



Spatial variability in bedload transport rates determined by river pattern

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Abstract. Local spatial patterns in flow hydraulics generate temporal variations in bedload transport rates. The nature of this local spatial variability changes as larger spatial scales are considered. Here, we investigate the hypothesis that spatial variability in bedload transport is a function of river pattern defined at the reach scale. A high-resolution system-scale DEM, which fuses bathymetric and topographic surveys, is used for two-dimensional hydraulic modelling to predict distributions of flow depth, velocity and shear stress. From this modelling, we predict bedload transport rates in four contiguous reaches with different (meandering, wandering, braided, deltaic) river patterns. Spatial and frequency distributions of bedload transport rate reveal distinct signatures associated with each river pattern. The results enable the real-world variance in the continuum of river patterns and bedload transport to be characterised, with implications for assessing channel change from, for example, anthropogenic modification and restoration.

1 Introduction

Fluctuations in bedload transport rates are ubiquitous in time series data and are fundamental to understanding bed material transport dynamics (Ancey, 2020). Although dependent on measurement methodology, these fluctuations scale with transport rate and influence the morphodynamics of bedforms at all scales (Ancey, 2020; Ghilardi et al., 2014; Redolfi et al., 2018). Transport rate fluctuations are frequently related to spatial patterns of transport across a riverbed at a given time (Hoey et al., 2000; Lisle et al., 2000), and the spatial variability in the hydraulics that control bedload movement is itself suggested to be a function of channel morphology (Paola, 1996; Nicholas, 2000).

Whether for defining sampling protocols (Ancey and Pascal, 2020), predicting transport rates (Adams and Eaton, 2022), determining reach-scale morphodynamic adjustments (Dhont and Ancey, 2018; Redolfi et al., 2018), assessing the



consequences of sediment inputs (Reiterer et al., 2025), or understanding the impacts of engineering (Lisle et al., 1997), understanding bedload transport is critical. Although monitoring instantaneous bedload transport rates across entire river reaches remains impossible, advances in fluvial remote sensing (Piegay et al., 2020) have enabled the generation of high-resolution catchment-scale Digital Elevation Models (DEMs) that incorporate river bathymetry (e.g. Lague and Feldmann, 2020). Together with estimates of surface roughness and hydrology, these DEMs can provide boundary conditions for 2D hydraulic simulation (Bates, 2022) and bedload transport prediction. Reliable, verified hydraulic models enable flow properties (i.e. water depth, velocity, shear stress) to be predicted at catchment- or reach-scale (Lisle et al., 2000; Williams et al., 2011, Segura and Pitlick, 2015), from which bedload transport rates can be computed (Reid et al., 2019).

Relating channel morphology to transport dynamics first requires identification of distinct morphologies. Channel patterns lie on continua (e.g. Huang and Nanson, 2007; Brierley and Fryirs, 2005) and are increasingly being described in terms of dynamics (Boothroyd et al., 2025; Graf, 2000) rather than using temporal snapshots. Accepting that the boundaries between channel patterns may be fuzzy, contrasting channel patterns are often identifiable using different classifications and descriptive measures (e.g. Tejedor et al., 2022). This approach enables individual river reaches to be identified that have distinct morphologies and process environments (Kasprak, 2016).

We hypothesise that reach-scale spatial variability in bedload transport, expressed through probability density functions, is a function of river pattern. To test this, we numerically simulate two-dimensional flow dynamics of a gravel-bed riverscape (Fig. 1a) using a 0.5 m resolution topo-bathymetric DEM (Fig. 1c). Modelled shear stresses (Fig. 1g) are then combined with grain size observations to compute predicted bedload transport rates (Fig. 1h). We use a simplified qualitative classification of river planform morphology to define four contiguous reaches with contrasting channel patterns (Fig. 1a and 1b). Selecting multiple different reaches within a single river enables direct comparisons to be made between the four planforms, avoiding complications arising from differences in model boundary conditions between different rivers and their associated patterns. Since bedload transport remains difficult to predict (Recking et al., 2012; Recking, 2013), especially with mixed grain-sizes and complex flow histories, simplifying assumptions are required. We assume constant flow for three different magnitude flood events, grain-size distributions that are identical throughout the riverscape and which are represented by single grain sizes (i.e. D16, D50, D84), and fixed bed conditions. Together, this enables us to compare frequency distributions of these predicted bedload transport rates with each river pattern to reveal their distinct signatures.

2 Results

2.1 Area and rate of bedload transport

For all three flow magnitudes, the proportion of the riverbed where there is bedload transport (ABTA) decreases downstream from meandering (73% at Q_{50}) to wandering (46%), braided (20%) and deltaic (9%) patterns (Fig. 2). Only within the



meandering reach does the ABTA value increase significantly with discharge, rising from 66% at Q_{10} to 74% at Q_{100} . Within all of the other pattern types ABTA remains within $\pm 1.5\%$ as discharge increases. Bedload transport is concentrated in one dominant channel in all reaches (Fig. 2). Bedload transport rates (Fig. 3a) also show consistent decreases from meandering (median $g_b = 1204 \text{ g.s}^{-1}$ at Q_{50}) to wandering (301 g.s^{-1}), braided (100 g.s^{-1}) and deltaic (62 g.s^{-1}) reaches. Median bedload transport rates and the range of these rates increase for all reaches as flow is increased (Fig. 3a).

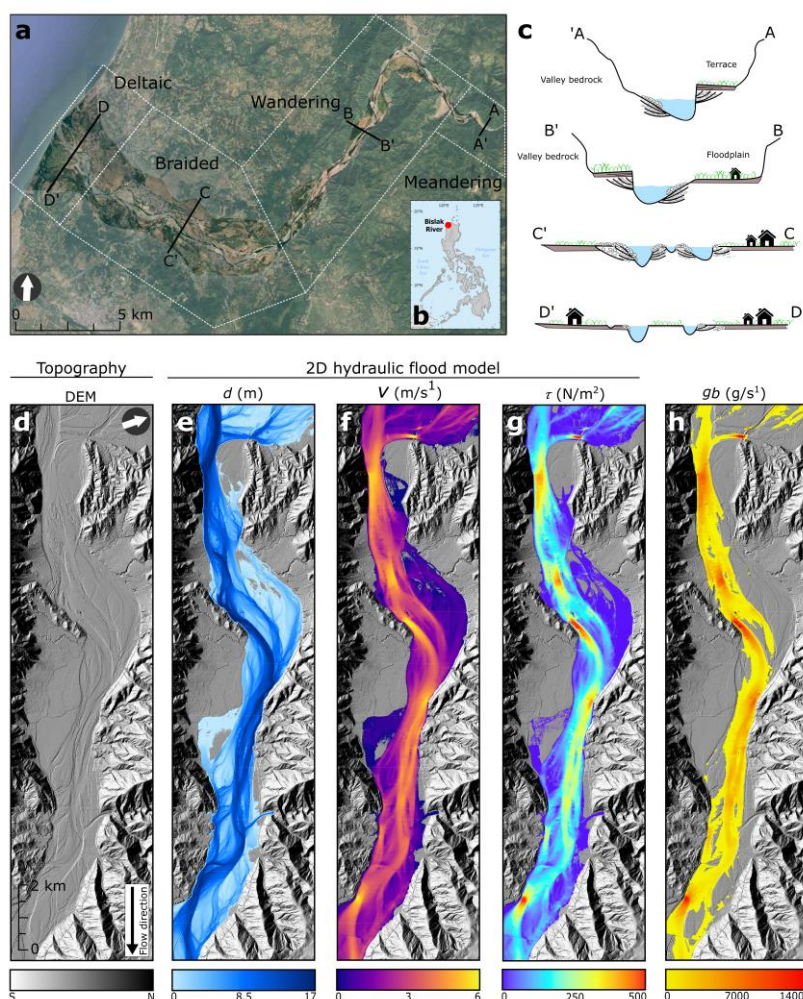


Figure 1: a. Extent of different river patterns along the gravel-bed Bislak River, the Philippines (b). c. Conceptual cross-sections of each river pattern based on Tolentino et al. (2022). d. A section of the 2019 0.5 m resolution Bislak River DEM used for HEC-RAS hydraulic flood modelling to predict depth (e), velocity (f) and shear stress (g) for the Q_{100} event. g. Bedload transport rate predictions, calculated using estimated shear stress, grain size measurements and the generalised Meyer-Peter Müller relation (Equation 1). Aerial imagery shown in (a) is © ESRI Living Atlas.



The mobility of different grain sizes, uncorrected for hiding, repeats the sequence of decreasing mobility from meandering (ABTA = 73% for D_{50} at Q_{50}) to wandering (46%), braided (20%) and deltaic (9%). There are significant changes in the mobile area for different grain sizes at the same discharge (Fig. 4). At Q_{50} , ABTA increases from 1% for D_{84} to 28% for D_{16} in the deltaic reach, and from 4% for D_{84} to 45% for D_{16} in the braided reach. In the meandering reach, bedload transport at Q_{50} is present over higher proportions of the bed than in the multi-channel reaches, with ABTA rising from 54% for D_{84} to 86% for D_{16} . Note that transport is longitudinally continuous for D_{16} in all four patterns, regardless of flow magnitude, with discontinuities observed for both D_{50} and D_{84} reflecting locations where bed shear stress is below the threshold for that grain size due to low, or locally negative, bed slope. Calculated transport rates decrease with grain size (Fig. 3b), once again consistently between the four patterns.

2.2 Covariance of water discharge and bedload transport rates

Unit discharges of both water and bedload show visually consistent spatial patterns across all four reaches (Figs. 1d-h,2,4). These distributions are visualized using re-scaled double-mass plots (Fig. 5a-c) of cumulative bedload transport across all cells as a function of cumulative water discharge. For all flow magnitudes, relationships between cumulative bedload transport and cumulative water discharge are close to linear relationships for the meandering reach, becoming progressively more concave in the same sequence as ABTA values and bedload transport rates decrease, namely from meandering, to wandering, braided and deltaic. The greatest change in these curves (Fig. 5a-c) occurs between wandering and braided reaches.

These results illustrate the role of the excess shear stress, which depends on both discharge and grain size, in controlling bedload transport as a greater proportion of wetted cells in the braided and deltaic reaches are either below or not far above the critical stress for bedload transport. The same effect is shown by the curves for different grain-sizes (Fig. 5d-f), which represent decreasing excess stress as grain size increases. Here, close to linear curves are observed for D_{16} in all reaches, with the reduction in excess stress in many wetted cells for D_{84} shown by the concave curves for braided and deltaic reaches (Fig. 5f).

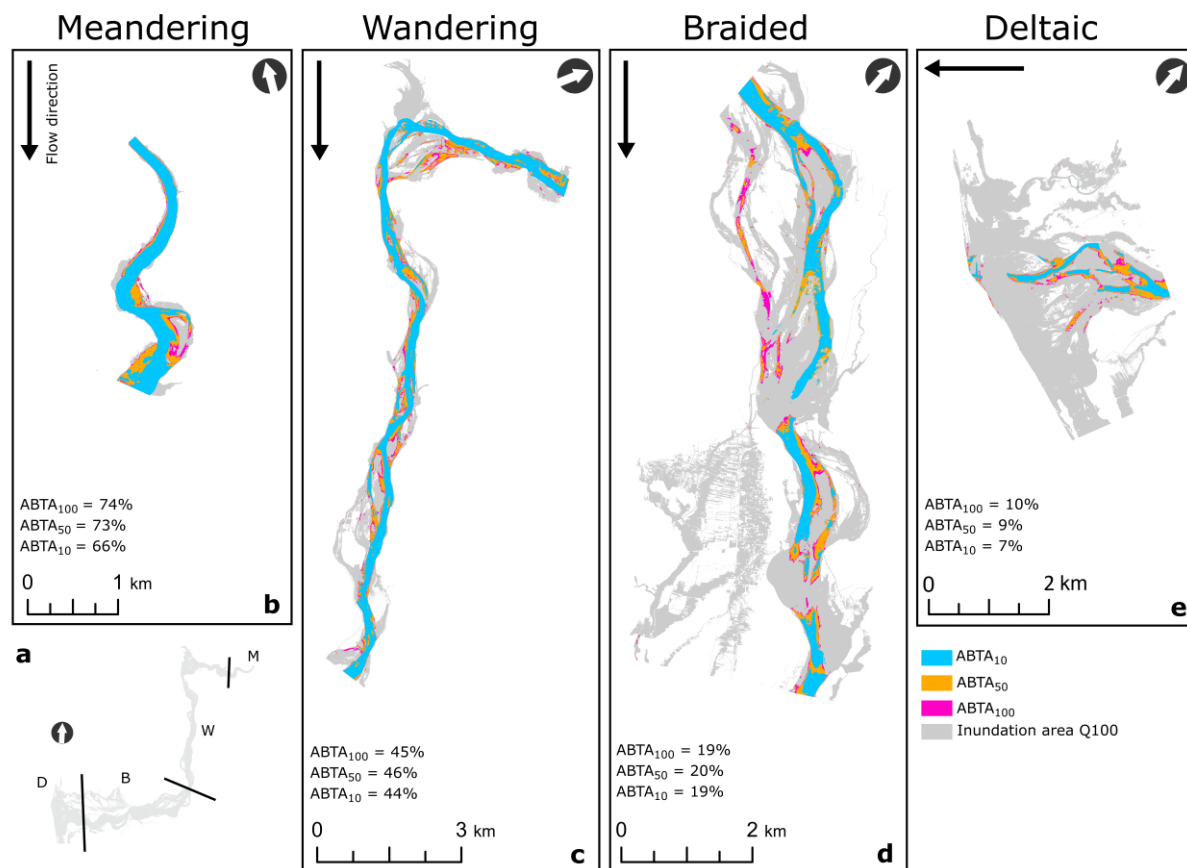


Figure 2: a. Location of four different river patterns along the Bislak River (M: Meandering, W: Wandering, B: Braided, D: Deltaic). b-e. Active bedload transport area (ABTA) for each river pattern, for three flow magnitudes (Q_{10} , Q_{50} , Q_{100}). Grey shading shows the area of inundation for Q_{100} .

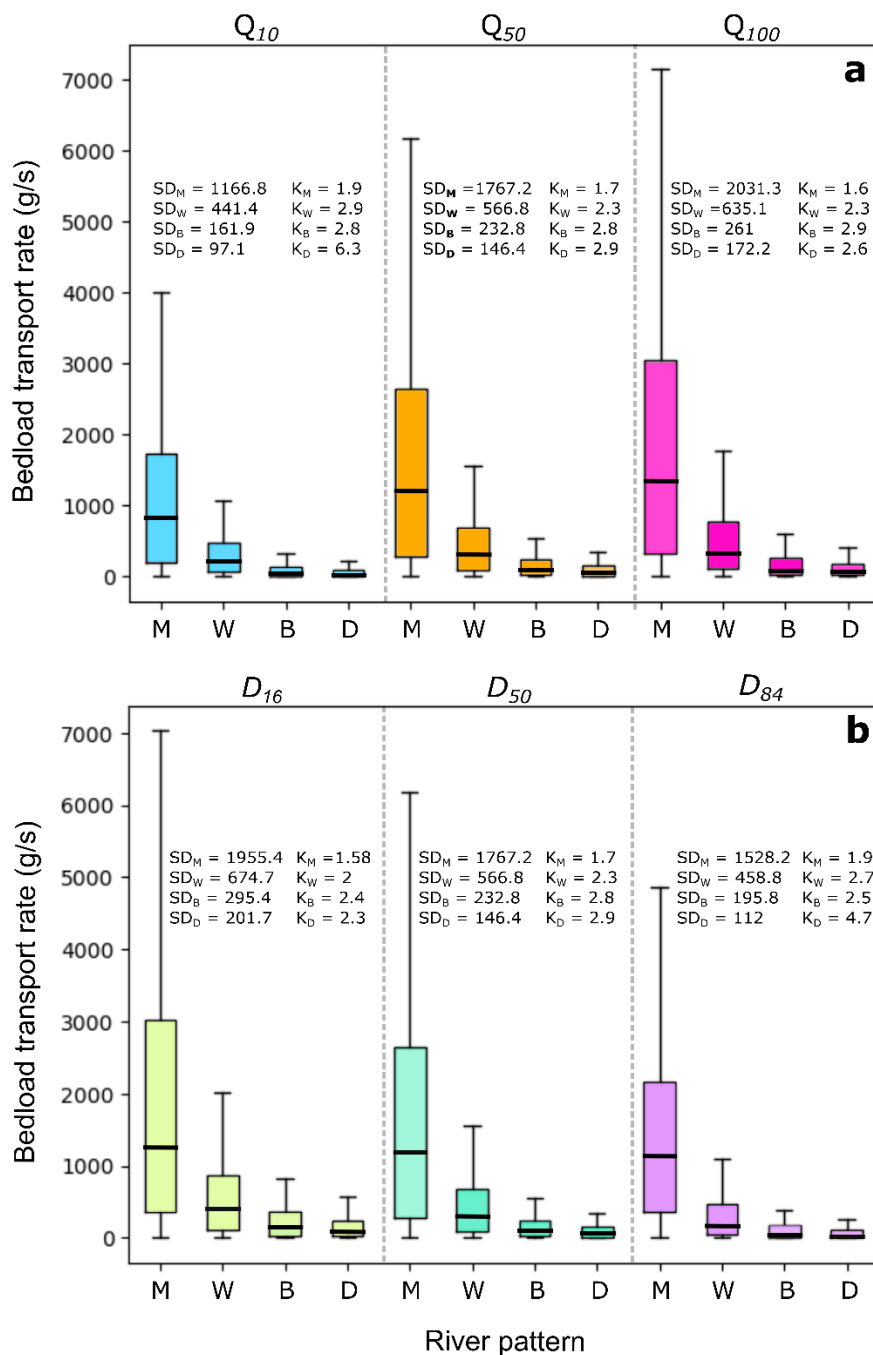


Figure 3: Bedload transport rates for the four identified river patterns (meandering, wandering, braided, deltaic) along the Bislak River. a. Bedload transport rates for each river pattern (D50 grain size) for different flow magnitudes (Q_{10} , Q_{50} , Q_{100}). b. Bedload transport rates for each river pattern for a single flow magnitude (Q_{50}), with different grain sizes (D_{16} , D_{50} and D_{84}).

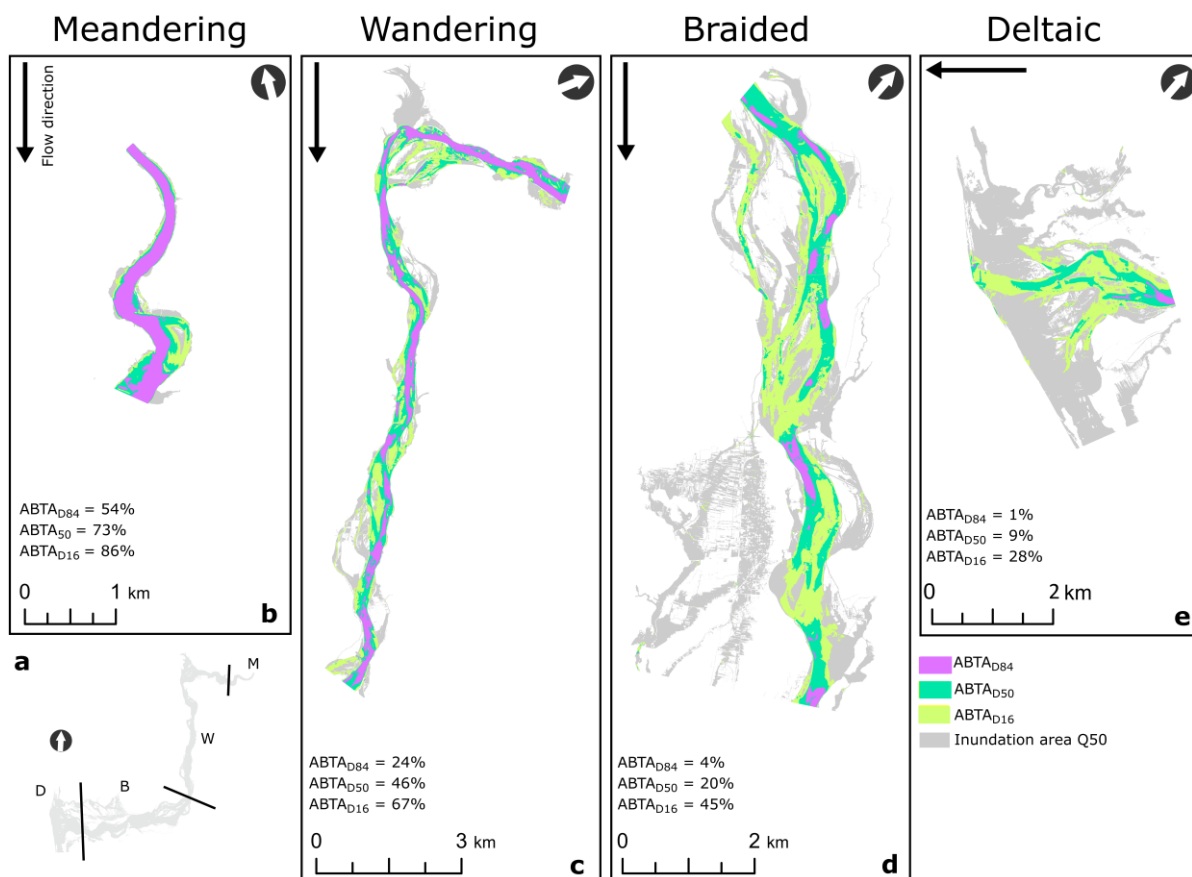


Figure 4: a. Location of four different river patterns along the Bislak River (M: Meandering, W: Wandering, B: Braided, D: Deltaic). b-e. Active bedload transport area (ABTA) for each river pattern for a single flow magnitude (Q_{50}), with different uniform grain sizes (D_{16} , D_{50} and D_{84}).

3 Discussion

3.1 Spatial patterns of bedload transport

Although the total inundated area increases with flow magnitude (Fig. 2), the proportion of that inundated riverbed that experiences bedload transport (ABTA; Fig. 2) remains notably constant within each pattern type, usually concentrated within one main channel. ABTA values decrease systematically downstream as river morphology becomes less confined and the expanding flow produces shallow inundation of large areas of riverbed and floodplains that generates shear stresses below threshold. Although we have not considered transport of sediment mixtures, changing the grain size shows how the relative extent of bedload transport reduces as grain size increases (Fig. 4) through increasing the critical shear stress.



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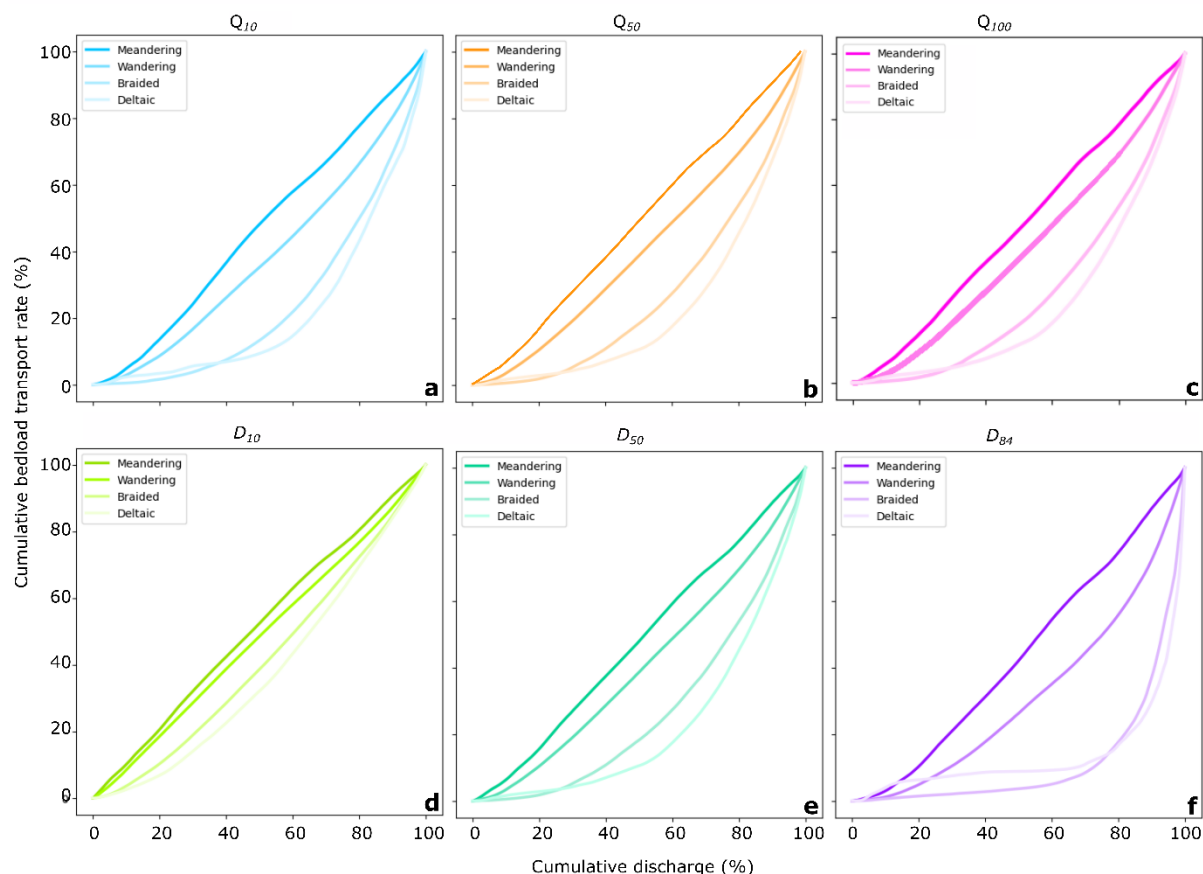


Figure 5: Cumulative bedload transport rate against cumulative water discharge for each model cell in rank order of water discharge. All data re-scaled onto a 0-100% scale to enable comparison of the shapes of distributions. Data are shown for different discharges (Q_{10} , Q_{50} and Q_{100}) (a-c) and grain sizes (D_{10} , D_{50} and D_{84}) (d-f).

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Bedload transport rates calculated for single grain sizes within each reach are positively skewed, with higher median values in the meandering and wandering reaches (Fig. 3) than in the braided and deltaic reaches. In the absence of data on spatial variability of sediment size, the distributions of bedload transport rates within each reach are more informative than their absolute values. These distributions correlate with the distributions of water discharge (Fig. 5) and hence shear stress across each reach.

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Both the locations and rates of bedload transport show significant differences between the four reaches. Whether in terms of flow magnitude or bed grain size, both inundated areas (Figs. 2,4) and transport rates (Fig. 3) show consistent changes from meandering through to deltaic patterns. These results support the initial hypothesis, and the double-mass plots (Fig. 5) demonstrate how the roles of overall mean shear stress, represented by water discharge, and critical shear stress, represented by grain size, interact to produce distinct patterns of bedload transport in the different reaches. The temporal fluctuations in transport rates that are increasingly seen as intrinsic features of bedload processes (Ancey, 2020; Paola, 1996) are thus determined by channel pattern at larger scales, consistent with formalization of bedform Church & Jones (1982) and bedload (Hoey, 1992) scales. Our results begin to quantify the influence of channel pattern on sediment transport, enabling improved understanding of the causes of unsteady sediment transport (Dhont & Ancey, 2018).

3.2 Controls over channel pattern

The spatial distributions of bedload transport are correlated with channel pattern and hence influence the maintenance of the morphologies of each reach. Downstream changes in channel pattern in the Bislak are related to confinement reducing downstream, resulting from both natural and anthropogenic reasons that are beyond our scope; rather, we consider the reaches as independent exemplars of different channel patterns. Progressing downstream, bedload transport occurs over a decreasing proportion of bed area, and that transport is at decreasing rates (Fig. 3). The scales of temporal variations in bedload transport will also change systematically in response to changes in flow depths and velocities, bed grain-size and consequently bedform types and sizes. As bedload transport is more size selective at lower excess stresses (Wilcock et al., 2009), local sorting of bedload and down-bar fining will become more apparent downstream (Rice & Church, 2009). Consequently, spatial patterns of deposition and erosion will determine the scale and sedimentology of sedimentary deposits formed in the different reaches (Kostic & Aigner, 2007; Rice & Church, 2009).

The concentration of bedload into dominant channels (Fig. 2) echoes analysis from braided (Ettema & Armstrong, 2019; Williams et al., 2015) and alternate bar rivers (Adams & Eaton, 2022), supporting arguments for considering channel pattern in terms of distributions of channels (Ghosh et al., 2023; Tejedor et al., 2022) or bed elevations (Andréault et al., 2024). Calibration of point-scale bedload transport relations remains challenging (Ancey, 2020; Ancey & Pascal, 2020) and improved descriptions of channel form that allow total bedload transport rates to be computed using simplified hydraulics (Adams & Eaton, 2022) would have practical benefits. Distributions of shear stress and sediment transport also inform understanding of in-stream habitats (Schwendel et al., 2010) with implications for river management and restoration.

The analysis above uses a single DEM, ignores grain sorting and makes other simplifying assumptions. There are numerous opportunities to extend this analysis, for example relating differences between successive DEMs to spatial patterns of shear stress. Ongoing improvements to data availability, including bathymetric LiDAR to accelerate DEM production (Kastdalen et al., 2024) and remotely sensed grain size (Marchetti et al., 2022), will enable refinement of the approach.



4 Conclusions

A 2D hydraulic model over a high-resolution DEM along 33 km of four distinct, contiguous reaches of a gravel-bed river was used to predict spatial patterns and frequency distributions of bed shear stress and bedload transport. Bedload is concentrated within deeper and faster flowing areas of the bed in all reaches, with excess shear stress decreasing downstream from meandering to wandering to braided and deltaic reaches. Estimated bedload transport rates also decline downstream, and double-mass plots show how bedload becomes increasingly concentrated in areas of high excess stress in the braided and deltaic reaches. Spatial variability in bedload transport is thus shown to be a function of channel pattern, with implications for our understanding of temporal variability in bedload, process-form relationships in different river patterns, design and maintenance of critical river infrastructure, and the management and restoration of riverscape habitat.

Appendix 1: Methods

A1.1 Study area

The gravel-bed Bislak River, the Philippines, features a longitudinal sequence of meandering, wandering, braided and deltaic channel patterns within a 33 km reach (Fig. 1A; Table S1; Tolentino et al., 2022). The confined single thread meandering reach has a moderate sinuosity main channel. The partially-confined and low sinuosity wandering reach shows a transition from single- to multi-thread channels. The braided reach contains multiple channels at all flow stages, and the deltaic reach contains multiple distributary channels. Both the braided and deltaic reaches have low overall sinuosity and are laterally unconfined. The longitudinal gradient progressively decreases downstream.

A1.2 Topographic survey

A seamless representation of the wet and dry parts of the study area was generated by fusing an airborne LiDAR survey, echo-sounding of pools > 2 m deep and spectrally-based depth retrieval estimates (Legleiter, 2021) from orthoimagery acquired at the time of the LiDAR survey. Vertical errors are detailed in Quick et al. (2025); the dry LiDAR, echo-sounding and depth retrieval components had Root Mean Square Errors (RMSE) of 0.045, 0.250 and 0.345 m, respectively. The 12.96 km² system-scale DEM was used for two-dimensional hydraulic modelling.

A1.3 Hydraulic modelling

Flow was simulated using the full St Venant shallow water equations in widely-used (e.g. Gori et al., 2020; Masafu et al., 2024) HEC-RAS2D. 3 m and 5 m 2D grid cells were used for the active channel and floodplain, respectively. The model was calibrated by varying Mannings n and comparing outputs to a cloud-free K3 satellite image of a 3 km long braided section acquired during the 1043 m³.s⁻¹ Typhoon Ineng high-flow event (23/08/2019). A constant n value of 0.05 achieved a fit congruency (Bates and De Roo, 2000) of 75% (Tolentino et al., 2024), similar to that achieved for other braided rivers (e.g.



Williams et al., 2013). A steady-state input boundary condition used 10-, 50- and 100-year return period flows, from calibrated rainfall-runoff modelling (Paringit et al., 2017). The downstream boundary condition was normal depth. Shear stress calculations for all model cells were exported for bedload transport rate calculations.

A1.4 Bedload transport rate

Unit bedload transport rate by mass, g_b , was calculated using a generalised form of the Meyer-Peter and Müller relation:

$$g_b = c[\tau - \tau_c]^k = c[g\rho RS - \tau_c]^k \quad (1)$$

where τ is bed shear stress (N.m^{-2}), τ_c critical shear stress (N.m^{-2}), g acceleration due to gravity (m.s^{-2}), ρ density of water (kg.m^{-3}), and R hydraulic radius (m). R is A/P , where A is wetted area (m^2) and P is wetted perimeter (m) of a grid cell face. S is the slope of the energy grade line (m/m), calculated between the centres of adjacent downstream cells. The constant c is set to 1 for convenience and k was taken as 1.5 (results for $k=1.8$ are in SI) (Huang, 2010).

Critical shear stress, τ_c , was calculated as:

$$\tau_c = \theta_c g D (\rho_s - \rho) \quad (2)$$

where θ_c is the dimensionless critical shear stress, D a representative grain size (m), and ρ_s particle density (kg.m^{-3}). Soulsby & Whitehouse's (1997) approximation of the Shields (1936) curve (equation 3) was used to calculate θ_c where D_* is the dimensionless grain-size (equation 4):

$$\theta_c = [0.30 + 1.2D_*] + 0.055[1 - \exp(-0.020D_*)] \quad (3)$$

$$D_* = [g(s_s - 1)/\nu^2]^{1/3} D \quad (4)$$

where s_s is ρ_s/ρ and ν kinematic viscosity at a specific water temperature ($\text{m}^2.\text{s}^{-1}$), taken as 20°C . Three representative grain sizes were used; D_{16} , D_{50} , and D_{84} of the active layer (Hoey & Ferguson, 1994) calculated by combining grain size distributions from five bulk surface and five bulk subsurface samples.

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230 **Author contributions**

Conceptualisation: LQ, TBH, RDW

Investigation: LQ, TBH, RDW

Methodology: LQ, TBH, RDW

Data curation: LQ, CM

235 Formal analysis: LQ

Visualisation: LQ

Writing – section draft and editing: LQ, TBH, RDW, RJB

Writing – manuscript review and editing: RDW, TBH, RJB, PMLT, CPCD

Funding acquisition: RDW, CPCD, TBH, PMLT

240 **Open research**

Data used in this manuscript is available from https://glamy.sharepoint.com/:f/g/personal/richard_williams_glasgow_ac_uk/EkgMYz4UhH9Lsv8Rg60BftwBjS2ngnRtzIUidsGdDE4fXQ?e=wwp3fS Following peer review, these data will be made freely available from the UKRI-NERC Environment Information Data Centre (dataset currently under embargo during peer review).

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