The development, parametrisation and evaluation of the DO<sub>3</sub>SE-crop model for Xiaoji, China – Supplementary Material

## S1a. Resistance and diffusivity of gases across leaf boundary layers

The leaf-level quasi laminar boundary layer resistance term  $r_b$  (McNaughton and van der Hurk, 1995) incorporates empirically derived constants for heat and gas conductance (see Table S1, in mol TLA m<sup>-2</sup> s<sup>-1</sup>), cross-wind leaf dimension L (given in m) and the wind speed at the leaf surface u(h) (given in m/s). N.B. TLA is Total Leaf Area.

**Table S1**. Empirically derived constant conductance (mol TLA  $m^{-2} s^{-1}$ ) (and resistance (PLA s/m)) values for heat and gas (H<sub>2</sub>O, CO<sub>2</sub> and O<sub>3</sub>) from a single leaf surface.

Matter	Conductance (mol TLA m <sup>-2</sup> s <sup>-1</sup> )	Resistance (PLA s/m)
		Rounded down
Heat	0.135	150
Water vapour, H <sub>2</sub> O	0.147	139
Carbon dioxide, CO <sub>2</sub>	0.110	186
Ozone, O <sub>3</sub>	0.105	195

N.B. The conversion of constants from conductance to resistance is achieved by multiplying by 2 to convert from single surface to PLA, dividing by 41 to convert from mol  $m^{-2} s^{-1}$  to m/s, and calculating the reciprocal to give a resistance term (e.g. for heat the conversion is 1/(0.135\*2)/41 which gives 151.85 and is then rounded down to 150).

Leaf boundary layer resistance for heat (for forced convection)  $(r_{b,heat})$  can be calculated according to eq. [S1] after (Campbell, G.S., Norman, 1998), using the 150 value for boundary layer resistance to heat in s/m, these formulations take into account both sides of the leaf and therefore provide  $r_{b,heat}$  for PLA (Projected Leaf Area)).

$$r_{bheat_{forced}} = 150. \sqrt{\frac{L}{u(h)}}$$
[S1]

To estimate boundary layer resistance values for other gases simply substitute the relevant gas constant for resistance into eq. [S1].

### S1b. Diffusivities of gases for stomatal conductance

The conversion factors are derived from Graham's law which assumes that the ratio of the diffusivities is equal to the inverse of the square root of the ratio of molecular weights (as described in (Campbell, G.S., Norman, 1998)).

e.g. mol  $H_2O m^{-2} s^{-1} = 0.61 mol O_3 m^{-2} s^{-1}$ 

mol CO<sub>2</sub> m<sup>-2</sup> s<sup>-1</sup> = 0.96 mol O<sub>3</sub> m<sup>-2</sup> s<sup>-1</sup>

Molecular	Ratio of	Ratio of	Ratio of	Inverse	Inverse	Inverse
weight	molecular	molecular	molecular	sq. root	sq. root	sq. root
	weights	weights	weights	of ratio of	of ratio of	of ratio of
	(to H <sub>2</sub> O)	(to CO <sub>2</sub> )	(to O₃)	molecular	molecular	molecular
				weight (to	weight (to	weight (to
				H₂O)	CO <sub>2</sub> )	O <sub>3</sub> )

H₂O	18	1	0.409	0.375	1	1.56	1.63
CO <sub>2</sub>	44	2.44	1	0.92	0.64	1	1.04
O <sub>3</sub>	48	2.67	1.09	1	0.61	0.96	1

### S2. Irradiance absorption by the canopy

Solar radiation is the key determinant of the productivity of any crop. The radiation absorbed (direct and diffuse) photosynthetically active radiation,  $PAR_{tot}$  (in W/m<sup>2</sup>)) by crops will have a direct impact on canopy photosynthesis (and associated stomatal conductance) and affect crop leaf phenology and hence net primary productivity (*NPP*). *PAR* absorbed by crops is divided into two categories, direct (*PAR<sub>dir</sub>*) and diffuse (*PAR<sub>diff</sub>*) radiation. *PAR<sub>dir</sub>* is the *PAR* which reaches the crop leaf surface without being scattered, whereas *PAR<sub>diff</sub>* can be naturally (by cloud cover and naturally occurring particles in the atmosphere) or artificially scattered (e.g. by pollutant aerosol). *PAR* can also be reflected by surfaces.

To estimate the total irradiance ( $PAR_{tot}$  which is equal to  $PAR_{dir} + PAR_{diff}$ ) incident on sunlit and shaded parts of the canopy we use the method of (De Pury and Farquhar, 1997).

### S2a. Total Photosynthetic Active Radiation (PAR<sub>tot</sub>)

PAR absorbed per unit leaf area is divided into  $PAR_{dir}$ ,  $PAR_{diff}$  which also includes scattered (rereflected by the canopy) beam calculated by,

$$PAR_{dir} (LAI) = (1 - \rho_{cb}(\beta)) K_b' I_b(0) \exp(-k_b' LAI)$$
[S1]

Where,  $\rho_{cb}(\beta) = 1 - \exp[\frac{2\rho_h k_b}{1+k_b}]$  -eq.S2;  $K_b$ 'is beam and scattered beam PAR extinction coefficient ;  $I_b(0)$  is the initial beam irradiance, representing the intensity of direct sunlight before it interacts with the canopy

$$PAR_{diff} (LAI) = (1 - \rho_{cd}) k_d' I_d(0) exp(-k_d'LAI)$$
[S3]  
Where,  $\rho_{cd} = \frac{1}{I_d(0)} \int_0^{\frac{\pi}{2}} N_d (\alpha) \rho_{cb} (\alpha) d\alpha$ -eq.[S4];  
 $K'_d$  is diffuse and scattered diffuse PAR extinction coefficient

The total absorbed irradiance per unit leaf area is calculated as:

$$PAR_{total} = PAR_{dir} (LAI) + PAR_{diff} (LAI)$$
[S6]

Estimations of the direct, diffuse and scattered (re-reflected) irradiance are necessary to calculate the *PAR* incident on the sunlit (*LAI*<sub>sun</sub>) and shaded (*LAI*<sub>shade</sub>) portions of the canopy, which are then calculated based on the equations described below:

### S2b. Total irradiance absorbed as shaded leaves ( $I_{lsh}$ (LAI))per unit leaf area are calculated as ;

$$PAR_{sh}(LAI) = PAR_{diff}(LAI) + PAR_{bs}(LAI)$$
[S7]

where  $PAR_{diff}(LAI)$  is diffuse irradiance (see eq.) and  $PAR_{bs}(LAI)$ , direct scattered beam (another form of diffuse radiation) is calculated as:  $PAR_{bs}(LAI) = PAR_b$  (0) [ $PAR_{dir} - (1 - \sigma)k_bexp(-k_bLAI)$ } [S8]

#### S2c. Total irradiance absorbed by per unit leaf area of the sunlit leaf

$$PAR_{sun}(LAI,\beta) = PAR_{sh}(LAI) + PAR_{bsun}(\beta)$$
[S9]

Where;  $PAR_{sh}$  (*LAI*) is irradiance absorbed by shaded leaves (see equation S7) and  $PAR_{bsun}$  ( $\beta$ ), beam irradiance absorbed by sunlit leaves and calculated as below:

$$PAR_{bsun}(\beta) = (1 - \sigma)I_b(0)\frac{\cos_{\alpha l}}{\sin\beta}$$
[S10]

#### **S3.** Solar elevation Angle

 $sin\beta$  which is defined as the solar elevation angle, varies over the course of the day as a function of latitude and day length as described in eq. 8, this eq. and the other solar geometry equations required for its calculation are taken from Campbell & Norman, (1998).

$$\sin\beta = \sin\lambda \cdot \sin\delta + \cos\lambda \cdot \cos\delta \cdot \cos hr$$

where  $\beta$  is the solar elevation above the horizontal,  $\lambda$  is the latitude,  $\delta$  is the angle between the sun's rays and the equatorial plane of the earth (solar declination), *hr* is the hour angle of the sun and is given by [15(t-t0)] where *t* is time and *t<sub>o</sub>* is the time at solar noon.

The solar declination ( $\delta$ ) is calculated according to eq. 9.

$$\delta = -23.4cos[360(td + 10)/365]$$
S12

where  $t_d$  is the year day.

The time, t is in hours (standard local time), ranging from 0 to 23. Solar noon  $(t_s)$  varies during the year by an amount that is given by the equation of time (e, in min) and calculated by:-

$$t_o = 12 - LC - e$$

where LC is the longitude correction. LC is + 4 or -4 minutes for each degree you are either east or west of the standard meridian. e is a 15 to 20-minute correction, which depends on the year day according to eq. 11.

$$e = \frac{-104.7 \sin f + 596.2 \sin 2 f + 4.3 \sin 3 f - 12.7 \sin 4 f - 429.3 \cos f - 2.0 \cos 2 f + 19.3 f}{3600}$$

where  $f = 279.575 + 0.9856 t_{d}$  in degrees.

It is also necessary to calculate the day length so that the hour angle of the sun can be calculated throughout the day. Day length is defined as the number of hours that the sun is above the horizon and requires the hour angle of the sun, hr, at sunrise or sunset to be calculated with eq. S14.

$$\cos hr = -tan\lambda.tan\delta$$
 S14

so that day length in hours equals 2hr/15.

Parameters	Description	Value	Units
K <sub>b</sub> '	Beam and scattered beam PAR extinction coefficient	0.46/sinβ	
K <sub>d</sub> '	Diffuse and scattered diffuse PAR extinction coefficient	0.719	
$ ho_{cb}$	Canopy refection coefficient for beam PAR		
$ ho_{cd}$	Canopy reflection coefficient for diffuse PAR		
β	Solar elevation angle		Radians
δ	Solar declination angle		Radians
I <sub>lb</sub> (LAI)	Absorbed beam plus scattered beam PAR per unit leaf area		$\mu mol m^{-2} s^{-1}$
I <sub>ld</sub> (LAI)	Absorbed diffuse plus scattered diffuse PAR per unit leaf area		$\mu mol m^{-2} s^{-1}$
$I_l$ (LAI)	Total absorbed PAR per unit leaf area		$\mu mol m^{-2} s^{-1}$
$I_b$ (LAI)	Direct PAR per unit ground area		$\mu mol \ m^{-2} \ s^{-1}$
$I_d$ (LAI)	Diffuse PAR per unit ground area		$\mu mol \ m^{-2} \ s^{-1}$
$I_d$ (0)	Diffuse PAR per unit ground area at the top of the canopy		$\mu mol \ m^{-2} \ s^{-1}$
<i>I<sub>b</sub></i> (0)	Beam PAR per unit ground area at the top of the canopy		μmol m <sup>-2</sup> s <sup>-1</sup>
I <sub>lbb</sub> (LAI)	Absorbed beam PAR without scattering per unit leaf area		$\mu mol \ m^{-2} \ s^{-1}$
I <sub>bs</sub> (LAI)	Absorbed scattered beam PAR per unit leaf area		μmol m <sup>-2</sup> s <sup>-1</sup>
I <sub>lbsun</sub> (LAI)	Beam PAR absorbed by sunlit leaves per unit leaf area		µmol m <sup>-2</sup> s <sup>-1</sup>
I <sub>lsh</sub> (LAI)	Beam PAR absorbed byshaded leaves per unit leaf area		$\mu mol \ m^{-2} \ s^{-1}$

Table S2. Variables and parameters used to calculate the multi-layer canopy irradiance after De Pury and Farquhar (1997).

I <sub>lsun</sub> (LAI)	Total PAR absorbed by sunlit leaves per unit leaf area		$\mu mol \ m^{-2} \ s^{-1}$
(LAI)	Cumulative leaf area index from top of canopy (L=0 at top)		$m^2 m^{-2}$
$f_{1,2}$ (LAI)	Fraction of leaf area in a leaf-angle class		
f <sub>sh</sub> (LAI)	Fraction of leaves that are shaded		
f <sub>sun</sub> (LAI)	Fraction of leaves that are sunlit		
σ	Leaf scattering coefficient for PAR	0.15	
α <sub>1</sub>	Angle of beam irradiance to the leaf normal	0.5	Radians

## **S4.** Methodology for gap-filling and standardisation of data for AgMIP Ozone

This document describes the methodological approach that was applied in order to search for gaps and quality issues in time-series (gas concentration and meteorological) datasets, and the approach used for filling gaps.

Where gaps had already been filled by the team collecting the data then this interpolated data was left under the assumption that it would be a more accurate reflection of the experimental conditions.

Gap filling methodology for hourly data : During the data standardisation process some data gaps were identified. These ranged in size from a single hour of missing data, to several consecutive hours, to several consecutive days, weeks, or even months. A requirement of input data for modellers is that it is continuous; the following gap filling methodology was therefore devised. These gap filling methods are only applied for the duration of the plants growing season (i.e. between sowing and harvest):

Single hours of missing data were filled by taking the average of the hourly values coming the hour before, and the hour after, the missing value.

Several consecutive hours of missing data (23 hours or less) were filled by taking the average of the corresponding hour the day before, and the day after; and repeating this for each missing hour of data. If data were unavailable from that hour of the previous day, then only the value from the day after was used and vice versa. If there is no data available in either the day before or after, then the method is used (see below point 2.).

Gaps larger than 24 hours could be filled using the following methods:

1. Gaps between 24 hours and 168 hours (i.e. from 1 day up to 1 week) would be filled with the averages from that same hour of the equivalent day, the week before and the week after (i.e. averaging 2 numbers). If data were unavailable from those hours

of the previous week, then only the values from the week after would be used (and vice versa).

2. Gaps longer than 1 week would be filled with the diurnal averages from one week before and after the period of missing data (i.e. potentially averaging 14 hours of data, but in cases where data is sparse then it could only be a couple of hours). Gap filled values would not be used in calculating averages. Where data is daily, i.e. some meteorological data, the average of the 7 days before and/or after is used.

There were some instances where data gaps extended for several months. For these extensive gaps, the following methods were used:

- A. All datasets from Xiaoji, China, had about a 4-month gap in meteorological and ozone data at the start of the growing season. At this stage of the growing season, plants will either have not yet emerged or have a very small LAI and therefore any ozone uptake would have been minimal. Ozone gaps were filled with the diurnal averages of the first two weeks of the ambient experimental data for each year. Meteorological data was filled using Nasa Power data (https://power.larc.nasa.gov/data-access-viewer/). The variables selected are in the appendix below. In Xiaoji China, global radiation was measured, whereas the Nasa Power data platform only provides Photosynthetically Active Radiation (PAR). To convert global radiation to PAR, values were multiplied by two and divided by 24 to be comparable with global radiation in MJ/m2/hour.
- B. If the gap occurs before exposure data begins then the ambient or non-filtered treatment is gap filled using the above methodology and then this data is used for all treatments to ensure that concentrations are not overestimated. If there is no ambient treatment then averages of the treatment closest to ambient is used. If there are gaps in gas data after the beginning of exposure date, then averages from that treatment are used (as opposed to ambient). If no date for start of exposure is provided, then exposure is assumed to start when the gas data begins (even if it is na). Similarly, once exposure has ended then only averages from the period after exposure were used. If there was not enough data to base averages on then ambient data was used (Nottingham 1996).
- C. Any ozone values of less than 0 were treated as gaps and filled following the above methods, depending on the size of gap.
- D. If mean air temperature was not available but minimum and maximum air temperature was, the average of these two values was used and the source of the data was label 'c' for calculated.
- E. Sections of the dataset which had been gap filled were clearly identified using a categorisation system in an adjacent 'data source' column, so that these data could be identified at a later stage, and so that alternative measured or modelled data could be sought. The percentage of gap-filled data within the total time-series for each gas concentration and meteorological variable was also reported in the readme file accompanying each dataset.
- F. The Parameters downloaded from (<u>https://power.larc.nasa.gov/data-access-viewer/</u>)
- G. Hourly data was downloaded from the Nasa Power data access viewer for Xiaoji, China to fill gaps in meteorological data. The following parameters were selected: 1. Agroclimatology community; 2. Hourly; 3. Lat/long: 32.58333: 119.7; 4. Time extent: Determined by data gap in each year; 5. Format: CSV format; 6. Parameters: a) temp at 2m, b)relative humidity at 2m, c)wind speed at 2m, d) precipitation, e) radiation: "All Sky Surface photosynthetically active radiation" (PAR Total) (MJ/m<sup>2</sup>/day). This was converted to hourly global radiation (MJ/m<sup>2</sup>/h) by dividing to 24 and multiplying with 2 because PAR ~ 0.5 \* global radiation

### S4. O<sub>3</sub> Resistance

### **Atmospheric Resistance**

$$r_a = \frac{1}{K u^*} \left( \log \left( \frac{z_2}{z_1} \right) - \Psi_h \left( \frac{z_2}{L} \right) + \Psi_h \left( \frac{z_1}{L} \right) \right)$$

 $u^*$  Friction velocity m/s

- *K* Von Karman's constant
- *L* Monin-Obukhov length m
- $z_1$  Lower height m
- $z_2$  Upper height m
- $\Psi_h$  Flux-gradient stability function for heat

#### Heat flux

$$\Psi_h(x) = \begin{cases} 2\log\left(\frac{1+\sqrt{1-16x}}{2}\right) & x < 0\\ -5x & x \ge 0 \end{cases}$$

Quasi-laminar boundary layer resistance

$$r_{b,03} = \frac{2}{Ku^*} \left( \frac{\left(\frac{V}{diff}\right)}{PR} \right)^{\frac{2}{3}}$$

 $u^*$  Friction velocity m/s

*K* Von Karman's constant

- V Kinematic viscosity of air at 20°C m<sup>2</sup>/s
- diff Molecular diffusivity in air m<sup>2</sup>/s

PR Prandtl number

In-canopy resistance

$$r_{inc} = 14 \frac{SAI h}{u^*}$$

External plant cuticle resistance

$$r_{ext} = \frac{2500}{SAI}$$

Stomatal resistance

$$r_{sto} = \min\left(100000, \frac{41000}{g_{sto}}\right)$$

Surface resistance per layer

$$r_{c} = \begin{cases} r_{b} + \frac{1}{\left(\frac{1}{r_{sto}} + \frac{1}{r_{ext}}\right)} & LAI > 0\\ r_{b} + r_{ext} & SAI > 0 \end{cases}$$

**S5**. The timing of crop emergence, anthesis and harvest

Fig S1. The Chinese FACE-O3 dataset were used to plot modelled phenological stages against experimental dataset for the year a) 2008 (training set) and b) 2007 and 2009 (testing set)



**Fig S2.** The Chinese FACE-O3 dataset were used to plot modelled grain dry matter  $(g/m^2)$  against experimental dataset for the year 2008 for tolerant (Y16) and sensitive cultivar (Y2) (training set)



# Table S3. DO₃SE-Crop variables

Variable	Unit	Description
T <sub>eff</sub>	°C days	Effective temperature accumulated between sowing to maturity
DVI	-	Development index
T <sub>air</sub>	°C	Surface air temperature in degrees Celsius
T <sub>air,k</sub>	degrees Kelvin	Surface air temperature in Kelvin
T <sub>min</sub>	°C	Daily minimum surface air temperature
T <sub>max</sub>	°C	Daily maximum surface air temperature
V <sub>dd</sub>	days	Accumulated vernalised days
V	days	Vernalised days
$V_d$	days	Devernalised days
VF	-	Vernalisation factor
PP	hrs	Photoperiod
PF	-	Photoperiod factor
A <sub>net</sub>	µmol CO <sub>2</sub> m <sup>-2</sup> s <sup>-1</sup>	Net photosynthesis or rate of CO <sub>2</sub> assimilation
A <sub>c</sub>	µmol CO <sub>2</sub> m <sup>-2</sup> s <sup>-1</sup>	RuBP (ribulose-1,5-bisphosphate) limited $A_{net}$
$A_j$	µmol CO <sub>2</sub> m <sup>-2</sup> s <sup>-1</sup>	Electron transport limited A <sub>net</sub>
$A_p$	µmol CO <sub>2</sub> m <sup>-2</sup> s <sup>-1</sup>	TPU (triose phosphate) limited $A_{net}$
R <sub>d</sub>	µmol CO <sub>2</sub> m <sup>-2</sup> s <sup>-1</sup>	Dark respiration
$f_{sw}$	-	Plant available soil water stress factor
ASW	m <sup>3</sup> /m <sup>3</sup>	Plant available soil water
$C_i$	µmol/mol	Intercellular CO <sub>2</sub> partial pressure
<i>O</i> <sub><i>i</i></sub>	mmol/mol	Intercellular O <sub>2</sub> concentrations
Γ*	µmol/mol	CO <sub>2</sub> compensation point in the absence of respiration
Г	µmol/mol	CO <sub>2</sub> compensation point
J	µmol CO <sub>2</sub> m <sup>-2</sup> s <sup>-1</sup>	electron transport rate
VPD	kPa	Leaf to air vapour pressure deficit
$f_{st}$	nmol O3 m <sup>-2</sup> s <sup>-1</sup>	Leaf level stomatal O <sub>3</sub> flux
accf <sub>st</sub>	mmol O3 m <sup>-2</sup>	Accumulated stomatal O <sub>3</sub> flux
$f_{03,s}(d)$	-	Effect of daily cumulative stomatal O <sub>3</sub> flux on $Vc_{max}$
$f_{03,s}(h)$	-	Effect of hourly cumulative stomatal O <sub>3</sub> flux on $Vc_{max}$
$f_{03,s}(d-1)$	-	Previous days effect of cumulative stomatal O <sub>3</sub> flux on $Vc_{max}$
r <sub>03,s</sub>	-	Incomplete overnight recovery of $O_3$ affected $Vc_{max}$
$f_{LA}$	-	Leaf age related capacity to recover from accumulated stomatal O <sub>3</sub> flux
f03 <sub>l</sub>	-	Weighted accumulated stomatal $O_3$ flux that determines the onset of leaf senescence
$f_{LS}$	-	Accumulated stomatal O <sub>3</sub> flux effect on leaf senescence
tl	°C days	Effective temperature accumulated by a leaf after emergence ( $DVI = 0$ )

tl <sub>ep</sub>	-	Effective temperature accumulated by a leaf between full expansion and the onset of leaf
		senescence
$tl_{ep_{03}}$	-	Effective temperature accumulated by a leaf between full expansion and the onset of leaf
		senescence brought forward by O <sub>3</sub>
tl <sub>se</sub>	-	Effective temperature accumulated by a leaf between the onset of leaf senescence and
		maturity
tl <sub>seo3</sub>	-	Effective temperature accumulated by a leaf between the onset of leaf senescence and
		maturity brought forward by $O_3$
<i>g</i> <sub>CO2</sub>	μmol CO <sub>2</sub> PLA m <sup>-2</sup> s <sup>-1</sup>	Stomatal conductance to CO <sub>2</sub>
<i>f</i> <sub>VPD</sub>	-	Relationship between VPD and relative stomatal conductance
C <sub>S</sub>	mol CO₂/mol	Leaf surface CO <sub>2</sub> concentration
C <sub>S</sub>	mol CO₂/mol	Quasi laminar boundary layer surface CO <sub>2</sub> concentration
$g_{bCO2}$	mol m <sup>-2</sup> s <sup>-1</sup>	Quasi laminar boundary layer conductance to CO <sub>2</sub>
Cz	nmol O <sub>3</sub> m <sup>-3</sup>	$O_3$ concentration at reference height (z)
$C_l$	nmol O <sub>3</sub> m <sup>-3</sup>	O <sub>3</sub> concentration at the upper surface of the laminar layer of a leaf
<i>g</i> <sub>03</sub>	mmol O <sub>3</sub> PLA m <sup>-2</sup> s <sup>-1</sup>	Stomatal conductance to O <sub>3</sub> (in mmol O <sub>3</sub> m <sup>-2</sup> s <sup>-1</sup> )
<i>g</i> <sub>03<i>m/s</i></sub>	m/s	Stomatal conductance to $O_3$ (in m/s)
r <sub>c</sub>	s/m	Leaf surface resistance to O <sub>3</sub>
r <sub>b,03</sub>	s/m	Quasi laminar leaf boundary layer resistance to O <sub>3</sub>
$r_a$	s/m	Atmospheric resistance to O <sub>3</sub>
r <sub>inc</sub>	s/m	In-canopy resistance to O <sub>3</sub>
r <sub>ext</sub>	s/m	External plant cuticle resistance to O <sub>3</sub>
r <sub>sto</sub>	s/m	Stomatal resistance to O <sub>3</sub>
u <sub>z</sub>	m/s	Wind speed at a reference height z
$u_l$	m/s	Wind speed at the upper surface of the laminar layer of a leaf
LAI	m <sup>2</sup> m <sup>-2</sup>	Leaf Area Index
PAR <sub>dir,i</sub>	W/m <sup>2</sup>	Direct PAR in canopy layer i
PAR <sub>diff,i</sub>	W/m <sup>2</sup>	Diffuse PAR in canopy layer <i>i</i>
PAR <sub>total</sub>	W/m <sup>2</sup>	Direct and diffuse PAR at the top of the canopy
NPP	kg C m <sup>-2</sup>	Net primary productivity
GPP	kg C m <sup>-2</sup>	Gross primary productivity
$R_p$	kg C m <sup>-2</sup>	Plant respiration
R <sub>pm</sub>	kg C m <sup>-2</sup>	Plant maintenance respiration
R <sub>pg</sub>	kg C m <sup>-2</sup>	Plant growth respiration
A <sub>netc</sub>	kg C m <sup>-2</sup>	Canopy net photosynthesis
R <sub>dc</sub>	kg C m <sup>-2</sup>	Non-water stressed canopy dark respiration
$f_{sw}R_{dc}$	kg C m <sup>-2</sup>	Water stressed modified canopy dark respiration
Croot	kg C m <sup>-2</sup>	Root C pool

C <sub>leaf</sub>	kg C m <sup>-2</sup>	Leaf C pool
C <sub>stem</sub>	kg C m <sup>-2</sup>	Stem C pool
C <sub>resv</sub>	kg C m <sup>-2</sup>	Reserve C pool
$C_{harv}$	kg C m <sup>-2</sup>	Harvest pool
Proot	-	Root C pool partition coefficient
P <sub>leaf</sub>	-	Leaf C pool partition coefficient
P <sub>stem</sub>	-	Stem C pool partition coefficient
P <sub>resv</sub>	-	Reserve C pool partition coefficient
P <sub>harv</sub>	-	Harvest C pool partition coefficient
$C_{leaf,green}$	kg C m <sup>-2</sup>	Green leaf C
C <sub>leaf,brown</sub>	kg C m <sup>-2</sup>	Brown leaf C
SLA	m² kg-1	Specific Leaf Area
h	m	Crop height
Yield <sub>grain</sub>	g C m <sup>-2</sup>	Grain yield

Table S4. DO<sub>3</sub>SE-Crop parameters for wheat. Highlighted are the parameters (and their associated ranges) which require calibration when applying DO3SE-Crop to varying environmental conditions.

Parameter	Unit	Default	Description	Reference	Range	Calibrated
		Value				Parameter
						Value
$T_b$	°C	0	Base temperature	(Tao, Zhang and Zhang, 2012;	-0.5-3	-0.25
				Osborne <i>et al.,</i> 2015)		
$T_o$	°C	20	Optimum temperature	(Tao, Zhang and Zhang, 2012;		17.79
				Osborne <i>et al.,</i> 2015)		
$T_m$	°C	30	Maximum temperature	(Tao, Zhang and Zhang, 2012;		23.87
				Osborne <i>et al.,</i> 2015)		
TT <sub>emr</sub>	°C d	100	Thermal time between sowing and	(Lu et al., 2018; Luo et al.,		220.6
			emergence	2020)		
TT <sub>veg</sub>	°C d	940	Thermal time between emergence	Xiaoji experimental dataset	400-940	940
-			and anthesis			
TT	0C 4	204	Thermal time between anthesis and	(Wang at al. 2012a): Viacij	200 650	204
1 rep	°C u	504	meturity	experimental dataset	300-030	504
DIV		1 5	Vernalisation coefficient	(Tao, Zhang and Zhang, 2012)	201	20
r i v		1.5	Verhalisation coefficient	(1a0, 2hang and 2hang, 2012, Wang et al. 2013)	2.5-4	2.9
PID		40	Photoperiod coefficient	(Wang et al. 2013)	40-57	40
		40	riotopenoù coencient	2016: 7bao et al 2020)	40-37	40
VT	<u>ەر</u>	30	Maximum daily temperature for	Zheng et al. 2015		
• • max	C	50	vernalisation			
VTmin	°C	15	Minimum daily temperature for	Zheng et al. 2015		
· - min			vernalisation			
ASW	m <sup>3</sup> /m <sup>3</sup>	50	Plant available soil water below			
110 W max	,		which stomatal conductance will			
			start to reduce			
ASWmin	m <sup>3</sup> /m <sup>3</sup>	0	Plant available soil water at which			
mun			stomatal conductance will equal			
			fmin			
V <sub>cmax</sub>	µmol CO <sub>2</sub> m <sup>-2</sup> s <sup>-1</sup>	90	Maximum carboxylation capacity at	(Büker <i>et al.,</i> 2012)	90-140	137
			25°C			
J <sub>max</sub>	µmol CO <sub>2</sub> m <sup>-2</sup> s <sup>-1</sup>	180	Maximum rate of electron transport	(Büker <i>et al.,</i> 2012)	180-250	228
			at 25°C			
K <sub>c</sub>	µmol/mol	404.9	Rubisco Michaelis-Menten constants	(Medlyn <i>et al.,</i> 2002)		
			for CO <sub>2</sub>			

K <sub>0</sub>		278.4	Rubisco Michaelis-Menten constants	(Medlyn <i>et al.,</i> 2002)		
0	mmol/mol		for O <sub>2</sub>			
$\Gamma^*$	µmol/mol	42.75	CO <sub>2</sub> compensation point in the	(Medlyn <i>et al.,</i> 2002)		
			absence of respiration			
а	-	4	Electron requirement for the	(Sharkey <i>et al.,</i> 2007)		
			formation of NADPH			
b	-	8	Electron requirement for the	(Sharkey <i>et al.,</i> 2007)		
_			formation of ATP			
R <sub>dcoeff</sub>	-	0.015	Leaf dark respiration coefficient	(Clark <i>et al.,</i> 2011)	0.01-0.03	
f <sub>min</sub>	µmol CO <sub>2</sub> /m <sup>2</sup> /s	1000	Minimum daytime stomatal	(Ewert and Porter, 2000)		
			conductance to CO <sub>2</sub>			
m	-	7	composite sensitivity slope constant	(Büker <i>et al.,</i> 2012)	4-15	5
VPD <sub>0</sub>	kPa	2.2	stomatal conductance sensitivity to VPD	UNECE, 2017; Pande et al. sub		
γ1	-	0.027	O <sub>3</sub> short-term damage co-efficient	(Ewert and Porter, 2000)		
γ2	(nmol O <sub>3</sub> m <sup>-2</sup> s <sup>-1</sup> ) <sup>-1</sup>	0.0045	O <sub>3</sub> short-term damage co-efficient	(Ewert and Porter, 2000)		
γ3	(µmol O <sub>3</sub> m <sup>-2</sup> ) <sup>-1</sup>	0.00005	O <sub>3</sub> long-term damage co-efficient	(Ewert and Porter, 2000)	0.00001-0.00009	0.00002
γ4	-		O <sub>3</sub> long-term damage co-efficient		1-6	5
			determining onset of senescence			
γ5	-		O <sub>3</sub> long-term damage co-efficient		0.2-0.5	0.4
			determining maturity			
CLsO3	mmol O <sub>3</sub> m <sup>-2</sup>	12.9,22.5	Critical accumulated stomatal O3	(Osborne <i>et al.,</i> 2019; Feng <i>et</i>	12.9-22.5	13.5
			flux that determines the onset of	al., 2022)		
			leaf senescence			
r <sub>ext</sub>	m/s	2500	External leaf cuticular resistance to	UNECE, 2017		
			O <sub>3</sub> uptake			
L	m	0.02	Cross wind leaf dimension for wheat	UNECE, 2017		
$P_{st}$	Pa	1.013 x 10 <sup>5</sup>	Standard air pressure at 20°C	UNECE, 2017		
T <sub>st</sub>	°C	20	Standard temperature	UNECE, 2017		
R	J/mol/K	8.31447	Universal gas constant	UNECE, 2017		
$n_e$	mol CO <sub>2</sub> m <sup>-2</sup> s <sup>-1</sup> kg C	0.0008	Constant relating leaf nitrogen to	(Clark <i>et al.,</i> 2011)		
	(kg N) <sup>-1</sup>	0.070	rubisco carboxylation capacity			
	kg N[kg C] <sup>-1</sup>	0.073	Top canopy leaf N concentration	(Clark <i>et al.</i> , 2011)		
<u>KN</u>		0.78	Nitrogen profile co-efficient	(Clark <i>et al.</i> , 2011)		
R <sub>gcoeff</sub>	-	0.25	Plant growth respiration coefficient	(Osborne <i>et al.</i> , 2015)	0.15-0.25	0.16
$\alpha_{root}$	-	18.5	Coefficient for determining	(Usborne <i>et al.,</i> 2015)	16-19	18.4
			partitioning			
$\alpha_{stem}$	-	16.0	Coefficient for determining	(Usborne <i>et al.,</i> 2015)	16-17	16.8
			partitioning			

α <sub>leaf</sub>	-	18.0	Coefficient for determining	(Osborne <i>et al.,</i> 2015)	18-19	18.4
$\beta_{root}$		-20.0	Coefficient for determining partitioning	(Osborne <i>et al.,</i> 2015)	20-21	-20.9
$\beta_{stem}$	-	-15.0	Coefficient for determining partitioning	(Osborne <i>et al.,</i> 2015)	14-16	-14.5
$\beta_{leaf}$	-	-18.5	Coefficient for determining partitioning	(Osborne <i>et al.,</i> 2015)	18-19	-18.11
$f_c$	-	0.5	Carbon fraction of dry matter	(Osborne <i>et al.</i> , 2015)		
Ŷ	m <sup>-2</sup> kg <sup>-1</sup>	27.3	Coefficient for determining specific leaf area	(Osborne <i>et al.,</i> 2015)	14-28	15
δ	-	-0.0507	Coefficient for determining specific leaf area	(Osborne <i>et al.,</i> 2015)		
k	-	1.4	allometric coefficient which relates $C_{stem}$ to $h$	(Osborne <i>et al.,</i> 2015)		
τ	-	0.4	allometric coefficient which relates $C_{stem}$ to $h$	(Osborne <i>et al.,</i> 2015)	0.3-0.6	0.5
D <sub>w</sub>	-	1/0.84	Conversion factor to allow for grain moisture content	(Mulvaney and Devkota, 2020)		
Eg	-	0.85	Conversion factor for grain to ear ratio	(Nagarajan <i>et al.,</i> 1999; Kutman, Yildiz and Cakmak, 2011)	0.7-0.85	0.85

# Table S5. DO<sub>3</sub>SE-crop phenology parameters description and relation to the thermal time

Paramter	Description	% of thermal time, from start of growing season
f <sub>tl,em</sub> <sup>a</sup>	Crop emergence (DVI=0 <sup>b</sup> ), end of TT <sub>emr</sub> <sup>b</sup>	5
f <sub>tl,ma</sub> a	Start of anthesis to maturity <sup>a</sup> , f <sub>tl,ep</sub> <sup>a</sup> + f <sub>tl,se</sub> <sup>a</sup>	50
f <sub>tl,ep</sub> <sup>a</sup>	Start of anthesis <sup>a</sup> (DVI=1 <sup>b</sup> ) to flag leaf senescence <sup>a</sup> , flag leaf	34
	fully developed <sup>a</sup> , start of TTrep <sup>b</sup>	
f <sub>tl,se</sub> a	Start of flag leaf senescence to harvest(DVI=2 <sup>b</sup> )	16
Mid-anthesis, start of fphen_3_ETS, start of fphen_4_ETS	Half way through flowering	8

<sup>a</sup>(Ewert and Porter, 2000), <sup>b</sup>(Osborne *et al.*, 2015), <sup>c</sup>Mapping manual,2007

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