

Evaluation of middle atmosphere temperature and wind measurements and ~~and~~ their disturbance characteristics by meteorological rockets

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Abstract. It is necessary to carry out the in-situ detection based on the meteorological rocket to deepen the cognitive level of the middle atmosphere environment, though there is still a lack of systematic research on the data accuracy and the physical mechanism affecting the measurement results, which restricts the effective use of rocket data. Based on thermistor and Beidou positioning, combined with temperature correction technology, middle atmosphere temperature and wind measurements from 20-60 km are obtained in northwest China by two meteorological rockets. The detection results are compared with satellite, empirical model and reanalysis data, and the error analysis theory is carried out in combination with the of the drop sounding and atmospheric disturbance characteristics. The results show that the data quality of the rocket detection is ideal, and the variation trend of temperature and wind profile with altitude is consistent with other data. The difference comes from the deviation of the matching data in time and space and the excessive measurement error in the initial fall stage. Also, it is found that the instability of the parachute causes poor positioning data quality and fast falling speed, and eventually cause the measurement error at the corresponding height to be significantly larger. Besides, the profile fluctuation of the first detection is more obvious, which is caused by the fragmentation of the high-altitude gravity wave. Wave dissipation leads to the weakening of atmospheric stability and the generation of denser small-scale layered structures on the profile, making significant wind field changes at the height below through the momentum ~~deposition~~deposited.

1. Introduction

The near space is located in the region of 20-100 km, which can cover the stratosphere, the mesosphere and the low thermosphere. The near-space atmosphere is far from the ground and does not have the weather phenomena common in the troposphere (cyclones, thunderstorms, fronts, etc.), but its unique importance still prompts extensive attention and research. First, the near space is the upper boundary of the troposphere, which can be coupled with the troposphere and affect it from top to bottom. The stratospheric atmosphere, due to its slow evolution characteristics (compared with the troposphere), can provide important information for the prediction of extreme weather and climate in the troposphere (Gray et al., 2018; Jin et al., 2023). For example, the weakening of the stratospheric polar vortex is often a precursor to the occurrence of cold waves

35 in the Northern Hemisphere. Second, the near space is the lower boundary atmosphere of space weather,
 36 which can act as a "display screen" for solar activity, and the influence of solar activity on Earth's weather
 37 and climate can be reflected in it. For example, solar activity can change the ozone in the middle atmosphere
 38 and transmit this change to the troposphere through the action of planetary waves (Krivolutsky et al., 2015).
 39 In addition, the near space is the combination of aerospace and aviation, and changes in the internal
 40 environment will directly affect the flight attitude and effect of aerospace vehicles (Chen et al., 2023; Roney,
 41 2007). Atmospheric disturbances, as the superposition of waves at different scales (including turbulence,
 42 gravity waves, planetary waves, etc.), are one of the main dynamic processes in the near space. As the height
 43 increases, the density decreases exponentially. The amplitude of these disturbances, such as gravity waves,
 44 gradually increases during the upward propagating process, and the impact of the wave becomes more and
 45 more significant (Lindzen, 1981; Alexander et al., 2010).

46 Since the near space is showing more and more important value, it is urgent to improve the
 47 understanding of its internal atmospheric environment. The necessary condition to support this demand is to
 48 carry out accurate detection and adequate research. Satellite remote sensing can provide atmospheric profile
 49 data with global coverage, but the detection ability of wind field is still insufficient, and the vertical resolution
 50 of data is rough (Ern et al., 2022; Thies and Bendix, 2011). Lidar and MST (Meso-Stratosphere-Troposphere)
 51 radars can obtain three-dimensional wind fields and temperatures, but the global distribution of detection
 52 sites is limited, and the data quality is affected by atmospheric environment and retrieve accuracy (She et al.,
 53 2003; Daren et al., 2018; Qiao et al., 2020). Flat-floating balloons with zero pressure or overpressure, can
 54 realize continuous detection in the horizontal direction of the stratosphere, but the characteristics of its own
 55 drift in the wind bring the uncertainty of detection, and require strict trajectory control technology (He et al.,
 56 2024; Alexander et al., 2021). Radiosonde balloons can detect meteorological elements with long time series
 57 and high precision, but the highest detection height is generally less than 30 km, and cannot cover higher
 58 airspace (He et al., 2022; Yoo et al., 2020). In contrast, the meteorological rocket sounding is the only in-situ
 59 detection method that can obtain the atmospheric environment in the altitude range of 20~100 km. The
 60 effective evaluation and inspection of rocket detection accuracy is an important prerequisite for the correct
 61 use of this means.

62 The meteorological rocket sounding mainly includes two methods: falling spheres detection and
 63 thermistor detection. The falling spheres can obtain the atmospheric density profile of 30-100 km, and then
 64 calculate the wind field, temperature and pressure, ~~the~~ ~~The~~ thermistor measurement can obtain the
 65 atmospheric temperature from 20 to 60 km, and then calculate the density, pressure, and wind field
 66 (Eckermann et al., 1995; Wang et al., 2006). Due to the large amplitude of atmospheric waves in this height
 67 range, the momentum and energy dissipated by wave fragmentation can cause drastic changes in
 68 meteorological elements such as wind field, density and temperature in the surrounding atmosphere.
 69 Therefore, analyzing the interaction mechanism between atmospheric wave and background atmosphere has
 70 always been one of the important research directions of in-situ observational data. By comparing with satellite,
 71 balloon and reanalysis data, thermistor rockets launched from Hainan Station and East China Sea have shown

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72 good detection results, and the atmospheric disturbance characteristics in near space are also extracted
 73 (Guoying et al., 2011; Song et al., 2024). Atmospheric density is measured using GPS data on a rigid falling
 74 ball and the measured deviation from ~~Atmospheric density are measured using GPS data on a rigid falling~~
 75 ~~ball and found that the deviation from~~ the model results was less than 10% (Yuan et al., 2017). Using passive
 76 ball falling experiments in northwest China, in-situ wind field and gravity wave information are analyzed
 77 from 30 to 100 km (Ge et al., 2019). A comprehensive evaluation of the detection accuracy of the TK-1
 78 meteorological rocket is performed and the reliability is demonstrated (Fan et al., 2013). It can be seen that
 79 the current results of near space rocket detection are still few, encouraging researchers to work in greater
 80 depth.

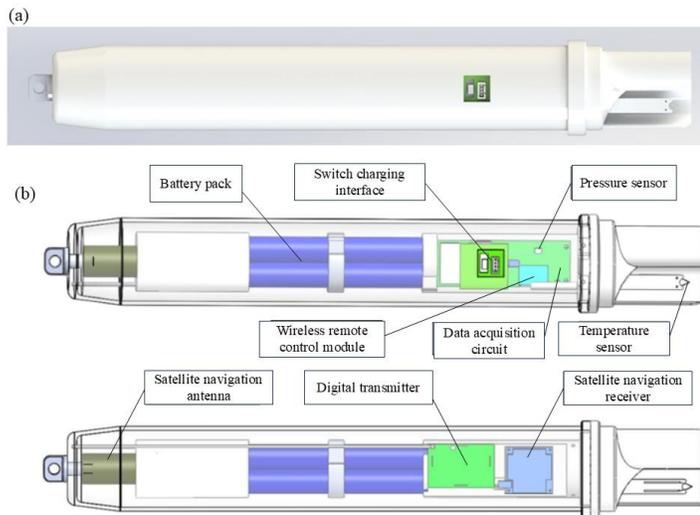
81
 82 In this paper, two meteorological rockets launched in the northwest of China are used to obtain
 83 meteorological detection data from 20 to 60 km ~~to obtain near space meteorological detection data from 20~~
 84 ~~to 60 km~~, error analysis and accuracy evaluation are carried out, and wave disturbance characteristics are
 85 also extracted. The structure of the paper is as follows: in the second section, the used data is introduced; in
 86 the third section, the temperature correction and error calculation method are given; in the fourth section, the
 87 comparison results of rocket detection profile and reference data are discussed, in the fifth section, the error
 88 analysis is performed; in the sixth section, the characteristics of wave perturbations and their effects on the
 89 background atmosphere are discussed; in the seventh section, the conclusion and prospect are given.

90 2. Rockets instrument and detection principle

91 The rocket radiosonde is mainly composed of temperature sensors, pressure sensors, satellite navigation
 92 and positioning modules, data acquisition circuits, transmitters, wireless remote control modules, batteries,
 93 switches, fixed frames, insulation boxes and fiberglass reinforced plastic shells, etc. The temperature sensor
 94 adopts a bead thermistor, purchased from the shelf, model MF51MP-D (Blue Crystal Electronics). The
 95 pressure sensor adopts a high-precision digital pressure sensor, purchased from the shelf, model ms5607
 96 (Switzerland). The navigation and positioning module adopts the high-precision positioning module of
 97 Beidou, and the antenna uses a four-arm helical antenna, which is a customized product. The main MCU of
 98 the data acquisition circuit adopts a 32-bit processor with ARM core, featuring low power consumption and
 99 mixed signal processing capabilities. It has a 14-bit A/D conversion accuracy, which can meet the
 100 measurement accuracy requirements of sensors. The digital transmitter is composed of dedicated RF chips
 101 and power amplifier modules to form a frequency point digital transmitter. It has the advantages of small size
 102 and adjustable frequency. When used in conjunction with ground receiving equipment, it can achieve data
 103 transmission within a diagonal distance range of 200 kilometers. The physical appearance and structural
 104 layout of the rocket sounding instrument are shown in Figure 1, and the main performance indicators of the
 105 rocket sounding instrument are shown in the table A1.

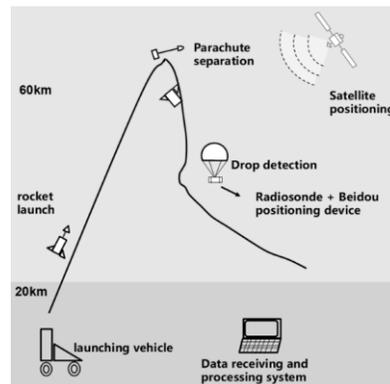
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106
107 **Figure 1. (a) The physical appearance and (b) structural layout of the rocket sounding instrument,**

108 The rocket detection mechanism is shown in Figure 1. The meteorological sonde is carried up by the
109 rocket, under the action of thrust, it rises at a high speed according to the established trajectory. After the
110 engine stops working, the rocket uses inertia to continue rising. When the rocket rises near the top of its
111 trajectory, the parachute carries the sonde and separates from the arrow body. The sonde pulls the parachute
112 and begins to fall.



113
114 **Figure 1. meteorological rocket detection mechanism.**

115 During this process, the atmospheric parameters are measured in situ and the data is transmitted down
116 to the ground receiving system. The thermistor sensor is used to obtain the atmospheric temperature in the
117 altitude range of 20-60 km, and the atmospheric pressure is obtained layer by layer from iterative calculation

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118 based on the base pressure (measured by the pressure sensor at 20 km). Then the atmospheric density is
 119 calculated through the ideal gas equation. The real-time position coordinates (X, Y, Z) of the sonde are
 120 obtained by using the Beidou positioning system, and the first derivative is obtained by linear fitting after the
 121 smoothing position coordinates point by point to calculate the northward, eastward and vertical velocity
 122 (represented by \dot{x} , \dot{y} , and \dot{z}). The corresponding acceleration is obtained by quadratic fitting (represented by
 123 \ddot{x} , \ddot{y} , and \ddot{z}). Based on the velocity and acceleration information, the meridional, zonal, and synthetic wind
 124 are calculated (represented by W_x , W_y , and W), and the wind direction (θ) can be further obtained. The
 125 specific calculation formula is shown in (1)-(4)

$$126 \quad W_x = \dot{x} - \frac{\ddot{x}}{z-g} \dot{z} \quad (1)$$

$$127 \quad W_y = \dot{y} - \frac{\ddot{y}}{z-g} \dot{z} \quad (2)$$

$$128 \quad W = \sqrt{W_x^2 + W_y^2} \quad (3)$$

$$129 \quad \theta = \begin{cases} \arctan \left| \frac{W_y}{W_x} \right| + 180^\circ, (W_x > 0, W_y > 0) \\ -\arctan \left| \frac{W_y}{W_x} \right| + 180^\circ, (W_x > 0, W_y < 0) \\ -\arctan \left| \frac{W_y}{W_x} \right| + 360^\circ, (W_x < 0, W_y > 0) \\ \arctan \left| \frac{W_y}{W_x} \right|, (W_x < 0, W_y < 0) \end{cases} \quad (4)$$

130 The air pressure at each height layer is calculated from the measured base point air pressure (20 km)
 131 using the pressure height formula:

$$132 \quad P = P_d \exp \frac{-g_0(H - H_d)}{R \cdot T_d}$$

133 Among them, P represents the air pressure at the calculated height, P_d is the air pressure of the adjacent
 134 lower layer, H is the geopotential, H_d is the geopotential of the adjacent lower layer, R is the dry air gas
 135 constant, and T_d is the temperature of the adjacent lower layer. Given the temperature and air pressure, the
 136 atmospheric density can be calculated through the ideal gas state equation.

137 The specific calculation process of atmospheric parameters is shown in Figure 2.

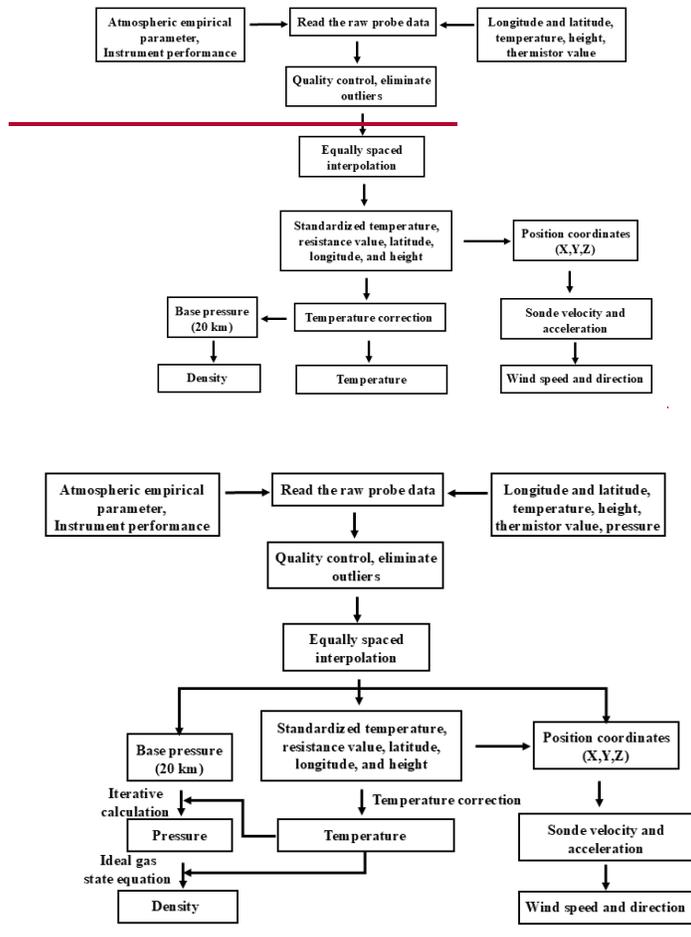


Figure 2. Atmospheric parameters calculation process.

141 **3. Data introduction**

142 The data for the two rockets used in this paper are launched in northwest China in the autumn of 2023,
 143 the vertical profile of wind velocity (synthetic wind, zonal wind, meridional wind), wind direction,
 144 atmospheric temperature, -pressure-, and density ~~form from~~ 20~60 km (effective height interval for analysis)
 145 are obtained.

146 Sounding of the Atmosphere using Broadband Emission Radiometry (SABER) carried on TIMED
 147 satellite, can obtain the vertical profile of atmospheric temperature, pressure, geopotential height, ozone and

148 other trace gas volume mixture ratio by limb scanning. Here the Level 2A temperature data from Saber
149 version 2.0 is selected.

150 MERRA2 (Modern Era Retrospective analysis for Research and Applications version 2) data is an
151 upgraded version of MERRA data, which is the second generation of high-precision data sets. The data has
152 a time resolution of 6 h and contains 42 pressure layers ranging from 1000 hPa to 0.1 hPa. The data used in
153 this paper are zonal wind, meridional wind and atmospheric temperature data. The spatial resolution of the
154 original data was $0.5^\circ \times 0.625^\circ$.

155 The NRLMSISE-00 atmospheric empirical model covers the altitude interval from the ground to the
156 thermosphere (0~1000 km), which can provide reference for the environmental state of the relevant missions
157 in the space industry. The input parameters include the solar and geomagnetic activity index, date, latitude,
158 longitude, altitude and local time, and the output elements are the temperature and density profile of the
159 neutral atmosphere.

160 When using reanalysis, empirical model, satellite data to compare with rocket detection results, it is
161 necessary to match the time and location of data effectively. The verification data close to the time (<5 h)
162 and within a certain deviation range of latitude (< 4°) and longitude (< 4°) are selected and interpolated to the
163 same vertical grid points as the data processed by the rocket.

164 4. Temperature correction and error calculation

165 4.1 Temperature correction

166 During the process of parachute fall, thermistor and the outside atmosphere has been a heat exchange,
167 in unit time, thermistor internal energy ΔE , self-heating L , convection exchange heat H , radiation exchange
168 heat Q , viscous exchange heat M , lead conduction heat exchange N have the following relationships (Wagner,
169 1964):

$$170 \quad \Delta E = L + H + Q + M + N, \quad (5)$$

171 According to the modified formula given by the World Meteorological Organization on the temperature
172 detection data of the rocket sonde, formula (5) is expanded to (Organization, 2008):

$$173 \quad T_\infty = T_f - \frac{rv_f^2}{2c_p} + \frac{m_r C}{Ah} \frac{dT_f}{dt} - \frac{A_m \rho_m \alpha_s J}{Ah} - \frac{\alpha_t \sigma (A_a T_a^4 + A_b T_b^4 + A_c T_c^4)}{Ah} + \frac{\varepsilon \sigma T_f^4}{h} - \frac{Q_c}{Ah} - \frac{W_f}{Ah} \quad (6)$$

174 Where T_f is the original temperature, T_∞ is the temperature after correction. The heating term $\frac{rv_f^2}{2c_p}$
175 reflects the influence of heat exchange between the thermistor and its boundary layer on the temperature
176 indication value. The temperature hysteresis term $\frac{m_r C}{Ah} \frac{dT_f}{dt}$ represents the influence of the hysteresis of
177 thermistor heat exchange on the temperature indication value. The reflected radiation term $\frac{A_m \rho_m \alpha_s J}{Ah}$
178 represents the influence of the short-wave solar radiation reflected by the ground and clouds to the sonde on
179 its temperature indication. The long wave radiation term $\frac{\alpha_t \sigma (A_a T_a^4 + A_b T_b^4 + A_c T_c^4)}{Ah}$ represents the influence of
180 radio frequency radiation and infrared radiation in the environment of the sonde on the temperature indication.

181 The external radiation term $\frac{\varepsilon\sigma T_f^4}{h}$ represents the influence of the thermal radiation of the sensor to the sonde
 182 on its temperature indication. The structural heat conduction term $\frac{Q_c}{Ah}$ represents the influence on the
 183 thermistor indication due to the thermal conduction of the sonde support to the thermistor. Measuring current
 184 heating term $\frac{W_f}{Ah}$ indicates the amount by which the temperature indication of the resistance changes due to
 185 the heating of the current. The sonde takes shading measures to ignore the direct solar radiation. The
 186 meanings of each item in equation (6) are shown in Table A1.

187 4.2 Error calculation

188 Temperature measurement error is composed of thermistor static calibration error σT_1 , temperature
 189 error caused by position error σT_2 , and temperature correction error ΔT_3 (Wagner, 1964, 1961), the
 190 calculation formula is as follows:

$$191 \quad \delta T = \sqrt{\sigma T_1^2 + \sigma T_2^2 + \Delta T_3^2}, \quad (7)$$

192 σT_1 and σT_2 are the systematic errors of the instrument, which are fixed values in calculation, ΔT_3 is
 193 the residual error after temperature correction (Eq. 6), and the formula is calculated as:

$$194 \quad \Delta T_3 = \Delta(T_\infty - T_f) = \Delta\left(-\frac{rv_z^2}{zc_p}\right) + \Delta\left(\frac{m_T c}{Ah} \frac{dT_f}{dt}\right) + \Delta\left(-\frac{A_s \alpha_s l}{Ah}\right) + \Delta\left(-\frac{Am \rho_m \alpha_s l}{Ah}\right) +$$

$$195 \quad \Delta\left(-\frac{\alpha_t \sigma (A_a T_a^4 + A_b T_b^4 + A_c T_c^4)}{Ah}\right) + \Delta\left(\frac{\varepsilon \sigma T_f^4}{h}\right) + \Delta\left(-\frac{Q_c}{Ah}\right) + \Delta\left(-\frac{W_f}{Ah}\right), \quad (8)$$

196 Wind speed error is composed of systematic error and random error. Systematic error is written as:

$$197 \quad \begin{cases} \Delta W_x = \Delta \dot{x} - \frac{\dot{z}}{\dot{z}-g} \Delta \dot{x} - \frac{\ddot{x}}{\dot{z}-g} \Delta \dot{z} + \frac{\ddot{x}\dot{z}}{(\dot{z}-g)^2} \Delta \ddot{z} \\ \Delta W_y = \Delta \dot{y} - \frac{\dot{z}}{\dot{z}-g} \Delta \dot{y} - \frac{\ddot{y}}{\dot{z}-g} \Delta \dot{z} + \frac{\ddot{y}\dot{z}}{(\dot{z}-g)^2} \Delta \ddot{z} \end{cases} \quad (9)$$

198 Random error is written as:

$$199 \quad \begin{cases} \sigma_{W_x}^2 = \sigma_{\dot{x}}^2 + \left(\frac{\dot{z}}{\dot{z}-g} \sigma_{\dot{x}}\right)^2 + \left(\frac{\ddot{x}}{\dot{z}-g} \sigma_{\dot{z}}\right)^2 + \left[\frac{\ddot{x}\dot{z}}{(\dot{z}-g)^2} \sigma_{\ddot{z}}\right]^2 \\ \sigma_{W_y}^2 = \sigma_{\dot{y}}^2 + \left(\frac{\dot{z}}{\dot{z}-g} \sigma_{\dot{y}}\right)^2 + \left(\frac{\ddot{y}}{\dot{z}-g} \sigma_{\dot{z}}\right)^2 + \left[\frac{\ddot{y}\dot{z}}{(\dot{z}-g)^2} \sigma_{\ddot{z}}\right]^2 \end{cases} \quad (10)$$

200 g is the gravity acceleration, $\Delta \dot{x}$, $\Delta \dot{y}$ and $\Delta \dot{z}$ are velocity fitting deviations, $\Delta \ddot{x}$, $\Delta \ddot{y}$, and $\Delta \ddot{z}$ are
 201 acceleration fitting deviations, $\sigma_{\dot{x}}$, $\sigma_{\dot{y}}$, and $\sigma_{\dot{z}}$ are speed random errors, $\sigma_{\ddot{x}}$, $\sigma_{\ddot{y}}$, and $\sigma_{\ddot{z}}$ are acceleration
 202 random errors.

203 The total error of wind speed and direction is calculated as follows:

$$204 \quad \begin{cases} \delta W_\varepsilon = \sqrt{\delta W_{x,\varepsilon}^2 + \delta W_{y,\varepsilon}^2} \\ \delta G = \frac{180}{\pi} \sqrt{\left(\frac{W_x \delta W_{y,\varepsilon}}{W_x^2 + W_y^2}\right)^2 + \left(\frac{W_y \delta W_{x,\varepsilon}}{W_x^2 + W_y^2}\right)^2} \end{cases} \quad (11)$$

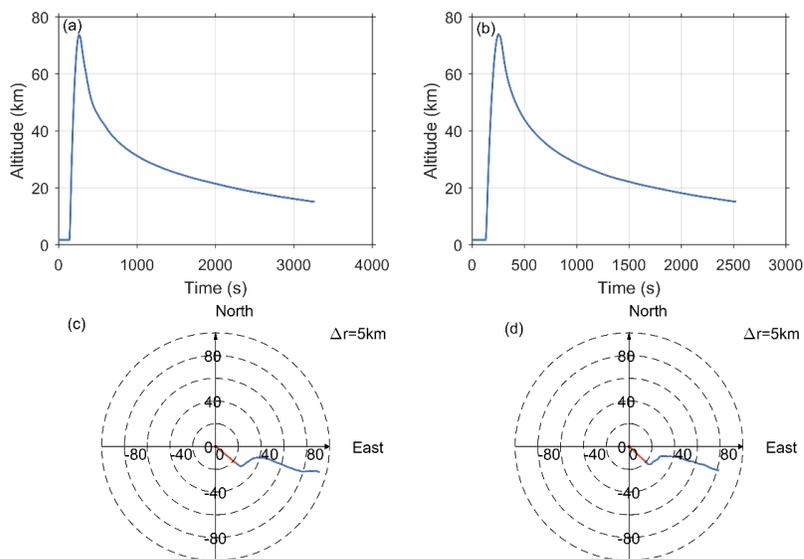
205 Where $\delta W_{x,\varepsilon} = \sqrt{\sigma_{W_x}^2 + \Delta W_x^2}$ is the meridional wind synthesis error, and $\delta W_{y,\varepsilon} = \sqrt{\sigma_{W_y}^2 + \Delta W_y^2}$ is the
 206 zonal wind synthesis error.

207 **5. Comparison of rocket detection results with reference data**

208 **5.1 Data quality and trajectory analysis**

209 The two rockets are referred to as HJ-1 and HJ-2, respectively. HJ-1 is launched at 9:00 UTC on the
210 first day, and HJ-2 is launched at 5:00 UTC on the next day.

211 The time-height curves of HJ-1 and HJ-2 are shown in Figure 3 (top). The actual detection altitude of
212 HJ-1 is about 74 km, the ascent time is about 2 minutes, and the fall time (from the highest point to an altitude
213 of 20 km) is 25 minutes. HJ-2 can reach a maximum altitude of 76 km, the ascent time is about 2 minutes,
214 and the fall time is 31 minutes. Taking the launch point as the central point, the horizontal motion trajectory
215 of the ascending stage of rocket launch and the sonde/parachute drift stage are plotted as shown in Figure 3
216 (below). When the rocket is launched, it rises basically eastward, and after reaching the highest point, the
217 sonde drifts eastward as it falls with the parachute, which is determined by the background wind field over
218 the area (the trajectory indicates that the entire layer is dominated by westerly winds). The sonde remained
219 within 100 km from the launch point during the entire detection process (from the beginning of the launch to
220 the 20 km falling height).

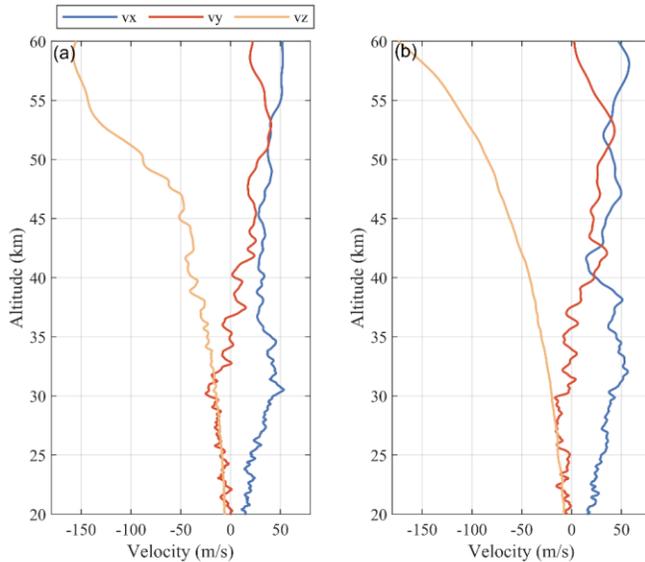


221

222 **Figure 3. Time-altitude curves of (a) HJ-1 and (b) HJ-2, and horizontal motion trajectory of (a) HJ-1 and (b) HJ-**
223 **2 (red for rocket ascent, blue for sonde/parachute drift).**

224 In order to further analyze the trajectory characteristics of the sonde during its fall, the vertical
225 distribution of zonal velocity (v_x), meridional velocity (v_y) and vertical velocity (v_z) are shown in Figure 4.
226 The zonal velocity of the two rockets is positive, and the meridional velocity gradually changes from positive
227 to negative, which corresponds to the characteristics of the falling trajectory drifting first to the northeast and

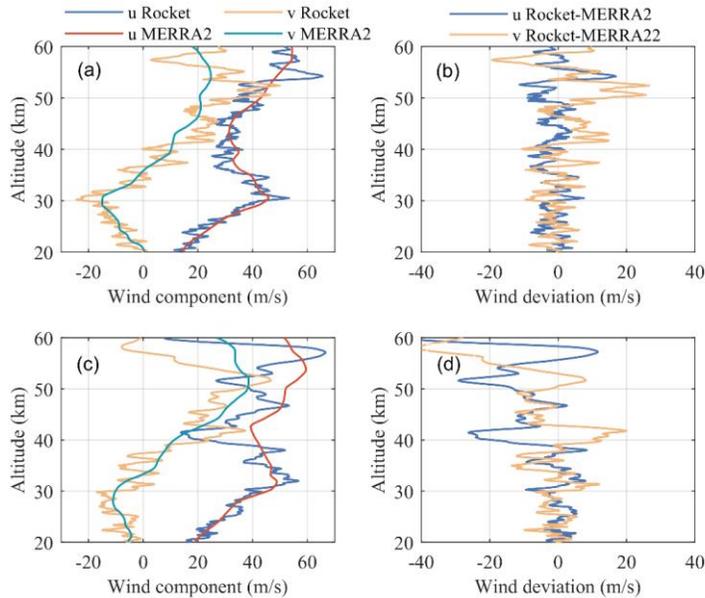
228 then to the southeast in Figure 3. It is worth noting that there is an obvious disturbance characteristic (denser
 229 small scale layered structure) of vertical velocity for HJ-1, compared with that of HJ-2. After the same data
 230 processing method, the obvious difference of v_z profile roughness may reflect the great difference of
 231 disturbance in the vertical direction at high altitudes.



232
 233 **Figure 4. Velocity-altitude curves of (a) HJ-1 and (b) HJ-2.**

234 5.2 Wind and temperature measurements

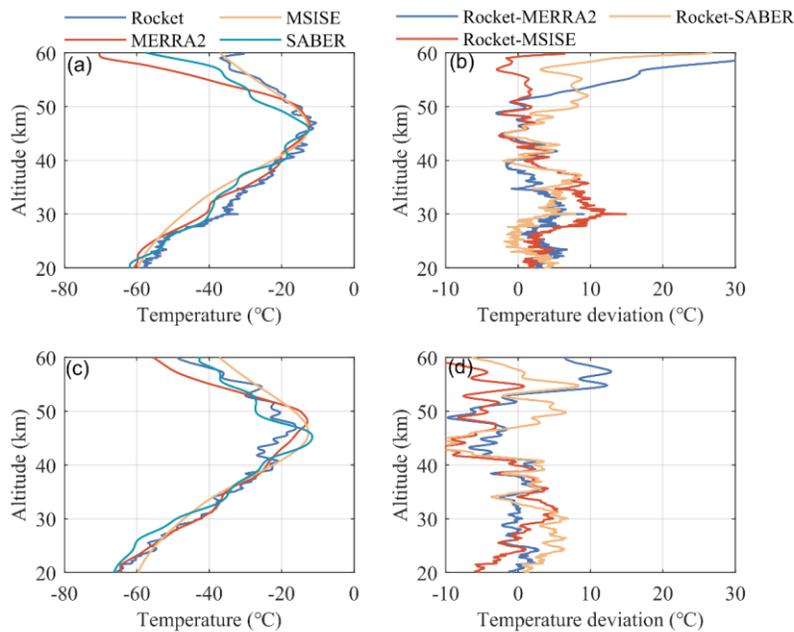
235 Figure 5 shows the comparison of the zonal and meridional winds obtained by the two rockets with the
 236 MERRA2 data. Before the launch of the rocket, the balloon sounding is also carried out. In the detection
 237 altitude range of the balloon, the wind speed and direction from the rocket are in good agreement with the
 238 balloon profile, and the details of the disturbance are basically consistent (Figure A1), indicating the
 239 reliability of the retrieved wind field results. The meridional winds of the two rockets both reach the
 240 maximum value near 50 km, exceeding 40 m/s. As reflected in Figure 3, in the initial stage of fall after the
 241 rocket body-parachute separation, the trajectory turns from south to north, which proves that the strong
 242 meridional winds dominate at high altitudes.



243
244 **Figure 5. (a) The vertical distribution of zonal wind and meridional wind of HJ-1, (b) the difference of HJ-1**
245 **velocity component with MERRA2, (c) the vertical distribution of zonal wind and meridional wind of HJ-2, and**
246 **(d) the difference of HJ-2 velocity component with MERRA2.**

247 Here, we use the deviation result describes the gap between the rocket detection data and the reference
248 value (satellite, reanalysis, etc.). The purpose is to demonstrate the degree of consistency or deviation
249 between the rocket detection results and other data, and it is a comparison between different data. HJ-1 and
250 MERRA2 have basically the same variation trend of wind speed components at the altitude of 20~60 km,
251 and the zonal wind deviation is relatively small in the whole altitude, while the meridional wind deviation
252 has large positive and negative fluctuations between 50~60 km. The average deviation (absolute value) of
253 the zonal wind at the whole altitude is 3.3 m/s, and that of the meridional wind is 5.4 m/s. In contrast, the
254 measured wind of HJ-2 has greater fluctuation than that of MERRA2, and the deviation between the two
255 increases significantly above 40 km. The average deviation of zonal wind is 7.5 m/s and that of meridional
256 wind is 7.6 m/s. In the altitude range of 20~45 km, the variation trend of wind speed is consistent. At higher
257 altitudes, the measured wind speed of the rocket can show more significant fluctuation characteristics. There
258 are maximum wind speed areas near 30 km and 55 km for both the two rockets, and the maximum near 55
259 km is difficult to reflect in the MERRA2 data. This indicates that the reanalysis data may lack observation
260 results for assimilation at higher altitudes, and the difference of wind field in the upper stratosphere is
261 obviously greater than that in the lower stratosphere even in the close spatiotemporal range. Considering that
262 the output from the model tends to reflect the average trend, and the transient results of a single detection are
263 more prominent, it is reasonable to have differences between the rocket detection and the model.

264 Figure 6 shows the vertical distribution of temperature from rocket, SABER, MSISE, and MERRA2
 265 data and the corresponding deviation from them. Results before and after temperature correction and
 266 corresponding sub-term correction amount are shown in Figure A2, the temperature correction is larger above
 267 50 km, and gradually decreases below 50 km. Among the various correction sub-items for rocket detection
 268 temperature, the influence degree of pneumatic heating, current heating, and temperature hysteresis are
 269 relatively large, and these influences gradually decrease as the height decreases overall. The corrected
 270 temperature is smaller than original temperature in the entire height. According to the maximum temperature,
 271 the stratopause height measured by the rocket (the height of the inflection point) is around 47 km. The
 272 stratopause height is consistent with other reference data for HJ-1, but shows some differences for HJ-2. The
 273 temperature profiles of the four data have a consistent trend from 20 km to 50 km, with small deviation.
 274 The deviation between the reference data and the rocket detection results increases above 50 km. In this interval,
 275 the temperature deviation between HJ-1 and MISIS is the smallest, while the difference between HJ-2 and
 276 SABER is the smallest. It is worth noting that the temperature deviation of HJ-1 above 57 km has a sharp
 277 trend, which may be resulted from its measurement error (discussed later). The difference of data comparison
 278 may be due to the following reasons: 1) There are deviations in the position and time of the reference data
 279 matching with the rocket; 2) The results of the model reflect the average over time and space, which is indeed
 280 different from the single-point profile.

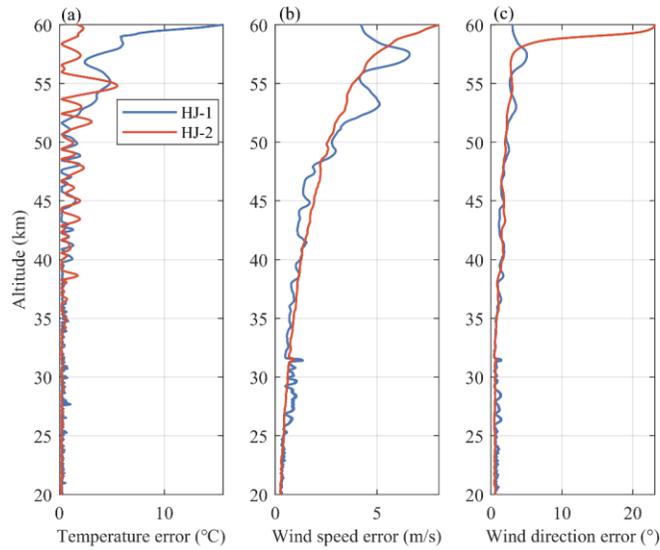


281
 282 **Figure 6. (a) The vertical distribution of temperature for HJ-1, (b) the difference of HJ-1 temperature with**
 283 **MERRA2, MSISE, and SABER, (c) the vertical distribution of temperature for HJ-2, and (d) the difference of**
 284 **HJ-2 temperature with MERRA2, MSISE, and SABER.**

285 The vertical distribution of rocket detection density and their relative deviations with MERRA2, MSISE,
286 and SABER are also shown in Figure A3. The density relative deviation of HJ-1 shows a significant
287 maximum value between 40 and 50 km (the deviation can reach about 10% for the above three reference
288 data), while the relative density deviation of HJ-2 is significantly smaller, especially with excellent
289 consistency with the SBAER data (the relative deviation within the entire detection height range is within
290 5%). The large density deviation of HJ-1 in the upper atmosphere is, on the one hand, due to the significant
291 reduction in the density itself, which makes the difference more prominent. On the other hand, it is very likely
292 that there are other strong atmospheric disturbances causing drastic changes in density (discussed later),
293 which have not been captured by the model and satellite data.

294 6. Error analysis

295 Accurate measurement is the prerequisite for conducting further data analysis and application. To further
296 analyze the sources of deviation between the rocket detection results and other data, as well as the reliability
297 of the disturbance analysis, the error level of the rocket instrument is discussed here, which is a comparison
298 among different heights and sub-items within the rocket own detection results. Temperature and wind
299 measurement errors of HJ-1 and HJ-2 can be obtained according to Eq. 8 and Eq. 11, as shown in Figure 7.
300 Systematic and random errors of wind speeds are shown in Figure A3 and Figure A4, respectively. The
301 atmospheric temperature error level (regional average) of HJ-1 is 0.31 °C, 0.53 °C and 5.5 °C at 20-30 km,
302 30-50 km and above 50 km, while that of HJ-2 is 0.24 °C, 0.55 °C and 1.75 °C. The wind speed error level
303 of HJ-1 is 0.63 m/s, 1.12 m/s and 4.95 m/s at 20-30 km, 30-50 km and above 50 km, while that of HJ-2 is
304 0.38 m/s, 1.19 m/s and 4.0 m/s. The wind direction error levels of HJ-1 are 0.81°, 1.08° and 3.15° at 20-30
305 km, 30-50 km and above 50 km, respectively, while that of HJ-2 is 0.54°, 1.11° and 4.25°. According to Eq.
306 9 and Eq. 10, when the vertical acceleration and vertical velocity are too large, the denominator $\ddot{z} - g$
307 decreases and the numerator \dot{z} increases, which can obviously affect the results of systematic error and
308 random error. In the whole detection section, the same smooth fitting points are used, so the velocity error is
309 consistent. However, due to the large jump of the positioning data, the acceleration ratio in the inertial
310 velocity will also jump. When the falling velocity is large, the product will also increase, resulting in a
311 significantly larger error margin at the high altitudes.



312

313 **Figure 7. Error-height curves of (a) temperature, (b) wind speed, and (c) wind direction for HJ-1 and HJ-2.**

314 The original temperature vertical gradient and vertical acceleration of HJ-1 and HJ-2 are shown in
 315 Figure 8. In the initial falling stage (50-60 km) after the parachute separation, the falling speed is too large,
 316 and the acceleration fluctuates significantly in this height range. The vertical acceleration of HJ-1 has two
 317 peaks between 50-60 km, and there are also maximum values in the corresponding height of the wind speed
 318 random error and systematic error profile (Fig. A3). The vertical acceleration of HJ-2 increases rapidly above
 319 50 km, which also corresponds to the increasing trend of wind speed component in systematic error and
 320 random error. According to the error equation, the measurement error of wind speed depends largely on the
 321 velocity error and acceleration error. At the same time, the temperature error is also related to the vertical
 322 gradient of the measured temperature indication value (in HJ-1, the obvious gradient deviation above 58 km
 323 and its ratio to the convective heat exchange coefficient cause the temperature error to increase sharply),
 324 which is also the reason why the temperature error and wind field error in Figure 7 have inconsistent trends.
 325 Through the above analysis, we believe that the intensity of vertical acceleration fluctuation directly affects
 326 the error results of wind field measurement. At high altitudes (near to 60 km), the parachute swing is large,
 327 and the data reception is not stable, resulting in the relatively low positioning data quality and the large
 328 position error, which finally lead to the relatively large wind field error. As the detection height gradually
 329 decreases, the positioning data quality increases and the measurement error decreases gradually as the
 330 parachute falls steadily.

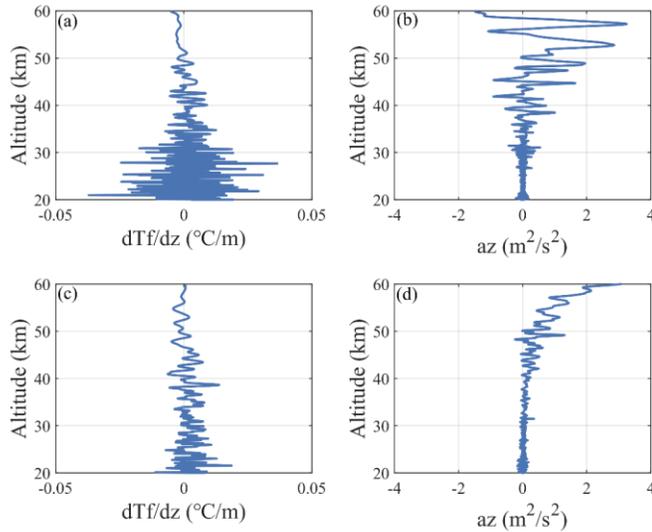


Figure 8. (a) Temperature gradient-height curve and (b) vertical velocity-altitude curve for HJ-1, (c) Temperature gradient-height curve and (d) vertical velocity-altitude curve for HJ-2.

7. Disturbance characteristic analysis

In the accuracy analysis of the two rocket detection results, we find that compared with HJ-2, HJ-1 has a more intense falling velocity disturbance, and the deviation from the reference data is larger. Profile deviation phenomena discovered in the result above are inferred to be closely related to the strong disturbance at this height. Therefore, it is necessary to further verify these phenomena in the atmosphere through disturbance characteristic analysis. Conducting wave disturbance analysis here, on the one hand, verify the previous detection results, and on the other hand, it is also an application study of rocket detection data, enhancing the theoretical nature and completeness of the rocket data analysis results.

7.1 Wave energy and background field analysis

Due to the lack of measured wind field data at high altitudes (30-60 km), the fine structure cognition of wind disturbance at corresponding interval is not sufficient. Many of the sharp peaks in the wind profile captured by balloon and rocket detections are real perturbations in the atmosphere (Figure 5 and Figure A1), which are smoothed out in the reanalysis. In other words, using rocket data may be more suitable for analyzing wave disturbance characteristics at high altitude, since reanalysis data failed to capture these details. The apparent differences in vertical velocity and acceleration of the sonde during its fall (Figure 8) also indicate significant differences in upper atmospheric disturbances. By analyzing the atmospheric background

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350 state and gravity wave (GW) information, we compare the difference characteristics of atmospheric
 351 disturbance in two detection processes.

352 GWs are generated by the excitation source at the lower atmosphere, and their amplitudes increase
 353 gradually as the atmospheric density decreases during upward propagation. Wind shear is an important
 354 disturbance source of high-altitude GWs, which can cause GWs to be generated or broken (Larsen, 2002;
 355 Larsen and Fesen, 2009). Vertical wind shear can be calculated by the following formula:

$$356 \quad \frac{dU}{dz} = \sqrt{\left(\frac{du}{dz}\right)^2 + \left(\frac{dv}{dz}\right)^2}, \quad (12)$$

357 Buoyancy frequency N can reflect the unstable state of the atmosphere. $N^2 > 0$ is the static stable state,
 358 and $N^2 < 0$ is the static unstable state. The square buoyancy frequency can be calculated by the following
 359 formula:

$$360 \quad N^2 = \frac{g}{T} \left[\left(\frac{dT}{dz} \right) + \frac{g}{c_p} \right], \quad (13)$$

361 The gradient Richardson number R_i can reflect the ratio of buoyancy work term to shear stress work
 362 term, which can be obtained by the ratio of the square of buoyancy frequency to the square of wind shear:

$$363 \quad R_i = \frac{N^2}{\left(\frac{du}{dz}\right)^2 + \left(\frac{dv}{dz}\right)^2}, \quad (14)$$

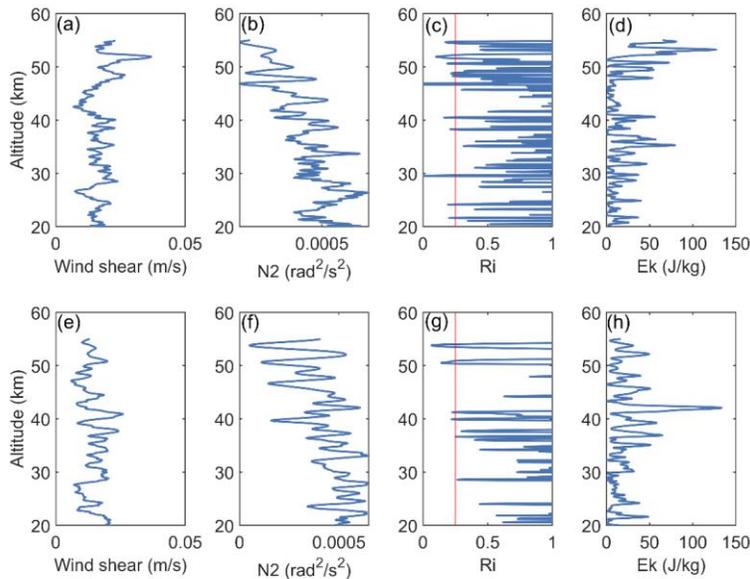
364 Atmospheric GWs can be regarded as superimposed disturbances to the background field. First, a 20-
 365 point sliding average is performed on the profile interpolated with equal spacing (50 m interval) to eliminate
 366 errors caused by random motion and turbulence. Then the smoothing profile is fitted by fifth-order
 367 polynomial to get the background profile. After the background profile is removed, high-pass filtering with
 368 a cut-off wavelength of 10 km is performed to obtain the disturbance profile caused by GWs. The kinetic
 369 energy E_k of GW is calculated by the following formula:

$$370 \quad E_k = \frac{1}{2} (u'^2 + v'^2), \quad (15)$$

371 Where u' and v' are the disturbance components of the zonal and meridional wind field caused by GWs,
 372 respectively.

373 In the error analysis, considering that the error becomes significant above 55 km (Figure 7), the height
 374 interval selected for disturbance analysis here is 20~55 km. The vertical distribution of wind shear, square
 375 buoyancy frequency, Richardson number and kinetic energy obtained according to HJ-1 and HJ-2 detection
 376 results are shown in Figure 9. The wind shear of HJ-1 has the first peak (strongest) near 45-55 km and the
 377 second peak near 30-40 km, while the wind shear peak of HJ-2 is between 30-40 km. The buoyancy frequency
 378 is positive at the whole altitude, indicating that the atmosphere is statically stable, but there is a tendency to
 379 decrease with the increase of altitude. HJ-1 has a buoyancy frequency minimum (even close to 0) between
 380 45 and 55 km, corresponding to large wind shear, resulting in a relatively concentrated area of $R_i < 0.25$,
 381 indicating strong dynamic instability. In contrast, HJ-2 has a smoother profile with smaller wind shear and
 382 larger buoyancy frequency, resulting in fewer dynamic instability regions. For HJ-1, the peak kinetic energy
 383 of GW is above 50 km, corresponding to the maximum value region of wind shear, and the dynamic
 384 instability region is relatively concentrated, indicating that Kelvin-Holtzmann instability has produced strong

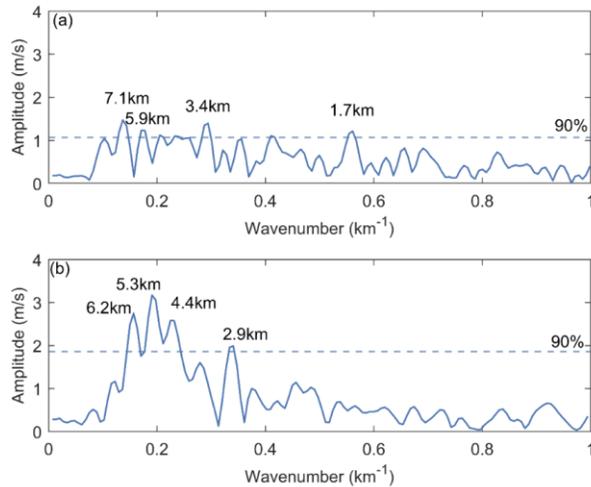
385 high-altitude wave disturbance. Below 50 km, the GW energy of HJ-1 is significantly smaller than that of
 386 HJ-2, which is mainly due to the attenuation of zonal wave disturbance (Figure A5).



387
 388 **Figure 9. (a) wind shear, (b) square buoyancy frequency, (c) Richardson number and (d) kinetic energy of HJ-1,**
 389 **and (e) wind shear, (f) square buoyancy frequency, (g) Richardson number and (h) kinetic energy of HJ-2.**

390 7.2 Spectral analysis

391 Lomb-Scargle spectrum analysis is performed to the disturbance profile of the synthesized wind speed,
 392 and the vertical wave-number spectrum caused by GWs are obtained, as shown in Figure 10. The amplitudes
 393 of GWs measured by HJ-1 are significantly weaker than those measured by HJ-2, and the vertical
 394 wavelengths of the dominant GWs (amplitudes greater than 90% confidence) are more dispersed, with scales
 395 ranged from 1.7 km to 7.1 km present. In contrast, the dominant GWs measured by HJ-2 have stronger
 396 amplitudes and are concentrated at wavelengths around 4-6 km and 2.9 km.



397
398 **Figure 10. Gravity wave information for (a) HJ-1 and (b) HJ-2 obtained from the disturbance profile of the wind**
399 **field, dashed lines represent 90% confidence, and dominant wavelengths with amplitudes above this threshold are**
400 **labeled.**

401 Through atmospheric instability analysis and GW spectrum analysis, we found that the atmospheric
402 disturbance for HJ-1 is more complex. The GW breaks, resulting in enhanced turbulent activity (more
403 dynamic unstable regions), which also leads to a significant reduction in stratification stability (reduced
404 buoyancy frequency) with more small-scale stratification (Held et al., 2019; van Haren et al., 2015). The GW
405 kinetic energy can be reduced and the amplitude corresponding to the dominant wavelength decreases.
406 Therefore, compared with HJ-2, the measured temperature and wind field profile of HJ-1 have more obvious
407 fluctuations and a denser small-scale layered structure. In addition, the wave energy of HJ-1 is significantly
408 lower than that of HJ-2 in the range of 40-50 km (Figure 9), which is considered to be the main region where
409 wave dissipation occurs. At this time, the zonal and meridional winds of HJ-1 are also smaller than those of
410 HJ-2 between 40-50 km, while their trends and magnitudes below 40 km are indeed similar (Figure 5), which
411 further indicates that wave dissipation weakens the local winds. The fragmentation and dissipation of GWs
412 in the upper stratosphere can reasonably explain the difference of detection profiles in adjacent two days.

413 7.3 Wave dissipation revealed from Stokes parameter method and ERA5 results

414 In order to further prove that the GW at the height of 40-50 km in the detection of HJ-1 has broken up,
415 Stokes parameter method (Vincent et al., 1987; Eckermann., 1996) is used here to extract the typical
416 characteristic parameters of the GW. The main realization path is as follows: Fourier transform is applied to
417 the zonal wind and meridional wind disturbances, and corresponding real and imaginary parts are obtained
418 respectively. Then four Stokes parameters I, D, P and Q are calculated, and information such as scale,

419 propagation and frequency of polychromatic gravity waves can be further obtained. The specific method can
420 be referred to the previous paper (He et al., 2022).

421 Considering that the wave breaking mainly occurs below 50 km, the GW parameters are calculated for
422 the two height intervals of 40-50 km and 20-50 km, corresponding to disturbance information in the local
423 and entire height range, respectively. The kinetic energy, horizontal wavelength, intrinsic frequency, vertical
424 group velocity and horizontal propagation direction extracted from the two detections are shown in Table 1.
425 For a local wave disturbance (40-50 km), there is a low-frequency GW of HJ-1, with an intrinsic frequency
426 (the ratio of wave frequency to inertial frequency) of 2.53. The order of wavelength, kinetic energy and
427 vertical group velocity is within a reasonable range. In contrast, the intrinsic frequency and vertical group
428 velocity of HJ-1 are abnormally large, while the horizontal wavelength ~~are is~~ abnormally small, which should
429 belong to the omitted cases. The outliers of the characteristic parameter also reflect the breaking of GWs in
430 this region from the perspective of abnormal high frequency waves (Fritts and Alexander, 2003), meaning
431 that GWs can no longer maintain their normal state and dissipate. For the entire wave disturbance (20-50
432 km), HJ-2 has no obvious wave breaking, and the parameters such as wavelength and frequency are close to
433 the local disturbance, which means a consistent wave propagation process throughout the entire height. In
434 contrast, the wavelength and kinetic energy of the entire wave disturbance of HJ-1 are smaller than that of
435 HJ-2 due to local wave breaking. The wave propagation direction of HJ-2 is significantly different in the
436 entire and local ranges, possibly due to significant wind speed changes near 40 km (Figure 5c).

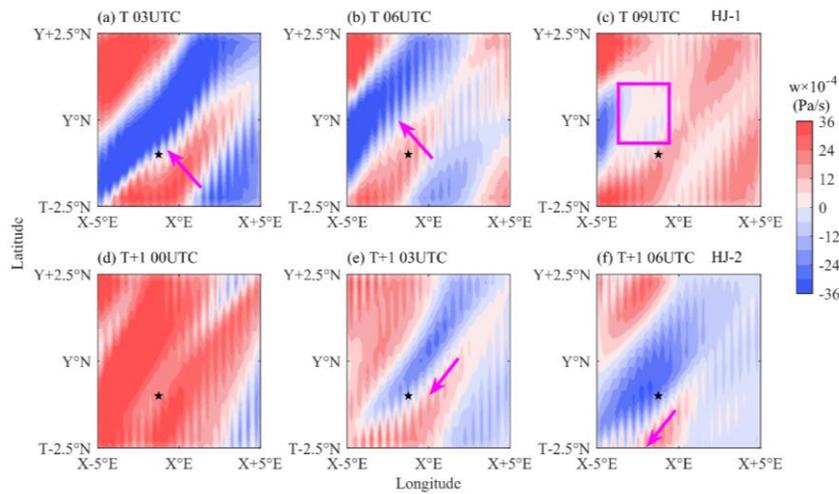
437 Table 1. Gravity wave parameters extracted by Stokes parameter method

detection zone	kinetic energy (J/kg)	horizontal wavelength (km)	intrinsic frequency (w/f)	vertical group velocity (m/s)	horizontal propagation direction
HJ-1 (40-50 km)	13.55	1.08	434.71	15.77	138°
HJ-2 (40-50 km)	28.16	235	2.53	0.088	215°
HJ-1 (20-50 km)	14.38	140	3.74	0.12	145°
HJ-2 (20-50 km)	20.79	296	2.53	0.10	-36°

438 Although the time interval of the two detections is one day apart, considering that the momentum
439 deposition of GW to the mean flow is continuous and slow (Liu et al., 1999), the comparison of the wind
440 field results from the two detections may still indicate the effect of GW drag. For the local wave breaking of
441 HJ-1 (40-50 km), the propagation direction is northwest (the degrees in Table 1 represent angle measured
442 anticlockwise from x axis), and the deposited momentum produces negative drag (deceleration) on the zonal
443 wind and positive drag (acceleration) on the meridional wind. Compared with the earlier detection,
444 significantly stronger meridional wind and significantly weaker zonal wind can be seen near 40 km in the
445 later detection (Figure 5). This suggests that the drag effect of local wave breaking through deposited
446 momentum is captured at an altitude of 40 km by HJ-2, and the acceleration of tens of meters per day is also
447 reasonable (Li et al., 2022).

448 In order to further support the wave breaking at high altitude during HJ-1 detection, ERA5 data is used
449 to plot the longitude-latitude cross section of vertical velocity at 3hPa (near 41km) in the corresponding

450 region (10° longitude \times 5° latitude), as shown in Figure 12. HJ-1 detection is close to 09UTC (launched at
 451 9.5UTC) on the first day (T), and HJ-2 detection is close to 06UTC (launched at 5.5UTC) on the second day
 452 (T+1). In this pressure layer, the vertical velocity (w) has an obvious alternating positive and negative
 453 perturbation, which indicates the GW activity. For the first day of detection, at 03UTC and 06UTC, the
 454 northwestward movement of the GW is observed. At 09UTC, there is a distinct wave breaking (purple
 455 rectangular box). For the second day of detection, at 03UTC and 06UTC, the southwestward movement of
 456 the perturbation peaks can be observed, and no wave dissipation occurs in the corresponding region. Both
 457 the time of wave dissipation and the direction of wave propagation are consistent with the results calculated
 458 by Stokes parameter method from rocket data (Table 1), which further proves the reliability of the results.



459

460 **Figure 12.** Regional distribution of ERA5 vertical velocity (w) at 3hPa for (a) 03UTC, (b) 06UTC, and (c) 09UTC
 461 on the first day, and (d) 00UTC, (e) 03UTC, and (f) 06UTC on the second day, with the five-pointed star
 462 representing the rocket detection position. The purple arrow represents the direction in which the wave travels,
 463 and the purple rectangular box represents the region where the wave dissipates occurs. The launch point of rocket
 464 is ($X^\circ\text{E}, Y^\circ\text{N}$).

465 8. Summary

466 In this study, the detection effects and data quality of two meteorological rocket launched in the
 467 northwest of China in the autumn of 2023 are analyzed. First, using the modified temperature correction
 468 model and wind field retrieval algorithm, the atmospheric temperature, pressure, density, wind speed and
 469 wind direction measured by the rocket are obtained, and compared with the matched reanalysis, satellite and
 470 empirical model data. Then, using the methods of error transfer and error synthesis, the measuring error and
 471 data accuracy from rocket detection are calculated, and the influence effect is evaluated. Finally, the
 472 characteristics of atmospheric instability and GW activity are analyzed and discussed. The main conclusions
 473 are as follows:

474 (1) The data acquisition rate of the two rockets is ideal, and the motion trajectory of the ascending and
475 falling stages is normal and smooth. It is a relatively successful detection experiment, which can obtain good
476 quality meteorological data in the range of 20 to 60 km.

477 (2) The rocket detection wind field and MERRA2 wind field have a good agreement below 40 km, and
478 the deviation becomes larger above 40 km. The temperature detection data below 50 km has a good agreement
479 with MERRA2, MISIS and SABER, and the deviation above 50 km begins to increase. The difference in
480 time and space of the matching data, as well as the difference between the model average and the
481 instantaneous detection may be the source of the result bias.

482 (3) Below 50 km, the wind measurement error and temperature measurement error are maintained at a
483 small level, less than 2 m/s and 1.8 °C, respectively. Above 50 km, the error begins to increase. This is
484 because in the early stage of fall, the parachute swing is large, so the position error is large. The data reception
485 is not stable, and the relative speed of the sensor and the air is too large. The above phenomenon leads to the
486 large error.

487 (4) The difference in the intensity of GWs causes the obvious difference in vertical velocity of the
488 dropsonde. For HJ-1, the amplitude of GWs over this region is reduced, and turbulent activity is enhanced,
489 resulting in reduced stability of atmospheric stratification and a denser small scale hierarchical structure on
490 the profile. For HJ-2, the stratification stability of the upper atmosphere is stronger. GWs are more stable and
491 less likely to break, allowing the amplitude to grow to a larger degree.

492 (5) The local breaking of GWs at 40-50 km can be captured ideally from HJ-1. The GWs deposited
493 momentum and energy to the mean flow, and the effect of the wave drag changed the wind field structure
494 below, making HJ-2 with one day delay can detect significant wind field changes near the altitude of 40 km.
495 This reflects the forcing effect of wave dissipation on the background wind field through the observation
496 results. The results of ERA5 data further support the wave dissipation and propagation characteristics
497 extracted by rocket data.

498 The analysis shows that due to the high vertical resolution and in-situ detection method, the rocket drop
499 sounding can capture the fine structure of the atmosphere close to the real state. Accurate and detailed wind
500 field results are very valuable, especially in the region above 30 km. The large measurement error above 55
501 km also indicates that it is necessary to improve the data reception quality at the beginning of the drop, and
502 optimize the high-altitude parachute opening and stability control technology to improve the detection
503 accuracy. The existence of atmospheric gravity wave causes the local feature difference of the detection
504 profile, meaning that the high-altitude disturbance characteristics need to be considered in the rocket
505 detection. This study can support the application of the wave dissipation theory in the upper stratosphere by
506 using the rocket data, while the corresponding ideal observation examples at this altitude are scarce. More
507 subsequent rocket detections are also encouraged to be carried out, thereby improving the cognition level of
508 the near-space atmospheric environment in multi-regions and multi-time.

509

510 Appendix A

511 Table A1. Main performance indicators of rocket radiosondes

<u>Indicator name</u>	<u>Performance parameters</u>	
<u>Transmitter frequency</u>	400MHz ~ 406MHz	
<u>Carrier frequency stability</u>	±20kHz	
<u>Emission spectral width</u>	≤50kHz (-50dB)	
<u>Transmitter power</u>	100mW ~ 200mW	
<u>Digital signal transmission mode</u>	GFSK	
<u>Data transmission rate</u>	4800bps	
<u>Data update rate</u>	≥2Hz	
<u>Positioning accuracy</u>	<u>Horizontal direction</u>	5m (CEP 90%)
	<u>Vertical direction</u>	5m (CEP 90%)
	<u>Speed</u>	0.2m/s (CEP 90%)
<u>Temperature</u>	<u>Measurement range</u>	-90°C ~ +55°C
	<u>Static calibration accuracy of the sensor</u>	≤±0.2°C
	<u>Resolution</u>	0.1°C
	<u>Measurement range</u>	1060hPa ~ 5hPa
<u>pressure</u>	<u>Static calibration accuracy of the sensor</u>	≤±0.8hPa
	<u>Resolution</u>	0.1hPa

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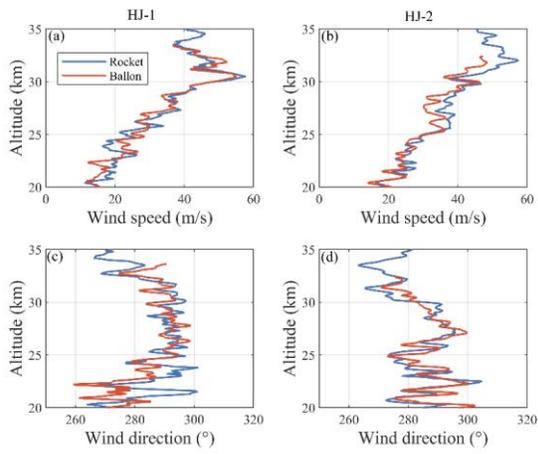
Table A+A2. variable meaning in the equation (6)

<u>variable</u>	<u>meaning</u>	<u>variable</u>	<u>meaning</u>
r	Thermistor boundary layer temperature recovery coefficient	α	Stefan-Boltzmann constant
v_r	The speed at which the thermistor moves with respect to the atmosphere	J	Solar constant
c_p	Specific heat capacity of air at constant pressure	α_t	Absorption rate of long wave by thermistor
$m_T C$	Heat capacity of a thermistor	$A_a/A_b/A_c$	The effective area of the thermistor receiving upper/body/lower bound atmospheric long wave radiation

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A	The surface area of the thermistor	$T_a/T_b/T_c$	Equivalent blackbody temperature of upper/body/lower bound atmospheric long-wave radiation source
h	Convective heat exchange coefficient between thermistor and air	ϵ	Thermistor the emissivity of thermal radiation
$\frac{dT_f}{dt}$	The rate of change of temperature with time	Q_c	Heat conduction coefficient
A_m	The area of the thermistor reflected by the ground and clouds	W_f	Current work coefficient
ρ_m	Combined reflection coefficient of ground and cloud		

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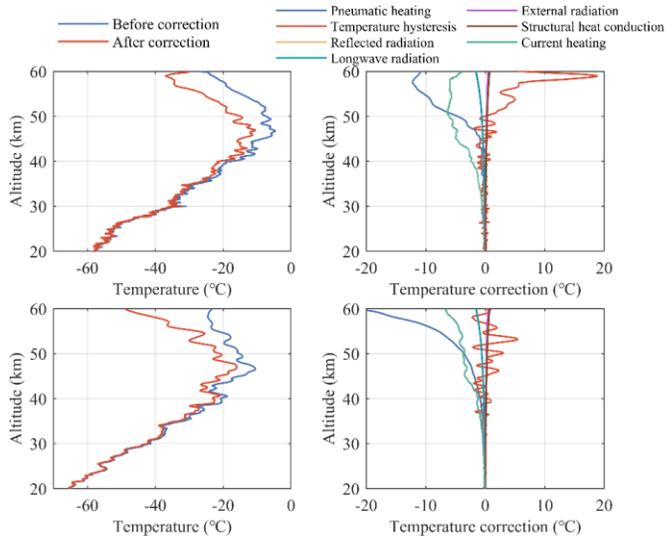


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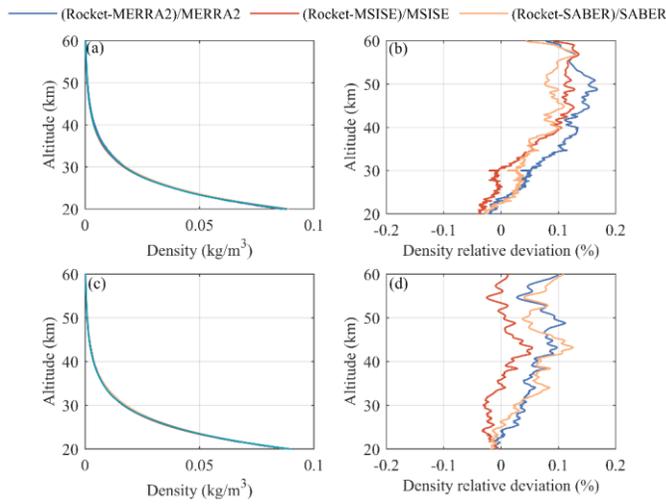
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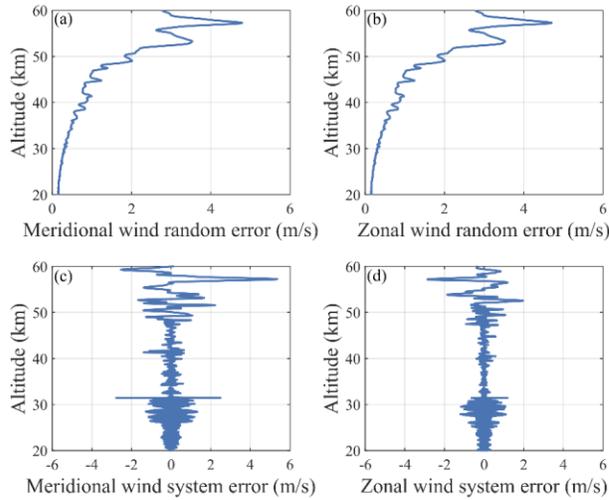
Figure A1. Comparison of wind speeds measured by rockets and balloons for (a) HJ-1 and (b) HJ-2, and comparison of wind directions measured by rockets and balloons for (c) HJ-1 and (d) HJ-2



525
526 **Figure A2. The vertical distribution of (a) original and corrected temperature, and (b) each correction subterm.**



527
528 **Figure A2A3. The vertical distribution of rocket detection density for (a) HJ-1 and (c) HJ-2. The relative deviation**
529 **of rocket detection density with MERRA2, MSISE, and SABER for (b) HJ-1 and (d) HJ-2.**
530 **The vertical distribution**
531 **of (a) original and corrected temperature, and (b) each correction subterm.**

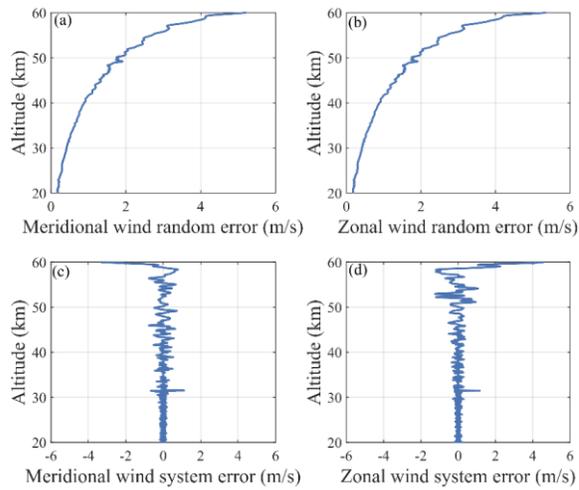


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Figure A3A4. Random error of (a) meridional wind and (b) zonal wind, and systematic error of (c) meridional wind and (d) zonal wind for HJ-1

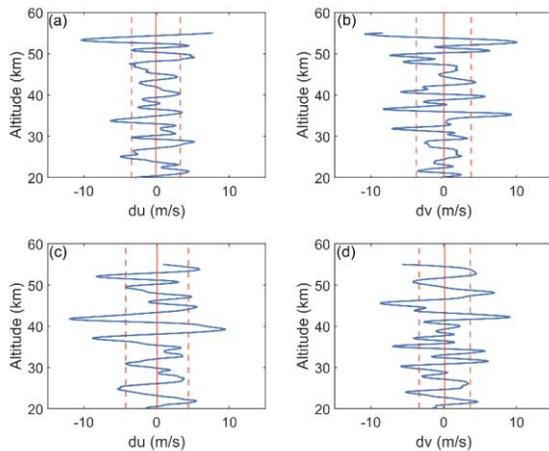


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Figure A4A5. Random error of (a) meridional wind and (b) zonal wind, and systematic error of (c) meridional wind and (d) zonal wind for HJ-2



538
 539 **Figure A5A6.** (a) Zonal wind and (b) Meridional wind disturbance profile caused by GWs for HJ-1, and (c) Zonal
 540 wind and (d) Meridional wind disturbance profile caused by GWs for HJ-2. The solid and dashed lines represent
 541 the mean and standard deviation over the entire height, respectively

542 Code and data availability

543 SABER data are available from ftp://saber.gats-inc.com/Version2_0/Level2A/ website, MERRA2 data
 544 are available from <https://disc.gsfc.nasa.gov/> website. The data processing scripts and the rocket data are
 545 available from the first author upon reasonable request.

546 Author contributions

547 HM and SZ initiated the study. HY and HJP designed the scheme, HY analyzed data and drew figures,
 548 HY wrote the manuscript. All the authors interpreted results and revised the manuscript.

549 Competing interests

550 The contact author has declared that neither of the authors has any competing interests.

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 553 and the National Natural Science Foundation of China (Grant no. 42275060). Additionally, helpful comments
 554 by the editors and the specific anonymous reviewers are gratefully acknowledged.

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