Accuracy of tracer-based methane flux quantification: underlying impact of calibrating~~Measuring~~ acetylene measurements~~with a cavity ring-down spectroscopy gas analyser and its use as a tracer to quantify methane emissions~~

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Abstract. Facility-scale methane emission fluxes can be derived by comparing tracer and methane mole fraction measurements downwind of a methane emission source, where a co-located tracer gas is released at a known flux rate. Acetylene is a commonly used methane tracer ~~for methane~~ due to its availability, low cost and low atmospheric background. Acetylene mole
15 fraction can be measured using infrared gas analysers such as the cavity ring-down spectroscopy Picarro G2203~~, using cavity ring-down spectroscopy~~. However, failure to calibrate tracer gas analysers may influence methane flux estimation, due to inaccurate~~if~~ raw tracer mole fraction measurements ~~diverge from their true levels~~. We conducted extensive Picarro G2203 laboratory characterisation testing. Picarro G2203 acetylene measurements were calibrated by diluting a high concentration of acetylene with ambient air. ~~In order to determine t~~The precise level of acetylene in each dilution blend~~calibration gas mixture~~
20 was determined by diluting~~,~~ a high concentration methane source ~~was diluted~~ in an identical way, with reliable methane mole fraction measurements used to quantify the true level of dilution. A linear calibration fit applied to raw acetylene mole fraction measured by the Picarro G2203 showed~~It was found~~ that these~~raw Picarro G2203 acetylene mole fraction~~ measurements could be corrected through direct multiplication with a calibration gain factor of 0.94~~, derived by applying a linear fit between raw measured and reference acetylene mole fraction~~. However, this specific calibration for the Picarro G2203 tested in this study
25 is only valid from an acetylene mole fraction of 1.16 ppb, below which unstable measurements were observed ~~by the Picarro G2203 tested in this study~~. The same Picarro G2203 was used during a~~A~~ field study to~~was then conducted by~~ perform~~ing~~ fourteen successful transects downwind of an active landfill site, where a point-source acetylene ~~was~~ release was conducted ~~from a single point location~~ at a fixed flow rate. Methane fluxes were derived by integrating the methane and acetylene mole fraction plumes, as a function of distance along the sampling road. This resulted in a ±56% flux variability ~~of 56%~~ between
30 ~~methane flux estimates from~~ different transects which was principally due to ~~flux~~ errors associated with the tracer release location and downwind sampling positioning. Methane fluxes were also derived using raw uncalibrated Picarro G2203 acetylene mole fraction ~~measurements~~ instead of calibrated measurements, which resulted an average methane emission flux

underestimation of approximately 87.6% for this specific study, compared to fluxes derived using calibrated measurements. Unlike a random uncertainty, this 7.6% bias represents a consistent flux underestimation that cannot be reduced bywith improvingements to the field sampling methodology; the only solution is using calibrated acetylene mole fraction measurements. The magnitude of the bias is principally due to the 0.94 multiplicative gain factor. Therefore, a similar level of methane flux bias can be expected in other studies when using uncalibrated acetylene mole fraction measurements from the Picarro G2203 tested in this work. This study therefore emphasises the equal importance of calibrating both target as well as tracer gas measurements, regardless of the instrument being used to obtain these measurements. Otherwise, biases can be induced within target gas flux estimates. For the example of methane, this can influence our understanding of the role of certain facility-scale emissions within the global methane budget.

1. Introduction

The greenhouse effect, which was first proposed over a century ago, is responsible for elevating Earth's near-surface temperature (Arrhenius, 1896). It is caused by various atmospheric species of which methane is the third most important (Mitchell, 1989), in terms of overall radiative forcing (Schmidt *et al.*, 2010). Methane had an effective radiative forcing in 2019 compared to prior to the onset of the industrial era (defined here as the year 1850) of 0.504 W m^{-2} in 2019(Forster *et al.*, 2021), which was one quarter that of carbon dioxide (Dentener *et al.*, 2021). Methane has an annualised average background mole fraction of greater than 1.9 ppm (Dlugokencky *et al.*, 1994, Lan *et al.*, 2024), which is over twice as high as it has ever been up to 800 000 years prior to the onset of the industrial era, defined here as the year 1850 (Chappellaz *et al.*, 1990, Etheridge *et al.*, 1998, Loulergue *et al.*, 2008). Recent estimates suggest that direct anthropogenic emissions may be responsible for over 50% of total methane emissions (Saunois *et al.*, 20240). Yet there remain large uncertainties in the global methane budget (Dlugokencky *et al.*, 2011, Kirschke *et al.*, 2013, Nisbet *et al.*, 2019, Saunois *et al.*, 2020, Lan *et al.*, 2021), which is in large part due to uncertainties in emissions from anthropogenic facility-scale sources (Jackson *et al.*, 2020, Nisbet *et al.*, 2021, Bastviken *et al.*, 2022, Saunois *et al.*, 2024) such as oil and gas extraction infrastructure (Foulds *et al.*, 2022, Wang *et al.*, 2022), agricultural facilitates (Shah *et al.*, 2020, Hayek and Miller, 2021, Marklein *et al.*, 2021), wastewater treatment facilities (Moore *et al.*, 2023, Song *et al.*, 2023) and landfill sites (Maasakkers *et al.*, 2022, Kumar *et al.*, 2024, Wang *et al.*, 2024). Saunois *et al.* (20240) estimated that landfills and waste collectively contributed towards approximately 109% of total methane emissions in the year 20207.

Emissions from individual facility-scale methane sources can be quantified either using inventory-based bottom-up methods or atmospheric measurement-based top-down methods (Chen and Prinn, 2006, Nisbet and Weiss, 2010, Alvarez *et al.*, 2018, Desjardins *et al.*, 2018, Vaughn *et al.*, 2018). Bottom-up fluxes typically multiply a quantitative activity factor (representative of the amount of an emitting activity taking place) by a qualitative emission factor (Saunois *et al.*, 2016, Allen *et al.*, 2022). These bottom-up emission factors may be more general values assigned for a geographical region (Scarpelli *et al.*, 2020, Bai

et al., 2023), developed from knowledge of source emissions (Wolf *et al.*, 2017, Lin *et al.*, 2021) or informed by process models (Scheutz *et al.*, 2009, Stavert *et al.*, 2021). Meanwhile, most top-down emission estimates rely on atmospheric methane measurements combined with wind data to infer emissions within an inversion model (Denmead *et al.*, 2000, Ars *et al.*, 2017, Cusworth *et al.*, 2021). Top-down facility-–scale methane emission flux ($Q_{methane}$) estimates are essential to complement, improve and verify corresponding bottom-up estimates (Guha *et al.*, 2020, Delre *et al.*, 2017, Hayek and Miller, 2021, Marklein *et al.*, 2021, Johnson *et al.*, 2023).

Various approaches can be employed to derive top-down $Q_{methane}$ (Johnson and Johnson, 1995, Bastviken *et al.*, 2022). Some methods use remote sensing sampling, where mole fraction measurements are integrated over a certain distance (Cusworth *et al.*, 2020, Hrad *et al.*, 2021, Maasakkers *et al.*, 2022, Cossel *et al.*, 2023). However, ~~here~~ we focus here on methods using *in situ* sampling, which provides methane mole fraction ($[CH_4]$) measurements at the sampling point (Feitz *et al.*, 2018). There are many ways to derive top-down $Q_{methane}$ estimates by applying an extensive variety of inversion dispersion methods to downwind *in situ* sampling (Flesch *et al.*, 1995, Sonderfeld *et al.*, 2017, Hrad *et al.*, 2021, Shaw *et al.*, 2021, Liu *et al.*, 2024). Rather than using measurements from a single location, downwind sampling transects can be used in more accurate flux methods. For example, both one-dimensional (Foster-Wittig *et al.*, 2015, Yacovitch *et al.*, 2015, Albertson *et al.*, 2016, Riddick *et al.*, 2020, Kumar *et al.*, 2021, Kumar *et al.*, 2022) and two-dimensional (Lee *et al.*, 2018, Shah *et al.*, 2019) downwind transects can be used within Gaussian plume modelling, while mass-balance box modelling can be applied to two-dimensional downwind sampling (Denmead *et al.*, 1998, Foulds *et al.*, 2022, Pühl *et al.*, 2024).

As well as simply using downwind $[CH_4]$ *in situ* sampling, top-down $Q_{methane}$ values can be derived using a tracer gas release, where the release of a carefully controlled quantity of a tracer gas is co-located with the methane emission source (Lamb *et al.*, 1995, Czepiel *et al.*, 1996). Tracer-based $Q_{methane}$ estimation relies on simultaneous *in situ* downwind measurements of both $[CH_4]$ and the tracer gas mole fraction, with no wind measurements required (Johnson and Johnson, 1995, Mønster *et al.*, 2014, Ars *et al.*, 2017). The ratio between the enhancement (above background levels) of the mole fractions of the two gases can be used to yield $Q_{methane}$ by direct multiplication with the known tracer release rate (Yacovitch *et al.*, 2017, Feitz *et al.*, 2018, Mønster *et al.*, 2019). A more accurate $Q_{methane}$ estimate can be derived by taking the ratio between integrated downwind methane and tracer gas plumes (Scheutz *et al.*, 2011, Mønster *et al.*, 2015, Yver Kwok *et al.*, 2015a), which is especially useful to minimise errors due to suboptimal acetylene release co-location with the methane emission source (Ars *et al.*, 2017). Although this manuscript focuses on methane as the target gas of interest, the same principles and outcomes apply to any other target gas whose emission flux is derived using a tracer gas release.

The well-established tracer-based flux method has widely been considered to be a more accurate top-down flux quantification approach for localised facility-–scale sources, against which to test other methods, although good execution of the method (*i.e.* suitable tracer release location and downwind sampling location) is essential for optimal flux~~$Q_{methane}$~~ estimation (Yver Kwok *et al.*, 2015a, Bell *et al.*, 2017, Mønster *et al.*, 2019, Song *et al.*, 2023). The accuracy of tracer-based fluxes has been confirmed

during various controlled release experiments using co-located target gas~~methane~~ and tracer point source releases (Mønster *et al.*, 2014, Feitz *et al.*, 2018, Liu *et al.*, 2024), but also with an offset tracer and target gas~~methane~~ source, which can result in greater flux uncertainty (Ars *et al.*, 2017, Fredenslund *et al.*, 2019). Raw tracer-based $Q_{methane}$ has been derived in countless previous studies from a multitude of facility-scale methane sources, for example from cattle (Johnson *et al.*, 1994, Daube *et al.*, 2019, Vechi *et al.*, 2022), oil and gas extraction infrastructure (Lamb *et al.*, 1995, Omara *et al.*, 2016, Yacovitch *et al.*, 2017), anaerobic digesters (Scheutz and Fredenslund, 2019), wastewater treatment facilities (Yver Kwok *et al.*, 2015a, Delre *et al.*, 2017, Delre *et al.*, 2018) and landfill sites (Czepiel *et al.*, 1996, Galle *et al.*, 2001, Mønster *et al.*, 2015, Matacchiera *et al.*, 2019, Mønster *et al.*, 2019).

The choice of tracer gas for methane has also evolved (Scheutz *et al.*, 2009, Delre *et al.*, 2018, Mønster *et al.*, 2019). Originally, sulphur hexafluoride was favoured (Johnson and Johnson, 1995, Czepiel *et al.*, 1996) due to its inert properties and almost absent atmospheric background. However, sulphur hexafluoride is an incredibly potent greenhouse gas with an atmospheric lifetime of roughly 1 000 years (Kovács *et al.*, 2017). Carbon dioxide has also been used as a tracer gas (Lamb *et al.*, 1995, Allen *et al.*, 2019), but it has extensive background variability due to a multitude of localised sources and sinks (Grimmond *et al.*, 2002, Schwandner *et al.*, 2017). Nitrous oxide is a more recent alternative tracer gas option to quantify methane emissions (Galle *et al.*, 2001, Mønster *et al.*, 2015, Omara *et al.*, 2016). Though this is a potent greenhouse gas, it has a~~n finite~~ atmospheric lifetime of approximately 110 years (Prather *et al.*, 2015) due to its reaction with atmospheric oxygen radicals and due to soil consumption (Cicerone, 1989, Kroeze, 1994, Tian *et al.*, 2020). Finally, acetylene has more recently been used as a tracer for methane (Yver Kwok *et al.*, 2015a, Fredenslund *et al.*, 2019, Scheutz and Fredenslund, 2019, Vechi *et al.*, 2022). It readily reacts with the hydroxyl radical, resulting in a relatively short lifetime of up to a month (Kanakidou *et al.*, 1988, Gupta *et al.*, 1998, Hopkins *et al.*, 2002, Crounse *et al.*, 2009). Acetylene is also cheap to produce. However, it has a flammable atmospheric range of between 2.5% and approximately 80% (Williams and Smith, 1969), which is the largest range of any readily available gas. Nevertheless, background levels of no greater than 1 ppb (Kanakidou *et al.*, 1988, Gupta *et al.*, 1998, Hopkins *et al.*, 2002, Xiao *et al.*, 2007), makes it a preferred option compared to nitrous oxide, which can otherwise be emitted from many sources including agricultural activities, resulting in a variable atmospheric nitrous oxide background (Tian *et al.*, 2020).

The ability to obtain *in situ* measurements of both methane and the chosen tracer gas underpins the accuracy of any derived tracer-based flux. Acetylene mole fraction ($[C_2H_2]$) has traditionally been measured using flame-ionisation gas chromatography (Kanakidou *et al.*, 1988, Hopkins *et al.*, 2002, Crounse *et al.*, 2009) and Fourier-transform infrared (IR) spectroscopy (Xiao *et al.*, 2007, Feitz *et al.*, 2018), which are both slow *in situ* techniques. The recent use of acetylene as methane tracer has largely been facilitated by the development of fast-response (less than 1-minute sampling frequency) *in situ* measurement techniques. Yacovitch *et al.* (2017) derived tracer-based fluxes with a sensor using direct IR spectroscopy with a tuneable laser, manufactured by Aerodyne Research, Inc. (Billerica, Massachusetts, USA), with a detection limit of 78 ppt and a $[C_2H_2]$ linear calibration uncertainty of 3% (assuming a zero intercept). This calibration was performed by diluting

gas from an acetylene cylinder, although the [C_2H_2] testing range is not provided (Yacovitch *et al.*, 2017). The Ultraportable Methane-Acetylene Analyzer (ABB Ltd, Zürich, Switzerland) has also been used to measure [C_2H_2], which uses off-axis integrated cavity output spectroscopy, with a manufacturer-rated precision of less than 1 ppb at 0.2 Hz (Fredenslund *et al.*, 2019). Feitz *et al.* (2018) tested this instrument to verify its~~for~~ linearity using two cylinders with a [C_2H_2] of~~containing~~ 4 ~~-~~100 ppb ~~[C₂H₂]~~ and 20 ~~-~~600 pp~~b~~m ~~[C₂H₂]~~, although without providing correlation results.

The Picarro G2203 (Picarro, Inc., Santa Clara, California, USA) is one of the most widely used acetylene gas analysers, which has been operated in numerous tracer release studies (Mønster *et al.*, 2015, Yver Kwok *et al.*, 2015a, Ars *et al.*, 2017, Delre *et al.*, 2017, Delre *et al.*, 2018, Vechi *et al.*, 2022). It uses cavity ring-down spectroscopy (CRDS) to detect small [C_2H_2] enhancements of less than 1 ppb (Mønster *et al.*, 2014). The Picarro G2203 has a manufacturer-rated precision of less than ±0.6 ppb at 0.5 Hz (Picarro, Inc., 2015). Mønster *et al.* (2014) provided a brief testing overview of the Picarro G1203 (which is spectroscopically similar to the Picarro G2203, but with older electronics) using a testing cylinder ~~containing~~with a [C_2H_2] of 103 ppb ~~[C₂H₂]~~ in synthetic air, with a 10% [C_2H_2] accurac~~uncertaint~~y. However, they provided limited details on their characterisation testing procedure, such as whether the gas was diluted to sample lower [C_2H_2] levels and the number of sampling steps, if any (Mønster *et al.*, 2014). In a tracer release study by Omara *et al.* (2016), regular Picarro G2203 calibrations were conducted using a single ~~100 ppb [C₂H₂]~~ gas standard with a [C_2H_2] of 100 ppb to check for drift. They measured a raw acetylene mole fraction ([C_2H_2]$_r$) of (112±3.~~2~~) ppb (Omara *et al.*, 2016); this +12% error emphasises the risk in using raw measurements from tracer gas analysers.

To summarise, there exists a large body of research having used tracer-based methods to estimate $Q_{methane}$, but a lack of emphasis in calibrating the tracer gas measurement in these previous studies. It is vitally important to conduct independent rigorous testing of gas analysers such as the Picarro G2203, across the full [C_2H_2] range expected during field sampling. This is essential due to the reliance of tracer-based $Q_{methane}$ estimates to inform site operators and policy makers. Any disparity in [C_2H_2] measurements may be projected as persistent biases in $Q_{methane}$ estimates, emphasising the key importance of this work.

We provide here the first detailed characterisation, to our knowledge, of the Picarro G2203 gas analyser for measuring [C_2H_2] in **Sect. 2**, including the influence of water. We describe the implementation of the gas analyser to conduct an acetylene release from a landfill site in France in **Sect. 3**. We also present a comprehensive description of the equipment used within our acetylene release method in **Sect. 3**. The purpose of this study is not to evaluate emissions from this specific landfill site in the context of methane emissions compared to other sources, but rather to focus on the tracer-based flux quantification method itself. In this study, the chosen landfill site serves only as a complex heterogeneous test site with which to test our methods and the specificities of this particular site are beyond the scope of this work. $Q_{methane}$~~Flux~~ results from this study site are presented in **Sect. 4**, where we discuss the variability in $Q_{methane}$ results and disparity between $Q_{methane}$ values derived using raw versus calibrated mole fraction measurements. We summarise the implications on $Q_{methane}$ quantification of using raw mole fraction measurements without applying an acetylene calibration in **Sect. 5**.

2 Instrument acetylene response characterisation

2.1 Testing equipment

The Picarro G2203 gas analyser uses CRDS to measure $[C_2H_2]_r$, raw water mole fraction ($[H_2O]_r$) and raw methane mole fraction ($[CH_4]_r$). This section is dedicated to characterising Picarro G2203 $[C_2H_2]_r$, measurements, with a Picarro G2203 $[CH_4]_r$ measurement calibration provided in **Sect. S1** in the **Supplement**. A Picarro G2401 (Picarro, Inc.) gas analyser was ~~also~~ used during this Picarro G2203 characterisation work, which also measures $[H_2O]_r$ and $[CH_4]_r$, but not $[C_2H_2]_r$. The CRDS method used by the Picarro G2230 and Picarro G2401 gas analysers derives mole fraction measurements using a spectrum of the characteristic exponential decay "ring-down" time of IR radiation leaking out of a cavity (Paldus and Kachanov, 2005) held under controlled pressure and temperature (Crosson, 2008). IR radiation from a tuneable distributing feedback laser is injected into the cavity at discrete points across a narrow wavelength range, which is tuned to the absorption peak of interest (Crosson, 2008). IR absorption occurs in the cavity following the Beer-Lambert Law at absorbing wavelengths (Lambert, 1760). Following laser build-up, the laser is switched off and radiation leaks out of the cavity (Paldus and Kachanov, 2005). The ring-down times of leaking radiation are used to produce an absorbance spectrum as a function of wavelength. The ratio between the maximum absorbance signal and the signal at a baseline wavelength (representative of sampling in an empty cavity) is used to derive gas mole fraction using internal instrumental algorithms.

Throughout each laboratory test conducted during this work, the Picarro G2203 and Picarro G2401 were connected in parallel. Both the Picarro G2203 and Picarro G2401 record raw mole fraction measurements for each gas individually, each with a unique timestamp. Therefore, all Picarro G2401 measurements were shifted to the Picarro G2203 timestamp, by applying a lag time correction. ~~At the time of testing, Picarro G2203 $[C_2H_2]_r$ measurements had an average observed sampling frequency of (0.3±0.1) Hz in dry conditions.~~ The observed time interval between each $[C_2H_2]_r$ measurement for the Picarro G2203 used in this particular study followed a roughly 40 s periodic cycle every ten measurements of roughly 2 s, 4 s, 2 s, 4 s, 2 s, 4 s, 2 s, 4 s, 2 s and 13 s between measurements. This sampling cycle is automatically determined by the gas analyser and may be due to different IR wavelength ranges being scanned at each step (a larger scan takes more time, but is useful for a better IR absorbance baseline fit), alongside $[CH_4]_r$ and $[H_2O]_r$ samples also being made, with a different laser used to sample water and methane independently of acetylene. Therefore, at the time of testing, Picarro G2203 $[C_2H_2]_r$ measurements had an overall observed sampling frequency of 0.24 Hz in dry conditions (when averaging over the discontinuous sampling rate). All $[C_2H_2]_r$ and $[CH_4]_r$ measurements presented in this manuscript are ~~defined as wet~~raw measurements, with no applied internal instrumental water correction ~~applied to this data~~. This means to say that they represent mole fractions of gases compared to all air molecules, including those of water when present.

During characterisation testing, a specially prepared 20 dm^3 acetylene calibration cylinder was used (Air Products N.V., Diegem, Belgium). This was volumetrically filled with a declared~~n~~ $[C_2H_2]$ of 10 180 ppb in argon with a ±3% uncertainty, according to the cylinder provider. This high $[C_2H_2]$ level was chosen to allow for high levels of dilution, to minimise the

effect of the argon in this cylinder on the natural balance of air; changes in air composition can affect spectral fitting by changing the shape of IR absorption peaks (Lim *et al.*, 2007, Rella *et al.*, 2013). A 20 dm^3 methane calibration cylinder (Air Products N.V.) was also used during testing. This was gravimetrically filled with a declared [CH$_4$] of 995.4 ppm in argon with a ±0.5% uncertainty, according to the cylinder provider. Unfortunately, it was not possible to further verify the declared [CH$_4$] level in the methane calibration cylinder using a reference instrument, due to its high argon content. Dilution of these two calibration cylinders was performed using gas from three cylinders containing natural ambient compressed outside air, assumed to contain a background acetylene mole fraction ([C$_2$H$_2$]$_0$) level of 0 ppb (due to the absence of nearby acetylene sources).

All tests were conducted using mass-flow controller (MFC) units (EL-FLOW Select, Bronkhorst High-Tech B. V., AK Ruurlo, Netherlands), which were used to generate gas blends and to control gas flow. All laboratory testing was conducted using either stainless-steel (SS) tubing or Synflex 1300 tubing (Eaton Corporation plc, Dublin, Ireland) with an outer diameter (OD) of 0.25 inches, in conjunction with standard SS Swagelok fittings (Swagelok Company, Solon, Ohio, USA) which were used to connect tubing and various components. The influence of Synflex 1300 tubing on [C$_2$H$_2$] is evaluated in **Sect. S2** of the **Supplement**, which shows no a measurable effect on [C$_2$H$_2$]$_r$, allowing for its use during laboratory testing. The gGas stream was filtered using 2 μm particle filters (SS-4FW-2, Swagelok Company) to protect downstream instrumentation. One of either two diaphragm pumps was used during testing to pressurise the gas stream: the N86KN.18 (KNF DAC GmbH, Hamburg, Germany) has fittings compatible with Swagelok fittings whereas the 1410VD/12VDC (Gardner Denver Thomas GmbH, Fürstenfeldbruck, Germany) has barbed fittings which were connected to short lengths of Tygon S3 E-3603 tubing (Saint-Gobain Performance Plastics, Inc., Solon, Ohio, USA) to which Swagelok fittings were attached. A needle valve (SS-4MG, Swagelok Company) was used to stabilise and restrict the pressure downstream of the diaphragm pumps. A check valve (SS-4C-1, Swagelok Company) was also used to direct gas flow during testing.

As water vapour is naturally present in air, the [C$_2$H$_2$]$_r$ response of the Picarro G2203 was tested under various water mole fraction ([H$_2$O]) levels which could be controlled using three different methods. Water could be added to the gas stream using a dew-point generator (LI-610, LI-COR, Inc., Lincoln, Nebraska, USA) to saturate passing gas to a fixed dew-point setting. This was incorporated into the gas stream by connecting standard plastic Swagelok fittings to the standard Bev-A-Line IV tubing (Thermoplastic Processes Inc, Georgetown, Delaware, USA) used by the dew-point generator, which has an OD of 0.25 inches and an inner diameter of 0.125 inches. The internal pump of the dew-point generator was by-passed by cutting and adding a standard plastic Swagelok fitting to the Bev-A-Line IV tubing on the instrument labelled as "to condenser". A three-way ball valve (B-42XS4, Swagelok Company) was placed both upstream and downstream of the dew-point generator; these were used to direct the instrument away from the gas line and towards a direct vent to the atmosphere (*i.e.* with no connection) when adding water to the condenser, to ensure an atmospheric pressure both upstream and downstream of the dew-point generator. Conversely water could be removed from the gas stream using a Nafion-based gas dryer (MD-070-144S-4, Perma Pure LLC, Lakewood, New Jersey, USA), which contains a Nafion membrane (The Chemours Company FC, LLC,

Wilmington, Delaware, USA), which reduced observed Picarro G2203 [H$_2$O]$_r$ measurements to less than 0.1%. The Nafion-
225 based gas dryer was connected in reflux mode during testing, whereby the gas dryer was placed between the Picarro G2203
and its downstream vacuum pump, to create a vacuum outside the Nafion membrane through which the sample gas passed, as
described in detail by Welp *et al.* (2013). Water could be dried further through chemical absorption, by passing the gas stream
through~~using~~ magnesium perchlorate grains (ThermoFisher (Kandel) GmbH, Kandel, Germany) in a water scrubber. The effect
of any potential artefacts of the Nafion-based gas dryer, the magnesium perchlorate scrubber and the dew-point generator is
230 present~~was test~~ed in **Sect. S3~~2~~** in the **Supplement**, ~~which~~ show~~ing~~ed no significant effect on [C$_2$H$_2$]$_r$ response. It was especially
important to verify this for the dew-point generator which bubbles gas through a water reservoir, as acetylene has a solubility
in water of 1.1 g dm^{-3} at 20° C (Priestley and Schwarz, 1940).

2.2. Water tests

Water can potentially affect IR mole fraction measurements of any gas due to three key reasons, as described by Rella *et al.*
235 (2013). Two of these reasons are specifically due to IR spectroscopy, although the ~~magnitude and~~ importance of each of these
effects depends on the specific measured gas in question. Firstly, spectral interference can occur where a water IR absorption
line overlaps with a target gas absorption line (this can affect baseline fitting in the CRDS method). Secondly, an independent
peak broadening effect occurs whereby the shape of the absorption peak for the target gas of interest can change due to
interactions with water in the gas mixture, which effect the dipole of the target gas in question, therefore causing a change in
240 the peak shape. Although any gas can affect the peak shape and cause spectral overlap, the natural balance of air is usually a
constant blend of nitrogen, oxygen and argon resulting in a constant effect on the methane spectrum, with water the main
variable in ambient air. It is therefore conventional to characterise IR peak shape in the absence of water. Finally, a natural
dilution effect occurs (which is not exclusive to IR spectroscopy) where the fraction of target gas molecules that would
otherwise be present in dry gas is reduced due to the additional presence of water in the overall gas mixture. It is therefore a
245 standard procedure to convert all gas mole fraction measurements into dry mole fractions as a first step, to which water can
then be subsequently reintroduced at a later stage, if required in flux analysis.

An evaluation of the influence of specific spectral effects of water on [C$_2$H$_2$]$_r$ measurements is beyond the scope of this study.
In this work, the net influence of [H$_2$O] on [C$_2$H$_2$]$_r$ measurements is instead characterised empirically. Preliminary testing was
conducted by sampling five different targeted acetylene mole fraction ([C$_2$H$_2$]$_t$) levels (6 ppb, 12 ppb, 20 ppb, 30 ppb and
250 40 ppb) by directly blending gas from the acetylene calibration cylinder with gas from a natural ambient compressed air
cylinder. This is illustrated schematically in **Fig. 1** for this test, where the check valve was used to avoid back-flow into the
dew-point generator when sampling pure dry gas, therefore minimising the mixing of residual wet air with the dry gas stream.
Nine different [H$_2$O] levels were sampled at each [C$_2$H$_2$]$_t$ setting. This was achieved by humidifying a portion of gas using the
dew-point generator with a 20° C setting and then blending this with dry air from the same original gas stream, passing though

255 the magnesium perchlorate scrubber, to ensure dryness. First, dry air was sampled for 60 minutes before sampling each wet setting for 15 minutes. The results of this test are presented in **Fig. 2**.

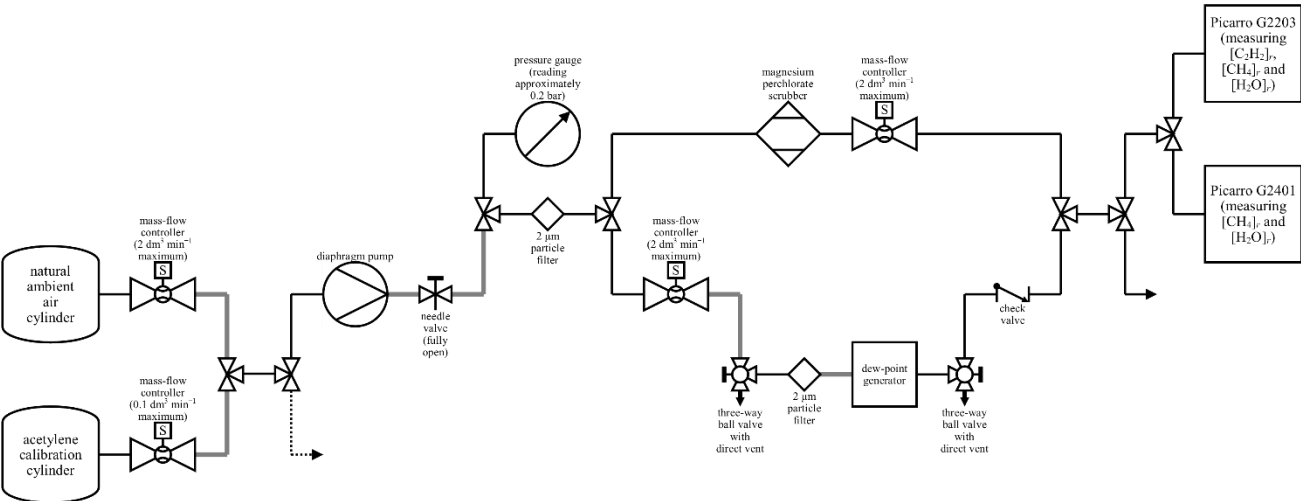



Figure 1: A schematic of the set-up during water testing. An arrow represents a vent to the atmosphere. Solid black lines represent either SS tubing or Synflex 1300 tubing with an OD of 0.25 inches. Solid grey lines represent SS connections between two components
260 **of approximately 0.04 m. The black dashed line represents SS tubing with an OD of 0.125 inches. All connections used standard SS Swagelok fittings. Maximum MFC flow rates are representative of corresponding volumetric flow rates for dry air at 101 325 Pa and 273.15 K. The three-way ball valves were directed towards the gas stream during testing and away from the direct vent to the atmosphere.**

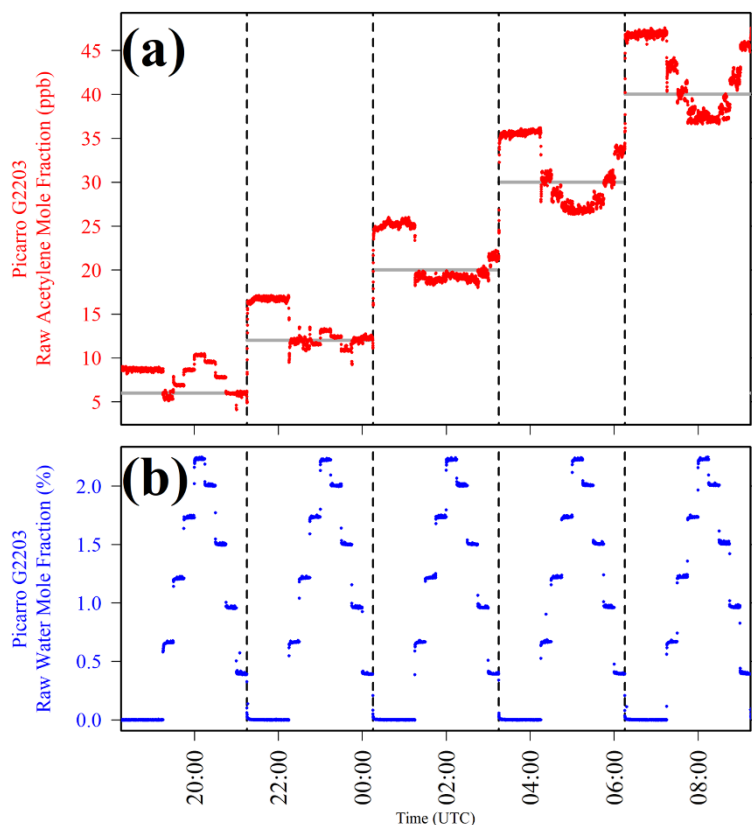



Figure 2: (a) Picarro G2203 $[C_2H_2]_r$ plotted as red dots and (b) Picarro G2203 $[H_2O]_r$ plotted as blue dots, when sampling nine different $[H_2O]$ levels at five different $[C_2H_2]_t$ settings, with the change between each different $[C_2H_2]_t$ setting indicated by dashed vertical lines. $[C_2H_2]_t$ calculated from MFC settings is plotted in (a) as light grey lines.

Figure 2 shows that at each fixed $[C_2H_2]_t$ level (the periods between vertical dashed lines), $[C_2H_2]_r$ as measured by the Picarro G2203 ~~(red dots in **Fig. 2** (a))~~ changed in response to $[H_2O]$. However, $[C_2H_2]_t$ (light grey lines in **Fig. 2** (a)) is consistently lower than $[C_2H_2]_r$ (red dots in **Fig. 2** (a)) when sampling in dry conditions (see blue dots in **Fig. 2** (b)). This is either because $[C_2H_2]_t$ is not calibrated, because of MFC offsets during gas blending or a combination of both effects. In any case, this means that this analysis must be treated as an empirical test to evaluate the effect of Picarro G2203 $[H_2O]_r$ measurements on $[C_2H_2]_r$ measurements. The relationship between $[C_2H_2]_t$ and $[C_2H_2]$ is discussed in the subsequent subsections.

Figure 2 shows that the nature of the $[C_2H_2]_r$ response as a function of increasing $[H_2O]_r$ (blue dots in **Fig. 2** (b)) was not consistent at the different tested $[C_2H_2]_t$ levels. ~~(light grey lines in **Fig. 2** (a))~~ At a~~6 ppb~~ $[C_2H_2]_t$ of 6 ppb, $[C_2H_2]_r$ appeared to increase with increasing $[H_2O]_r$. Yet at a $[C_2H_2]_t$ of 12 ppb ~~$[C_2H_2]_t$~~and 20 ppb ~~$[C_2H_2]_t$~~ there was no clear $[H_2O]_r$ relationship with $[C_2H_2]_r$. At a $[C_2H_2]_t$ of 30 ppb and 40 ppb ~~$[C_2H_2]_t$~~, $[C_2H_2]_r$ appeared to decrease with $[H_2O]_r$. While use of a dew-point generator may potentially explain this behaviour (due to solubility of acetylene in the water reservoir (Priestley and Schwarz, 1940)), testing presented in **Sect. S3**~~2~~ in the **Supplement** shows no such effect, suggesting~~making it clear~~ that the~~se~~ effects presented in **Fig. 2** are due to the gas analyser itself. In addition, $[C_2H_2]_r$ measurements were excessively noisy in the presence

of water compared to dry sampling conditions, particularly at higher $[C_2H_2]_t$ levels. The specific cause of these water effects on $[C_2H_2]_r$ (in the context of spectral effects) is beyond the scope of this empirical study. Nevertheless, ~~this result allows us to conclude the~~eat noisy $[C_2H_2]_r$ measurements at high $[H_2O]_r$, combined with the inconsistent directions of $[C_2H_2]_r$ changes in response to $[H_2O]_r$ changes. suggest~~s~~ that it is not straightforward to derive a reliable simple empirical water correction model across a $[H_2O]$ range typically observed in ambient atmospheric conditions.

Figure 2 shows that $[C_2H_2]_r$ response was most stable (least noisy) at lower $[H_2O]$ levels. Therefore $[C_2H_2]_r$ response to $[H_2O]_r$ was instead tested in dryer conditions. This simulates a $[H_2O]$ range experienced with sole use of the Nafion-based gas dryer, which reduces $[H_2O]_r$ measurements to less than 0.1%. Such a correction could be useful if using the Nafion-based drier to obtain semi-dry gas sampling during eventual field deployment. In this test, the dew-point generator was fixed to a $0°$ C setting to enable a lower range of $[H_2O]$ levels to be sampled. The same procedure as for the previous test was carried out, but in this test, the entire procedure was performed twice to test for repeatability. The results of this test are presented in **Fig. 3**.

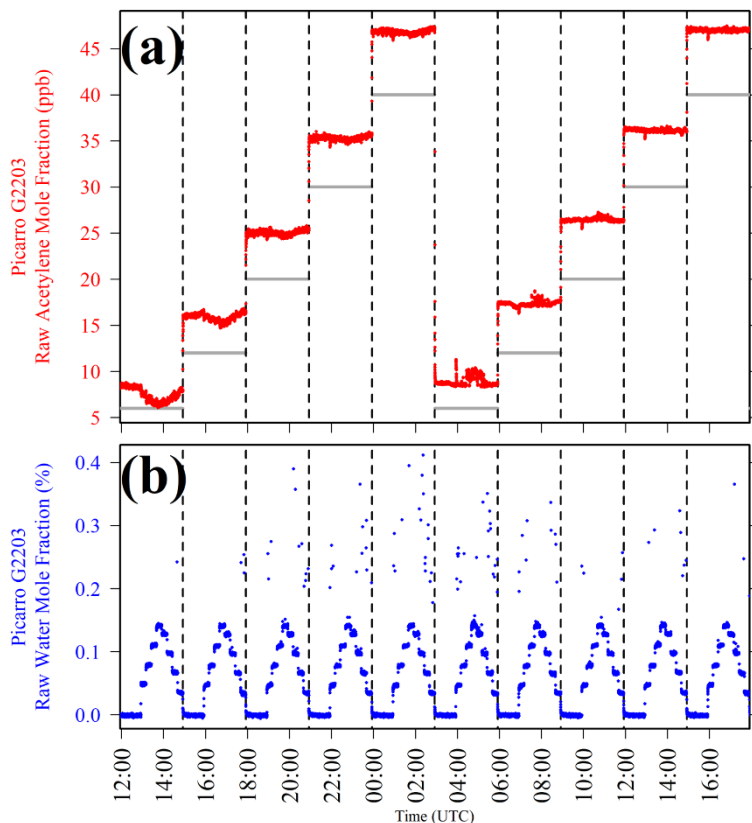



Figure 3: (a) Picarro G2203 $[C_2H_2]_r$ plotted as red dots and (b) Picarro G2203 $[H_2O]_r$ plotted as blue dots, when sampling nine different low $[H_2O]$ levels at five different $[C_2H_2]_t$ settings over two testing cycles, with the change between each different $[C_2H_2]_t$ setting indicated by dashed vertical lines. $[C_2H_2]_t$ calculated from MFC settings is plotted in (a) as light grey lines.

Figure 3 shows that despite limiting [H$_2$O]$_r$ measurements to mostly below 0.2% (blue dots in **Fig. 3** (b)), [C$_2$H$_2$]$_r$ remained unpredictable at each fixed [C$_2$H$_2$]$_t$ setting, (although [C$_2$H$_2$]$_r$ appeared relatively stable at the highest [C$_2$H$_2$]$_t$ levels in this water test). It is particularly concerning that [C$_2$H$_2$]$_r$ first decreased with increasing [H$_2$O]$_r$ at 6 ppb% [C$_2$H$_2$]$_t$ while the opposite behaviour was observed during the second period at the same [C$_2$H$_2$]$_t$ level. At the other [C$_2$H$_2$]$_t$ settings, the relationship

300   between [C$_2$H$_2$]$_r$ and [H$_2$O]$_r$ was less obvious. Nevertheless, it is clear that there is some impact on [C$_2$H$_2$]$_r$ due to the presence of water. This test also shows that [H$_2$O]$_r$ occasionally spiked, which can be seen in **Fig. 3** (b); yet Picarro G2401 [H$_2$O]$_r$ measurements were used to confirm that~~when~~ there w~~ere~~as no corresponding [H$_2$O] spike~~, which was confirmed by Picarro G2401 [H$_2$O]$_r$ measurement~~s (see **Sect. S4**~~3~~ in the **Supplement**). This means that in reality, these [H$_2$O]$_r$ outliers were an artefact of the instrumental Picarro G2203 response. This is probably due to issues in spectral water fitting at low (but non-

305   zero) [H$_2$O]$_r$ levels. It can therefore be concluded that a reliable and repeatable [H$_2$O]$_r$ correction is difficult to apply to [C$_2$H$_2$]$_r$ as the relationship is too unpredictable, even if limiting [H$_2$O]$_r$ to below 0.1% with a Nafion-based gas dryer during field deployment. Therefore, optimum Picarro G2203 field sampling requires fully dry conditions. This avoids the complications associated with having to devise a reliable [H$_2$O]$_r$ correction and also, with having to identify and remove spurious [H$_2$O]$_r$ spikes. It follows that [C$_2$H$_2$]$_r$ response should be calibrated in fully dry conditions.

310   **2.3 Calibration gas blending characterisation**

In order to calibrate dry Picarro G2203 [C$_2$H$_2$]$_r$ measurement response, precise reference [C$_2$H$_2$] testing gas mixtures are required. As we had no access to acetylene gas standards for~~with which to~~ calibrat~~i~~on~~e [C$_2$H$_2$]$_r$ response~~, gas from the acetylene calibration cylinder could instead be carefully diluted using precise MFC blends. However, preliminary testing revealed MFC flow rates to be unreliable and offset from their predicted settings, which may be due to MFC contamination (due to particles,

315   debris or oils, for example, getting trapped inside the instrument) or general ageing over time. This was especially concerning at low flow rate settings, compared to the maximum range of each MFC.

To characterise any disparity between the actual [C$_2$H$_2$] level in the gas mixture and [C$_2$H$_2$]$_t$ (according to MFC settings), an empirical mass-flow controller correction factor (C_{MFC}) was derived, with each C_{MFC} value corresponding to a specific set of MFC settings. This factor can be directly applied to the enhancement in [C$_2$H$_2$]$_t$ above the [C$_2$H$_2$]$_0$ level in the dilution gas

320   where

$$[C_2H_2] = \left(C_{\text{MFC}} \cdot \left([C_2H_2]_t - [C_2H_2]_0 \right) \right) + [C_2H_2]_0, \tag{1}$$

to yield reference [C$_2$H$_2$] levels. C_{MFC} values can be derived as a function of each set of MFC settings by comparing targeted and measured mole fraction levels of a different proxy gas, when blended with a dilution gas using the same MFC settings. Methane was used as a proxy gas for this purpose following

325   $$C_{\text{MFC}} = \frac{[CH_4] - [CH_4]_0}{[CH_4]_t - [CH_4]_0}, \tag{2}$$

which uses the enhancement in targeted methane mole fraction ($[CH_4]_t$) above the background methane mole fraction ($[CH_4]_0$) level in the dilution gas. Accurate $[CH_4]$ measurements could be obtained ~~here~~ by calibrating Picarro G2401 $[CH_4]_r$ measurements using six certified gas standards traceable to the World Meteorological Organisation (WMO) greenhouse gas scale for methane (WMO X2004A) of between 1.6 ppm and 3.3 ppm $[CH_4]$. This yielded a gain factor of 1.0073 and an offset of −0.002647 ppm with a calibration root-mean squared error (RMSE) of ±0.000079 ppm, for the Picarro G2401 used in this work. This method makes the effect of any specific MFC errors in $[C_2H_2]_t$ and $[CH_4]_t$ estimation redundant, as they cancel out when correcting $[C_2H_2]_t$ using Eq. **(1)** in conjunction with Eq. **(2)**.

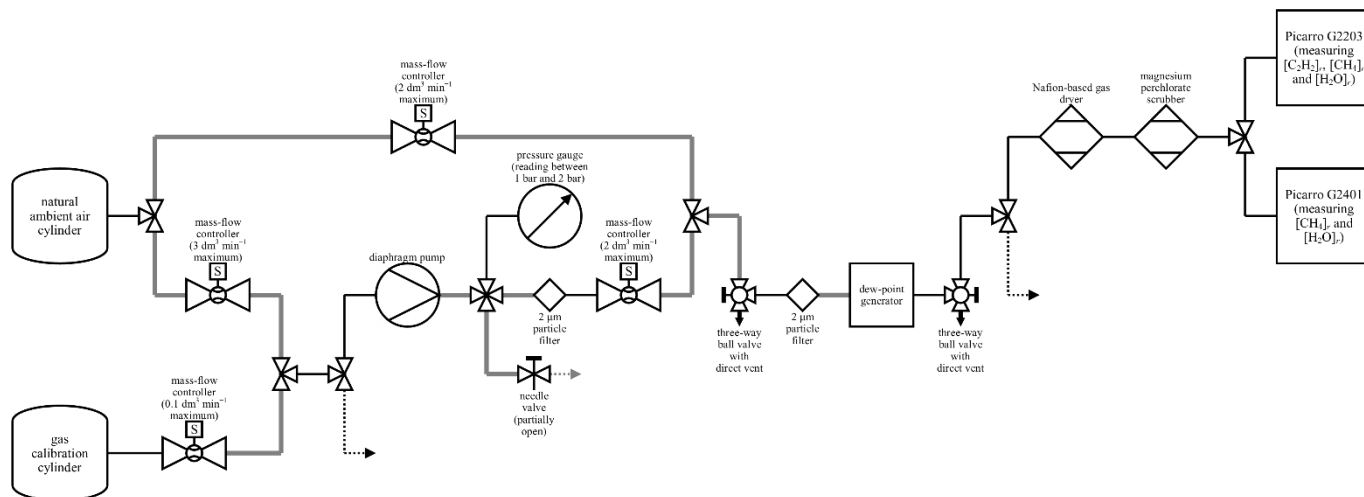
To derive C_{MFC}, the methane calibration cylinder was used as it is gravimetrically filled with a fixed $[CH_4]$ level declared by the cylinder provider, although a ±0.5% $[CH_4]$ uncertainty induces uncertainty in $[CH_4]_t$ calculation and hence, C_{MFC} calculation, the effects of which are evaluated in in **Sect. S5** of the **Supplement**. ~~G~~gas from the methane calibration cylinder was blended with gas from a natural ambient compressed air cylinder, with a $[CH_4]_0$ of 2.057 ppm. Twenty different $[CH_4]_t$ levels were targeted between $[CH_4]_0$ and 11.82 ppm. First, $[CH_4]_0$ (*i.e.* pure natural ambient compressed air) was sampled for 60 minutes before sampling each other $[CH_4]_t$ setting for 15 minutes. This cycle was repeated three times before finally sampling $[CH_4]_0$ for 60 minutes. As the methane calibration cylinder has a high (995.4 ppm) $[CH_4]$ content, the total quantity of gas from this cylinder reaching the gas analysers was less than 1% (*i.e.* representing a small argon enhancement and thus, causing minimal influence on spectral shape). Low $[CH_4]_t$ levels were obtained through a system of double dilution, as illustrated schematically in **Fig. 4**. First, gas from the methane calibration cylinder was diluted with natural ambient compressed air. This was then subsampled and blended with compressed air a second time.

345 **Figure 4: A schematic of the set-up during acetylene calibration and MFC blending characterisation. An arrow represents a vent to the atmosphere. Solid black lines represent either SS tubing or Synflex 1300 tubing with an OD of 0.25 inches. Solid grey lines represent SS connections between two components of approximately 0.04 m. The black dashed line represents SS tubing with an ~~OD~~outer diameter of 0.125 inches. The grey dashed line represents SS tubing with an OD of 0.0625 inches. All connections used standard SS Swagelok fittings. Maximum MFC flow rates are representative of corresponding volumetric flow rates for dry air at**
350 **101 325 Pa and 273.15 K. The gas calibration cylinder ~~was~~represents the methane calibration cylinder during MFC blending characterisation and the acetylene calibration cylinder during acetylene calibration. The three-way ball valves were directed towards the gas stream during testing and away from the direct vent to the atmosphere.**

Figure 5 shows Picarro G2401 results for ~~the~~ methane MFC blending characterisation ~~test for the Picarro G2401~~, where all $[CH_4]_r$ measurements have been converted into $[CH_4]$, using the WMO standard calibration coefficients given above. To derive

355 C_{MFC} values from this data, a 5-minute average Picarro G2401 $[CH_4]$ value was taken from towards the end of each 15-minute sampling step (except when sampling $[CH_4]_0$). This averaging period was used to enable the Picarro G2401 to stabilise and to flush all gas tubing. As the cycle was repeated thrice, each $[CH_4]_t$ level has three corresponding 15-minute $[CH_4]$ averages, of which the average was used within Eq. **(2)** to derive C_{MFC} values, which are plotted in **Fig. 5** (c) as a function of ~~corresponding~~ $[C_2H_2]_t$ values corresponding to~~derived using~~ the same MFC settings (see next subsection for details). The standard deviation

360 of each average (*i.e.* the standard deviation between each of three 5-minute $[CH_4]$ averages at each $[C_2H_2]_t$ level greater than $[CH_4]_0$) was on average ($\pm 0.002 \pm 0.001$) ppm. This small variability demonstrates the reliability in MFCs to consistently provide the same gas blends on multiple occasions over time, with a relatively large gap of 5.75 hours between each of the three sampling cycles. In summary **Fig. 5** (c) C_{MFC} values show that the influence of a $[C_2H_2]$ enhancement above $[C_2H_2]_0$ can be over 200% larger than a corresponding $[C_2H_2]_t$ enhancement (above $[C_2H_2]_0$), emphasising the importance of this MFC

365 blending characterisation approach, as opposed to erroneously assuming $[C_2H_2]$ to simply equal $[C_2H_2]_t$ in the subsequent acetylene calibration analysis.

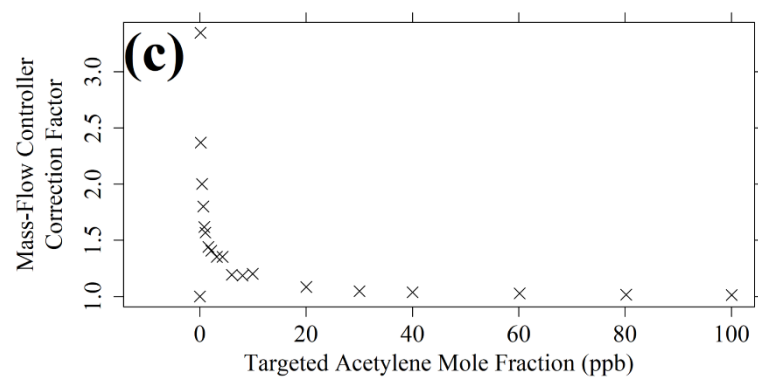
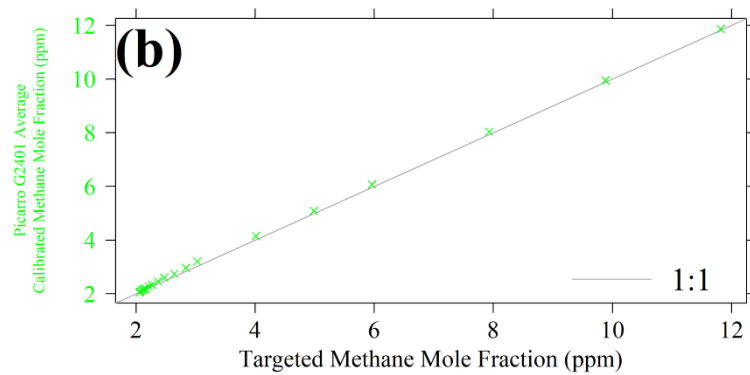
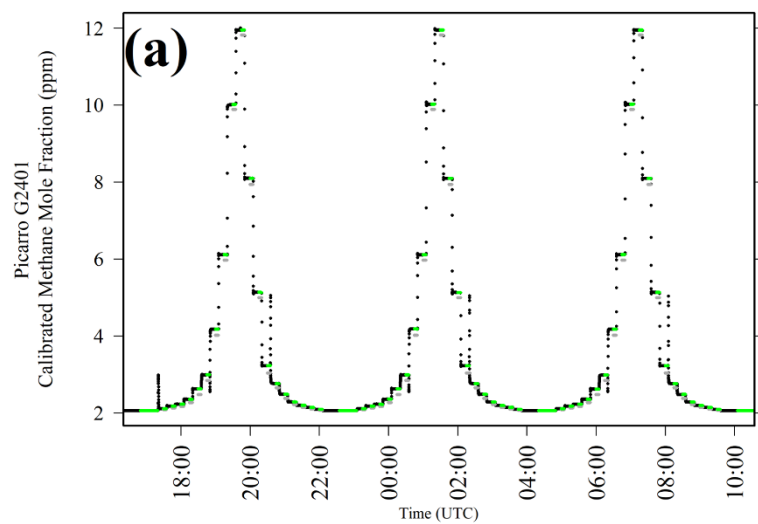
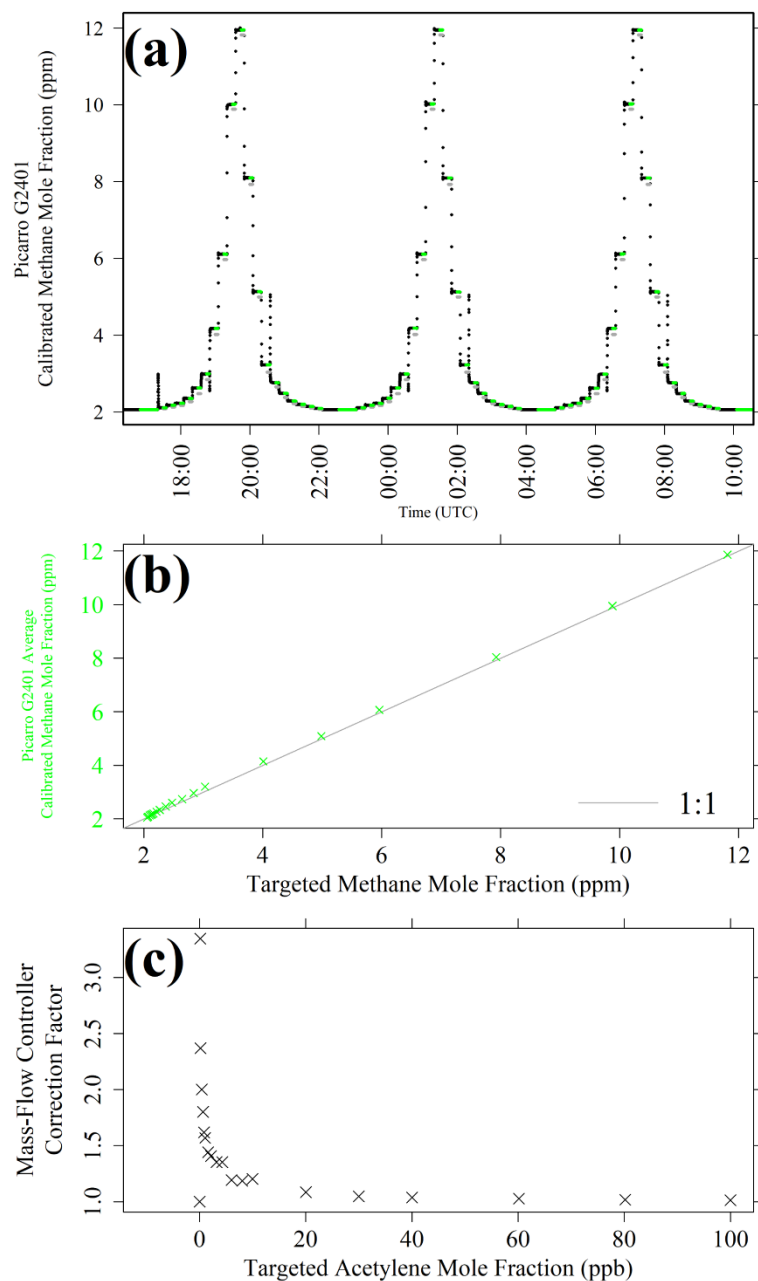



Figure 5: (a) Picarro G2401 [CH4] plotted as black dots, (b) corresponding [CH4] 5-minute averages plotted as green crosses against calculated [CH4]$_t$ ~~calculated from MFC settings~~ and (c) C_{MFC} as a function of corresponding calculated [C2H2]$_t$ levels, derived from three testing cycles by blending gas from the methane calibration cylinder with natural ambient compressed air. Periods used to derive averages are highlighted as green dots and corresponding calculated [C2H2]$_t$ levels are shown in the background as light grey dots in (a). An identity line is shown as a solid light grey line in (b).

2.4. Acetylene calibration

Following theHaving characterisationed of MFC gas blending capability at specific MFC flow rate settings, calculated $[C_2H_2]_t$ values can be converted into corresponding $[C_2H_2]$ levels using Eq. **(1)**. This provides corrected $[C_2H_2]$ gas blend standards with which to calibrate Picarro G2203 $[C_2H_2]_r$ measurements. The acetylene calibration cylinder was used here for dilution, however, as for the methane calibration cylinder, the $\pm3\%$ volumetric uncertainty in the declared $[C_2H_2]$ level induces uncertainty in $[C_2H_2]_t$ calculation, the influence of which is evaluated in **Sect. S5** of the **Supplement**. Gas from the acetylene calibration cylinder was blended with gas from the same natural ambient compressed air cylinder used during MFC blending characterisation, containing 0 ppb $[C_2H_2]_0$. The same process of double dilution was used, as illustrated schematically in **Fig. 4**, with absolutely no changes made to any of the flow connections (except for swapping the methane calibration cylinder with the acetylene calibration cylinder) and with no MFC power loss. Both the MFC blending characterisation test and acetylene calibration test were conducted within a 48-hour window, to minimise drift in MFC performance. Identical flow rate settings to those used during MFC blending characterisation resulted in the sampling of twenty different $[C_2H_2]$ levels being sampled between 0 ppb and 101.3 ppb (*i.e.* where each $[C_2H_2]_t$ level is corrected here by its corresponding C_{MFC} value given in **Fig. 5** (c)). First, an $[C_2H_2]$ of 0 ppb [C₂H₂]was sampled for 60 minutes before sampling each other $[C_2H_2]$ levelsetting for 15 minutes. Both the MFC blending characterisation test and acetylene calibration test were conducted within a 48-hour window, to minimise drift in MFC performance, and with no MFC power loss. This $[C_2H_2]$ range is deemed to be sufficient to capture most $[C_2H_2]$ measurements typically expected to be measured downwind of a controlled acetylene release, although a larger calibration range may be required if sampling nearer to the source, where higher $[C_2H_2]$ sampling may be expected.

Ordinarily, gas from compressed cylinders is already dry, so no dying is required. However, during this test (as well as during the blending characterisation describedtest above), all gas passed through the dew-point generator with a $8°$ C setting, to humidify the gas stream. The gas then passed though the Nafion-based gas dryer to significantly reduce $[H_2O]$ before finally passing through the magnesium perchlorate scrubber, to ensure dryness. This counterintuitive procedure of humidification followed by drying was used to best replicate sampling in the field when using both the Nafion-based gas dryer as well as the magnesium perchlorate scrubber, to account for potential artefacts on $[C_2H_2]$ at the point of measurement. Although a dew-point generator is not present during field sampling, **Sect. S32** in the **Supplement** shows that this has no noticeable effect on $[C_2H_2]_r$ measurements, alongside the Nafion-based gas dryer and the magnesium perchlorate scrubber. Nevertheless, it was still preferred to carry out this humidification and drying procedure as an added precaution.

Sampling results are presented in **Fig. 6** for the Picarro G2203 acetylene calibration test for the Picarro G2203. **Figure 6** (b) shows a stable Picarro G2203 $[H_2O]_r$ level throughout testing, as expected. A calibration could be derived from this data by taking a 5-minute average Picarro G2203 $[C_2H_2]_r$ value from towards the end of each 15-minute sampling step. However, for each 60-minute $[C_2H_2]_0$ sampling period, a 30-minute average was used, as $[C_2H_2]_r$ measurements are slightly more noisy at 0 ppb $[C_2H_2]$. For the lowest three non-zero reference $[C_2H_2]$ levelsettings (0.349 ppb, 0.464 ppb and 0.867 ppb), unstable

$[C_2H_2]_r$ measurements were observed, with $[C_2H_2]_r$ occasionally resolving to the $[C_2H_2]_r$ level observed at 0 ppb $[C_2H_2]$ (see **Sect. S64** in the **Supplement** for an example), despite the fact that the same constant gas stream was being sampled. This probably corresponds to the Picarro G2203 temporarily losing the acetylene IR absorption peak, due to its small size at low $[C_2H_2]$ levels. Therefore, the $[C_2H_2]_a$ calibration was derived excludesing these data points.

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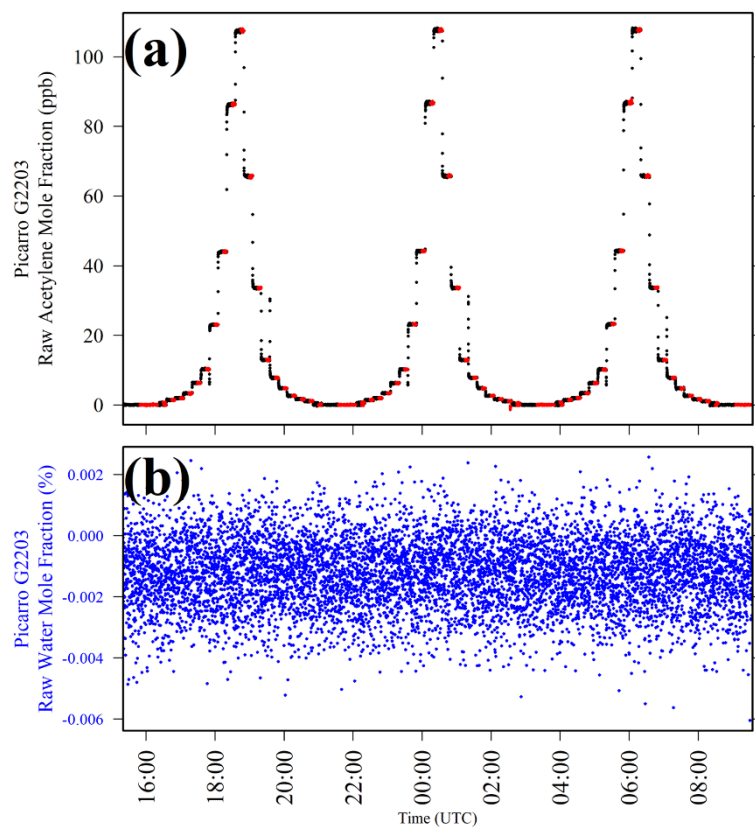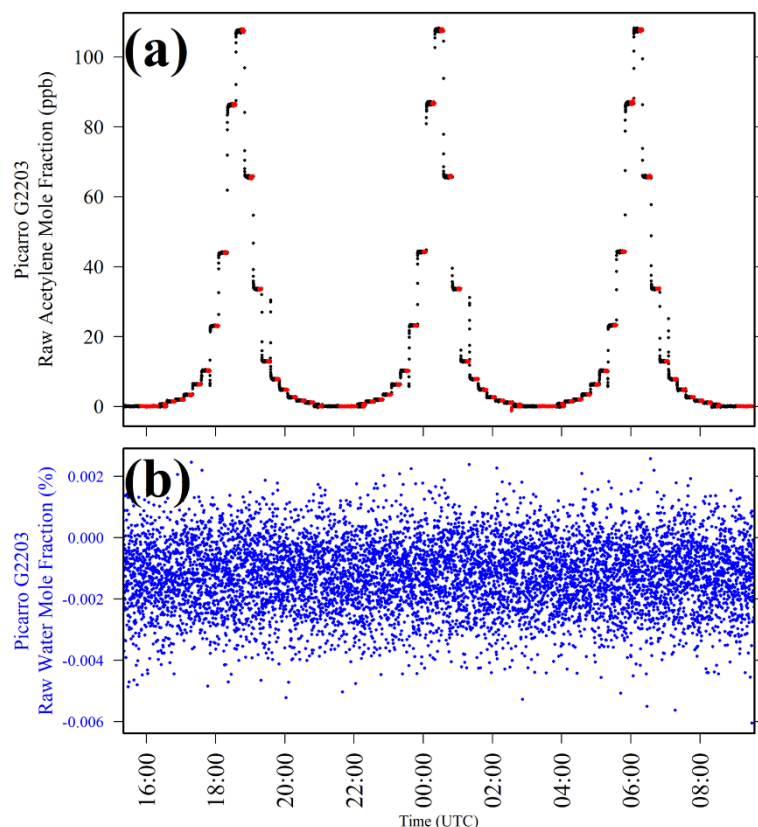
Figure 6: (a) Picarro G2203 [C₂H₂]ᵣ plotted as black dots and (b) Picarro G2203 [H₂O]ᵣ plotted as blue dots, when sampling twenty different standard [C₂H₂] levelsettings over three testing cycles by blending gas from the acetylene calibration cylinder with natural ambient compressed air. Periods used to derive averages are highlighted as red dots in (a).

A linear regression was applied by comparing $[C_2H_2]$ to $[C_2H_2]_r$ (presented in **Fig. 7**) for all $[C_2H_2]$ levelsettings except the lowest four, yielding a gain factor of 0.943 and an offset of −0.147 ppb, with a RMSE of ±0.0676 ppb. Due to the high general stability of the CRDS method over periods of years for other gases (Crosson, 2008, Yver Kwok *et al.*, 2015b, Gomez-Pelaez *et al.*, 2019, Yver-Kwok *et al.*, 2021), it can be assumed that these acetylene calibration coefficients remain sufficiently stable over prolonged time periods. Yet, tThis calibration is only valid when sampling above the lowest stable $[C_2H_2]$ level of 1.16 ppb (corresponding to $[C_2H_2]_r$ measurements of greater than 1.38 ppb). It may be possible to sample at a slightly lower $[C_2H_2]$ level, but further exhaustive testing through trial and error would be required to precisely identify this threshold. The linear calibration fit has a low RMSE of ±0.0676 ppb, indicating low fitting uncertainty. However, there may be an additional uncertainty in calibration coefficients as $[CH_4]_t$ (and hence, C_{MFC}) relies on the declared methane calibration cylinder $[CH_4]$ level and $[CH_4]_t$ relies on the declared acetylene calibration cylinder $[C_2H_2]$ level, both of which have an associated uncertainty, as discussed above. The combined effect of these cylinder uncertainties is evaluated in in **Sect. S5** of the **Supplement**, which reveals that in a worst-case scenario, the calibration gain factor could take a range of between 0.911 and 0.977.
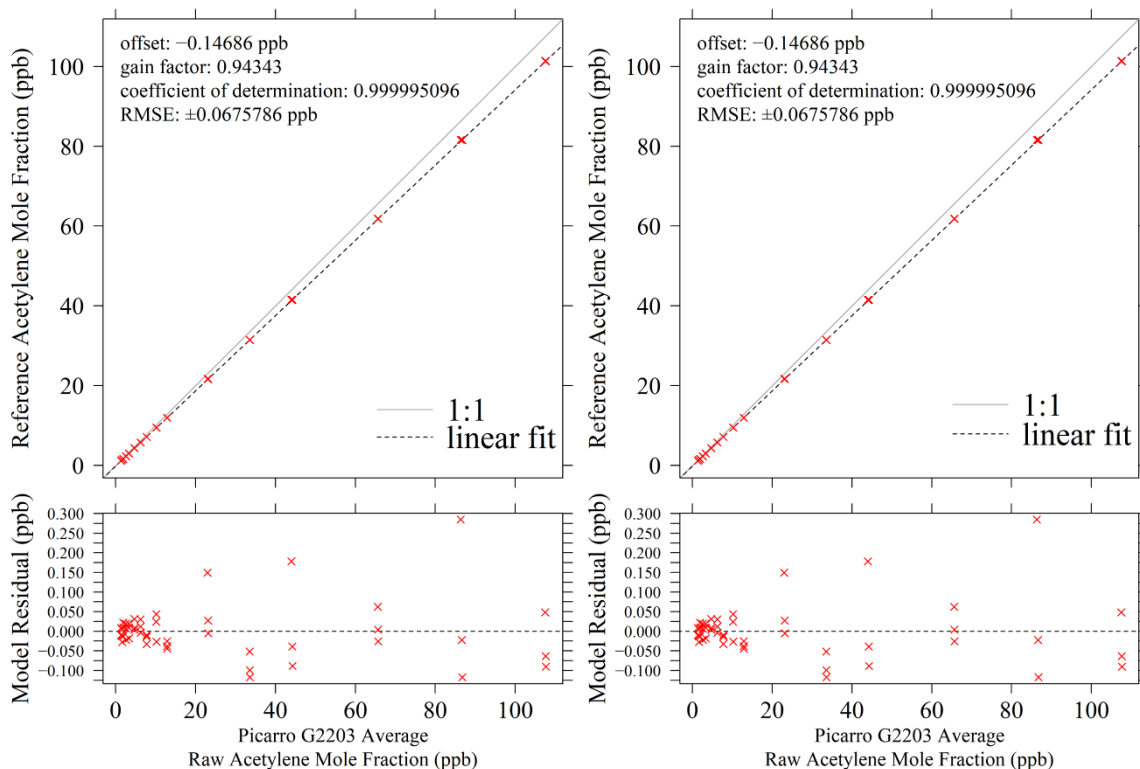
Figure 7: (top) Picarro G2203 5-minute average [C$_2$H$_2$]$_r$ measurements, when combining gas from the acetylene calibration cylinder with natural ambient compressed air, plotted against reference [C$_2$H$_2$] levels (red crosses), with a linear regression model shown as a dashed black line and an identity line shown as a solid light grey line. (bottom) Corresponding model residuals between [C$_2$H$_2$]$_r$ and [C$_2$H$_2$] (red crosses), with a 0 ppb [C$_2$H$_2$] residual shown as a horizonal dashed black line.

It is important to note that the calibration results presented in this work are specific to the Picarro G2203 gas analyser tested here. Other instruments may result in other calibration coefficients, which would need to be tested for each individual gas analyser. The **Fig. 7** fit shows that when sampling at a fixed [C$_2$H$_2$] of 10 ppb, the Picarro G2203 tested here reports 10.76 ppb [C$_2$H$_2$]$_r$. This +8% error is the same order of magnitude to the +12% error reported by Omara *et al.* (2016) for Picarro G2203 [C$_2$H$_2$]$_r$ measurements when sampling a 100 ppm [C$_2$H$_2$] standard. The error presented here could be significant when deriving tracer-based fluxes of a target gas. This therefore emphasises the importance calibrating all [C$_2$H$_2$]$_r$ measurements obtained during field sampling. Although a calibration could ~~an~~not be derived between 0 ppb and 1.16 ppb [C$_2$H$_2$] using this testing data, it can be concluded that sampling gas containing 0 ppb [C$_2$H$_2$] corresponds to a [C$_2$H$_2$]$_r$ measurement of 0.012~~5~~ ppb. This value corresponds to the average of the four measured 30-minute [C$_2$H$_2$]$_r$ averages obtained when sampling 0 ppb [C$_2$H$_2$] during the calibration test. It is also interesting that this value is different to the calibration linear model zero intercept (or offset), which suggests that the Picarro G2203 behaves slightly differently in the absence of acetylene. Although this can be used to correct [C$_2$H$_2$]$_r$ measurements when sampling air containing 0 ppb [C$_2$H$_2$], it is not always possible to know if a [C$_2$H$_2$]$_r$ measurement made at this 0.012~~5~~ ppb level actually corresponds to sampling 0 ppb [C$_2$H$_2$] or whether this erroneously

445 corresponds to a slightly higher undetectable [C₂H₂] level, which remains a limitation of using the Picarro G2203 tested in this work.

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As an additional test, the calibration procedure was repeated but instead, using gas from the zero-air generator (UHP-300ZA-S, Parker Hannifin Manufacturing Limited, Gateshead, Tyne and Wear, UK) for dilution. Details of this test and presented in

455 **Sect. S75** in the **Supplement**. This test serves to check the validity of the acetylene calibration coefficients given above in a different gas mixture with no background levels of methane present. This additional test yielded a gain factor of 0.941 and an offset of +0.0014 ppb, with a RMSE of ±0.0356 ppb, when comparing standard [C₂H₂] levels to [C₂H₂]ᵣ measurements. This gain factor is almost the same as when using natural ambient compressed air for dilution, with a similar offset close to zero. Nevertheless, small changes in [C₂H₂]ᵣ response in different background gases may have an influence on applications in field sampling, which should be considered, although it does not appear to be so important for the Picarro G2203 tested here.

2.5 Measurement stability

As a final test, the stability of Picarro G2203 acetylene measurements was assessed by conducting an Allan variance (σ_A^2) test, which characterises the variability between sets of measurements over different timescales, ranging from the interval between consecutive measurements up until half of the duration of the test (although timescales of greater than a few hours hold little statistical value). Gas from a~~First,~~ natural ambient compressed air ~~from a~~ cylinder ~~containing 2.076 ppm [CH₄]~~ was blended with gas from the acetylene calibration cylinder to sample ~~10.9 ppb~~a [C₂H₂]$_r$ of 10.9 ppb (corresponding to~~ an [C₂H₂] of 10.1 ppb [C₂H₂])~~, which was sampled~~ for 12 hours. This blending assumes the MFCs to provide a constant flow rate, as any potential variability in MFC flow rate may be convolved with measurement noise, which is a limitation of this approach. An additional σ_A^2 test was performed at an [C₂H₂] of ~~Next, pure natural ambient compressed air from the same gas cylinder was sampled for 12 hours, corresponding to~~ 0 ppb, with details and results provided in **Sect. S8** of the **Supplement**~~[C₂H₂]. To conduct this test, a similar set-up was used as for the acetylene calibration, as illustrated schematically in **Fig. 4**, when sampling 10.1 ppb [C₂H₂]. A modified version was used for the 0 ppb [C₂H₂] test to save gas, as no dilution is required; the compressed air cylinder was connected directly to a MFC, before subsequent humidification and drying.~~

To evaluate measurement stability, all [C₂H₂]$_r$ measurements were first calibrated using calibration coefficients from the previous subsection. ~~when sampling 10.1 ppb [C₂H₂]. [C₂H₂]$_r$ measurements made at 0 ppb [C₂H₂] were corrected by subtracting 0.0125 ppb, as the linear model fit is not valid below 1.16 ppb [C₂H₂] (although, in theory, this offset correction has no effect in this analysis on variance). Then an~~before performing an σ_A^2 test using~~was conducted on~~ subsets of this~~each~~ prolonged dataset, as described by Werle *et al.* (1993). As the measurement frequency is inconsistent, the integration time was derived by finding the average of differences between the time corresponding to the first measurement in each subset and the first measurement in the next subset. In addition, the σ_A^2 test was repeated ten times by moving the starting and ending datapoint for each of the ten analyses, as the duration between each measurement follows a cycle of ten [C₂H₂]$_r$ measurements (as discussed previously~~above~~). These repeated tests were therefore used to obtain an average of the σ_A^2 values and corresponding integration times from the ten analyses.

A l~~L~~ogarithmic plot~~s~~ showing Allan deviation precision (σ_A) as a function of integration time is~~are~~ given in **Fig. 8**, with a white noise line~~s~~ also shown. The σ_A at the smallest integration time is ±0.0863 ppb (4.22 s integration time), which suggests that variability between individual consecutive measurements is small when sampling ~~10.1 ppb [C₂H₂] and ±0.0577 ppb (4.24 s integration time) when sampling 0 ppb [C₂H₂]~~a single gas. The~~Values of~~ σ_A at the smallest integration time did not use averaging of multiple measurements and simply took the variance between individual consecutive measurements, as each averaging bin contained one single element. **Figure 8** ~~plots~~show~~s~~ consistently decreasing σ_A with integration time, as expected, with a trend close to the white noise line. ~~However, the [C₂H₂] plot at 0 ppm [C₂H₂] has an interesting feature in the first 100 s where σ_A increases slightly before continuing its decline as a function of integration time, following a trend close to the white noise line (although offset from σ_A at the lowest integration time). This could be associated with the roughly 40 s [C₂H₂]$_r$~~

measurement cycle, with the Picarro G2203 consistently struggling to fit for an absence of acetylene over each of the ten samples. The difference between the two **Fig. 8** fits supports the suggestion from the previous subsection, that the Picarro G2203 [C₂H₂] response is different at very low [C₂H₂] levels, close to 0 ppb. Nevertheless, neither σ_A^2 test shows a clear sustained inflection in σ_A decrease with integration time. This suggests that there is minimal drift over a 12-hour period compared to variability between individual measurements. This 12-hour duration is far longershorter than a typical field sampling campaign (a few hours), demonstrating that Picarro G2203 measurements are unlikely to drift during field sampling. Furthermore, both tests reveal an σ_A of less than ±0.1 ppb at the lowest integration time which suggests that variability between individual consecutive measurements is small, when sampling a single gas.
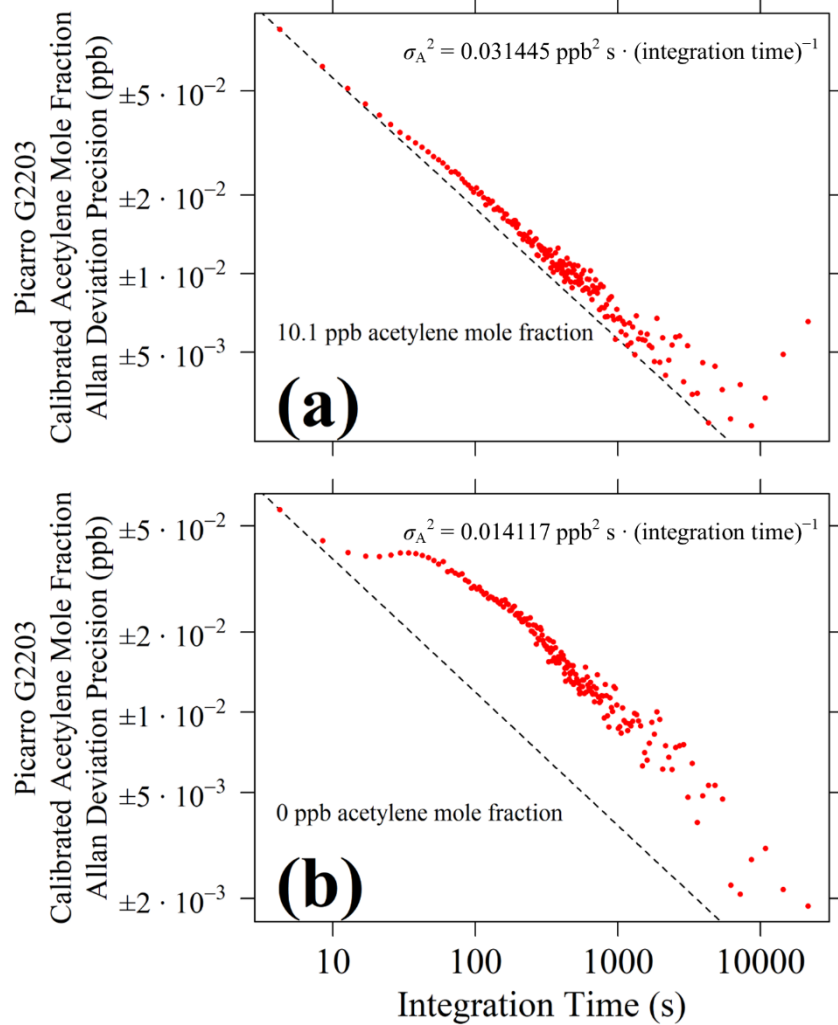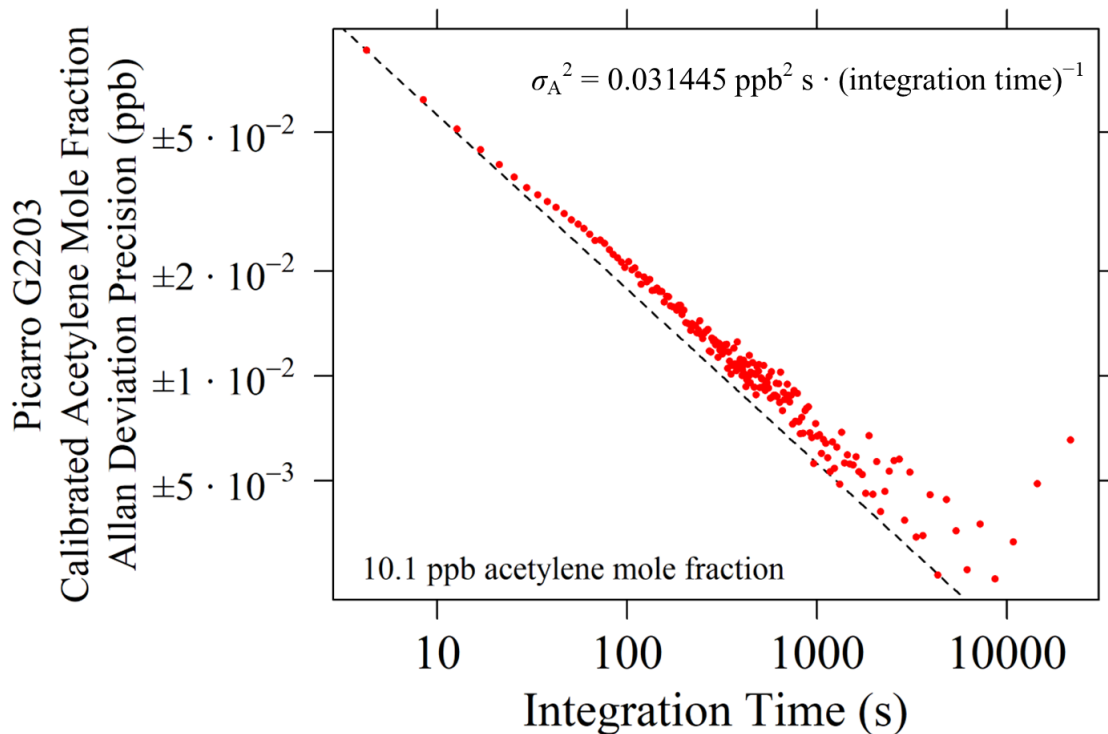
Figure 8: σ_A **for Picarro G2203 calibrated [C₂H₂] measurements as a function of integration time derived from an average of ten different tests, plotted as red dots, when** ~~(a)~~ **sampling** an [C₂H₂] of **10.1 ppb** ~~[C₂H₂] and (b) sampling 0 ppb [C₂H₂]~~**. Logarithmic axes are used** ~~in each plot~~**.** The b~~B~~**lack dashed line**s **depict**s **white noise, with** this~~each~~ **fit forced to intersect with** σ_A **at the lowest integration time (the fitting coefficient is provided inside** the~~each~~ **plot).**

3 Field testing methane flux inversion method using an acetylene tracer release

3.1 Acetylene release method

Standard details on the acetylene release method ~~itself~~ are provided here. Dry a~~A~~cetylene with a 99.5% purity is released from an 8.7 kg acetylene gas cylinder (Acétylène Industriel X50S, Air Products S.A.S., Saint Quentin Fallavier, France)~~, with a 99.5% purity,; as gas from such cylinders is naturally dry, it is released pure without any treatment. The cylinder is~~ connected to an acetylene regulator (0783640, GCE Ltd, Warrington, UK)~~, with a maximum output pressure of 1.5 bar~~. The acetyleneGas flow rate ($Q_{acetylene}$) is manually adjusted using a downstream metering valve (SS-4L, Swagelok Company). As ~~the gauge pressure of~~ gaseous acetylene gauge pressure must not exceed~~be kept below~~ 1.5 bar for safety reasons, ~~the pressure range of~~ the acetylene regulator pressure range is targeted to between 0.5 bar and 1.0 bar whilst simultaneously adjusting the metering valve for the desired flow rate. As only 10% of the cylinder contents ~~of the cylinder~~ can safely be release~~emitt~~ed per hour, the maximum sustained ~~acetylene flow rate ($Q_{acetylene}$) level from this acetylene cylinder~~ is 0.23942 g s^{-1}. $Q_{acetylene}$ is measured using an acetylene flow meter (8C3B04-20X1/0, Cubemass C 300, Endress+Hauser Group Services AG, Reinach,

Switzerland), which ~~measures $Q_{acetylene}$ us~~esing the Coriolis technique (Baker, 2016), with an accuracy of no greater than 0.00389 g s^{-1} ~~when sampling~~ below an $Q_{acetylene}$ of 0.778 g s^{-1} and no greater than 0.005 multiplied by $Q_{acetylene}$ itself ~~when measuring~~ above an $Q_{acetylene}$ of 0.778 g s^{-1}. Further ~~details on the~~ acetylene flow meter details are provided in **Sect. S9~~6~~** of the **Supplement**. Following each acetylene release, all equipment downstream of the regulator is flushed with nitrogen gas.

The acetylene release point is connected to the rest of the acetylene release equipment using Synflex 1300 tubing with an OD of 0.5 inches (the null effect of Synflex 1300 on acetylene is discussed in **Sect. S2 of the Supplement**). A 0.5 inches to 0.25 inches standard SS Swagelok fitting reducer (SS-810-R-4, Swagelok Company) ~~is used to~~ connects to this wider tube, ~~which is~~ chosen to minimise the pressure drop up to the release point. At the point of release, the tubing is split into four upwards-facing co-located Synflex 1300 tubes all with an OD of 0.5 inches, as illustrated in **Fig. 9**, to promote more even plume dissipation ~~of the plume above ground level~~. A 6 m safety exclusion zone is designated around~~as being 6 m away from~~ the release point as described in **Sect. S10 of the Supplement**, based on~~with all acetylene release equipment placed outside this zone. This distance was calculated such that [C₂H₂] cannot exceed its lower atmospheric flammable limit of 2.5% (Williams and Smith, 1969) considering a $Q_{acetylene}$ of 0.5 g s⁻¹ and using~~ Gaussian plume modelling ~~in the worst-case Pasquill stability class~~ (Turner, 1994)~~, with a mean wind speed of 0.1 m s⁻¹ to accentuate [C₂H₂]. The boundaries of the safety exclusion zone are designated by cones, with the zone being constantly manned by the release operator who stands outside the zone and continuously surveys the acetylene release equipment.~~
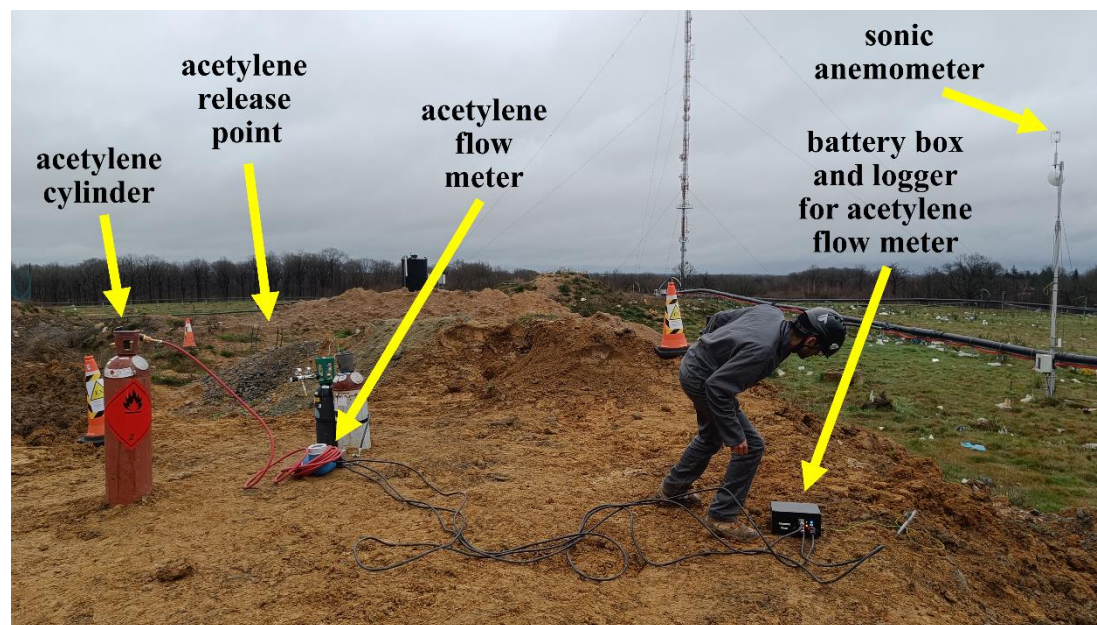
Figure 9: A photograph of the acetylene release equipment when deployed during the campaign at the landfill site. The cones indicate the boundaries of the safety exclusion zone (not all cones are visible).

A schematic illustration of the entire acetylene release set-up is shown in **Fig. 10**. All components are selected for compatibility with acetylene. Equipment for acetylene conventionally has British Standard Pipe parallel (BSPP) left-hand (LH) G threads. BSPP LH G threads are converted into threads for standard SS Swagelok fittings using a SS 12 mm to 0.25 inches union (SS-12M0-6-4, Swagelok Company) and a brass BSPP LH G 0.375 inches to 12 mm adapter. In addition, the acetylene flow meter has threads for VCO SS Swagelok fittings, which are converted into threads for standard SS Swagelok fittings using a VCO to standard SS Swagelok fitting union (SS-4-VCO-6-400, Swagelok Company). Acetylene release equipment is protected from exposure to flammable gas mixtures using non-return valves. Flashback arrestors prevent an accidental flame from reaching upstream components and eventually, potentially entering the acetylene cylinder. A 5 bar flashback arrestor with a built-in non-return valve (50951, GCE Ltd) is connected directly downstream of the acetylene regulator. A 10 m reinforced high tensile synthetic textile acetylene hose (GCE Ltd) with an in-built non-return valve is used to connects the cylinder to the acetylene flow meter. An additional 2.0 bar flashback arrestor with a built-in non-return valve (Flashback Arrestor Super 66, WITT-Gasetechnik GmbH & Co KG, Witten, Germany) is connected upstream of the acetylene flow meter. The entire acetylene release set-up is illustrated schematically in **Fig. 10**. All fittings and connectors were selected for compatibility with acetylene, with any copper alloys (including brass) containing no more than 65% copper.
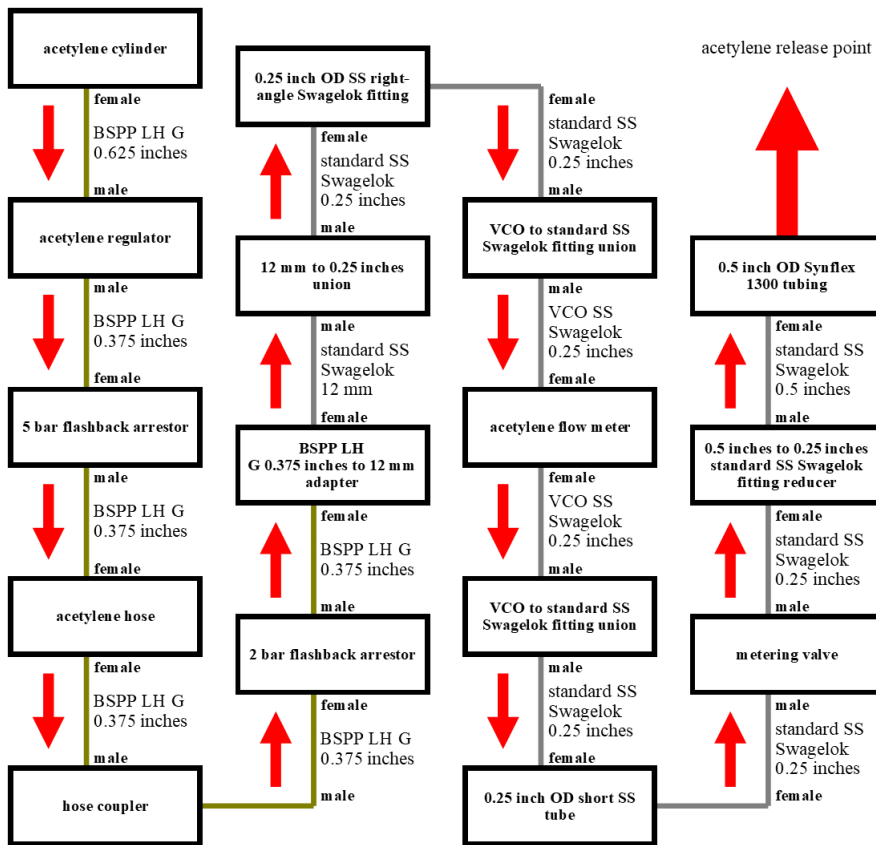
Figure 10: A schematic of each individual component (in black boxes) used when conducting an acetylene release. Dark yellow lines indicate brass connections and grey lines indicate SS connections. The thread type between each component is given next to each line and the gender of the threads is given in bold text outside of each box. The direction of acetylene gas flow is indicated by red arrows.

Equipment for use with acetylene conventionally uses threads for British Standard Pipe parallel (BSPP) left hand (LH) G fittings, as opposed to right-hand fittings which are conventionally used in most other applications. These BSPP LH G fittings are converted into threads for standard SS Swagelok fittings using a SS 12 mm to 0.25 inches union (SS-12M0-6-4, Swagelok Company) and a brass BSPP LH G 0.375 inches to 12 mm adapter. In addition, the inlet and outlet for the acetylene flow meter has threads for VCO SS Swagelok fittings. A VCO to standard SS Swagelok fitting union (SS-4-VCO-6-400, Swagelok Company) is therefore used to obtain threads for standard SS Swagelok fittings, for integration with the rest of the set-up.

3.2 Landfill site release campaign

To test our acetylene release and corresponding $Q_{methane}$ calculation methods, an acetylene release was conducted from within a landfill site. This particular landfill site was chosen as it a known facility-scale methane source, for which we were able to acquire site access. The specificities of this specific study site (for example waste content, waste quantity, site age and site management) are irrelevant in this study; this study is dedicated to the acetylene release method itself in the context of $Q_{methane}$

quantification methods in general. Therefore, the magnitude of any derived $Q_{methane}$ rate is beyond the scope of this study and

will be discussed in a future publication. An aerial photograph of the site is shown in **Fig. 11**. The acetylene release location

from within the site was selected due to accessibility with regards to transportation and installation of a heavy acetylene

570   cylinder. We were not authorised to conduct a release from a more central location due to site activities and the presence of

active open landfill cells. In general, the acetylene release location should be as close to the source as possible, to trace emission

of the methane source as it disperses through the atmosphere, although this can be difficult from a complex heterogeneous area

source such as a landfill site (Fredenslund *et al.*, 2019). The complications associated with tracer release positioning is

discussed in further detail in **Sect. 4**. A three-dimensional sonic anemometer (WindMaster Pro, Gill Instruments Limited,

575   Lymington, Hampshire, UK) measured winds at 20 Hz, near to the acetylene release point, as illustrated in **Fig. 10**, which was

visually aligned with an uncertainty of approximately ±4° and erected to a height of approximately 6 m above ground level.
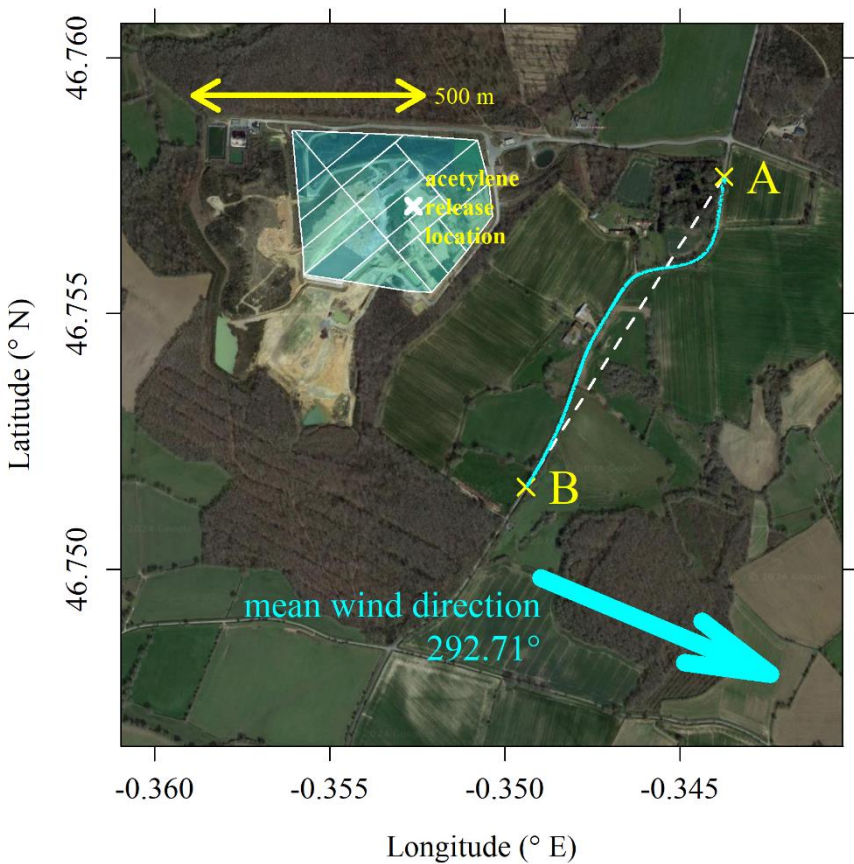
Figure 11: The location of the acetylene release (white cross) which was conducted at ground level, plotted on top of a background map. Transparent shaded cyan polygons indicate both active and inactive cells, as identified by the landfill site operator. The location

580   **of Picarro G2203 [C₂H₂]ᵣ measurements are shown as cyan dots on a sampling road between Point A and Point B, indicated by the yellow crosses. The plane between Point A and Point B is shown as a dashed white line. The average direction in which the wind vector was blowing is shown as a cyan arrow, as recorded by the sonic anemometer, from 20 minutes before the first transect until the end of the final transect. The background image is taken from Google Maps (imagery (2024): Maxar Technologies).**

Rather than relying on stationary (zero-dimensional) downwind sampling, the methane and acetylene plumes were instead sampled through multiple plume transects for subsequent integration, as $Q_{methane}$ derived from one-dimensional transects results in improved flux accuracy (as discussed in **Sect. 1**). Twenty vehicular transects were conducted on a nearbly downwind sampling road during the acetylene release. The position and nature of downwind transects can have an impact on $Q_{methane}$ estimates if the acetylene release location is not perfectly co-located with the methane source, which is discussed in further detail in **Sect. 4**. The vehicle was equipped with the Picarro G2203 gas analyser, for which all sampled air passed through the Nafion-based gas dryer followed by a magnesium perchlorate scrubber. The air inlet was fixed to the roof of the vehicle (approximately 2 m above ground level). The Picarro G2203 was powered using a portable mains power supply bank. A LI-COR LI-7810 (LI-COR, Inc.) gas analyser was also installed in the vehicle which shared the same air inlet as the Picarro G2203 (but was connected upstream of theno dryer), measuring $[CH_4]_r$ and $[H_2O]_r$ at a frequency of approximately 1 Hz. The LI-COR LI-7810 was powered by its internal battery. A global navigation satellite system (GNSS) positional logger made measurements of vehicular position at 1 Hz. The timestamp of Picarro G2203 and LI-COR LI-7810 measurements were individually adjusted to GNSS time by breathing into the air inlets at a fixed GNSS time and recording the time of the $[CH_4]_r$ responses. This could be achieved as a member of our team exhales methane; most humans do not exhale detectable methane enhancements (Dawson *et al.*, 2023).

The sampling campaign duration is defined as 20 minutes before the start of first transect up to the time of the point of the final transect. $Q_{acetylene}$ was largely stable for the full duration of the sampling campaign, with an average $Q_{acetylene}$ level of 0.239 g s^{-1} and a standard deviation variability of ±0.001 g s^{-1}, as presented in **Sect. S117** in the **Supplement**. The 20-minute period of continuous acetylene flow in advance of vehicular sampling allowed the acetylene plume to become well establish itselfed and to stabilise in the atmosphere (Fredenslund *et al.*, 2019). The average wind direction was 292.7° with respect to True North and the average wind speed was 3.84 m s^{-1}, for the duration of the sampling campaign (see **Sect. S117** in the **Supplement**).

The limits of the sampling road for $Q_{methane}$ calculation purposes were defined as being between Point A and Point B (indicated in **Fig. 11** as yellow crosses); although vehicular sampling protruded these points to sample on a longer stretch of road, the landfill emission plumes remained within this spatial range, serving as sensible limits for subsequent analysis. All Picarro G2203 $[C_2H_2]_r$ measurements from each transect are projected onto the vertical plane between Point A and Point B in **Fig. 12** (a). During six transects (transect 2, 5, 9, 14, 17 and 18), a feature containing $[C_2H_2]_r$ measurements of less than −0.5 ppb was observed. These negative $[C_2H_2]_r$ measurements were observed just before observing the acetylene peak, making these periods clearly distinguishable from instrumental noise. Furthermore, consistent negative $[C_2H_2]_r$ measurements were made during each feature, as opposed to random noise which generally varied between randomly positive and negative measurements. These erroneous measurements were probably due to complications associated with the Picarro G2203 internal spectral fitting algorithms, in response to a sudden sharp $[C_2H_2]$ change. This may have been due to mis-fitting issues as the Picarro G2203

takes some time to complete a scan against all wavelengths across the acetylene IR absorption peak. These six transects have therefore been removed from the subsequent flux analysis, resulting in fourteen remaining successful transects.
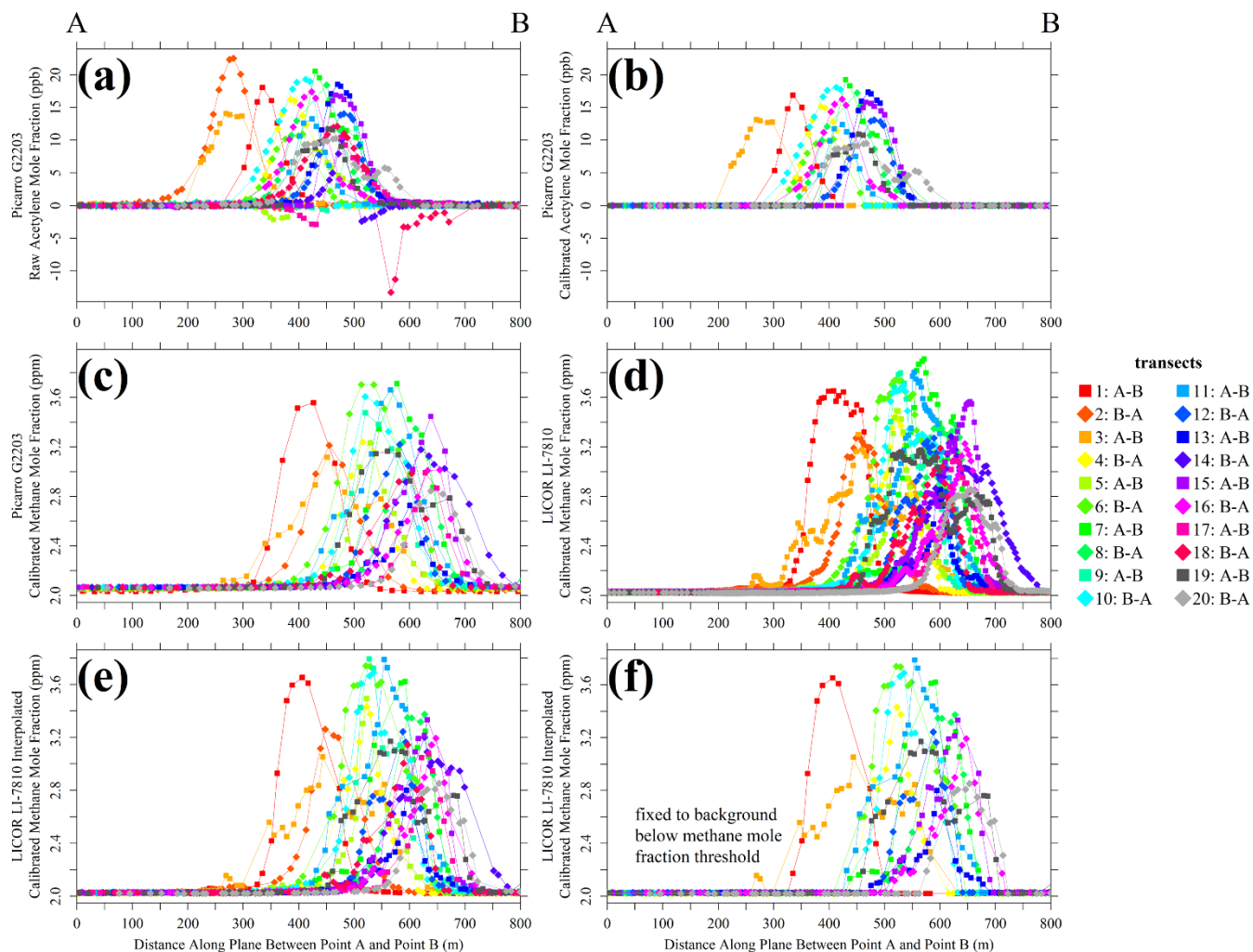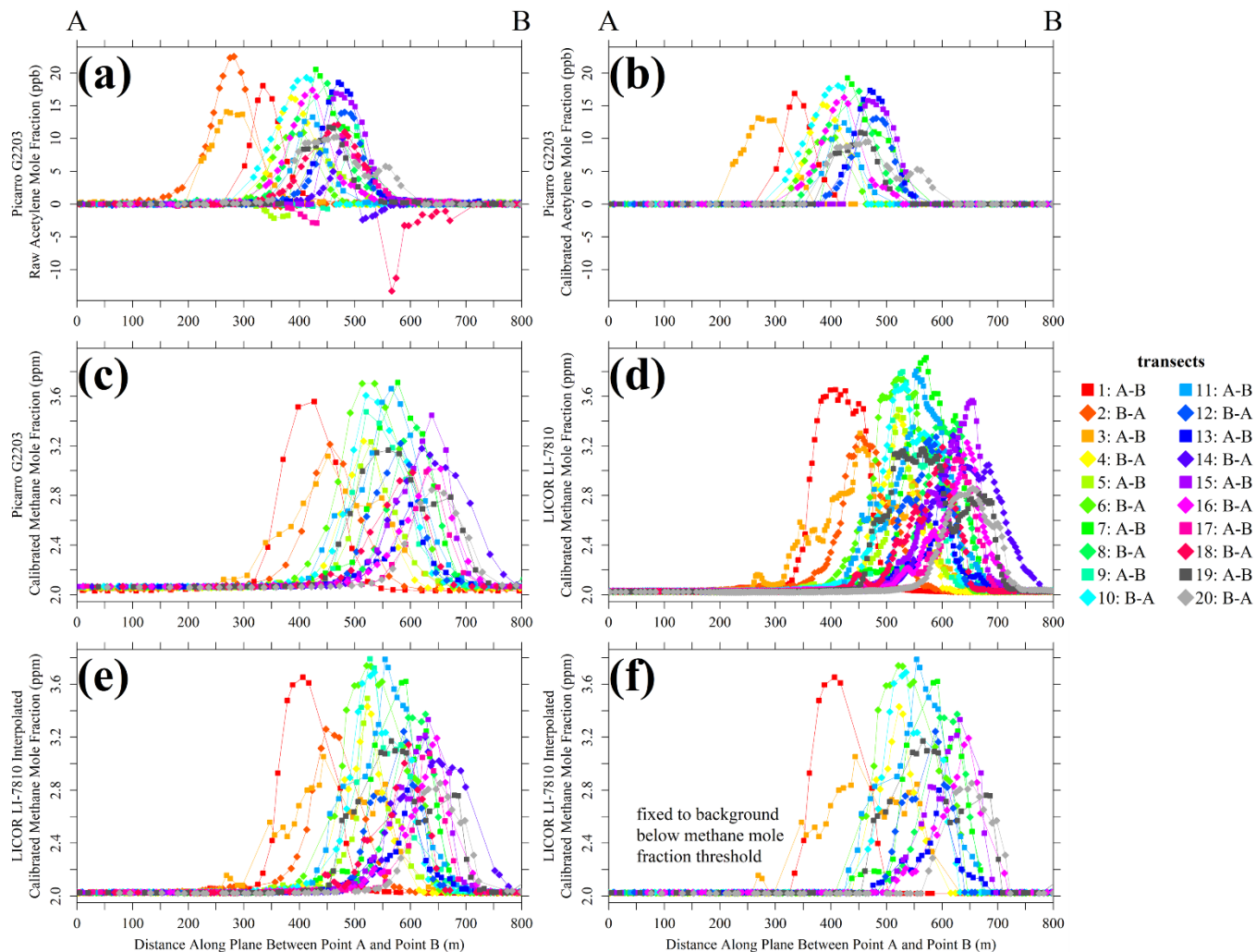
Figure 12: (a) Raw Picarro G2203 $[C_2H_2]_r$ measurements, **(b)** calibrated Picarro G2203 $[C_2H_2]_r$ measurements, **(c)** calibrated Picarro G2203 $[CH_4]$ measurements, **(d)** calibrated LI-COR LI-7810 $[CH_4]$ measurements, **(e)** calibrated LI-COR LI-7810 $[CH_4]$ measurements interpolated to the Picarro G2203 $[C_2H_2]_r$ timestamp and **(f)** calibrated LI-COR LI-7810 $[CH_4]$ measurements interpolated to the Picarro G2203 $[C_2H_2]_r$ timestamp with $[CH_4]$ below $[CH_4]_{threshold}$ set to $[CH_4]_0$ for each transect, all plotted as coloured dots (see legend for transect colours) on the plane between Point A and Point B downwind of a landfill site. Only successful transects are shown in **(b)** and **(f)**.

For the fourteen remaining transects, all $[C_2H_2]_r$ measurements above 1.38 ppb from the Picarro G2203 were converted into dry calibrated measurements using laboratory-derived coefficients from **Sect. 2**. These calibrated $[C_2H_2]$ measurements are presented in **Fig. 12** (b), as a function of distance along the plane between Point A and Point B. All Picarro G2203 $[C_2H_2]_r$ measurements of less than 1.38 ppb were fixed to 0 ppb $[C_2H_2]$, as this sampling may be unstable and some non-zero $[C_2H_2]$ sampling in this range can erroneously resolve to the $[C_2H_2]_r$ observed at 0 ppb $[C_2H_2]$ (as discussed in **Sect. 2**). The influence of this step when applied to low (but non-zero) $[C_2H_2]$ sampling, on $Q_{methane}$, is dealt with in the next subsection. Picarro G2203 $[CH_4]_r$ measurements from all twenty transects were converted in dry calibrated $[CH_4]$ using the coefficients provided in **Sect.**

S1 in the **Supplement**. All $[CH_4]_r$ measurements from the LI-COR LI-7810 were converted into dry calibrated $[CH_4]$, by first applying an empirical water correction followed by a calibration which could be cross-referenced to standards on the WMO greenhouse gas scale for methane (WMO X2004A). Calibrated Picarro G2203 and LI-COR LI-7810 $[CH_4]$ measurements from each transect are also shown in **Fig. 12** (c and d, respectively), as a function of distance along the plane between Point A and Point B.

3.3 Landfill site methane emission flux calculation

In this study, two sets of $Q_{methane}$ values were calculated using both $[C_2H_2]$ as well as $[C_2H_2]_r$ as model input, to compare any influence of Picarro G2203 acetylene calibration on $Q_{methane}$ results. The principle of using acetylene as a tracer gas for methane, requires mole fraction measurements from both the acetylene and the methane plume to calculate $Q_{methane}$. $Q_{methane}$ was derived in this work by integrating the observed methane and acetylene emission plume as a function of distance along the sampling road. This form of spatial integration is used to apply equal weighting to each mole fraction measurement as a function of distanced covered, especially with irregular spatial measurements due to irregular driving speed and sampling frequency. Although, in theory, $Q_{methane}$ can be derived from a single downwind measurement point (as discussed in **Sect. 1**), spatial integration results in better accuracy, especially if the methane and acetylene plumes do not perfectly overlap, as illustrated in **Fig. 12**.

Before conducting this integration, LI-COR LI-7810 $[CH_4]$ measurements were first interpolated to the lower frequency (and less regular) Picarro G2203 $[C_2H_2]$ timestamp so that each $[C_2H_2]$ had a corresponding spatial $[CH_4]$ measurement, as shown in **Fig. 12** (e). In general, the likelihood of sampling close to the maximum of each emission plume decreases with larger sampling gaps. Yet, due to the far superior LI-COR LI-7810 $[CH_4]$ sampling frequency, this data was assumed to capture the full methane plume shape, allowing the loss of sampling points from this methane plume to replicate the data loss from the acetylene plume. Due to the intermediate Picarro G2203 $[CH_4]$ sampling frequency, these measurements were not used in this analysis. By contrast, interpolating Picarro G2203 $[C_2H_2]$ to the LI-COR LI-7810 $[CH_4]$ would be less appropriate as acetylene plume measurements would be artificially generated from a lack of information on acetylene plume shape (*i.e.* artificial gap filling). As a general caveat, perfect replication of methane plume information loss requires the methane and acetylene plumes to perfectly overlap in space. As the plumes were slightly offset (see **Fig. 12**), this interpolation method did not result in identical information loss from both the acetylene plume and the methane plume (see **Sect. 4** for discussion). Nevertheless, interpolation to the lower Picarro G2203 $[C_2H_2]$ timestamp ensured that the likelihood of loss of information on the methane emission plume using interpolated LI-COR LI-7810 $[CH_4]$ measurements remained the same, thereby avoiding any bias in multiple $Q_{methane}$ estimates derived from individual transects.

$Q_{methane}$ also requires background mole fraction values ($[C_2H_2]_0$ and $[CH_4]_0$) values to characterise the enhancement of the tracer and methane emission plume above the background. $[CH_4]_0$ was derived by taking the average of the lowest five non-

interpolated LI-COR LI-7810 [CH$_4$] measurements from each transect. This accounts for [CH$_4$]$_0$ natural regional variability over time. This also corrects for any [CH$_4$] measurement offset that may occur due to instrumental drift. For acetylene, [C$_2$H$_2$]$_0$ was fixed to 0 ppb for all transects, as negligible levels of acetylene are otherwise expected in the natural ambient background. Thus, this approach does not account for potential changes in [C$_2$H$_2$]$_r$ measurement offset. While taking the lowest five [C$_2$H$_2$]$_r$ measurements from each transect was considered for an uncalibrated [C$_2$H$_2$]$_0$, due to the noisy baseline, this would inevitably result in capturing the noise's weakest values, making this method unsuitable. For the calibrated [C$_2$H$_2$] data (derived following the procedure outline above), instrumentalsensor baseline drift cannot be deduced from the lowest measurements, as all [C$_2$H$_2$]$_r$ of less than 1.38 ppb are fixed to 0 ppb [C$_2$H$_2$]. But with the stability of CRDS (Crosson, 2008, Yver Kwok *et al.*, 2015b, Gomez-Pelaez *et al.*, 2019, Yver-Kwok *et al.*, 2021), drift in the acetylene calibration is unlikely to be a major issue, which is supported by the $\sigma_A{}^2$ test results given in **Sect. 2** which showed no [C$_2$H$_2$] drift over a period of 12 hours.

As an additional step it is important to take into account the potential loss of low (but non-zero) [C$_2$H$_2$] sampling due to setting a maximum [C$_2$H$_2$]$_r$ threshold of 1.38 ppb (corresponding to 1.16 ppb [C$_2$H$_2$]), below which all [C$_2$H$_2$] is fixed at 0 ppb. In theory, this is not likely to be an issue away from of the acetylene plume, as there are no major acetylene sources and [C$_2$H$_2$]$_0$ is expected to consistently equal 0 ppb. However, a small number of non-zero [C$_2$H$_2$] enhancements may be lost from the edges of each plume, leading to a slightly lower acetylene plume integral. To replicate this effect on [CH$_4$] measurements, any interpolated [CH$_4$] measurements below a methane mole fraction threshold ([CH$_4$]$_{threshold}$) from each of the fourteen successful transects were fixed to [CH$_4$]$_0$, as illustrated in **Fig. 12** (f). [CH$_4$]$_{threshold}$ is calculated for each successful transect using

$$[CH_4]_{threshold} = \left(\left(\frac{\text{maximum } [CH_4] - [CH_4]_0}{\text{maximum } [C_2H_2] - [C_2H_2]_0} \right) \cdot 1.16 \text{ ppb} \right) + [CH_4]_0, \tag{3}$$

which takes the ratio between maximum mole fraction enhancements from each transect (using interpolated [CH$_4$] measurements). Although this is not a perfect approach as the maximum height of both the methane and acetylene plume were unlikely to be captured (due to large sampling gaps and an offset acetylene plume), the distance of the maximum [C$_2$H$_2$] and [CH$_4$] measurements from the acetylene and methane plume centres, respectively, should average out over a sufficient number of transects, resulting oin a null overall effect on $Q_{methane}$. These modified [CH$_4$] values must be used alongside calibrated [C$_2$H$_2$] measurements, during $Q_{methane}$ calculation. However, $Q_{methane}$ derived using uncalibrated [C$_2$H$_2$]$_r$ does not require modified [CH$_4$], as this tests flux estimation assuming all uncalibrated [C$_2$H$_2$]$_r$ measurements to be correct. **Fig. 12** (e and f) shows that interpolated [CH$_4$] measurements without this threshold are similar to modified [CH$_4$] measurements with the imposed threshold. Nevertheless, this step is important to minimise the effect of inflated methane plumes due to erroneously low [C$_2$H$_2$] measurements (without corresponding erroneously low [CH$_4$] measurements) from biasing $Q_{methane}$.

$Q_{methane}$ was finally calculated following

$$Q_{methane} = Q_{acetylene} \cdot \left(\frac{\sum_{i=2}^{n-1} \left(([CH_4]_i - [CH_4]_0) \cdot \varDelta x_i \right)}{\sum_{i=2}^{n-1} \left(([C_2H_2]_i - [C_2H_2]_0) \cdot \varDelta x_i \right)} \right) \cdot \left(\frac{M_{methane}}{M_{acetylene}} \right), \tag{4}$$

where i represents each individual measurement within each transect and n represents the total number of measurements within each transect. Δx is the average spatial distance between adjacent measurements given by

$$\Delta x_i = \frac{\Delta x_{i-1 \rightarrow i} + \Delta x_{i \rightarrow i+1}}{2}, \tag{5}$$

where $\Delta x_{a \rightarrow b}$ is the spatial distance between any measurement point a and any other measurement point b. $\Delta x_{a \rightarrow b}$ is derived using the difference in latitude and longitude between point a and point b. Equation (4) requires [CH$_4$] and [C$_2$H$_2$] to be in the same mole fraction units (*e.g.* ppm) and for both mole fractions to be either dry or wet (dry mole fractions are used here). M_{methane} is the molar mass of methane (16.0425 g mol^{-1}) and $M_{\text{acetylene}}$ is the molar mass of acetylene (26.0373 g mol^{-1}).

4 Results and discussion

4.1 Landfill flux results

Landfill Q_{methane} results derived using Eq. (4) are presented in **Fig. 13**. The average Q_{methane} ~~average~~ from the fourteen individual vehicular transects is 17.3 g s^{-1}, with a standard deviation variability between ~~the~~ different transect Q_{methane} estimat~~flux~~es of ±9.6 g s^{-1}, when using calibrated [C$_2$H$_2$] (and [CH$_4$] fixed to [CH$_4$]$_0$ below [CH$_4$]$_{\text{threshold}}$). The significance of Q_{methane} in the context of overall landfill emissions from this specific study site and in comparison to Q_{methane} derived using other methods will be discussed in a forthcoming study. A combined Q_{methane} was also derived by combining data from all successful transects simultaneously within Eq. (4) (where separate [C$_2$H$_2$]$_0$ and [CH$_4$]$_0$ values were subtracted from data corresponding to each transect) to yield a single combined emission Q_{methane}~~flux~~ estimate of 15.8 g s^{-1}. This is consistent with the average of the fourteen individual Q_{methane} valu~~flux~~es, within the standard deviation uncertainty range. Using the uncalibrated [C$_2$H$_2$]$_r$ data as Eq. (4) input (and unaltered interpolated [CH$_4$]) yielded smaller Q_{methane} values, with an average of the fourteen individual vehicular transects of 16.0 g s^{-1} and a standard deviation variability between the different transects of ±8.6 g s^{-1}. This represents a Q_{methane}~~flux~~ underestimation of −7.6% compared to Q_{methane} derived using calibrated [C$_2$H$_2$] as Eq. (4) input.
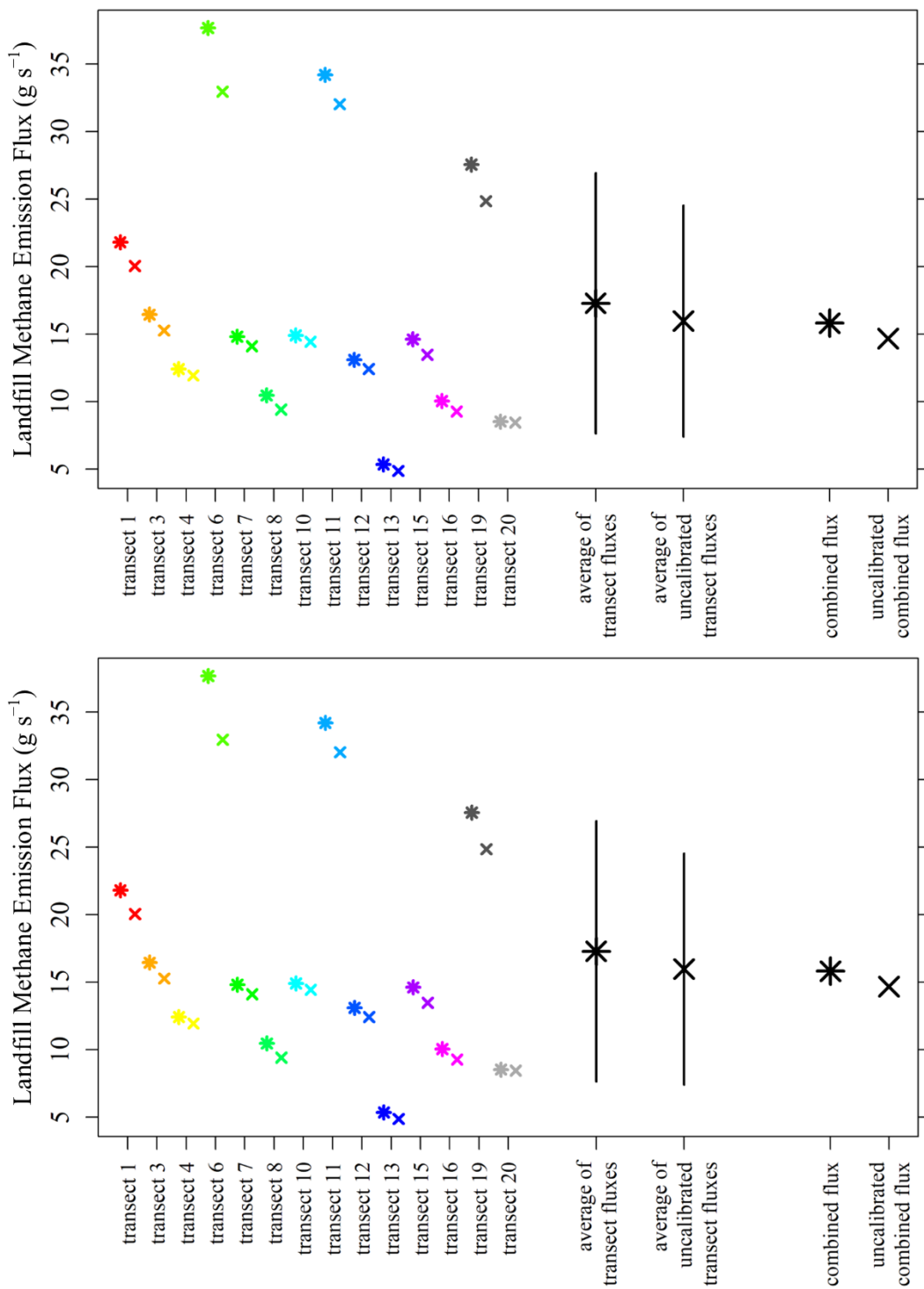
Figure 13: Individual landfill $Q_{methane}$~~methane flux~~ estimates for each individual transect, corresponding averages and the overall combined ~~landfill $Q_{methane}$methane emission flux~~ estimate, plotted as stars using calibrated [C_2H_2] (with [CH_4] below [CH_4]$_{threshold}$ fixed to [CH_4]$_0$) and crosses using uncalibrated [C_2H_2]$_r$ as Eq. (4) input. The black lines indicate the standard deviation variability between individual ~~methane~~ transect $Q_{methane}$ ~~estimat~~fluxes.

4.2 Discussion

Figure 13 shows that there is a large disparity between $Q_{methane}$ estimates for individual transects, with a ±56% standard deviation variability.~~;~~ This variability~~which~~ is primarily due to differing turbulent patterns between methane and acetylene plume dispersion, partially caused by a suboptimal acetylene release location (discussed below). This emphasises the importance of conducting a sufficient number of transects to average over this variability, representative of the true emission flux. Although an aspect of calculated $Q_{methane}$ variability may be due to variability in true landfill methane emissions (which is a limitation of this work), this is expected to be relatively small over the limited sampling window (less than 3 hours). Landfill emissions are relatively consistent in the absence of abrupt environmental or operational changes. Thus, a constant true landfill $Q_{methane}$~~methane emission flux~~ value is assumed for all transects, with observed $Q_{methane}$ variability between transects driven by limitations in sampling and the nature of the tracer release (discussed below). $Q_{methane}$ for transect 13 was particularly low; **Fig. 12** (f) shows that this was due to a disproportionately narrow methane plume compared to a large acetylene plume. If the methane and acetylene plume were to share better spatial overlap, this issue would likely diminish, as both methane and acetylene plumes would be equally small at the time and location of measurement. Transect 20 ~~is~~ similarly result~~ed~~s in a low $Q_{methane}$, where a small methane plume was detected. ~~Conversely, transect 13 resulted in a small $Q_{methane}$ due to a large acetylene plume.~~ Transect 6 resulted in the largest $Q_{methane}$ due to a large methane plume. However, transect 7, which included the largest [CH_4] measurement (of the fourteen successful transects) did not result in such a high $Q_{methane}$ due to the accompanied detection of a substantially sized acetylene plume.

Previous studies have shown that tracer poor localisation with the methane emission source can cause $Q_{methane}$ variability (Mønster *et al.*, 2014, Yver Kwok *et al.*, 2015a, Ars *et al.*, 2017), as observed across the fourteen transect~~s~~ $Q_{methane}$ valu~~flux~~es presented here (see **Fig. 13**), resulting in a poor methane and acetylene plume overlap (see **Fig. 12**). Good tracer and methane source co-location is essential for accurate tracer-based fluxes (Delre *et al.*, 2018, Fredenslund *et al.*, 2019, Lui *et al.*, 2024). This ensures good mixing of the entire tracer plume with the methane plume (Matacchiera *et al.*, 2019) with identical dispersion (Johnson *et al.*, 1994, Lamb *et al.*, 1995, Daube *et al.*, 2019, Mønster *et al.*, 2019), such that ~~even~~ a mole fraction ratio at any single point is capable of yielding~~s~~ an accurate emission flux (Omara *et al.*, 2016, Ars *et al.*, 2017). A large disperse methane emission facility such as a landfill site may require multiple acetylene release points for improved plume overlap, such that the individual acetylene plumes overlap into a larger overall acetylene plume more representative of the shape of the complex methane emission plume emanating from the complex heterogenous surface emission source (Scheutz and Fredenslund, 2019, Matacchiera *et al.*, 2019, Mønster *et al.*, 2019, Vechi *et al.*, 2022). Yet, organising an acetylene release from other central locations at our landfill study site was challenging, especially from over active waste. Authorisation was secured many months in advance, making short term on-site changes difficult to implement. Furthermore, the ideal tracer release location can be

750 unique to each site (Matacchiera *et al.*, 2019), making it difficult to anticipate. Tracer localisation issues can be addressed by using a hybrid approach such as that of Ars *et al.* (2017), which combined tracer-based fluxes with a statistical inversion and an atmospheric transport model, for significantly improved overall flux estimates despite poor tracer localisation.

In conjunction with acetylene release location, good downwind positioning is essential for good plume mixing and overlap (Scheutz *et al.*, 2011, Daube *et al.*, 2019), to allow sufficient distance between the sources and the sampling location (Galle *et*
755 *al.*, 2001, Feitz *et al.*, 2018), so the full extent of the emission plume is captured (Mønster *et al.*, 2015, Delre *et al.*, 2018). Tracer-based fluxes are fundamentally limited to locations with downwind site access (Bell *et al.*, 2017). Yet our study had limited sampling options, with only one near-site downwind sampling road. For plumes that do not perfectly overlap (as in this study), integrating along the sampling road requires the road to be straight and perpendicular to wind direction (Yacovitch *et al.*, 2017), to avoid the methane and acetylene plumes being detected at different distances (Ars *et al.*, 2017). Measurements
760 closer to the site have a higher mole fraction with respect to the plane perpendicular to wind direction. But if the sampling road is nearly straight and perpendicular to wind direction (assumed here), the importance of these errors declines. In addition, sampling a sufficient distance from the source can reduce potential complication~~issue~~s due to poor tracer co-location with the source, as the two plumes have more time to mix (Fredenslund *et al.*, 2019).

Although a perfectly co-located acetylene release yields ideal $Q_{methane}$ estimates, it is also possible to derive $Q_{methane}$ if the
765 acetylene source is slightly offset from the methane source (Mønster *et al.*, 2014), as in this study. In such a scenario, the two plumes will be detected at different downwind locations (Ars *et al.*, 2017), but similar ~~plume dispersion~~turbulent conditions allow for similar plume dispersions ~~the ratio between these two integrated plumes to yield a flux~~. Yet this requires the two sources to be an equal distance from the sampling road, perpendicular to wind direction (Mønster *et al.*, 2014, Ars *et al.*, 2017, Daube *et al.*, 2019). It also requires identical wind conditions for the duration of each transect. Otherwise, the methane and
770 acetylene plumes may have dispersed under different conditions upon detection, resulting in lower mole fraction measurements during higher winds and *vice versa*. A similar amount of information is also required from each plume (Delre *et al.*, 2018), which was achieved in this work by interpolating [CH$_4$] measurements to the lower (Picaro G2203 [C$_2$H$_2$]) timestamp, thereby avoiding the contentious practice of gap filling. Although it is difficult to perfectly satisfy all above conditions, getting close enough can yield acceptable $Q_{methane}$ estimates.

775 Our [CH$_4$] interpolation approach ensured that each [C$_2$H$_2$] measurement had a corresponding spatiotemporal [CH$_4$] measurement. This allowed all measurements to be integrated as a function of distance along the sampling road, using the summation approach given by Eq. (**4**). An alternative integration approach is to continuously model the emission plumes as a function of distance, for analytical integration rather than summation (Fredenslund *et al.*, 2019), although this requires a sufficient sampling density to characterise plume shape (Delre *et al.*, 2018). This latter method would be challenging with the
780 Picarro G2203 instrument used in this work due to its irregular [C$_2$H$_2$]$_r$ sampling frequency, resulting in large gaps on plume dispersion information from downwind transects, with a maximum measurement time gap of 13 s. Interpolating the higher

frequency LI-COR LI-7810 [CH$_4$] measurements to the lower frequency Picarro G2203 [C$_2$H$_2$] timestamp mirrored this data loss in our summation integration (Eq. (4)). The average ~~measur~~observed 0.24~~(0.3±0.1)~~ Hz [C$_2$H$_2$] sampling frequency of the Picarro G2203 is lower than 0.5 Hz proposed by the manufacturer (Picarro, Inc., 2015). This may be due to the age and irregular operation of this specific Picarro G2203 gas analyser, which was manufactured in September 2015. It is important to state that the Picarro G2203 used in this study experienced some spectral fitting issues in the past~~.~~, which~~These~~ were resolved following manufacturer support. However, this may have inadvertently resulted in the irregular low sampling frequency as a residual unresolved issue. During a previous testing campaign, we experienced instrument failure during excessive acetylene exposure, which may explain this effect, although we cannot be certain. The slow sampling rate may also be associated with the unusual behaviour observed when sampling wet air, with [H$_2$O]$_r$ peaks and unpredictable [C$_2$H$_2$]$_r$ response, as described in **Sect. 2**.

At the minimum 0.24 Hz sampling frequency of the Picarro G2203 tested in this work, a 0.24 Hz σ_A of ±0.0863 ppb was derived at an [C$_2$H$_2$] of 10.1 ppb. When deriving tracer-based fluxes, it is important to evaluate the magnitude of peak mole fraction enhancements above instrumental noise (which can be characterised by σ_A) of any gas analyser, to ensure that the plume is detectable and can be characterised when subtracted from the background mole fraction level (Yver Kwok *et al.*, 2015a, Ars *et al.*, 2017, Yacovitch *et al.*, 2017, Delre *et al.*, 2018, Fredenslund *et al.*, 2019). The average [C$_2$H$_2$] peak height was (15±3) ppb for the fourteen useable transects in this study. This is far larger than the 0.24 Hz σ_A at an [C$_2$H$_2$] of 10.1 ppb, allowing it to be concluded that the $Q_{acetylene}$ level was sufficiently high and downwind sampling distance was sufficiently close to the source to detect acetylene emission plumes with a sufficiently high [C$_2$H$_2$] resolution.

Drift in calibration coefficients is also an important consideration for [C$_2$H$_2$] measurements used to derive $Q_{methane}$. In this study, the sampling campaign was conducted in February 2024 and [C$_2$H$_2$]$_r$ calibration coefficients were derived in October 2024. This assumes that Picarro G2203 [C$_2$H$_2$]$_r$ measurement performance did not significantly drift during this time window and in different sampling conditions (*i.e.* pressure and temperature), which is based on the stability of other Picarro instruments used to measure methane and carbon dioxide (Crosson, 2008, Yver Kwok *et al.*, 2015b, Gomez-Pelaez *et al.*, 2019, Yver-Kwok *et al.*, 2021). A future investigation on the stability Picarro G2203 [C$_2$H$_2$]$_r$ calibration coefficients would be useful to confirm this.

The [C$_2$H$_2$]$_r$ measurement response of the Picarro G2203 tested in this work was calibrated by diluting gas from an acetylene calibration cylinder. Methane served as a proxy gas to indicate the level of dilution achieved at each MFC blending step, by diluting gas from a methane calibration cylinder in the exact same way. Thus, any potential MFC blending errors should cancel out in this approach. Yet, there is a ±3% ~~[C$_2$H$_2$]~~uncertainty in the declared [C$_2$H$_2$] for the acetylene calibration cylinder and a ±0.5% uncertainty in the declared [CH$_4$] for the methane calibration cylinder, which are~~is a~~ limiting factors in this method, as acetylene calibration depends on these cylinder mole fractions to be known. We show that the Picarro G2203 acetylene calibration gain factor could take a range of between 0.911 and 0.977, assuming these cylinder uncertainties to have a worst-case impact in our [C$_2$H$_2$]$_r$ calibration procedure, as described in **Sect. S5** of the **Supplement**. This translates to a 10 ppb

[C$_2$H$_2$]$_r$ measurement resulting in an extreme [C$_2$H$_2$] range of between 8.96 ppb and 9.61 ppb. Thus [C$_2$H$_2$] is consistently lower than [C$_2$H$_2$]$_r$, despite the calibration uncertainty induced due to calibration cylinder uncertainties. Fredenslund *et al.* (2019) propose that uncertainty in ~~calibration~~ mole fraction calibration can be treated as a random uncertainty in overall $Q_{methane}$~~flux~~ estimates, which may be a useful approach ~~(given as 8%~~ in ~~their study). Perhaps such an~~overall uncertainty budgeting~~should instead be treated as a bias, as a poorly calibrated instrument will consistently bias flux estimates in one direction. Nevertheless, the cylinder mole fraction uncertainty is small in this work, compared to the correction induced from the derived calibration which reduces a 10 ppb [C$_2$H$_2$]$_r$ measurement down to 9.29 ppb [C$_2$H$_2$].~~

Yet it is concerning that the Picarro G2203 reports unstable [C$_2$H$_2$]$_r$ measurements when sampling at low (but non-zero) [C$_2$H$_2$] levels, with a maximum stable [C$_2$H$_2$] level of 1.16 ppb observed during testing. In this low [C$_2$H$_2$] range, Picarro G2203 [C$_2$H$_2$]$_r$ measurements occasionally resolved to the [C$_2$H$_2$]$_r$ level observed at 0 ppb [C$_2$H$_2$]. This means that any [C$_2$H$_2$]$_r$ measurement made at below 1.38 ppb bears some uncertainty, as it could correspond to any [C$_2$H$_2$] level between 0 ppb and 1.16 ppb [C$_2$H$_2$], although this upper uncertainty limit may be reduced slightly with further calibration testing. In this work, it was assumed that [C$_2$H$_2$]$_0$ in ambient air is 0 ppb. Therefore, measurements made away from an observed acetylene plume peak were assumed to equal 0 ppb [C$_2$H$_2$], with the key uncertainty occurring at the edges of the observed plume, which were also fixed to 0 ppb [C$_2$H$_2$] in this work. This was dealt with by additionally fixing some [CH$_4$] measurements (below [CH$_4$]$_{threshold}$) from each transect to [CH$_4$]$_0$, to avoid biasing $Q_{methane}$ results. Thus, a subset of both [C$_2$H$_2$] and [CH$_4$] measurements from each transect were forced to their corresponding background levels.

~~When deriving tracer-based fluxes, it is also important to evaluate the magnitude of peak mole fraction enhancements above instrumental noise, to ensure that the plume is detectable and can be characterised when subtracted from the background mole fraction level (Yver Kwok *et al.*, 2015, Ars *et al.*, 2017, Yacovitch *et al.*, 2017, Delre *et al.*, 2018, Fredenslund *et al.*, 2019). The average [C$_2$H$_2$] peak height of (15±3) ppb for the fourteen useable transects is far superior than the 0.24 Hz σ_A of ±0.0863 ppb at 10.1 ppb [C$_2$H$_2$]. Thus, we can conclude that the acetylene release emission flux was sufficiently high and downwind sampling distance was sufficiently close to the source to detect acetylene emission plumes with a sufficiently high [C$_2$H$_2$] resolution.~~

As a conseque~~The $Q_{methane}$ results presented in this work emphasise the importa~~nce of ~~calibrating all gas mole fraction measurements, even th~~ose ~~of a tracer gas. To our knowledge, a small number of previous studies using the Picarro G2203 have tested its [C$_2$H$_2$]$_r$ measurement response (Mønster *et al.*, 2014, Omara *et al.*, 2016), with no previous studies demonstrating a~~ calibration procedures for the~~with which to correct~~ Picarro G2203 ~~[C$_2$H$_2$]$_r$ measurements.~~ used i~~I~~n this study, us~~e of~~ing raw uncalibrated [C$_2$H$_2$]$_r$ measurements as Eq. (**4**) input resulted in $Q_{methane}$ estimates that were consistently lower than corresponding estimates using calibrated [C$_2$H$_2$] measurements, with an average underestimation of 7.6%. This is a key outcome of this study. This approximately 8% underestimation principally occurs due to the use of calibrated [C$_2$H$_2$] measurements. Yet, in theory, a 0.94 calibration gain factor for acetylene would result in exactly 6% $Q_{methane}$ underestimation

using $[C_2H_2]_r$ instead of $[C_2H_2]$ as Eq. (4) input. Any gain factor applied to the denominator of Eq. (4) is inversely proportional to $Q_{methane}$. However, an average underestimation of approximately 8% was instead observed in this study for a number of reasons. Setting all $[C_2H_2]$ measurements below 1.16 ppb $[CH_4]$ to 0 ppb and thus, applying a $[CH_4]_{threshold}$ to $[CH_4]$ measurements to account for this (as described above) both effect $Q_{methane}$ estimation. These two effects are influenced by the location and magnitude of mole fraction measurements made during each specific transect. Additionally, the $[C_2H_2]_r$ calibration includes a small offset correction (−0.147 ppb) which also influences $Q_{methane}$ estimation. These combined effects result in an average $Q_{methane}$ underestimation of approximately 8% from the fourteen transects in this study, rather than 6%, although a different level of $Q_{methane}$ underestimation was observed for each unique transect due to the different influence of the aforementioned effects. Therefore, while we derived an average $Q_{methane}$ bias of approximately −8% from a limited number of transects, in theory, an infinite number of transects may further refine this average bias value, causing this value to change slightly. Nevertheless, a similar bias is expected for other studies conducted in similar sampling conditions, using the Picarro G2203 gas analyser tested in this work.

The disparity between $Q_{methane}$ results derived from calibrated measurements versus uncalibrated tracer mole fraction measurements presented in this work emphasises the importance of calibrating all gas mole fraction measurements, even those of a tracer gas. To our knowledge, a small number of previous studies using the Picarro G2203 have tested its $[C_2H_2]_r$ measurement response (Mønster *et al.*, 2014, Omara *et al.*, 2016), with no previous studies demonstrating a calibration with which to correct Picarro G2203 $[C_2H_2]_r$ measurements. Each acetylene gas analyser requires independent characterisation and calibration. In addition, different Picarro G2203 instruments may perform differently when calibrated, resulting in a different influence on $Q_{methane}$ bias, which would need to be evaluated in future work.

Various previous studies have derived tracer-based fluxes downwind of controlled tracer releases, reporting various uncertainty ranges (Mønster *et al.*, 2014, Feitz *et al.*, 2018). For example, Ars *et al.* (2017) reported a tracer-based methane flux uncertainty of +14% for a controlled tracer release that was perfectly co-located with the methane emission source, although each tracer release study is unique ~~and~~can cannot be compared directly (for example, higher tracer release rates can result in a lower uncertainty). Liu *et al.* (2024) reported an average tracer-based error of 19% compared to known emission fluxes from thirteen integrated transects. Fredenslund *et al.* (2019) conducted an uncertainty budget for their tracer-based flux approach, with an overall error of 15%. Yet the overall uncertainty from these previous studies is generally given as a random uncertainty and does not distinguish between systemic emission bias due to lack of tracer gas calibration and other random methodological errors. This bias may be an important contributory factor within the overall uncertainty of tracer-based flux estimates. For example, consistently using $[C_2H_2]_r$ measurements from our Picarro G2203 would consistently underestimate Eq. (4) $Q_{methane}$; this is more concerning than random methodical uncertainties which, should cancel each other out over a sufficiently large sampling average. Such biases may be propagated which may influence our understanding of the importance of certain facility-scale emission sources contributing towards the global methane budget.

5. Conclusions

The first detailed characterisation ~~and calibration~~ of [C₂H₂]ᵣ~~acetylene~~ measurements made by the Picarro G2203 gas analyser is presented. Initially, ~~water response was tested. This showed that characterising~~ [C₂H₂]ᵣ characterisation was attempted at different~~response as a function of~~ [H₂O] ~~is unfeasible~~levels, but ~~due to an inconsistent~~ [C₂H₂]ᵣ measurements were found to be noisy and unpredictable in the presence of water~~response~~. Furthermore, [H₂O]ᵣ measurements were observed~~appear~~ to episodically erroneously spike at low (but non-zero) [H₂O] levels~~, making any such water characterisation of [C₂H₂]ᵣ response prohibitive~~. For this reason~~Instead~~, [C₂H₂]ᵣ calibration was conduct~~haracteris~~ed in dry conditions. ~~As there are no readily available acetylene gas standards,~~This calibration was performed by diluting gas from an acetylene calibration cylinder (containing an [C₂H₂] of 10 180 ppb ~~[C₂H₂]~~) with compressed ambient air~~was diluted~~. Th~~e~~o quantit~~f~~y ~~the level~~ of acetylene in each~~dilution, methane was used as a proxy~~ gas blend was inferred from [CH₄] measurements made when~~, by first~~ diluting gas from a methane calibration cylinder (with a [CH₄] of 995.4 ppm) in the exact same way~~containing methane~~. ~~The observed~~Accurate [CH₄] measurements~~level~~ w~~ere~~as compared to ~~the~~ predicted [CH₄] level~~s~~ to characterise~~ascertain the~~ MFC blending efficacy, thereby yielding~~and quantify the correction required to obtain the true mole fraction in the gas blend. This allowed~~ accurate [C₂H₂] calibration reference standards~~to be derived, despite systematic uncertainties in the blending method, by conducting the same dilution steps but with the acetylene calibration cylinder in place of the methane calibration cylinder~~. During calibration testing, it was observed that [C₂H₂]ᵣ measurements were unstable and erratic at [C₂H₂] levels of below 1.16 ppb. Therefore~~is yielded~~ a linear calibration fit with a lower [C₂H₂] limit of 1.16 ppb was derived, yielding a multiplicative [C₂H₂]ᵣ correction ~~gain~~ factor ~~with which to correct [C₂H₂]ᵣ~~ of 0.94~~, although this is only valid above 1.16 ppb [C₂H₂], below which unstable [C₂H₂]ᵣ measurements were observed~~. As an a~~dditional~~ly, $\sigma_A{}^2$ test~~ing yielded,~~ a 0.24 Hz σ_A of ±0.0863 ppb ~~was derived~~ at an [C₂H₂] of approximately 10 ppb ~~[C₂H₂]~~, ~~which~~ represent~~ing~~s the amount by which [C₂H₂] is expected to vary between ~~each~~ consecutive measurement~~s~~. Th~~is~~e highlight~~emphasise~~s the stability of the ~~Picarro G2203~~ [C₂H₂]ᵣ measurement stability. It is important to emphasise that these results are specific to the Picarro G2203 gas analyser tested in this work; a different instrument may exhibit different behaviour~~The protocols used here can be applied to other gas analysers, especially in the absence of reference gas standards~~.

The importance of calibrating [C₂H₂]ᵣ measurements made by our~~same~~ Picarro G2203 gas analyser was evaluated in the context~~used to sample downwind~~ of using~~a controlled~~ acetylene ~~release alongside a LI-COR LI7810 gas analyser measuring [CH₄]. The acetylene release was conducted from within an active landfill site which was emitting~~as a tracer gas for methane. A~~cetylene was released with a fixed $Q_{acetylene}$ ~~of~~ (0.2~~3~~942 g s⁻¹) from a landfill site. ~~was measured by an acetylene flow meter, using a logging computer to automatically record $Q_{acetylene}$.~~ The Picarro G2203 and a separate methane gas analyser sampled during~~A vehicle conducted~~ twenty ground-level downwind transects, where all gas entering the Picarro G2203 was dried. ~~of which fourteen could be used; s~~Six transects were discarded as~~recorded features containing~~ [C₂H₂]ᵣ measurements of less than −0.5 ppb were observed, probably due to spectral fitting issues in response to a sharp [C₂H₂] increase~~, which the Picarro G2203 probably failed to spectrally fit on first instance~~. [CH₄]~~Calibrated~~ Picarro G2203 [C₂H₂] measurements were ~~used in~~

combination with corresponding LI-COR LI-7810 $[CH_4]$ measurements ~~(~~interpolated to the lower Picarro G2203 $[C_2H_2]_r$ timestamp~~) to derive a landfill methane emission flux. As all~~Yet, there was no certainty on the magnitude of $[C_2H_2]_r$ measurements ~~of~~ below 1.38 ppb (corresponding to a $[C_2H_2]$ of 1.16 ppb); thus, all such measurements were fixed to ~~0 ppb~~ the $[C_2H_2]_0$ of 0 ppb. To account for th~~ise calibrated dataset, a proportion of~~ $[C_2H_2]_r$ threshold, all $[CH_4]$ measurements below a $[CH_4]_{threshold}$ value w~~ereas set~~as ~~also fixed~~ to $[CH_4]_0$ for each transect; this step is essential to avoid forcing data points from the acetylene plume to $[C_2H_2]_0$ without applying a similar effect to the methane plume.~~overall flux bias during $Q_{methane}$ calculations.~~

$Q_{methane}$ estimates were derived for each transect using the ratio between the integrated methane plume and integrated acetylene plume, with both plumes integrated as a function of distance along the sampling road. Th~~is~~e resulted in an average measured landfill $Q_{methane}$ for the fourteen successful transects of (17.3 ± 9.6) g s^{-1} when~~derived~~ using calibrated ~~Picarro G2203~~ $[C_2H_2]$ measurements ~~was 17.3 g s^{-1},~~ (with $[C_2H_2]$ less than 1.16 ppb fixed to 0 ppb) and when applying a $[CH_4]_{threshold}$~~with a standard deviation variability between the fourteen successful flux estimates of ±9.6 g s^{-1}. This large variability can be attributed to the positioning of the source and downwind sampling positioning. The acetylene release point was not perfectly co-located with the centre of the methane source; successfully achieving this is challenging in a complex environment such a landfill site. This manifested itself through methane and acetylene plumes which~~ that did not perfectly overlap on a downwind sampling plane. ~~Another factor was the slow $[C_2H_2]_r$ sampling frequency, with gaps of up to 13 s leading to information of the downwind sampling plumes being lost. A key outcome from this study was the derivation of~~However, conducing the same flux~~es~~ method but using uncalibrated raw ~~Picarro G2203~~ $[C_2H_2]_r$ with no applied $[CH_4]_{threshold}$ resulted in~~measurements in place of calibrated $[C_2H_2]$, which yielded~~ a ~~lower~~ $Q_{methane}$ of (16.0 ± 8.6) g s^{-1}, which corresponds to approximately 8% underestimation. This negative bias is a direct effect of failure to calibrate the Picarro G2203, although applying a 1.16 ppm $[C_2H_2]$ threshold and $[CH_4]_{threshold}$ influences $Q_{methane}$ underestimation magnitude for each individual transect (these effects average out over a sufficient number of transects). Although this approximately 8~~7.6~~% underestimation ~~(compared to $Q_{methane}$ derived using calibrated $[C_2H_2]$)~~ is smaller than $Q_{methane}$~~the~~ variability between individual transect~~flux estimate~~s, ~~it is possible to reduce~~ the~~e~~ $\pm$56% random ~~flux~~ variability can be reduced by~~with~~ improve~~ing~~~~ments in~~ the acetylene release methodology, for example by optimising the release location, with improved downwind sampling, sampling during better winds, conducting multiple acetylene releases or releasing acetylene at a higher ~~rate~~$Q_{acetylene}$. By contrast, the bias induced due to a lack of calibration is persistent and cannot be reduced by changing field sampling conditions. This therefore emphasises the importance of calibrating acetylene gas analysers used to derive tracer-based $Q_{methane}$~~methane~~ estimat~~flux~~es. Failure to do so could result in persistent biases in tracer-based $Q_{methane}$~~flux~~ estimates and hence, a biased understanding of the contribution of facility-~~ ~~scale methane sources towards the overall global methane budget.

Data availability

All data during laboratory testing and the field campaign will be published on a public repository upon final publication of this manuscript.

Author contributions

AS conducted laboratory characterisation testing of the Picarro G2203, with support from OL, LL and CP. CY and OL arranged the supply of gas cylinders. AS and OL devised the acetylene calibration methodology. AS, TD and ML conducted the field sampling campaign. EE, CR and MT arranged for field site access. AS designed all field logging systems. AS and PK devised the emission flux quantification methodology, with support from GB. AS conducted all data analysis. AS wrote an initial draft of the manuscript which was revised by GB, OL, PK, PC, CY, TD and EE. PC, OL, GB, EE and CR organised funding for this work.

Competing interests

The authors declare that they have no conflict of interest.

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