

Simulation of the heat mitigation potential of unsealing measures in cities by parameterizing grass grid pavers for urban microclimate modelling with ENVI-met (V5)

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Abstract. Many urban areas are characterized by both a growing population and an intensification of summer heat events in the context of climate change. Thus, more and more people are exposed to heat stress and corresponding health consequences. Measures for climate change adaptation such as unsealing strategies are needed in the existing urban fabric to reduce sensible
10 heat flux by increasing latent heat flux to cool down the urban environment without requiring additional space or changing the basic function of the area. Unsealing measures like grass grid pavers (GGPs) can also help to reduce flooding risks due to increased infiltration and water storage capacities. Up to now, a parameterization of GGPs for microclimatic simulations is not available. To fill this research gap, we here present a new GGP model parameterization developed for the fluid dynamics
15 microclimate ENVI-met model based on field measurements with double-ring infiltrometers etc. which can also be implemented in other microscale models in the field of urban climatology. To analyse the microclimatic effects and the cooling potential of this GGP parameterization, scenario analyses were performed using a validated ENVI-met model setup for an urban high-density study area in Cologne/Germany. An extreme scenario was designed to address the maximum cooling potential of the GGPs in comparison to the dominant sealed asphalt surfaces in the study area, and a more realistic scenario with a usage-compatible installation of GGPs in the model domain only in side streets and inner courtyards while main streets
20 remain sealed. We found a maximum cooling potential of up to -20.1 K for ground surface temperature and up to -7.1 K for air temperature in 1 m above ground level for the hottest hour of a simulated 3-day heat wave in summer 2022 which represents a 20-year heat event in Cologne. On spatial average, a decrease of up to -11.1 K for surface temperature and up to -2.9 K for air temperature was determined. On temporal average for the 3-day heat event, statistically significant mean temperature differences of -5.8 K for surface temperature and -1.1 K for air temperature were simulated. Cooling effects are more
25 pronounced during daytime for surface temperature especially on unshaded areas, while cooling effects for air temperature are strongest during nighttime. Model results also show that the entire air volume in the study area is cooled down due to this adaptation measure, even in areas of the domain where no surfaces have been unsealed in the scenario design. The more realistic GGP scenario shows cooling effects of a comparable magnitude as the extreme GGP scenario. Thus, even partial GGP unsealing is an effective adaptation measure for reducing extreme temperatures in cities if water availability is not limited.

30 1. Introduction

Urban areas are particularly affected by climate change effects such as heat, droughts or flash floods from high precipitation intensity. The frequency, duration and intensity of extreme events has significantly increased during the past decades, and negative consequences for urban dwellers will significantly increase in future (EYRING et al., 2021; KLEEREKOPER et al., 2012). The overheating of urban areas can be attributed to radiation and heat trapping by the urban structures, the high energy storage
35 capacity of building and surface materials, the low albedo of many built surfaces, and a reduced evapotranspiration, infiltration and water storage capacity due to surface sealing (TSOKA et al., 2020; PARKER, 2010). The high percentage of dark and impervious surfaces, typically between 24 % to 45 % of city areas, leads to high radiation absorption and low evaporative cooling (NWAKAIRE et al., 2020).

The demand for new infrastructure and housing results in an increasing trend of sealed surfaces which is expected to continue in the next decades in many European agglomerations (WILKE, 2022). Therefore, potentials of climate change adaptation measures in cities have increasingly been investigated in recent years (BALANY et al., 2020; TSOKA et al., 2020). As the temperature of sealed surfaces is up to 20 °C higher than that of the surrounding areas (NWAKAIRE et al., 2020), unsealing strategies are a central adaptation approach. To reconcile the requirements for climate change adaptation and urban development, strategies are needed to increase infiltration and evapotranspiration as well as decrease shortwave radiation absorption and at the same time do not require additional space (MULLANEY & LUCKE, 2014). Compared to asphalt or concrete roads and pavements, unsealed areas can increase the surface albedo and allow for evaporation or evapotranspiration if vegetated (KOUSIS & PISELLO, 2023). Thus, the partitioning of the radiation balance into sensible and latent heat flux will be shifted towards latent heat flux, reducing the sensible and ground heat flux (DEL SERRONE et al., 2022). Furthermore, unsealed urban surfaces increase infiltration and enable a higher storage of water in the city for longer time periods to reduce flooding and drought effects. This buffering effect for extreme heat and flood improves the urban microclimate through more and longer-lasting evapotranspiration from unsealed soil water storages. Adaptation potentials and thermal effects of unsealing measures depend on many factors such as their size, structure or physical surface properties (SEIFEDDINE et al., 2023). The area available to implement adaptation measures such as unsealing surfaces is largely limited by urban structural constraints, development and traffic usage, especially in densely populated cities (MULLANEY & LUCKE, 2014). Thus, adaptation potentials of unsealing approaches must be assessed based on the given local conditions to achieve the best possible cooling effects during heat and droughts.

Grass grid pavers (GGPs) are an unsealing measure, which on the one hand enables evapotranspirative cooling, and on the other hand can still be used for traffic, walking, parking or other activities. GGPs are a form of evaporative, porous and vegetative pavements, which increase water storage capacity and latent heat flux, and also have a higher reflectivity and emissivity than conventional urban surfaces (NWAKAIRE et al., 2020; QIN, 2015; PELUSO et al., 2022). GGPs not only show cooling effects for surface temperature but also for the surrounding area (HUANG & CHEN, 2020; SANTAMOURIS, 2013). In addition to their temperature-regulating function, GGPs can also increase water availability for the surrounding vegetation like street trees (FINI et al., 2017; MULLANEY & LUCKE, 2014), and reduce storm water flow through a decrease in surface flow due to a higher surface roughness, infiltration and depression storage. Thus, GGPs contribute to reducing peak discharges and prevent flooding. In addition, they help improving water quality by filtering pollutants (BEAN et al., 2007). GGPs are even suitable for sub-optimal locations with slopes of over 10 % (PANNICKE-PROCHNOW et al., 2021).

There are studies that have measured the air temperature above or the surface temperature of mixed grass and concrete surfaces and found a cooling effect in direct comparison to sealed surfaces (TAKEBAYASHI & MORIYAMA, 2009; FINI et al., 2017). In a modelling analysis by BÖTTCHER (2017) using the METRAS model for the city of Hamburg, interlocking pavers with a grass component have been parameterized and simulated to assess the climatic impacts for the region. The parameterization was conducted for an intra-urban and not obstacle-resolving mesoscale and found a slight cooling effect of 1 to 2 K on the surface and less than 1 K in the air. However, GGPs have not been parameterized yet for microclimate modelling such as with the established numerical ENVI-met model. Until now, microclimate modelling studies only represented GGPs or similar surfaces as a separate mixture of pure grass and pure concrete in a stripe or chess board arrangement. Nonetheless, cooling effects for the urban microclimate in terms of air and surface temperature, mean radiant temperature and physiological equivalent temperature (PET) were found. Those studies using ENVI-met focused on research areas in Italy (BATTISTA et al., 2022; BATTISTI et al., 2018; PELUSO et al., 2022), Malaysia (SAITO et al., 2015; TEOH et al., 2022), China (JIA & WANG, 2021), Austria (REZK, 2021) and Switzerland (HOFFMANN & GEISLER, 2022). There is no ENVI-met study simulating GGP effects for Germany yet. TEOH et al. (2022) used the surface layer for grass already parameterized in ENVI-met for the GGPs. REZK (2021) adjusted the albedo and root depth of the pre-parameterized grass. In the study conducted by BATTISTI et al. (2018), alternating grass and concrete strips were implemented in the model domain to roughly approximate the characteristics of

GFPs. Simulated cooling effects of such implementations were more pronounced at the surface than in the atmosphere, and narrow side streets with a width between 6 and 9 meter show the strongest cooling effects (SAITO et al., 2015). JIA & WANG (2021) also found that the location of adaptation measures can have an important influence on the cooling potential. Unshaded places such as large squares showed clearer cooling effects than shaded areas like street canyons (BATTISTI et al., 2018). According to BATTISTA et al. (2022), the installation of GFPs on a large square in Rome showed even higher cooling effects than a simulation with a high-albedo surface material or the implementation of shading measures. In many of the previously mentioned studies, GFPs were not analyzed as a single adaptation measure in the model setup but are combined with other strategies. Thus, isolated direct cause and effect relationships between GFPs and temperature cannot be determined (TEOH et al., 2022). Our literature review shows that there is a high research interest in cooling potentials of GFP unsealings, but until now, no combined parameterization of GFPs has been developed for microclimate modelling. Modelling of GFPs in ENVI-met has only been carried out sporadically by a conceptual implementation separate grass and pavement arrangements, but GFPs have never been parameterized in any study. Thus, microclimate modelling of parameterized GFPs in ENVI-met to analyze cooling effects and adaptation potentials in dense urban environments represents a novelty.

To fill this research gap, this study presents a new parametrization of GFPs based upon in-situ measurements. The suitability of the parameterization is tested by analyzing the effects of unsealing surfaces by GFPs on the urban microclimate by scenario analyses using the high-resolution physically-based 3D ENVI-met model. Therefore, a parameterized model domain for a high-density residential research area in the city of Cologne/Germany was used to simulate a 20-year heat event in summer 2022. The study area is particularly exposed to heat stress. In the past, an urban heat island (UHI) effect of up to 10 K was observed in Cologne (LANUV, 2013). Local climate change projections show, that not only the frequency of heat events is expected to increase in future, but also the intensity. The model simulations are driven by meteorological measurements from our research-grade station in the study area. The model is calibrated and the model results are validated using data from a setup densely-distributed and quality-controlled microclimate sensor network within the study area (EINGRÜBER et al., 2022). To evaluate the effects on air temperature and on surface temperature, GFPs are parameterized based on field measurement campaigns in the study area and implemented in the setup model domain according to the given spatial constraints. In relation to a simulation of the current sealed status-quo, two scenarios are assessed: 1) GFP implementation for all sealed areas in the model domain to identify the maximum cooling potential, and 2) usage compatible GFP implementation only in private spaces and low-traffic areas (courtyards, little frequented side streets, parking areas) while the lanes of all main roads remain sealed to identify the realistic cooling potential. Model simulation results of the current situation are compared to the two unsealing scenarios with respect to changes in the simulated air and surface temperatures using statistical analyses and significance tests to reject the hypothesis that the implementation of GFPs has no significant microscale cooling effect.

2. Methods

2.1 Study area and ENVI-met model setup

Model simulations are performed for a 16-ha study area located in the southern part of the inner city of Cologne/Germany (EINGRÜBER et al., 2021). The study area can be classified as development types 2 and 5 (compact to open medium-high buildings) according to the local climate zone (LCZ) classification (DEMUZERE et al., 2022). Overall, around 20 % of the study area is characterized by green infrastructure such as the Volksgarten park or gardens in inner courtyards of the building blocks. Two main traffic axes run through the study area. The Vorgebirgsstraße in northeast-southwest direction and the Volksgartenstraße in a northwest-southeast direction. The lanes of Volksgartenstraße are spatially divided by a double-avenue of trees with an unsealed footpath. Furthermore, there are smaller side streets, parking areas as well as front gardens of various sizes in the study area (EINGRÜBER et al., 2024c).

A 3D-gridded model domain with 1 m spatial resolution was developed and parameterized for the study area using the ENVI-met model Version V5.1.2 (BRUSE et al, 2022) based on field observations and remote sensing data. More information on the setup of the ENVI-met model can be found in EINGRÜBER et al., 2024d. In this way, real urban environment is represented in the model domain of this physically-based, spatially distributed and continuous time series model with a temporal resolution of 1 s and a spatial resolution of 1 m. The model is driven by measurements from a research-grade meteorological station of the manufacturer Campbell Scientific that we installed in the urban park to define the forced lateral boundary conditions (EINGRÜBER et al., 2022).

The model performance was evaluated using sensitivity analyses. A model validation of air temperature using field measurements from a densely-distributed network of 39 quality-controlled NETATMO sensors within the study area showed a high accuracy with a mean Nash Sutcliffe Model Efficiency Coefficient (NSE) of 0.91 for different weather conditions (EINGRÜBER et al., 2023b).

To analyze the cooling potentials of GGPs, a 72-hour simulation of an extreme heat event was run using this validated model. The period from 18th to 20th July 2022 represents the three hottest consecutive days of the year with a maximum temperature of up to 40.14 °C (EINGRÜBER et al., 2023a). This event can be assigned as a 20-year heat event for Cologne when fitting historical measurements of daily maximum temperature at the DWD weather station at Cologne Airport to a Gumbel extreme value distribution (EINGRÜBER & KORRES, 2022)). This heat event was characterized by very low wind speeds of maximum 0.386 m/s and represents the beginning of a longer extreme drought period in the region.

2.2 Parameterization of grass grid pavers

In the ENVI-met Database Manager (DBManager), a new soil profile consisting of different soil and surface materials was parameterized to represent GGPs. Typical GGPs consist of 8 cm thick concrete stones (HOFFMANN & GEISSLER, 2022; HUNT & COLLINS, 2008; ICPI, 2020; LIN et al., 2013; STARKE et al., 2011). A soil profile of GGPs according to Figure 1 is implemented in ENVI-met. This requires a mixed parameterization of the concrete and substrate as well as a separate parameterization of the grass growing in the gaps, as ENVI-met does not enable a direct mixing of vegetation and surface materials. Furthermore, sand and gravel are used as bedding layers for the soil profile.

As in the entire study area, sandy loam is the predominant natural soil type, which is already parameterized in the database. Parameters for sand are available in the database, but these had to be adjusted according to the GGP construction materials catalog by HOFFMANN & GEISSLER (2022) by adjusting the thermal conductivity and heat capacity density. For the typical gravel soil below the GGPs, the heat capacity and the thermal conductivity were parameterized according to HOFFMANN & GEISSLER (2022). The hydraulic conductivity for gravel ranges between 10^{-1} m/s and 10^{-3} m/s, depending on the literature source, which is why a value of 10^{-2} m/s is assumed (DAS, 2010; FREEZE & CHERRY, 1979; SHACKELFORD, 2013). For the water content of a gravel soil, the values of the coarsest-grained parameterized sand soil are assumed.

For the parameterization of the GGPs itself, the heat capacity and conductivity were taken from HOFFMANN & GEISSLER (2022). The saturated hydraulic conductivity, the water content at saturation and the albedo were measured in-situ within the study area for the database parameterization. The matrix potential, the water content at field capacity and wilting point as well as the mixing coefficient water and turbidity are derived according to the substrate in the concrete grid paver and then included as a percentage for the proportion of soil. The Z_0 roughness length for concrete is 0.010 m according to the DBManager and 0.015 m for all natural soils except sand. Due to the edge between concrete and the substrate, the Z_0 for the GGP is slightly higher than that of pure concrete. Thus, the roughness was also measured in the field.

Grass is already parameterized in ENVI-met and was adapted to the characteristics of grass growing in GGPs. Therefore, the grass height and the Leaf Area Density (LAD) were determined in the field and adjusted according to the ratio of concrete to grass.

2.2.1 Field measurements of the GGP parameters

In-situ measurements of saturated hydraulic conductivity, soil moisture at saturation and albedo were conducted in the northern part of the study area in a GGP parking lot area at Vondelstrasse 37 in spring 2023. In addition, the GGP dimensions and the height and LAD of the grass were measured. The substrate in the gaps was sampled to be analysed in the laboratory. The areal substrate-concrete ratio of the GGPs was determined in the field (39 % substrate to 61 % concrete) and is used to compute the combined GGP parameterization of the mentioned parameters taken from the literature or measured on site (see Figure 2).

The saturated hydraulic conductivity of the GGPs was determined using infiltration measurements in the parking lot. The infiltration rate was measured using three double-ring infiltrometers. The double-ring infiltrometers consist of two concentric stainless steel infiltration rings which are filled to equal level with water to avoid lateral flow. The vertical infiltration flux is measured in the inner ring (EJKELKAMP, 2012). As it is not possible to drill the rings into the soil on concrete such as GGPs, the rings were sealed with clay on the ground to prevent lateral leakage. Measurements were carried out at five different test sites on different parking lots in the study area. Water levels for the five tests were measured every 10 minutes. The final and constant infiltration rate was recorded as saturated hydraulic conductivity after the infiltration rate became constant for at least three consecutive measurements. With 1.2, 1.1, 1.1, 0.8 and 1.3 cm per 10 minutes, an average constant infiltration rate of 1.1 cm within 10 minutes was found for the GGPs, which corresponds to 66 mm/h. This results in a saturated hydraulic conductivity of $18.3 \text{ m/s} \cdot 10^{-6}$ to be used for the parameterization in the ENVI-met DBManager.

Soil moisture at saturation of the substrate within the GGPs was measured at four test sites on the GGP parking lots with six repetitions each (24 measurements in total) using a calibrated ThetaProbe ML2x probe connected to an HH2 Moisture Meter and given as volumetric soil moisture content (vol. %) calculated from the changes in the dielectric constant of the soil with an oscillation frequency of 100 MHz. Prior to the measurements, the substrate was fully saturated with water. With 32.4, 27.8, 29.7 and 28.9 % on average for each of the four test sites, an overall average soil moisture at saturation of 29.7 % was found for the GGP substrate. As the substrate only covers 39 % of the area of the GGPs, and the pavers itself are not permeable (saturation soil moisture 0 %), the value for the combined GGP parameterization was calculated as a weighted mean. Thus, a mixed soil moisture at saturation of $0.116 \text{ m}^3/\text{m}^3$ was used in the ENVI-met DBManager.

In order to address the soil parameters as precisely as possible, substrate samples were taken from paver gaps and dried at 105°C in the laboratory to fully dry the soil material to be sieved. A 0.063 mm sieve was used to separate the sand from the silt and clay. A mixture of 71 % sand and 29 % silt-clay was found which corresponds to loamy sand according to the soil type classification. Thus, loamy sand is used as soil material for the parameterization in the DBManager.

To define the Z_0 roughness length for the GGP parameterization, a profile measurement was conducted. As description of the extent to which the GGP surface deviates from a completely flat surface by elevations, the number of edges between substrate and concrete and their height were measured in the field similar to the procedure in SANTOS & JULIO (2013). 14 substrate/concrete edges are given per profile meter with a height difference of 0.5 to 4.0 cm each (1.5 cm on average) resulting in a Z_0 of 0.21 m for the GGP parameterization in the DBManager of ENVI-met (see Figure 2). As the geometrical structure of the GGPs are evenly repeating parallelograms characterized by full point symmetry in itself, the orientation of the profile meter does not play a role for the number of substrate/concrete edges.

The shortwave albedo of the GGPs was determined using a PYR-BTA pyranometer (from the company VERNIER, 2012). The radiation was measured alternately for the incoming solar radiation and the outgoing reflection from the GGPs in a height of 1.5 meters above ground level. The albedo is calculated as the division between the incoming and outgoing radiation. The measurements in the study area were conducted during a dry period (several days without any precipitation) on a day with clear-sky conditions in spring 2023. Ten measurement repetitions have been implemented. The albedo varied between 0.133 and 0.177 with an average of 0.144 to be used for the GGP parameterization in the ENVI-met DBManager. These measurements represent a more realistic albedo of GGPs exposed to environmental influences after some years of installation

205 in contrast to the albedo values (0.20 - 0.25) published in the literature which are based on new (lighter) GGPs after factory production (BATTISTI et al., 2018; HOFFMANN & GEISLER, 2022; PELUSO et al., 2022).

For grass growing above the GGP layer, the grass profile of the database was modified according to field measurements of the grass growing in the GGPs of the parking lots in the study area. The grass height was determined on site in representative GGPs by measuring the grass stems growing therein and calculating the mean value. The mean height of the grass in the database was adjusted accordingly to 0.045 m, and the mean root depth was changed to 0.053 m. For the Leaf Area Density (LAD) of the grass, the average length of the grass stems with their side stems was multiplied with the average width of the stems to calculate the grass density per GGP gap. As there are 49 grass gaps per m², a resulting LAD of 0.9702 m²/m³ was observed for ideally overgrown GGPs. The LAD is assumed to be uniform for all z-height levels of the grass (see Figure 4).

2.2.2 Implementation of the GGP parameterization in the soil profile

215 The parameters for the parameterization of the three soil materials making up the GGP surface (GGPs, sand and gravel) were directly measured in the field, calculated from the substrate-concrete ratio, or taken from literature are given in Table 1. These three individually developed soil and surface material parameterizations for GGPs, sand and gravel were then combined to a vertical soil profile according to the structure given in Figure 1. The final soil profile thus consists of an 8 cm thick GGP layer, which is the combined parameterization of substrate and concrete. This material is defined as a natural material to enable water flow and transportation within the material in the model. This layer is followed by a 2 cm layer of the new parameterized sand and a 10 cm bedding layer of the new parameterized gravel, followed by the ENVI-met DB parameterization for sandy loam as natural standing substrate in the study area (see Figure 3). This soil profile was defined as non-irrigated, and an emissivity of 0.9 was assumed according to the DBManager and in agreement with PELUSO et al. (2022). The parameterized grass from Figure 4 is placed on that soil profile of Figure 3 to represent the entire GGP structure in the ENVI-met model domain.

2.3 Scenario design

In this study, two scenarios with GGP implementation are compared to a reference run (Figure 5). Simulation 1 (S1), the reference run, describes the actual status of the study area where nearly all surfaces in the urban development are sealed by impermeable asphalt or concrete pavement surfaces, and unsealed grass areas can only be found in the urban park, road medians, front gardens of houses or back gardens in inner courtyards of building blocks. Simulation 2 (S2) represents an extreme scenario in which all sealed surfaces were replaced with GGPs. This scenario aims at quantifying the maximum effect to be expected due to GGPs for the given meteorological conditions.

Simulation 3 (S3) is intended to represent a more realistic scenario in the transition between complete sealing and a complete GGP implementation. For this scenario, the limitations of the ground surface and the actual situation in the study area were taken into account. In this usage compatible scenario, GGP unsealings were only implemented on private space and low-traffic areas like inner courtyards, little frequented side streets or parking areas while the lanes of all main roads remain sealed as in the reference run. This more realistic scenario encompasses 18,333 GGP grid cells compared to the extreme scenario with 19,958 GGP grid cells. With 0.9702 m² of grass per m³, this results in around 77,453 m³ of additional green space in S2 and around 71,147 m³ in S3. This means that there is 8.2 % less green space in S3 compared to S2. GGPs are not designed to carry high traffic loads and the higher roughness causes inconvenience for light vehicles and pedestrians (MORETTI et al., 2019; PELUSO et al., 2022). It would therefore be advisable to install them in side streets, on pedestrian pathways, in inner courtyards or in parking lots (MANTEGHI & TASNEEM, 2020). Therefore, for the design of the realistic scenario S3 with a usage compatible GGP implementation, the lanes of high-traffic roads were kept as asphalt surfaces. While GGPs were set for all side streets, the lane width of the main traffic axes Volksgartenstraße (double-avenue in the middle of the street) and Vorgebirgsstraße were measured to determine the number of sealed grid cells in the model domain. For an assumed minimum sealed lane width

245 of 4 meters for the main traffic roads, corresponding polygons which are not changed to GGPs are created in QGIS and implemented in the model domain INX file using ENVI-met Monde. For all other sealed areas, the predominant asphalt and concrete sealings were replaced by GGPs for the scenario design (see Figure 5).

2.4 Statistical evaluation methods

Descriptive statistical analyses and significance tests are performed to test these hypotheses:

250 I) The applied GGPs in the scenarios S2 and S3 do not show a significant microscale cooling effect on surface temperature and air temperature in comparison to the reference run S1.

II) The cooling effect of GGPs is not significantly higher at the surface than in the atmosphere.

III) There are no significant differences of the cooling effect for the scenarios between day and night.

IV) The cooling effect of GGPs is not significantly lower on unshaded areas in relation to shaded areas.

255 For the analyses, the surface temperature and air temperatures at 1, 3 and 5 m height above ground level of all GGP pixels of all scenarios were extracted from the EDT/EDX model output files converted into a NetCDF format. To separate nighttime and daytime hours for the third hypothesis we defined 8 a.m. to 6 p.m. as daytime because the first GGP pixels are sunny at 8 a.m. and the last ones at 6 p.m. based on the shadow flag parameter. Nighttime is defined accordingly. For the fourth hypothesis, the shadow flag parameter was used to extract shaded and unshaded areas. The output data of the corresponding
260 pixels were extracted using Python Version 3.9 executed in Leonardo DataStudio (BRUSE et al, 2022).

For comparability reasons between the three simulations, exactly the same GGP pixels of S2 were also evaluated for S1 and S3. In this way, data of 19,958 pixels were extracted for all 72 simulation hours for each simulation with Python to be compared. Hourly mean values of all pixels were calculated using R Version R-4.3.0 (R Core Team 2022) as well as frequency distributions and descriptive statistical parameters, namely mean, median, variance, minimum and maximum. Box plots were
265 generated for intercomparison of the three simulations. Differences in mean temperature values were checked for statistical significance using a t-test. A significance level of 0.05 was assumed for all statistical tests. The same test procedure was also performed for the selected nighttime and daytime data as well as for the shaded and unshaded daytime pixels to compare the effects of shaded GGPs with GGPs directly exposed to irradiation. Additionally, NetCDF model output data was loaded into QGIS in order to map mean differences between the scenarios. The hourly layers were averaged using the raster calculator for
270 individual days and for the entire 72-hour simulation period.

To analyse, if GGPs not only show a cooling effect on air temperature but also lead to an increase in thermal outdoor comfort, biometeorological indices are calculated. While a decrease in temperature increases thermal outdoor comfort, an increase of relative humidity due to GGP evapotranspiration as well as an increase in reflected, secondary radiation due to the higher albedo of GGPs might reduce thermal comfort. To quantify the overall effects of GGPs on comfort of human organisms, the
275 biometeorological indices UTCI (Universal Thermal Climate Index) and PET (Physiological Equivalent Temperature) are determined based on the model outputs of the three simulations for all atmospheric grid cells in the model domain using BIO-met software (BRÖDE et al, 2011; HÖPPE, 1999; BRUSE et al, 2022).

3. Resulting cooling effects of the parameterized GGP scenarios

3.1 Spatial variability of temperature differences

280 Cooling effects for surface temperature (T_s) from -2.00 K up to -8.26 K can be identified for all grid cells where GGPs have been implemented. Figure 6 maps the absolute difference in T_s between the reference run S1 and the extreme scenario S2 as a mean value per pixel for the 72-hour period. In built-up areas as well as in areas which are already unsealed in the reference run like the Volksgarten park or other vegetated areas, hardly any T_s differences can be detected. On average for all surface

grid cells of the entire 16 ha study area, a cooling effect of -3.00 K in Ts was found. For individual hours such as 1 p.m. of the
285 hottest day (19th July 2022), Ts was decreased by up to -20.01 K for single GGP grid cells.

Figure 7 shows the absolute difference in 1-meter air temperature (Ta) between the reference run S1 and the extreme scenario
S2 as a mean value per pixel for the 72-hour period. In general, Ta differences are much less pronounced than on the ground
surface with changes of -0.19 up to -2.73 K. The areas with GGPs also show clearer cooling effects, but cooling effects can be
found throughout the entire study area and thus also in areas where no GGPs have been implemented such as the urban park
290 or courtyard gardens. This means that the air volume of the entire study area is cooled down in this GGP scenario. The areas
in the northern part of the Vorgebirgsstraße have a noticeably higher Ta difference. On average for all 1-m height atmosphere
grid cells of the study area, a cooling effect of -0.92 K for Ta was found. For individual hours like for 12 a.m. of the hottest
day (19th July 2022), Ta was decreased by up to -7.01 K for single grid cells in the model domain.

In Figure 8, differences between Ts and Ta are compared for the three individual days of the heat event. All days show cooling
295 effects for Ts and Ta. On the hottest day, 19th July, the strongest cooling effects can be observed with up to -9.04 K for Ts and
up to -5.13 K for 1-meter Ta. On 18th July, weaker cooling effects can be found under street trees and in the avenue, while on
19th July, stronger cooling effects occur around the trees. Similarly, weaker effects are given on 20th July. Although the
strongest cooling effects are given for the hottest day 19th July, the cooling effects are a little weaker for 20th than for 18th
despite the 20th being hotter than 18th. As the difference of the soil water content to the field capacity (FC) continuously
300 increases over the three days, the available water for transpiration of the GGPs decreases over time and causes smaller cooling
effects on the third day with a deficit in relation to FC of up to -90 % in relation to the first day where no soil water content
deficit in relation to FC was given. Although there was a decrease over time, the water content of all GGPs was still sufficient
for plant evaporation throughout all three days. The soil water content of GGPs decreased much less in shaded areas like under
street trees.

305 3.2 Surface temperature differences

The boxplots in Figure 9a illustrate the distribution of Ts for the three different scenarios based on the 72 hourly values
calculated from the average of all GGP pixels for each hour. For S1, a large interquartile range (IQR) of 13.96 °C can be
observed. With 28.54 °C, the median is higher than in the GGP scenarios (23.1 °C for S2). S2 and S3 also show a smaller IQR
of 9.27 °C and 9.47 °C, respectively. For S2, a maximum Ts difference of -11.12 K can be observed on 19th July at noon. On
310 temporal average of the 72 hourly mean values of all GGP pixels, Ts is 5.76 K cooler in S2 and 5.27 K cooler in S3 than in
S1. These average cooling effects of GGPs on Ts are statistically significant according to the applied t-test for both scenarios
S2 and S3 in relation to S1, but more significant for the extreme scenario S2 (see Appendix 2). In Figure 10a, an hourly
timeseries of the mean Ts is given for the three scenarios. Maximum Ts differences between the scenarios can be observed
during the hottest hours of the day between 12 a.m. and 7 p.m., while the smallest Ts differences were simulated between 7
315 p.m. and midnight.

The deviation of the dataset into day and night is illustrated in the boxplots of Figure 9b. During night hours, smaller deviations
in both the maximum and average Ts values for both scenarios S2 and S3 can be found. With -4.4 K on average, daytime
cooling effects are much more pronounced than at nighttime for S2 (-4.09 K for S3). Since p-values are lower during the day
than at night, cooling effects are stronger and more significant during the day, but still significant for nighttime. The deviation
320 of the dataset into shaded and unshaded areas is represented in the boxplots of Figure 9c. The differences in Ts are also
significantly higher on unshaded areas than on shaded areas. In scenario S2, a Ts difference of up to -13.43 K can be observed
on unshaded areas, whereas this is only -10.85 K in shaded areas. The higher Ts differences on the unshaded areas can primarily
be observed in the reduction of the maximum Ts of the days. While significant Ts differences were found between the different
scenarios both for shaded and for unshaded areas, p-values are lower for unshaded areas and thus, cooling effects are stronger
325 and more significant for direct sunlit surfaces.

3.3 Air temperature differences and thermal outdoor comfort

While cooling effects of GGPs on T_s are highest during daytime, cooling effects on T_a are stronger during nighttime. The boxplots in Figure 11a illustrate the distribution of T_a for the three different model runs based on the 72 hourly values calculated from the average of all atmosphere grid cells above GGP pixels (for 1 m, 3 m and 5 m height above ground level) for each hour. T_a reacts less sensitive to the installation of the GGPs. All boxplots show similar scattering with a similar IQR and standard deviation. The reference run S1 has the warmest T_a at every height level, and the extreme GGP scenario S2 shows the lowest T_a while the realistic scenario S3 ranges in between. The difference in the cooling effects between the scenarios is strongest at a height of 1 m and decreases with increasing distance to the ground surface. Thus, cooling effects are larger in lower height levels. The strongest cooling effect of -2.89 K on T_a occurs at 1 m height level on 19th July at 11 a.m. for scenario S2. These average cooling effects of GGPs on T_a are statistically significant at 1 m height above ground level according to the applied t-test for both scenarios S2 and S3 in relation to S1, but more significant for the extreme scenario S2. For greater heights like 5 m, cooling effects are not statistically significant (see Appendix 2). On temporal average of the 72 hourly mean values of all atmosphere grid cells 1 m above GGP pixels, T_a is 1.08 K cooler than in S1. In Figure 10b, an hourly timeseries of mean T_a is given for the three scenarios and the three height levels above ground surface. During the coldest and warmest hours of the days, T_a is highest at 5 m altitude in S2 and S3 and lowest at 1 m altitude, while for S1, T_a is sometimes slightly higher at 1 m altitude and smallest in 5 m altitude, and sometimes hardly any differences of T_a with height can be observed for S1. Thus, T_a increases with height for S2 and S3 while decreases for S1. Greater T_a differences between the scenarios can be observed mainly during the coldest hours of the day between 1 a.m. and 7 a.m. The deviation of the dataset into daytime and nighttime is illustrated in the boxplots of Figure 11b exemplarily for a height level of 1 m above ground surface. It becomes clear, that the differences between the scenarios are more pronounced at nighttime. According to the median, there is a slightly higher T_a cooling effect during the nights.

Sensible and soil heat fluxes decreased due to GGP implementation, while reflected radiation and latent heat flux (and thus also relative humidity) increased due to the unsealing, LAD and different material properties like lower heat capacity and higher thermal conductivity of the GGPs. To analyse, if the cooling effect of GGPs on T_a also leads to an increase in thermal outdoor comfort despite relative humidity and reflected, secondary radiation increases, thermal comfort indices have been calculated. A map of the absolute difference in the Universal Thermal Climate Index (UTCI) between the reference run S1 and the extreme scenario S2 is shown in Figure 12. It becomes clear, that thermal comfort is significantly increased on areas where GGPs have been implemented. Especially in the street canyons, a decrease of UTCI by up to -2.6 K was calculated. On temporal and spatial average for all grid cells in 1 m height above GGP pixels, an UTCI improvement of -1.7 K was found. In S2, the perceived temperatures drop from very strong heat stress to only strong heat stress on temporal and spatial average for all grid cells in 1 m height above GGP pixels. Also, the Physiological Equivalent Temperature (PET) shows a decrease of the perceived temperature on temporal and spatial average of all areas where GGPs have been implemented by -2.6 K and up to -6.8 K. A corresponding map for the absolute difference in PET between S1 and S2 is given in Appendix 1.

The four initially defined hypotheses can all be rejected according to the performed statistical significance t-tests, and the corresponding alternative hypotheses can be accepted as follows:

- I) The applied GGPs in the scenarios S2 and S3 show a significant microscale cooling effect on T_s and T_a in comparison to the reference run S1.
- II) The cooling effect of GGPs are significantly higher at the surface than in the atmosphere.
- III) There are significant differences of the cooling effect for the scenarios between day and night.
- IV) The cooling effect of GGPs is significantly lower on unshaded areas in relation to shaded areas.

Furthermore, we found that the cooling effects are more pronounced on the hottest day of the three-day simulation period (19th July with fully-autochthonous weather conditions), but for all days, a temperature reduction was observed. This clearly states

that even on July 20th where partial cloudiness has pronounced after noon, a significant heat mitigation potential can be concluded for the parameterized GGP.

370 4. Discussion

The identified significant temperature differences across all GGP pixels indicate the overall cooling effects on average, but do not account for spatial variations within the study area. The variety of surfaces and shapes in urban areas exhibits a high diversity of features influencing the urban microclimate. The interaction and interplay of these diverse surfaces contribute to the complexity of the urban environment and must be considered. The intrinsic characteristics of surfaces are additionally
375 influenced by external factors such as radiation, geometry, position within the flow field, and immediate surroundings (OKE, 1982). For Ta in 1 m height above ground level, particularly between the Volksgarten park and the adjacent tree-lined double avenue, strongest cooling effects might occur, as combinations of various adaptation strategies usually yield the best results. In this context, both the closeby park and the tree-lined avenue, in combination with the GGPs are likely to be most effective. In a study by PELUSO et al. (2022), the combination of cool surfaces, hedges and trees achieved the best cooling effects as Ta
380 could be reduced by over 3 K. BATTISTI et al. (2018) also concluded that combining GGPs with trees and green roofs leads to the best results. In the same way, the high cooling effects along the eastern section of the avenue Volksgartenstraße and the northern part of the Vorgebirgsstraße in our study area can be explained. Numerous trees have been planted at these locations, which noticeably reduce Ta even at heights of 5 m above ground surface. The identified significant cooling effects of GGPs on Ts are strongest during the hottest hours, which can be explained by the thermal properties of the GGPs. Ta, on the other
385 hand, is indirectly reduced by lower sensible heat flux of the ground surface which leads to smaller cooling effects of Ta.

Measurement and simulation studies are in agreement with the magnitude of the cooling effect of the newly-developed GGP parameterization for ENVI-met in this paper, like the analyses for Rome and Fondi/Italy of BATTISTA et al. (2022) and PELUSO et al. (2022). The results from Ipoh and Malacca/Malaysia show very similar maximum Ts effects, but only about half of the cooling effect for maximum Ta (SAITO et al., 2015; TEOH et al., 2022). It should be noted that the analyses in Ipoh only
390 examined the joint effect of GGPs with roadside trees. In many of the mentioned studies, it is therefore difficult to determine the isolated effect of GGPs as different adaptation measures were often combined with each other. Results for Ta in Vienna are significantly lower than in this study, although GGPs were represented by pure grass there (REZK, 2021). A simulation in Hong Kong also concludes weaker cooling effects for Ta (JIA & WANG, 2021). Results cannot directly be compared due to the hotter and drier climatic conditions. At the same time, it needs to be taken into account that all of these studies have not applied
395 a specific parameterization for GGPs and thus, transferability is highly limited. Our findings of significant differences in the cooling effect with increasing height above ground surface is also in agreement with theoretical studies and can be explained by the mixing of warmer and cooler vortices in the air with higher altitude above ground (OKE et al., 2017).

The observed significant differences in the Ts cooling effects between day and night, which are greater during daytime in our simulations can be traced back to the fact that the sensible heat flux was reduced by approx. 130 to just around 10 W/m² in S3.
400 TAKEBAYASHI & MORIYAMA (2009) performed tests with various parking lot surfaces, also including concrete-grass mixtures, and compared them with each other and with an asphalt parking lot. Ts of grass areas also showed a stronger cooling effect during daytime compared to the asphalted parking areas due to a reduction of sensible heat flux ranging between 100 W/m² and 150 W/m². This change in sensible heat flux agrees well with the magnitude of the change in sensible heat flux of our study while absolute values differ due to other surface material and vegetation properties. In addition, a lower absorption of
405 heat by GGPs can be explained by the thermal material properties. Increasing the thermal inertia and minimizing the ratio between net radiation and heat conduction into the ground can reduce Ts (WANG et al., 2021). A smaller proportion of heat is dissipated into the ground despite the higher thermal conductivity of the GGPs, as a higher proportion of energy is directly transferred into latent heat flux. In addition, the high thermal conductivity in deeper layers of the ground reduces Ts during the

day. The thermal inertia of the soil can be reduced by the lower volumetric heat capacity of the GGP's resulting in a lower heat storage during the day, especially during the hottest hours (PELUSO et al., 2022). According to GUI et al. (2007), heat conduction and heat capacity only cause a reduction in maximum temperatures. The results of our study therefore contradict the statement by MANTEGHI & TASNEEM (2020) that porous surfaces only have a marginal cooling effect when filled with soil. With the substrate assumed in our study, this also causes an average of 35 % of the cooling effect.

Although the albedo of the GGP's and the grass (0.144 and 0.2) is smaller than of the mean pavements in S1 (0.35) resulting in a higher energy input, cooling through evapotranspiration compensates and even exceeds this effect which is also proven by LEE et al. (2016) who found a cooling effect for T_a of up to 3.4 K and an average of 1.1 K during the course of the day similar to our simulations. At nighttime, cooling effects of GGP's on T_s are significantly smaller than during daytime, while more significant cooling effects on T_a occur during nighttime in both S2 and S3. The process of heat dissipation during the night can be reduced by installing GGP's. On the one hand, the lower volumetric heat capacity results in lower storage of solar energy during the day. On the other hand, nocturnal cooling is also controlled by the process of evaporation of the surface. This means that the surface and especially the air layers close to the ground are cooled at night. This can explain why ΔT_a in S2 and S3 was on average around 11 % to 16 % smaller during daytime compared to nighttime. In a study in Basel at 4 a.m., also a lower T_a was found over GGP's compared to other surfaces such as asphalt, concrete, stone slabs and gravel (HOFFMANN & GEISLER, 2022). In the study by TAKEBAYASHI & MORIYAMA (2009), more significant differences were also found for T_a at nighttime. GUI et al. (2007) also observed a higher reduction in minimum T_a than in maximum T_a . In agreement to our determined significant differences in the cooling effects between shaded and unshaded GGP areas being more pronounced over sunny areas, higher T_a differences on unshaded surfaces have also been found in BATTISTI et al. (2018). A study on Mancini Square in Rome also demonstrated that the GGP's have the strongest cooling effects especially in the center of the square without any shadings. Locations at the edge of the square next to a building and in an adjacent street under trees showed significantly lower cooling effects (BATTISTA et al., 2022). The positioning of the GGP is therefore of central importance.

On unshaded surfaces, lower p-values, and thus greater T_s differences, were found in our study as more energy is absorbed at unshaded areas which leads to higher T_s . A greater reduction in T_s can then be achieved by installing GGP's in unshaded areas. On the other hand, grass growing on unshaded areas can die earlier during extreme drought events. This could cause smaller cooling effects on unshaded areas in relation to shaded areas when the evapotranspiration of the dead grass reaches zero, and due to the smaller albedo of that surface in contrast to the sealed surfaces of S1, all irradiated energy is then transferred into sensible and ground heat flux. Soil water content has already decreased slightly within the three simulated days and caused smaller cooling effects on the third day. The smaller simulated cooling effects on 20th than on 18th despite the 20th being hotter than 18th can be attributed to a limitation of the cooling effects of the GGP's due to a lack of plant-available water. After several days without any precipitation and artificial irrigation, the effect of evaporative cooling could therefore become negligible on unshaded areas, while grass can survive for longer periods on shaded surfaces like under street trees with higher water availability. Our results also clearly showed that water availability is higher in the direct vicinity of trees. Irrigation of GGP's during particularly dry phases could therefore maintain the cooling function permanently. The combined implementation of GGP's and urban trees can make GGP's more resilient even during prolonged drought periods. Some studies also showed that permeable pavements in combination with urban trees improve water availability for both trees and GGP's (FINI et al., 2017; MULLANEY & LUCKE, 2014).

It was shown in this study that the cooling effects of the GGP's are highest on the hottest simulation day 19th July and higher for the extreme scenario S2 than for the more usage-compatible scenario S3. Also, GGP's not only cool down the air above the surfaces where GGP's have been implemented, but T_a was also decreased in other parts of the study area where no GGP's have been set in the scenarios like in the urban park or in inner courtyard gardens. Thus, the GGP's are able to cool down the air volume of the entire study area. As the strongest cooling effects occur during the midday hours, GGP's are an effective measure

to minimize peak temperatures, which are particularly harmful to human health. The calculated biometeorological indices PET and UTCI prove that thermal stress can significantly be reduced by the parameterized GGP especially during the hottest hours of the simulated days.

455 The identification and expression of cooling effects in the context of urban heat mitigation is complex, and largely depends on the crucial selection of thermal metrics which are not generalizable (MIDDEL et al., 2021). While metrics like T_s can directly represent the physical processes at energy conversion surfaces resulting in the greatest effects, T_a as an integrative energy description of a volume is less sensitive due to external effects like wind flow, but more relevant for pedestrians and better describes the overall cooling effects for an urban environment. Mean Radiant Temperature and thermal comfort indices like
460 UTCI or PET are well suited for describing heat perception and stress of human individuals and take into account parameters like clothing and metabolism parameters as well as personal characteristics like body mass index. Nevertheless, comfort indices have limitations with regard to generalization and transferability for people with different ages, sizes, gender and weight, and therefore are subjective to assumed standardizations. Quantification of cooling effects should therefore always use different metrics to instead of single ones to describe the direct physical causalities as well as the integrative effects and the
465 consequences for perception (ANDERS et al., 2023).

Besides the significant cooling effects of GGPs and other benefits such as water filtration and storage, it should not be neglected that GGPs also present particular challenges. These include the potential for damage if traffic volumes are too high, as the stones are not designed to bear high loads, and the reduction in infiltration performance due to compaction and clogging of the pores after some time (PANNICKE-PROCHOW et al., 2021). Therefore, GGPs require regular maintenance. GGP albedo can also
470 be further reduced while aging. Another key challenge is the death of the grass in extremely dry and hot regions, which is why the implementation of GGPs should always be examined on a site-specific basis (MULLANEY & LUCKE, 2014). Furthermore, accessibility for cyclists, pedestrians and people with walking disabilities must be guaranteed (TAKEBAYASHI & MORIYAMA, 2009). In reality, further sealed strips would be needed for users such as cyclists, and possibly a partial sealing of side streets would still be necessary. Thus, the more usage-compatible scenario S3 is still not a realistic one. But although S3 includes 8.2
475 % less GGP implementation than S2, cooling effects are only slightly smaller. This demonstrates, that there is no linear relationship, and even smaller GGP implementations (percentages) can have significant cooling effects in comparison to S1. Particular attention should be paid to water availability in the overall context of neighborhood planning. In terms of water management, GGPs can be a central strategy for flood protection measures due to increased infiltration and water storage for reducing surface runoff and thus peak flows (BEAN et al., 2007).

480 The results of this study prove the suitability of the newly-developed parameterization of GGPs for microclimate modelling in ENVI-met to fill the identified research gap which could also be used in the broader field of urban microclimate modelling and implemented in models on a similar scale like PALM-4U or MITRAS. The simulations showed that partial unsealing with GGPs is a suitable climate change adaptation measure. Full unsealing scenarios could have even stronger cooling effects. Even higher adaptation potentials can also be expected when combining GGP unsealings with further technical solutions and nature-
485 based solutions like with blue or green roofs (EINGRÜBER et al., 2023c; EINGRÜBER et al., 2024a). Overall, our findings can have important implications for decision-making in urban planning aiming to mitigate future heat stress, droughts, flooding and improve thermal outdoor comfort. Thus, these climate adaptation pathways can contribute to several sustainable development goals (SDGs) of the United Nations (UN), especially the goals 3, 11 and 13.

5. Conclusion

490 As GGPs have never been parameterized for microclimate modelling with ENVI-met before, a new parameterization was developed using in-situ measurements to fill this research gap which can also be implemented in other urban microclimate models. Based on measurements of saturated hydraulic conductivity with double-ring infiltrometers, of soil moisture at

saturation point using FDR probes, of surface albedo using pyranometers, as well as many other measurements of the substrate and vegetation of GGP, a new database profile for ENVI-met was parameterized. To analyse the cooling potential of the GGP, scenario analyses were performed for an urban high-density study area in Cologne/Germany using a validated ENVI-met model. An extreme scenario with hypothetical GGP installation on all sealed surfaces, and a more usage compatible scenario where GGP were not installed on main traffic roads were implemented in the model domain to investigate the microclimatic effects of this parameterization. The GGP unsealings are highly effective in mitigating urban heat stress in the entire city quarter to adapt to the negative effects of anthropogenic climate change as they significantly reduce T_s and T_a . During the hottest hours, differences of up to -20.1 K were found for T_s , while differences of up to -7.1 K were identified for T_a in 1 m height above ground level. On spatial average for the entire model domain, cooling effects of up to -11.1 K for T_s and up to -2.9 K for 1 m T_a were simulated during this 20-year heat event in Cologne in summer 2022. On temporal average for the 3-day heat event, statistically significant mean differences of -5.8 K for T_s and -1.1 K for 1 m T_a were concluded. Cooling effects are more pronounced during daytime for T_s especially on unshaded areas, while cooling effects on T_a are strongest during nighttime as the GGP store less thermal energy during the day and therefore emit less into the atmosphere at night. While T_s is only decreased in areas with GGP installations, T_a indicates that the entire air volume in the study area is cooled, even in areas of the model domain where no surfaces have been unsealed in relation to the reference run like in the urban park or inner courtyard gardens. The cooling effect of the GGP on T_a decreases with the distance from the ground surface as a cooling source. As the more usage compatible GGP scenario shows cooling effects of nearly the same magnitude as the extreme GGP scenario, even partial GGP implementations represent an effective adaptation measure for temperature regulation in dense urban environments. Based on the model outputs, it was also found that the thermal material properties of the GGP cause about one third of T_s differences, while the evapotranspiration is the main cooling process driver. Within the study area, a high spatial variability of cooling effects was found. Thus, adaptation potentials of GGP must be assessed by urban planners based on the given local conditions to achieve the best possible cooling effects including factors such as radiation, geometry, position within the flow field, and immediate surroundings. Our results also showed that GGP not only reduce T_a , but also increase thermal outdoor comfort as the indices PET and UTCI also quantify a significant reduction of heat stress for humans in the study area. The adaptation potential of the GGP is largely limited by water availability. Our simulations demonstrated that the effect of evaporative cooling reduced during the 3-day heat period, especially in unshaded areas, while water availability is higher in the direct vicinity of street trees. In further research, combinations of this new GGP parameterization with other technical and nature-based adaptation strategies like roof and facade greenings or sunsails should be investigated to identify potential reinforcing effects. Especially a combination of GGP with street trees could be a reliable approach to increase water availability for both during extreme, prolonged heat and drought periods to increase resilience by reducing urban heat stress and health risks in a changing climate. It would also be interesting to analyse the microclimatic effects of GGP which are designed using water-permeable concrete or which are made of surface materials with an even higher albedo. Further research could also analyse more specifically which of the parameters of the new GGP parameterization like the albedo of the GGP surface, the heat conductivity and heat storage capacity of the applied materials or the evapotranspiration of the GGP vegetation cause the highest percentage contribution to the overall cooling effect simulated in this study. In this way, it could also be identified if GGP still have a cooling potential when fully dried. To optimize the performance of this climate change adaptation strategy in urban areas, further research could also intercompare the cooling effects of this GGP parameterization in our mid-latitude study area to study areas with different climatic conditions like semiarid climates, or to other cities with different urban geometries and arrangements to better evaluate the usability of GGP for future urban planning.

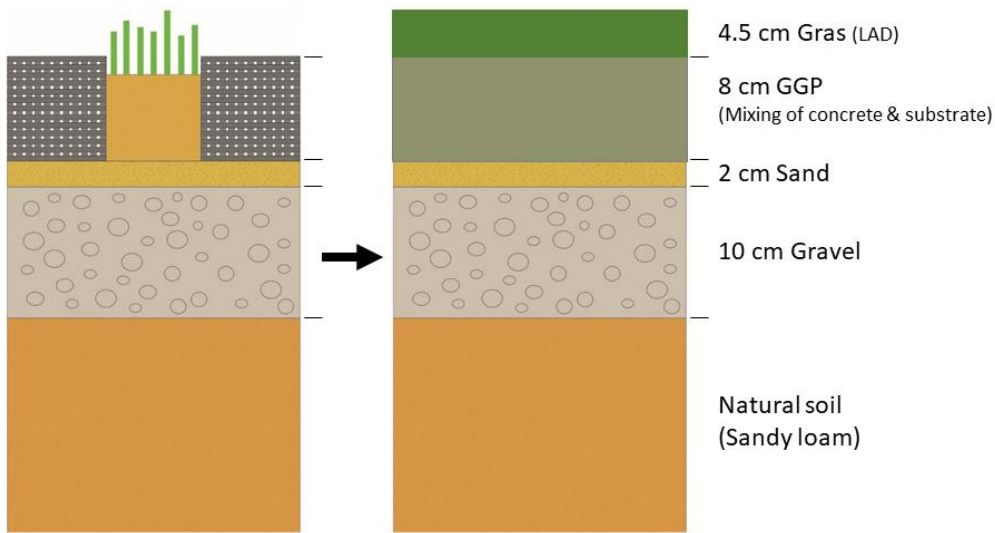
References

- Anders, J., Schubert, S., Sauter, T., Tunn, S., Schneider, C., and Salim, M.: Modelling the impact of an urban development project on microclimate and outdoor thermal comfort in a mid-latitude city. *Energy and Buildings*, 296, 113324, <https://doi.org/10.1016/j.enbuild.2023.113324>, 2023.
- Balany, F., Ng, A. W. M., Muttill, N., Muthukumaran, S., and Wong, M. S.: Green Infrastructure as an Urban Heat Island Mitigation Strategy-A Review, *Water*, 12, 3577, <https://doi.org/10.3390/w12123577>, 2020.
- Battista, G., de Lieto Vollaro, E., Evangelisti, L., and de Lieto Vollaro, R.: Urban Overheating Mitigation Strategies Opportunities: A Case Study of a Square in Rome (Italy), *Sustainability*, 14(24), 16939, <https://doi.org/10.3390/su142416939>, 2022.
- Battisti, A., Laureti, F., Zinzi, M., and Volpicelli, G: Climate Mitigation and Adaptation Strategies for Roofs and Pavements: A Case Study at Sapienza University Campus, *Sustainability*, 10, 3788, <https://doi.org/10.3390/su10103788>, 2018.
- Bean, E. Z., Hunt, W. F., and Bidelspach, D. A.: Evaluation of Four Permeable Pavement Sites in Eastern North Carolina for Runoff Reduction and Water Quality Impacts, *Journal of Irrigation and Drainage Engineering*, 133(6), 583-592, [https://doi.org/10.1061/\(ASCE\)0733-9437\(2007\)133:6\(583\)](https://doi.org/10.1061/(ASCE)0733-9437(2007)133:6(583)), 2007.
- Böttcher, M.: Selected climate mitigation and adaptation measures and their impact on the climate of the region of Hamburg (Doctoral dissertation, Staats-und Universitätsbibliothek Hamburg Carl von Ossietzky), 2017.
- Bröde, P., Fiala, D., Blazejczyk, K., Holmer, I., Jendritzky, G., Kampmann, B., Tinz, B., & Havenith, G.: Deriving the operational procedure for the Universal Thermal Climate Index (UTCI), *International Journal of Biometeorology*, 56, 481-494, 2011.
- Bruse, M., Simon, H. and Sinsel, T.: ENVI-met 5.0: updated model overview, University of Bochum, www.envi-met.com, 2022.
- Das, B. M.: Hydraulic conductivity, in: *Principles of Geotechnical Engineering (7th ed.)*, Cengage Learning, Stamford, ISBN-13: 978-0-495-41130-7, 2010.
- Del Serrone, G., Peluso, P., and Moretti, L.: Evaluation of Microclimate Benefits Due to Cool Pavements and Green Infrastructures on Urban Heat Islands, *Atmosphere*, 13(10), 1586, <https://doi.org/10.3390/atmos13101586>, 2022.
- Demuzere, M., Kittner, J., Martilli, A., Mills, G., Moede, C., Stewart, I. D., and Bechtel, B.: A global map of Local Climate Zones to support earth system modelling and urban scale environmental science, *Earth System Science Data Discussions*, 2022, 1-57, 2022.
- Eijkelpamp: 09.04 Doppelring-Infiltrometer Gebrauchsanweisung, Eijkelpamp, Giesbeek, <https://geotechnik-shop.de/WebRoot/Store22/Shops/48ba4854-b193-4bce-af16-f28523b06652/MediaGallery/Gebrauchsanweisungen/Doppel-Ringinfiltrometer.pdf>, last access: 30 April 2024, 2012.
- Eingrüber, N. and Korres, W.: Climate change simulation and trend analysis of extreme precipitation and floods in the mesoscale Rur catchment in western Germany until 2099 using Statistical Downscaling Model (SDSM) and the Soil & Water Assessment Tool (SWAT model), *Science of The Total Environment*, 838P1, 155775, <https://doi.org/10.1016/j.scitotenv.2022.155775>, 2022.
- Eingrüber, N., Korres, W., and Schneider, K.: Pathways for climate change adaptation in urban areas - first results from field measurements and ENVI-met modeling, EMS Annual Meeting 2021, online, 6-10 Sep 2021, Vol. 18, EMS2021-374, <https://doi.org/10.5194/ems2021-374>, 2021.
- Eingrüber, N., Korres, W., and Schneider, K.: Microclimatic field measurements to support microclimatological modelling with ENVI-met for an urban study area in Cologne, *Adv. Sci. Res.*, 19, 81–90, <https://doi.org/10.5194/asr-19-81-2022>, 2022.
- Eingrüber, N., Schneider, K., and Korres, W.: Evaluation of microclimatic variations and adaptation effects in a central European city during the most excessive heat wave in summer 2022 by ENVI-met modelling, EGU General Assembly 2023, Vienna, Austria, 24–28 Apr 2023, EGU23-11806, <https://doi.org/10.5194/egusphere-egu23-11806>, 2023a.

- Eingrüber, N., Korres, W., Löhnert, U., and Schneider, K.: Investigation of the ENVI-met model sensitivity to different wind direction forcing data in a heterogeneous urban environment, *Adv. Sci. Res.*, 20, 6571, <https://doi.org/10.5194/asr-20-65-2023>, 2023b.
- Eingrüber, N., Krekeler, C., Korres, W., Löhnert, U., and Schneider, K.: High-Resolution Microclimate Modelling to Evaluate Urban Heat Mitigation Potentials of Rainfed Climate Change Adaptation Measures on Buildings under Various Climatic Conditions, AGU Fall Meeting 2023, San Francisco, CA, USA, 11-15 Dec 2023, H23V-1850, <https://doi.org/10.22541/essoar.171052572.20758573/v1>, 2023c.
- Eingrüber, N., Korres, W., and Schneider, K.: Comparison of heat mitigation effects of blue roofs and green roofs on building wall temperature and thermal outdoor comfort based on scenario analyses using 3D microclimate modelling for a dense urban district, EGU General Assembly 2024, Vienna, Austria, 14-19 Apr 2024, EGU24-9967, <https://doi.org/10.5194/egusphere-egu24-99671>, 2024a.
- Eingrüber, N., Domm, A., Korres, W., and Schneider, K.: Parameterization of grass grid pavers for urban microclimate modelling to simulate the heat mitigation potential of unsealing measures in cities (1.1), Zenodo [data set], <https://doi.org/10.5281/zenodo.10966370>, 2024b.
- Eingrüber, N., Schneider, K., Nehren, U., and Dlugoß, V.: Climate change adaptation through citizen participation: Simulation of the effect of willingness to act on the heat mitigation potential in urban neighborhoods with different social milieu composition, EMS Annual Meeting 2024, Barcelona, Spain, 2-6 Sep 2024, Vol. 21, EMS2024-547, <https://doi.org/10.5194/ems2024-547>, 2024c.
- Eingrüber, N., Berg, P., Korres, W., Löhnert, U., and Schneider, K.: Parameterization and Validation of a High-Resolution Microclimate Model to Identify Temperature Patterns in a Climate Change Adapted Urban High-Density Area, Available at SSRN, 4912045, 2024d.
- ENVI-met GmbH: ENVI_MET Software Versions, <https://envi-met.info/doku.php?id=files:downloadv4>, last access: 30 April 2024, 2023.
- Eyring, V., Gillette, N. P., Achuta Rao, K. M., Barimalala, R., Barreiro Parrillo, M., Bellouin, N., Cassou, C., Durack, P. J., Kosaka, Y., McGregor, S., Min, S., Morgenstern, O., and Sun, Y.: Human Influence on the Climate System, <https://doi.org/10.1017/9781009157896.005>, 2021.
- Fini, A., Frangi, P., Mori, J., Donzelli, D., and Ferrini, F.: Nature based solutions to mitigate soil sealing in urban areas: Results from a 4-year study comparing permeable, porous, and impermeable pavements, *Environmental Res.*, 156, 443-454, <https://doi.org/10.1016/j.envres.2017.03.032>, 2017.
- Freeze, A. and Cherry, J.: *Groundwater*, Prentice-Hall, Englewood Cliffs, Jersey, ISBN-13: 9780133653120, 1979.
- Gui, J. (Gavin), Phelan, P. E., Kaloush, K. E., and Golden, J. S.: Impact of Pavement Thermophysical Properties on Surface Temperatures, *Journal of Materials in Civil Engineering*, 19(8), 683-690, [https://doi.org/10.1061/\(ASCE\)0899-1561\(2007\)19:8\(683\)](https://doi.org/10.1061/(ASCE)0899-1561(2007)19:8(683)), 2007.
- Hoffmann, C. and Geissler, A.: *Baumaterialien für Städte im Klimawandel Materialkatalog mit Empfehlungen*, Bundesamt für Wohnungswesen, Basel, <https://www.bwo.admin.ch/bwo/de/home/wie-wir-wohnen/umwelt/publikationen-bwo/baumaterialien.html>, last access: 30 April 2024, 2022.
- Höppe, P.: The physiological equivalent temperature – a universal index for the biometeorological assessment of the thermal environment, *International Journal of Biometeorology*, 43(2), 71-75, 1999.
- Huang, J.-M. and Chen, L.-C.: A Numerical Study on Mitigation Strategies of Urban Heat Islands in a Tropical Megacity: A Case Study in Kaohsiung City, Taiwan, *Sustainability*, 12(10), 3952, <https://doi.org/10.3390/su12103952>, 2020.
- Hunt, W. F. and Collins, K. A.: *Permeable Pavement: Research Update and Design Implications*, Urban Waterways, North Carolina Cooperative Extension Service, https://nacto.org/docs/usdg/urban_waterways_permeable_pavement_hunt.pdf, last access: 30 April 2024, 2008.

- ICPI: Tech Spec 8, Concrete Grid Pavements, Interlocking Concrete Pavement Institute (ICPI), https://www.orco.com/wp-content/uploads/2020/05/ICPI_Tech_Spec_8_Feb_20.pdf, last access: 30 April 2024, 2020.
- 620 Jia, S. and Wang, Y.: Effect of heat mitigation strategies on thermal environment, thermal comfort, and walkability: A case study in Hong Kong, *Building and Environment*, 201, 107988, <https://doi.org/10.1016/j.buildenv.2021.107988>, 2021.
- Kleerekoper, L., van Esch, M., and Salcedo, T. B.: How to make a city climate-proof, addressing the urban heat island effect, *Resources, Conservation and Recycling*, 64, 30-38, <https://doi.org/10.1016/j.resconrec.2011.06.004>, 2012.
- 625 Kousis, I. and Pisello, A. L.: Evaluating the performance of cool pavements for urban heat island mitigation under realistic conditions: A systematic review and meta-analysis, *Urb. Clim.*, 49, 101470, <https://doi.org/10.1016/j.uclim.2023.101470>, 2023.
- LANUV: Klimawandelgerechte Metropole Köln. Abschlussbericht, Landesamt für Natur, Umwelt und Verbraucherschutz Nordrhein-Westfalen, Recklinghausen, https://www.lanuv.nrw.de/fileadmin/lanuvpubl/3_fachberichte/30050.pdf, last access: 30 April 2024, 2013.
- 630 Lee, H., Mayer, H., and Chen, L.: Contribution of trees and grasslands to the mitigation of human heat stress in a residential district of Freiburg, Southwest Germany, *Landscape and Urban Planning*, 148, 37-50, <https://doi.org/10.1016/j.landurbplan.2015.12.004>, 2016.
- Lin, J. D., Hsu, C. Y., Citraningrum, A., and Adhitana, P.: The Impact of Different Types of Permeable Pavement Utilization on Air Temperature above the Pavement, *Advanced Materials Research*, 723, 678-685, <https://doi.org/10.4028/www.scientific.net/AMR.723.678>, 2013.
- 635 Manteghi, G. and Tasneem, M.: Evaporative Pavements as an Urban Heat Island (UHI) Mitigation Strategy: A Review, *International Transaction Journal of Engineering, Management, & Applied Sciences & Technologies.*, 11(1), 1-15, <https://doi.org/10.14456/ITJEMAST.2020.17>, 2020.
- Middel, A., Al Khaled, S., Schneider, F. A., Hagen, B., and Coseo, P.: 50 grades of shade. *Bulletin of the American Meteorological Society*, 102(9), E1805-E1820, <https://doi.org/10.1175/BAMS-D-20-0193.1>, 2021.
- 640 Moretti, L., Di Mascio, P., and Fusco, C.: Porous Concrete for Pedestrian Pavements, *Water*, 11(10), 2105, <https://doi.org/10.3390/w11102105>, 2019.
- Mullaney, J. and Lucke, T.: Practical Review of Pervious Pavement Designs, *Clean Soil Air Water*, 42(2), 111-124, <https://doi.org/10.1002/clen.201300118>, 2014.
- 645 Nwakaire, C., Onn, C., Soon Poh, Y., Yuen, C. W., and Onodagu, P.: Urban Heat Island Studies with emphasis on urban pavements: A review, *Sustainable Cities and Society*, 63, 102476, <https://doi.org/10.1016/j.scs.2020.102476>, 2020.
- Oke, T. R.: The energetic basis of the urban heat island, *Quarterly Journal of the Royal Meteorological Society*, 108, 1-24, <https://doi.org/10.1002/qj.49710845502>, 1982.
- Oke, T. R., Mills, G., Christen, A., and Voogt, J. A.: *Urban Climates*, Cambridge University Press, Cambridge, <https://doi.org/10.1017/9781139016476>, 2017.
- 650 Pannicke-Prochnow, N., Krohn, C., Albrecht, D. J., and Thinius, K.: Bessere Nutzung von Entsiegelungspotenzialen zur Wiederherstellung von Bodenfunktionen und zur Klimaanpassung, Umweltbundesamt, Dessau-Roßlau. https://www.umweltbundesamt.de/sites/default/files/medien/479/publikationen/texte_141-2021_bessere_nutzung_von_entsiegelungspotenzialen_zur_wiederherstellung_von_bodenfunktionen_und_zur_klimaanpassung.pdf, last access: 30 April 2024, 2021.
- Parker, D. E.: Urban heat island effects on estimates of observed climate change, *WIREs Climate Change*, 1, 123-133, <https://doi.org/10.1002/wcc.21>, 2010.
- Peluso, P., Persichetti, G., and Moretti, L.: Effectiveness of Road Cool Pavements, Greenery, and Canopies to Reduce the Urban Heat Island Effects, *Sustainability*, 14(23), 16027, <https://doi.org/10.3390/su142316027>, 2022.
- 660 Qin, Y.: A review on the development of cool pavements to mitigate urban heat island effect, *Renewable and Sustainable Energy Reviews*, 52, 445-459, <https://doi.org/10.1016/j.rser.2015.07.177>, 2015.

- R Core Team: R: A language and environment for statistical computing. R Foundation for Statistical Computing, Version R-4.3.0, <https://www.r-project.org/>, last access: 30 April 2024, 2022.
- Rezk, K.: Computational Parametric Assessment of Desealing Measures in the Urban Domain, Technische Universität Wien, <https://doi.org/10.34726/hss.2021.85327>, 2021.
- 665 Saito, K., Said, I., and Shinozaki, M.: Scenario-based application of neighborhood greening methods towards mitigating urban heat environment in a world heritage site - Malacca, Malaysia, The 13th International Congress of Asian Planning Schools Association (APSA), Universiti Teknologi Malaysia, Johor Bahru, http://eprints.utm.my/61439/1/Scenario-BasedApplicationOfNeighborhoodIsmailSaid2015_GreeningMethodsTowardsMitigatingUrbanHeatEnvironment.pdf, 2015.
- 670 Santamouris, M.: Using cool pavements as a mitigation strategy to fight urban heat island - A review of the actual developments, *Renewable and Sustainable Energy Reviews*, 26, 224-240, <https://doi.org/10.1016/j.rser.2013.05.047>, 2013.
- Santos, P. M. D. and Júlio, E. N. B. S.: A state-of-the-art review on roughness quantification methods for concrete surfaces, *Construction and Building Materials*, 38, 912-923, <https://doi.org/10.1016/j.conbuildmat.2012.09.045>, 2013.
- Shackelford, C. D.: *Geoenvironmental Engineering*, In Reference Module in Earth Systems and Environmental Sciences, Elsevier, ISBN: 9780124095489, 2013.
- 675 Seifeddine, K., Amziane, S., Toussaint, E., and Ouldboukhitine, S. E.: Review on thermal behavior of cool pavements, *Urban Climate*, 51, 101667, <https://doi.org/10.1016/j.uclim.2023.101667>, 2023.
- Starke, P., Göbel, P., and Coldewey, W.: Effects on evaporation rates from different water-permeable pavement designs, *Water science and technology*, 63(11), 2619-2627, <https://doi.org/10.2166/wst.2011.168>, 2011.
- 680 Takebayashi, H. and Moriyama, M.: Study on the urban heat island mitigation effect achieved by converting to grass-covered parking, *Solar Energy*, 83(8), 1211-1223, <https://doi.org/10.1016/j.solener.2009.01.019>, 2009.
- Teoh, M.-Y., Shinozaki, M., Saito, K., and Said, I.: Developing climate-led landscapes and greenery in urban design: a case study at Ipoh, Malaysia, *Journal of Asian Architecture and Building Engineering*, 21(4), 1640-1656, <https://doi.org/10.1080/13467581.2021.1942881>, 2022.
- 685 Tsoka, S., Tsikaloudaki, K., Theodosiou, T., and Bikas, D.: Urban Warming and Cities' Microclimates: Investigation Methods and Mitigation Strategies - A Review, *Energies*, 13(6), 1414, <https://doi.org/10.3390/en13061414>, 2020.
- Vernier: Pyranometer (PYR-BTA), Vernier, Beaverton, <https://www.vernier.com/files/manuals/pyr-bta.pdf>, last access: 30 April 2024, 2012.
- Wang, C., Wang, Z.-H., Kaloush, K. E., and Shacat, J.: Cool pavements for urban heat island mitigation: A synthetic review, *Renewable and Sustainable Energy Reviews*, 146, 111171, <https://doi.org/10.1016/j.rser.2021.111171>, 2021.
- 690 Wilke, S.: Bodenversiegelung, Umweltbundesamt, <https://www.umweltbundesamt.de/daten/flaeche-boden-land-oekosysteme/boden/bodenversiegelung>, last access: 30 April 2024, 2022.



695 **Figure 1: Schematic structure of a GGP on the left, and developed implementation in ENVI-met on the right (own illustration based on HOFFMANN & GEISLER 2022).**

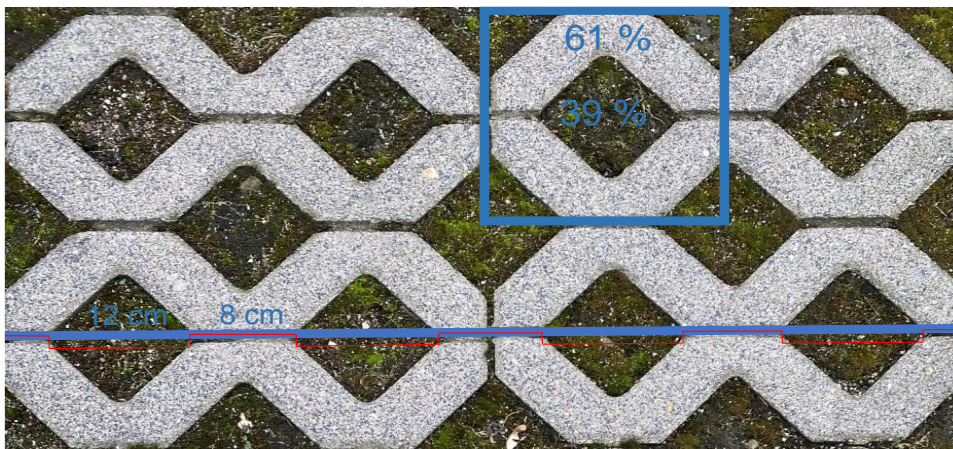
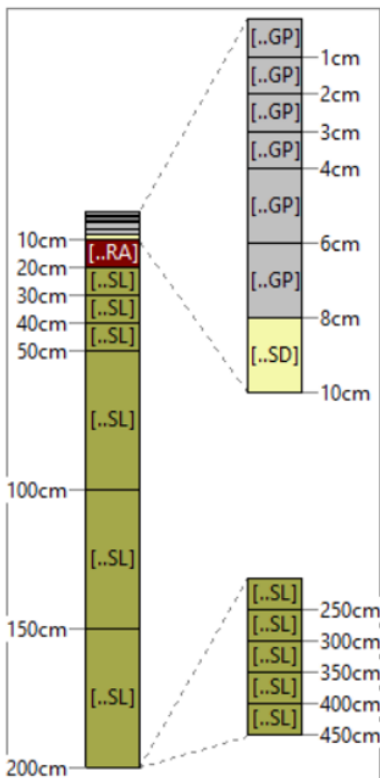


Figure 2: Dimensions of the grass grid pavers measured in the study area and location of the profile for roughness determination.



700 **Figure 3: Vertical structure of the GGP soil profile in the Database Manager; SL = Sandy Loam, RA = Gravel, SD = Sand, GP = Grass Grid Pavers (own illustration in ENVI-met DBManager).**

Table 1: Parameterization of the soil materials for the construction of grass grid pavers in the Database Manager; FC = Field Capacity, WP = Wilting Point, LS = Loamy Sand.

Parameter	Grass Grid Paver	Sand	Gravel
Type of Material (Definition)	Natural material (Water flow is occurring)	Natural soil (Water flow is occurring)	Natural soil (Water flow is occurring)
Water content at saturation/FC/WP [m ³ (Water)/m ³ (Soil)]	0.11578 / 0.0585 / 0.02925 (Own measurement, FC+WP: DB Manager LS*0.39)	0.395 / 0.135 / 0.0068 (DBManager Sand)	0.395 / 0.135 / 0.0068 (DBManager Sand)
Matrix potential [m]	-0.0351 (DB Manager LS*0.39)	-0.121 (DBManager Sand)	-0.121 (DBManager Sand)
Hydraulic conductivity [m/s*10 ⁻⁶]	18.3 (Own measurement)	176 (DBManager Sand)	10000 (DAS, 2010; FREEZE & CHERRY 1979; SHACKELFORD, 2013)
Volumetric heat capacity [J/(m ³ K)*10 ⁻⁶]	1.54 (HOFFMANN & GEISSLER 2022)	1.463 (DBManager Sand)	1.28 (HOFFMANN & GEISSLER 2022)
Clapp Hornberger Constant b [dimensionless]	1.7082 (DB Manager LS*0.39)	4.05 (DBManager Sand)	4.05 (DBManager Sand)
Thermal conductivity [W/(mK)]	2.0 (HOFFMANN & GEISSLER 2022)	1.6 (HOFFMANN & GEISSLER 2022)	0.7 (HOFFMANN & GEISSLER 2022)
Z ₀ Roughness length [m]	0.21 (Own profile measurement)		
Albedo [fraction]	0.144 (Own measurement)		
Emissivity [fraction]	0.9 (DBManager Sandy Loam/Concrete)		
Mixing coefficient Water [m ² /s]	0.001 (DBManager Sandy Loam/Concrete)		
Turbidity Water [1/m]	2.1 (DBManager Sandy Loam/Concrete)		

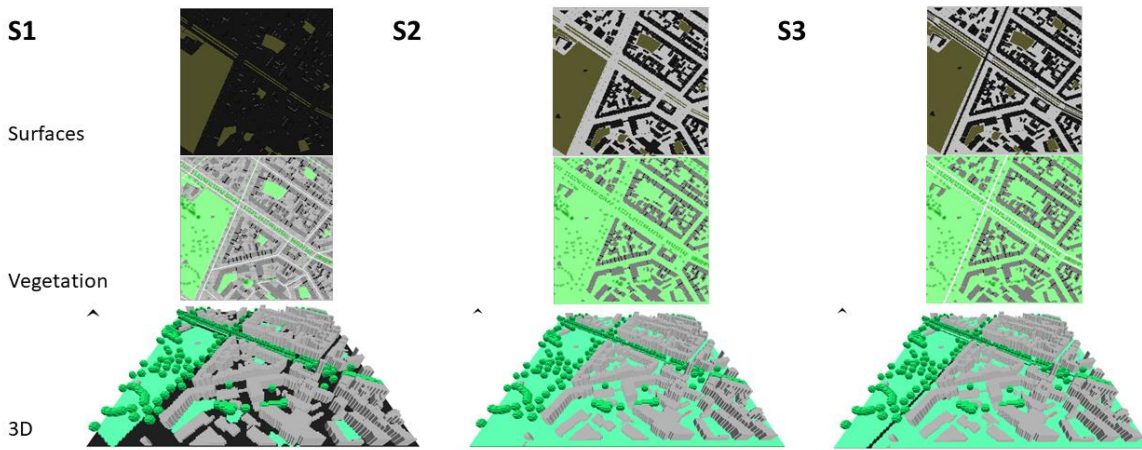
Database-ID: [\[1XXCSG\]](#)

Name: [Grass 4,5 cm aver. dense \(Cologne Südstadt\)](#)

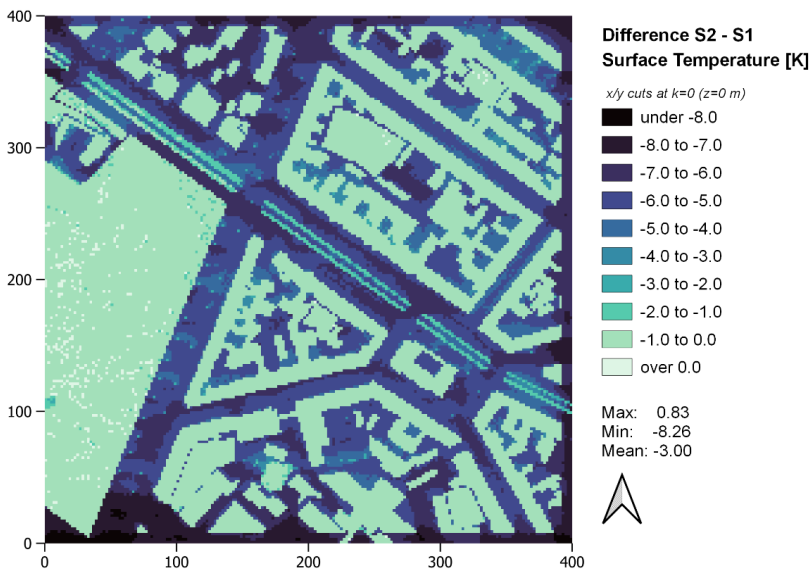
Color:  ▾

Parameter	Value
Alternative Name	(None)
CO2 Fixation Type	C3
Leaf Type	Gras
Albedo	0.20000
Emissivity	0.97000
Transmittance	0.30000
Plant height	0.04500
Root Zone Depth	0.05300
Leaf Area (LAD) Profile	0.97020,0.97020,0.97020,0.97020,0.97020,0.97020,0.97020,0.97020,0.97020,0.97020
Root Area (RAD) Profile	0.10000,0.10000,0.10000,0.10000,0.10000,0.10000,0.10000,0.10000,0.10000,0.00000
Season Profile	0.80000,0.80000,0.80000,1.00000,1.00000,1.00000,1.00000,1.00000,1.00000,0.80000,0.80000,0.80000

Figure 4: Parameterization of the grass growing above the GGPs (own illustration in ENVI-met DBManager).



710 **Figure 5: Representation of the surfaces, vegetation and 3D model domain for the designed scenarios (S1 = reference run without any GGP but asphalt in all streets (black-coloured surfaces), S2 = extreme scenario: GGP implementation on all sealed surfaces (grey-coloured surfaces), S3 = realistic scenario: usage compatible GGP implementation on low-traffic areas while lanes of the main traffic roads Volksgartenstraße (W to E) and Vorgebirgsstraße (N to S) are still sealed).**



715 **Figure 6: Spatial distribution of the mean differences in surface temperature [K] between S1 (reference run) and S2 (extreme scenario) over the entire 72-hour simulation period (18th - 20th July 2022). The x and y axes indicate the spatial distance in the study area [in m].**

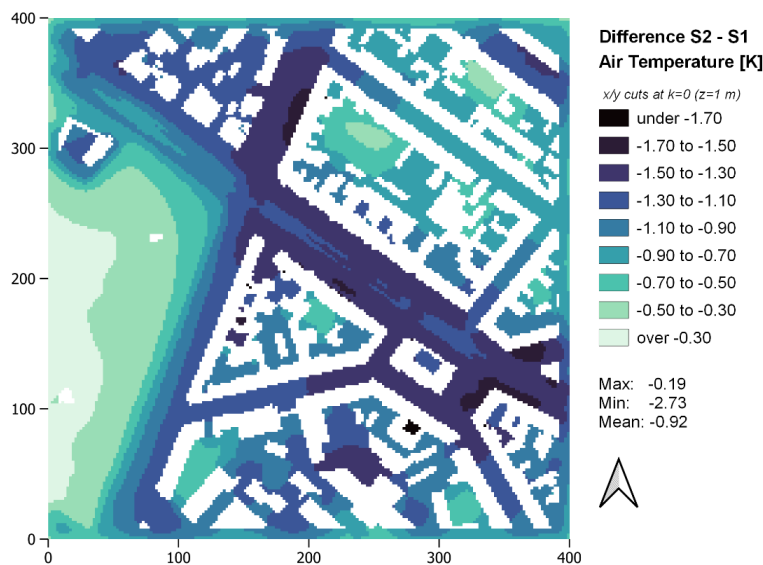
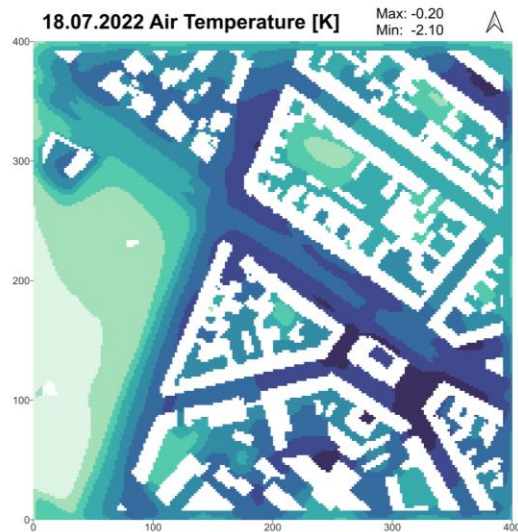
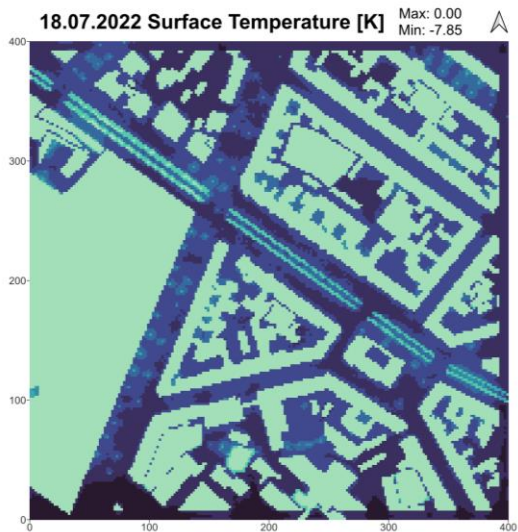
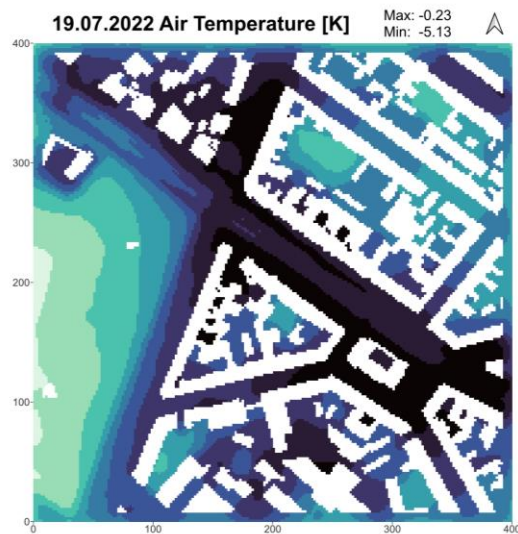
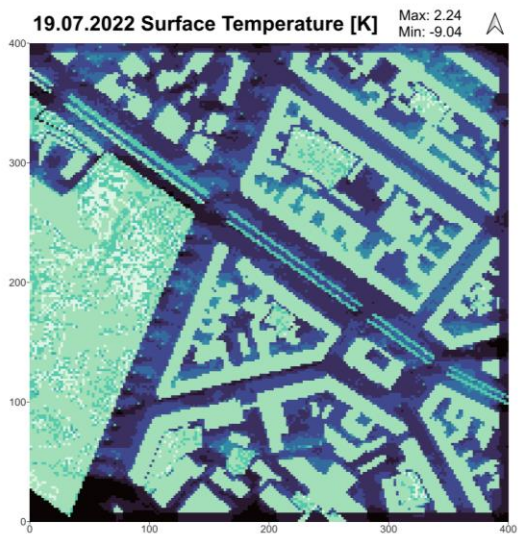
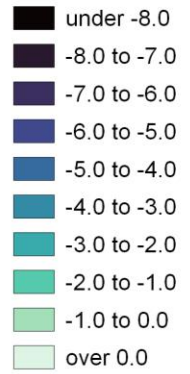


Figure 7: Spatial distribution of the mean differences in 1 meter height air temperature [K] between S1 (reference run) and S2 (extreme scenario) over the entire 72-hour simulation period (18th - 20th July 2022). The x and y axes indicate the spatial distance in the study area [in m].



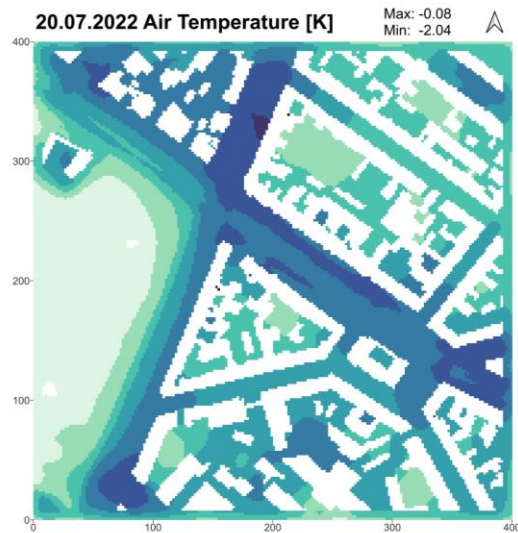
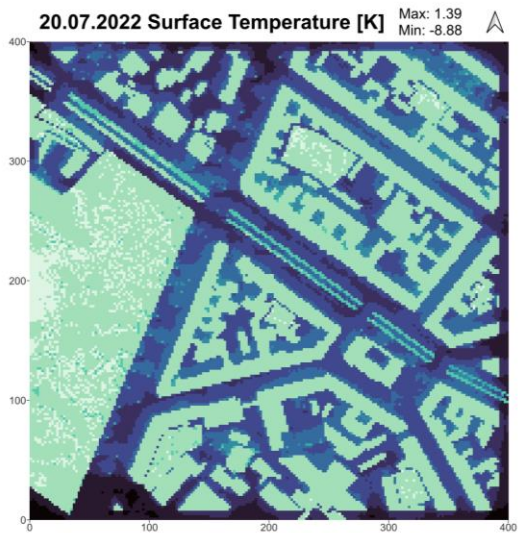
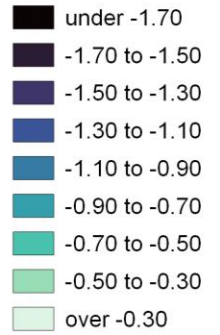
**Difference S2 - S1
Surface Temperature [K]**

x/y cuts at k=0 (z=0 m)



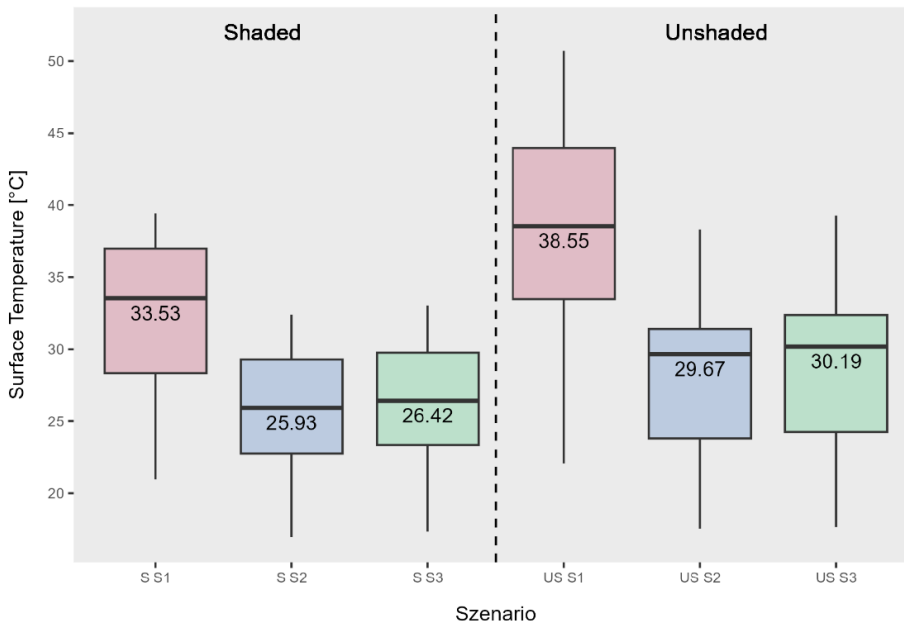
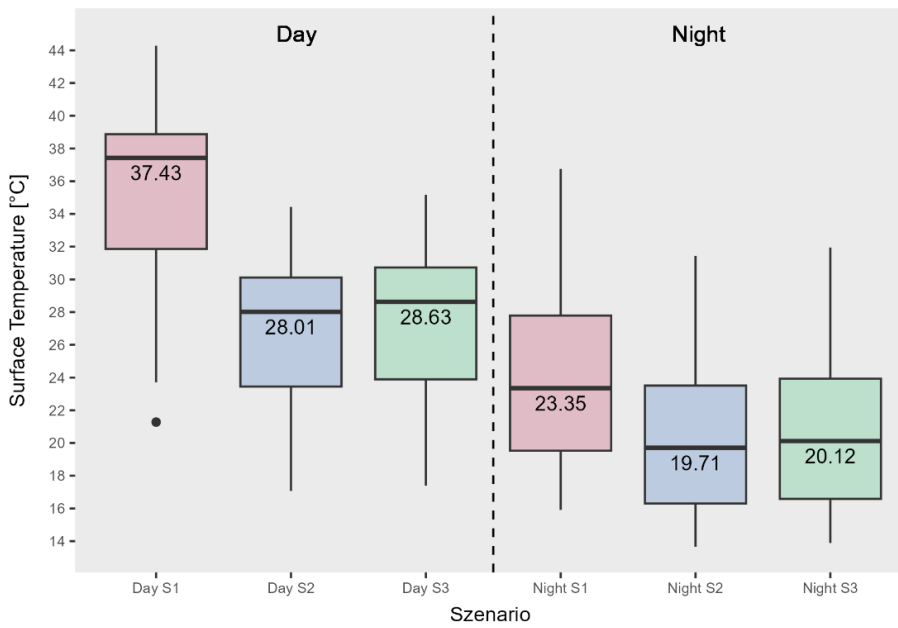
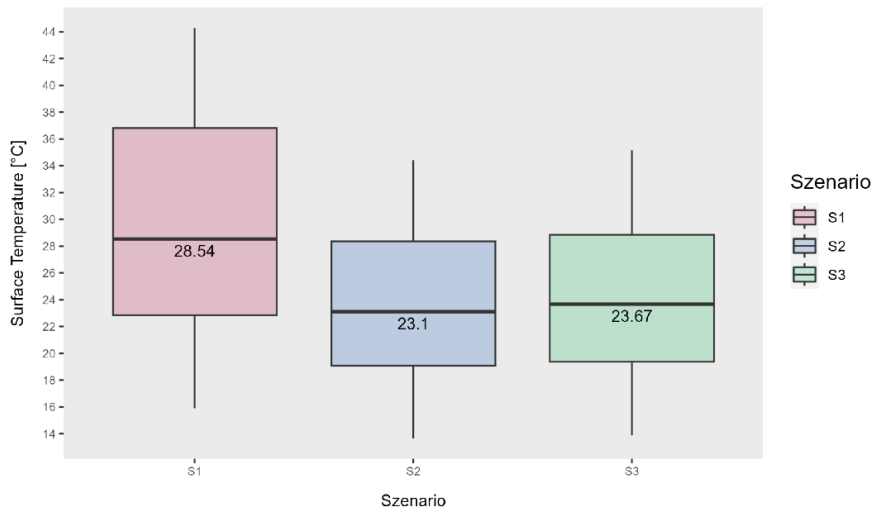
**Difference S2 - S1
Air Temperature [K]**

x/y cuts at k=0 (z=1 m)



720

Figure 8: Spatial distribution of the mean differences in surface temperature [K] (left) and air temperature [K] (right) between S1 (reference run) and S2 (extreme scenario) for all three single days of the study period. The x- and y-axes indicate the spatial distance in the study area [in m].



725 **Figure 9a (above):** Boxplots of the mean surface temperature for the three simulations S1, S2 and S3. Averages of all GGP grid cells for the 72 hourly output values.

Figure 9b (middle): Boxplots of the mean surface temperature for the three simulations S1, S2 and S3 divided into daytime (left) and nighttime (right). Averages of all GGP grid cells for the 72 hourly output values.

730 **Figure 9c (below):** Boxplots of the mean surface temperature for the three simulations S1, S2 and S3 divided into shaded areas (left) and unshaded areas (right). Averages of all GGP grid cells for the 72 hourly output values.

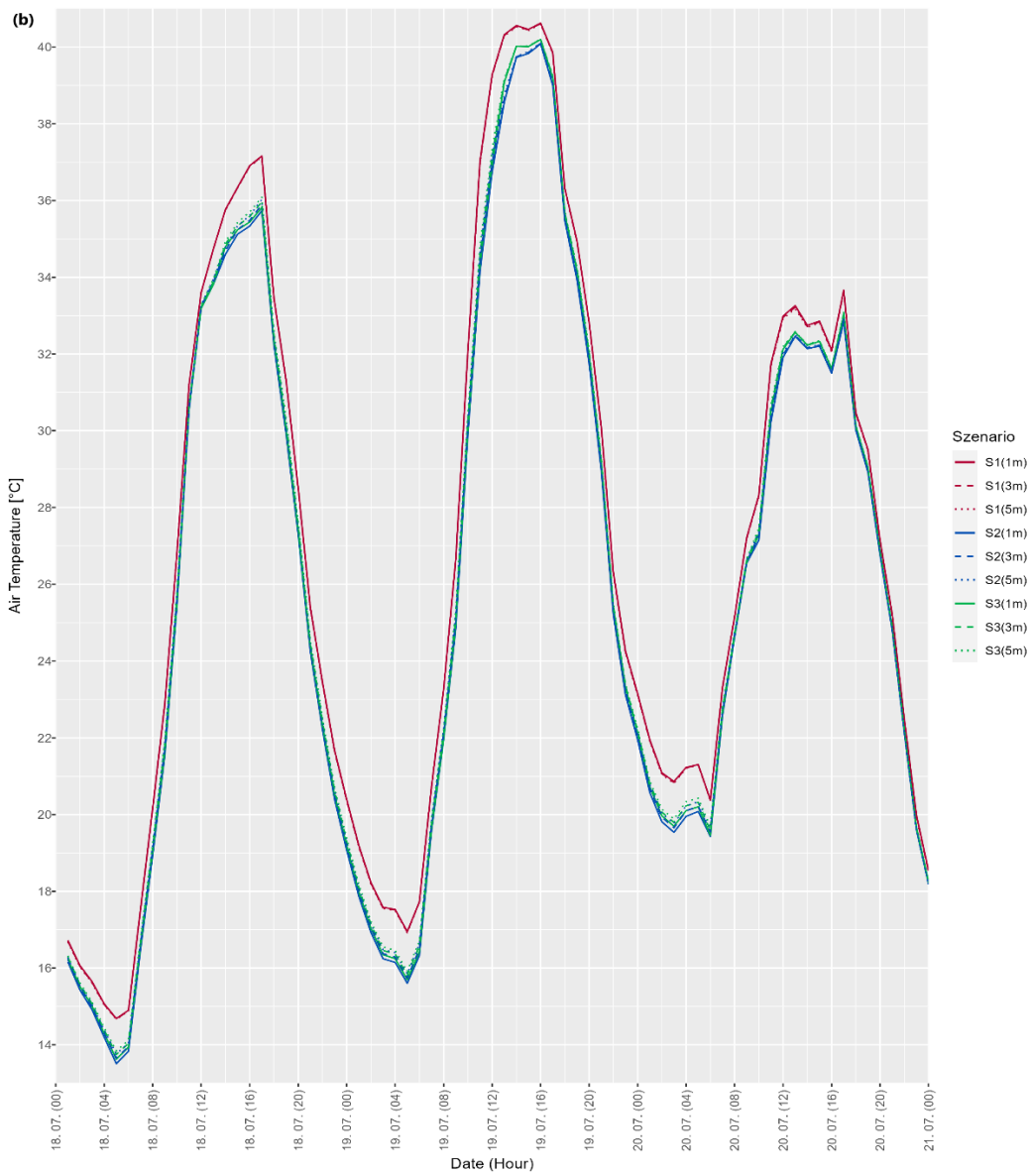
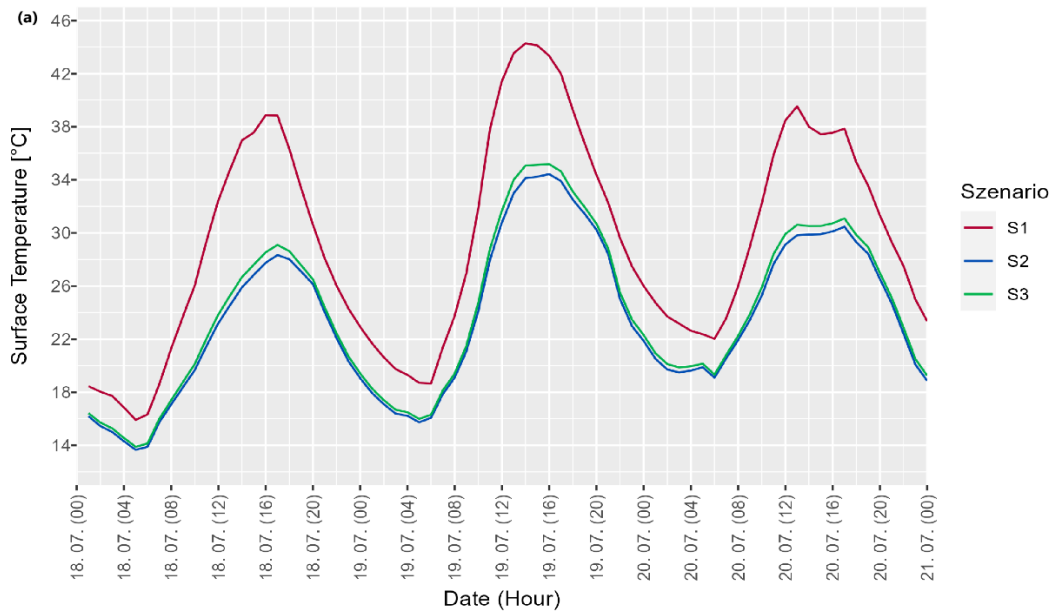


Figure 10a (above): Hourly time series of the mean surface temperature of all GGP grid cells in the model domain for the simulations S1, S2 and S3.

Figure 10b (below): Hourly time series of the mean air temperature of all atmosphere grid cells in the model domain in 1 m height above ground level (solid lines), in 3 m height above ground level (dashed lines), and in 5 m height above ground level (dotted lines) each for the simulations S1, S2 and S3.

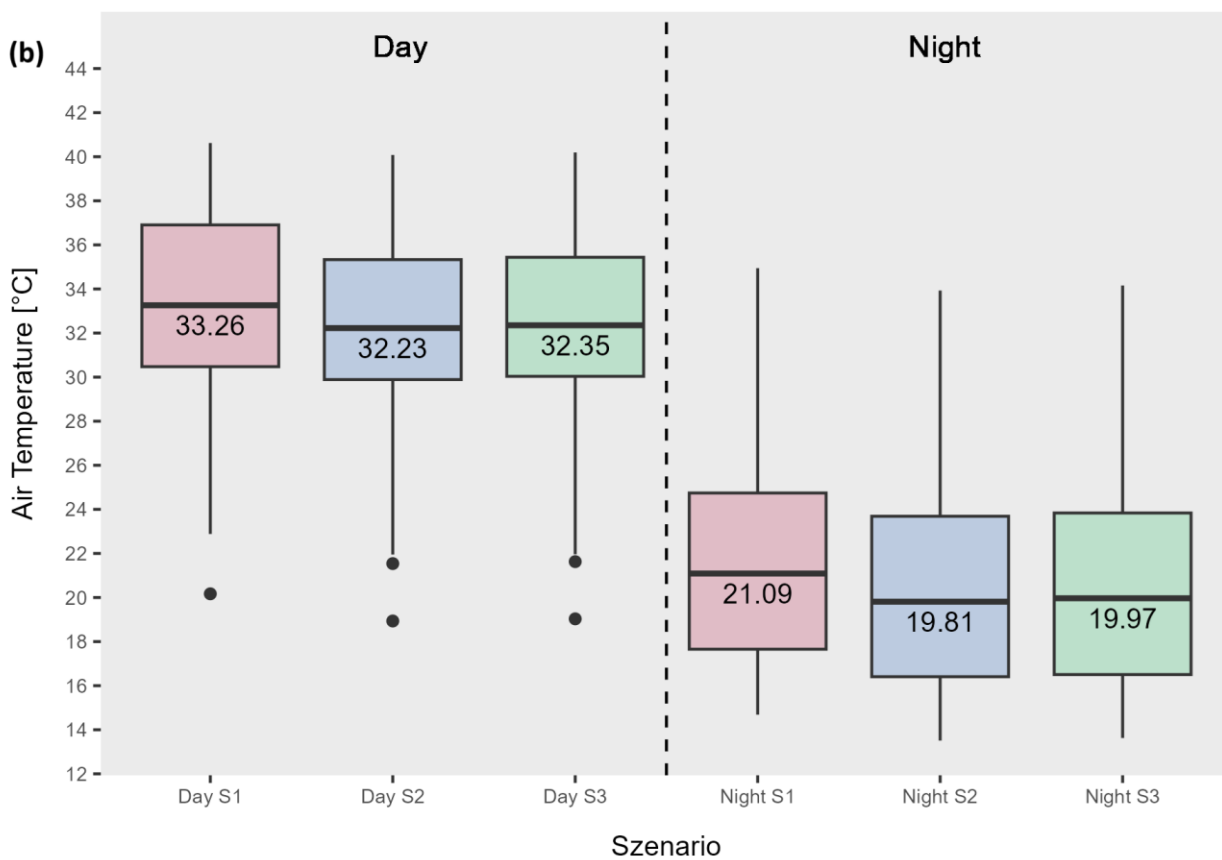
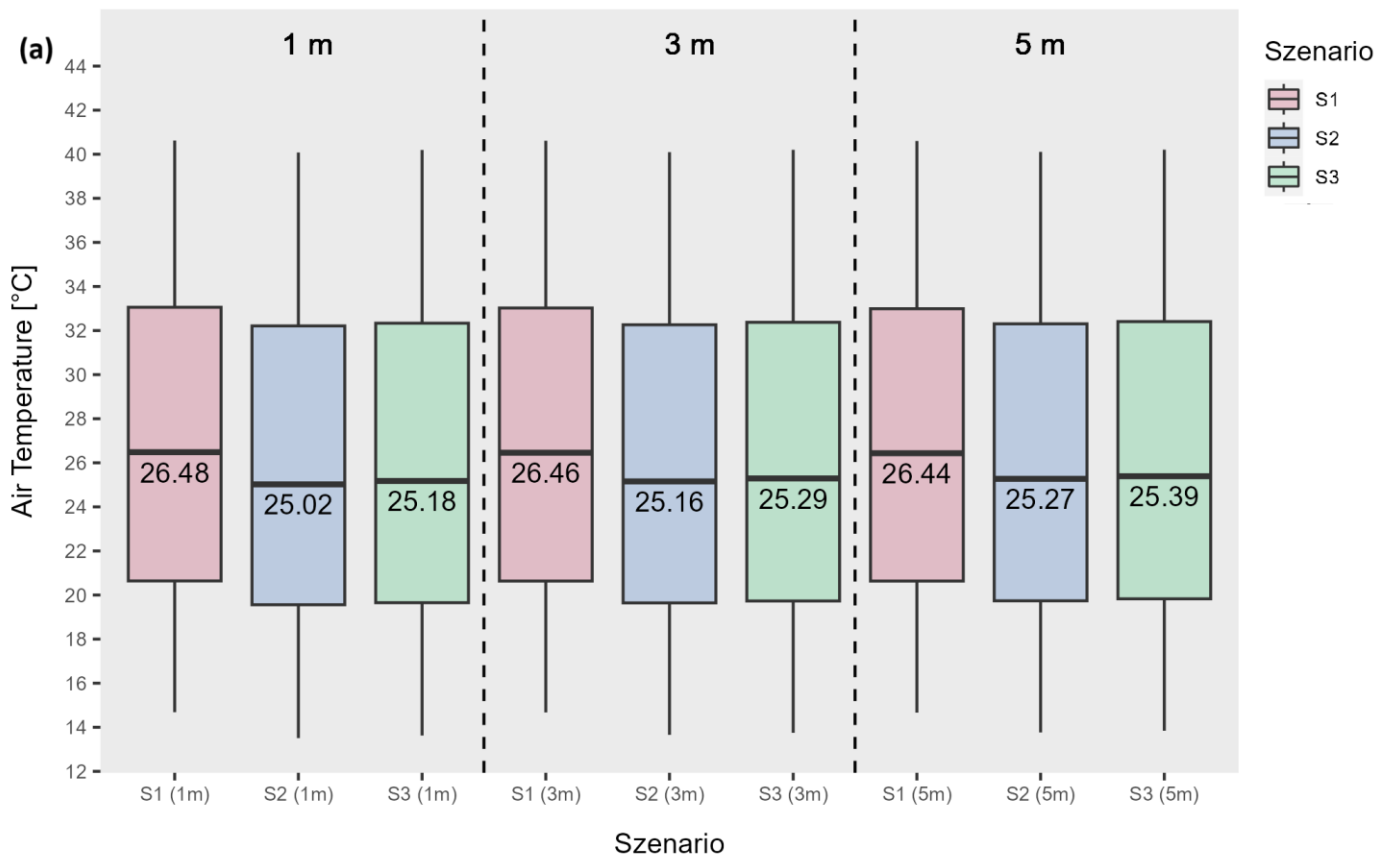
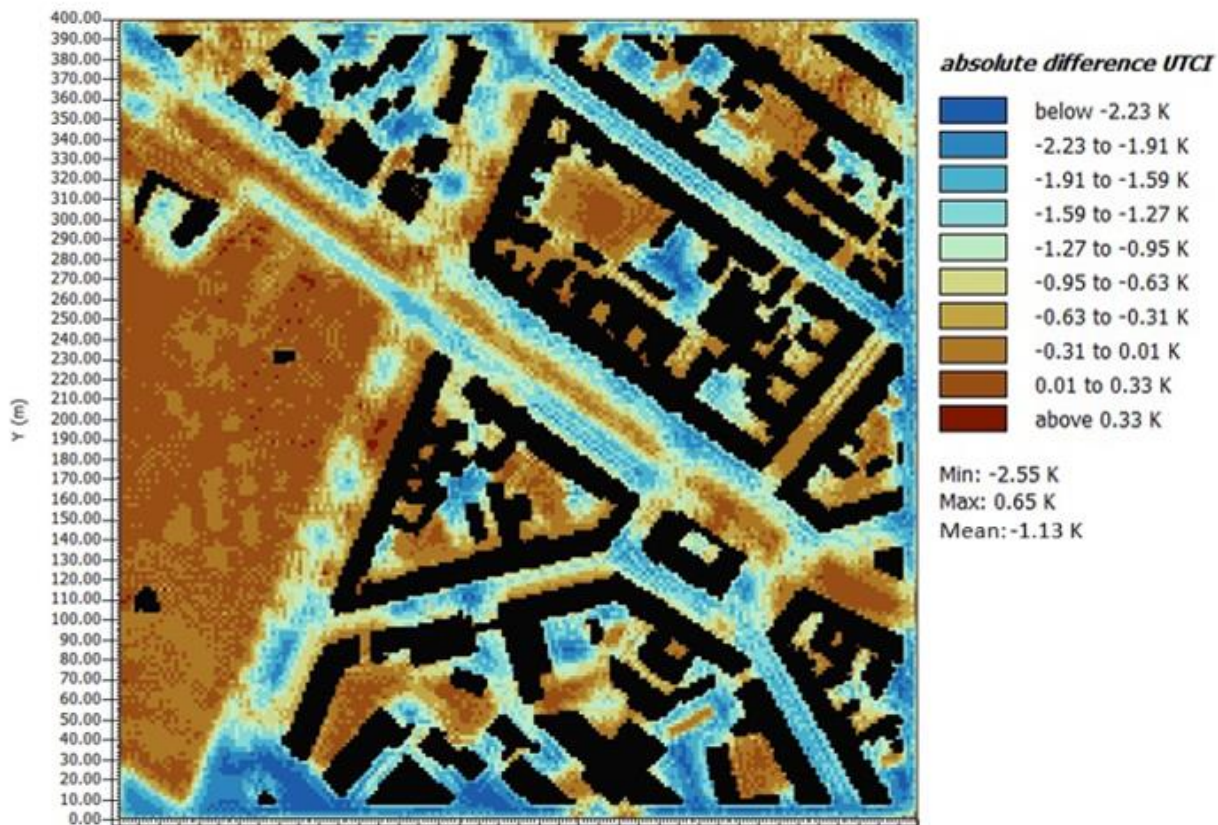


Figure 11a (above): Boxplots of the mean air temperature for the three simulations S1, S2 and S3 in 1 m height above ground level (left), 3 m height above ground level (middle), and 5 m height above ground level (right). Averages of all GGP grid cells for the 72 hourly output values.

Figure 11b (below): Boxplots of the mean air temperature in 1 m height above ground level for the three simulations S1, S2 and S3 divided into daytime (left) and nighttime (right). Averages of all GGP grid cells for the 72 hourly output values.



745 **Figure 12:** Absolute difference in the biometeorological Universal Thermal Climate Index (UTCI) between the reference run S1 and the extreme scenario S2 in a height of 1 m above ground level.

Appendix 1: Absolute difference in the biometeorological index Physiological Equivalent Temperature (PET) between the reference run S1 and the extreme scenario S2 in a height of 1 m above ground level.

750 **Appendix 2:** Table of significance test results (p-values of t-tests) for Ts divided into daytime, nighttime, shaded and unshaded, as well as for Ts divided into 1 m, 3 m, and 5 m height above ground level for the S2 and S3 in relation to S1 each.

Code/Data availability

The exact version (V 5.1.2 Compatibility Release) of the ENVI-met model used for this paper, the parameterizations and the input data to run the ENVI-met model and to reproduce the model outputs of all the performed scenario simulations shown in this paper, as well as all the scripts for post-processing of the model output data needed to derive the presented results of this manuscript are permanently archived as supplementary material files on the Zenodo repository (EINGRÜBER et al., 2024b).

Author contributions

NE developed the model domain and setup the ENVI-met microclimate model for the study area. AD performed the field measurements in the study area for the GGP parameterization, and statistically analysed the simulation outputs. KS and WK supported in the implementation of the modelling concept and data analyses. NE and AD prepared the manuscript draft. KS and WK participated in writing and supervising the work. All have read and accepted the manuscript for submission.

Competing interests

The contact author has declared that none of the four authors has any competing interests.

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Acknowledgements

770 We would like to thank all citizen scientists and local cooperation partners within the study area who make it possible to carry out our measurements in private spaces. We acknowledge partial financial support for the project from the Gesellschaft für Erdkunde zu Köln (GfE), and financing of the Article Processing Charge from the DFG (German Research Foundation, grant no. 491454339).

Financial support

775 We acknowledge partial financial support for the project from the Gesellschaft für Erdkunde zu Köln (GfE), and financing of the Article Processing Charge from the DFG (German Research Foundation, grant no. 491454339). This open-access publication was funded by Universität zu Köln.

500-character short summary

780 Climate change adaptation measures like unsealings can reduce urban heat stress. As grass grid pavers have never been parameterized for microclimate model simulations with ENVI-met, a new parameterization was developed based on field measurements. To analyse the cooling potential, scenario analyses were performed for a densely-developed area in Cologne. Statistically significant average cooling effects of up to -11.1 K were found for surface temperature, and up to -2.9 K for 1 m air temperature.