, the three systems exhibit distinct SDS concentrations of 2.71, 7.27, and 5.10 mM, with corresponding surface tensions of 68.49, 53.15, and 25.10 mN m⁻¹, respectively. These discrepancies imply a complex correlation between particle OIR and the surfactant concentration thresholds.

The change in total surface free energy (G_s) during spreading depends not only on the spreading coefficients (S_i) but also on the changes in surface and interface areas of the organic and inorganic phases (dA) (Torza and Mason, 1970; Shaw, 1992):

$$132 dG_{\rm S} = -S_i dA (S1)$$

Thus, while the three systems have varying concentrations of organic and inorganic phases, resulting in distinct surface and interfacial tensions during LLPS, the differences in SDS concentration thresholds can be partially attributed to different volume ratios. This is another key factor affecting total surface free energy, in addition to interfacial tensions. Similar to previous studies, our findings emphasize the importance of considering both interfacial tensions and the volumes of separated

- phases, related to particle OIR, for accurately predicting final particle morphology
- 140 (Kwamena et al., 2010).

141 S2. Surface Tension Predictions for Aqueous Systems with

142 **Decreasing RH**

- Wexler and Dutcher (2013) developed an equation based on statistical
- mechanics to describe the relationship between the surface tension (σ) of a solution
- 145 and solute activity (a_A) :

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$$\sigma = \sigma_{W} + \frac{kT}{rS_{W}} \ln \left(\frac{1 - Ka_{A}}{1 - Ka_{A}(1 - C)} \right)$$
 (S2)

- where $\sigma_{\rm W}$ is the surface tension of pure water (N m⁻¹), k is Boltzmann's constant (J
- 148 K⁻¹), T is the ambient temperature (K), and S_W is the area occupied by a water
- molecule, typically assumed to be 0.1 nm². The remaining three unknown parameters,
- 150 r, K, and C, are specific to each solute, with r representing the average number of
- water molecules displaced from the surface by each solute molecule, while K and C
- relate to sorption energies.
- For aqueous AS solution, Boyer et al. (2015) estimated values of r = -4.04 and
- K = 0.99, based on electrolyte fits using Equation (S2). Coupled with the surface
- tension of pure solute ($\sigma_S = 184.99 \text{ mN m}^{-1}$ for molten AS) (Dutcher et al., 2010), the
- parameter C is calculated as 670.39 using the formula C = 1 [1 (1 1)]
- 157 K)exp $(rS_W(\sigma_W \sigma_S)/kT)]/K$ (Wexler and Dutcher, 2013). Therefore, the surface
- tension of sulfate-containing aqueous droplets can be predicted as a function of solute
- 159 activity, which varies with decreasing RH, based on the evolution of AS
- 160 concentration.
- Dutcher et al. (2011) extended the Brunauer-Emmett-Teller (BET) and
- 162 Guggenheim-Anderson-de Boer (GAB) adsorption models to account for additional

adsorbed monolayers when determining solute and solvent activities in aqueous solutions over a wide concentration range. Assuming each solute entity is surrounded by three hydrated layers of water molecules, the solute molality (m_A) can be expressed as a function of water activity (a_W) according to the three-layer model (Dutcher et al.,

167 2011):

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$$m_{\rm A} = \left(\frac{1 - a_{\rm W} K_{\rm A}}{M_{\rm W} r_{\rm A} C_{\rm A,1} a_{\rm W} K_{\rm A}}\right) \left(\frac{1 - K_{\rm A} a_{\rm W} (1 - C_{\rm A,1}) - K_{\rm A}^2 a_{\rm W}^2 C_{\rm A,1} (1 - C_{\rm A,2})}{(1 - a_{\rm W} K_{\rm A})^2 + (2 - a_{\rm W} K_{\rm A}) a_{\rm W} K_{\rm A} C_{\rm A,2}}\right)$$
 (S3)

- The solute activity (a_A) can also be expressed as a function of water activity (a_W)
- 170 (Dutcher et al., 2011):

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$$a_{A} = \left(\frac{1 - K_{A} a_{W}}{1 - K_{A} a_{W} (1 - C_{A,1}) - K_{A}^{2} a_{W}^{2} C_{A,1} (1 - C_{A,2})}\right)^{r_{A}}$$
 (S4)

- Here, $M_{\rm W}$ is the molecular weight of water (the adsorbate) (kg mol⁻¹), $r_{\rm A}$ represents 172 173 the number of adsorption sites on solute A, while K_A , $C_{A,1}$, and $C_{A,2}$ are energy 174 parameters related to the exponent of the difference between the energy of adsorption 175 to a layer and the bulk energy of liquefaction. In Dutcher's later work, the values for the aqueous AS solution were determined to be $r_{\rm A}$ = 1.872, $K_{\rm A}$ = 0.9876, $C_{\rm A,1}$ = 176 0.0812, and $C_{\rm A,2}$ = 34.77 (Dutcher et al., 2013). Using the EAIM model, the molality 177 of aqueous AS across the entire RH range for the OIR = 1:1 system can be simulated, 178 allowing $a_{\rm W}$ and $a_{\rm A}$ at specific RH levels to be calculated using Equations (S3) and 179 180 (S4). Combined with the relationship between surface tension and solute activity in Equation (S2), the surface tension of the mixed droplets (org:sulf:SDS = 1:1:0.001) 181 182 can be predicted, considering only AS concentration changes as RH decreases.
- For the contribution of SDS to droplet surface tension, the empirical Szyskowski equation can be applied (Szyskowski, 1908):

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$$\sigma = \sigma_{W} - a \ln \left(1 + \frac{c_{SDS}}{b} \right)$$
 (S5)

where c_{SDS} is the concentration of SDS (mol L⁻¹), and parameters a and b are determined by fitting surface tension data of pure SDS solutions, measured using the hanging droplet method (Figure 3c). The evolution of SDS concentration with decreasing RH is evaluated based on the fixed molar ratio of AS to SDS.

When considering both AS and SDS contributions, the surface tension parametrization for the ternary SDS/AS aqueous solution is obtained with the modified Szyskowski equation (Prisle et al., 2010):

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$$\sigma = \sigma_{W} + \left(\frac{d\sigma_{AS}}{dc_{AS}}\right)c_{AS} - a\ln\left(1 + \frac{c_{SDS}(c_{AS} + b_2)}{b_1}\right)$$
 (S6)

As the solutions are dilute, the gradient of surface tension for aqueous AS (σ_{AS}) with respect to its molar concentration (c_{AS}), denoted by ($\frac{d\sigma_{AS}}{dc_{AS}}$), was measured to be 2.362 mN m⁻¹/mol L⁻¹ (Svenningsson et al., 2006). Surface tension depression in SDS/AS aqueous solutions was determined for fixed AS concentrations of 0, 0.1, or 1 mol L⁻¹, using the hanging droplet method (Figure 4c). The least squares method was applied to determine the optimal values of a, b_1 , and b_2 . Consequently, the surface tension can be estimated for specific AS and SDS concentrations at given RH levels, as predicted by the EAIM model.

S3. Changes in SRH and ERH with Varying Initial Surfactant

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Concentrations

205 Figure S17 illustrates the changes in SRH and ERH values for OIR = 1:4, 1:1, and 4:1 particles in the presence of surfactants (SDS, CTAC, and Triton X-100) at 206 different initial concentrations, with 1,2,6-hexanetriol and AS set at 0.1 or 0.4 mol L⁻¹. 207 208 The original SRH and ERH values for mixed particles without surfactants are 209 assumed to be 76% and 45%, respectively. As shown in Figure S17a, at relatively low 210 surfactant concentrations, surfactant molecules tended to form a thin organic layer on 211 the particle surface, inhibiting water transport across the aqueous-air interface and 212 reducing SRH values (Faust and Abbatt, 2019; Miñambres et al., 2014). For instance, 213 the SRH of OIR = 1:1 particles decreases by approximately 9.0% with the addition of 214 0.001 mM CTAC. As surfactant concentration increases, the enhanced salting-out 215 effect raises the SRH, reaching up to 90.6% RH for OIR = 1:1 particles with 100 mM 216 Triton X-100. 217 In ERH measurements, low concentrations of ionic surfactants (SDS and CTAC) reduce the ERH of mixed particles (Figure S17b). For example, 0.001 mM CTAC 218 lowers the ERH to 38.3% due to the inhibiting effect of the surface surfactant 219 220 monolayer (Harmon et al., 2010). Conversely, high concentrations of ionic surfactants 221 promote efflorescence of aqueous droplets at higher RH compared to the surfactant-free system. Considering the very high ERH of the pure SDS system 222 223 (Figure S18), we infer that the SDS efflorescence induced the heterogenous

nucleation of AS (Ma et al., 2021b). Additionally, Triton X-100 inhibits AS

- 225 efflorescence across the entire concentration range due to its lack of heterogenous
- efficacy.

Supplementary Figures

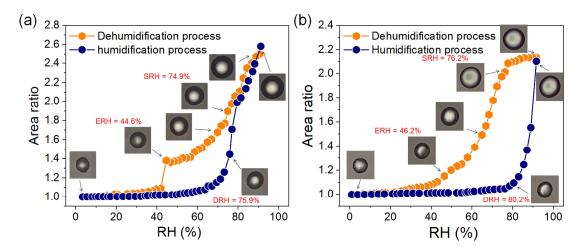


Figure S1. Hygroscopic growth curves for the OIR = 1:1 system without SDS (a) and the org:sulf:SDS = 1:1:0.001 system (b). The panels display optical images corresponding to area ratios at specific RH values. The SRH, ERH and DRH values are indicated in red.

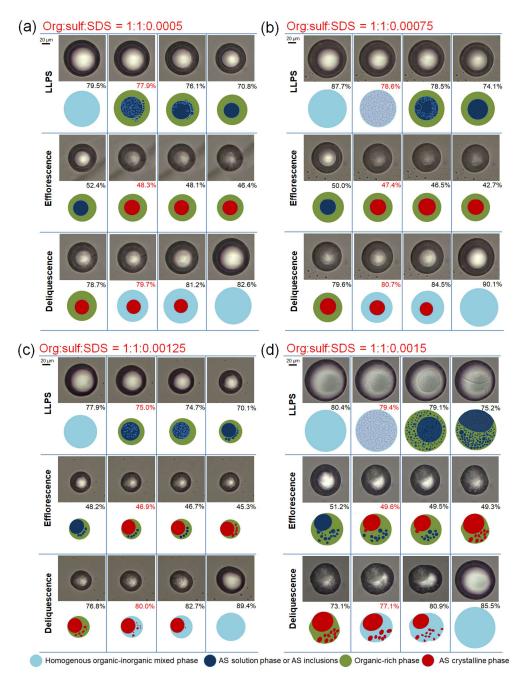


Figure S2. Optical images and corresponding illustrations of mixed 1,2,6-hexanetriol/AS/SDS particles with org:sulf:SDS ratios of 1:1:0.0005 (a), 1:1:0.00075 (b), 1:1:0.00125 (c), and 1:1:0.0015 (d) during LLPS, efflorescence, and deliquescence. The RH percentage is indicated in each frame, with specific values highlighted in red to signify the occurrence of phase transitions.

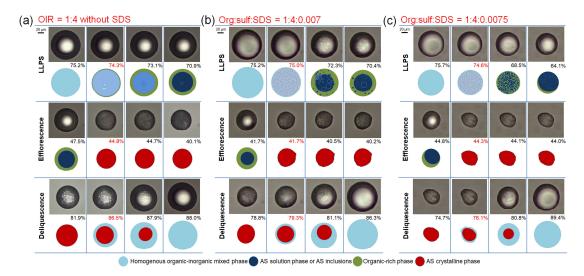


Figure S3. Optical images and corresponding illustrations of mixed 1,2,6-hexanetriol/AS particles with an OIR of 1:4 without SDS (a), and with org:sulf:SDS ratios of 1:4:0.007 (b) and 1:4:0.0075 (c), during LLPS, efflorescence, and deliquescence. The RH percentage is indicated in each frame, with specific values highlighted in red to signify the occurrence of phase transitions.

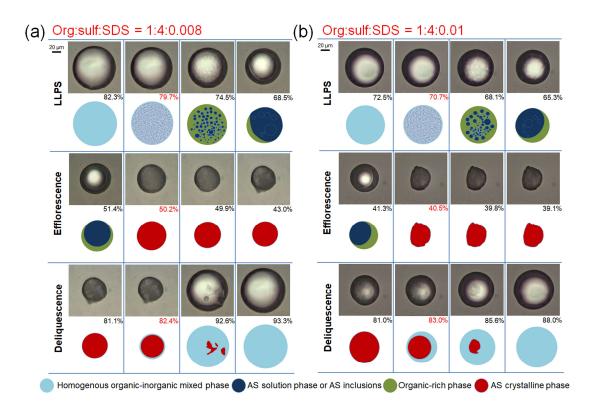


Figure S4. Optical images and corresponding illustrations of mixed 1,2,6-hexanetriol/AS/SDS particles with org:sulf:SDS ratios of 1:4:0.008 (a) and 1:4:0.01 (b) during LLPS, efflorescence, and deliquescence. The RH percentage is indicated in each frame, with specific values highlighted in red to signify the occurrence of phase transitions.

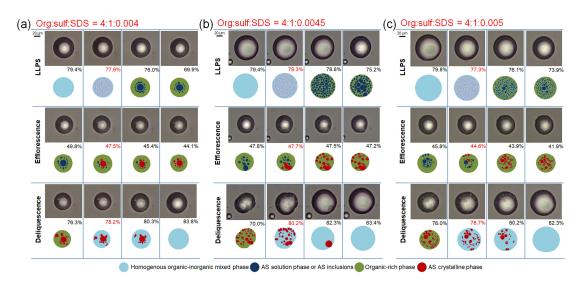


Figure S5. Optical images and corresponding illustrations of mixed 1,2,6-hexanetriol/AS/SDS particles with org:sulf:SDS ratios of 4:1:0.004 (a), 4:1:0.0045 (b), and 4:1:0.005 (c) during LLPS, efflorescence, and deliquescence. The RH percentage is indicated in each frame, with specific values highlighted in red to signify the occurrence of phase transitions.

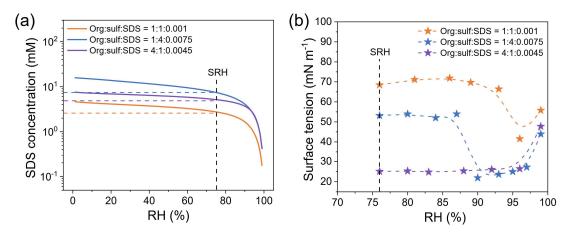


Figure S6. SDS concentration evolutions predicted by the EAIM model (a) and surface tension measurements from simulated SDS/AS mixed solutions (b) as a function of ambient RH for particles with org:sulf:SDS ratios of 1:1:0.001, 1:4:0.0075, and 4:1:0.0045. AS and SDS concentrations in the simulated SDS/AS solutions are derived from EAIM predictions. Each surface tension measurement represents the average of three replicates.

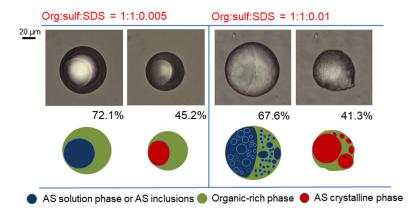


Figure S7. Optical images and corresponding illustrations of mixed 1,2,6-hexanetriol/AS/SDS particles with org:sulf:SDS ratios of 1:1:0.005 and 1:1:0.01 after LLPS and efflorescence. The RH percentage is indicated in each frame.

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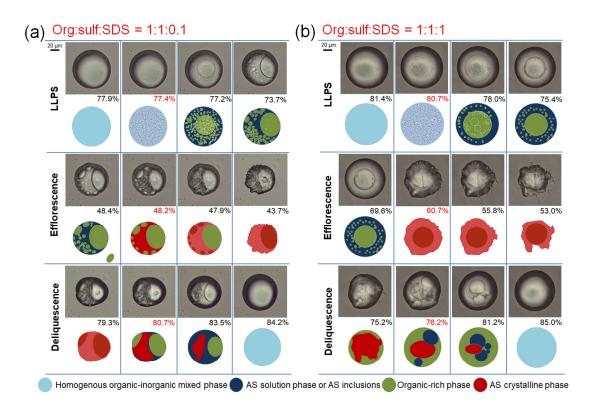


Figure S8. Optical images and corresponding illustrations of mixed 1,2,6-hexanetriol/AS/SDS particles with org:sulf:SDS ratios of 1:1:0.1 (a) and 1:1:1 (b) during LLPS, efflorescence, and deliquescence. The RH percentage is indicated in each frame, with specific values highlighted in red to signify the occurrence of phase transitions.

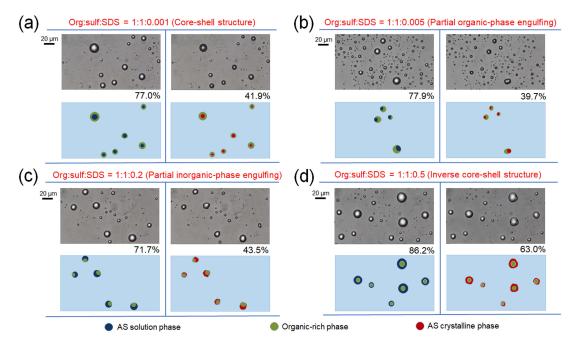


Figure S9. Optical images and corresponding illustrations of mixed 1,2,6-hexanetriol/AS/SDS particles with org:sulf:SDS ratios of 1:1:0.001 (a), 1:1:0.005 (b), 1:1:0.2 (c), and 1:1:0.5 (d) after LLPS and efflorescence. The corresponding RH values during dehumidification are indicated in each frame. Note that the illustrations depict only the biphasic particles with identifiable mixing states.

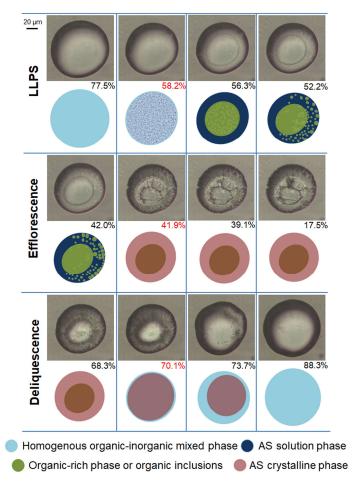


Figure S10. Optical images and corresponding illustrations of mixed 1,2,6-hexanetriol/AS/SDS particles with an org:sulf:SDS ratio of 1:1:0.01, obtained from mixture solutions at pH 1.5, during LLPS, efflorescence, and deliquescence. The RH percentage is indicated in each frame, with specific values highlighted in red to signify the occurrence of phase transitions.

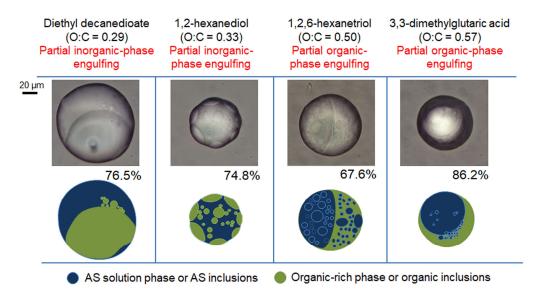


Figure S11. Optical images and corresponding illustrations of mixed organic/AS/SDS particles with an org:sulf:SDS ratio of 1:1:0.01 after LLPS.

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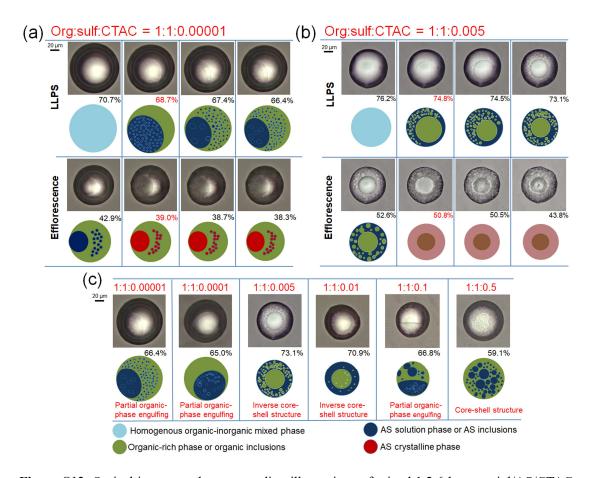


Figure S12. Optical images and corresponding illustrations of mixed 1,2,6-hexanetriol/AS/CTAC particles with org:sulf:CTAC ratios of 1:1:0.00001 (a) and 1:1:0.005 (b) during LLPS, efflorescence, and deliquescence. The RH percentage is indicated in each frame, with specific values highlighted in red to signify the occurrence of phase transitions. (c) Equilibrium particle morphologies after LLPS for 1,2,6-hexanetriol/AS/CTAC particles at different initial CTAC concentrations.

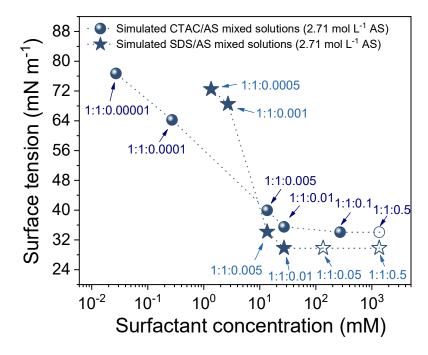


Figure S13. Surface tension measurements at varying concentrations of CTAC and SDS for simulated CTAC/AS and SDS/AS mixed solutions, with a fixed AS concentration of 2.71 mol L⁻¹. Hollow symbols indicate estimated approximate surface tension values.

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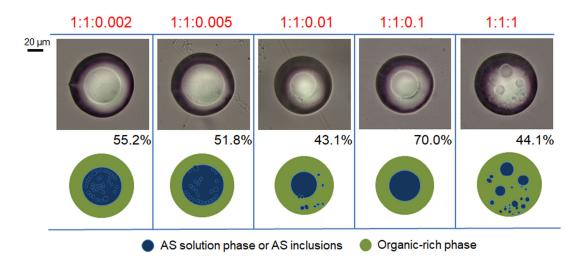


Figure S14. Optical images and corresponding illustrations of mixed 1,2,6-hexanetriol/AS/Triton X-100 particles with varying org:sulf:Triton X-100 ratios after LLPS.

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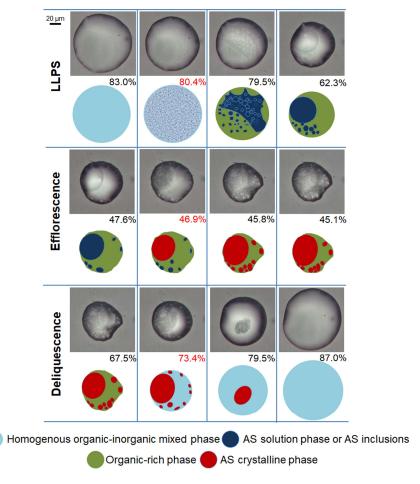


Figure S15. Optical images and corresponding illustrations of mixed 1,2,6-hexanetriol/AS/PFOA particles with the molar ratio of 1:1:0.1 during LLPS, efflorescence, and deliquescence. The RH percentage is indicated in each frame, with specific values highlighted in red to signify the occurrence of phase transitions.

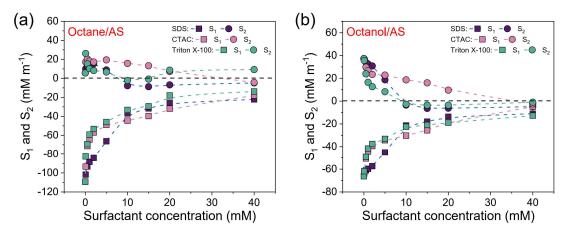


Figure S16. Calculated spreading coefficients, S_1 and S_2 , as a function of surfactant concentration for model systems of octane/AS (a) and octanol/AS (b) with the addition of SDS, CTAC, or Triton X-100.

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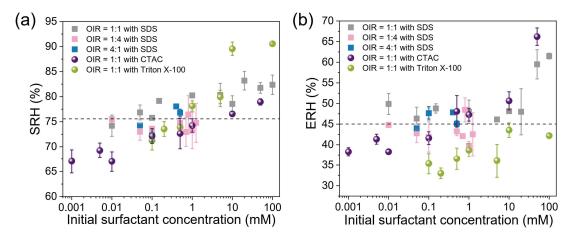


Figure S17. SRH (a) and ERH (b) values for OIR = 1:4, 1:1, and 4:1 particles with varying initial concentrations of SDS, CTAC, and Triton X-100. The dotted lines indicate the original SRH and ERH values for 1,2,6-hexanetriol/AS mixed particles without surfactants.

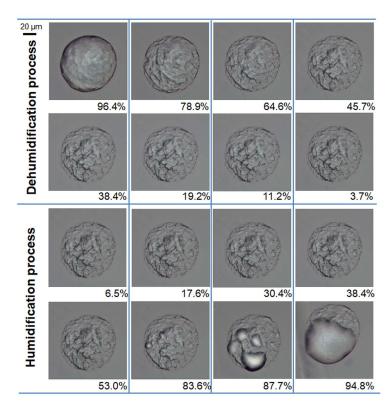


Figure S18. Optical images of pure SDS system during an RH cycle. The RH percentage is indicated in each frame.

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