

A quantitative methodology for analysing physical damage and recovery dynamics from concurrent and consecutive hazards: forensic insights from Puerto Rico

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Abstract. Space and time play a crucial role in multi-hazard impact assessment. When two or more natural hazards occur at the same location simultaneously or in sequence, the physical integrity of assets and infrastructures can be compromised, and the resulting damage can be greater than that generated by individual hazards occurring in isolation. Despite widespread conceptual recognition of these interactions, the literature lacks quantitative, standardised methods for systematically analysing multi-hazard impacts. This study presents a quantitative methodology for evaluating multi-hazard physical damage to the built environment, translating qualitative impact dynamics into a transparent and reproducible analytical framework, implemented as modular Python code. The approach covers both concurrent and consecutive hazards by modelling: (i) the increased damage resulting from the combined impact of two or more concurrent hazards that overlap in space and time, and (ii) the effects of cumulative damage on asset vulnerability and the recovery dynamics in case of consecutive hazards that overlap in space. Using the Python implementation, a model behaviour analysis is conducted to systematically explore how variations in inter-event time intervals, vulnerability interactions, and recovery trajectories affect cumulative physical damage. The methodology is applied to a real multi-hazard sequence in Puerto Rico, including the concurrent wind and flood impacts of Hurricane Maria and the consecutive seismic impacts of the 2019–2020 earthquake sequence. The forensic reconstruction highlights that ignoring residual hurricane damage would significantly underestimate the subsequent earthquake losses, and that damage accumulation is path-dependent, strongly influenced by event timing and recovery processes. By providing a generalised, transparent, and reproducible quantitative structure, this study offers a tool for forensic analysis of past multi-hazard events, systematic exploration of damage drivers, and scenario-based assessment of alternative hazard and recovery conditions, supporting both post-disaster learning and planning-oriented applications.

1 Introduction

20 In recent years, increasing attention from the scientific community and international frameworks has been drawn to multi-
(hazard)-risk assessment and management (Ward et al., 2022). There has been a growing acknowledgement that natural hazard
events may occur simultaneously, in cascade, or cumulatively over time, and can interplay with societal factors such as exposure
and vulnerability, to generate complex multi-risk disaster scenarios (de Ruiter et al., 2020; de Ruiter and van Loon, 2022). These
compound events, such as heavy rainfall and extreme wind from the same convective storm (e.g. Tilloy et al. (2022)), cascading
25 events such as earthquakes triggering tsunamis (e.g. Mimura et al. (2011)), or even consecutive independent events (e.g. NASA
(2021)), can generate an impact that is different from that of individual hazards occurring in isolation (Gill and Malamud,
2014). Moreover, in an increasingly interconnected world, natural hazards' impacts cascade across geographical and sectoral
boundaries, leading to considerable challenges for disaster risk managers, including emergency management agencies, asset
managers, and operators of critical infrastructures and lifelines (Hochrainer-Stigler et al., 2023; Pasino et al., 2021). Although
30 more complex, approaches that account for multiple hazards and their interconnections better capture the real risk many areas
of the world are exposed to and can support the definition of effective disaster risk reduction (Kappes et al., 2012).

In contrast to single-hazard risks, the multi-risk assessment poses a series of challenges at each step of the risk or impact
assessment, from the hazard modelling to the vulnerability characterisation, until the final risk or impact assessment (Kappes
et al., 2012; De Angeli et al., 2022). Although significant improvements have been made in developing approaches that can
35 identify and quantify interrelationships between hazards (Tilloy et al., 2019), as well as understanding their spatial and tempo-
ral overlap dynamics (Claassen et al., 2023), the quantification of impacts arising from multiple hazards and the development
of generalised models for assessing multi-hazard physical damage remain a partially unexplored domain (Gentile et al., 2022).
Several conceptual frameworks offer qualitative descriptions of multi-hazard impact interactions, as well as schematic repre-
sentations of their temporal dynamics in the form of graphs and conceptual schemes, such as those proposed by de Ruiter et al.
40 (2020), De Angeli et al. (2022), and Wenzel et al. (2026). These frameworks also identify key factors that can influence the
magnitude of impacts, such as spatial overlap, the time window between successive events, and the recovery dynamics of the
impacted elements, among others. Specifically, in the case of consecutive events, the impacts of an earlier event are likely to
change the vulnerability at the time of the next event (de Ruiter and van Loon, 2022). In addition, recovery of vulnerability to
pre-disaster conditions after the event ended plays a key role. Societies and systems that recover quickly from disasters become
45 less vulnerable to the next event than societies that follow a slower recovery path (Di Baldassarre et al., 2018).

Nevertheless, there remains a lack of studies that attempt to translate these considerations into a quantitative formulation
and move towards their quantification. The majority of available multi-hazard physical impact quantitative models are seismic-
related models, i.e., models where at least one of the two considered hazards is an earthquake, and focus on specific critical
infrastructures, such as bridges (Gentile et al., 2022). Furthermore, modelling of the recovery process remains a significant
50 challenge (Mohammadi et al., 2024). Most of the damage models currently used do not address the temporal dimension of
post-disaster loss and recovery or treat it in a simplistic fashion (Miles and Chang, 2006; Sarker and Lester, 2019). Very little
research has been conducted on how recovery proceeds over time (e.g., Cimellaro et al. (2010); Loos et al. (2023)), or on the

social and economic factors that affect the recovery process (e.g., Miles et al. (2019); Koliou et al. (2020); Hariri-Ardebili et al. (2022)). Consequently, a deeper understanding of how these factors affect cumulative multi-hazard impacts is still lacking.

55 This paper aims to bridge this gap by providing a structured quantitative methodology that translates conceptual representations of multi-hazard damage dynamics into an explicit and reproducible analytical structure. To this end, compound and consecutive impact dynamics described graphically and schematically by de Ruiter et al. (2020) and De Angeli et al. (2022) are reformulated into a compact mathematical expression and implemented as a modular Python code. This formulation enables explicit representation of inter-event time intervals, state-dependent vulnerability interactions, and recovery trajectories
60 within a unified structure. Using this implementation, a model behaviour analysis is conducted to systematically investigate how these key parameters influence compound and cumulative physical damage in a multi-hazard context. Although such mechanisms are widely acknowledged qualitatively in the literature, they are rarely modelled in quantitative terms within a single coherent framework. The primary contribution of this work, therefore, lies in offering a reproducible analytical template that supports systematic exploration of multi-hazard damage interactions and facilitates structured post-disaster interpretation
65 and learning. Beyond reconstructing past events, the proposed methodology can also support anticipatory and scenario-based analyses, enabling exploration of how cumulative multi-hazard damage may evolve under alternative assumptions, such as different recovery pathways or inter-event intervals.

The proposed approach is then applied to a real multi-hazard sequence in Puerto Rico from a forensic perspective. In this application, the multi-hazard damage model is used to reconstruct and interpret the evolution of direct physical damage following Hurricane Maria and the subsequent seismic sequence, illustrating how residual vulnerability and incomplete recovery
70 shape cumulative impacts. The case study, therefore, serves as a demonstration of how the proposed quantitative structure can support post-disaster analysis and learning in complex multi-hazard contexts.

This paper is organised as follows. Section 2 presents the structured quantitative methodology for analysing multi-hazard damage dynamics, beginning with the mathematical formulation of the damage model and followed by the analysis of model
75 behaviour. Section 3 illustrates the forensic application of the approach to a real-world case study in Puerto Rico, addressing the concurrent wind and flood impacts of Hurricane Maria and the consecutive impacts of the 2019–2020 seismic sequence. Finally, Section 4 discusses limitations and future developments, and Section 5 summarises the main conclusions.

2 From qualitative frameworks to quantitative multi-hazard dynamics

Based on the works by de Ruiter et al. (2020) and De Angeli et al. (2022), two main multi-hazard impact dynamics can be
80 identified: (i) concurrent impacts, generated by hazards which either completely or partially overlap in space and time; (ii) consecutive impacts, generated when spatially overlapping hazards occur close enough in time that the assets do not have sufficient time to completely recover before the onset of the second hazard. These two dynamics are qualitatively depicted in Fig. 1, using the physical integrity as an impact variable. The physical integrity $y_j(t)$ of an asset j is related to its physical damage $d_j(t)$ by the relationship:

$$85 \quad y_j(t) = 1 - d_j(t), \quad y_j \in [0, 1] \quad (1)$$

$y_j(t) = 1$ indicates no impact on the element's physical integrity and $y_j(t) = 0$ represents complete destruction.

Concurrent impacts result from two hazard events that overlap in space and time, either completely or partially. The second event occurs simultaneously with the first or during its response phase, so that recovery has not yet begun when the second event occurs. Real-world examples include the 2018 events in Indonesia, where a 7.5 magnitude earthquake in Sulawesi triggered a tsunami, causing extensive coastal damage (Sabah and Sil, 2023; Naik et al., 2023; Opabola et al., 2023). Another example, which does not involve causal relationships between events, is the 2013 earthquake in the Philippines, followed by a typhoon before recovery from the earthquake had begun (Lagmay and Eco, 2014; Pormon et al., 2023; Lagmay et al., 2015). In such scenarios, the impacts of both events combine and affect the asset. The primary challenge is to quantitatively assess the overall amplification of physical damage caused by the superimposition of multiple loads.

Consecutive impacts occur when hazard events that spatially overlap occur close enough in time that assets do not have sufficient time to completely recover before the onset of the second hazard. Real-world examples include the sequence of earthquakes and floods in Nepal in 2015. An earthquake with a magnitude of 8.0 struck Nepal in April 2015, causing significant structural and non-structural damage. The region was then hit by heavy rains and floods in 2017 (Gautam and Dong, 2018). Recovery and reconstruction documents (He et al., 2018; Liu et al., 2021) show that the floods affected structures and areas still recovering from the previous earthquake. Another example is Hurricane Irma and Maria, which devastated Puerto Rico in 2017, followed by an earthquake in the same area two years later. This case is analyzed in detail in Sect. 3. The main challenge with consecutive impacts is to estimate residual damage based on the asset's recovery dynamics and to understand how the residual damage influences vulnerability to the subsequent hazard.

To enable the quantitative investigation of compound and consecutive impacts, the dynamics graphically described in Fig. 1 are translated into a compact and easily implementable mathematical formulation, as presented in Appendix A. This generalised piecewise defined function allows the estimation of relative damage over time to an asset or infrastructure j exposed to n natural hazards. The behaviour of the function is controlled by the parameters Θ and μ , defined by Eqs. (A5) and (A6) in Appendix A. Depending on the values assumed by the parameters, the formulation represents different multi-hazard impact dynamics:

- If $\Theta = 0$, the function models concurrent impacts, i.e., damage caused by hazards that overlap in space and time, either fully or partially.
- If $\Theta = 1$ and $\mu = 0$, it models consecutive impacts, where spatially overlapping hazards occur close enough in time that the asset has insufficient time to fully recover before the second hazard occurs.

If $\Theta = 1$ and $\mu = 1$, the impacts are treated as independent, allowing the function to perform a series of single-hazard damage assessments without incorporating any multi-hazard interactions. The detailed formulation of the two multi-hazard impact dynamics, concurrent and consecutive, is presented in Sect. 2.1 and Sect. 2.2 respectively. The formulation for independent impacts is provided in Appendix A1.

The generalised formulation is implemented in Python to enable reproducible and modular multi-hazard damage assessment. The implementation follows directly the mathematical structure described in Appendix A, where event classification (concurrent, consecutive, independent) is determined dynamically through the parameters Θ and μ , and damage evolution is

120 computed at the asset level across discrete time steps. Within the tool, recovery functions $R_{j,i}(t)$ are explicitly defined as time-dependent functions (linear, exponential, logistic, or user-defined), allowing different durations and restoration trajectories depending on asset type and contextual assumptions. After each hazard event, the state of the asset is updated by storing residual damage, which subsequently modifies the vulnerability function applied to the next event in the case of consecutive impacts. This ensures consistency between recovery progression and state-dependent fragility adaptation. The framework is

125 modular in structure: hazard inputs, exposure data, fragility curves, and recovery assumptions are treated as interchangeable components. This design allows users to test alternative recovery trajectories, introduce modified fragility parameters, or simulate different event sequences without altering the core computational logic. While the present study applies the implementation for model behaviour analysis and forensic validation in Puerto Rico, the structure supports broader scenario-based applications and integration with external hazard workflows. Full implementation details and data access are provided in Sect. *Code and*

130 *data availability*.

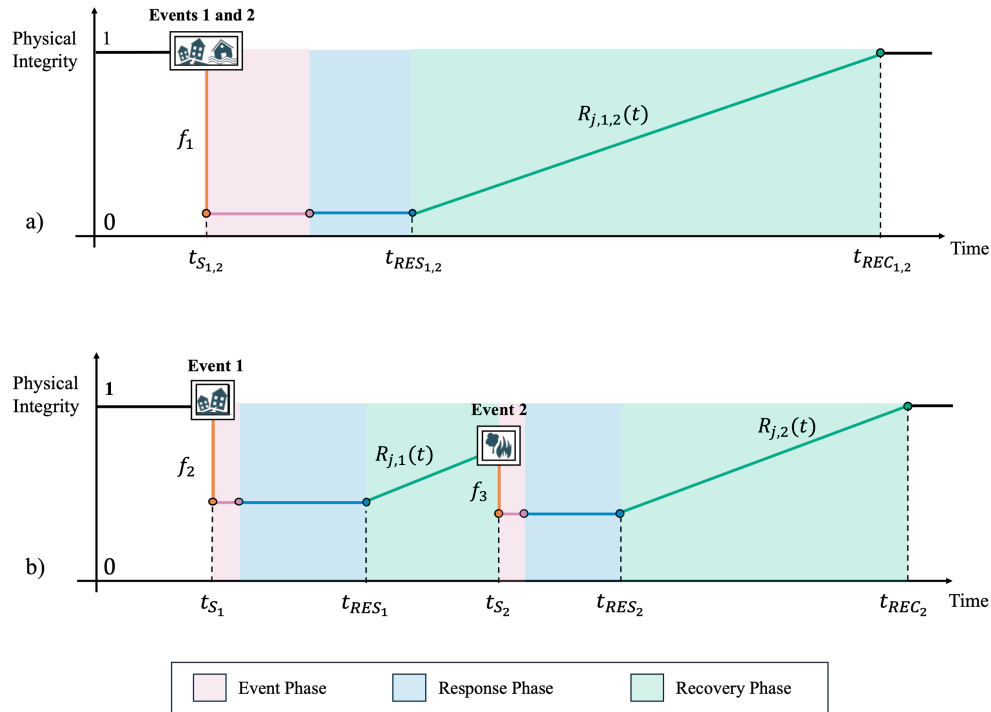


Figure 1. Variation of physical integrity over time for concurrent and consecutive multi-hazard impact dynamics. **Panel a:** The impacts are concurrent. The second event in temporal order affects the asset during the response phase of the previous one. The second impact and the preceding one are considered simultaneous. The loss of physical integrity is the amplified combination of the two stressors. Details in Sect. 2.1. **Panel b:** The impacts are consecutive. The second event in temporal order affects the asset during the long-term recovery phase of the previous one. Details in Sect. 2.2.

2.1 Concurrent impact dynamics

Direct physical damage over time t to an asset or infrastructure j caused by two concurrent impacts, as graphically represented in Fig. 1, panel (a), can be calculated according to Eq. (2).

$$d_j(t)[t_{S_1}, t_{REC_{1,2}}] = \begin{cases} f_1 & \text{if } t_{S_1} \leq t < t_{RES_{1,2}} \\ f_1 \cdot R_{j,1,2}(t) & \text{if } t_{RES_{1,2}} \leq t < t_{REC_{1,2}} \end{cases} \quad (2)$$

135 with

$$f_1 = f_{v_{j,1,2}}(h_{1,\max}, h_{2,\max}) \quad (3)$$

According to Eq. (2), at any time t between the start of the first hazard event t_{S_1} and the end of the response phase of the multi-hazard event $t_{RES_{1,2}}$, asset j experiences a level of damage equal to f_1 . After the response phase of the multi-hazard event concludes (i.e., for $t \geq t_{RES_{1,2}}$), the asset begins to recover from the concurrent impacts according to the recovery function $R_{j,1,2}(t)$, until $t = t_{REC_{1,2}}$.

Equation (A1) represents the damage model used to quantify the effects of two concurrent hazards, referred to as the "concurrent damage model." This model assesses the combined impact of both hazards on asset performance. In the literature, concurrent damages are typically evaluated using bivariate vulnerability or fragility functions. Accordingly, the model is expressed as $f_{v_{j,1,2}}$, where the resulting damage depends on the maximum intensity of each hazard event, $h_{1,\max}$ and $h_{2,\max}$. Gentile et al. (2022) classifies this approach as a "vector-valued fragility model." Bivariate vulnerability functions have been applied in single-hazard scenarios, such as assessing flood damage considering both flow velocity and duration (Elmer et al., 2010; Nofal and van de Lindt, 2020; Ming et al., 2015), and in multi-hazard contexts, such as hurricanes, where structural impacts are evaluated by combining the effects of coastal surges and wind forces (Do et al., 2020; Nofal et al., 2021). However, there are instances where concurrent damages are calculated using "state-dependent fragility models" (Gentile et al., 2022), where the fragility of an asset to a secondary hazard is conditional on its damage state after the primary hazard. This approach is applied, for example, to assess the impacts of an earthquake-tsunami combination, where the fragility curve for the post-shock tsunami depends on the earthquake-induced damage (Xu et al., 2021; Gómez Zapata et al., 2023).

2.2 Consecutive impact dynamics

Direct physical damage over time t to an asset or infrastructure j caused by two consecutive impacts is calculated according to Eq. (4).

$$d_j(t)[t_{S_1}, t_{REC_2}] = \begin{cases} f_2 & \text{if } t_{S_1} \leq t < t_{RES_1} \\ f_2 \cdot R_{j,1}(t) & \text{if } t_{RES_1} \leq t < t_{S_2} \\ f_3 \cdot [1 - f_2 \cdot R_{j,1}(t_{S_2})] + f_2 \cdot R_{j,1}(t_{S_2}) & \text{if } t_{S_2} \leq t < t_{RES_2} \\ \{f_3 \cdot [1 - f_2 \cdot R_{j,1}(t_{S_2})] + f_2 \cdot R_{j,1}(t_{S_2})\} \cdot R_{j,2}(t) & \text{if } t_{RES_2} \leq t < t_{REC_2} \end{cases} \quad (4)$$

with

$$f_2 = f_{v_{j,1}}(h_{1,\max}) \quad (5)$$

$$f_3 = f_{v_{j,2|d(t_{S_2})}}(h_{2,\max}) \quad (6)$$

160 According to Eq. (4), at time t_{S_1} , due to the impact of the first hazard event, the asset j experiences a level of damage equal to f_2 . Equation (A2) represents a single hazard damage model (e.g., a depth-damage curve for floods or a fragility curve for earthquakes), as a function of the maximum intensity of the hazard events $h_{1,\max}$. After the response phase of the first event is complete (that is, for $t \geq t_{RES_1}$), the asset begins to recover from the impacts of a single danger according to the recovery function $R_{j,1}(t)$. At time t_{S_2} , the asset is still recovering from the previous hazard event when it is impacted by a second event.

165 The damage caused by this consecutive event is expressed as $f_3 \cdot [1 - f_2 \cdot R_{j,1}(t_{S_2})] + f_2 \cdot R_{j,1}(t_{S_2})$. This expression accounts for the sum of the residual damage at time t_{S_2} , denoted by $R_{j,1}(t_{S_2})$, and the additional damage from the second event, which is calculated as the percentage damage caused by the second event, represented by f_3 , applied to the remaining undamaged portion of the asset, i.e., $[1 - f_2 \cdot R_{j,1}(t_{S_2})]$. This approach prevents the double-counting of damage. After the response phase of the second event concludes (i.e., for $t \geq t_{RES_2}$) the asset begins to recover from the consecutive impacts according to the

170 recovery function $R_{j,2}(t)$, until $t = t_{REC_2}$. This evolution of damage in time, as described in Eq. (4), is graphically represented in Fig. 1, panel (b).

Equation (A3) represents the damage model used to quantify the effects of two consecutive impacts, known as the "consecutive damage model." This model is based on a "state-dependent fragility model" (Gentile et al., 2022), denoted as $f_{v_{j,2|d(t_{S_2})}}$. It defines the fragility or vulnerability of an asset to a secondary hazard, conditional on the asset's residual damage state due to

175 incomplete recovery. The resulting damage is a function of the maximum intensity of the second hazard $h_{2,\max}$ and the residual damage to the asset calculated at t_{S_2} according to the recovery function of the asset. State-dependent fragility models are relatively scarce in the literature and are mainly developed within the seismic field to assess the effects of a primary event followed by aftershocks on an already weakened asset (Li et al., 2014; Aljawhari et al., 2021). Another application in the seismic domain involves evaluating the worsening condition of assets, often bridges, due to factors like time and corrosion. In this scenario, the

180 primary seismic event impacts an asset in a deteriorated state, resulting in increased damage (Otárola et al., 2022).

2.3 Model behaviour under consecutive multi-hazard impact dynamics

To investigate the internal mechanics of the proposed formulation under consecutive multi-hazard dynamics, a model behaviour analysis is conducted via a structured parameter influence assessment. The objective is to examine how the mechanisms embed-

ded in Eq. 4 generate additional cumulative damage relative to the independent baseline configuration. The analysis, therefore,
 185 isolates the endogenous amplification effects arising from the interaction between residual damage, recovery progression, and
 state-dependent vulnerability. The investigation focuses on consecutive interactions because their cumulative effects emerge
 over time as each hazard occurs sequentially. In consecutive events, residual damage and evolving fragility modify the re-
 sponse to subsequent loading, producing additional loss amplification through the recursive update term in Eq. 4–A3. In
 contrast, concurrent impacts are captured directly by the bivariate damage function in Eq. 2, which defines the combined effect
 190 of simultaneous hazards at a single time step. Since concurrent effects are already structurally integrated in the formulation, the
 analysis concentrates on consecutive interactions to isolate and quantify the unique mechanisms driving cumulative damage
 across sequential events.

Three parameters are examined, consistent with the conceptual drivers identified by de Ruiter et al. (2020) and De Angeli
 et al. (2022):

- 195 (i) the inter-event time interval (Δt);
- (ii) the recovery trajectory $R_{j,1}(t)$;
- (iii) state-dependent modifications of the second-event vulnerability function.

Figure 2 reports additional cumulative loss as a function of Δt under three alternative recovery trajectories: exponential,
 linear, and logistic. These functional forms, commonly adopted in resilience modelling (Cimellaro et al., 2010; Loos et al.,
 200 2023), represent distinct temporal distributions of restoration capacity and therefore different persistence patterns of residual
 damage.

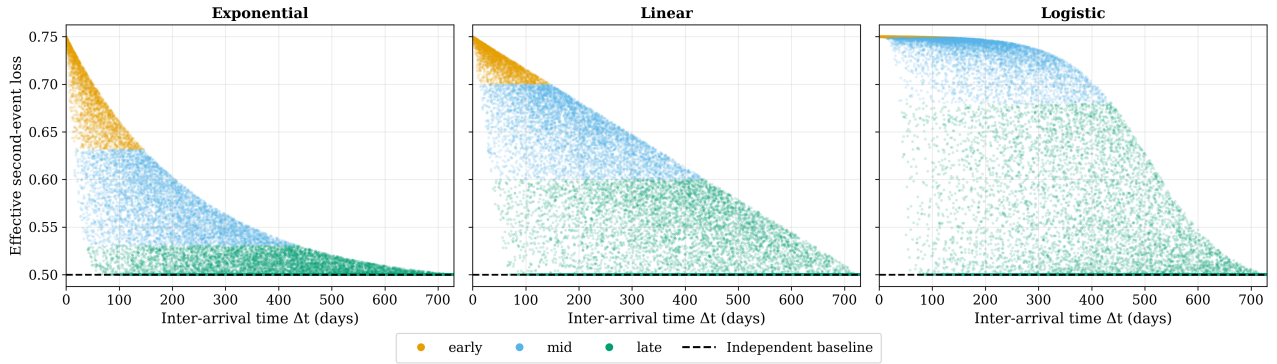


Figure 2. Additional cumulative loss as a function of inter-arrival time (Δt) under exponential, linear, and logistic recovery assumptions. The dashed line represents the independent baseline.

When the second event occurs during the early recovery phase, cumulative damage substantially exceeds the independent
 baseline. As Δt increases, additional cumulative loss decreases and asymptotically converges toward independent behaviour.

However, both the rate and magnitude of convergence are governed by the functional form of $R_{j,1}(t)$. Under exponential recovery, rapid early restoration reduces residual damage quickly, limiting amplification. Linear recovery produces intermediate behaviour. Logistic recovery, characterised by delayed early restoration and accelerated later recovery, prolongs vulnerability persistence and sustains elevated amplification over a wider Δt range. These results show that recovery trajectory assumptions are structurally influential within Eq. 4. The assumed recovery trajectory directly determines how long residual damage persists and, therefore, how likely the second event is to interact with a weakened system. Assuming instantaneous or implicitly complete recovery collapses this mechanism and systematically biases cumulative loss toward additive behaviour. The second test isolates the contribution of state-dependent vulnerability (Eq. A3). The vulnerability function of the second event is progressively shifted (+10%, +20%, +30%) to represent increasing fragility due to incomplete recovery. Although state-dependent fragility formulations have been explored primarily in seismic contexts (Gentile et al., 2022; Gómez Zapata et al., 2023), they are rarely embedded within a general multi-hazard quantitative structure.

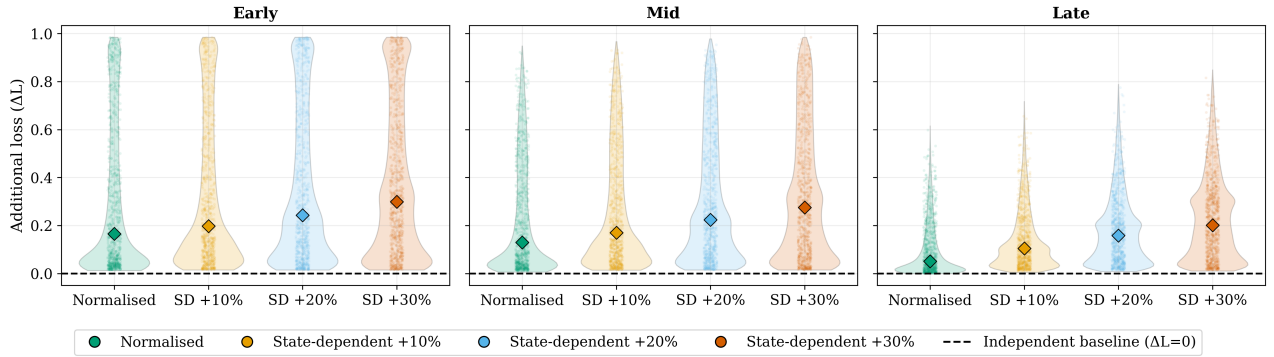


Figure 3. Distribution of additional cumulative loss (ΔL) under increasing state-dependent vulnerability modification. The dashed line indicates the independent baseline ($\Delta L = 0$).

Figure 3 shows that state-dependent vulnerability modification generates convex, non-linear amplification of cumulative damage. Even moderate fragility shifts (+10%) produce measurable increases in additional loss, while larger shifts (+30%) substantially increase both median outcomes and upper-tail behaviour. Crucially, amplification does not arise solely from residual damage magnitude, but from the alteration of the fragility profile itself. Through Eq. A3, incomplete recovery modifies the system's response function, changing the probability structure of damage exceedance. In this sense, consecutive multi-hazard interaction is not merely additive accumulation but a structural reconfiguration of vulnerability between events. The recovery trajectory should not be interpreted as an abstract modelling parameter. Empirical evidence shows that recovery dynamics reflect governance effectiveness, institutional capacity, infrastructure robustness, and socioeconomic conditions (Miles et al., 2019; Koliou et al., 2020; Hariri-Ardebili et al., 2022). At the macro scale, such dimensions can be synthesised through composite recovery capacity indicators, such as the Recovery Gap Index (RGI) (Borre et al., 2025). Lower recovery capacity implies prolonged vulnerability persistence, increasing the likelihood that subsequent hazards interact with residual damage and trigger multiplicative effects.

Overall, the parameter influence analysis shows that cumulative loss in consecutive multi-hazard scenarios depends primarily on three factors: the time interval between events, the speed and shape of recovery, and possible modifications of vulnerability due to residual damage. When the second event occurs after substantial recovery has taken place, total damage remains close to the sum of the two independent events. In contrast, when recovery is incomplete and vulnerability is increased, the second event acts on a weakened system, producing higher cumulative losses than those obtained under independent modelling assumptions. The proposed formulation makes these mechanisms explicit by linking inter-event timing, recovery progression, and vulnerability modification within a single damage function. Rather than assuming that assets fully recover between events, the model allows vulnerability to evolve over time and directly influence subsequent damage estimates. In Sect. 3, this modelling framework is applied to the Puerto Rico disaster sequence, where incomplete recovery and evolving fragility conditions significantly influenced cumulative impacts.

3 Forensic multi-hazard damage analysis in Puerto Rico

Puerto Rico offers a highly relevant and well-documented case of consecutive multi-hazard interaction, having experienced a sequence of major disasters within a relatively short time window. The impacts of Hurricanes Irma and Maria in 2017 were followed by the 2019–2020 seismic sequence, creating a configuration in which the second hazard occurred during an incomplete recovery phase from the first.

The objective of this section is to apply the proposed quantitative multi-hazard damage formulation to a real disaster sequence to assess its explanatory capacity under empirical conditions. Adopting a forensic perspective, the analysis evaluates whether explicitly modelling residual damage and recovery trajectory, as formalised in Sect. 2.2 and analysed in Sect. 2.3, improves consistency between simulated and officially reported losses. In contrast to independent hazard modelling approaches, the proposed multi-hazard damage model allows vulnerability to evolve dynamically between events through the recovery trajectory $R_{j,1}(t)$ and state-dependent vulnerability modification. The Puerto Rico sequence provides an empirical setting in which these mechanisms can be evaluated against observed damage outcomes.

In September 2017, Puerto Rico was struck by Hurricanes Irma and Maria, causing extensive structural damage and infrastructure disruption (Amir et al., 2020; Morales-Velez et al., 2021; Kwasinski et al., 2019; Cangialosi et al., 2018; Pasch et al., 2023; Fischbach et al., 2020). Hurricane Maria alone resulted in nearly \$90 billion in damage (FEMA, 2018a). Reconstruction progressed unevenly, and by the end of 2019, significant portions of the building stock had not yet been fully restored (FEMA, 2019a; GAO, 2020). In January 2020, a magnitude 6.4 earthquake struck the island as part of a broader seismic sequence (Melendez-Colon et al., 2021; Hu et al., 2019), affecting regions that were still recovering from hurricane-induced damage. This temporal configuration makes Puerto Rico a particularly suitable case for examining the role of residual damage and incomplete recovery in shaping cumulative loss. Figure 4 illustrates the sequence and overlap of the two major types of hazards that affected Puerto Rico during the 2017–2020 period.

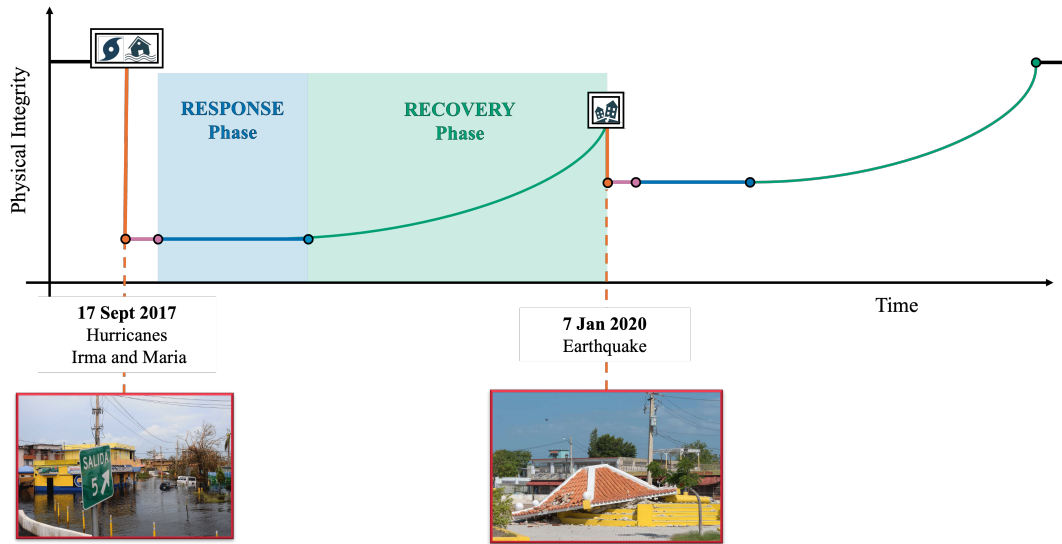


Figure 4. Representation of Puerto Rico's 2017-2020 disaster sequence. Images, from left to right: (i) Flooded area in Carolina, Puerto Rico, following Hurricane Maria's impact on the island, 29 September 2017. Photo by Sgt. Jose Ahiram Diaz-Ramos. Online image, Flickr. (ii) Severe earthquake damage to a gazebo in a public park in Guánica, Puerto Rico, 11 February 2020. Photo by Liz Roll/FEMA. Online image, NARA & DVIDS Public Domain Archive.

Puerto Rico is a densely inhabited island, characterised by a higher concentration of buildings in the San Juan metropolitan area, adjacent northern municipalities, and in the southern region around Ponce. These areas not only host a large share of the residential, commercial, and public infrastructure but also represent key nodes in the island's economic and logistical networks. The multi-hazard damage assessment performed applying our framework focuses on damages to the built-up area, using as input a portfolio of buildings provided by FEMA (2020). This portfolio was compiled as part of a recent data inventory conducted on the island after Hurricane Maria, and includes the following categories, along with their corresponding estimated replacement values FEMA (2020):

- **Residential:** $\sim 1.5 \times 10^6$ buildings; estimated replacement value ~ 300 billion USD.
- **Commercial:** $\sim 6 \times 10^3$ buildings; estimated value ~ 12 billion USD.
- **Industrial:** $\sim 1 \times 10^3$ buildings; estimated value ~ 2 billion USD.
- **Educational:** $\sim 1.2 \times 10^3$ buildings; estimated value ~ 3 billion USD.

The analysis is carried out in two phases. In the first, the impacts of Hurricane Maria are modelled by implementing a compound damage model (Sect. 2.1) that integrates wind and flood impacts. The central objective of the case study is to assess the damage dynamics associated with the subsequent seismic sequence and its interaction with a partially recovered built environment. Accordingly, the compound damage assessment from the hurricane impact simulation primarily serves to define

the post-event damage and recovery status that constitute the input for the consecutive damage model applied to the earthquake phase. The fragility curves used for this phase are those provided by FEMA for the specific context of Puerto Rico (Federal Emergency Management Agency, 2020). In the second phase, the consecutive damage model (Sect. 2.2) is applied to simulate the seismic impacts on structures already weakened by hurricane damage. Here, standard fragility curves provided by FEMA are modified ad-hoc to capture the changed vulnerability of assets previously affected by the hurricane and still exhibiting residual damage.

Input data includes:

- **Structural parameters:** Material, type, number of stories, code compliance.
- **Hazard inputs:** Wind speed, flood depth, spectral acceleration.
- **Vulnerability functions:** Hazus-based curves, modified to reflect state dependency.
- **Economic indicators:** Repair cost per unit area, downtime, and replacement costs.

The results are expressed in terms of physical loss (reduction in structural integrity) and economic cost.

3.1 Compound hurricane impacts: wind and flood interaction

The 2017 landfall of Hurricane Maria provides a real configuration of concurrent multi-hazard interaction, in which wind and flood hazards overlapped spatially and temporally across Puerto Rico. In this setting, damage amplification arises from the simultaneous action of multiple stressors acting on the same asset during the emergency phase, as formalised in Eq. 2.

Within the proposed damage model, compound hurricane damage is represented through a multi-parameter vulnerability formulation $f_{v,j,1,2}(h_{1,\max}, h_{2,\max})$ that accounts for the joint influence of peak wind intensity and flood depth under overlapping conditions. In practice, the concurrent formulation integrates standard Hazus wind fragility curves and flood depth-damage functions within the unified structure of Eq. 2. Hazus does not provide an explicit bivariate fragility surface for combined wind–flood loading. Instead, wind- and flood-induced damages are evaluated consistently using the respective Hazus vulnerability components, while their interaction is represented through the concurrent damage operator, which accounts for their temporal and spatial superposition. This approach ensures methodological consistency with the standard Hazus framework while preserving the multi-hazard interaction logic embedded in the proposed formulation.

Vulnerability functions are derived from the FEMA Hazus-MH methodology (FEMA, 2020). Wind fragility curves are parametrized according to structural typology, construction material, roof anchorage, number of storeys, and code compliance level. Flood damage is represented through depth-damage functions calibrated for different occupancy classes. From a physical standpoint, wind and flood mechanisms are structurally interdependent. High wind speeds induce roof uplift, envelope breach, and cladding failure, increasing structural susceptibility to water ingress. Subsequent or simultaneous inundation accelerates the deterioration of load-bearing and non-structural components. Post-event assessments indicate that buildings exposed to overlapping wind and flood loading experienced repair costs 30–40% higher than buildings exposed to a single hazard (FEMA,

2018b). Field observations further show that flood depths exceeding 1.5 m resulted in near-complete failure of unreinforced
305 masonry structures, particularly where prior wind damage had reduced lateral resistance (Rodriguez et al., 2021).

The modelled compound loss for Hurricane Maria is approximately \$90 billion, consistent with official economic assessments (National Oceanic and Atmospheric Administration, 2018). The agreement with reported losses does not result from post-event parameter fitting, but from the direct application of observed hazard intensities and standardised Hazus vulnerability functions within the concurrent formulation. In this phase of the Puerto Rico sequence, vulnerability parameters are
310 not modified between hazards; amplification derives from hazard superposition under overlapping conditions rather than from recovery-mediated fragility evolution. The subsequent seismic sequence, in contrast, introduces a fundamentally different mechanism, where damage persistence and state-dependent vulnerability shifts govern cumulative impacts.

3.2 The recovery process and subsequent seismic impacts

The earthquake sequence that began in late 2019 and culminated in the magnitude 6.4 event on 7 January 2020 struck Puerto
315 Rico at a time when many regions were still in the process of recovering from Hurricane Maria. This temporal overlap between the recovery phase and the occurrence of a new hazard event represents a critical scenario within multi-hazard damage assessment, where pre-existing damage and delayed reconstruction substantially influence the vulnerability landscape.

To spatially contextualise this interaction, Fig. 5 integrates three key spatial data sets: the track of Hurricane Maria (September 2017), the distribution of buildings still damaged as of November 2018 (based on Hazus post-event assessments), and the
320 contours of the peak ground acceleration (PGA) from the January 2020 earthquake. The post-hurricane assessment identified nearly 138,000 buildings in Puerto Rico that had not yet been fully repaired more than a year after the hurricane.

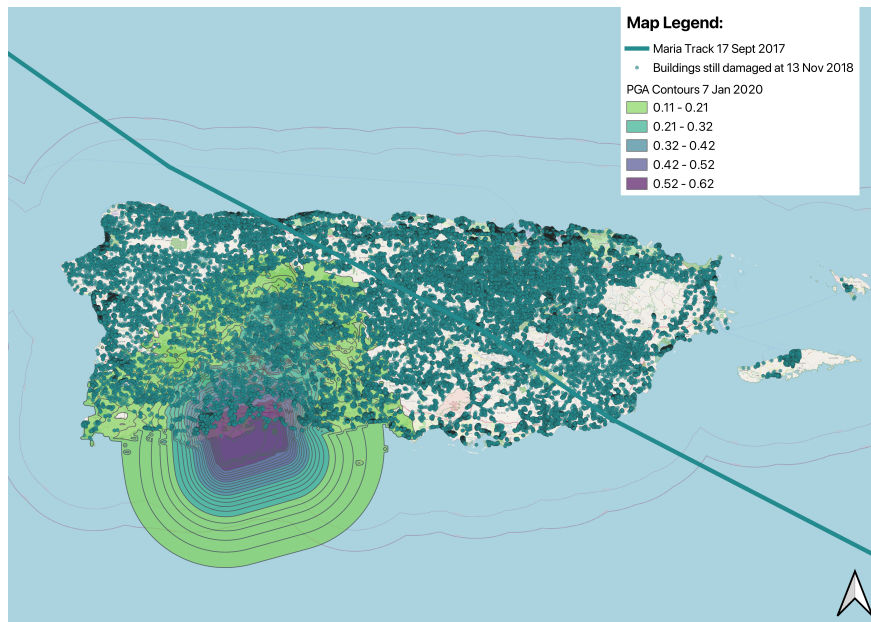


Figure 5. Map showing the track of Hurricane Maria (Sept. 2017), the spatial distribution of buildings with remaining hurricane damage (as of Nov. 2018), and PGA [g] contours from the January 2020 earthquake.

As illustrated in Fig. 5, many of the damaged buildings were concentrated in coastal and southern municipalities, including regions such as Ponce and Guayanilla, which later experienced the highest levels of ground shaking during the earthquake ($\text{PGA} > 0.5g$). These areas faced dual exposure, first to high winds and flooding from Hurricane Maria and later to seismic loading from the 2020 event. Residual structural weaknesses, whether due to incomplete reconstruction or substandard repairs, likely increased the risk of damage and collapse.

To model the seismic impacts on the buildings still damaged by the hurricane, a consecutive damage model (Sect. 2.2) is applied. Standard fragility curves provided by FEMA (Federal Emergency Management Agency, 2012) are transformed into state-dependent curves to properly account for residual damage. The approach introduces parametric adjustments to account for pre-existing damage conditions. Specifically, the median values of both structural and non-structural fragility curves are shifted according to hypothetical levels of residual damage. Given the absence of detailed spatialized building-level recovery data, a homogeneous distribution of residual damage is assumed throughout the building portfolio. In the absence of spatially explicit residual damage data, a predefined range of vulnerability modifications (5–30%) is explored, representing plausible reductions in structural capacity. The objective is not parameter calibration, but to evaluate how different residual damage assumptions influence cumulative loss estimates and their consistency with reported values. Although the modifications were applied uniformly, their impact is particularly pronounced in areas with high PGA values, where even small increases in vulnerability result in disproportionately large increases in expected losses.

Figure 6 illustrates the conceptual effect of residual damage on fragility curves. As residual damage increases, the curves change to the left, reflecting a greater susceptibility to damage at lower levels of seismic demand.

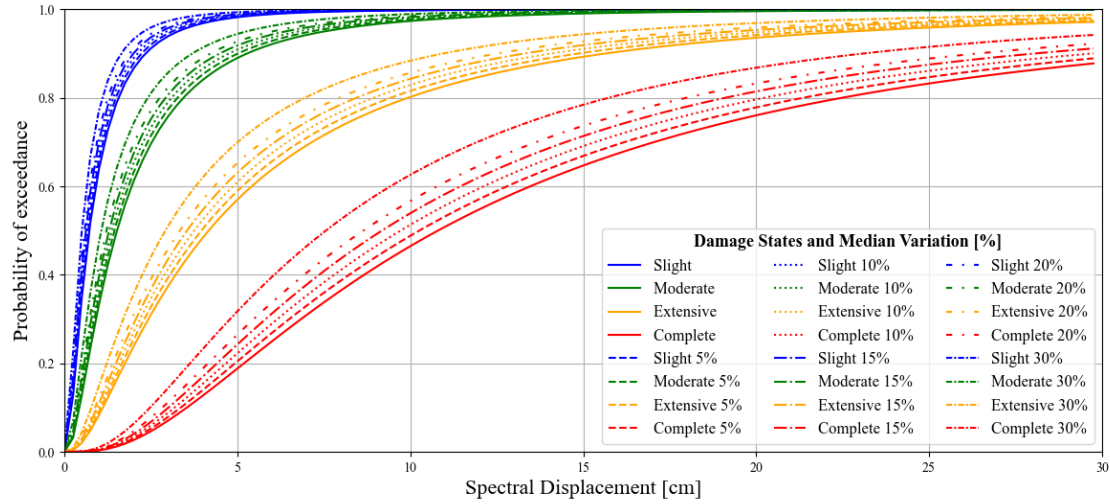


Figure 6. State-dependent fragility curves reflecting changes in structural vulnerability due to residual damage.

340 Simulated damage probabilities are translated into direct economic losses using the Hazus-MH damage-to-loss methodology (FEMA, 2020). For each building class and damage state, Hazus defines empirically derived loss ratios representing expected repair costs as a percentage of total replacement value. These ratios are based on historical U.S. claims data and post-disaster reconstruction evidence, and differentiate between structural and non-structural components. In this study, replacement values are taken directly from the FEMA building inventory for Puerto Rico (FEMA, 2020), ensuring internal consistency between exposure, vulnerability, and economic conversion assumptions. Total portfolio loss is obtained by multiplying damage state exceedance probabilities by the corresponding loss ratios and aggregating across building typologies.

To explore these variations, structural and non-structural fragility medians were progressively shifted between 5% and 30%, representing increasing levels of residual vulnerability. For each modification level, seismic damage was recomputed and converted into economic loss, allowing systematic evaluation of how cumulative impacts vary under different recovery assumptions. The results show that total loss increases more than proportionally as fragility medians are shifted toward lower capacity. Even modest modifications produce noticeable increases in simulated loss, while larger shifts lead to disproportionately higher damage estimates. The complete numerical matrix of results is reported in Appendix B, while Fig. 7 illustrates how total loss varies across structural and non-structural modification levels.

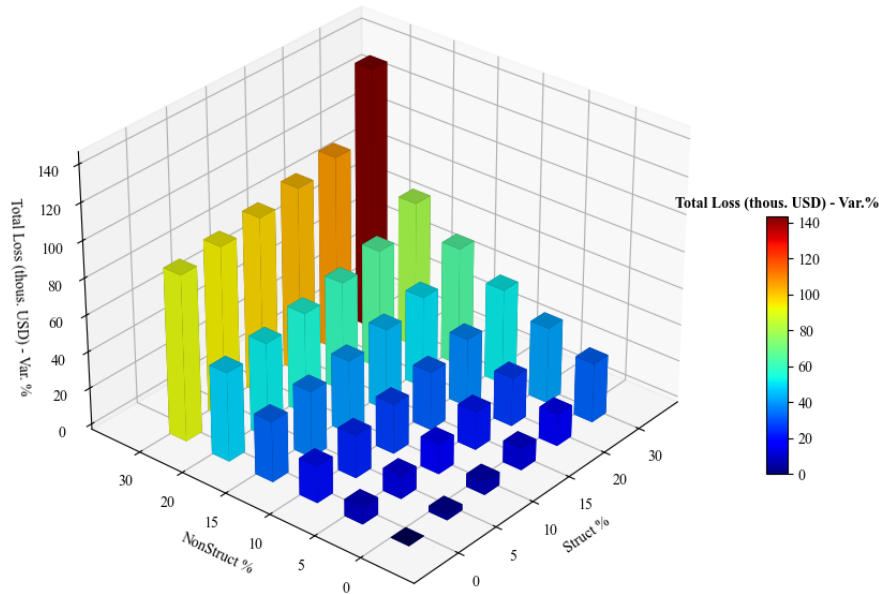


Figure 7. Relative (%) change in total simulated losses compared to the single-hazard case for increasing structural and non-structural vulnerability modifications.

Official damage estimates for the 2019–2020 seismic sequence amount to approximately 1,700,000 USD (Government of
 355 Puerto Rico, 2020). When the earthquake is modelled as an independent single-hazard event—thus assuming full recovery
 of building vulnerability after Hurricane Maria—the simulated loss equals 1,205,525 USD. This configuration underestimates
 the official figure by approximately 29%. The discrepancy indicates that assuming complete restoration of structural capacity
 before the earthquake is not consistent with the observed loss pattern. When state-dependent vulnerability is introduced, by
 shifting the median of both structural and non-structural fragility curves by 15%, the simulated total loss increases to 1,742,296
 360 USD, closely matching the official estimate. This modification represents a plausible level of residual vulnerability at the time
 of the seismic sequence and falls within the systematic range explored in Sect. 2.3 (5–30%).

The difference between the two modelling configurations directly reflects the mechanism described in Eq. 4. In the inde-
 pendent configuration, the recovery function implies full restoration before the second event, and the earthquake acts on an
 undamaged system. In the state-dependent configuration, residual damage from the hurricane shifts the fragility curves to-
 365 ward lower capacity, increasing damage probabilities under the observed PGA levels. The improved agreement with reported

Table 1. Comparison between official and modelled seismic losses (USD).

Source	Total damage [USD]
Official Government of Puerto Rico (Government of Puerto Rico, 2020)	1,700,000
Modelled damage with state-dependent vulnerability modification (15%)	1,742,296
Modelled damage with independent fragility curves	1,205,525

losses does not result from ex-post parameter fitting, but from the structural effect of incorporating incomplete recovery within the vulnerability formulation. The 15% modification lies within the predefined exploration range and represents one plausible residual capacity scenario rather than a calibrated value. The Puerto Rico case confirms that neglecting residual damage persistence leads to systematic underestimation of cumulative impacts in consecutive multi-hazard sequences.

370 **4 Discussion**

This study translates key concepts frequently discussed qualitatively in the multi-hazard risk literature by translating them into a structured quantitative methodology, implemented as an open-source Python code. The results demonstrate that these concepts are not only theoretically relevant but can quantitatively affect damage estimates when explicitly represented. While the mathematical formulation builds on existing single-hazard models, its novelty lies in its capacity to integrate multiple
375 elements that, when addressed quantitatively, are usually treated separately (such as multi-hazard vulnerability models and recovery dynamics), and in its practical and easy-to-use application through the development of a dedicated Python code.

The methodology accounts for damage mechanisms arising from both concurrent and consecutive hazards, including the combined effects of simultaneous hazards and the influence of residual damage and recovery in successive events. By adopting a hazard-independent formulation, the model can be applied to any combination of sudden-onset hazard typologies. Furthermore,
380 it allows for the seamless integration of existing multi-hazard damage models, including vector-valued or state-dependent fragility models (Gentile et al., 2022).

The model behaviour analysis (Sect. 2.3) identifies inter-event time intervals, vulnerability interactions, and recovery trajectories (shape and duration) as key drivers of multi-hazard direct physical damage. Additional cumulative loss is highest when subsequent events occur during early recovery, and its magnitude strongly depends on the assumed recovery trajectory. Slower
385 or prolonged recovery phases sustain vulnerability and increase compound losses. Even moderate vulnerability modification levels generate non-linear increases in cumulative damage, indicating that incomplete recovery alters the fragility profile of assets rather than simply adding residual damage. Overall, the results confirm that multi-hazard impacts are path-dependent and may transition from additive to multiplicative behaviour depending on the interaction between event timing and evolving system conditions.

390 The forensic application to Puerto Rico (Sect. 3) provides a real-world setting in which both concurrent (wind–flood interactions during Hurricane Maria) and consecutive (hurricane–earthquake sequence of 2019–2020) damage mechanisms were observed. After estimating hurricane-induced losses, the model simulates the additional impact of the subsequent seismic se-

quence on a portfolio of buildings. Central to this application is the development of ad hoc seismic state-dependent fragility curves, systematically explored within a predefined modification range to reflect the residual damage conditions caused by the hurricane. Rather than applying standard fragility functions, the approach adjusts fragility parameters for both structural and non-structural components according to the conditional post-event damage state, thereby embedding incomplete recovery directly into the vulnerability representation. This forensic reconstruction allows damage accumulation mechanisms to be explicitly quantified. Multi-hazard impacts are evaluated in both physical and economic terms, enabling comparison with official earthquake loss estimates (Table 1). The closer agreement between modelled and reported losses demonstrates that incorporating temporally dynamic vulnerability substantially improves cumulative impact estimation. The results confirm that damage is not just additive in concurrent and consecutive events, but is path-dependent and strongly conditioned by event order, timing, and recovery dynamics.

Notably, quantitative forensic analyses of multi-hazard events do more than retrospectively explain observed losses, as they can provide a pathway for extrapolating and refining multi-hazard impact models. By reconstructing impact sequences and explicitly quantifying how vulnerability evolves between events, such approaches can enable, for example, the derivation and calibration of state-dependent vulnerability functions that capture inter-event interactions, as those derived for the Puerto Rico building portfolio.

Beyond retrospective investigation, the quantitative methodology implemented here has potential for anticipatory and planning-oriented applications. By systematically varying key parameters, such as recovery trajectories, inter-event time intervals, or vulnerability interactions, the model allows exploration of how cumulative damage may develop under alternative scenarios. Such scenario-based and “what-if” analyses can inform preventive planning and mitigation strategy assessment. However, the reliability of these forward-looking applications depends on the availability of empirically grounded parameterisations and robust calibration of vulnerability and recovery functions. Without calibration, results remain illustrative rather than fully predictive, but they still provide a comparison of alternative scenarios, structured information on how total damage responds to variations in key parameters, supporting post-disaster analysis and scenario comparison.

4.1 Assumptions and limitations

The quantitative methodology presented for multi-hazard damage dynamics and its forensic application in Puerto Rico are subject to assumptions and limitations that define the scope of validity of the results.

Focus on sudden-onset hazards. The multi-hazard damage formulation proposed in this study primarily targets sudden-onset hazards, characterised by short-duration events such as hurricanes and earthquakes, where the event phase is brief compared to the subsequent response and recovery phases. This assumption is particularly relevant for the Puerto Rico case study, where Hurricane Maria and the 2019-2020 earthquake sequence are treated as discrete events with well-defined temporal boundaries. However, this focus excludes slow-onset hazards such as droughts, sea-level rise, or subsidence, which evolve over extended periods and may blur the distinctions between the event, response, and recovery phases (Terzi et al., 2022). Although this limitation does not diminish the applicability of the framework to sudden-onset events, it underscores the need for ad-hoc modelling approaches for long-duration slow-onset hazards.

Direct physical impacts only. The quantitative implementation focuses exclusively on direct physical damage to the built environment and does not capture indirect effects such as business interruptions, supply chain disruptions, or social impacts. In Puerto Rico, the prolonged loss of electricity and water after Hurricane Maria led to widespread socioeconomic challenges, including health crises, migration, and economic decline in key sectors such as agriculture and tourism (Fischbach et al., 2020; Peters et al., 2021). These indirect effects, while significant, fall outside the scope of the presented quantitative investigation.

Assumptions about the recovery process. In the Python code, and as a consequence, in the model behaviour analysis presented, the recovery process is modelled as a series of linear or exponential functions representing slow, medium, or fast recovery speeds. This approximation facilitates analysis but oversimplifies the inherently non-linear nature of recovery, which is influenced by a multitude of factors. In Puerto Rico, for example, bureaucratic inefficiencies, delayed federal funding, and inequitable distribution of resources significantly delayed recovery efforts in certain regions (Group, 2020; OCHA, 2020). Moreover, the proposed multi-hazard damage formulation assumes uniform recovery rates across structural and non-structural components, which may not reflect reality. Non-structural elements, such as utilities and interior finishes, often recover faster than structural systems, leading to mismatches in the actual recovery trajectory (FEMA, 2019b).

Simplification of temporal dynamics. In the proposed multi-hazard damage formulation, it is assumed that physical integrity is lost immediately at the onset of the event, and no further degradation occurs during the response phase. While this assumption is practical for mathematical modelling, it does not capture cases where damage continues to accumulate after the hazard peaks, such as when flooding persists or secondary hazards occur. In addition, physical integrity is assumed to remain constant during the response phase, despite minor fluctuations that may occur due to emergency repairs or further deterioration. Although these simplifications do not introduce significant bias, they limit the ability to model more complex temporal dynamics observed in real-world scenarios (Porter et al., 2020).

Generalized spatial resolution. The forensic analysis in Puerto Rico adopts a portfolio-based approach, grouping buildings into categories based on general characteristics such as structural type, construction material, and occupancy use. While this approach is suitable for regional-scale assessments, it does not capture localised variations in vulnerability or hazard exposure. In Puerto Rico, differences in topography, proximity to fault lines, and floodplain dynamics played a significant role in shaping the spatial distribution of damage (Baker et al., 2021; FEMA, 2020). These localised effects were approximated rather than explicitly modelled, potentially reducing the precision of damage estimates.

Economic impact modelling limitations. The economic losses in the Puerto Rico case study were estimated using standard unit repair costs, downtime estimates, and sector-specific multipliers. Although these methods provide a useful approximation, they do not account for broader macroeconomic effects, such as long-term population decline, loss of workforce productivity, or disruptions in international trade. For example, the loss of agricultural infrastructure during Hurricane Maria had cascading effects on food security and export revenues, which are not explicitly captured in this study (Fischbach et al., 2020; Group, 2020).

Uncertainty in state-dependent fragility curves. Adjustment of fragility curves to reflect residual damage is based on proportional modifications to the median curve values. Although this method effectively accounts for cumulative damage, it assumes uniform vulnerability changes across all buildings within a category. In reality, building-specific factors such as construction

quality, maintenance history, and localised damage patterns may lead to significant variability in vulnerability (Nofal and van de Lindt, 2020; Porter et al., 2020). This limitation highlights the need for more granular data to refine the state-dependent fragility model.

465 In conclusion, while the proposed approach provides a reproducible analytical template that supports systematic exploration of multi-hazard damage interactions and facilitates forensic analyses, its assumptions and limitations must be carefully considered, specifically when interpreting the results of the Puerto Rico case study. Addressing these limitations in future developments, such as incorporating more sophisticated recovery models, indirect impacts, and higher spatial resolution, will improve the accuracy and applicability of the approach, allowing more comprehensive assessments of compound and consecutive multi-hazard impact scenarios.

4.2 Future developments

Building on the current limitations of the proposed methodology, several promising avenues for improvement can be identified. These advances would not only improve the accuracy and applicability of the approach but also broaden its potential for integration into various fields of disaster risk reduction and management. Key directions for future developments are discussed below.

Better understanding and modelling recovery dynamics. The dynamics of the recovery process are central to the assessment of residual damage and the interactions between consecutive hazard impacts. Specifically, the timing of the response phase (t_{RES}) determines whether the hazard impacts are classified as concurrent or consecutive, while the timing and shape of the recovery phase (t_{REC} and $R_j(t)$) significantly influence the residual damage for subsequent events. The response phase, while critical for civil protection and disaster preparedness, has received limited attention in the scientific literature, often being conflated with the recovery phase. However, its proper evaluation is essential to improve disaster safety plans and understand its cascading effects on recovery (UNISDR, 2015; Consiglio dei Ministri, 2018; IFRC, 2020; Toyoda et al., 2021). More attention has been paid to recovery dynamics, particularly in the context of seismic resilience. Recovery dynamics are highly variable, often following linear, exponential, or logistic patterns depending on socio-economic, political, and governance factors. The pioneering work of Miles and Chang introduced one of the first models of recovery behaviour after an earthquake, proposing recovery trajectories of the community (Miles and Chang, 2006). Based on this, Cimellaro et al. (2010) developed an advanced method for the quantification of resilience by integrating recovery and preparedness metrics. Recent studies have highlighted the importance of recovery models in post-disaster decision-making (Marasco et al., 2022; Fountain and Cradock-Henry, 2020; Loos et al., 2023), underscoring the need for reliable recovery functions. However, challenges remain in quantifying recovery due to the complexity of the influencing factors, including governance, technology, economic conditions, and social cohesion. Emerging methodologies, such as Agent-Based Models (ABMs), offer promising avenues to simulate recovery processes by integrating interactions between individuals, institutions, and resources (Xu and Chopra, 2022). These models complement traditional approaches like community surveys and questionnaires, which are invaluable for understanding local recovery dynamics and identifying barriers to resilience (Jones and Ballon, 2020; Opabola et al., 2023).

495 ***Providing more reliable multi-hazard damage models.*** Improving multi-hazard damage models is essential for capturing the cumulative effects of consecutive hazards. Future research should focus on integrating damage-state-dependent functions that dynamically modify vulnerability and fragility curves based on residual damage from prior events. For example, scenarios involving hurricanes followed by earthquakes, as demonstrated in the Puerto Rico case study, require models capable of adapting to changes in structural and non-structural vulnerabilities caused by sequential impacts (Porter et al., 2020; Nofal and
500 van de Lindt, 2020).

Evaluating dynamic exposure over time. In the current implementation, exposure is assumed to remain constant and is not explicitly modelled within the framework. However, exposure is inherently dynamic, evolving over time due to maintenance, retrofitting, and functional changes in assets. Hazard impacts can reduce exposure through physical damage, but exposure may increase following recovery processes or new construction. Future developments should aim to model these variations over
505 time, capturing the cyclical nature of exposure changes in response to hazards and human interventions (Gomez-Cunya et al., 2022; Loos et al., 2023).

Incorporating indirect impacts through functionality modelling. The presented approach currently focuses on direct physical damage but does not explicitly address indirect impacts, such as loss of functionality, economic disruption, or cascading failures in interconnected systems. Future iterations could incorporate functionality as a key metric, using physical integrity as
510 a proxy to estimate functionality (Miles et al., 2019; Opabola et al., 2023). This approach would enable assessments of broader systemic impacts, including business interruptions and supply chain disruptions.

Adapting the formulation to slow-onset hazard dynamics. The multi-hazard damage assessment formulation is tailored to sudden-onset hazard dynamics, where event durations are short relative to the response and recovery phases. However, slow-onset hazards such as droughts, coastal erosion, and subsidence require a fundamentally different modelling approach.
515 Extending the framework to account for these dynamics would improve its applicability to a wider range of hazard scenarios (Terzi et al., 2022).

Advancing the model toward predictive multi-hazard applications. While the present approach demonstrates its value in forensic reconstruction and model behaviour analysis, its extension toward predictive multi-hazard risk assessment represents a crucial direction for future research. At present, vulnerability transitions and recovery trajectories are parameterised using
520 stylised assumptions that are suitable for exploratory analysis but may not be sufficiently robust for forward-looking risk forecasting. To enable predictive applications, future developments should focus on: (i) empirical calibration of state-dependent fragility transitions across hazard combinations, (ii) development of transferable parameter sets that can be applied in data-scarce regions, and (iii) integration with probabilistic hazard occurrence models to simulate realistic multi-hazard event sequences. In particular, coupling the current damage accumulation formulation with stochastic event generation models would
525 allow simulation of long-term compound risk under different climate or seismic scenarios. Such integration would transform the model from a post-event analytical tool into a prospective decision-support instrument capable of evaluating mitigation strategies and recovery policy alternatives under uncertainty. However, achieving this transition requires a stronger empirical foundation. Without these developments, predictive outputs may remain highly sensitive to modelling assumptions, limiting their reliability for operational risk management.

This paper provides a structured quantitative methodology for assessing direct physical damage to exposed assets subjected to multiple natural hazards that can overlap or occur sequentially over time. Specifically, it translates previously conceptual representations of multi-hazard impact dynamics into an explicit and reproducible analytical structure, implemented as a modular Python code. Unlike existing models that focus on specific asset-hazard combinations, the proposed formulation is designed to be broadly applicable to multiple hazards, capturing the complexities of concurrent, consecutive, and independent hazard interactions. A key contribution of this work is the incorporation of recovery dynamics and state-dependent vulnerability interactions into the damage assessment process. The modular Python implementation ensures flexibility, enabling users to customise hazard parameters, vulnerability functions, and recovery processes and apply the methodology to their specific case study. It can support structured forensic reconstruction of past multi-hazard events, such as the Puerto Rico sequence, as well as forward-looking scenario-based analyses under alternative assumptions of hazard timing, vulnerability evolution, and recovery pathways.

A structured model behaviour analysis was conducted through the Python code to systematically investigate how inter-event timing, vulnerability interactions, and recovery trajectories influence compound and cumulative physical damage. While such mechanisms are widely acknowledged qualitatively in the literature, they are rarely examined quantitatively within a single coherent and reproducible analytical structure. The results highlight that neglecting recovery dynamics or state-dependent vulnerability adjustments can lead to substantial underestimation of multi-hazard damage. The model behaviour analysis also illustrates the potential of the approach for scenario-based planning, as it enables systematic exploration of alternative assumptions on hazard timing, recovery pathways, and vulnerability evolution, supporting anticipatory multi-hazard risk assessment.

The proposed approach is then applied to a real multi-hazard sequence in Puerto Rico from a forensic perspective. In this application, the Python-based quantitative structure is used to reconstruct and interpret the evolution of direct physical damage following Hurricane Maria and the subsequent seismic sequence. By incorporating state-dependent fragility curves to adjust asset vulnerability based on residual damage, the model reproduces damage patterns consistent with reported loss estimates, highlighting the importance of explicitly accounting for hazard interactions and recovery dynamics to capture multi-hazard losses better. Importantly, the forensic application also enabled the derivation of state-dependent damage curves from observed cumulative impacts, demonstrating that post-disaster analysis can inform vulnerability models that explicitly account for residual damage and incomplete recovery.

Despite its contributions, the methodology has limitations, particularly in assuming uniform recovery rates and focusing solely on direct physical impacts while neglecting broader indirect socio-economic consequences. Future developments will address these challenges by refining recovery modelling, incorporating dynamic exposure changes, and expanding the applicability of the framework to slow-onset hazards. In addition, integrating functionally-based assessments and indirect economic losses will enhance its comprehensiveness.

Code and data availability. The Python implementation of the framework, along with detailed documentation, is freely available on GitHub at the following link: <https://github.com/AlessandroBorre/multi-hazard-impact-framework.git>

Appendix A: Multi-hazard damage formulation

565 The continuous piecewise-defined function presented in Table A1 provides the relative damage over time $d_j(t)$ to an asset or infrastructure j caused by n natural hazard events. The events $i \in [1, n]$ are ordered according to their starting time t_{S_i} , and considered two by two.

Table A1. Generalised damage formulation across time intervals for asset j

Start Time	End Time	Damage Function $d_j(t)$
t_{S_i}	$\Theta \cdot t_{RES_i} + (1 - \Theta) \cdot t_{S_{i+1}}$	$\Theta \cdot f_2 + (1 - \Theta) \cdot f_1$
t_{RES_i}	$t_{S_{i+1}}$ (only if $\Theta = 1$)	$\Theta \cdot f_2 \cdot R_{j,i}(t)$
$t_{S_{i+1}}$	$\Theta \cdot t_{RES_{i+1}} + (1 - \Theta) \cdot t_{RES_{i,i+1}}$	$\Theta \cdot (\mu \cdot f_4 + (1 - \mu) \cdot (f_3 + [f_2 \cdot R_{j,i}(t_{S_{i+1}})] \cdot (1 - f_3))) + (1 - \Theta) \cdot f_1$
$\Theta \cdot t_{RES_{i+1}} + (1 - \Theta) \cdot t_{RES_{i,i+1}}$	$\Theta \cdot t_{REC_{i+1}} + (1 - \Theta) \cdot t_{REC_{i,i+1}}$	$\Theta \cdot (\mu \cdot f_4 + (1 - \mu) \cdot (f_3 + [f_2 \cdot R_{j,i}(t_{S_{i+1}})] \cdot (1 - f_3))) \cdot R_{j,i+1}(t) + (1 - \Theta) \cdot f_1 \cdot R_{j,i,i+1}(t)$

with

$$f_1 = f_{v_{j,i,i+1}}(h_{i,\max}, h_{i+1,\max}) \quad (\text{A1})$$

570 $f_2 = f_{v_{j,i}}(h_{i,\max}) \quad (\text{A2})$

$$f_3 = f_{v_{j,i+1|d(t_{S_{i+1}})}}(h_{i+1,\max}) \quad (\text{A3})$$

$$f_4 = f_{v_{j,i+1}}(h_{i+1,\max}) \quad (\text{A4})$$

and the parameters reported in Table A2.

Table A2. Description of symbols used in the multi-hazard damage formulation.

Symbol	Description
t_{S_i}	Starting time of hazard event i
t_{F_i}	Ending time of hazard event i
t_{RES_i}	End of the response phase from hazard event i
$t_{RES_{i,i+1}}$	End of the response phase from the overlapping events i and $i + 1$
t_{REC_i}	End of the recovery phase from hazard event i
$t_{REC_{i,i+1}}$	End of the recovery phase from overlapping events i and $i + 1$
$f_{v_{j,i}}$	Single-impact damage model for asset j under hazard event i
$f_{v_{j,i+1,i}}$	Concurrent impact damage model: vulnerability function quantifying damage caused by compound impacts from overlapping events i and $i + 1$
$f_{v_{j,i d}}$	Consecutive impact damage model: vulnerability function quantifying damage caused by event i , conditional on residual damage d
$h_{i,\max}$	Maximum magnitude reached by hazard event i
$R_{j,i}$	Recovery rate of asset j from the damage caused by hazard event i
$R_{j,i,i+1}$	Recovery rate of asset j from the damage caused by overlapping events i and $i + 1$

The type of impact interaction is governed by the parameters Θ and μ , which allow the model to represent different dynamics (concurrent, consecutive, or independent) within a single, consistent framework. These parameters are formally defined using Heaviside step functions as follows:

$$\Theta(t_{S_{i+1}}, t_{RES_i}) = \mathcal{H}(t_{S_{i+1}} - t_{RES_i}), \quad (A5)$$

$$\mu(\Theta, t_{S_{i+1}}, t_{REC_i}) = \mathcal{H}(t_{S_{i+1}} - t_{REC_i}), \quad \text{if } \Theta = 1. \quad (A6)$$

The parameters classify the type of multi-hazard impact as follows:

- $\Theta = 0$: Impacts are classified as *concurrent*. The formulation in Table A1 simplifies to Eq. (2) in the main text.
- $\Theta = 1, \mu = 0$: Impacts are classified as *consecutive*. The formulation in Table A1 simplifies to Eq. (4) in the main text.
- $\Theta = 1, \mu = 1$: Impacts are classified as *independent*. The formulation simplifies to Eq. (A7) reported in this appendix.

A1 Independent impacts

In the case of two consecutive hazards where the second hazard event occurs after the end of recovery of the first one, the
585 impacts can be considered independent. In such a case, the evolution of the damage over time can be seen as a series of single-hazard dynamics.

Direct physical damage over time t to an asset or infrastructure j caused by concurrent impacts can therefore be simply calculated according to Eq. (A7).

$$d_j(t)[t_{S_1}, t_{REC_2}] = \begin{cases} f_2 & \text{if } t_{S_1} \leq t < t_{RES_1} \\ f_2 \cdot R_{j,1}(t) & \text{if } t_{RES_1} \leq t < t_{REC_1} \\ 0 & \text{if } t_{REC_1} \leq t < t_{S_2} \\ f_4 & \text{if } t_{S_2} \leq t < t_{RES_2} \\ f_4 \cdot R_{j,2}(t) & \text{if } t_{RES_2} \leq t < t_{REC_2} \end{cases} \quad (A7)$$

590 with

$$f_2 = f_{v_{j,1}}(h_{1,\max}) \quad (A8)$$

$$f_4 = f_{v_{j,2}}(h_{2,\max}) \quad (A9)$$

According to Eq. (A7), at time t_{S_1} , the first hazard event causes the asset j to sustain damage quantified as f_2 . Once the response phase of the first event concludes (i.e., for $t \geq t_{RES_1}$), the asset begins to recover from the damage using the recovery
595 function $R_{j,1}(t)$. By $t = t_{REC_1}$, the asset has fully recovered, resulting in a residual damage level of zero, which remains unchanged until a second hazard occurs at t_{S_2} .

At t_{S_2} , the second hazard affects the asset, causing damage quantified as f_4 . Similarly, once the response phase of this second event is completed (i.e., for $t \geq t_{RES_2}$), the asset begins to recover according to the recovery function $R_{j,2}(t)$. By $t = t_{REC_2}$, the asset again reaches a residual damage level of zero. Equations (A8) and (A9) describe single-hazard damage models as
600 functions of the maximum intensities of hazard events, $h_{1,\max}$ and $h_{2,\max}$, respectively. It is assumed here that the damages from both events occur entirely at the onset of each event. This evolution of damage in time, as described in Eq. (A7), is graphically represented in Fig. A1.

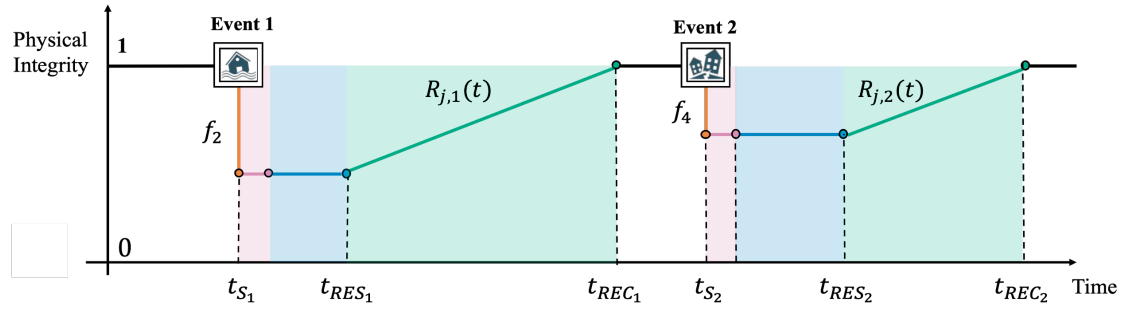


Figure A1. Variation of physical integrity over time in the case of two independent impacts. The second event in temporal order affects the asset when it has already completed the recovery phase of the previous one.

Although it may seem that the impacts in this scenario could be assessed by treating the two events as independent single hazards, the situation is more complex. In an ideal analytical scenario, the system's vulnerability may have either decreased or increased after reconstruction following the first event. Some studies suggest that both structural and non-structural attributes can improve in response to previous events, as seen in the "build back better" theory (Kennedy et al., 2008; Neeraj et al., 2021). Consequently, a second event with similar characteristics could cause more or less damage, depending on how the recovery and reconstruction process unfolded after the initial response phase. Given this scenario, it becomes crucial for risk assessment and management to update the system's vulnerability and exposure after the recovery process to accurately calculate the risks posed by consecutive hazards.

Appendix B: Numerical results for state-dependent vulnerability modification

This appendix reports the complete numerical matrix of simulated seismic losses for different combinations of structural and non-structural vulnerability modification levels applied in the Puerto Rico case study (Sect. 3.2).

The baseline fragility curves are derived from FEMA Hazus (Federal Emergency Management Agency, 2012). State-dependent vulnerability modification is introduced by progressively reducing the median parameters of the fragility functions between 0% and 30% for both structural and non-structural components. For each combination, seismic damage probabilities are computed and converted into economic loss using the Hazus damage-to-loss ratios described in Sect. 3.2.

Loss values are expressed in USD and represent aggregated portfolio losses across all building classes included in the FEMA inventory for Puerto Rico.

Table B1. Total simulated seismic losses (USD) under different combinations of structural and non-structural vulnerability modification levels.

	NonStruct 0%	NonStruct 5%	NonStruct 10%	NonStruct 15%	NonStruct 20%	NonStruct 30%
Struct 0%	1,205,525	1,316,141	1,446,902	1,602,471	1,789,239	2,294,623
Struct 5%	1,245,367	1,355,773	1,486,192	1,641,565	1,828,054	2,331,851
Struct 10%	1,292,172	1,402,442	1,532,614	1,687,487	1,873,685	2,376,321
Struct 15%	1,347,889	1,457,732	1,587,716	1,742,296	1,927,840	2,429,457
Struct 20%	1,414,843	1,524,206	1,653,575	1,807,901	1,933,072	2,493,172
Struct 30%	1,595,392	1,703,806	1,832,623	1,985,067	2,168,596	2,934,148

620 The matrix shows that loss increases more than proportionally when both structural and non-structural vulnerability modifi-
cations are combined.

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editing, T.G.: Conceptualization, Writing – review & editing, R.R.: Conceptualization, G.Z.: Methodology, G.B.: Conceptualization, Writ-
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