

# Runoff Evaluation in an Earth System Land Model for Permafrost

## Regions in Alaska

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**Abstract.** Modeling of hydrological runoff is essential for accurately capturing spatiotemporal feedbacks within the land-atmosphere system, particularly in sensitive regions such as permafrost landscapes. However, substantial uncertainties persist in the terrestrial runoff parameterization schemes used in Earth system and land surface models. This is particularly true in permafrost regions, where landscape heterogeneity is high and reliable observational data are scarce. In this study, we evaluate the performance of runoff parameterization schemes in the Energy Exascale Earth System Model (E3SM) land model (ELM). Our proposed framework leverages simulation results from the Advanced Terrestrial Simulator (ATS), which is a physics-based integrated surface/subsurface hydrologic model that has been successfully evaluated previously in Arctic tundra regions. We used ATS to simulate runoff from 22 representative hillslopes in the Sagavanirktok River basin, located on the North Slope of Alaska, then compared the output with ELM's parameterized representation of total runoff. Results show that 1) ELM's total runoff was the same order of magnitude as the ATS simulations, and both models were similarly variable over time; 2) minor adjustments to coefficients in ELM's runoff parameterization improved the match between the ATS simulation and ELM's parameterized representation of annual and seasonal total runoff; 3) overall, runoff responses in ATS and ELM are more similar in flat hillslope environments compared to steep hillslopes; and 4) shallower active layer thicknesses and higher precipitation simulations resulted in lower correlations between the two models due to greater total runoff. By incorporating the optimized runoff coefficients from the Sagavanirktok River basin into ELM, the simulated total runoff better matched the streamflow observations at a small watershed located on the Seward Peninsula of Alaska. Our findings revealed important insights into the effectiveness of runoff parameterizations in land surface models and pathways for improving runoff coefficients in typical Arctic regions.

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34 **1 Introduction**

35 Runoff parameterization schemes play a critical role in the accuracy of Earth system models, particularly in sensitive  
36 environments such as high latitude permafrost regions. These areas are increasingly vulnerable to climate variability, and the  
37 hydrological responses associated with warming temperatures can have profound implications for ecosystems and water  
38 resources (Bring et al., 2016; Yang & Kane, 2020). The interplay between hydrology and climate dynamics in permafrost  
39 zones is complex because conditions such as vegetation, snow, soil wetness, ground ice content, and biogeochemical activities  
40 vary significantly over small spatial extents (Holmes et al., 2013; Bennett et al., 2022). At the same time, Earth system models  
41 and land surface models are designed for pan-Arctic scale simulations, creating a strong mismatch between the scale at which  
42 these processes occur and the models designed to represent them (Lique et al. 2016).

43 Despite the importance of runoff in accurately modeling ecosystem dynamics, considerable uncertainties remain in the  
44 parameterization schemes employed by land surface models. The accuracy of one process often depends on the scheme chosen  
45 for another, creating interdependencies that can complicate model accuracy. In permafrost regions, the presence of ice-rich  
46 permafrost can disrupt water infiltration processes, leading to increased surface runoff and altered drainage patterns (Kuchment  
47 et al., 2000; Walvoord & Kurylyk, 2016; Bennett et al., 2023). These heterogeneous conditions complicate efforts to accurately  
48 represent hydrological dynamics and highlight the necessity for improved modeling techniques. The scarcity of observational  
49 data and unmeasurable model parameters exacerbate these challenges, resulting in significant discrepancies between model  
50 outputs and real-world hydrological behavior (Bring et al., 2016; Clark et al., 2015, 2017). Addressing these uncertainties is  
51 essential for developing reliable predictive models that can support resource management and conservation efforts within  
52 rapidly changing Arctic ecosystems (Schädel et al., 2024).

53 Recent land model intercomparison projects (e.g., Boone et al., 2004; Lawrence et al., 2016; Collier et al., 2018; Mwanthi et  
54 al., 2024) have summarized various implementations of runoff schemes, ranging from simple bucket models to more advanced  
55 topography-based runoff models. These studies highlight significant variability in lateral surface runoff and subsurface runoff  
56 (baseflow) among different land models. Clark et al. (2015) emphasized the need to integrate groundwater-surface water  
57 interactions in Earth system models, while Maxwell et al. (2014) demonstrated the benefits of coupling surface and subsurface  
58 models for better predictions in complex landscapes. By improving soil freeze-thaw processes and incorporating soil  
59 heterogeneity, Liang & Xie (2001) and Swenson et al. (2012) achieved better runoff alignment with observed streamflow. Fan  
60 et al. (2019) identified lateral water flow as a crucial runoff component for the water cycle in the Arctic, with additional studies  
61 highlighting significant uncertainties in runoff parameterization schemes in high-latitude cold regions (e.g., Zheng et al., 2017;  
62 Hou et al., 2023; Abdelhamed et al., 2024). These efforts collectively highlight the pressing need to refine hydrological runoff  
63 simulations to improve predictions, particularly in permafrost regions as climate change intensifies.

64 Many previous studies have evaluated runoff parameterization by comparing different schemes against streamflow  
65 observations at large scales and coarse resolutions (e.g., [Niu et al., 2007](#); [Li et al., 2011](#); [Swenson et al., 2012](#); [Zheng et al.,](#)  
66 [2017](#); [Li et al., 2024](#)), however, high-quality streamflow data that can be used to validate runoff production are difficult to  
67 obtain in permafrost regions. This highlights the need for a more cost-effective and flexible framework to rapidly evaluate  
68 parameterization effectiveness using alternative approaches, for example, leveraging simulations from robust computational  
69 tools for physics-based permafrost thermal hydrology processes. The permafrost thermal hydrology capability ([Painter et al.](#)  
70 [2016](#)) in the Advanced Terrestrial Simulator (ATS) ([Coon et al., 2020](#)) has emerged as a valuable tool in this regard. ATS has  
71 been successfully compared to snow depth, supra-permafrost water table depth, and vertical profiles of soil temperatures  
72 ([Atchley et al. 2015](#); [Harp et al. 2016](#); [Jan et al. 2020](#)) and to catchment-scale evapotranspiration and runoff ([Painter et al.,](#)  
73 [2023](#)) in continuous permafrost regions. ATS's permafrost thermal hydrology capabilities have been used in a variety of  
74 modeling studies (e.g., [Atchley et al. 2016](#); [Sjöberg et al., 2016](#); [Jafarov et al. 2018](#); [Abolt et al., 2020](#); [Jan & Painter, 2020](#);  
75 [Hamm & Frampton, 2021](#); [Painter et al. 2023](#))

76 This study aims to evaluate and improve the parameterization of runoff processes in the Department of Energy's Energy  
77 Exascale Earth System Model (E3SM) Land Model (ELM) (e.g., [Oleson et al., 2013](#); [Bisht et al., 2018](#); [Xu et al., 2022](#); [Shi et](#)  
78 [al., 2024](#)) using detailed simulations from ATS. We quantitatively assess ELM's runoff parameterization, focusing on total  
79 runoff rather than individual components separately. The method we detail in this work directly addresses the scale gap  
80 between local- to global-scale process representation in models, using intercomparison with local-scale ATS simulations and  
81 parameters updates in ELM to improve Arctic runoff processes. By adopting a total water mass balance perspective, this  
82 approach provides insights into the strengths and limitations of ELM's runoff schemes, ultimately enhancing its predictive  
83 capabilities in Arctic environments. Additionally, it offers a comprehensive understanding of how landscape features and  
84 thermal hydrological processes interact in permafrost regions.

## 85 **2. Model description**

### 86 **2.1. ELM runoff parameterization schemes**

87 The runoff parameterization within ELM is designed to represent how water moves across the land surface between grid cells  
88 and is influenced by numerous factors, including soil moisture, topography, vegetation cover, etc. ELM's runoff scheme  
89 (ported from CLM v4.5, [Oleson et al., 2013](#)) is based on a simple TOPMODEL-based concept with a simplified topography  
90 representation ([Niu et al., 2005](#)). The runoff in ELM is partitioned into surface and subsurface flows, both of which are assumed  
91 to be related to water storage, vertical infiltration, and groundwater-soil water interactions ([Beven & Kirkby, 1979](#); [Niu et al.,](#)  
92 [2005, 2007](#)). There are more than twenty runoff components (variables) defined in ELM, but essentially, they can be  
93 categorized into three groups in a simulation with fixed land use: i) surface runoff, ii) subsurface runoff, and iii) runoff from  
94 overland water bodies like wetlands, lakes, and glaciers. The top 10 layers in ELM considered soil to a depth of ~3.8 m and

95 are hydrologically and biogeochemical active. The remaining five ground layers in each column are considered to be dry  
 96 bedrock that extend to a depth of ~42.1 m. Here, we only explicitly list the key equations representing the crucial components  
 97 of the former two groups representing for surface/subsurface runoff; for a more detailed description of the underlying physics  
 98 and complete formulations, readers are referred to existing literature (Oleson et al., 2013; Niu et al., 2005; Bisht et al., 2018;  
 99 Liao et al., 2024).

100 Surface runoff is composed of two components: i) outflow from the saturated portion of a grid cell with excess water,  $q_{over}$ ,  
 101 and ii) outflow from surface water storage such as a pond,  $q_{h2osfc}$ . The first term is written as:

$$102 \quad q_{over} = q_{liq,0} f_{max} \exp\left(-0.5 f_{over} z_{\nabla, perch}\right) \quad (1)$$

103 where  $q_{liq,0}$  is the sum of liquid precipitation reaching the ground and melt water from snow ( $\text{kg}\cdot\text{m}^{-2}\cdot\text{s}^{-1}$ );  $f_{max}$  is the ratio of  
 104 the area that has higher compound topographic index (CTI) values than the mean CTI value of the grid cell, with a consideration  
 105 of geomorphological features;  $f_{over}$  is a decay factor that is often calibrated using the recession curve of the observed  
 106 hydrograph, taken as  $0.5 \text{ m}^{-1}$ ;  $z_{\nabla, perch}$  is the perched groundwater table depth (m) within the thawed soil layers. The second  
 107 term is formulated as:

$$108 \quad q_{h2osfc} = k_{h2osfc} f_{connected} (W_{sfc} - W_c) \frac{1}{\Delta t} \quad (2)$$

109 where the storage coefficient  $k_{h2osfc} = \sin(\beta)$  is a function of grid cell mean topographic slope  $\beta$  (in radians);  $f_{connected}$  is  
 110 the fraction of the inundated portion of the interconnected grid cell, calculated as  $f_{connected} = (f_{h2osfc} - 0.5)^{0.14}$ , if  $f_{h2osfc}$  is  
 111 greater than 0, otherwise equal to 0, where  $f_{h2osfc}$  is the fraction of the area that is inundated.  $W_{sfc}$  represents surface storage  
 112 water ( $\text{kg}\cdot\text{m}^{-2}$ ), determined by the surface-inundated fraction  $f_{h2osfc}$ , the slope  $\beta$ , the ponded water height, and  
 113 microtopographic features.  $W_c$  is the amount of surface water present when  $f_{h2osfc} = 0.5$ ; and  $\Delta t$  is the model time step.

114 Subsurface runoff is also composed of two components: i) drainage in the frozen soils where the groundwater table remained  
 115 dynamic under partially frozen conditions,  $q_{drain}$ , and ii) drainage from the thawed active layer,  $q_{drain, perch}$ . The first term is  
 116 based on the following exponential relationship:

$$q_{drain} = 10^{\Theta_{ice}} \cdot 10 \sin(\beta) \cdot \exp(-2.5z_{\nabla}) \quad (3)$$

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118 where  $\Theta_{ice}$  is an exponent of the ice impedance factor. It is calculated as

$$\Theta_{ice} = -6 \left( \frac{\sum_{i=jwt}^{N_{levsoi}} S_{ice,i} \Delta z_i}{\sum_{i=jwt}^{N_{levsoi}} \Delta z_i} \right), \text{ where}$$

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$S_{ice,i}$  is the saturation degree of ice in soil layer  $i$ ;  $\Delta z_i$  is the layer thickness;  $jwt$  is the index of the layer directly above the

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water table; and  $N_{levsoi} = 15$  refers to the total number of soil layers.  $z_{\nabla}$  is the groundwater table depth (m). It should be

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noted that for continuous permafrost or frozen soil, its drainage is equal to zero or tiny values, and here the last term in Eq. (3)

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is reduced to a very small value, i.e.,  $2.8 \times 10^{-10}$ . The second term refers to the lateral drainage from the perched saturated zone

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between layers  $N_{perch}$  and  $N_{frost}$ , written as:

$$q_{drain,perch} = 10^{-5} \sin(\beta) \left( \sum_{i=N_{perch}}^{i=N_{frost}} 10^{-6 \left( \frac{S_{ice,i} + S_{ice,i+1}}{2} \right)} k_{sat,i} \Delta z_i \right) (z_{frost} - z_{\nabla,perch}) \quad (4)$$

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where  $k_{sat,i}$  is soil hydraulic conductivity ( $m \cdot s^{-1}$ ) at saturated unfrozen status in soil layer  $i$ .  $z_{frost}$  is the frost table defined as

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the shallowest frozen layers having an unfrozen layer above it (m).  $z_{\nabla,perch}$  is the perched groundwater table depth (m) within

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the thawed layers above icy permafrost ground.

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In this study, the total runoff from ELM is calculated as the sum of the above four runoff components, expressed as

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$q_{total} = q_{drain} + q_{drain,perch} + q_{over} + q_{h2osfc}$  (with units in mass water flux,  $kg \cdot m^{-2} \cdot s^{-1}$ ).

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## 2.2. ATS runoff generation schemes

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ATS solves integrated surface/subsurface flow in complex topographic landscapes with complex soil structures, which can

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capture a wide array of processes and their interactions to produce a holistic system understanding of a system (Painter et al.,

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2016; Coon et al., 2020; Gao & Coon, 2022). As a physics-based hydrological model, ATS uses physically based

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representations for surface runoff, subsurface runoff, and river routing. Here, only the key governing equations are presented.

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The subsurface variably saturated flow is based on the Richards equation with phase change to solve the conservation of water

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mass, written as:

$$\frac{\partial}{\partial t} \left[ \phi \left( \omega_g m_g s_g + m_l s_l + m_i s_i \right) \right] = -\nabla \cdot (m_l \mathbf{q}_l) + Q_w \quad (5)$$

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138 where  $\phi$  is porosity; the subscripts  $g$ ,  $l$ , and  $i$  refer to the gas, liquid, and ice phases;  $\omega$  is the gaseous mole fraction (mol·mol<sup>-1</sup>) referring to a molar fraction of water vapor within all gas in the pore space;  $m$  is the molar density of a particular phase (mol·m<sup>-3</sup>);  $s$  is saturation ( $s_g + s_l + s_i = 1$ ); and  $Q_w$  refers to sources and sinks (mol·s<sup>-1</sup>). The Darcy velocity (m·s<sup>-1</sup>) is presented as  $\mathbf{q}_l = -k_{\text{int}}k_{\text{rl}}/\mu_l(\nabla P_l + \rho_l \mathbf{g}\nabla z)$ , where  $k_{\text{int}}$  is intrinsic permeability (m<sup>2</sup>),  $k_{\text{rl}}$  is relative permeability,  $\mu_l$  is dynamic viscosity (Pa·s),  $P_l$  is pressure head (Pa),  $\rho_l$  is water density (kg·m<sup>-3</sup>),  $\mathbf{g}$  is the gravitational acceleration (m·s<sup>-2</sup>), and  $z$  is the vertical elevation (m). The vapor pressure in the pore space is assumed to be in equilibrium with the liquid phase above the freezing temperature and in equilibrium with the ice phase below freezing. The parameterizations and constitutive relationships, such as the van Genuchten soil water retention curve and water-ice phase transition functions, are omitted here. The conservation of energy in the subsurface assumes local thermal equilibrium among the ice, liquid, gas, and solid grains, presented as:

$$148 \quad \frac{\partial}{\partial t} \left[ \sum_{j=l,g,i} \phi m_j s_j u_j + (1-\phi) C_e T \right] = -\nabla \cdot (m_l h_l \mathbf{q}_l) + \nabla \cdot (\lambda_e \nabla T) + Q_E \quad (6)$$

149 where  $T$  is the temperature (K);  $u$  is the specific internal energy (J·mol<sup>-1</sup>);  $h$  is the specific enthalpy (J·mol<sup>-1</sup>);  $C_e$  and  $\lambda_e$  are the equivalent heat capacity (J·m<sup>-3</sup>·K<sup>-1</sup>) and thermal conductivity (W·m<sup>-1</sup>·K<sup>-1</sup>) of the soil composite (liquid, ice, gas, and solid grains);  $Q_E$  is the thermal energy sources and sinks (W·m<sup>-3</sup>).

152 The thermal surface flow with phase change is governed by three core equations (Painter et al., 2016): the mass balance for water in the liquid and ice phases, a diffusion wave approximation for surface flow extended to include an immobile ice phase, and the energy balance equation. The effects of surface water freezing and thawing are incorporated through a liquid–ice partitioning factor, or unfrozen fraction  $\chi$ , which depends on the surface water temperature and varies smoothly from 0 to 1 as the temperature rises through the freezing point. These governing equations are expressed as follows:

$$157 \quad \frac{\partial}{\partial t} \left[ \delta_w \chi m_l + \delta_w (1-\chi) m_i \right] + \nabla \cdot (\delta_w \chi m_l \mathbf{U}_w) = Q_{ss} \quad (7)$$

$$158 \quad \mathbf{U}_w = - \frac{(\chi \delta_w)^{2/3}}{n_{\text{mann}} (\|\nabla Z_s\| + \varepsilon)^{1/2}} \nabla (Z_s + \delta_w) \quad (8)$$

$$\frac{\partial}{\partial t} [\delta_w \chi m_l u_l + \delta_w (1 - \chi) m_l u_l] + \nabla \cdot (\delta_w \chi m_l \mathbf{U}_w h_l) - \nabla \cdot [\delta_w (\chi \kappa_l + (1 - \chi) \kappa_i) \nabla T_s] = Q_{ess} \quad (9)$$

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where  $\mathbf{U}_w$  is the surface flow velocity ( $\text{m}\cdot\text{s}^{-1}$ );  $Q_{ss}$  and  $Q_{ess}$  are the mass ( $\text{mol}\cdot\text{m}^{-2}\cdot\text{s}^{-1}$ ) and energy ( $\text{W}\cdot\text{m}^{-2}$ ) source/sink terms,

respectively;  $\delta_w$  is ponded depth (m);  $n_{mann}$  is Manning's coefficient ( $\text{s}\cdot\text{m}^{-1/3}$ );  $\epsilon$  is a small positive regularization (m) to

keep the equations non-singular in regions with zero slope ratio. The ponded depth and surface elevation  $Z_s$  are defined in two dimensions (x-y), and the vector operators are to be interpreted accordingly.

The land surface energy is calculated either at the surface of a snowpack or ponded water, presented as:

$$(1 - \alpha) Q_{sw}^{in} + Q_{lw}^{in} + Q_{lw}^{out} + Q_h(T_s) + Q_e(T_s) + Q_c(T_s) = 0 \quad (10)$$

where  $\alpha$  is surface albedo and  $T_s$  is the surface temperature (K);  $Q_{sw}^{in}$  is incoming shortwave radiation ( $\text{W}\cdot\text{m}^{-2}$ );  $Q_{lw}^{in}$  is

incoming longwave radiation ( $\text{W}\cdot\text{m}^{-2}$ );  $Q_{lw}^{out}$  is outgoing longwave radiation ( $\text{W}\cdot\text{m}^{-2}$ );  $Q_h$  is the sensible heat flux ( $\text{W}\cdot\text{m}^{-2}$ );

$Q_e$  is the latent heat flux ( $\text{W}\cdot\text{m}^{-2}$ ); and  $Q_c$  is the conductive heat flux ( $\text{W}\cdot\text{m}^{-2}$ ).

The above Eqs (5)–(10) represent the integrated surface–subsurface thermal hydrological processes. Continuity of primary scalar fields and fluxes (e.g., pressure, temperature, and water content) is enforced across the surface–subsurface interface. The fully coupled system is solved simultaneously to capture key hydrological dynamics, including freeze–thaw transitions and energy–water exchanges, enabling the generation of physically consistent hydrological outputs. Here, we consider the cumulative discharge ( $\text{mol}\cdot\text{s}^{-1}$ ) at the downstream outlet as the total runoff from the simulation domain.

### 3. Methodology

#### 3.1. Study areas

The first study area is located in the Sagavanirktok (Sag) River basin, located on the North Slope of Alaska (Figure 1a). Temperatures in the Sag range from  $-25^\circ\text{C}$  in January to  $15^\circ\text{C}$  in July, with approximately half of the annual precipitation occurring as snowfall from September through April, while summer rainfall contributes around 50 % of the total precipitation. The basin is characterized by broad alluvial valleys and rolling tundra topography underlain by continuous permafrost. Vegetation is dominated by Arctic tundra communities, including mosses, lichens, and dwarf shrubs. Soils are generally silty loams with an organic-rich active layer overlying mineral, and permafrost extends to considerable depths. The shallow active

182 layer, typically less than 1.0 m, strongly regulates hydrological processes, as thaw depth controls infiltration, runoff generation,  
183 and subsurface drainage. These conditions make the Sag basin representative of cold, dry Arctic watersheds.

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185 The second study area is the Teller watershed, a 2.5 km<sup>2</sup> drainage basin located approximately 27 miles from Nome on Teller  
186 Highway, located on the Seward Peninsula of Alaska (hereafter referred to as Teller27, [Figure 1b](#)). Compared to the cold and  
187 dry climate of the Sag River basin, the Teller27 site experiences a warmer and wetter climate. The Sag site receives over twice  
188 the annual snowfall of Teller27, while the Teller27 site is 7–8°C warmer on average ([Gao & Coon, 2022](#)). The watershed is  
189 situated in a landscape of rolling hills underlain by discontinuous permafrost, where thaw depth varies considerably across  
190 slope positions and is strongly influenced by soil and vegetation cover. The land cover is dominated by moist tundra  
191 ecosystems, including mosses, dwarf shrubs, and patches of willow along riparian zones. Soils generally consist of an organic-  
192 rich surface horizon underlain by silty to loamy mineral substrates. Streamflow measurements were collected at the Teller27  
193 watershed river outlet ([Busey et al., 2019](#)) from 2016-2023. For additional climate, snow, subsurface properties, and permafrost  
194 at the Teller27 site, refer to [Bennett et al. \(2022\)](#), [Jafarov et al. \(2018\)](#), [Léger et al. \(2019\)](#), [Thaler et al. \(2023\)](#), and [Wang et al. \(2024\)](#).

### 196 **3.2 Numerical Experiment Design**

197 Our experimental design for this work consists of three main steps as follows. First, results from detailed ATS simulations at  
198 the Sag River basin were compared to ELM’s runoff parameterization schemes. Specifically, ATS-simulated thaw depth,  
199 water table depth, and ice content were used in ELM’s parameterization Eqs. 1-4, and the results were then compared to ATS-  
200 simulated total discharges. Second, runoff coefficients derived from the Sag site were implemented into ELM’s source code  
201 and tested for transferability at the Teller27 site, without the need for additional ATS simulations. Third, ELM simulations at  
202 the Teller27 site were evaluated directly against observed streamflow data from the Teller watershed to assess the performance  
203 and generalizability of the adjusted runoff coefficients.

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205 The ATS model was implemented to simulate local-scale hillslope hydrological processes at the Sag River site only.  
206 Meteorological forcing data for this region are sourced from the Daymet version 4 dataset ([Thornton et al., 2020](#)), developed  
207 at a daily timestep. ATS modeling follows three steps. First, a soil column with an initial temperature above freezing was  
208 subjected to bottom-up freezing by imposing a constant temperature of -10 °C at the bottom boundary until a steady-state  
209 frozen soil profile was formed. In this stage, only the subsurface flow-energy processes were included. The resulting pressure  
210 and temperature profiles were then used to initialize spin-up runs for each hillslope model until a cyclically steady state was  
211 achieved. During the spin-up phase, the full physics system was applied, including surface and subsurface thermal flow as well  
212 as surface energy balance processes, using smoothed meteorological forcings. Each cyclically steady hillslope was then used  
213 as the initial condition for transient simulations driven by real forcings. For all hillslope simulations, the bottom boundary  
214 temperature was fixed at -10 °C. Closed boundary conditions were applied to all other subsurface and surface boundaries

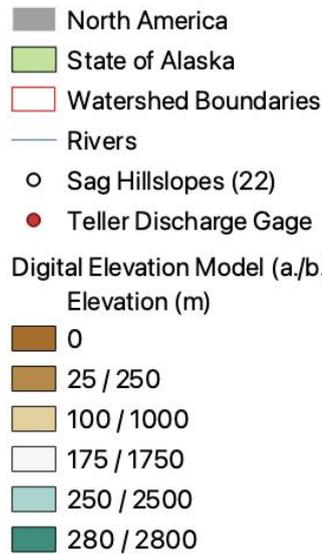
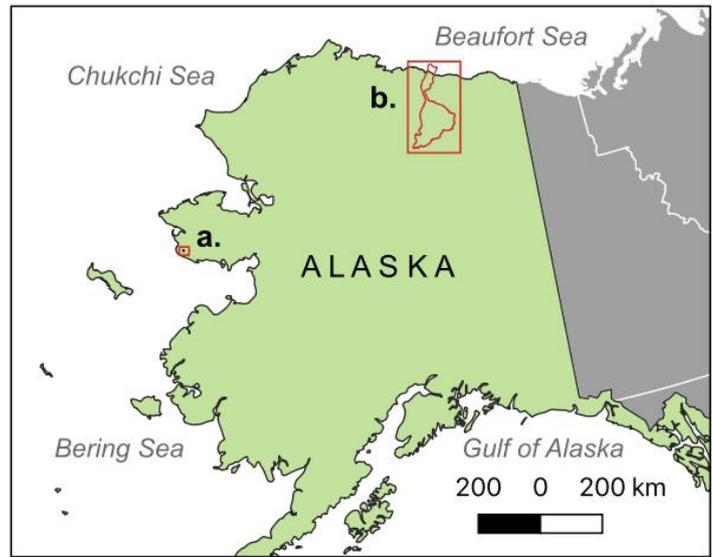
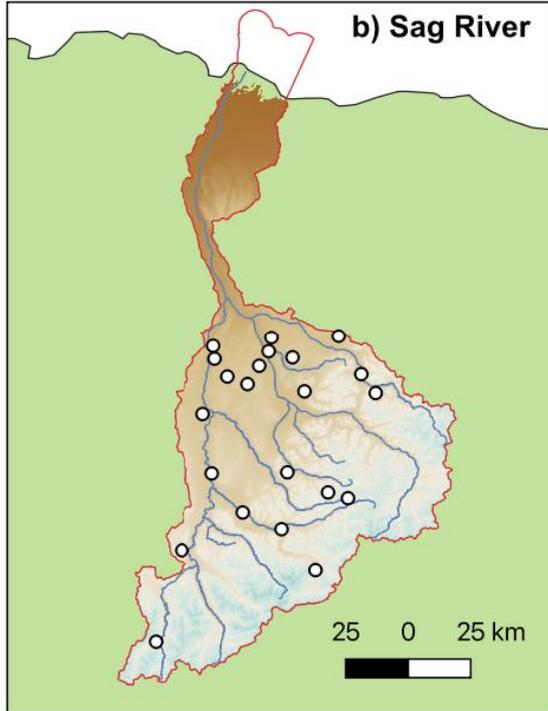
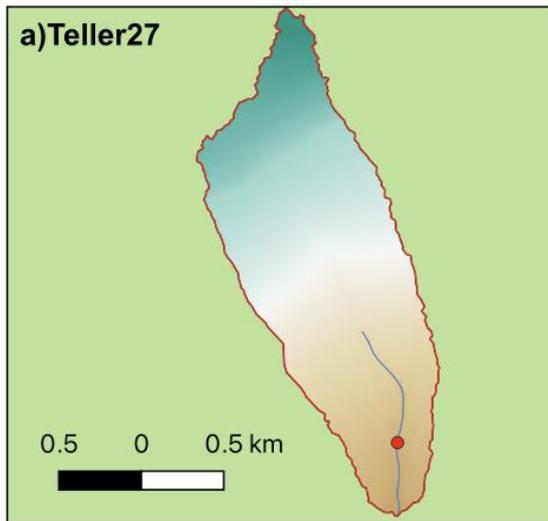
215 except at the surface outlet, where a seepage face boundary condition was applied. Both the column and hillslope models were  
216 represented with three soil layers: the top two organic soil layers (i.e., acrotelm, catotelm) and the bottom mineral layer. The  
217 thickness and properties of the soil layers for hillslopes were determined based on the corresponding land cover types according  
218 to O'Connor et al. (2020). The soil properties of each soil layer are listed in the Supplement (Table S1). The thermal  
219 conductivity representation followed Atchley et al. (2015). For further details on ATS model mesh generation, boundary  
220 conditions, model setup, and initialization, refer to Jan et al. (2020), Gao & Coon (2022), and Coon et al. (2022). We randomly  
221 selected 22 hillslope sites within the Sag River basin, ensuring representation across a range of slope, aspect, and drainage  
222 area, providing a basis for sensitivity analysis.

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224 ELM was implemented to simulate subgrid hillslope hydrological processes specifically for the Teller27 watershed. We  
225 configured ELM at a spatial resolution of 0.5 degrees, incorporating finer-scale surface and land use input parameters, but not  
226 recently developed features such as the topounit or elevation bands that represent sub-grid variability (Hao et al. 2022; Tesfa  
227 and Leung, 2017). ELM was driven by 1-hourly meteorological forcing data from ERA5-Land (Muñoz-Sabater et al., 2021),  
228 ensuring realistic and high-temporal-resolution atmospheric inputs. We used the Offline Land Model Testbed (OLMT) to  
229 standardize the ELM case setup and model spin-up (e.g., Sinha et al., 2023). Model spin-up proceeds through two phases after  
230 Thornton & Rosenbloom (2005): the first phase features accelerated biogeochemical cycling, while the second phase uses  
231 standard biogeochemical reaction rates. These spin-up phases are run for 260 and 200 years, respectively, to ensure vegetation  
232 and biogeochemistry have approached a steady-state condition before beginning a transient run that spans 1850-2024. To  
233 validate the runoff from ELM, we used the streamflow measurements collected at the gage. To evaluate the influence of soil  
234 property parameters on ELM-simulated runoff, a series of parameter sensitivity analyses was conducted. In each simulation,  
235 one parameter was perturbed by  $\pm 50$  % from its default average value (ELM's surface and land use files are extracted from  
236 the global 0.5-degree resolution files), while the values of all other parameters were fixed.

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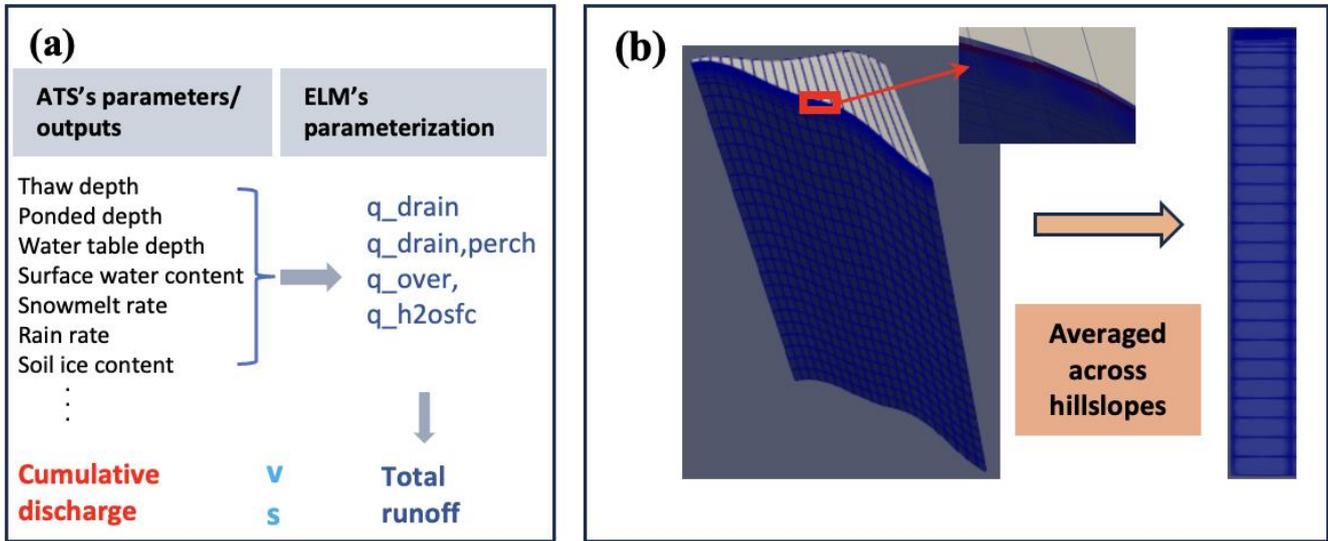
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**Figure 1:** Map of the a) Teller27 and the b) Sag River sites, and inset map of Alaska with sites indicated with red boxes. Detailed site maps a) and b) include watershed boundaries (red), rivers (blue), Sag River hillslopes (white dots, 22), the Teller27 discharge gauge (red dot), and the Digital Elevation Models (DEMs) for each site. The 2.5 km<sup>2</sup> Teller27 site, being much smaller and with much more limited elevational range than the Sag River site, is 10 times smaller than the Sag River basin elevational range (see legend). Sag hillslopes (22) are not found on the lower elevation North Slope coastal plain, below 250 m.

245 **3.3 ELM runoff parameterization evaluation**

246 We constructed variable-width hillslope models for each of the 22 hillslope sites to represent both vertical and lateral dynamics  
 247 and simulated the fully coupled cryo-hydrological processes using ATS. To facilitate comparison with ELM, we post-  
 248 processed the ATS simulation outputs by averaging the surface and subsurface variables across ATS’s multiple horizontal  
 249 units (columns), preserving the number of vertical layers (rows, Figure 2). This produced a 1D multi-layer (rows), single  
 250 column profile that mimics ELM’s 15-layer subgrid-scale structure. From this 1D multi-layer representation, key model  
 251 variables such as maximum seasonally thawed depth of the upper soil layers above the permafrost (referred to as active layer  
 252 thickness, ALT), surface water content, water table depth, soil moisture and ice content were extracted and used as inputs to  
 253 ELM’s runoff parameterization equations (Eqs. (1)–(4)) to compute surface and subsurface runoff components. The resulting  
 254 total runoff from ELM was then compared against the cumulative runoff stimulated directly by ATS. Figure 2 illustrates the  
 255 overall workflow, including the extraction and processing of ATS’s variables, the calculation of ELM runoff components, and  
 256 the comparison with ATS’s discharge accumulation at the outlet, as well as the averaging of ATS horizontal units to a 1D  
 257 multi-layer representation. Layers can be of variable depth, as indicated in Figure 2.



258  
 259 **Figure 2: Map (a) Workflow for calculating ELM’s total runoff, highlighting key variables, runoff components, and computational**  
 260 **steps involved. (b) Averaging of ATS’s simulation results, illustrating the transformation from high-resolution pseudo-2D ATS**  
 261 **outputs averaged across all hillslopes, to simplified 1D ELM column representations.**

262  
 263 To obtain the optimized runoff coefficients, we formulated objective functions that minimize the difference between the ATS-  
 264 simulated runoff and a weighted sum of ELM’s runoff components. The optimization was carried out using a constrained  
 265 numerical minimization algorithm, with non-negativity bounds imposed on all coefficients. This procedure was conducted  
 266 across multiple hillslope sites and under both annual and seasonal (warm–cold) conditions, resulting in site-independent

267 adjusted coefficients for each case. To assess the performance of the optimized runoff coefficient and quantify the differences  
 268 between them, three statistical metrics were calculated: root mean square error (RMSE), mean absolute error (MAE), and  
 269 Nash–Sutcliffe efficiency coefficient (NSE). These metrics were selected as complementary evaluation measures following  
 270 standard hydrological model assessment practices (Moriassi et al., 2007). RMSE emphasizes large errors and highlights peak  
 271 mismatches, MAE reflects the average magnitude of deviations and is less sensitive to outliers, and NSE evaluates overall  
 272 model efficiency relative to the observed mean. Together, they provide a balanced and robust assessment of ELM runoff  
 273 performance. They are defined as follows:

$$274 \quad RMSE(c_1, c_2, c_3, c_4) = \sqrt{\frac{1}{n} \sum_{i=1}^n (y_i - \hat{y}_i)^2} \quad (11)$$

$$275 \quad MAE(c_1, c_2, c_3, c_4) = \frac{1}{n} \sum_{i=1}^n |y_i - \hat{y}_i| \quad (12)$$

$$276 \quad NSE(c_1, c_2, c_3, c_4) = 1 - \frac{\sum_{i=1}^n (y_i - \hat{y}_i)^2}{\sum_{i=1}^n (y_i - \bar{y}_i)^2} \quad (13)$$

277 where  $y_i$  and  $\bar{y}_i$  represent the ATS simulated value and its average value, respectively;

278  $\hat{y}_i = c_1 q_{drain} + c_2 q_{drain, perch} + c_3 q_{over} + c_4 q_{h2osfc}$  is the calculated (or optimized) value based on ELM's equations. The

279 coefficients  $c_1$ ,  $c_2$ ,  $c_3$ , and  $c_4$  are weighting factors used to evaluate the relative contribution of each component. In the non-

280 adjusted case, all four coefficients are set to 1.0, directly summing all runoff components. In the adjusted case, the coefficients

281 are optimized through regression against the ATS-simulated runoff to best match the observed behavior.  $n$  is the number of

282 annual or seasonal cumulative runoff values used in the comparison.

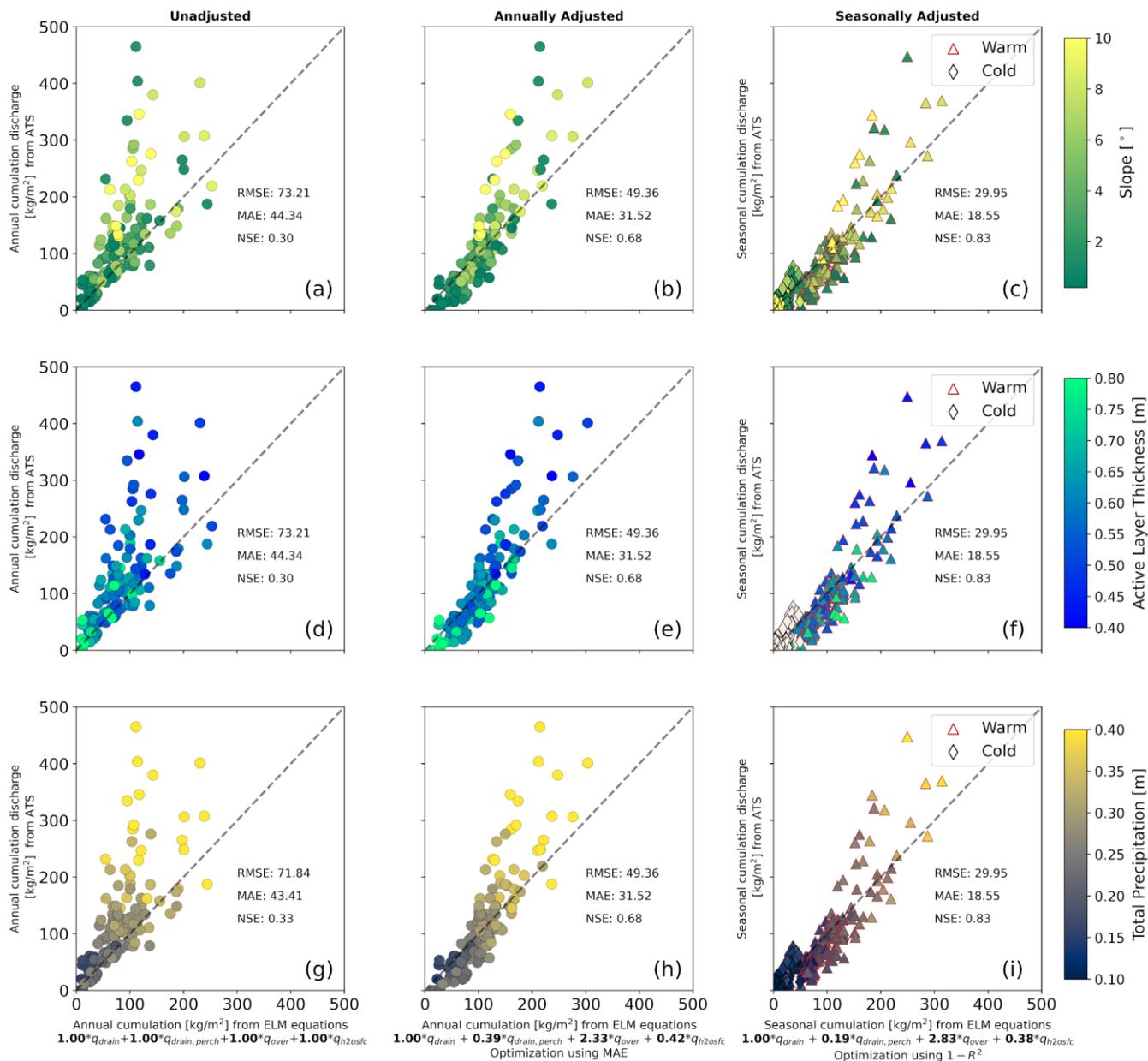
## 283 4. Results

### 284 4.1 Evaluation of the runoff schemes in ELM

285 ELM runoff results were evaluated in comparison with ATS's drainage at the outlet. In the plots below, we compared the

286 annual and seasonal total cumulative runoff using both adjusted and non-adjusted coefficients  $c_i$ , under a variety of conditions

287 across different hillslope sites (e.g., forcings, slope, ALT, etc.). The three columns in Figure 3 correspond to different ELM  
 288 parameterization cases: (1) unadjusted coefficients, (2) annually optimized coefficients, and (3) seasonally (warm-cold)  
 289 optimized coefficients. The three rows represent different color-coded variables: slope (top), ALT (middle), and total  
 290 precipitation (bottom).  
 291



292  
 293 **Figure 3. Comparison of cumulative total runoff between ATS and ELM models under various hillslope conditions. The different**  
 294 **colors represent slope (a-c), active layer thickness (d-f), and total precipitation (g-i). Columns (from left to right) correspond to**

295 **different coefficient settings in ELM: unadjusted (a, d, g), annually adjusted (b, e, h), and seasonally adjusted (c, f, i). The results**  
296 **are displayed for different runoff parameterization coefficients (as indicated on the x-axis) in ELM and compared against ATS-**  
297 **simulated runoff.**

298

299 It can be seen that ELM's annual total cumulative runoff is generally smaller than ATS's runoff when using unadjusted runoff  
300 coefficients, with an NSE of 0.30 (Figure 3a). However, when adjusted coefficients are applied, the two models show much  
301 better agreement, achieving an NSE of 0.68 when adjusted based on annual discharge (Figure 3b) and 0.83 when optimized  
302 using separate adjustments for the warm and cold periods (Figure 3c). The seasonal total cumulative runoff is calculated for  
303 the warm season (May to August) and cold season (September to April) within the calendar year. This improved alignment in  
304 the seasonal total cumulative runoff is also reflected in performance metrics, with the RMSE, MAE, and NSE increasing by  
305 39 %, 41 %, and 22 %, respectively, over the total runoff without adjusted coefficients, respectively.

306 The total runoff during the cold season is normally lower than that of the warm season. This is primarily because when the

307 ground is fully frozen, overland flow ( $q_{over}$ ) becomes the only dominant component of total runoff, which occurs due to  
308 excess meltwater from snow after limited vertical infiltration. As shown by the diamond symbols in Figures 3c, 3f, and 3i,  
309 ELM's results are generally well-aligned with ATS's drainage during cold seasons, though some values are slightly lower. In  
310 the cold season, no active layer exists, whereas it does exist during the warm season. Cold-season runoff on steeper slopes  
311 tends to be lower, likely due to limited infiltration in frozen soils, which reduces subsurface flow pathways. In contrast, during  
312 the warm season, total runoff generally increases with slope, as shown in Figure 3c, likely due to enhanced overland flow and  
313 faster hydrological response. Despite this trend, the runoff alignment in the seasonal total runoff (Figure 3c) remains better  
314 compared to the total annual (Figure 3b). This indicates that runoff differences between the two models cannot be fully  
315 explained by variations in slope, highlighting the influence of additional factors such as model parameterizations and physical  
316 processes.

317 By carefully examining the results with the adjusted coefficients in Figure 3b, we observed that ELM performs well in  
318 representing lower slopes compared to the ATS benchmark, with a few exceptions. On steeper slopes (> 8 degrees), ELM  
319 predicts lower runoff values than ATS, with differences reaching up to 150 kg·m<sup>-2</sup>. Interestingly, ELM also underpredicts  
320 runoff on shallower slopes (< 2 degrees), suggesting that runoff differences between the two models are influenced by more  
321 than just slope. This variation could arise from differences in how the two models handle topographic gradients, basin size, or  
322 spatial heterogeneity in climate forcings. Figure 3e highlights that ELM performs better with deeper ALT, likely because these  
323 active layers experience less freezing, allowing for increased water storage in the deeper thawed zones and reduced lateral  
324 drainage. Figure 3h reveals a strong relationship between total cumulative runoff and precipitation, and ELM generally  
325 captures lower precipitation events more accurately, leading to correspondingly lower total runoff. As expected, Figure 3i  
326 reveals a clear trend between warm-season total runoff and precipitation magnitude. However, ELM tends to underpredict

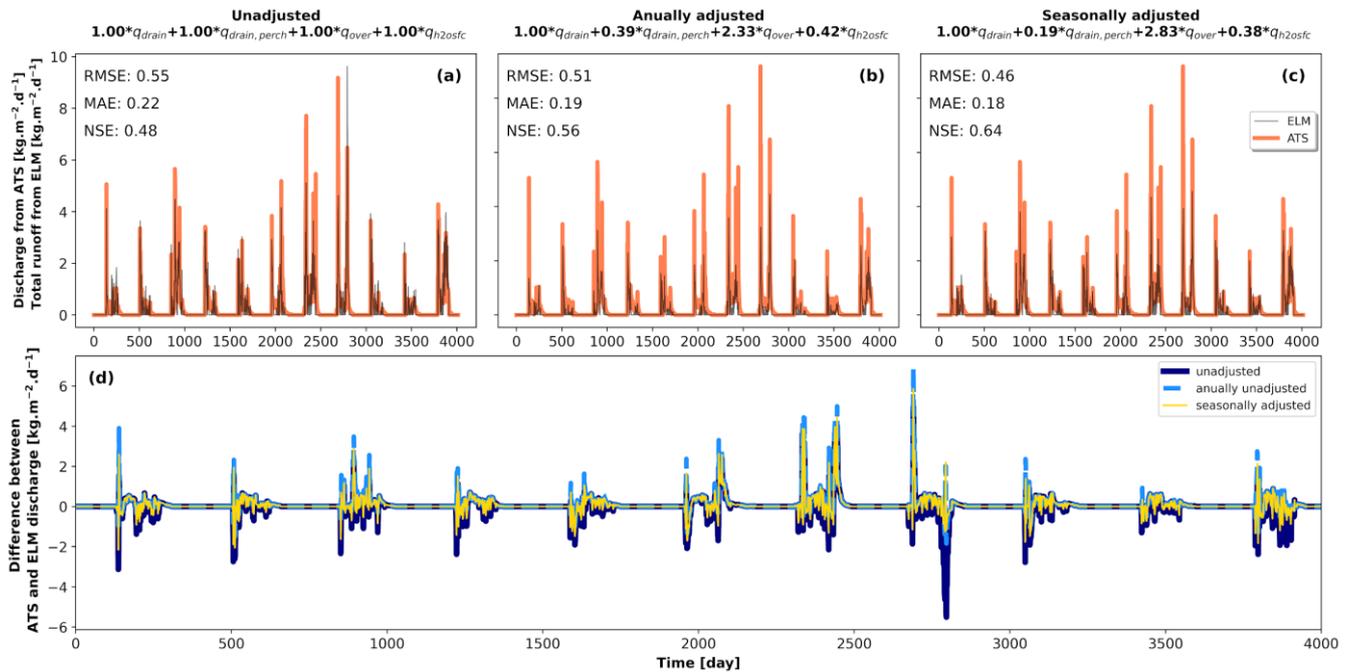
327 runoff under higher precipitation conditions. This underscores the critical role of climate forcing data in shaping model  
328 performance and highlights ELM's sensitivity to precipitation variability.

329 To better understand these findings, it may be important to consider spatial variations in terrain landforms (e.g., concave vs.  
330 convex) across the modeled hillslopes, as well as alternative hillslope representations through structural formulations (e.g.,  
331 [Swenson et al., 2019](#); [Lawrence & Swenson, 2024](#)). In addition, these watersheds span a broad latitudinal range (approximately  
332 68° to 70°N), which likely introduces considerable climatic and topographic variability. For example, steeper slopes can  
333 promote rapid surface runoff, while gentler slopes with deeper thawed layers may enhance water retention and reduce lateral  
334 drainage.

335 This improved alignment between ELM and ATS's annual total cumulative runoff is also evident in time series comparisons  
336 of total runoff from a selected hillslope, shown in [Figure 4](#), both with and without adjusted coefficients. [Figure 4a](#) illustrates  
337 the results using the unadjusted coefficients, where ELM underestimates runoff peaks and exhibits a relatively weak correlation  
338 with ATS discharge. The RMSE, MAE, and NSE values (0.55, 0.22, and 0.48, respectively) indicate moderate agreement but  
339 suggest room for improvement, particularly in capturing peak runoff events. [Figure 4b](#) shows the impact of applying annually  
340 adjusted coefficients, which improves model performance, as reflected by reduced RMSE (0.51) and MAE (0.19), along with  
341 a higher NSE (0.56). The adjusted coefficients result in better agreement during high-runoff periods, though some  
342 discrepancies remain in capturing the full variability of runoff responses. [Figure 4c](#) presents the results with seasonally adjusted  
343 coefficients, which yield the best overall performance among the three cases. The RMSE and MAE decrease further to 0.46  
344 and 0.18, respectively, while the NSE increases to 0.64, demonstrating a stronger correlation between ELM and ATS runoff.  
345 The seasonal adjustment appears to enhance the model's ability to capture the timing and magnitude of runoff peaks (see  
346 [Figure 4d](#)), particularly during snowmelt periods. However, some deviations remain, likely due to limitations in parameterizing  
347 snowmelt-driven surface flow and subsurface hydrological interactions in ELM.

348 These results highlight the importance of refining runoff coefficients and incorporating seasonal variations to improve the  
349 predictive capability of ELM, particularly in Arctic environments where snowmelt dynamics play a dominant role in runoff  
350 generation. In general, better alignment is observed when ATS's cumulative runoff remains below a certain threshold, such as  
351  $15 \text{ kg} \cdot \text{m}^{-2} \cdot \text{d}^{-1}$ . For larger runoff, ELM tends to underpredict total runoff, indicating limitations in its ability to represent higher  
352 runoff scenarios accurately.

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Figure 4. Time series comparison of total runoff between ATS and ELM for a typical hillslope with an average slope of 6.6°, a watershed area of 2.43 km<sup>2</sup>, and the ALT ranging from 0.43 to 0.59 meters. Results are shown with (a) unadjusted coefficients, (b) annually-adjusted coefficients, and (c) seasonally-adjusted coefficients.

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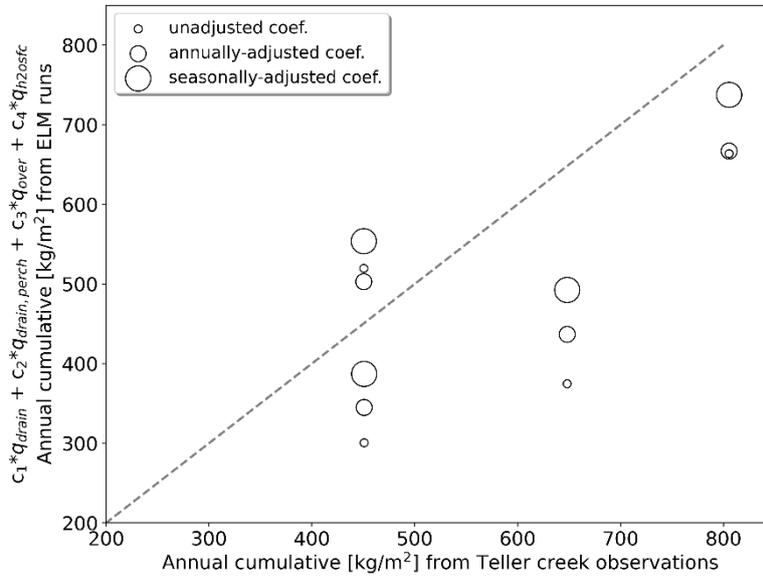
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#### 4.2 Teller27 watershed evaluation

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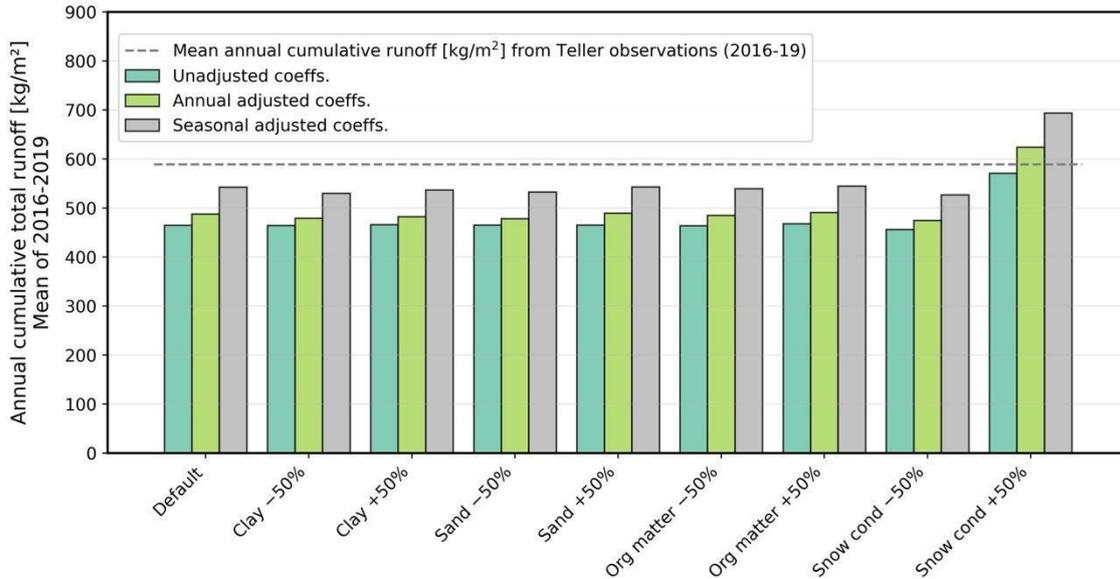
The improved ELM runoff coefficients were evaluated using observed streamflow data from the Teller27 watershed, spanning 2016–2019 (Busey et al., 2019). Results in Figure 5 indicate that the adjusted coefficients significantly enhance the agreement between ELM-simulated runoff and observations. The unadjusted coefficients consistently underpredict runoff, with the largest discrepancy observed in 2016 (ELM: 374.66 kg·m<sup>-2</sup>, observed: 648.25 kg·m<sup>-2</sup>). Both annually and seasonally adjusted coefficients reduce this gap, with the seasonally adjusted coefficients providing better performance, particularly in years with greater interannual variability in precipitation and thaw depth.

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**Figure 5. Comparison of cumulative annual total runoff between ELM-simulated and observed data at the Teller27 watershed, Alaska, from 2016 to 2019. Symbol sizes represent ELM results using unadjusted coefficients, annually adjusted coefficients, and seasonally adjusted coefficients.**



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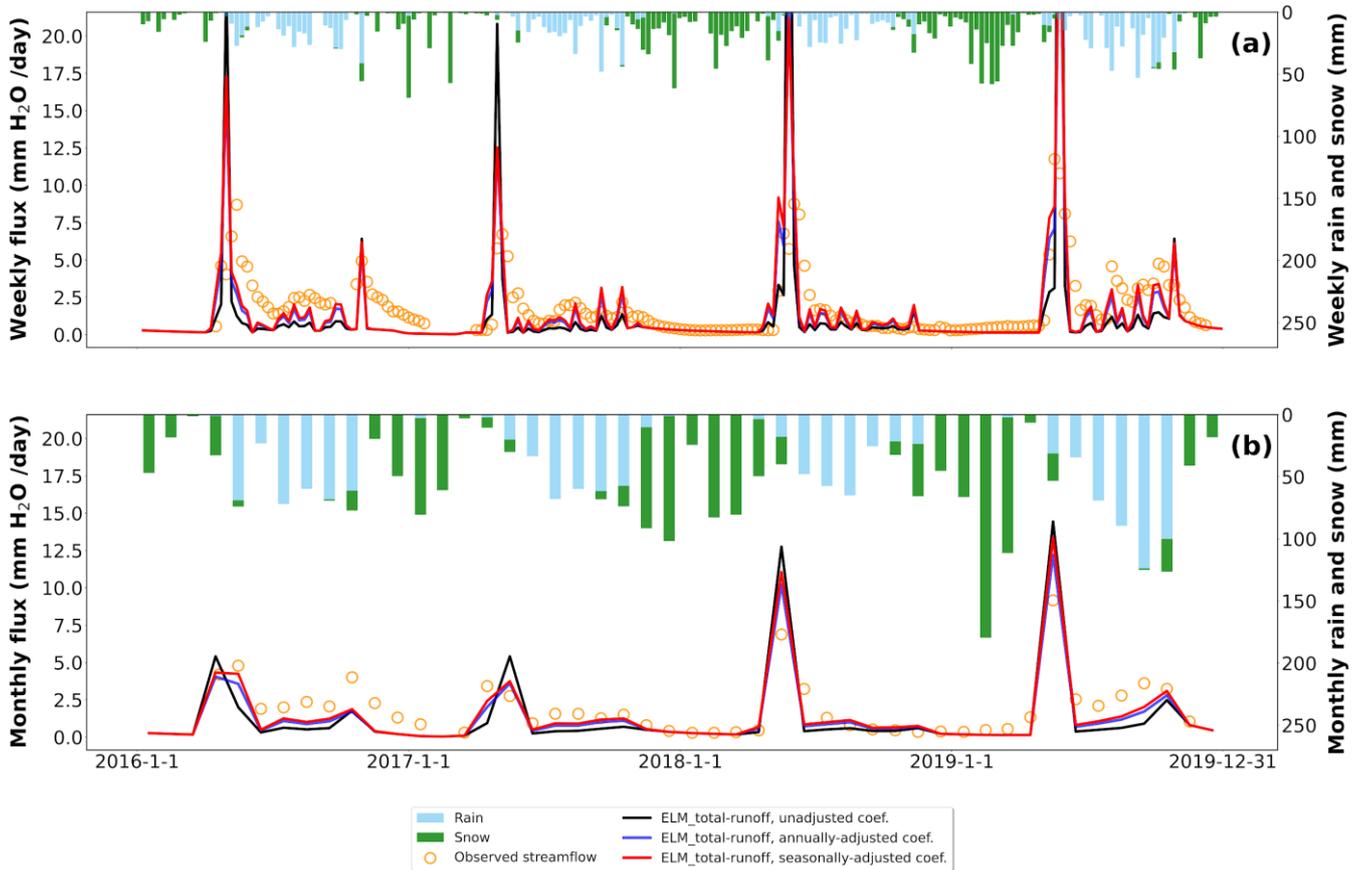
**Figure 6. Variations in annual cumulative total runoff from ELM simulations at the Teller27 watershed, Alaska for the mean of all years (2016-2019). Different bars groupings along the x-axis illustrate scenarios where parameters are reduced or increased from their default average values in ELM's soil physical property and snow thermal conductivity. Bar colours represent results with**

376 unadjusted coefficients (teal), annually adjusted coefficients (green), and seasonally adjusted coefficients (grey). The mean annual  
377 cumulative runoff from Teller observations (mean all years 2016-2019) is given in the dashed line.

378  
379 Figure 6 presents the outcomes of the parameter sensitivity experiments, illustrating how changes in land surface properties  
380 influence simulated total runoff. It can be seen that total runoff is relatively insensitive to variations in surface soil properties  
381 such as clay, sand, and organic matter content, suggesting that soil texture and composition play a secondary role in controlling  
382 runoff dynamics within the model. Simulated runoff totals under these parameter perturbations remained within a relatively  
383 narrow envelope, regardless of whether baseline or optimized runoff coefficients were applied. This occurs because runoff is  
384 most due to overland flow during the spring snowmelt, when the ground is still frozen. These differences were notably smaller  
385 than the variations observed across different years or watersheds. The broader implications of these findings are further  
386 discussed in Section 5.2.

387 Figure 7 shows a temporal comparison of weekly and monthly total runoff, while Table 1 quantifies performance using RMSE,  
388 MAE, and NSE metrics. The adjusted coefficients yield lower RMSE and MAE values and higher NSE scores than the  
389 unadjusted coefficients, confirming their effectiveness, despite being derived from a study site some distance from the Teller27  
390 watershed. These results clearly demonstrate that ELM's subgrid-scale runoff scheme performs well at the monthly timescale,  
391 but struggles to capture sub-monthly (e.g., weekly) runoff variability. Although ELM's total runoff is of the same order of  
392 magnitude as the observed discharge at Teller creek, discrepancies arise during specific events. Notably, spikes in runoff occur  
393 during rapid snowmelt in early spring due to ponded surface water, and the baseflow during recession periods are poorly  
394 simulated.

395 The weekly average results (Figure 7a) reveal significant discrepancies in runoff peaks with unadjusted coefficients, while  
396 those biases are reduced by the simulations with adjusted coefficients. This may be due to large peak flow simulated during  
397 snowmelt in ELM that is not represented in the observations, thus flows throughout the rest of the summer are too low in the  
398 simulations. We believe that this response may be occurring due to a frozen active layer that leads to fast runoff that is not  
399 observed in the hydrological records. While we observed this overestimate of flow peaks, the seasonally adjusted coefficients  
400 still perform better in capturing both the timing and magnitude of runoff peaks, perhaps because the seasonal coefficients  
401 adjust for some attenuation of runoff. The monthly results (Figure 7b) show improved agreement with observed data during  
402 high runoff periods, particularly those driven by snowmelt and seasonal precipitation. This is likely because the monthly results  
403 accumulate flow responses over longer periods of time, accounting for and spreading out this large peak flow runoff response  
404 that was incorrectly simulated at the weekly time scale. For example, at the monthly scale, NSE improves markedly from 0.07  
405 with unadjusted coefficients to 0.58 and 0.60 with annually and seasonally adjusted coefficients, respectively. These results  
406 highlight the efficacy of the adjusted coefficients and the critical role of incorporating seasonal variability into runoff  
407 parameterization for improving ELM's performance.



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**Figure 7. Comparison of ELM-simulated (a) weekly and (b) monthly total runoff with observed data at the Teller27 watershed, Alaska. Simulated results are displayed using different runoff parameterization coefficients in ELM, represented by distinct colored lines. Rain and snow precipitation are shown as bar plots using the top X-axis (time) and left Y-axis (mm) in both subplots.**

**Table 1. Performance metrics (RMSE, MAE, and NSE) for ELM-simulated total runoff compared to observed streamflow across all temporal scales (daily, weekly, and monthly) at the Teller27 watershed, Alaska.**

Temporal average of total runoff	Adjustment of runoff coefficients	ELM	RMSE	MAE	NSE
Daily	unadjusted		12.66	1.96	-32.16
	annually-adjusted		5.80	1.62	-5.95
	seasonally-adjusted		5.55	1.66	-5.37
Weekly	unadjusted		4.91	1.73	-4.80
	annually-adjusted		2.61	1.22	-0.64
	seasonally-adjusted		2.49	1.20	-0.48
Monthly	unadjusted		1.76	1.20	0.07
	annually-adjusted		1.18	0.84	0.58

415

416 **5. Discussion**

417 Intercomparison studies to consider differences and similarities between a land surface scheme to a physically-based model  
418 are useful because they allow for quantitative evaluation of each model and its performance for different components of the  
419 hydrologic cycle. The technique applied here was to extract the land surface parameterization schemes and evaluate them  
420 within a fine-scale, physics model, to consider the total cumulative runoff from the land surface scheme ( $y^{\text{ELM\_runoff}}$ ) and  
421 compare it with the physics model estimates ( $y^{\text{ATS\_runoff}}$ ). This novel approach allowed us to focus on the formulations over  
422 other interacting effects that may have potentially obscured the results. We were then able to make an estimate of runoff  
423 coefficients that could be applied to improve the match between the physics-model and the land surface model. These  
424 coefficients, when applied to a small watershed located in sub-arctic Alaska, improved the land surface model ( $y^{\text{ELM\_runoff}}$ )  
425 significantly, suggesting that this approach may allow for fine-tuning of runoff within similar systems. Overall, further research  
426 is needed to determine how flexible these coefficients are; however, this work was foundational in that it provided a novel  
427 approach to both model intercomparison as well as for model improvement.

428 A sensitivity analysis conducted as part of this study identified that soil properties may exert less influence on the runoff  
429 dynamics in the land surface model than snow accumulation and melt processes, as well as subsurface thermal hydrology. This  
430 finding links this component of our research to investigations into snow processes and model improvement in these same  
431 systems (e.g., [Bennett et al. 2022](#); [Clark et al. 2015](#)). It is clear that to improve runoff processes within permafrost dominant  
432 systems, a holistic approach to understanding the system is required to determine the key processes and model components  
433 that require adjustment. This study provided an initial enquiry into this process that developed the foundation for our work  
434 towards improving the Earth system model for these Arctic systems.

435 **5.1 Differences in simulated runoff from representative hillslopes**

436 The apparent mismatch between  $y^{\text{ELM\_runoff}}$  and  $y^{\text{ATS\_runoff}}$  results from 22 representative hillslopes in the Sag River basin  
437 warrants a critical examination. However, such evaluations must consider the inherent differences between the two models.  
438 Several factors could contribute to these differences. First, a key distinction between ATS and ELM is their treatment of runoff  
439 generation processes. ATS implicitly simulates variably saturated flow, lateral subsurface flow and transport, and dynamic  
440 freeze-thaw cycles in a high-resolution 3D domain ([Painter et al., 2016](#); [Coon et al., 2020](#)). In contrast, ELM utilizes  
441 parameterized equations to represent subgrid-scale heterogeneities, which are not expected to fully capture the complexity of  
442 permafrost hydrology ([Bisht et al., 2018](#); [Xu et al., 2024](#)). This averaging process that reduces a 3D system into a pseudo-3D  
443 system in ATS can represent a loss of spatial variability in hydrological processes, particularly in heterogeneous permafrost  
444 regions where local-scale topography and subsurface heterogeneity play a critical role in runoff generation ([Zhao & Li, 2015](#);

445 [Abolt et al., 2024](#)). This simplification can also lead to discrepancies in how surface and subsurface runoff are partitioned  
446 ([Liao et al., 2024](#)), particularly in regions with high spatial variability in soil moisture, ice content, and thaw depth. For instance,  
447 ELM may under- or over-predict runoff during high precipitation events (see Figure 5) compared with the spatially resolved,  
448 physics-based implementation in ATS.

449 Secondly, although  $y^{\text{ATS\_runoff}}$  is treated as the benchmark in this study, it is not without uncertainties. The accuracy of  $y^{\text{ATS\_runoff}}$   
450 simulations depends on input data such as soil properties, meteorological forcings, and initial conditions, all of which contain  
451 inherent uncertainties ([Harp et al. 2016](#); [Jafarov et al., 2018](#); [Zhang et al., 2023](#); [Huang et al., 2024](#)). In permafrost landscapes,  
452 soil heterogeneity is particularly difficult to characterize, and small variations in soil thermal and hydrological properties can  
453 lead to substantial differences in runoff predictions ([Decharme et al., 2013](#); [Vereecken et al., 2022](#)).

454 Additionally, the accuracy of  $y^{\text{ELM\_runoff}}$  predictions is highly dependent on the parameterization of surface hydrological  
455 processes. Although optimized coefficients have been implemented to improve agreement with  $y^{\text{ATS\_runoff}}$ , these  
456 parameterizations may still inadequately capture the nonlinear interactions between infiltration, permafrost thaw, and lateral  
457 flow ([Swenson et al., 2012](#); [Liao et al., 2024](#)). This issue is particularly relevant in ice-rich permafrost terrains, where abrupt  
458 changes in thaw depth and active layer dynamics can lead to nonlinear responses in runoff generation (e.g., [Hinzman et al.,](#)  
459 [2022](#)). The lack of explicit lateral flow representation in ELM further limits its ability to capture runoff redistribution processes  
460 that are well-resolved in ATS simulations.

461 Another factor that may contribute to the mismatch is the difference in how the two models resolve seasonal freeze/thaw  
462 processes, especially under varying precipitation and thawing conditions. Runoff generation in permafrost regions is highly  
463 sensitive to seasonal thawing and freezing dynamics, as well as precipitation regimes (e.g., [Zhang et al., 2010](#); [Guo et al.,](#)  
464 [2025](#)). In particular, mismatches may arise during transitional periods such as spring snowmelt, when small differences in  
465 temperature and soil conditions can lead to substantial variations in runoff production.

466 Understanding these potential differences is crucial for interpreting the model responses and guiding future ELM model  
467 improvements. Addressing the uncertainties in ATS and refining the transformation of parameterization schemes between  
468 models could reduce these mismatches. Similarly, enhancing ELM's parameterization by incorporating insights from ATS  
469 simulations, such as better representation of lateral flow and freeze-thaw processes, could lead to improved alignment with  
470 ATS and more accurate predictions in Arctic environments under a changing climate.

## 471 **5.2 Sensitivity and uncertainties of model performance to land surface parameters in ELM**

472 The sensitivity analysis assessed the impact of various surface and subsurface parameters, including soil properties (clay, sand,  
473 and organic content) and snow thermal conductivity, on the simulated total  $y^{\text{ELM\_runoff}}$ . Understanding the sensitivity of  
474  $y^{\text{ELM\_runoff}}$  simulations to these parameters is crucial for improving hydrological predictions in permafrost regions, where land  
475 surface processes interact with freeze-thaw dynamics in complex ways ([Bisht et al., 2018](#); [Walvoord & Kurylyk, 2016](#)).

476 The limited sensitivity of total  $y^{\text{ELM\_runoff}}$  to soil property variations observed in our ELM simulations raises important  
477 implications for land surface model development. Previous studies have shown that soil texture can strongly affect bidirectional  
478 water exchange between groundwater and the soil during freeze–thaw transitions (e.g., [Xie et al., 2021](#); [Huang & Rudolph,  
479 2023](#); [Yang et al., 2025](#)). However, our findings suggest that these processes may have less influence on annual runoff  
480 generation in permafrost regions. This discrepancy may be explained by the dominant role of snowmelt dynamics and shallow  
481 subsurface hydrology in controlling surface runoff. In permafrost-dominated landscapes, runoff generation is often driven by  
482 the timing and intensity of snowmelt, seasonal freeze–thaw cycles, and the spatial distribution of near-surface permafrost.  
483 These factors likely outweigh the direct effects of variations in soil grain size or organic matter content (e.g., [Swenson et al.,  
484 2012](#)). The presence of an impermeable permafrost layer beneath the active layer restricts deep infiltration and causes excess  
485 water to remain near the surface, limiting the direct impact of soil properties on runoff partitioning. Similar findings have been  
486 reported in other permafrost hydrology studies, where hydraulic conductivity and soil texture exert minimal influence on runoff  
487 formation compared to freeze-thaw dynamics and snowmelt timing (e.g., [Zhang et al., 1999](#); [Walvoord & Kurylyk, 2016](#)).  
488 However, further investigation is needed to evaluate whether subsurface water redistribution, active layer depth variability,  
489 and lateral flow dynamics could play a more significant role in influencing ELM’s runoff performance.

490 In contrast to soil parameters, snow thermal conductivity exhibits a strong influence on simulated runoff, demonstrating its  
491 critical role in shaping hydrological responses in Arctic environments. An increase in snow thermal conductivity enhances  
492 heat transfer within the snowpack, leading to earlier and more rapid snowmelt. This, in turn, alters the seasonal timing of water  
493 availability and increases runoff magnitudes during peak melt periods ([Musselman et al., 2017](#)). Higher thermal conductivity  
494 results in faster warming of the snowpack, reducing the buffering effect of snow insulation and exposing the underlying soil  
495 to greater temperature fluctuations. This phenomenon has been observed in field studies, where changes in snow properties  
496 significantly impact the timing and magnitude of spring runoff ([Würzer et al., 2016](#); [Liljedahl et al., 2016](#)). The results in  
497 [Figure 6](#) suggest that accurate representation of snow properties is essential for improving  $y^{\text{ELM\_runoff}}$  predictions in permafrost  
498 landscapes. Over- or under-estimating snow thermal conductivity could lead to systematic biases in modeled  $y^{\text{ELM\_runoff}}$  timing,  
499 potentially affecting the accuracy of hydrological assessments in Arctic watersheds.

500 Collectively, these findings reinforce the critical role of snowmelt-driven hydrological processes in shaping runoff dynamics  
501 in permafrost landscapes and illustrate key sensitivities within ELM’s runoff parameterization. The results suggest that ELM’s  
502 performance is particularly influenced by representations of snow accumulation and melt processes, as well as subsurface  
503 thermal hydrology. In particular, sensitivity to snow density, thermal conductivity, and freeze–thaw transitions points to the  
504 value of incorporating physically based formulations that capture snowpack variability (e.g., [Bennett et al. 2022](#), [Lackner et  
505 al., 2022](#); [Tao et al., 2024](#), [Wang et al. 2025](#)) and lateral subsurface flow (e.g., [Swenson et al., 2012](#); [Liao et al., 2024](#)). These  
506 process-level influences appear to exert a stronger control on  $y^{\text{ELM\_runoff}}$  behavior than surface soil properties alone,  
507 underscoring their importance in cold-region hydrology and land surface modeling.

### 508 5.3 Implications for improving runoff parameterization coefficients in land surface models

509 Hydrological runoff-related parameters in land models are often calibrated against the observed streamflow data (e.g., [Niu et al., 2007](#); [Li et al., 2013](#)), which can be limited or unavailable in remote permafrost regions. This study introduces a novel  
510 evaluation framework, which shifts the traditional paradigm of directly comparing coarse-scale land surface models to fine-  
511 scale physics-based models, by deriving optimized runoff coefficients by leveraging high-fidelity simulations from the  
512 integrated surface/subsurface hydrological simulators such as the ATS. These optimized coefficients are then incorporated into  
513 the land surface model, allowing for physics-informed improvements without direct site-based calibration. This approach  
514 offers a process-oriented alternative to conventional calibration, providing an avenue for improving parameterizations in data-  
515 scarce regions.  
516

517 A key implication of this framework is its potential transferability across diverse Arctic watersheds. In this study, coefficients  
518 derived from the Sag River hillslopes were applied to the Teller27 watershed without additional tuning, resulting in  
519 significantly improved  $y^{\text{ELM\_runoff}}$  performance at monthly and seasonal scales. One possible reason for this is that while these  
520 two systems are located in very different environments and some distance from each other, they are similar in that both exhibit  
521 moderately graded slopes and elevations, vegetation of grasses and shrubs, and both have some degree of permafrost (albeit  
522 discontinuous permafrost in Teller27). However, in this iteration of ELM, most of the sub-grid variability within these features  
523 are not represented, despite their importance to the influence of snowmelt runoff and other water balances (e.g., [Beer et al. 2016](#);  
524 [Shirley et al. 2025](#)). This demonstration suggests that physically guided coefficients obtained through fine-scale process-  
525 resolving models may be generalized to other Arctic catchments with similar characteristics, offering a possible strategy for  
526 parameter refinement in Earth system land models at coarse scales. Such transferability is especially valuable for land model  
527 intercomparison projects that seek robust parameterizations applicable across diverse permafrost regions (e.g., [Clark et al., 2015](#);  
528 [Lawrence et al., 2019](#); [Fan et al., 2019](#)). However, more research is required to determine the extent of this transferability.  
529 Future applications of this approach at permafrost sites across the pan-Arctic, which is part of the next phase of this project,  
530 could further enhance the robustness and generalizability of this framework.

531 Our coefficient-calibration approach complements, but also differs from, the representative hillslope approach developed for  
532 the CLM ([Swenson et al., 2019](#); [Lawrence & Swenson, 2024](#)). In CLM's representative hillslope approach, intrahillslope  
533 lateral subsurface flow is explicitly represented and scaled through representative hillslopes that account for slope, aspect, and  
534 lateral redistribution of water. This structural modification allows the model to capture lateral connectivity in a process-based  
535 manner without requiring high-resolution benchmarks. By contrast, our method leverages physics-based ATS simulations to  
536 calibrate and optimize runoff coefficients in ELM and then evaluates their transferability across sites. Whereas the CLM  
537 approach introduces structural reformulations of runoff schemes, our framework focuses on refining existing parameterizations  
538 through calibration against physics-based permafrost models. Taken together, these strategies represent complementary  
539 pathways for advancing runoff representation in permafrost regions and for bridging local-scale hydrological processes with  
540 land surface components of Earth system models. At the same time, ELM has recently developed an improved subgrid hillslope

541 hydrologic connectivity, which represents lateral water movement across topographic units (topounits) within a gridcell. This  
542 new implementation shares similarities with the CLM hillslope approach. Future evaluation of the runoff performance of that  
543 parameterization alongside our coefficient-calibration framework will be an important next step for improving  
544 parameterization and scaling of hydrological processes in ELM. Such integration of coefficient calibration, representative  
545 hillslope formulations, and the new subgrid framework will be essential for capturing hydrological variability across diverse  
546 permafrost landscapes and for improving the predictive fidelity of Earth system land models under changing Arctic climate  
547 conditions.

## 548 **6. Limitations and future work**

549 Based on our analysis and discussion, we acknowledge several limitations that may be further improved in future studies:

- 550 1. Simplified watershed representation. The hillslopes used for ATS simulations in the Sag River basin are pseudo-  
551 2D variable-width simplifications of the 3D landscapes, which do not fully capture the heterogeneity of real  
552 Arctic landscapes, such as ice-wedge polygons, thermokarst features, and microtopographic variations. Future  
553 studies should incorporate many more diverse landscapes (up to hundreds of hillslope models) and ensure  
554 identical topographic representations across both models.
- 555 2. Transferability evaluation. The optimized runoff coefficients were derived from ATS simulations of Sag River  
556 hillslopes and then directly applied to the Teller Creek watershed without site-specific adjustments. This  
557 transferability was only evaluated at a single site (Teller27), further evaluation across diverse Arctic watersheds  
558 with long-term streamflow measurements is needed to build broader confidence in the generalizability of the  
559 approach. Moreover, because seasonal variability plays a key role in runoff generation, this approach may work  
560 reasonably well for colder Arctic regions but may be less applicable to sub-Arctic environments.
- 561 3. Limited consideration of lateral flow and subsurface heterogeneity. This study primarily focused on ELM's grid-  
562 scale runoff generation, neglecting lateral water movement and groundwater interactions. In Arctic environments,  
563 lateral subsurface flow can play a crucial role in redistributing water across permafrost landscapes, affecting both  
564 surface runoff and baseflow dynamics in different land units, which will be evaluated in future work.
- 565 4. Limited assessment of meteorological forcing biases. While the parameterization in this study is based on state  
566 variables derived from ATS simulations, rather than directly on precipitation or other forcings, model  
567 performance in applications such as the Teller Creek test can still be sensitive to uncertainties in meteorological  
568 inputs. In high-latitude regions, sparse station coverage and undercatch issues can introduce substantial  
569 uncertainty in precipitation, temperature, and radiation datasets. Future work should assess how these  
570 uncertainties propagate through the model and influence runoff simulations under different forcing scenarios.

## 571 **7. Conclusions**

572 We evaluated a land surface model's runoff parameterization using detailed fine-scale physics-based simulations of 22  
573 hillslopes in the Sag River basin and identified empirical adjustments that improve the runoff parameterization. Seasonal  
574 optimization of these coefficients improved the model's ability to capture hydrological variability at monthly scales,  
575 particularly in snowmelt-driven runoff processes. The adjusted parameterization improved ELM simulated runoff from the

576 Teller27 watershed. That demonstration of transferability of the adjusted parameterization is encouraging but needs further  
577 study across diverse Arctic catchments. Sensitivity analysis revealed that runoff in ELM is largely insensitive to soil properties  
578 but highly sensitive to snow thermal conductivity, underscoring the importance of accurate snow process representation in  
579 permafrost regions. These findings demonstrate the value of spatially resolved fine-scale simulators from physics-based  
580 models as benchmarks for refining land surface models and highlight the need for process-specific parameterization  
581 improvements in hydrological runoff schemes of land surface models.

582 Despite these advancements, challenges remain in capturing subsurface hydrological processes, including lateral flow,  
583 permafrost thaw dynamics, and active layer variability, which are critical for Arctic runoff simulations. Future improvements  
584 should focus on incorporating water redistribution within an ELM gridcell due to lateral flow, refining subgrid-scale  
585 hydrological parameterizations, and evaluating model updates across diverse Arctic catchments. By addressing these gaps,  
586 land surface models could achieve more accurate runoff predictions, ultimately enhancing their utility for climate impact  
587 assessments and water resource management in permafrost regions.

588  
589 *Code and data availability.* All data sets used in this work are archived at the Environmental System Science Data  
590 Infrastructure for a Virtual Ecosystem (ESS-DIVE). ELM and ATS data sets will be archived here:  
591 <https://doi.org/10.15485/2550570>. Data sets will become live once the paper is accepted. ERA5 forcing data to run the ELM  
592 model can be downloaded from the ECMWF Climate Data Store: [https://cds.climate.copernicus.eu/datasets/reanalysis-era5-](https://cds.climate.copernicus.eu/datasets/reanalysis-era5-single-levels?tab=overview)  
593 [single-levels?tab=overview](https://cds.climate.copernicus.eu/datasets/reanalysis-era5-single-levels?tab=overview). ATS forcings data can be retrieved from the Daymet version 4 dataset (Thornton et al., 2020).  
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596 Ecosystem Experiments (NGEE) Arctic, ESS-DIVE repository. Dataset. <https://doi.org/10.5440/1618330>. Data sets are in the  
597 transfer process between the NGEE Arctic data portal and the ESS DIVE repository, and will be updated as soon as possible.  
598 The description and codes of E3SM v3.0 (including ELM v3.0) are publicly available at  
599 <https://www.osti.gov/doecode/biblio/123310> (E3SM Project, 2024) and [https://github.com/E3SM-](https://github.com/E3SM-Project/E3SM/releases/tag/v3.0.0)  
600 [Project/E3SM/releases/tag/v3.0.0](https://github.com/E3SM-Project/E3SM/releases/tag/v3.0.0) (released: 4 March 2024), respectively.

601  
602 *Author contributions.* The study was conceptualized and designed by Yu Zhang, Scott Painter, Xiang Huang and Katrina  
603 Bennett. Xiang Huang completed the data analysis, visualization, and the original draft. All authors contributed to editing the  
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605  
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607

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