



1 **Managed aquifer recharge and exploitation impacts on dynamics of groundwater level**
2 **and quality in northern China karst area: Quantitative research by multi-methods**

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17
18 **Abstract**

19 Managed aquifer recharge (MAR) is an effective way to counter groundwater level decline and
20 spring depletion caused by excessive groundwater exploitation in karst areas. However, the unique
21 characteristics of karst groundwater systems make the groundwater quantity and quality more susceptible
22 to human activities, posing challenges for MAR research. This research employed multi-methods
23 including numerical simulations, isotope analysis, infiltration tests, flow monitoring and tracer tests to
24 quantitatively analyze the impacts of MAR and groundwater exploitation on the dynamics of



25 groundwater level and quality in a typical northern China karst area, the Baotu Spring area in Jinan
26 City. First, the percentage of surface water recharge in karst groundwater was calculated using isotope
27 data with the improved two-end-member mixing model. Next, the quantitative relationship between
28 volume of released water and actual recharge was established with data from infiltration tests and flow
29 monitoring. Then, the actual groundwater flow velocity and effective porosity of the karst aquifers were
30 calculated with former tracer test isochrone maps. Finally, the impacts of MAR and groundwater
31 exploitation on dynamics of groundwater level and quality were quantitatively analyzed with a
32 groundwater flow-solute transport model for the area. The results indicate that the MAR and groundwater
33 exploitation in the Baotu Spring area have significantly impacted karst groundwater levels and quality.
34 These complementary methods enhance the accuracy of decisions in MAR and groundwater exploitation.

35 **Keywords:** Managed aquifer recharge (MAR); Karst groundwater; Quantitative analysis; Multi-methods.

36 1. Introduction

37 Managed aquifer recharge (MAR) (Sherif et al., 2023), refers to the intentional recharge of aquifers
38 to address the ecological and environmental geological issues caused by excessive groundwater
39 exploitation (Aeschbach-Hertig & Gleeson, 2012; Foley et al., 2011). It has been demonstrated that
40 appropriate recharge can effectively elevate groundwater levels and improve groundwater quality to
41 some extent (Ajur & Baalousha, 2021; Alam et al., 2021; Standen et al., 2020).

42 Karst groundwater is a crucial component of water resources (Hartmann et al., 2014; Medici et al.,
43 2021). The research of MAR in karst areas has become a prominent focus in recent years (J. Li et al.,
44 2023; Zhang & Wang, 2021). However, the unique characteristics of karst groundwater systems make
45 the groundwater quantity and quality more susceptible to human activities (Allocca et al., 2014; Lorenzi
46 et al., 2024), posing challenges for MAR research. Due to the highly heterogeneous nature of karst



47 development, the actual effectiveness of MAR varies significantly across different locations (Daher et
48 al., 2011). The impact of recharge on the karst groundwater level and quality at different locations and
49 using various water sources shows significant variation. Additionally, the fast karst groundwater flow
50 (Bakalowicz, 2005) leads to extensive catchment areas for karst groundwater exploitation wells, and
51 over-exploitation would create large-scale groundwater level drawdown cones, causing secondary
52 geological hazards (Jiang et al., 2019). Moreover, if poor-quality source water were used for MAR,
53 pollutants would quickly spread downstream (H. Cao et al., 2023), severely threatening the quality of
54 karst groundwater (Xanke et al., 2017). Therefore, quantitatively assessing the effects of MAR and
55 groundwater exploitation on the quantity and quality of karst groundwater will facilitate stable, efficient,
56 and safe aquifer recharge and groundwater exploitation.

57 There are some relatively mature research methods regarding the effects of MAR and groundwater
58 exploitation on groundwater level and quality (Ringleb et al., 2016). However, most of these methods
59 are either qualitative or semi-quantitative. Hydrogeochemical and isotope methods are commonly used
60 in MAR studies (Akurugu et al., 2022; M. Li et al., 2023). By monitoring the changes in groundwater
61 quality before and after the recharge, the impact of MAR on groundwater quality can be qualitatively
62 analyzed. A primary issue with hydrogeochemical analysis is that its conclusions may be ambiguous, as
63 potential unknown sources of groundwater contamination could interfere with the results. In addition,
64 isotopes in groundwater are often used to identify recharge sources. By combining multiple
65 hydrochemical and isotopic indicators (Guo et al., 2019), the proportion of various recharge sources
66 contributing to groundwater can be estimated (Deng et al., 2022). However, in many cases, due to the
67 inability to accurately determine the isotopic values for each recharge source, this method can only
68 provide a rough estimate. Furthermore, due to the typical lack of long-term monitoring data on



69 groundwater isotopes, this approach is unsuitable for studying the dynamics in the effects of MAR on
70 groundwater.

71 Numerical simulation is a powerful tool for quantitative research of MAR ([Ghasemizadeh et al.,](#)
72 [2012](#); [Medici et al., 2021](#); [Ostad-Ali-Askari & Shayannejad, 2021](#)). The Equivalent Porous Medium
73 (EPM) model, represented by MODFLOW, is suitable for simulating laminar groundwater flow that
74 adheres to Darcy's law ([Jourde & Wang, 2023](#); [Ringleb et al., 2016](#)). In karst regions with low
75 development, such as the karst areas in northern China, groundwater flow is predominantly laminar,
76 largely complying with Darcy's law ([Chuanlei Li et al., 2022](#)). Therefore, the EPM model without
77 inserting karst-conduits embedded is well-suited for application in these regions ([Kang et al., 2011](#); [J. Li](#)
78 [et al., 2023](#); [Luo et al., 2020](#); [Scanlon et al., 2003](#)).

79 When conducting MAR studies using numerical simulation methods, accurately determining the
80 actual groundwater recharge volume is a crucial condition for ensuring the accuracy of the simulation
81 results. In the studies of MAR primarily driven by riverbed infiltration, methods such as riverbed
82 infiltration tests and river flow monitoring can be employed. By applying the principles of groundwater
83 dynamics and water balance, the actual surface water recharge to groundwater can be quantitatively
84 calculated.

85 Furthermore, it has been indicated that when using the EPM model for simulating solute transport
86 in karst groundwater, properly estimating the effective porosity of karst aquifers is critically important
87 ([Kidmose et al., 2023](#); [Ren et al., 2018](#)). Overestimating the effective porosity often results in a severe
88 underestimation of the actual groundwater velocity, leading to significant errors in karst groundwater
89 pollution control measures ([Medici & West, 2021](#); [Medici et al., 2019](#)). Therefore, to ensure the effective
90 application of the EPM model in groundwater solute transport simulating, it is advisable to consider



91 estimating the effective porosity of the karst aquifer medium using the actual groundwater flow velocity
92 calculated from tracer tests ([Worthington et al., 2019](#); [Zhu et al., 2020](#)).

93 In MAR studies conducted in actual regions, the results of various methods mentioned above can
94 be cross-validated to reduce the uncertainty caused by data scarcity or insufficient investigation, thereby
95 improving the accuracy of quantitative research related to MAR.

96 The Baotu Spring area in Jinan City is a typical representative of the karst areas in northern China
97 ([Liang et al., 2018](#)), with karst groundwater serving as one of the crucial water supply sources. In the
98 past decades, the increasing demand for water resources in Jinan has led to excessive groundwater
99 exploitation, causing a decline in groundwater levels and the drying up of springs ([Gao et al., 2023](#);
100 [Changsuo Li et al., 2022](#)). In order to balance the needs of water supply and spring protection, Jinan City
101 has implemented the project of MAR using the diverted water from the Yellow River ([Kang et al., 2011](#))
102 and the Yangtze River from the South-to-North Water Transfer Project ([Liu et al., 2020](#)) in recent years.
103 Studies have shown that there is a close hydraulic connection between surface water and karst
104 groundwater in certain reaches of the Yufu River and Xingji River, making them ideal sites for
105 implementing the MAR project ([J. Li et al., 2023](#)). However, when the flow of Yufu River is excessively
106 high, a portion of the flow downstream and cannot recharge the karst groundwater. Moreover, the
107 concentration of some hydrochemical components in the diverted water may be higher than those of the
108 local karst groundwater ([X. Cao et al., 2023](#); [J. Li et al., 2023](#); [Zheng et al., 2020](#)), and thus long-term
109 use of lower-quality water for recharge may lead to continuous deterioration of karst groundwater quality
110 ([J. Li et al., 2023](#); [Zhang & Wang, 2021](#)).

111 Therefore, to ensure the stability of the karst groundwater level and the long-term safety of water
112 quality, and to guarantee the sustainable exploitation of groundwater resources, the purpose of this

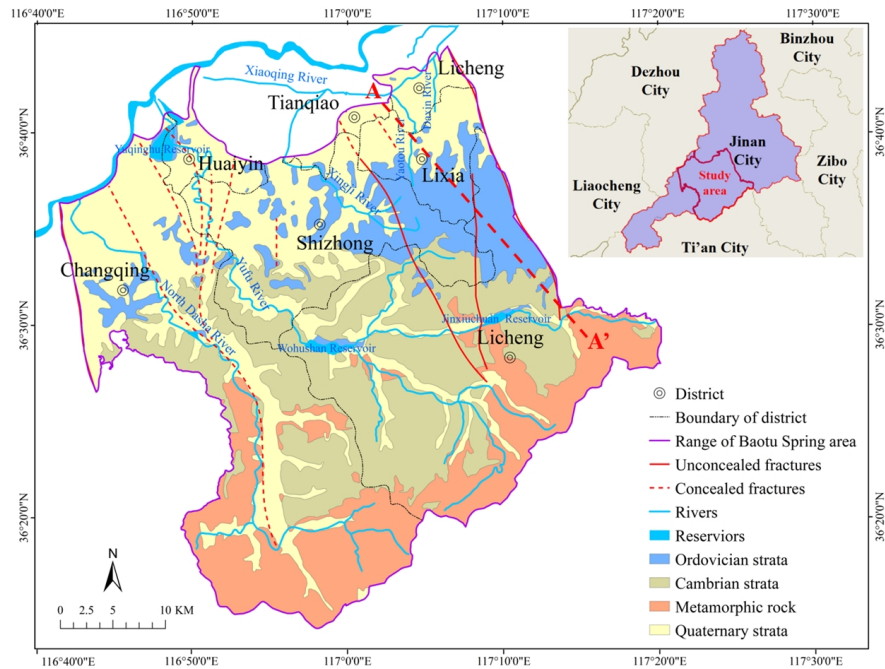


113 research is to quantitatively analyze the impacts of MAR and groundwater exploitation on the dynamics
114 of karst groundwater level and quality in the Baotu Spring area of Jinan City by multi-methods. The
115 method employed in this study primarily focuses on the numerical simulation of coupled groundwater
116 flow and solute transport. Complementary techniques such as isotope analysis, infiltration tests, flow
117 monitoring, and tracer tests are also utilized to enhance the accuracy of the numerical simulations.

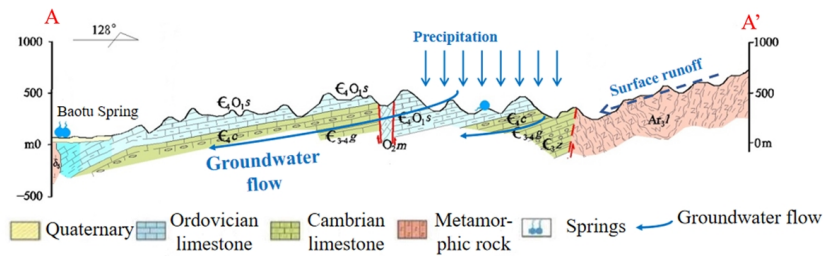
118 **2. Material and methods**

119 **2.1. Study area**

120 The study area of this paper is the Baotu Spring area, located in Jinan City, Shandong Province,
121 China, covering about 1,654 km² (Niu et al., 2021; Sun et al., 2013) (Fig.1). The terrain of Baotu Spring
122 area is higher in the south and lower in the north, with rolling steep mountains and deep canyons in
123 the south, low mountains and hills in the middle, and Piedmont inclined plains and alluvial plains
124 in the north. The Baotu Spring area is located in the mid-latitude inland area with a warm temperate
125 continental climate. The average annual precipitation from 1951 to 2023 is 690.4 mm, mostly falling
126 between June and September (accounting for 77% of the total), and southern mountainous areas receive
127 more precipitation than northern plains.



(a) Geological map



(b) Hydrogeological profile

Fig.1 Geological map and hydrogeological profile of Baotu Spring area

The main rivers in this region are the Yellow River, Yufu River, and Beisha River (Fig.1). The Yellow River forms the study area's northwestern boundary and is mainly used for agricultural irrigation and groundwater recharge. The Yufu River is a seasonal tributary of the Yellow River, and the reaches between Zhaiertou and Cuima Villages has excellent permeability, making it an ideal river for MAR (Guo et al., 2019; J. Li et al., 2023) (Fig.2). Additionally, the Xingji River in the northeast, though small,



138 also has a permeable riverbed making it suitable for MAR (Fig.2).

139 The stratigraphic units exposed in the study area from south to north, listed from oldest to youngest,
140 are as follows: Archaean Taishan Group metamorphic rocks, Cambrian limestone, Ordovician limestone,
141 and Quaternary loose sediments (Fig.1). The exploitable karst groundwater is stored in the Zhangxia
142 Formation of the middle Cambrian, the Chaomidian Formation of the upper Cambrian, and the Majiagou
143 Formation of the Ordovician. In the northern mountainous and hilly areas, karst groundwater is recharged
144 by precipitation and surface water, flowing northward along strata dips (Zhu et al., 2020). In the northern
145 piedmont alluvial plain, the karst aquifer is buried under Quaternary sediments. Large gabbro intrusions
146 from the late Mesozoic block the northward flow, causing the water to rise along fractures and form
147 springs (Niu et al., 2021; Wang et al., 2022), with Baotu Spring being the most popular of them (Guo et
148 al., 2019).

149 In addition, only few of the groundwater exploiting wells in the study area are still under
150 exploitation, which could be categorized into three groups (western suburbs wells, western Jinan
151 wells and eastern suburbs wells) based on the locations. Most of the MAR in the study area is
152 conducted along certain river reaches of the Yufu River and Xingji River, while a small portion of the
153 MAR is carried out through specific wells in the urban area (which are no longer used for exploitation
154 and are now solely dedicated to MAR) (Wang et al., 2017). The locations of all these exploiting wells,
155 MAR wells, and MAR river reaches are marked in Fig.2.

156 **2.2. Groundwater sampling and analysis**

157 In the study area, surface water is the primary source of MAR. In order to understand the current
158 water quality status of karst groundwater and surface water in the study area, identifying the
159 hydrochemical components in surface water that may influence groundwater quality, estimate the



percentage contribution of surface water and precipitation recharge to karst groundwater, and to provide a basis for the groundwater flow and solute transport model setup, sampling and analysis of groundwater and surface water in the study area were conducted in June 2022. The analyzed indicators included total dissolved solids (TDS), sulphate concentration, nitrate concentration, chloride concentration, $\delta^2\text{H}\%$, and $\delta^{18}\text{O}\%$. The locations of the sampling points are shown in Fig.2.

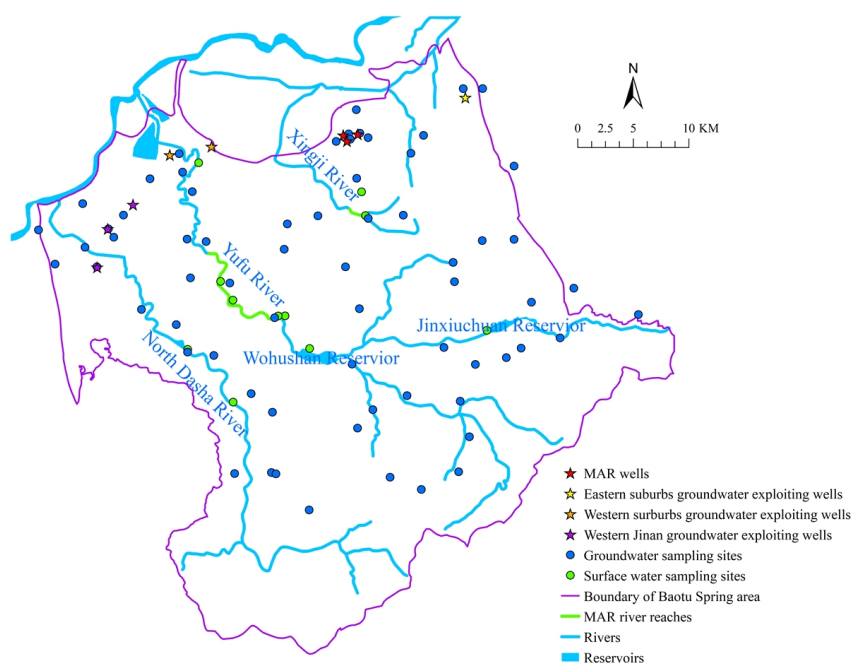


Fig.2 Locations of wells and sampling sites

After the analysis of groundwater and surface water samples, the origin and recharge sources of karst groundwater were determined by utilizing the $\delta^2\text{H}\%$ and $\delta^{18}\text{O}\%$ scatter plot of groundwater and surface water. The analysis of ^2H and ^{18}O requires referencing the Global Meteoric Water Line (GMWL) and the Local Meteoric Water Line (LMWL). The GMWL is given as (Craig, 1961):

$$\delta^2\text{H}=8\delta^{18}\text{O}+10 \quad (1)$$

Using the China Meteoric Water Line (CWML) as the LWML for the study area, which is:



$$\delta^2\text{H} = 7.7\delta^{18}\text{O} + 7 \quad (2)$$

Then, to quantitatively analyze the impact of MAR from surface water on karst groundwater, $\delta^2\text{H}\text{‰}$ and $\delta^{18}\text{O}\text{‰}$ values were used to determine the proportion of groundwater recharge from surface water. Groundwater in the study area has two main recharge sources: surface water and precipitation (Liu et al., 2021). An improved two-end-member mixing model was employed to calculate the mixing ratios of surface water and precipitation in groundwater samples. Assuming $\delta^2\text{H}\text{‰}$ and $\delta^{18}\text{O}\text{‰}$ values for surface water are x_s and y_s , for precipitation are x_p and y_p , and for groundwater are x_g and y_g , the mixing ratios from surface water (η_s) and precipitation (η_p) were calculated. The traditional two-end-member mixing model uses either $\delta^2\text{H}\text{‰}$ or $\delta^{18}\text{O}\text{‰}$ data to calculate these ratios with the formula:

$$\begin{cases} \eta_s = \frac{x_g - x_p}{x_s - x_p} \\ \eta_p = \frac{x_s - x_g}{x_s - x_p} \end{cases} \quad (3)$$

Or:

$$\begin{cases} \eta_s = \frac{y_g - y_p}{y_s - y_p} \\ \eta_p = \frac{y_s - y_g}{y_s - y_p} \end{cases} \quad (4)$$

For some samples, the mixing ratios calculated using formula (3) or (4) differ significantly. This paper proposes a method that calculates the mixing ratio by projecting groundwater sample points onto the precipitation-surface water mixing line in a $\delta^2\text{H}\text{‰}$ - $\delta^{18}\text{O}\text{‰}$ diagram. The derived formula for calculating the mixing ratio is as follows:

$$\begin{cases} \eta_s = \frac{(x_g - x_p)(x_s - x_p) + (y_g - y_p)(y_s - y_p)}{(x_s - x_p)^2 + (y_s - y_p)^2} \\ \eta_p = \frac{(x_s - x_g)(x_s - x_p) + (y_s - y_g)(y_s - y_p)}{(x_s - x_p)^2 + (y_s - y_p)^2} \end{cases} \quad (5)$$

In this research, the minimum $\delta^2\text{H}\text{‰}$ and $\delta^{18}\text{O}\text{‰}$ values of karst groundwater samples are considered as the values of precipitation recharge end-members, which are -64.56 and -9.30, respectively. The average $\delta^2\text{H}\text{‰}$ and $\delta^{18}\text{O}\text{‰}$ values of surface water samples are considered as the values of surface water recharge end-members, which are -50.53 and -6.815, respectively. Using formula (5), the mixing ratio



194 for all karst groundwater samples could be calculated.

195 **2.3. Infiltration test and flow monitoring of rivers**

196 To investigate the infiltration capacity of an MAR river reach, we selected five equidistant sites
197 along the MAR reach of Yufu River and measured the permeability coefficient of the riverbed based on
198 in-situ double-ring infiltration test (Li et al., 2019) (Fig.3). Then, the infiltration coefficient of the Yufu
199 River MAR reach was calculated using the double-ring infiltration test results. The theoretical maximum
200 recharge capacity was then determined based on the river's area.

201 Additionally, the flow monitoring data from multiple reaches of the Yufu River and Xingji River
202 from 2014 to 2016 were collected (Fig.3). According to the principle of water balance, the difference in
203 flow between the cross-sections of the MAR river reach is considered as the actual infiltration recharge
204 volume. For Yufu River, the water is released in Section #1, and the actual infiltration recharge volume
205 equals the difference between the flow rate at Section #1 and Section #5. For Xingji River, the water is
206 released in Section #6, and the actual infiltration recharge volume equals the difference between the flow
207 rate at Section #6 and Section #7. Then, based on the statistical data of the released water volume, the
208 quantitative relationship between the released water volume and the actual recharge volume is analyzed.

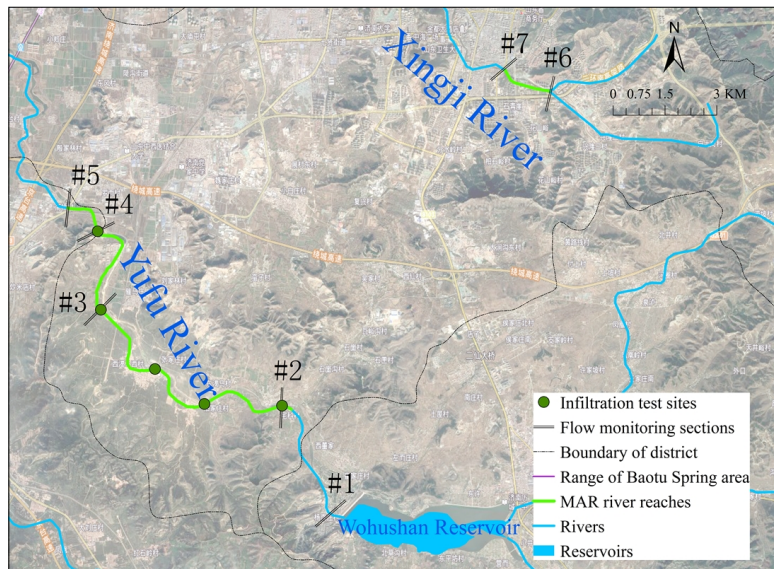


Fig.3 Infiltration test sites and flow monitoring sections

2.4. Estimation of effective porosity from tracer tests

Effective porosity is a crucial parameter for simulating groundwater solute transport. The actual groundwater velocity determined by tracer tests can be used to calculate the effective porosity of karst fractured aquifers (Zuber & Motyka, 1994), using the following formula:

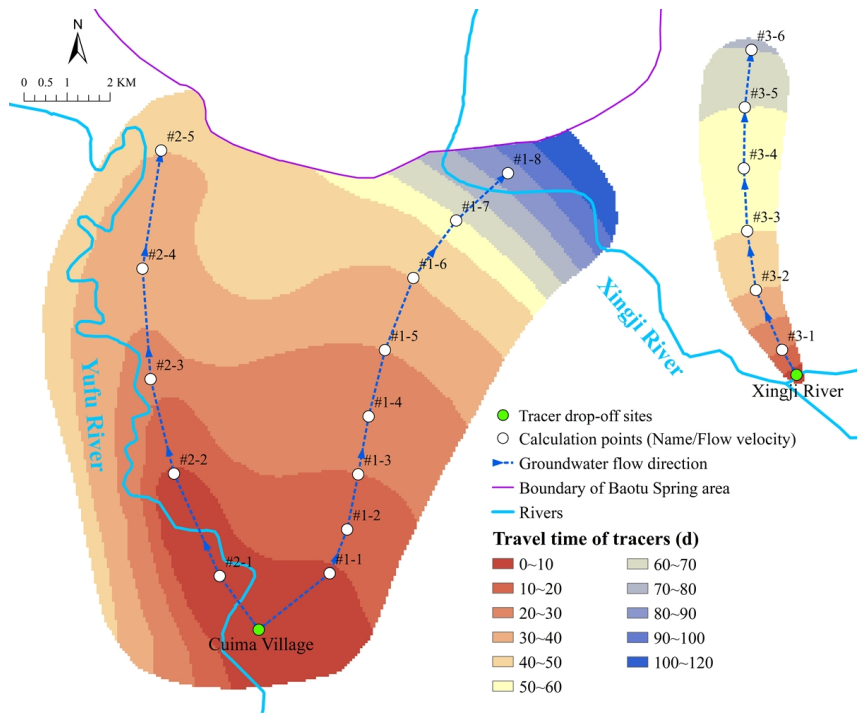
$$n_f = \frac{KI}{v_t} \quad (6)$$

This formula is derived based on Darcy's law. In the equation, “K” represents the hydraulic conductivity (m/d), “I” is the hydraulic gradient, and “ v_t ” is the actual groundwater velocity. There are two large-scale tracer tests which have been conducted at Cuima village in year 1989 and in Xingji River in year 2016 (Zhu et al., 2020). To determine the parameters required in the groundwater solute transport model, the actual groundwater flow velocity and the effective porosity of the karst aquifer were calculated based on the data from the two tracer tests (Fig.4).

First, three groundwater flow lines were extracted from the groundwater flow field, and several calculation points for groundwater flow velocity and effective porosity were selected at equal intervals.



224 Flow lines #1 and #2 represent the diffusion direction of the tracers from Cuima Village, while flow line
225 #3 represents the diffusion direction of the tracers from Xingji River. Using the isochrone map of tracer
226 peak concentration diffusion, the actual groundwater flow velocity was calculated based on the horizontal
227 distance between adjacent isochrones at each calculation point. The hydraulic gradient at the calculation
228 points on flow lines #1 and #2 was calculated using 1989 groundwater level monitoring data, and the
229 hydraulic gradient on flow line #3 was calculated using 2016 data. The permeability coefficient (K) for
230 each calculation point was determined using the groundwater flow model established in this research.
231 Finally, the effective porosity at each calculation point was calculated using formula (6).



232
233 Fig.4 Tracer tests conducted in Cuima Village and Xingji River

234 **2.5. Groundwater flow-solute transport simulation**

235 Numerical simulation is used to predict groundwater level and quality in this research. As mentioned
236 in the introduction, the EMP model without inserting karst-conduits embedded is capable for



237 groundwater flow simulation in karst regions with low development like the northern China karst areas.
 238 Therefore, the GMS software was used to establish a karst groundwater flow and solute transport model
 239 for the Baotu Spring area. The MODFLOW 2005 and MT3DMS packages were employed to solve the
 240 groundwater flow and solute transport equations using the finite difference method.

241 The numerical model encompasses the Baotu Spring area, simplifying the stratigraphy into four
 242 units: Quaternary pore phreatic aquifer, intrusive rock aquitard, Ordovician-Cambrian karst aquifer, and
 243 the aquitard below the Mantou Formation (Fig. 5(a)). The Ordovician-Cambrian karst aquifer is the main
 244 aquifer and the target aquifer for MAR and groundwater exploitation. The boundaries of the Ordovician-
 245 Cambrian karst aquifer are set as Fig.5(b). Additionally, the boundaries of other strata are all impervious.

246 The model's source and sink terms include precipitation recharge, MAR from rivers and wells,
 247 groundwater exploitation, spring discharge, agricultural irrigation exploitation, and agricultural irrigation
 248 re-infiltration. Precipitation recharge is calculated based on precipitation quantity, infiltration recharge
 249 coefficient, and recharge zone area. The infiltration recharge coefficient considers surface lithology,
 250 urbanization, and agricultural development. The MAR from rivers mainly occur through the Yufu and
 251 Xingji Rivers, and the actual recharge volume is discussed in Section 3.2. The locations of MAR wells,
 252 groundwater exploiting wells and MAR river reaches are displayed in Fig.5(b).

253 The hydraulic conductivity K consists of horizontal hydraulic conductivity K_x and vertical hydraulic
 254 conductivity K_y . The zoning and values of K_x are mainly based on the hydrogeological tests, and then
 255 identified and verified using groundwater level monitoring well data. K_y is uniformly set to 0.1 times K_x .
 256 The remaining hydrogeological parameters (specific yield, storage coefficient, and dispersity) are taken
 257 as empirical values. The determination of effective porosity has been discussed in Section 2.4. The
 258 simulation period spans from January 1, 2020, to December 31, 2022, with each stress period lasting one



259 month.

260 Next, the impact of MAR and groundwater exploitation on the dynamics of karst groundwater levels

261 was quantitatively analyzed using a groundwater flow model, with Baotu Spring's water level serving as

262 a representative indicator. The considered MAR are from Yufu River, Xingji River, and MAR wells. For

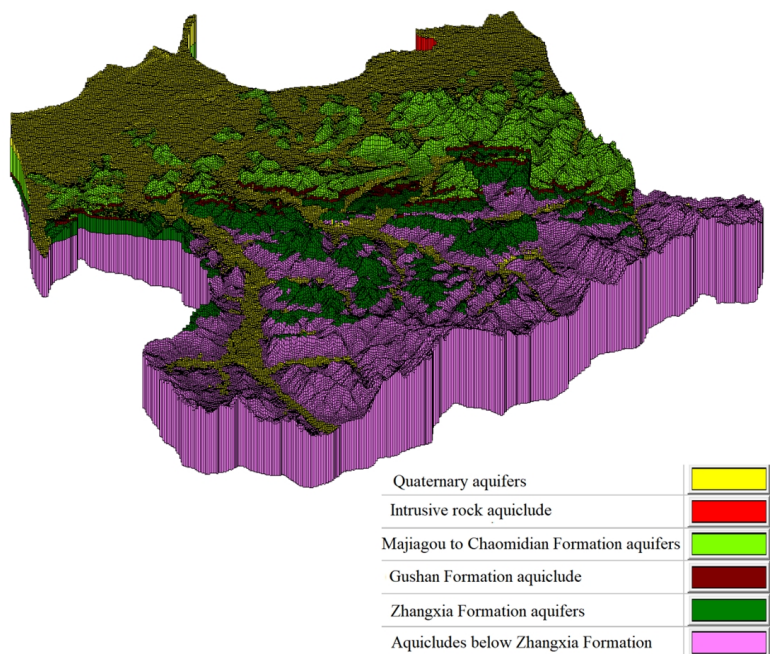
263 the simulation period of 2020-2022, the net variations of Baotu Spring water level caused by MAR and

264 groundwater exploitation were calculated.

265 Finally, to quantitatively compare the effects of various MAR and groundwater exploitation on the

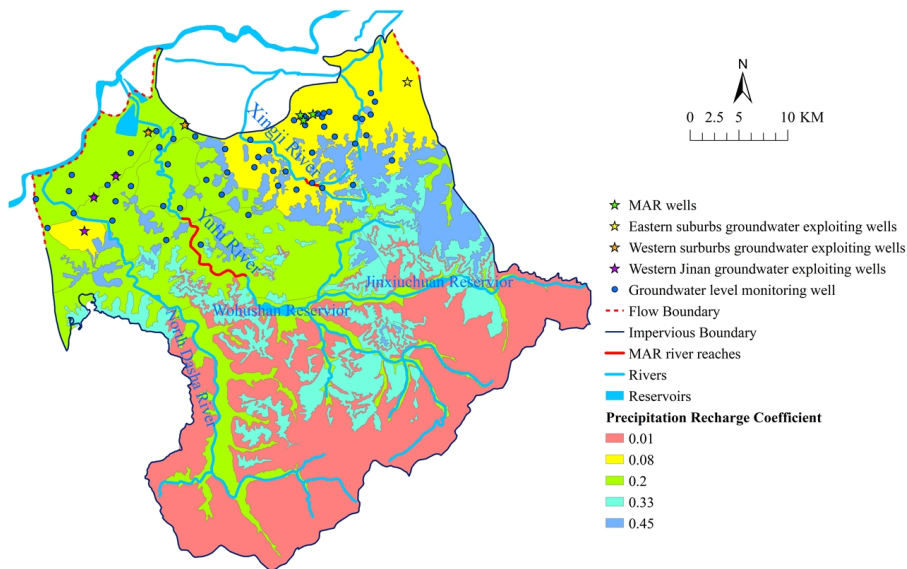
266 dynamics of Baotu Spring water level, the water level net variation after 1, 2, and 3 years of continuous

267 recharge and exploitation at a constant flow rate was calculated and compared.



268

269 (a) Geological model



(b) Settings of groundwater flow model

Fig.5 Geological model and groundwater flow model

For the solute transport simulation, sulphate is selected as the representative solute because its concentration in the surface water used for MAR is higher than that in the groundwater, while the concentrations of other solute components are either similar to or lower than those in the groundwater. The simulation is based on the groundwater flow model from 2020 to 2022, with all recharge/discharge values averaged over this period to mitigate seasonal flow variations. The initial sulphate concentration in karst groundwater is uniformly set at 50 mg/L, reflecting the average concentration in high-quality water from the wells in western suburbs. The model then simulates the dynamics of sulphate concentration in karst groundwater after 2, 6, and 18 months of continuous recharge with sulphate concentrations of 150 mg/L, 250 mg/L, and 350 mg/L in the MAR water.

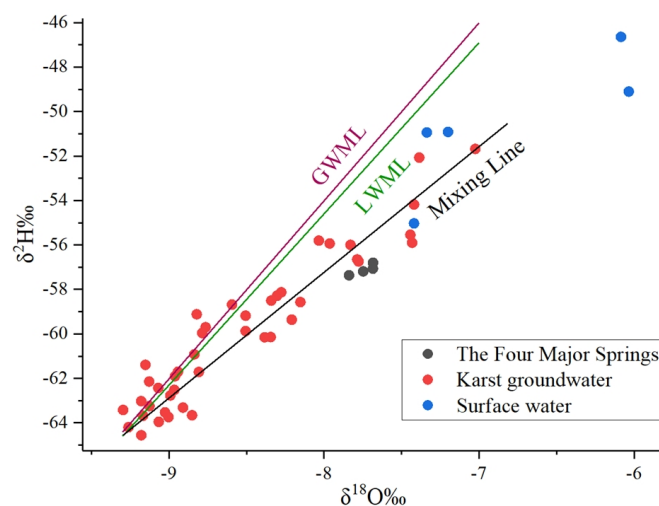
3. Results and discussion

3.1. Mixing percentages of groundwater recharge sources

A scatter plot of the $\delta^2\text{H}\text{‰}$ and $\delta^{18}\text{O}\text{‰}$ of groundwater and surface water is generated in Fig.6. It



285 shows that karst groundwater samples are distributed near the LWML, indicating that the karst
 286 groundwater in the study area originates from precipitation (Liu et al., 2021). The isotopic enrichment of
 287 ^2H and ^{18}O in surface water samples is significantly higher than that in karst groundwater samples,
 288 exhibiting a typical evaporation effect. Additionally, the karst groundwater samples gradually deviate
 289 from the LMWL with the enrichment of ^2H and ^{18}O , indicating the mixing of precipitation and surface
 290 water. This suggests that the karst groundwater is significantly recharged by surface water.



291
 292 Fig.6 Scatter plot of $\delta^2\text{H}\text{‰}$ and $\delta^{18}\text{O}\text{‰}$ in water samples

293 The mixing percentage of surface water recharge in groundwater is exhibited in Fig.7. According
 294 to the result, the closer the distance to the MAR reaches of Yufu River and Xingji River, the higher the
 295 mixing percentage of surface water recharge in the groundwater. In the southern metamorphic rock and
 296 Cambrian Zhangxia Formation limestone outcrop areas, as well as the northwestern Yellow River
 297 alluvial plain, the mixing percentage of surface water recharge is generally less than 20%. In contrast,
 298 in the middle and lower reaches of the Yufu River and North Dasha River basins, as well as the Xingji
 299 River basin, the mixing percentage of surface water recharge is relatively high. The highest mixing
 300 percentage is near the MAR reaches of the Yufu River and Xingji River. For example, in the villages

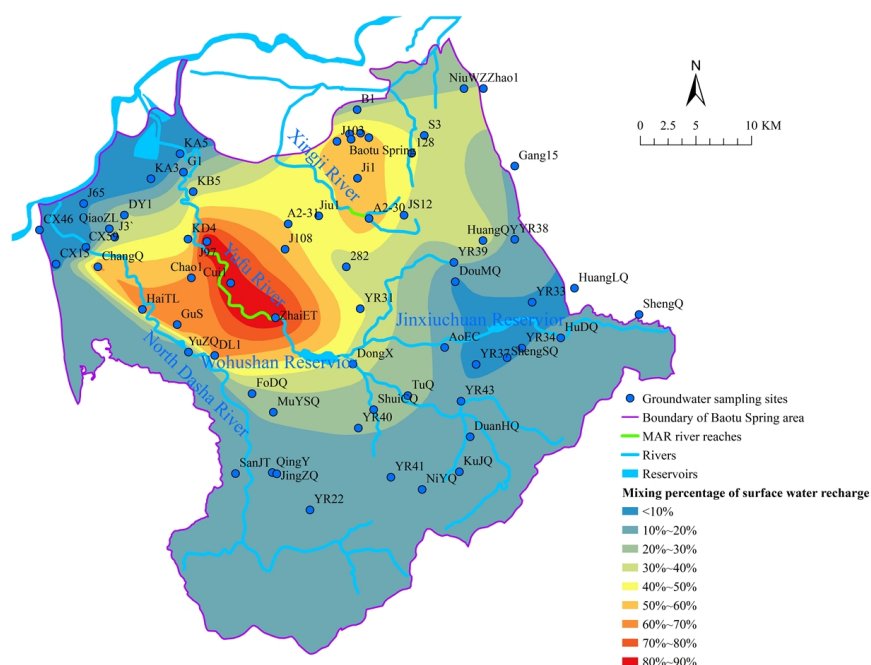


Fig.7 Mixing percentage of surface water recharge in groundwater

3.2. Infiltration efficiency of MAR river reaches

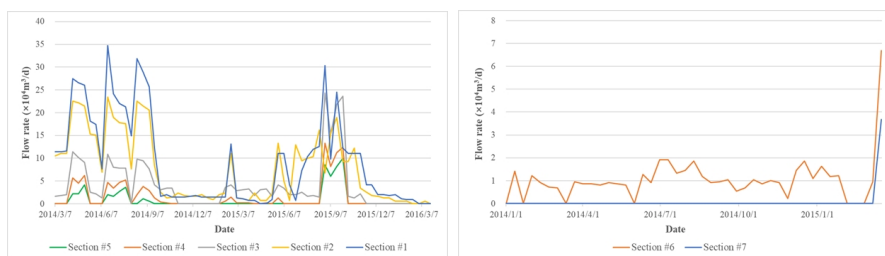


314 Darcy's Law, is approximately $114.9 \times 10^4 \text{ m}^3/\text{d}$.

315 Based on field surveys, large volume of released water in the Yufu River results in some flow
 316 escaping at the Section #5, failing to infiltrate and recharge karst groundwater, thereby reducing the
 317 actual recharge volume. To verify this, analysis of flow data from 2014 to 2016 (Fig.8) was conducted,
 318 revealing the relationship between actual recharge volume and released water volume. When the released
 319 water volume does not exceed $21.6 \times 10^4 \text{ m}^3/\text{d}$, the actual recharge volume equals the released water
 320 volume, indicating full infiltration of surface water before Section #5. However, when the released water
 321 volume exceeds $21.6 \times 10^4 \text{ m}^3/\text{d}$, the actual recharge volume is less than the released water volume, as
 322 some surface water flows past Section #5 without infiltrating karst groundwater. Calculations confirm
 323 that when the released water volume exceeds $21.6 \times 10^4 \text{ m}^3/\text{d}$, the relationship between the actual recharge
 324 volume and the released water volume follows formula (7).

$$325 \quad Q_{\text{Act}} = 0.843 \times Q_{\text{Rel}} + 3.396 \quad (7)$$

326 Where, Q_{Act} is the actual recharge volume in Yufu River (m^3/d), and Q_{Rel} is the released water
 327 volume in Yufu River Section #1 (m^3/d).



328

329 (a) Yufu River

(b) Xingji River

330 Fig.8 Flow rate curves at various sections of the Yufu River and Xingji River

331 Likewise, in Xingji River, the relationship between the actual recharge volume and the released
 332 water volume follows formula (8) when the released water volume exceeds $2 \times 10^4 \text{ m}^3/\text{d}$.



$$Q_{Act}=0.214\times Q_{Rel}+1.573 \quad (8)$$

Where, Q_{Act} is the actual recharge volume in Xingji River (m^3/d), and Q_{Rel} is the released water volume in Xingji River Section #6 (m^3/d).

Finally, the actual recharge volume of Yufu River and Xingji River from 2020 to 2022 was calculated in Fig.9, respectively. These calculations were used as surface water recharge inputs for the groundwater flow model.

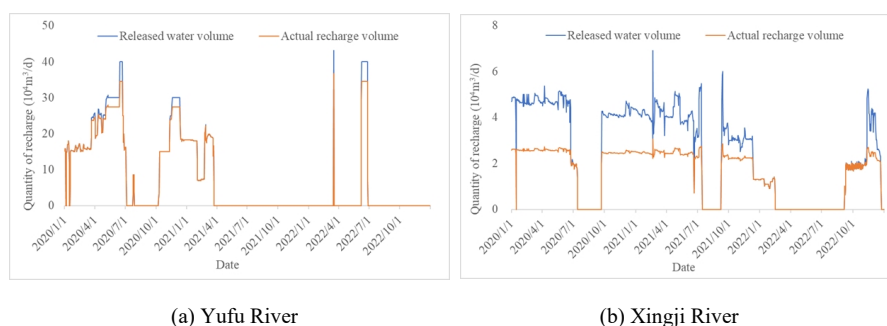


Fig.9 Released water volume VS. Actual recharge volume in Yufu River and Xingji River

3.3. Effective porosity of karst aquifers estimated from tracer tests

As discussed in Section 2.4, the effective porosity at each calculation point was calculated using formula (6), with the process and results shown in Tab.1. Obviously, the effective porosity of the aquifer varies widely, with the maximum, minimum, and average values being 4.39×10^{-4} , 1.28×10^{-5} , and 1.08×10^{-4} , respectively. This variability is closely related to the heterogeneity of the karst aquifer, aligning with studies in similar carbonate rock regions in the UK and Austria (Medici & West, 2021; Worthington et al., 2019). In this paper, the average effective porosity (1.08×10^{-4}) from all calculated points on three flow lines from the Cuima Village and Xingji River tracer tests was used to represent the karst aquifer's effective porosity for groundwater solute transport modeling.



352

Tab.1 Effective porosity at the calculation points

Name	Flow velocity (m/d)	Permeability (m/d)	Hydraulic gradient	Effective porosity
#1-1	233.6	10	4.23E-03	1.81E-04
#1-2	240.3	1	3.85E-03	1.60E-05
#1-3	266.9	2	1.70E-03	1.28E-05
#1-4	295.2	4	1.16E-03	1.58E-05
#1-5	225.5	20	1.20E-03	1.07E-04
#1-6	148.3	20	3.85E-04	5.19E-05
#1-7	82.4	120	3.01E-04	4.39E-04
#1-8	52.4	10	3.07E-04	5.85E-05
#2-1	449.6	10	2.46E-03	5.47E-05
#2-2	293.2	22	1.03E-03	7.70E-05
#2-3	193.5	80	1.67E-04	6.89E-05
#2-4	356.3	80	2.78E-04	6.24E-05
#2-5	307	50	4.42E-04	7.21E-05
#3-1	63	0.3	1.07E-02	5.09E-05
#3-2	96.8	0.3	1.26E-02	3.90E-05
#3-3	165.1	1	1.29E-02	7.83E-05
#3-4	287.7	20	2.08E-03	1.45E-04
#3-5	275.7	120	9.88E-04	4.30E-04
#3-6	71.8	8	8.65E-04	9.64E-05
Max	449.6	/	/	4.39E-04
Min	52.4	/	/	1.28E-05
Average	216	/	/	1.08E-04

353 3.4. Impacts of MAR and groundwater exploitation on groundwater level

354 According to the identification and verification of the groundwater flow model, the horizontal
 355 hydraulic conductivity of karst aquifers is exhibited in Fig.10(a). The calculated and observed
 356 groundwater flow field as of December 31, 2022, are exhibited in Fig.10(b), and the calculated and
 357 observed groundwater levels for representative monitoring wells are shown in Fig.10(c) to 10(f).

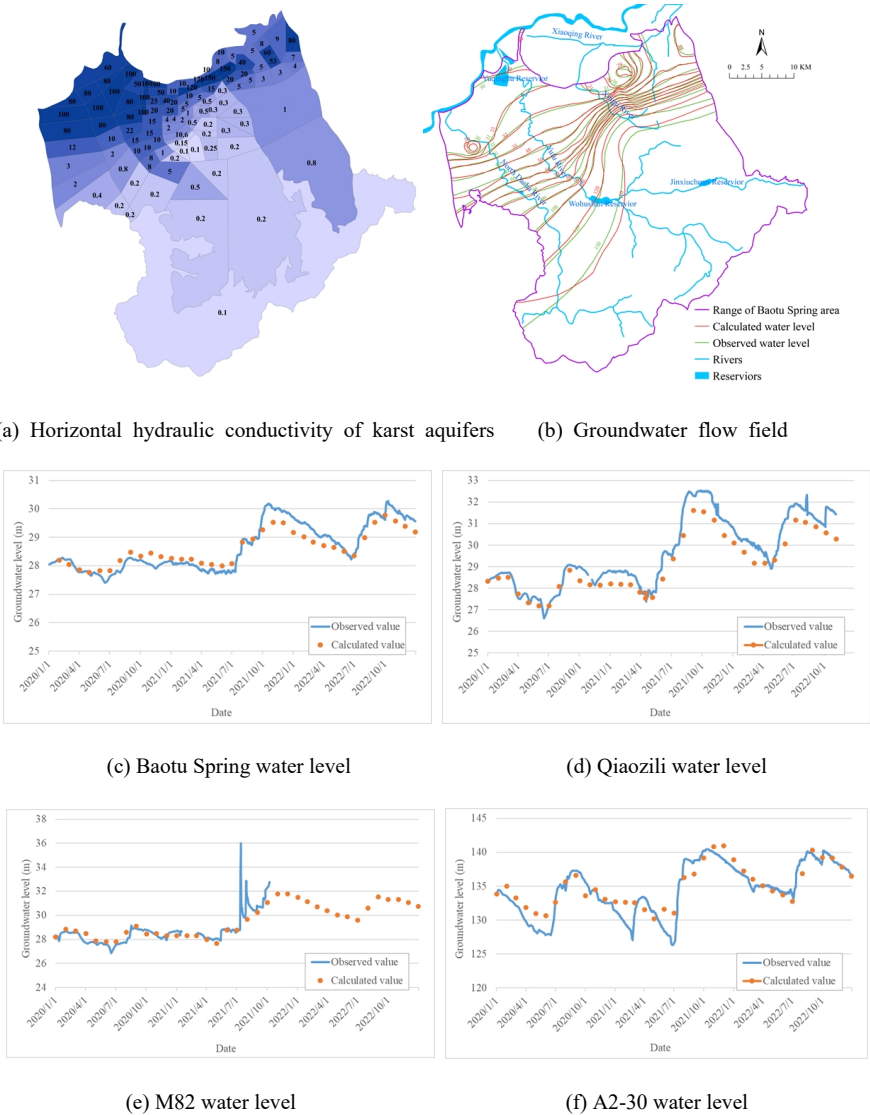


Fig.10 Identification and verification result of the groundwater flow model

The net variations of Baotu Spring water level caused by MAR and groundwater exploitation were simulated and are displayed in Fig.11. The "net variations of Baotu Spring water level" in Fig.11 refers to the portion of groundwater level fluctuation in Baotu Spring caused by MAR and groundwater exploitation. These variations are calculated using a numerical model based on actual MAR and



groundwater exploitation data. It shows that the water level of Baotu Spring clearly rises with MAR and drops with groundwater exploitation. There is also a lag in the impact of these factors on the water level.

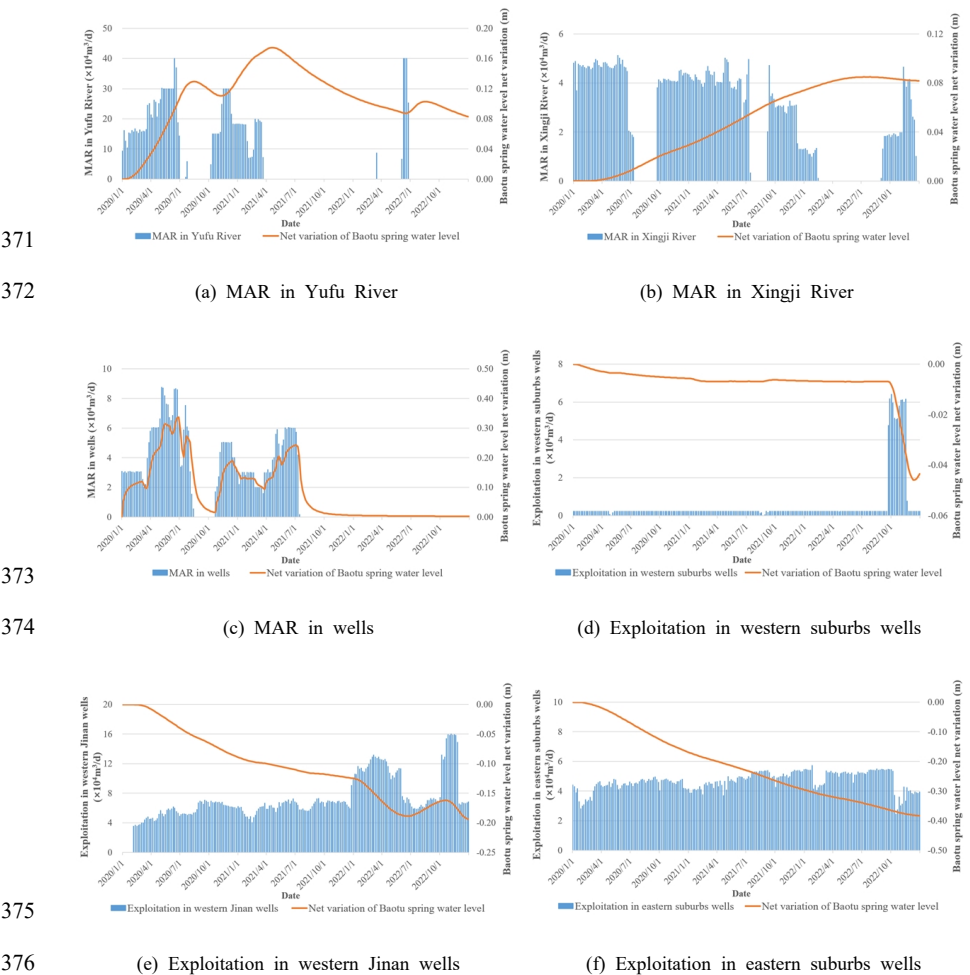


Fig.11 Net variations of Baotu Spring water level caused by MAR and groundwater exploitation (based on data in 2020-2022)

Then, the water level net variation after 1, 2, and 3 years of continuous recharge and exploitation at a constant flow rate was calculated and compared, with detailed results shown in Tab.2. Note that due to maximum recharge capacity constraints, scenarios with recharge volumes of Xingji River and MAR



382 wells exceeding $5 \times 10^4 \text{ m}^3/\text{d}$ were not included. Tab.2(a) illustrates the impact of MAR on Baotu Spring's
383 water level. It shows that, with the same recharge volume and duration, the MAR in wells has the greatest
384 effect, followed by Xingji River, and Yufu River has the least impact. Despite this, Yufu River's
385 maximum recharge capacity greatly exceeds that of Xingji River and the MAR wells. Additionally, the
386 water level rise under MAR wells recharge remains almost unchanged within the three years, indicating
387 that the maximum effect is achieved within the first year. This rapid response is due to the proximity of
388 the MAR wells to Baotu Spring (0.75 km, 0.81 km, and 0.35 km, respectively) and the high permeability
389 ($k=150 \text{ m/d}$) of the shared karst aquifer.

390 In practice, the most suitable MAR source should be chosen based on the following strategies.
391 Firstly, MAR in wells yields the best results and raises the Baotu Spring water level the fastest, but it has
392 a low maximum recharge capacity. Therefore, MAR in wells should be prioritized for a rapid short-term
393 rise in the Baotu Spring water level. Secondly, MAR in Xingji River is less effective and also has a low
394 maximum capacity, making it suitable for maintaining a small long-term rise in the Baotu Spring water
395 level in conjunction with MAR in wells. Thirdly, MAR in Yufu River is the least effective but has a high
396 maximum capacity, so for a significant long-term rise in the Baotu Spring water level, all three sources
397 should be considered, with MAR in Yufu River being the primary source.

398 Tab.2(b) illustrates the impact of groundwater exploitation on Baotu Spring's water level. Overall,
399 the exploitation in eastern suburbs wells has the most significant impact on Baotu Spring's water level,
400 followed by the western suburbs wells, with the western Jinan wells having the least impact. Between
401 2020 and 2022, daily average exploitation volume was $5,339 \text{ m}^3/\text{d}$ for western suburbs wells, $70,852$
402 m^3/d for western Jinan wells, and $46,487 \text{ m}^3/\text{d}$ for eastern suburbs wells. Therefore, to minimize the
403 impact on the water level of Baotu Spring while ensuring the basic groundwater exploitation needs in the



area, western suburbs wells still hold significant exploitation potential and consideration may be given to transferring a portion of exploitation from eastern suburbs wells to western suburbs wells.

Tab.2 The effect on groundwater level net variation at Baotu Spring resulting from a constant rate of continuous MAR and groundwater exploitation over 1 year, 2 years, and 3 years

(a). The effect on groundwater level rise resulting from MAR

MAR rate ($\times 10^4 \text{m}^3/\text{d}$)		Duration of groundwater recharge		
		1 year	2 years	3 years
Yufu River	2	19 mm	31 mm	36 mm
	5	49 mm	76 mm	90 mm
	10	97 mm	152 mm	179 mm
	20	194 mm	300 mm	353 mm
	30	266 mm	409 mm	480 mm
Xingji River	2	23 mm	60 mm	89 mm
	5	38 mm	100 mm	148 mm
MAR wells	2	85 mm	86 mm	86 mm
	5	212 mm	214 mm	216 mm

(b). The effect on groundwater level drop resulting from groundwater exploitation

Groundwater exploitation rate ($\times 10^4 \text{m}^3/\text{d}$)		Duration of groundwater exploitation		
		1 year	2 years	3 years
Western suburbs wells	5	115 mm	138 mm	142 mm
	10	230 mm	283 mm	293 mm
Western Jinan wells	5	87 mm	106 mm	107 mm
	10	175 mm	218 mm	221 mm
Eastern suburbs wells	5	199 mm	322 mm	382 mm
	10	397 mm	643 mm	765 mm

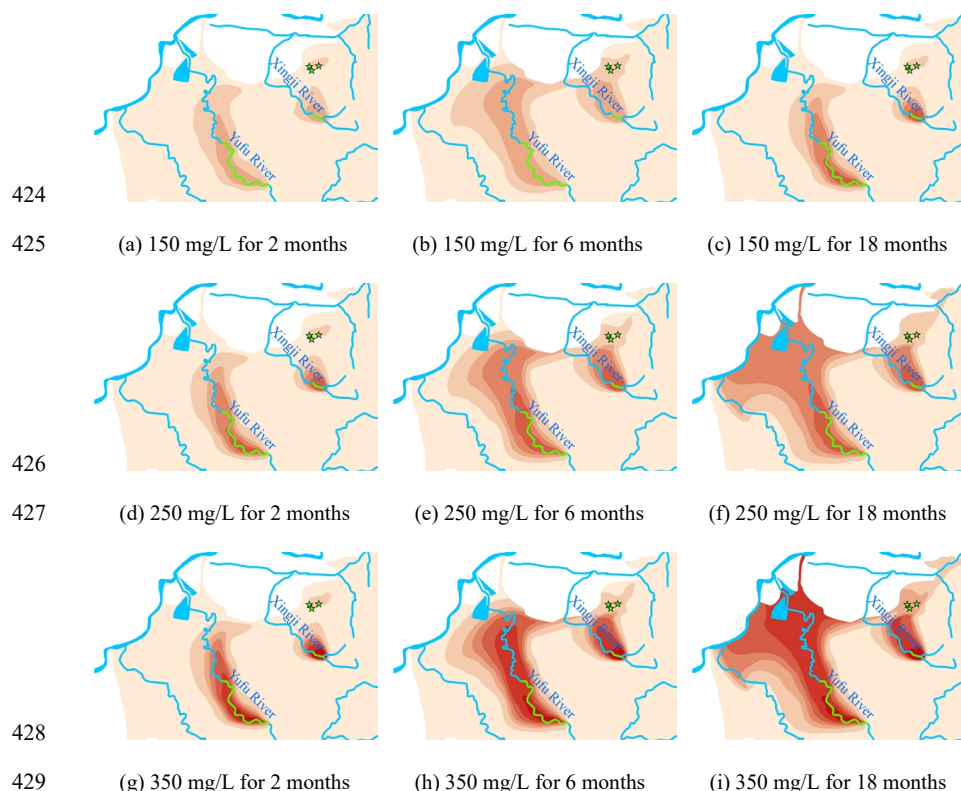
3.5. Impacts of MAR on groundwater quality

Based on the groundwater solute transport model established in this paper, simulations were conducted to monitor the dynamics of sulphate concentration in karst groundwater after continuous recharge of water with sulphate concentrations of 150 mg/L, 250 mg/L, and 350 mg/L over periods of 2 months, 6 months, and 18 months. As shown in Fig.12, with prolonged recharge duration and deteriorating recharge water quality, the sulphate concentrations in karst groundwater increase and the



416 affected area of karst groundwater quality expands continuously, indicating an increasing impact of MAR
 417 on karst groundwater quality over time. Therefore, deteriorating water quality from MAR poses risks to
 418 groundwater, and strict control and monitoring of recharge water quality are necessary.

419 Additionally, sulphate concentrations in karst groundwater reach stability after 12~18 months of
 420 continuous recharge, and a linear regression established a quantitative relationship between the sulphate
 421 concentrations in karst groundwater and in MAR water (Fig.13). In practice, target values for sulphate
 422 concentrations in karst groundwater should be preset, and the minimum control standards for sulphate
 423 concentrations in MAR water could be calculated using the relationship shown in Fig.13.



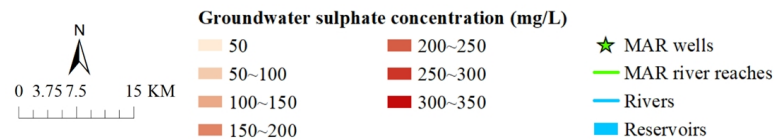


Fig.12 Evolution of sulphate concentration in karst groundwater under MAR

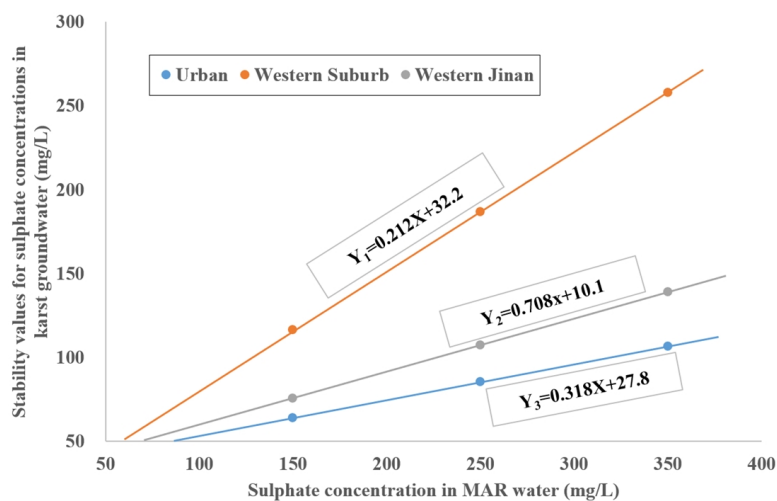


Fig.13 Linear relationships between sulphate concentrations in karst groundwater and MAR water

4. Conclusions

In this research, the impacts of MAR and groundwater exploitation on the dynamics of karst groundwater level and quality in the Baotu Spring area of Jinan City were quantitatively analyzed by multi-methods. The main conclusions are summarized as follows.

Firstly, the $\delta^2\text{H}\text{‰}$ and $\delta^{18}\text{O}\text{‰}$ values of groundwater and surface water reveals that surface water is an essential source of groundwater recharge and plays a crucial role in maintaining groundwater volume. In the southern metamorphic rock and Cambrian Zhangxia Formation limestone outcrop areas, as well as the northwestern Yellow River alluvial plain, the surface water recharge proportion is generally less than 20%. Near the MAR reaches of the Yufu River and Xingji River, the mixing percentage of surface water recharge exceed 80% and 50%, respectively.



444 Secondly, according to the analysis of the infiltration test results, the theoretical maximum recharge
445 capacity of the Yufu River to karst groundwater is about $114.9 \times 10^4 \text{ m}^3/\text{d}$ by infiltration tests. However,
446 the analysis of the rivers' flow monitoring results reveals that some surface water will flow out
447 downstream when the released water volume of the Yufu River and Xingji River exceeds $21.6 \times 10^4 \text{ m}^3/\text{d}$
448 and $2 \times 10^4 \text{ m}^3/\text{d}$, respectively, reducing the actual recharge volume.

449 Thirdly, the isoline map of tracer peak concentration diffusion estimated the effective porosity of
450 the karst aquifer in the study area to be 1.08×10^{-4} , providing a reference for solute transport modeling
451 in similar hydrogeological conditions. According to the simulations of the groundwater flow model,
452 MAR effectively raises karst groundwater levels, and the effectiveness varies for the three MAR sources.
453 MAR in wells has the best effect and fastest response, followed by the MAR in Xingji River, though
454 both have low maximum recharge capacities. The MAR from Yufu River has a lower effect but the
455 highest maximum recharge capacity. Furthermore, transferring some amount of the groundwater
456 exploitation from eastern suburbs wells to western suburbs wells might reduce the impact on the water
457 level of Baotu Spring.

458 Finally, poor quality of MAR water would negatively affect karst groundwater, and there is a linear
459 relationship between the concentration of hydrochemical component in MAR water and karst
460 groundwater, allowing for the pre-setting of karst groundwater quality targets and the determination of
461 minimum standards for MAR water quality based on this relationship.

462 In summary, the MAR projects in the Baotu Spring area of Jinan City have significantly impacted
463 the dynamics of karst groundwater level and quality. Proper planning and monitoring of the amount and
464 quality of MAR and groundwater exploitation are essential for maintaining groundwater levels, ensuring
465 continuous spring flow, and safeguarding groundwater quality.



466 **Statements and Declarations**

467 **Data availability**

468 The data underlying this article were provided by 801 Institute of Hydrogeology and Engineering
469 Geology, Shandong Provincial Bureau of Geology & Mineral Resources by permission. Data will be
470 shared on request to the corresponding author with permission.

471 **Author Contribution**

472 The respective contributions of all authors to this paper are as follows:

473 Han Cao: Conceptualization, Methodology, Writing-Original Draft.

474 Weihong Dong: Writing-Review and Editing, Supervision, Project administration.

475 Caiping Hu, Huanliang Chen: Resources, Funding acquisition, Investigation, Data Curation.

476 Jinlong Qian: Investigation, Data Curation.

477 Chunwei Liu, Minghui Lyu, Shuai Gao: Resources, Funding acquisition.

478 **Competing Interests**

479 The authors have no relevant financial or non-financial interests to disclose.

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