



# Explicit stochastic advection algorithms for the regional scale particle-resolved atmospheric aerosol model WRF-PartMC (v1.0)

Jeffrey H. Curtis<sup>1,2</sup>, Nicole Riemer<sup>1</sup>, and Matthew West<sup>2</sup>

<sup>1</sup>Department of Atmospheric Sciences, University of Illinois at Urbana-Champaign, 1301 W. Green St, Urbana, IL 61801, USA

<sup>2</sup>Department of Mechanical Science and Engineering, University of Illinois at Urbana-Champaign, 1206 W. Green St., Urbana, IL 61801, USA

**Correspondence:** Jeffrey H Curtis (jcurtis2@illinois.edu)

**Abstract.** This paper presents the development of a stochastic particle method to simulate advection in regional-scale models with a particle-resolving aerosol representation. The new method is based on finite volume discretizations with the flux terms interpreted as probabilities of particle transport between grid cells. We analyze the method in 1D and show that the stochastic particle sampling during transport injects energy at high spatial frequencies, which can be partially compensated for with the choice of a dissipative odd-order finite volume scheme. We then apply the stochastic third- and fifth-order advection algorithms with monotonic limiters in WRF-PartMC, using both idealized and realistic wind fields in 2D and 3D. In all cases we observe the expected convergence rates of the stochastic particle method to the finite volume solution as the number of computational particles is increased. This work enables the use of particle-based aerosol models on the regional scale.

## 1 Introduction

10 Aerosol particles influence the climate system as cloud condensation nuclei (CCN), as ice nucleating particles, and as scatterers and absorbers of radiation (Masson-Delmotte et al., 2021). Estimating the magnitude of the aerosol impact on climate requires not only the information of bulk aerosol composition and size distribution, but also the information of aerosol mixing state (Riemer et al., 2019), i.e., the way the chemical species are distributed across the particle population (Winkler, 1973). The aerosol mixing state can vary between a fully external mixture, where each particle contains only one chemical species which

15 can differ between different particles, and a fully internal mixture where each particle is composed of the same mixture of species. In reality, the mixing state is in between these two extreme cases (Bondy et al., 2018; O'Brien et al., 2015; Ye et al., 2018; Healy et al., 2014). Furthermore, many physical and chemical processes change the mixing state during the aerosol's lifetime in the atmosphere (Li et al., 2016). Representing these processes in models poses large challenges but is needed to predict the aerosol climate impact (Bauer et al., 2013; Fierce et al., 2017).

20 Atmospheric three-dimensional chemical transport models or Earth system models utilize a variety of aerosol representations that differ in their levels of detail. These can be categorized into bulk approaches (Koch, 2001; Tegen and Miller, 1998), modal modeling approaches (Whitby and McMurry, 1997), and sectional modeling approaches (Seigneur et al., 1986). These methods have in common that they do not fully resolve the mixing state of the aerosol, but instead use a priori assumptions.



For example, modal models assume that each mode is internally mixed, while different modes can differ in the set of species that they track. Sectional models capture the size dependence of aerosol composition but within one section only the average aerosol composition is known. These approaches can be refined by introducing additional modes (Bauer et al., 2008; Liu et al., 2012, 2016), additional one-dimensional sectional distributions (Jacobson, 2002; Zhang et al., 2014) or additional dimensions to the bin structure itself (Matsui et al., 2013; Matsui, 2016; Zhu et al., 2015; Ching et al., 2016), where each dimension represents one species or group of species. Comparing these more sophisticated types of models against versions that use more simplified mixing state representations shows that mixing state approximations impact the estimation of both optical and CCN properties and contribute to the structural and parametric model uncertainties. For example, Zhu et al. (2016) performed simulations with a sophisticated mixing-state-aware model (SCRAMS) for the region of Paris, France. Different mixing state treatments caused differences in aerosol water uptake, which propagated into differences in aerosol optical depths of up to 70%. Lee et al. (2016) carried out simulations with a mixing-state-resolving (source-oriented) version of WRF-Chem for the region of the Californian Central Valley. They found a decrease in the ratio of CCN to total aerosol number concentration from 94% with an internal mixture assumption to 80% with a more detailed source-oriented mixture. Furthermore, the range of uncertainties can depend on the degree to which mixing state is represented. This was shown by Matsui et al. (2018) who quantified the sensitivity of the present-day BC direct radiative effect due to uncertainties in emission size distributions. They found that the uncertainty is 5–7 times larger when the BC mixing state is sufficiently resolved compared to a simplified model representation where an internal mixture is assumed.

It is important to note that the storage requirements for multi-dimensional bin structures grow exponentially with the number of species (the curse of dimensionality). Therefore, in practice, the multi-dimensional bin approach is limited to two or three dimensions, whereas the composition space of the atmospheric aerosol contains tens or even hundreds of species. Hence, although this model approach carries more detail than 1D bin structures, it is still not able to resolve the mixing state fully.

In contrast to the above mentioned distribution-based methods, particle-resolved methods provide a different approach to representing the atmospheric aerosol (Riemer et al., 2009; Shima et al., 2009; Grabowski et al., 2019). They use a collection of discrete computational particles, where each particle can be thought of as a vector that stores the masses of each aerosol species and other particle attributes (e.g., information about particle shape or particle source) and that evolves over the course of the simulation. Aerosol mixing state is therefore intrinsically resolved and does not require any ad hoc assumptions. Furthermore, it is straight-forward to add more attributes to the particles as this does not result in an exponential increase of storage. Instead, it scales linearly with the number of particles. Particle methods are therefore beneficial for problems where high-dimensional data is involved as they break the curse of dimensionality.

In this paper we describe the development of stochastic advection algorithms that enable the particle-resolved aerosol model PartMC to be used on the regional scale, embedded within the Weather Research and Forecast model (WRF). This paper builds on previous work of developing the stochastic, particle-resolved PartMC-MOSAIC box model (Riemer et al., 2009; DeVille et al., 2011; Curtis et al., 2016; DeVille et al., 2019), and the one dimensional single-column model WRF-PartMC-MOSAIC-SCM (Curtis et al., 2017). These modeling tools have been used to investigate the black carbon aging process (Riemer et al., 2010; Fierce et al., 2015), to quantify the role of mixing state in determining CCN concentration (Ching et al.,



2012, 2016, 2017) and aerosol optical properties (Fierce et al., 2016; Yao et al., 2022), and to determine structural uncertainty  
60 in more approximate aerosol models (Fierce et al., 2017; Zheng et al., 2021).

The methods for particle transport due to turbulent diffusion described in Curtis et al. (2017) and for mean wind advection  
described in this paper are based on the idea that the movement of particles between grid cells is represented by stochastic  
sampling. Importantly, the particle position within the grid cell is not tracked. This concept is therefore distinct from the  
particle-based Lagrangian techniques in the cloud modeling community (Heus et al., 2010; Arabas et al., 2015; Grabowski  
65 et al., 2018). These methods are similar to ours in that they also explicitly simulate microphysical processes on a population  
of computational particles (called super-particles in the cloud physics community), each representing a large number of real  
particles. However, they are different in that they simulate transport by tracking the super-droplet positions within the Eulerian  
grid.

There are advantages and disadvantages to each method. First, stochastic methods for transport are computationally less  
70 expensive than tracking and updating particle position throughout the simulation. Second, a stochastic algorithm can be con-  
structed analogously to finite volume transport schemes used in numerical weather models and chemical transport models, as  
we will show in this paper. This is beneficial for direct comparisons of the aerosol representation, which is one of our main  
motivations for developing particle-resolved aerosol models on the regional scale. Third, stochastic methods are more easily  
implemented in models that rely on different numerical grid structures. However, stochastic transport algorithms have the dis-  
75 advantage of numerical diffusion similar to finite volume methods. This is in contrast to particle tracking methods that are  
inherently free of numerical diffusion.

The contribution of this paper is the development of stochastic transport algorithms for advection that remove the model-  
ing limitations of the single-column model (WRF-PartMC-MOSAIC-SCM) by enabling a fully three-dimensional model to  
allow particle-resolved simulations on the regional scale (WRF-PartMC). WRF-PartMC is a tool for error quantification and  
80 benchmarking of traditional chemistry-transport models (e.g., WRF-Chem or CMAQ) that apply simplified aerosol mixing  
state representation, without the advection schemes being a potential source of differences.

The paper is structured as follows. Section 2 develops the stochastic particle advection method. Section 3 analyzes a series of  
four numerical experiments of increasing complexity, ranging from simple one-dimensional test cases with constant, uniform  
wind fields to a simulation with complex terrain and evolving meteorological fields. Section 4 summarizes our work. See  
85 Table G1 for a list of symbols used throughout the paper.

## 2 Stochastic particle transport scheme

This section describes the spatial and temporal discretization of the advection equation and then explains the stochastic sam-  
pling algorithm for the use in particle-resolved models. We will present the detailed derivation for one spatial dimension.  
The generalization to three dimensions in space is straightforward and for brevity will not be explicitly written out, although  
90 see Sections 2.3 for notes on implementation details. The WRF-PartMC model was developed using WRFv3.9.1.1, coupled



with chemistry for gas scalar transport and PartMC-MOSAIC for gas and aerosol chemistry with an additional interface for simulating stochastic particle transport.

## 2.1 Spatial and temporal discretization

The one-dimensional advection equation of a scalar quantity with (number) concentration  $n(x, t)$  can be written as

$$95 \quad \frac{\partial n(x, t)}{\partial t} = -u \frac{\partial n(x, t)}{\partial x}, \quad (1)$$

where  $u > 0$  is the velocity of the advecting wind field (assumed to be constant in time and uniform in space here),  $x$  is the spatial coordinate, and  $t$  is time.

We discretize this equation spatially as

$$\frac{\partial n_i(t)}{\partial t} = -\frac{1}{\Delta x} (f_{i+\frac{1}{2}}(t) - f_{i-\frac{1}{2}}(t)), \quad (2)$$

100 where  $\Delta x$  is the grid spacing in the  $x$ -coordinate, and  $f_{i+\frac{1}{2}}(t)$  and  $f_{i-\frac{1}{2}}(t)$  are the fluxes through the right and left grid cell boundaries of grid cell  $i$  at time  $t$ , respectively, for  $i = 0, \dots, N_x - 1$ .

The fluxes can be spatially discretized to different orders, with the WRF schemes of orders 1 to 6 written as (Wicker and Skamarock, 2002; Shu, 2009):

$$f_{i-\frac{1}{2}}^{1st} = un_{i-1}, \quad (3)$$

$$105 \quad f_{i-\frac{1}{2}}^{2nd} = \frac{u}{2}(n_i + n_{i-1}), \quad (4)$$

$$f_{i-\frac{1}{2}}^{3rd} = \frac{u}{6}(2n_i + 5n_{i-1} - n_{i-2}), \quad (5)$$

$$f_{i-\frac{1}{2}}^{4th} = \frac{u}{12}(-n_{i+1} + 7n_i + 7n_{i-1} - n_{i-2}), \quad (6)$$

$$f_{i-\frac{1}{2}}^{5th} = \frac{u}{60}(-3n_{i+1} + 27n_i + 47n_{i-1} - 13n_{i-2} + 2n_{i-3}), \quad (7)$$

$$f_{i-\frac{1}{2}}^{6th} = \frac{u}{60}(n_{i+2} - 8n_{i+1} + 37n_i + 37n_{i-1} - 8n_{i-2} + n_{i-3}), \quad (8)$$

110 and similarly for the fluxes through the other boundary,  $f_{i+\frac{1}{2}}$ . We will explore the effect of using different orders of discretization in the context of stochastic particle-based advection in Sections 3.1 and 3.2.

For the temporal discretization, we use a 3rd-order Runge-Kutta method, analogous to the approach in WRF (Wicker and Skamarock, 2002), where the concentration at time  $\ell + 1$  is calculated from the values at time  $\ell$  as

$$n_i^\dagger = n_i^\ell - \frac{\Delta t}{3} \frac{1}{\Delta x} (f_{i+\frac{1}{2}}^\ell - f_{i-\frac{1}{2}}^\ell), \quad (9)$$

$$115 \quad n_i^{\dagger\dagger} = n_i^\ell - \frac{\Delta t}{2} \frac{1}{\Delta x} (f_{i+\frac{1}{2}}^\dagger - f_{i-\frac{1}{2}}^\dagger), \quad (10)$$

$$n_i^{\ell+1} = n_i^\ell - \Delta t \frac{1}{\Delta x} (f_{i+\frac{1}{2}}^{\dagger\dagger} - f_{i-\frac{1}{2}}^{\dagger\dagger}), \quad (11)$$

where  $\Delta t$  is the time step. The fluxes  $f_{i+\frac{1}{2}}^\dagger$ ,  $f_{i-\frac{1}{2}}^\dagger$ ,  $f_{i+\frac{1}{2}}^{\dagger\dagger}$  and  $f_{i-\frac{1}{2}}^{\dagger\dagger}$  are calculated as given in Eq. (3)–(8), using the concentrations  $n_i^\dagger$  and  $n_i^{\dagger\dagger}$ , respectively.



Next, we will show how the discretized equations defined above are translated to specify the probabilities of particles moving  
 120 between grid cells.

## 2.2 Stochastic sampling

To transform the method from Section 2.1 to a stochastic particle method, we consider a set of  $N_i^\ell$  particles in grid cell  $i$  at  
 time step  $\ell$ . In reality, each particle will have an exact spatial location with a well-defined  $x$  coordinate and will be moving  
 with constant velocity  $u$ . However, in our stochastic method we will not track this per-particle spatial location and instead only  
 125 track the set of particles in each grid cell. This is equivalent to the usual finite volume method of tracking the concentration  
 in each grid cell, except that we are now sampling the concentration with a finite set of particles, allowing us to capture the  
 high-dimensional variation in particle properties.

Note that the full WRF-PartMC model implementation explicitly tracks each particle in each grid cell so that it can store  
 additional information about each particle (e.g., particle diameter, chemical constituents, etc.). In the following exposition we  
 130 will not explicitly track the particles, but instead will only track the number of particles,  $N_i^\ell$ , in each grid cell. Section 2.4  
 contains further comments on translating the count-based scheme to a true per-particle method.

To advect the particles we relate the number of particles in each grid cell to the concentration in that grid cell, using

$$n_i^\ell = \frac{N_i^\ell}{V}, \quad (12)$$

where  $V$  is the computational sampling volume within each grid cell. We can think of  $V$  as controlling the “resolution” of the  
 135 particle sampling and it will generally be much smaller than the true grid cell volume.

Having computed the values of  $n_i^\ell$  for each grid cell, we then compute the finite volume fluxes  $f_{i+\frac{1}{2}}^{\dagger\dagger}$  through each boundary  
 from Eq. (11). This tells us that the average number of particles that should cross boundary  $i + \frac{1}{2}$  is

$$\bar{F}_{i+\frac{1}{2}}^\ell = V \frac{\Delta t}{\Delta x} f_{i+\frac{1}{2}}^{\dagger\dagger}. \quad (13)$$

We interpret this probabilistically to mean that each of the  $N_i^\ell$  particles has a probability of

$$140 \quad p_{i+\frac{1}{2}}^\ell = \frac{\bar{F}_{i+\frac{1}{2}}^\ell}{N_i^\ell} \quad (14)$$

of crossing the boundary and leaving grid cell  $i$ . We then sample the number of particles that actually cross the boundary using  
 a binomial distribution with  $N_i^\ell$  trials and probability  $p_{i+\frac{1}{2}}^\ell$ , to give the discrete particle flux across the boundary to be

$$F_{i+\frac{1}{2}}^\ell = \text{Binom}(N_i^\ell, p_{i+\frac{1}{2}}^\ell). \quad (15)$$

Finally, we update the number of particles in each grid cell according to

$$145 \quad N_i^{\ell+1} = N_i^\ell - F_{i+\frac{1}{2}}^\ell + F_{i-\frac{1}{2}}^\ell. \quad (16)$$

Note that this method obviously conserves the total number of discrete particles, because the  $F_{i+\frac{1}{2}}^\ell$  particles that leave grid  
 cell  $i$  will all be transferred to grid cell  $i + 1$ . In addition, because the mean of a binomial distribution is equal to the number



of trials times the probability of success, we see that the average value of  $N_i^1$  is exactly equal to  $Vn_i^1$  for the first time step. However, because the next time step will start from the stochastically sampled discrete value  $N_i^1$ , the average value of  $N_i^2$  will not be exactly equal to the average value of  $Vn_i^2$ .

### 2.3 Three-dimensional advection

The above derivation is for a one-dimensional domain, but the extension to three dimensions is straight forward. In three dimensions, we have a set of  $N_{i,j,k}^\ell$  particles in grid cell  $(i, j, k)$  at time step  $\ell$ . The fluxes are then defined as  $f_{i+\frac{1}{2},j,k}^\ell$  and  $f_{i,j+\frac{1}{2},k}^\ell$  and  $f_{i,j,k+\frac{1}{2}}^\ell$  for the fluxes through the three positive boundaries of grid cell  $(i, j, k)$ , respectively. The fluxes through the other boundaries are defined similarly. The fluxes are then computed from a 3D finite volume discretization, but with the concentrations  $n_i$  replaced by the number of particles  $N_{i,j,k}^\ell$ . This then yields probabilities of particles crossing each boundary using (14). However, we now have three different probabilities for each boundary, corresponding to the three different directions in which particles can move. We then sample the number of particles that move in each direction using a multinomial distribution with  $N_{i,j,k}^\ell$  trials and probabilities  $p_{i+\frac{1}{2},j,k}^\ell$ ,  $p_{i,j+\frac{1}{2},k}^\ell$ , and  $p_{i,j,k+\frac{1}{2}}^\ell$  for the three directions, respectively. See Curtis et al. (2017) for a detailed description of the multinomial sampling algorithm. Finally, the number of particles in each grid cell is updated according to Eq. (16).

### 2.4 Explicit tracking of individual particles

Much of the power of a particle-based aerosol model is the ability to track the chemical composition and potentially morphology of individual particles, as is done by the PartMC (Riemer et al., 2009) model, which explicitly tracks a set of particles  $\Pi_{i,j,k}^\ell$  in grid cell  $(i, j, k)$  at time step  $\ell$ . To apply the stochastic advection algorithm of Section 2.2 to such a case, the stochastic fluxes can be computed using the total number,  $N_{i,j,k}^\ell$ , of particles in each grid cell, to give  $F_{i+\frac{1}{2},j,k}^\ell$ ,  $F_{i,j+\frac{1}{2},k}^\ell$ , and  $F_{i,j,k+\frac{1}{2}}^\ell$  as the number of particles that will cross each boundary. However, rather than simply updating the particle counts using the fluxes, we uniformly randomly sample  $F_{i+\frac{1}{2},j,k}^\ell$  particles from the set  $\Pi_{i,j,k}^\ell$  to move across the boundary, and similarly for the other two directions. This approach is used in the WRF-PartMC model.

### 2.5 Monotonicity

It is advisable in WRF-Chem simulations to use monotonic, positive-definite advection schemes (Wang et al., 2009; Chapman et al., 2009). WRF advection schemes without limiters have the tendency to overshoot as well as locally produce unrealistically low values. This is particularly problematic for chemical variables that have strong gradients due to the heterogeneity of emissions. The host WRF model features only a fifth order scheme for monotonic limiters. However due to the high computational expense of WRF-PartMC and the required domain decomposition to adequately meet that expense, we implemented third-order advection with monotonic limiters in WRF. We focused on third and fifth order advection schemes because they combine good accuracy with some numerical diffusion at high spatial frequencies to suppress stochastic oscillations, as we will see in Sections 3.1 and 3.2.



## 2.6 Mixing ratio versus concentration

180 Many 3D atmospheric models such as WRF track the aerosol mixing ratio  $q$  (units of  $\#/kg$ ) rather than the number concentration  $n$  (units  $\#/m^3$ ) because this removes the need to adjust the tracer for changes in air density. However, the stochastic advection algorithm described above is based on the number concentration. In WRF-PartMC we convert the aerosol number concentration to a mass mixing ratio via  $q = n/\rho$ , compute mixing ratio fluxes using WRF's finite volume discretization, convert these back to number-concentration fluxes by multiplying by  $\rho$ , and then sample the stochastic particle transport  
185 with (14)–(16).

## 2.7 Variable sampling volumes and grid cell sizes

In Section 2.2 we assumed that the sampling volume  $V$  is a constant. However, in the WRF-PartMC model the sampling volume is allowed to vary in space and time. This is done by defining a set of  $V_{i,j,k}^\ell$  volumes in each grid cell  $(i, j, k)$  at time step  $\ell$ , and allows the “particle resolution” to be adaptive to increase the accuracy while minimizing the computational cost. In  
190 such simulations a target number of particles per grid cell,  $N_p$ , is chosen to be a fixed value and the sampling volume is then adapted using a halving/doubling procedure to maintain the actual number of particles per grid cell close to  $N_p$  (Riemer et al., 2009).

As described in detail in Curtis et al. (2017), the variable sampling volumes mean that the number of particles that move out of a grid cell (the “particle loss”) is no longer generally equal to the number of particles that move into the neighboring cell  
195 (the “particle gain”). Instead, if  $F_{i+\frac{1}{2},j,k}^\ell$  particles move out of grid cell  $(i, j, k)$ , then the number of particles that move into grid cell  $(i + 1, j, k)$  is scaled by the ratio of the sampling volumes. That is, the number of particles that move into grid cell  $(i + 1, j, k)$  is

$$F_{i+\frac{1}{2},j,k}^\ell \frac{V_{i+1,j,k}^\ell}{V_{i,j,k}^\ell}. \quad (17)$$

Similarly, if the grid cells have different physical volumes  $\text{Vol}_{i,j,k}^\ell$  then the above expression must be additional scaled by the  
200 ratio  $\text{Vol}_{i,j,k}^\ell/\text{Vol}_{i+1,j,k}^\ell$ . The advection algorithm in WRF-PartMC implements this scaling following the method in Curtis et al. (2017), which uses a variance-minimizing sampling algorithm that first samples the larger of the particle loss and gain terms and then subsamples from this to determine the other term.

## 2.8 Error metrics

To quantify the accuracy of the stochastic particle-resolved transport algorithm described above we use the relative root mean  
205 square error (RRMSE) between two solutions  $n$  and  $n'$  as given by

$$\text{RRMSE}(n, n') = \frac{\sqrt{\sum_i^{N_x} (n_i - n'_i)^2}}{\sqrt{\sum_i^{N_x} (n'_i)^2}}. \quad (18)$$





To determine the mean and confidence intervals for the RRMSE, we ran an ensemble of simulations with different random seeds for the stochastic sampling algorithm. The RRMSE was computed for each simulation run and then the overall mean and standard deviation were calculated, with the standard deviation being used to determine the 95% confidence interval for the RRMSE mean.

### 3 Numerical experiments

In this section we present numerical examples of increasing complexity and discuss their convergence properties as the number of computational particles increases. Sec. 3.1 presents a one-dimensional test case with a soft-hat initial condition advected by a constant, uniform wind velocity to quantify the convergence as the number of computational particles increases. Sec. 3.2 simplifies the 1D test case to a uniform initial condition to study how the order of the advection scheme impacts convergence. Sec. 3.3, presents an idealized two-dimensional test case for solid-body rotational flow developed within WRF-PartMC. Finally, Sec. 3.4, shows stochastic particle transport for a realistic model domain and with realistic and evolving meteorological fields as simulated by the WRF-PartMC model.

#### 3.1 One-dimensional test case: Soft hat advected by uniform wind

We begin with the 1D soft-hat test case from Wicker and Skamarock (2002), with initial condition

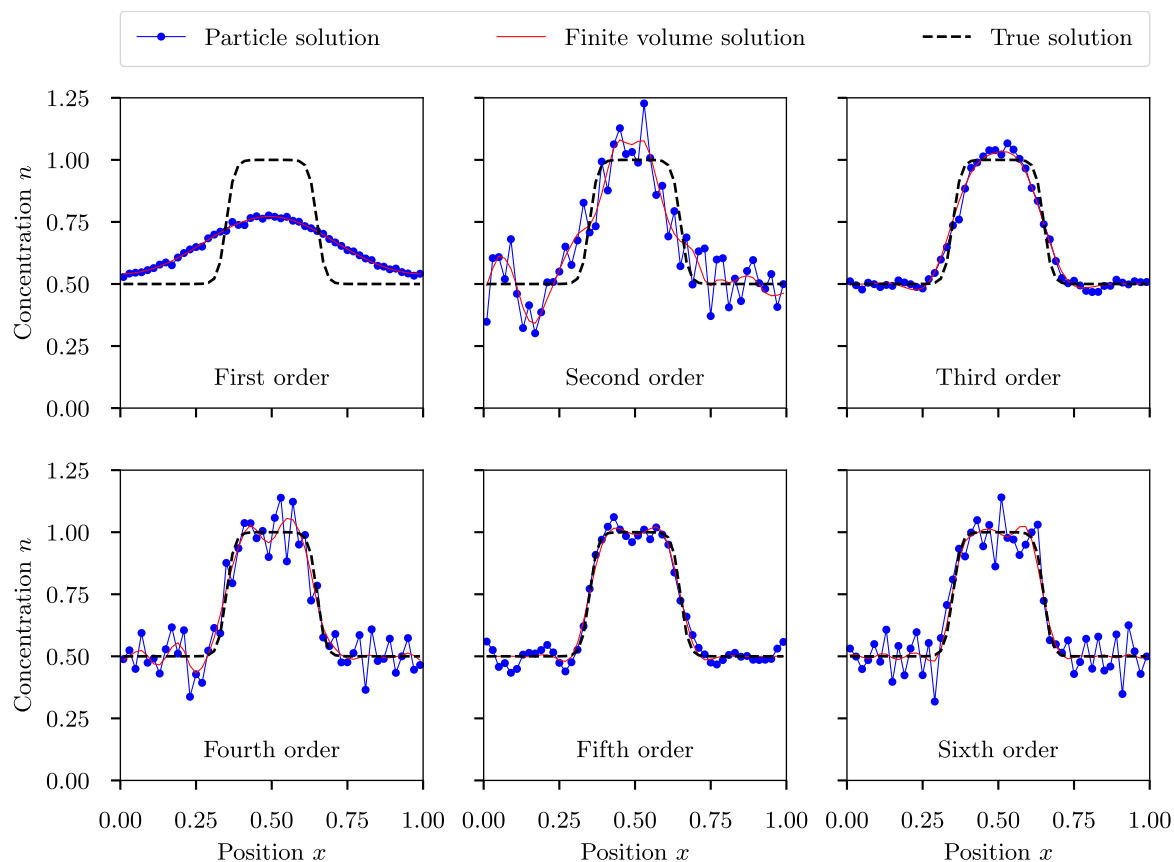
$$n(x, t = 0) = 0.5 + \frac{0.5}{1 + \exp^{80(|x-0.5|-0.15)}}, \quad (19)$$

on the periodic domain  $x \in [0, 1]$ . Eq. 19 was modified from the expression in Wicker and Skamarock (2002) to include a background concentration so that there are some particles everywhere throughout the domain. The uniform velocity field was  $u = 1$  (all quantities are taken as dimensionless here). For all presented results, the number of grid cells was  $N_x = 50$  and the time step was  $\Delta t = 0.008$ . The simulation duration was  $T = 2$ , giving two full revolutions of the domain.

Figure 1 shows the solution to the soft-hat problem after two revolutions ( $t = 2$ ) for the finite volume method and one ensemble member of the stochastic method. Considering the finite volume solutions, we observe that the even-order methods (2nd, 4th, 6th) produce more oscillatory solutions than the odd-order methods. This disparity between the even- and odd-order methods also occurs for the stochastic method, where the even-order solutions contain significantly more high-frequency noise than the odd-order solutions. We will analyze this phenomenon in more detail in Section 3.2.

We now turn to understanding the convergence of the stochastic particle method as the number of particles is increased. Figure 2(a) shows the ensemble mean error for the particle solution compared to the finite volume solutions for each order of advection, i.e., this is the error due to using a finite particle number but does not include any spatial discretization error as that is present for both the stochastic and finite volume methods. As the number of computational particles per grid cell,  $N_p$ , increased, the solution converged to the deterministic finite volume solution. The rate of convergence for these stochastic methods is expected to be  $\frac{1}{\sqrt{N_p}}$  due to the central limit theorem and is denoted by the dashed line with slope  $-\frac{1}{2}$ . The stochastic error is largest for the even-order methods and smallest for the first-order method. In Sec. 3.2 we will show that this is because

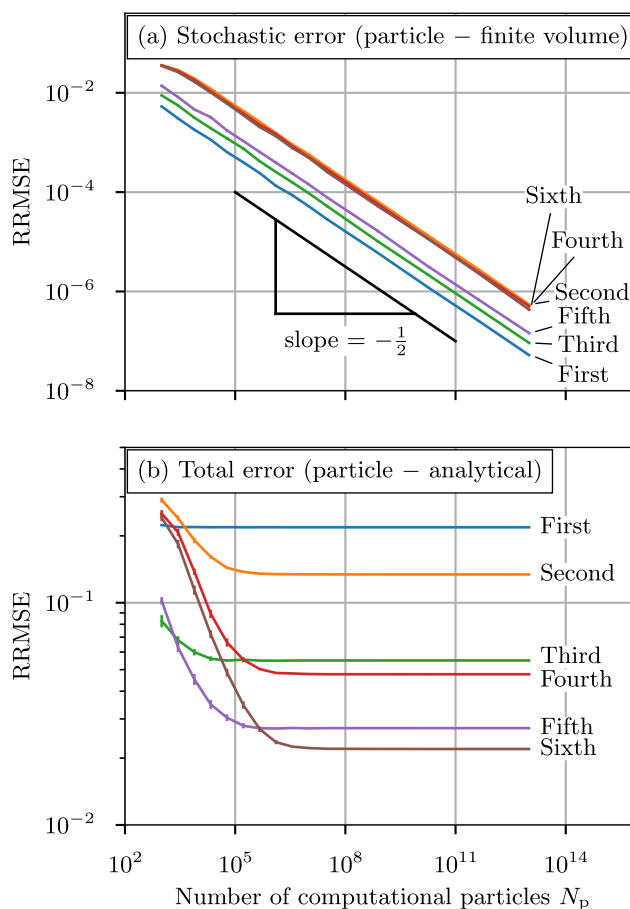




**Figure 1.** One dimensional soft-hat test case (Sec. 3.1): A single ensemble member of the stochastic solution is shown in blue for 1st to 6th order methods, the deterministic finite volume solution is represented by the solid red line, and the analytical solution is shown as a black dashed line. The stochastic solution was simulated using  $N_p = 10^4$  computational particles per grid cell.

the odd-order methods benefit from the damping of high frequency noise and the first-order method has the lowest stochastic error because it has the most damping.

240 Figure 2(b) shows the ensemble mean error for the particle solution compared to the analytical solution, i.e., the “total” error (finite volume error plus stochastic error). As the number of particles increases, the ensemble mean error approaches a constant value, which is the error due to the finite volume discretization. No matter how many computational particles are used, the total error cannot become smaller than the error introduced by the finite volume discretization. The finite volume error decreases in magnitude as the order of the advection method increases. For small values of  $N_p$ , the stochastic error dominates the total error. The odd-order methods (third and fifth order) have lower stochastic error than the even-order methods which results in  
 245 the total error converging to the finite volume error with fewer computational particles. In contrast, the first order method has such large finite volume error, shown with the poor comparison of the finite volume solution to the true solution in Fig. 1, and such low stochastic error, shown in Fig. 2, that the finite volume error dominates the total error immediately. In all cases the



**Figure 2.** One dimensional soft-hat test case (Sec. 3.1): (a) Relative root-mean square error (RRMSE) between the stochastic particle solution and the deterministic finite volume solution for 1st–6th order advection with varying number of computational particles. The dashed line shows the expected  $\frac{1}{\sqrt{N_p}}$  convergence rate. (b) Relative root-mean square error (RRMSE) between the particle solution and the analytical solution for 1st–6th order advection with varying number of computational particles per grid cell at  $T = 2$ . Error bars denote the 95% confidence interval as determined from an ensemble of 25 simulations.



finite volume error could also be reduced by decreasing the grid cell size, following the standard convergence analysis of finite  
250 volume methods (Durran, 2010).

In summary, these results show that the stochastic error of particle-resolved advection converges as expected with the rate of  
 $\frac{1}{\sqrt{N_p}}$ . Conservative even-order schemes exhibit high-frequency oscillations in the finite-volume solution that are compounded  
by high-frequency noise from the stochastic sampling. For the dissipative odd-order schemes, numerical diffusion damps the  
high-frequency oscillations, as will be shown in Sec. 3.2. We therefore recommend the use of dissipative (odd-order) advection  
255 schemes. We also note that the stochastic advection scheme will be especially useful in open domains where we have an outflow  
boundary condition. In this case, the artificial noise injected by the stochastic sampling will be advected out of the domain and  
will not accumulate.

### 3.2 One-dimensional test case: Uniform concentration advected by uniform wind

The difference observed in Fig. 1 between the even- and odd-order solutions is of course due to the amount of numerical  
260 dissipation in the methods, where the even-order methods are conservative, while the odd-order methods have numerical  
dissipation of energy at high spatial frequencies (see, e.g., Durran (2010, §§3.3.2–3.3.3)). To understand how this interacts  
with the stochastic particle solution we derived a simple explicit model for the power spectrum of the stochastic solution. The  
details of this derivation are given in Appendices C–E. Briefly, we considered the uniform initial condition

$$n(x, t = 0) = 1 \tag{20}$$

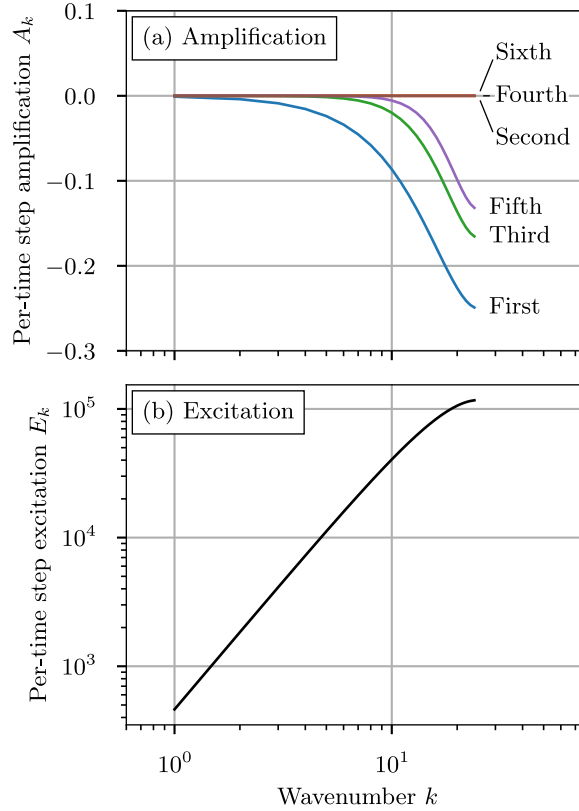
265 on the periodic domain  $x \in [0, 1]$  with the uniform velocity field  $u = 1$ . We discretized this with  $N_x = 50$  grid cells, a time  
step of  $\Delta t = 0.00125$ , and total time  $T = 2$  to give 1600 time steps for 2 revolutions. We used a computational volume of  
 $V = 10000$  which thus means the stochastic particle system started with  $N_p = 10000$  particles per grid cell.

The exact solution to this problem is clearly  $n(x, t) = 1$  for all  $x$  and  $t$ . However, as we will see, as the stochastic method  
moves particles from one grid cell to the next, it is sampling a per-grid random number that is uncorrelated between grid cells,  
270 and is thus injecting energy at high spatial frequencies. This energy is then dissipated by the numerical dissipation of the spatial  
discretization, if any, and the question is whether the dissipation can effectively control the energy injection. To answer this  
question we will derive a simple model for the power spectrum of the stochastic solution.

We start by writing  $\hat{n}_k$  for the discrete Fourier transform (DFT) of  $n_i$ , and recalling the classical fact that the power spectrum  
of the spatially-discretized system evolves according to

$$275 P_k^{\ell+1} = \exp(A_k) P_k^\ell, \tag{21}$$

where  $P_k^\ell = |\hat{n}_k^\ell|^2$  is the power at wavenumber  $k$  and time step  $\ell$ , and  $A_k$  is the amplification factor at wavenumber  $k$  (see  
Appendix A for details). Figure 3 shows the amplification factors for the different spatial discretizations. From this, we see  
that the even-order methods have an amplification factor of zero at all wavenumbers, meaning that these methods are exactly  
conservative. In contrast, the odd-order methods have negative amplification factors at higher wavenumbers, showing that these  
280 methods will dissipate high spatial frequency components.



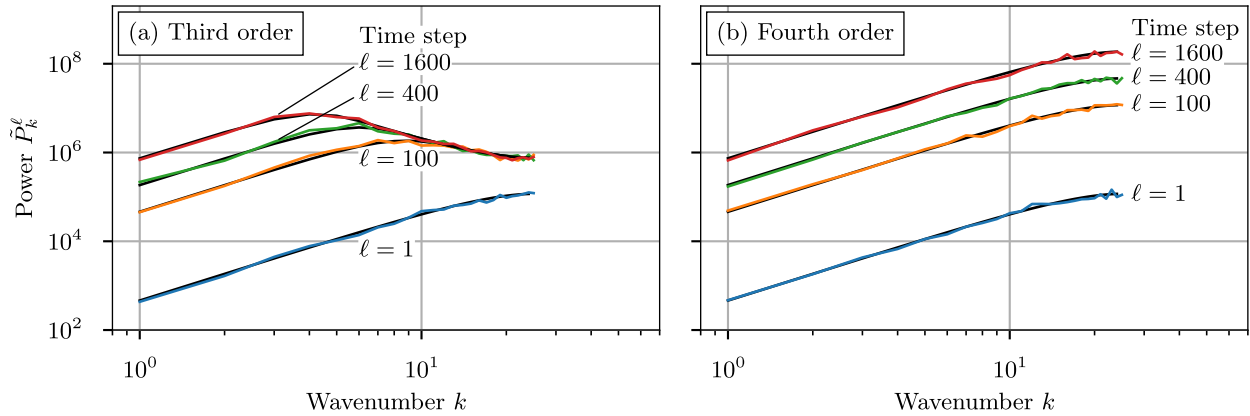
**Figure 3.** One dimensional uniform test case (Sec. 3.2): (a) Amplification factors,  $A_k$ , for the 1st to 6th order spatial discretizations. See Eq. (B8)–(B13) for details. (b) Excitation term,  $E_k$ . See Eq. (D12) for details.

To understand the interaction between the stochastic sampling and the spatial discretization dissipation, Appendix D derives a recurrence relation for the power spectrum of an approximation to the stochastic solution:

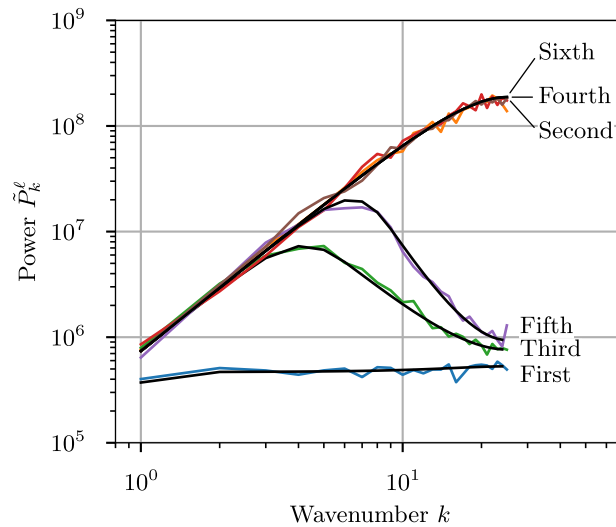
$$\tilde{P}_k^{\ell+1} = \exp(A_k)\tilde{P}_k^{\ell} + E_k, \quad (22)$$

where  $\tilde{P}_k^{\ell}$  is the power at wavenumber  $k$  and time step  $\ell$  of the approximate stochastic solution  $\tilde{N}$ ,  $A_k$  is the amplification factor of the spatial discretization, and  $E_k$  is a stochastic excitation term (see Appendix D for details). Figure 3(b) plots the excitation term and we see that it is injecting energy at higher wavenumbers, due to the uncorrelated random noise in each grid cell from the stochastic transport. By comparing panels (a) and (b) in Figure 3, we see that the negative amplification factors at high wavenumbers will tend to suppress the energy injection.

Figure 4 shows the power spectrum of the stochastic solution for third- and fourth-order advection after 1, 100, 400 and 1600 time steps, with the black lines showing the model prediction for the power spectrum (see Appendix E for details). Here we see the constant energy injection at high wavenumbers, with the fourth-order method steadily scaling up the power spectrum by the excitation term at each time step. In contrast, the third-order method has dissipation at higher wavenumbers which partially



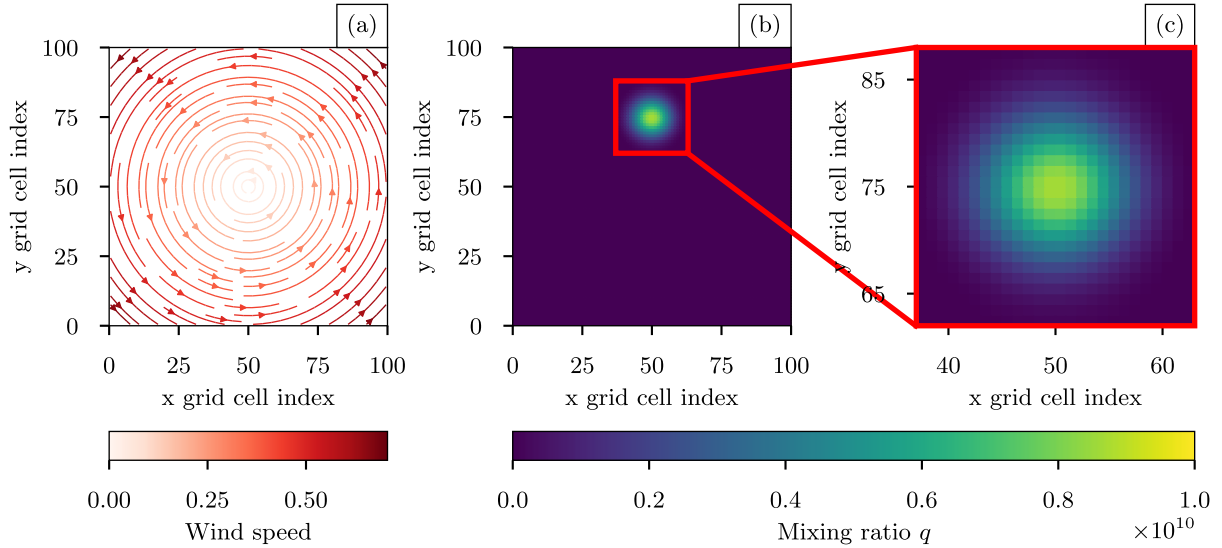
**Figure 4.** One dimensional uniform test case (Sec. 3.2): mean power spectra for third and fourth order advection methods after 1, 100, 400, and 1600 time steps. The overlaid black lines indicate the model prediction for each method at each time step. Each stochastic case was repeated 100 times to obtain the mean power spectra.



**Figure 5.** One dimensional uniform test case (Sec. 3.2): power spectra for 1st to 6th order advection methods after 1600 time steps (two full revolutions of the system). The overlaid black lines indicate the model predictions for each method.

suppresses the injected energy and eventually reaches an equilibrium. This serves to suppress the high-frequency noise in the solution and explains the difference between the even- and odd-order stochastic solutions in Figure 1.

295 This point is further emphasized in Figure 5 where all the stochastic methods are compared after 1600 time steps. The conservative even-order schemes all fall on the same curve, increasing in power at higher frequencies. For the dissipative odd-



**Figure 6.** Two dimensional test case (Sec. 3.3): (a) rotational wind field, (b) the true solution of the Gaussian cone after one complete revolution, and (c) true solution of the red outlined region in (b).

order methods, high frequencies are damped. As expected from Figure 3, the damping was least pronounced for the fifth-order method, and most pronounced for first order.

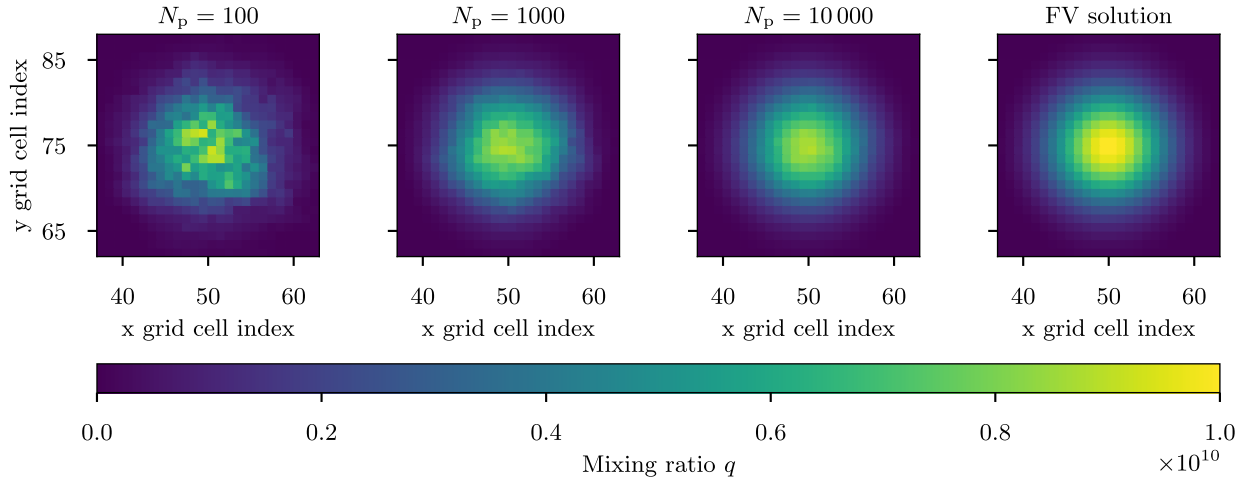
### 3.3 Two-dimensional test case: Gaussian cone advected by solid body rotational wind field

300 To test the schemes in 2D, we used a scalar advection problem modified from Wicker and Skamarock (2002) where a Gaussian cone is advected in a square domain by a prescribed solid-body rotation flow. Figure 6 shows the initial conditions. The domain is  $100 \times 100$  nondimensional units and the velocity field is defined as  $u(x, y) = -\omega(y - 50)$  and  $v(x, y) = \omega(x - 50)$  where  $\omega = \frac{2\pi}{628}$ . We took  $\Delta x = \Delta y = 1$  and  $\Delta t = 0.5$ , so that one full rotation requires 1256 time steps. The initial number concentration is given as

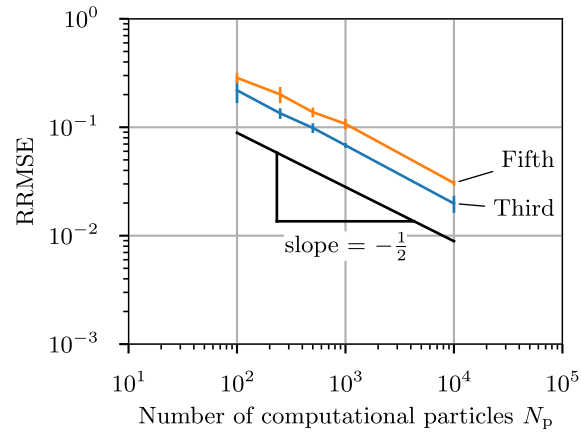
$$305 \quad q(x, y) = \max \left( 10^{10} \exp \left( - \left( \frac{r}{r_0} \right)^2 \right), 10^{-15} \right), \quad (23)$$

where  $r = \sqrt{(x - 50)^2 + (y - 75)^2}$  and  $r_0 = 6$ . The grid cell average values were constructed using  $5 \times 5$ -point Gaussian quadrature.

Figure 7 shows the solution after one revolution for the region of interest with 100, 1000 and 10 000 computational particles per grid cell as well as the finite volume solution. As the number of computational particles increased, the solution became  
 310 less noisy and more similar to the finite-volume solution. This is quantified in Figure 8, which shows the error of the particle solution compared to the finite volume solution. As expected, the stochastic error of the Monte Carlo method has a rate of



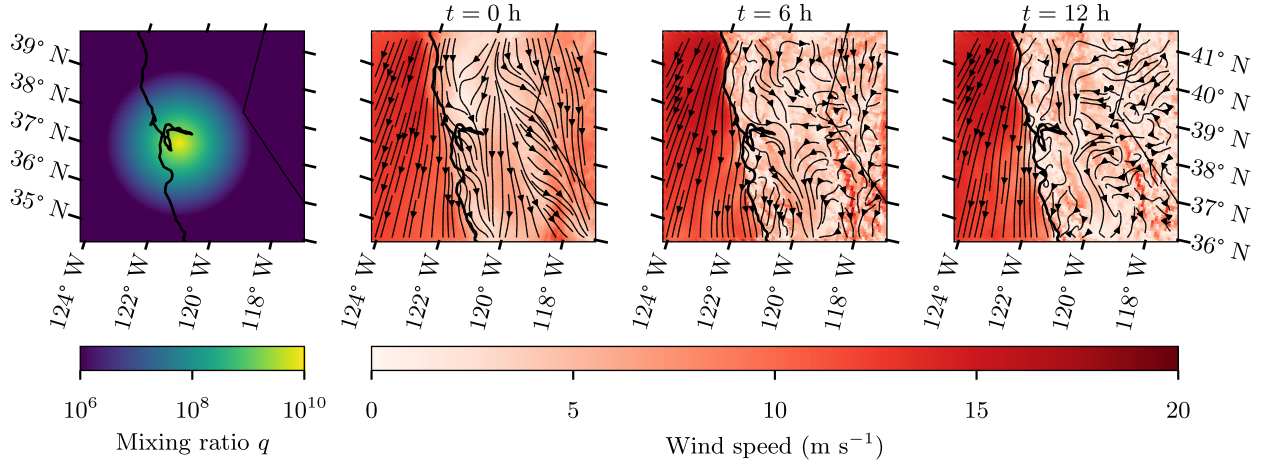
**Figure 7.** Two dimensional test case (Sec. 3.3): stochastic particle solution for 100, 1000 and 10000 computational particles per grid cell and the finite volume solution after one revolution for the region shown in red in Figure 6(b).



**Figure 8.** Two dimensional test case (Sec. 3.3): relative root-mean square error (RRMSE) between the particle solution and the finite volume solution for 3rd and 5th order monotonic advection. Error bars indicate the 95% confidence interval from 10 simulations. The black reference line indicates the theoretical convergence rate with slope  $\frac{1}{\sqrt{N_p}}$ .

convergence of  $\frac{1}{\sqrt{N_p}}$ . As the convergence of finite volume solutions to the analytical solution is well studied (Wicker and Skamarock, 2002), we do not include results showing convergence in  $\Delta x$  and  $\Delta y$ .





**Figure 9.** Three-dimensional test case (Sec. 3.4): the initial condition (left) and snapshots of the wind velocity field at times  $t = 0, 6$  and  $12$  h in the lowest model layer.

### 3.4 Three-dimensional test case: Plume transported by WRF simulated meteorology

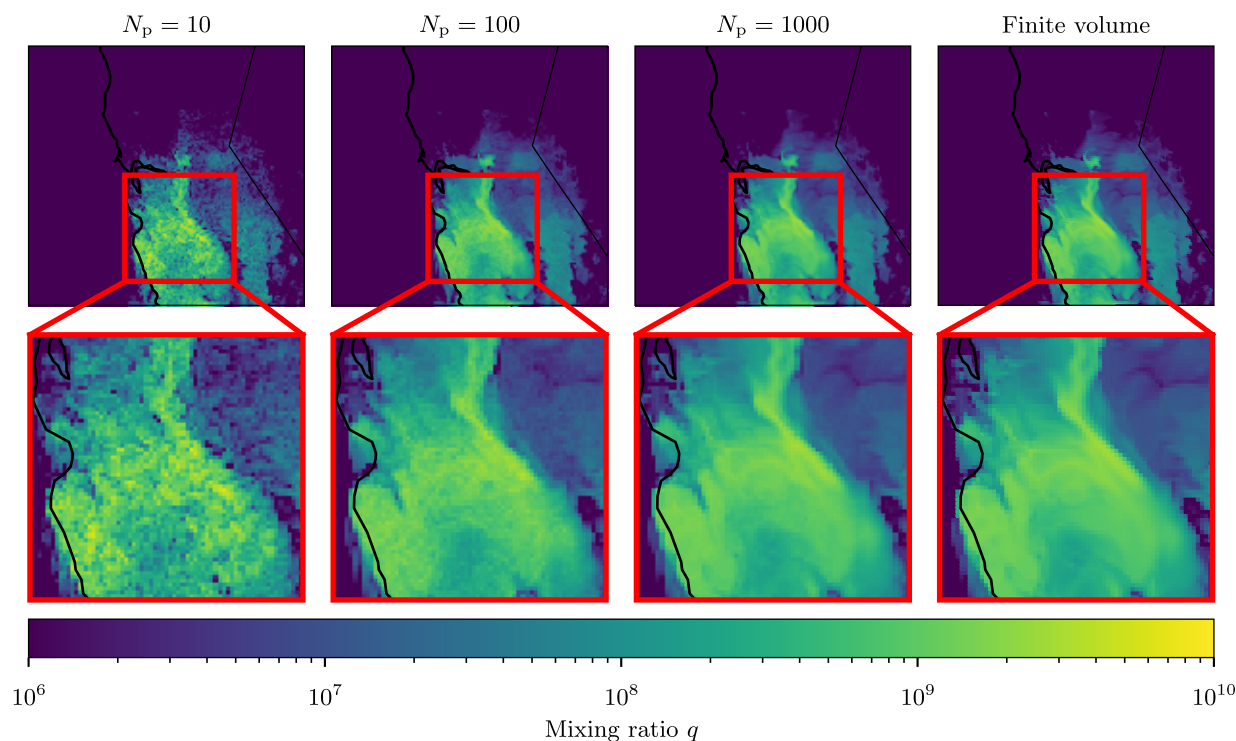
315 For this simulation we used WRF to fully simulate the meteorology, resulting in an evolving velocity field. We prescribed an idealized initial condition of particle number concentration and gas tracer mixing ratio. The gas tracer mixing ratio was used as a proxy for the solution of the finite volume method. The domain was  $170 \times 160 \times 40$  grid cells with  $\Delta x = \Delta y = 4$  km. For this case, an initial cloud of aerosol particle mixing ratio and gas mixing ratio was determined by

$$q_{\text{grid}}(x, y, z) = \max \left( 10^{10} \exp \left( - \left( \sqrt{\left( \frac{x-x_0}{r_x} \right)^2 + \left( \frac{y-y_0}{r_y} \right)^2 + \left( \frac{z-z_0}{r_z} \right)^2} \right) \right), 10^{-15} \right), \quad (24)$$

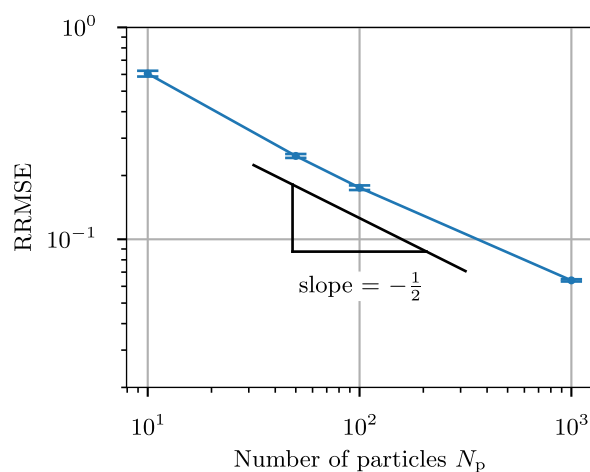
320 where  $r_x = r_y = 6$  and  $r_z = 4$ , and the cloud is centered at grid cell  $x_0 = 75$ ,  $y_0 = 75$ , and  $z_0 = 1$ . Here  $q_{\text{grid}}(x, y, z)$  is specified in grid coordinates (each grid cell is square of size  $1 \times 1 \times 1$  grid units) before being transformed to physical coordinates for the simulation. Figure 9(a) shows the initial condition described by Eq. (24) at the lowest model layer. The initial condition was advected by the dynamic meteorology over a 12 hour period on June 17, 2010. The temporal evolution of the wind field is shown in Figure 9(b) in increments of 6 hours. Gases and particles are subject only to advection and do not experience turbulent  
 325 diffusion or any removal processes.

Figure 10 shows the solution after 12 hours for a varying number of computational particles per grid cell, with the finite volume solution for comparison. The simulation with 10 particles per grid cell is noisy as expected, capturing only general features of the number concentration. As the number of computational particles was increased, the number concentration field becomes smoother and similar to the finite volume solution.

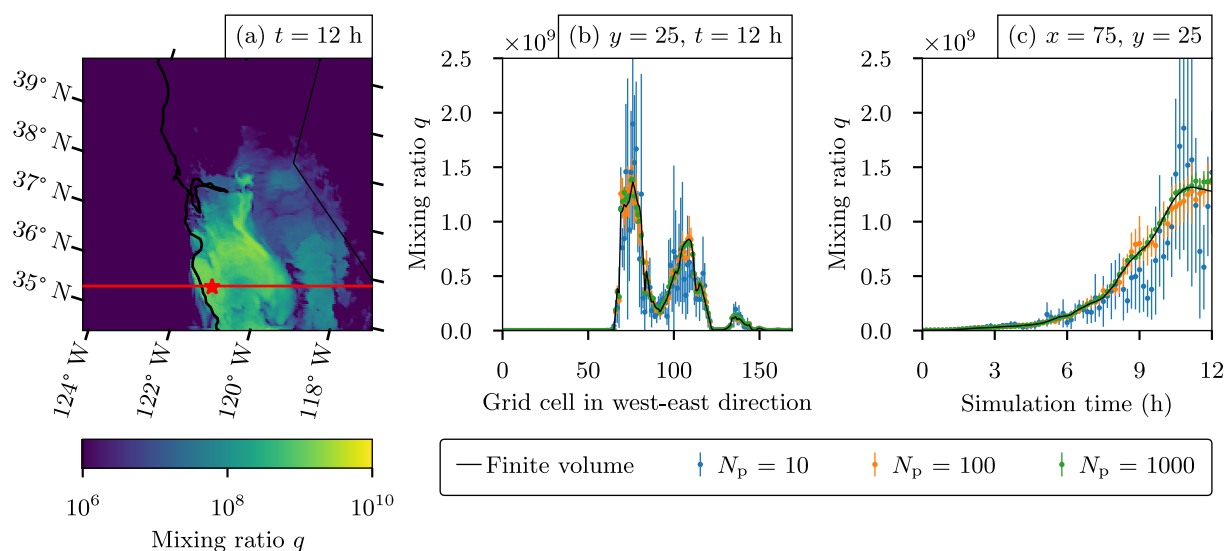
330 Figure 11 shows the convergence of the realistic case for third-order monotonic advection. As the number of computational particles increased, the error when compared to the finite volume solution converged at the expected rate of  $\frac{1}{\sqrt{N_p}}$ . Due to the



**Figure 10.** Three-dimensional test case (Sec. 3.4): lowest layer mixing ratios after 12 hours of simulation for 10, 100 and 1000 computational particles per grid cell, and the deterministic finite volume solution reference solution.



**Figure 11.** Three-dimensional test case (Sec. 3.4): convergence of the relative root-mean square error (RRMSE) between the stochastic solution and the finite volume solution as the number of computational particles per grid cell increases. Error bars show the 95% confidence interval from an ensemble of 5 simulations.



**Figure 12.** Three-dimensional test case (Sec. 3.4): (a) ensemble mean mixing ratio of 5 particle simulations after 12 hours for the lowest model layer with  $N_p = 100$  computational particles per grid cell, (b)  $x$  transect at  $y = 25$  for stochastic solutions of  $N_p = 10, 100$  and 1 000 computational particles per grid cell at  $t = 12$ h, and (c) time series at  $(x = 75, y = 25)$  for  $N_p = 10, 100$  and 1 000 computational particles per grid cell. The finite volume solution for the transect and time series is denoted by black lines. Error bars denote the 95% confidence interval from 5 simulations.

stochastic nature of the problem, monotonic limiters may be applied to the number concentration field that do not exist in the finite volume solution. As a result, a perfect  $\frac{1}{\sqrt{N_p}}$  convergence rate is not expected.

Figure 12(a) shows an  $x$ - $y$  cross section in the lowest model layer for the mean stochastic solution for  $N_p = 100$  with 5 simulations. The red line denotes the transect shown in Figure 12(b). The finite volume solution is shown with the ensemble mean of 10, 100 and 1000 computational particles. As the number of particles increased, the solution tended to the finite volume solution and contained significantly less variance. In Figure 12(c) shows the time series at the starred location in Figure 12(a).

#### 4 Conclusions

In this paper we presented the development of a stochastic particle advection method and demonstrated its performance for particle-resolved atmospheric aerosol transport in the combined WRF-PartMC model. The method is based on finite volume advection schemes but interprets the fluxes as probabilities of particle transport, which can then be stochastically sampled. We analyzed the method in the one-dimensional setting to show that the stochastic particle sampling injects noise at high spatial frequencies and so the method performs best when using dissipative finite-volume discretizations, such as the third- and fifth-order schemes used in WRF.



345 We applied the new method in WRF-PartMC with the existing monotonic limiter for the fifth-order scheme and a new  
limiter for third order. We considered two test cases: a solid-body rotational wind field in 2D, and an atmospherically-relevant  
dynamic wind field over complex terrain in 3D. In both cases we observed the expected rates of convergence of the stochastic  
particle transport to the finite volume solution as the number of computational particles per grid cell was increased. For these  
examples, significant stochastic noise was evident in simulations with 100 computational particles per grid cell but stochastic  
350 noise was found to be less than 10% for simulations with 1000 particles per grid cell. This is considered a reasonable number  
of computational particles for large-scale WRF-PartMC simulations, as these simulations typically use on the order of 10 000  
computational particles to accurately capture properties of the aerosol mixing state (Gasparik et al., 2020).

The value of this work is to enable direct comparison of particle-resolved aerosol representations to models that use ap-  
proximate aerosol representations with simplified assumptions regarding size and composition (e.g., internally mixed modes or  
355 bins). Because the stochastic particle method is based on the same finite volume schemes used for the approximate represen-  
tations, model comparisons can isolate the differences arising due to aerosol representation. Additionally, the new stochastic  
transport scheme allows the WRF-PartMC model to be used on the regional scale to quantify the impact of aerosol mixing  
state on climate-relevant aerosol properties, such as aerosol absorption and CCN concentration, and to compare these findings  
to existing studies (Matsui et al., 2013; Zhang et al., 2014; Zhu et al., 2016).

360 *Code and data availability.* WRF-PartMC version 1.0 is available at <https://doi.org/10.5281/zenodo.10794890> (Curtis et al., 2024a). The  
current version of WRF-PartMC is available at <https://github.com/open-atmos/wrf-partmc>. The Python Jupyter notebooks and WRF-PartMC  
simulation data to reproduce figures contained within this manuscript are available at Curtis et al. (2024b).

*Author contributions.* JHC implemented the code and performed the data analysis. MW derived the analytical equations for the 1D model.  
All authors contributed to conceiving the numerical experiments and writing the manuscript.

365 *Competing interests.* The authors declare that they have no conflict of interest.

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## 490 Appendix A: 1D advection in the frequency domain

To understand the behavior of the 1D deterministic and stochastic numerical methods it is helpful to write them in the frequency domain. To do this, we start in this section by considering only the deterministic (finite volume) case. We will then extend this to the stochastic case in the next section. We will use the vector notation

$$n = [n_0, n_1, \dots, n_{N_x-1}], \quad (\text{A1})$$

495  $f = [f_{\frac{1}{2}}, f_{3/2}, \dots, f_{N_x-\frac{1}{2}}]. \quad (\text{A2})$

We assume periodicity, so  $n_i = n_{i+N_x}$  and  $f_{i-\frac{1}{2}} = f_{i-\frac{1}{2}+N_x}$  for any  $i$ . Similarly, we encode the finite difference stencils as vectors:

$$r^{1\text{st}} = [1, 0, \dots, 0], \quad (\text{A3})$$

$$r^{2\text{nd}} = \frac{1}{2}[1, 0, \dots, 0, 1], \quad (\text{A4})$$

500  $r^{3\text{rd}} = \frac{1}{6}[5, -1, 0, \dots, 0, 2], \quad (\text{A5})$

$$r^{4\text{th}} = \frac{1}{12}[7, -1, 0, \dots, 0, -1, 7], \quad (\text{A6})$$

$$r^{5\text{th}} = \frac{1}{60}[47, -13, 2, 0, \dots, 0, -3, 27], \quad (\text{A7})$$

$$r^{6\text{th}} = \frac{1}{60}[37, -8, 1, 0, \dots, 0, 1, -8, 37]. \quad (\text{A8})$$

This allows us to express the fluxes (3)–(8) via a convolution:

505  $f = ur * n, \quad (\text{A9})$

$$f_{i+\frac{1}{2}} = u \sum_{j=0}^{N_x-1} r_{i-j} n_j. \quad (\text{A10})$$

Next, define the finite difference stencil

$$d = [1, -1, 0, \dots, 0] \quad (\text{A11})$$

so we can approximate the spatial derivative as

510  $\frac{\partial n}{\partial x} \approx \frac{1}{\Delta x} d * n. \quad (\text{A12})$



Using this we can write the spatially discretized advection equation (2) as

$$\frac{\partial n}{\partial t} = -\frac{1}{\Delta x} d * f \quad (\text{A13})$$

$$= -\frac{u}{\Delta x} d * r * n. \quad (\text{A14})$$

We denote the discrete Fourier transform (DFT) using a hat, so  $\hat{n} = \mathcal{F}(n)$  and similarly for other variables, and recall that the  
515 DFT is given by

$$\hat{n}_k = \sum_{j=0}^{N_x-1} n_j \exp(-i2\pi jk/N_x), \quad (\text{A15})$$

where  $i$  is the imaginary unit. Taking the DFT of (A14) gives

$$\frac{\partial \hat{n}_k}{\partial t} = -\frac{u}{\Delta x} d_k r_k n_k \quad (\text{A16})$$

for each wavenumber  $k$ . The solution over one time step is then given by

$$520 \quad \hat{n}_k^{\ell+1} = \exp(-C \hat{d}_k \hat{r}_k) \hat{n}_k^\ell, \quad (\text{A17})$$

where  $C$  is the Courant number given by

$$C = \frac{u \Delta t}{\Delta x}. \quad (\text{A18})$$

Composing  $\ell$  time steps gives the solution at time step  $\ell$  as

$$\hat{n}_k^\ell = \exp(-\ell C \hat{d}_k \hat{r}_k) \hat{n}_k^0. \quad (\text{A19})$$

525 To understand the numerical effect of the finite difference approximation we can compute the evolution of the power spectrum of the solution. The power spectrum is given by

$$P_k = |\hat{n}_k|^2 \quad (\text{A20})$$

and the evolution of the power spectrum over one time step is given by

$$|\hat{n}_k^{\ell+1}|^2 = \hat{n}_k^{\ell+1} \hat{n}_k^{\ell+1*} \quad (\text{A21})$$

$$530 \quad = \left( \exp(-C \hat{d}_k \hat{r}_k) \hat{n}_k^\ell \right) \left( \exp(-C \hat{d}_k \hat{r}_k) \hat{n}_k^\ell \right)^* \quad (\text{A22})$$

$$= \exp(-C \hat{d}_k \hat{r}_k) \exp(-C \hat{d}_k^* \hat{r}_k^*) \hat{n}_k^\ell \hat{n}_k^{\ell*} \quad (\text{A23})$$

$$= \exp(-2C \operatorname{Re}(\hat{d}_k \hat{r}_k)) |\hat{n}_k^\ell|^2. \quad (\text{A24})$$

The energy amplification of the method is thus given by

$$A_k = -2C \operatorname{Re}(\hat{d}_k \hat{r}_k) \quad (\text{A25})$$



535 and we can write the power spectrum evolution as

$$P_k^{\ell+1} = \exp(A_k)P_k^\ell. \quad (\text{A26})$$

If  $A_k$  is zero then the method conserves the energy in wavenumber  $k$ , while negative values indicate that the method will dissipate energy with each time step.

### Appendix B: DFT of finite difference stencils

540 The DFT of the finite difference stencils  $d$  and  $r$  are found by applying (A15) to (A11) and (A3)–(A8). This gives

$$\hat{d}_k = 1 - \exp(-i2\pi k/N_x) \quad (\text{B1})$$

and

$$\hat{r}_k^{1\text{st}} = 1, \quad (\text{B2})$$

$$\hat{r}_k^{2\text{nd}} = \frac{1}{2} \left( \exp(i2\pi k/N_x) + 1 \right), \quad (\text{B3})$$

545  $\hat{r}_k^{3\text{rd}} = \frac{1}{6} \left( 2 \exp(i2\pi k/N_x) + 5 - \exp(-i2\pi k/N_x) \right), \quad (\text{B4})$

$$\hat{r}_k^{4\text{th}} = \frac{1}{12} \left( -\exp(i2\pi 2k/N_x) + 7 \exp(i2\pi k/N_x) + 7 - \exp(-i2\pi k/N_x) \right), \quad (\text{B5})$$

$$\hat{r}_k^{5\text{th}} = \frac{1}{60} \left( -3 \exp(i2\pi 2k/N_x) + 27 \exp(i2\pi k/N_x) + 47 - 13 \exp(-i2\pi k/N_x) + 2 \exp(-i2\pi 2k/N_x) \right), \quad (\text{B6})$$

$$\hat{r}_k^{6\text{th}} = \frac{1}{60} \left( \exp(i2\pi 3k/N_x) - 8 \exp(i2\pi 2k/N_x) + 37 \exp(i2\pi k/N_x) + 37 - 8 \exp(-i2\pi k/N_x) + \exp(-i2\pi 2k/N_x) \right). \quad (\text{B7})$$

The amplification  $A_k$  of the above stencils can now be found by evaluating (A25) to give

550  $A_k^{1\text{st}} = C \left( -2 + 2 \cos(2\pi k/N_x) \right) \quad (\text{B8})$

$$A_k^{2\text{nd}} = 0 \quad (\text{B9})$$

$$A_k^{3\text{rd}} = \frac{C}{3} \left( -3 + 4 \cos(2\pi k/N_x) - \cos(2\pi 2k/N_x) \right) \quad (\text{B10})$$

$$A_k^{4\text{th}} = 0 \quad (\text{B11})$$

$$A_k^{5\text{th}} = \frac{C}{30} \left( -20 + 30 \cos(2\pi k/N_x) - 12 \cos(2\pi 2k/N_x) + 2 \cos(2\pi 3k/N_x) \right) \quad (\text{B12})$$

555  $A_k^{6\text{th}} = 0. \quad (\text{B13})$



### Appendix C: An approximate model for particle advection in 1D

We want to model the stochastic particle advection process as a deterministic advection process with some additional noise.

We start by writing Equation (15) as

$$F_{i+\frac{1}{2}}^\ell = \text{Binom}(N_i^\ell, p_{i+\frac{1}{2}}^\ell) \quad (\text{C1})$$

$$560 \quad = E[F_{i+\frac{1}{2}}^\ell] + S_{i+\frac{1}{2}}^\ell \quad (\text{C2})$$

$$= p_{i+\frac{1}{2}}^\ell N_i^\ell + S_{i+\frac{1}{2}}^\ell \quad (\text{C3})$$

$$= \bar{F}_{i+\frac{1}{2}}^\ell + S_{i+\frac{1}{2}}^\ell, \quad (\text{C4})$$

where  $\bar{F}_{i+\frac{1}{2}}^\ell$  is the deterministic mean flux and  $S_{i+\frac{1}{2}}^\ell$  is a zero-mean random variable representing the stochastic noise, given by

$$565 \quad S_{i+\frac{1}{2}}^\ell = \text{Binom}(N_i^\ell, p_{i+\frac{1}{2}}^\ell) - \bar{F}_{i+\frac{1}{2}}^\ell. \quad (\text{C5})$$

We approximate this stochastic noise by assuming that it is sampled from a constant uniform particle state with exactly  $\check{N}$  particles per grid cell. From Equation (12) we have

$$\check{n} = \frac{\check{N}}{V} \quad (\text{C6})$$

and because the velocity  $u$  is constant and uniform the discretized flux is given by

$$570 \quad \check{f}^{\dagger\dagger} = u\check{n}. \quad (\text{C7})$$

From Equations (13) and (14) we then have

$$\check{F} = V \frac{\Delta t}{\Delta x} \check{f}^{\dagger\dagger} \quad (\text{C8})$$

$$= V \frac{\Delta t}{\Delta x} u \frac{\check{N}}{V} \quad (\text{C9})$$

$$= C\check{N}, \quad (\text{C10})$$

$$575 \quad \check{p} = \frac{\check{F}}{\check{N}} \quad (\text{C11})$$

$$= C. \quad (\text{C12})$$

We can thus write the approximate stochastic noise by modifying Equation (C5) to give

$$\check{S}_i = \text{Binom}(\check{N}, \check{p}) - \check{F} \quad (\text{C13})$$

$$= \text{Binom}(\check{N}, C) - C\check{N}. \quad (\text{C14})$$

580 We want to write the approximate stochastic model in the frequency domain by taking a DFT. It is thus helpful to rewrite the equations in vector form, as we did in Section A. Similarly to Equations (A1) and (A2), we can write the particle counts



$N_i^\ell$  and particle fluxes  $F_{i-\frac{1}{2}}^\ell$  as vectors  $N^\ell$  and  $F^\ell$ , and also do the same for other variables such as the average particle flux  $\bar{F}_{i+\frac{1}{2}}^\ell$  and probabilities  $p_{i+\frac{1}{2}}^\ell$ .

Using the above vector notation and the difference stencil (A11) we can write the temporal update (16) as

$$585 \quad N_i^{\ell+1} = N_i^\ell - F_{i+\frac{1}{2}}^\ell + F_{i-\frac{1}{2}}^\ell, \quad (\text{C15})$$

$$N^{\ell+1} = N^\ell + d * F^\ell \quad (\text{C16})$$

$$= N^\ell + d * \bar{F}^\ell + d * S^\ell. \quad (\text{C17})$$

Taking the DFT now gives

$$\hat{N}_k^{\ell+1} = \hat{N}_k^\ell + \hat{d}_k \hat{F}_k^\ell + \hat{d}_k \hat{S}_k^\ell \quad (\text{C18})$$

$$590 \quad \approx \exp(-C \hat{d}_k \hat{r}_k) \hat{N}_k^\ell + \hat{d}_k \hat{S}_k^\ell \quad (\text{C19})$$

$$\approx \exp(-C \hat{d}_k \hat{r}_k) \hat{N}_k^\ell + \hat{d}_k \hat{S}_k^\ell. \quad (\text{C20})$$

In Equation (C19) we approximated the update of the deterministic component with the exact solution of the deterministic advection equation, as in (A17). That is, we approximated the Runge-Kutta time step update with the exact solution. We then approximated the update of the stochastic component in (C20) by using the approximate stochastic noise  $\check{S}$ .

595 Defining  $\tilde{N}$  to be the solution of the approximate model, we can write the final approximate model from (C20) and (C14) as

$$\hat{N}_k^{\ell+1} = \exp(-C \hat{d}_k \hat{r}_k) \hat{N}_k^\ell + \hat{d}_k \hat{S}_k^\ell, \quad (\text{C21})$$

$$\check{S}_i = \text{Binom}(\tilde{N}, C) - C \tilde{N}. \quad (\text{C22})$$

We observe that the approximate stochastic noise has mean and variance given by

$$\text{E}[\check{S}_i] = 0 \quad (\text{C23})$$

$$600 \quad \text{Var}[\check{S}_i] = C(1 - C) \tilde{N} \quad (\text{C24})$$

for all  $i$ . The initial condition for the approximate model is given by  $\tilde{N}_i^0 = \tilde{N}$  for all  $i$ , which has DFT given by

$$\hat{N}_k^0 = N_x \tilde{N} \delta_{k,0}. \quad (\text{C25})$$

#### Appendix D: Recurrence relations for the first and second moments of the approximate model

Our aim is to solve the approximate model (C21) and (C22) analytically. Because the process is stochastic we will solve for the first two moments of the particle counts  $\tilde{N}$  in the frequency domain and in this section we begin by deriving the appropriate recurrence relations.



Taking an expected value of (C21) gives the following recurrence relation for the first moment:

$$E[\hat{N}_k^{\ell+1}] = E[\exp(-C\hat{d}_k\hat{r}_k)\hat{N}_k^\ell + \hat{d}_k\hat{S}_k] \quad (D1)$$

$$= \exp(-C\hat{d}_k\hat{r}_k)E[\hat{N}_k^\ell] + \hat{d}_kE[\hat{S}_k] \quad (D2)$$

$$610 \quad = \exp(-C\hat{d}_k\hat{r}_k)E[\hat{N}_k^\ell] \quad (D3)$$

where we used the fact that the stochastic noise has zero mean.

Next we obtain a recurrence relation for the second moment of the particle counts. We use (C21) to compute

$$E[\hat{N}_k^{\ell+1}\hat{N}_k^{(\ell+1)*}] = E\left[\left(\exp(-C\hat{d}_k\hat{r}_k)\hat{N}_k^\ell + \hat{d}_k\hat{S}_k\right)\left(\exp(-C\hat{d}_k\hat{r}_k)\hat{N}_k^\ell + \hat{d}_k\hat{S}_k\right)^*\right] \quad (D4)$$

$$= \exp(-C\hat{d}_k\hat{r}_k - C\hat{d}_k^*\hat{r}_k^*)E[\hat{N}_k^\ell\hat{N}_k^{\ell*}] + \hat{d}_k\exp(-C\hat{d}_k^*\hat{r}_k^*)E[\hat{N}_k^\ell\hat{S}_k^*] \quad (D5)$$

$$615 \quad + \exp(-C\hat{d}_k\hat{r}_k)\hat{d}_kE[\hat{S}_k\hat{N}_k^{\ell*}] + \hat{d}_k\hat{d}_k^*E[\hat{S}_k\hat{S}_k^*] \quad (D6)$$

$$= \exp(-2C\text{Re}(\hat{d}_k\hat{r}_k))E[\hat{N}_k^\ell\hat{N}_k^{\ell*}] + \hat{d}_k\hat{d}_k^*E[\hat{S}_k\hat{S}_k^*]. \quad (D7)$$

In the final step above we used the fact that the approximate stochastic noise,  $\hat{S}_k$ , has zero mean and is uncorrelated with the current solution,  $\hat{N}_k$ , because the noise is sampled from a fixed distribution, (C22), at each time step. This means that  $E[\hat{N}_k^\ell\hat{S}_k^*] = E[\hat{S}_k\hat{N}_k^{\ell*}] = 0$  and so the cross terms vanish.

620 To compute the expected value of the squared magnitude of the stochastic noise,  $E[\hat{S}_k\hat{S}_k^*]$ , we use (F7) and the statistics (C23) and (C24) of the stochastic noise to obtain

$$E[\hat{S}_k\hat{S}_k^*] = N_x^2|E[\check{S}_0]|^2\delta_{k,0} + N_x\text{Var}[\check{S}_0] \quad (D8)$$

$$= N_xC(1-C)\check{N}. \quad (D9)$$

Substituting this into (D7) gives the recurrence relation

$$625 \quad E[|\hat{N}_k^{\ell+1}|^2] = \exp(A_k)E[|\hat{N}_k^\ell|^2] + |\hat{d}_k|^2N_xC(1-C)\check{N}, \quad (D10)$$

where we have also used the amplification factor  $A_k$  given by (A25).

Define the power at wavenumber  $k$  by

$$\tilde{P}_k^\ell = E[|\hat{N}_k^\ell|^2] \quad (D11)$$

and the excitation as

$$630 \quad E_k = |\hat{d}_k|^2N_xC(1-C)\check{N}, \quad (D12)$$

where we can evaluate

$$|\hat{d}_k|^2 = 2 - 2\cos(2\pi k/N_x). \quad (D13)$$



Using the above expressions we can write the final recurrence relation for the second moment (the power) as

$$\tilde{P}_k^{\ell+1} = \exp(A_k) \tilde{P}_k^\ell + E_k. \quad (\text{D14})$$

635 The first term on the right-hand side represents the evolution of the second moment due to the discretized advection scheme, which may preserve the second moment or dissipate it depending on the scheme. This first term is identical to the evolution of the power for the semi-discretization (A26). The second term on the right-hand side represents a constant injection of variance (energy) due to the stochastic noise.

### Appendix E: Analytical solution for the moments of the approximate model

640 In Appendix D we derived the recurrence relations for the first and second moments of the approximate model. In this section we solve these recurrence relations analytically. Starting with the first moment, the recurrence relation D3 has the solution

$$\text{E}[\hat{N}_k^\ell] = \exp(-\ell C \hat{d}_k \hat{r}_k) \text{E}[\hat{N}_k^0] \quad (\text{E1})$$

$$= \exp(-\ell C \hat{d}_k \hat{r}_k) N_x \check{N} \delta_{k,0} \quad (\text{E2})$$

$$= \exp(-\ell C \hat{d}_0 \hat{r}_0) N_x \check{N} \delta_{k,0} \quad (\text{E3})$$

645  $= N_x \check{N} \delta_{k,0} \quad (\text{E4})$

$$= \text{E}[\hat{N}_k^0], \quad (\text{E5})$$

where we used the initial condition (C25) and the fact that  $\hat{d}_0 = 0$ . From this we see that the first moment of the approximate model is constant in time and thus equal to its initial condition. We can write this as

$$\text{E}[\hat{N}_k^\ell] = \check{N}, \quad (\text{E6})$$

650 for all  $i$  and  $\ell$ . We thus see that the mean of the approximate model is identical to the solution (A19) of the deterministic spatial semi-discretization (A16), which is also constant for a uniform initial condition. That is, the approximate model mean is exactly the same as the exact time integration of the finite volume discretization, which is consistent with the observation that in Figure 1 the particle solution oscillates around the finite volume solution.

To solve the recurrence relation for the second moment (D14) we first recall that the linear first-order recurrence relation

655  $z^{\ell+1} = az^\ell + b \quad (\text{E7})$

for  $a \in [0, 1]$  has the solution

$$z^\ell = \begin{cases} a^\ell z^0 + (1 - a^\ell) z^\infty & \text{if } a < 1, \\ z^0 + \ell b & \text{if } a = 1, \end{cases} \quad (\text{E8})$$

where  $z^0$  is the initial condition and  $z^\infty$  is the steady state solution in the decaying case, given by

$$z^\infty = \frac{b}{1 - a}. \quad (\text{E9})$$





660 Applying this to (D14) gives

$$\tilde{P}_k^\ell = \begin{cases} \exp(\ell A_k) \tilde{P}_k^0 + (1 - \exp(\ell A_k)) \tilde{P}_k^\infty & \text{if } A_k < 1, \\ \tilde{P}_k^0 + \ell E_k & \text{if } A_k = 1, \end{cases} \quad (\text{E10})$$

where the limiting moments are

$$\tilde{P}_k^0 = N_x^2 \check{N}^2 \delta_{k,0}, \quad (\text{E11})$$

$$\tilde{P}_k^\infty = \frac{E_k}{1 - \exp(A_k)}, \quad (\text{E12})$$

665 using (C25). To evaluate the above expression we need the amplification factors (B8)–(B13), the excitation (D12), and the squared magnitude (D13).

#### Appendix F: Power identity for vectors with i.i.d. random components

Consider a vector of i.i.d. random variables  $z_i$  for  $i = 0, \dots, N_x - 1$ . We want to compute the expected value of the squared magnitude of the DFT of this vector, i.e.,  $E[|\hat{z}_k|^2]$  for each wavenumber  $k$ .

670 We start by observing that  $E[z_i z_j^*] = E[z_i] E[z_j^*] = |E[z_0]|^2$  for  $i \neq j$  because the random variables are independent. We also have  $E[z_i z_i^*] = E[|z_i|^2] = E[|z_0|^2] = \text{Var}[z_0] + |E[z_0]|^2$ . We can thus write

$$E[z_i z_j^*] = |E[z_0]|^2 + \text{Var}[z_0] \delta_{i,j}, \quad (\text{F1})$$

for all  $i, j$ , where  $\delta_{i,j}$  is the Kronecker delta.

We can now compute the expected value of the squared magnitude of the DFT:

$$675 \quad E[|\hat{z}_k|^2] = E[\hat{z}_k \hat{z}_k^*] \quad (\text{F2})$$

$$= E \left[ \left( \sum_{j=0}^{N_x-1} z_j \exp(-i2\pi jk/N_x) \right) \left( \sum_{\ell=0}^{N_x-1} z_\ell^* \exp(i2\pi \ell k/N_x) \right) \right] \quad (\text{F3})$$

$$= \sum_{j=0}^{N_x-1} \sum_{\ell=0}^{N_x-1} E[z_j z_\ell^*] \exp(-i2\pi(j-\ell)k/N_x) \quad (\text{F4})$$

$$= \sum_{j=0}^{N_x-1} \sum_{\ell=0}^{N_x-1} \left( |E[z_0]|^2 + \text{Var}[z_0] \delta_{j,\ell} \right) \exp(-i2\pi(j-\ell)k/N_x) \quad (\text{F5})$$

$$= |E[z_0]|^2 \sum_{j=0}^{N_x-1} \sum_{\ell=0}^{N_x-1} \exp(-i2\pi(j-\ell)k/N_x) + \text{Var}[z_0] \sum_{j=0}^{N_x-1} \sum_{\ell=0}^{N_x-1} \delta_{j,\ell} \exp(-i2\pi(j-\ell)k/N_x). \quad (\text{F6})$$

680 Consider the first term in the above expression. When  $k = 0$  the sum is  $N_x^2$  and when  $k \neq 0$  the sum is zero because the inner sum consists of  $N_x$  complex numbers that are spaced around the unit circle in a symmetric fashion. Now consider the second term. This collapses to  $\sum_{j=0}^{N_x-1} \exp(-i2\pi(j-j)k/N_x) = N_x$  for all  $k$ . We thus have the final expression

$$E[|\hat{z}_k|^2] = N_x^2 |E[z_0]|^2 \delta_{k,0} + N_x \text{Var}[z_0]. \quad (\text{F7})$$



We see that the power spectrum consists of a uniform component that depends on the variance of the random variable and a  
685 DC component that depends on the mean of the random variable.

### **Appendix G: Symbols used in this paper**

Table G1 lists the symbols used in this paper.



**Table G1.** Symbols used in this paper.

Symbol	Description	Reference
$A$	Amplification factor	(A25)
$C$	Courant number	(A18)
$d$	Finite difference derivative stencil	(A11)
$\delta$	Kronecker delta	(F1)
$\Delta t$	Time step	(9)–(11)
$\Delta x$	Spatial grid spacing	(2)
$E$	Excitation	(D12)
$f$	Concentration flux	(2)
$\bar{F}$	Average particle flux	(13)
$\mathcal{F}$	Discrete Fourier transform (DFT)	(A15)
$i$	Spatial grid index	(2)
$k$	Wavenumber index	(A15)
$\ell$	Time step index	(9)–(11)
$n$	Number concentration	(1)
$\hat{n}$	DFT (discrete Fourier transform) of $n$	(A15)
$N$	Number of computational particles in a grid cell	§2.2, (12)
$\tilde{N}$	Solution to the approximate model	(C21)
$\hat{\tilde{N}}$	DFT (discrete Fourier transform) of $\tilde{N}$	(C21)
$\check{N}$	Initial particle number for the approximate model	(C6)
$N_p$	Number of computational particles per grid cell	(2)
$N_x$	Number of spatial grid points	(2)
$p$	Probability	(14)
$P$	Power spectrum of the semi-discrete solution	(A20)
$\tilde{P}$	Power spectrum of the approximate model solution $\tilde{N}$	(D11)
$\Pi$	Particle set	§2.4
$q$	Mixing ratio	§2.6
$r$	Finite difference stencil coefficient	(A3)–(A8)
$S$	Stochastic noise	(C5)
$t$	Time	(1)
$T$	Total simulation duration	§3
$u$	Velocity	(1)
$V$	Computational volume	(12)
$x$	Spatial coordinate	(1)
$y$	Spatial coordinate	§3.3, §3.4
$z$	Spatial coordinate or generic complex variable	§3.4, §E, §F