

# The effect of groundwater depth on topsoil organic matter mineralization during a simulated dry summer in North-West Europe

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**Abstract.** With climate change expected to intensify the occurrence and severity of droughts, the control of groundwater table (GWT) depth and capillary rise on topsoil moisture may render a critical driver of biological activity. Consequently, GWT depth could influence topsoil carbon (C) mineralization. In this study, undisturbed 200 cm long soil columns of three different textures (loamy sand, sandy loam and silt loam) were subjected to two artificial GWT depths (–165 cm and –115 cm) in the  
15 laboratory. We examined (1) upward moisture flow by capillary action along the soil profile and specifically into the top 20 cm soil, and (2) consequently the effect of GWT on decomposition of an added <sup>13</sup>C-enriched substrate (ryegrass) over a period of ten weeks, with limited wetting events representing a dry summer. A 50 cm difference in GWT depth (–165 cm vs. –115 cm) resulted in different topsoil moisture for the sandy loam (31 % vs. 38 % Water-filled pore space (WFPS)) and silt loam (33 % vs. 43 % WFPS) soils. In the loamy sand soil, GWT-induced moisture differences appeared only up to 85 cm above the  
20 GWT. The expected acceleration of mineralization of the added ryegrass under a shallower GWT was not confirmed. In contrast, CO<sub>2</sub> efflux pulses after some of the wetting events were even higher for the drier –165 cm GWT than for the –115 cm GWT across all three soil textures. Additionally, a model fitted to cumulative ryegrass mineralization showed a lower mineralization rate for the stable C<sub>ryegrass</sub> pool in the silt loam soil with the shallowest GWT, where capillary rise contributed most significantly to topsoil moisture, compared to other combinations of soil texture and GWT depth. These findings suggest  
25 that the upward capillary moisture flow, along with the resulting increase in topsoil moisture and the anticipated enhancement of biological activity and ryegrass mineralization, might have been counteracted by other processes. One possible explanation could be that rewetting may have triggered a stronger mineralization response, commonly known as the Birch effect, in drier topsoils compared to conditions where the soil remained consistently wetter with a shallower GWT level. Based on our findings, including the process of texture-specific capillary supply from the GWT is required to adequately simulate moisture  
30 in the topsoil during droughts as they occurred over the past summers in North-West Europe, depending on GWT and texture

combination. However, the net effect on topsoil C mineralization is complex and warrants further investigation, including the integration of processes related to fluctuating soil moisture following rewetting.

## 1 Introduction

35 When soil desiccates, soil-water potential becomes strongly negative, making eco-physiological conditions for soil micro-organisms less favorable. In particular, intracellular turgor pressure and cellular integrity are no longer guaranteed (Malik and Bouskill, 2022; Wang et al., 2015), while diffusion of substrates and extracellular enzymes becomes impeded (Manzoni et al., 2016). As a result, there is a strong moisture dependency of carbon (C) and nitrogen (N) mineralization in soils. Soil C models therefore simulate moisture through hydrological modules. As precipitation and irrigation are usually the primary suppliers of  
40 topsoil moisture, most models do not account for lateral or upward moisture influxes. However, during prolonged dry periods, drying out of topsoil may lead to establishment of counter-gravity soil suction gradients inducing significant upward redistribution of water from the groundwater table (GWT) to the vadose zone through capillary action, and as such, control topsoil moisture. With progressing climate change throughout Europe, weather patterns are becoming more erratic, with already increased occurrence of unusually lengthy dry periods and even agricultural drought in the Maritime climatic region  
45 over the past years (Aalbers et al., 2023; CEU JRC, 2022).

Whether or not moisture supply via upward capillary flow is a relevant process to be accounted for by soil C models, will not only depend on climate, but also on factors such as the depth of the GWT and soil physical properties. But to date, the effect of the GWT depth and capillary moisture supply has nearly exclusively been studied in relation to crop yields (Awan et al., 2014; Feddes et al., 1988; Kroes et al., 2018; Zipper et al., 2015) and irrigation needs (Babajimopoulos et al., 2007; Jorenush and Sepaskhah, 2003; Prathapar et al., 1992; Yang et al., 2011). For example, Zipper et al. (2015) found optimal maize crop  
50 yield at GWT levels of 0.6, 0.8, and 0.9 m depth for sandy loam, loam, and silt loam soils, respectively, and attributed this to optimal water supply resulting from capillary action. When considering bare soils, simulations of the so-called extinction depth for GWT evaporation resulted in depths of 70, 130 and 420 cm for respectively loamy sand, sandy loam and silt loam soils (Shah et al., 2007). This diverse range of modeling outcomes highlights the site-specific nature of capillary rise. To the best of  
55 our knowledge, there exists no robust proof on whether or not, and when, GWT depth might significantly control topsoil heterotrophic activity. Such insights are essential to determine whether incorporating GWT depth and upward capillary moisture flow in updated soil C models is warranted. To validate simulation results, a few studies have been carried out with parallel small-scale field lysimeter experiments monitoring the soil water balance (Kelleners et al., 2005; Prathapar et al., 1992; Yang et al., 2011). Alternatively, Grünberger et al. (2011) injected a deuterium enriched solution to the GWT to follow  
60 capillary rise in arid areas. Both approaches, however, are labor intensive and/or require high investments and technical expertise. Li et al. (2022) instead simply excluded upward capillary moisture transport in a field trial on crop residue decomposition by placing a 5 cm gravel layer at a depth of 50 cm, and found that for sandy soils a GWT depth at just 60 cm

was not shallow enough to notably provide the top 25 cm soil with capillary moisture. However, this approach required disturbance of the topsoil and moreover the artificial break of capillary rise also unintentionally cancelled out unsaturated downward water redistribution. Most importantly perhaps, the main impediment of observational field approaches, such as the ones listed above, is their inability to control ambient factors such as GWT depth, precipitation, temperature and relative humidity. This limitation restricts our ability to study the effect of individual components of the soil water balance like capillary moisture supply.

As an alternative, a handful of laboratory-scale experiments have sought to infer the capillary moisture impact on soil biogeochemical processes. Rezanezhad et al. (2014) and Fiola et al. (2020) found that highest C mineralization was found at transient redox conditions above the capillary fringe, where moisture and oxygen are in balance. However, due to the small scale of the used setups (packed soil columns of 45 cm and 30 cm length, respectively) an appreciation of capillary rise was not possible. Malik et al. (1989), Shaw and Smith (1927) and Lane and Washburn (1947) assembled larger packed soil columns to determine maximum capillary rise height as a function of soil texture. They found capillary moisture supply up to 149 cm (loamy sand soil), 183 cm (sandy loam soil) and 359.2 cm (silt soil), respectively. But as those columns were repacked from sieved soil, soil structure was disrupted and in-field occurring heterogeneity and macropores were not well represented (Lewis and Sjöström, 2010), while neither the impact on C mineralization was assessed. In sum, there is little empirical evidence of the control of moisture dynamics by capillary water flow on topsoil organic matter (OM) mineralization. Not only the impact of GWT onto mean topsoil water content seems a blind spot, but possibly also the amplitude of soil moisture fluctuation in topsoil may depend on the magnitude of moisture supply by capillary action. After a rainfall event, rewetting of dry soil leads to strongly increased C mineralization, often referred to as the Birch effect (Birch, 1958). This effect depends on the magnitude of the soil moisture increment and/or drier pre-wetting condition (Liang et al., 2023). With a stronger continuous supply of moisture via capillary rise we may expect smaller fluctuations in topsoil moisture and then also smaller Birch-effect induced soil C mineralization peaks.

Our main aim was to study if, during a (simulated) period with limited rainfall, there would be a significant effect of capillary moisture flow from the GWT on topsoil moisture and OM mineralization for loess deposited arable lands in North-West Europe. We designed a setup wherein excavated 200 cm long undisturbed soil columns were incubated in the laboratory with ambient factors being regulated and soil moisture monitored. Columns of three soil textures were subjected to minimal watering events representing a dry summer and two GWT depths to study the interaction between both factors and to provide a representative depiction for our study region, i.e. North-West Europe. The decomposition of an introduced substrate, i.e. <sup>13</sup>C-enriched ryegrass, was monitored through CO<sub>2</sub> headspace measurements. We hypothesized that a deeper GWT would result in reduced topsoil moisture and as a result, C mineralization in the topsoil would be relatively inhibited compared to the treatment with shallower GWT. We expected an increasing susceptibility to reduced moisture of the C mineralization with coarser soil texture as water losses by evaporation would be less compensated by capillary moisture input. Although physicochemical protection of OM is stronger in finer-textured soils, we expected that such direct effect of soil texture on

mineralization of the added OM would be of less importance in the short term (10 weeks) as opposed to regulation of soil moisture by the soil texture and GWT depth combinations.

## **2 Material and methods**

### **2.1 Study area and undisturbed soil column collection**

100 Undisturbed soil columns were collected from three croplands in North-West Belgium with different soil texture, that is a loamy sand soil (50°55'43.8"N 3°32'54.7"E, Kruisem), a sandy loam soil (50°57'47.3"N 3°45'37.2"E, Bottelare) and a silt loam soil (50°55'15.8"N 3°45'03.0"E, Oosterzele). According to the WRB soil classification map of Flanders (Dondeyne et al., 2014), the soil profiles originating from Kruisem and Bottelare are classified as Eutric Retisols, while the soil profiles from Oosterzele are Eutric Cambisols (Siltic). The fields were chosen based on their GWT depths between 100 and 200 cm in the  
105 year prior to our experiment. A cylinder auger set and a motorized percussion hammer (Eijkelkamp, The Netherlands) were employed to excavate the soil columns (Ø: 9.7 cm). First, 100 cm long columns were taken from the soil surface down to –100 cm depth. Then, a 100 cm deep pit (2 m<sup>2</sup>) was dug to likewise collect columns from –100 cm to –200 cm depth within the pit. Additionally, disturbed topsoil samples (from 0 cm to –20 cm) were collected near each sampling location. The soil columns were carefully transferred into PVC liners (2 half pipes tied together by strong cable ties) and transported to the  
110 laboratory. The two soil columns taken within one soil profile were then combined in 200 cm long PVC tubes, that were cut lengthwise beforehand to enable the transfer and later sensor installation. On the inner walls of the PVC tubes a waterproof foil was applied to avoid moisture losses. To ensure a hydrological connection between the two 100 cm samples, 5 cm of silt clay loam soil (17 % sand, 48 % silt and 35 % clay) was added in between. Additionally, small breaks were restored by using this soil, but when confronted with larger damage, cores were discarded. Therefore, per field and depth increment, six columns  
115 were deliberately sampled to only retain the four best structurally intact replicates for our experiment. After closing the PVC tubes, cable ties were tightly applied to attain a solid setup and avoid sidewall effects (Lewis and Sjöström, 2010).

### **2.2 Experimental design**

#### **2.2.1 Laboratory setup and incubation**

A soil incubation experiment was set up in which mineralization of a model <sup>13</sup>C-labeled substrate amended to the topsoil was  
120 followed as a function of two constant GWT depths, viz. –165 cm and –115 cm (relative to the soil surface) (Fig. 1). The top 20 cm of the soil columns was removed, such that undisturbed columns of 180 cm length remained. The GWT treatments were consecutively applied to the same columns, resulting in two incubation periods under similar laboratory conditions but with renewed 20 cm topsoil on top of undisturbed columns. The setup was installed in a temperature controlled (20.8 ± 0.7 °C during GWT –165 cm and 20.8 ± 1.5 °C during GWT –115 cm) dark room. The soil columns were submerged in 220 L barrels  
125 with tap water, to a height of 35 cm or 85 cm height, representing the –165 cm or –115 cm GWT depth, respectively. The soil

columns were allowed to stabilize for 27 days. The loamy sand columns were covered by parafilm after 16 days to avoid further drying out. After this stabilization period, the disturbed topsoil samples (0 to –20 cm) collected near each sampling location in the field were mixed with  $^{13}\text{C}$ -enriched ryegrass and repacked to a 20 cm layer on top of the undisturbed soil columns as described in more detail below. For both GWT treatments, the columns followed these identical preparation steps.

130 We deliberately handled the deepest (–165 cm) GWT treatment first. This approach ensured that any potential impact of upward moisture transport on soil structure was confined to a height above the GWT, which was then exceeded during the subsequent, shallower (–115 cm) GWT treatment.

We used a model OM substrate (*in casu*  $^{13}\text{C}$ -labeled clipped ryegrass) and focused solely on the mineralization of this added substrate in the topsoil, without including data on native soil OM mineralization. This approach was chosen primarily because

135 the inherently different quality and quantity between the three soils would no longer allow studying the effect of GWT depth, soil texture and their interaction on soil OM mineralization. Additionally,  $\text{CO}_2$  effluxes from native soil OM included contributions from mineralization in the undisturbed subsoil column (from –20 to –200 cm), which was left unchanged between GWT treatment batches to reduce potential soil heterogeneity influences on moisture dynamics. As native soil OM in this subsoil had thus already undergone partial mineralization during the first GWT treatment, starting conditions would

140 differ for the second GWT treatment. Particularly so as subsoil was moreover kept uniform at 20 °C, which deviates strongly from expected field conditions, where temperature is lower and typically decreases with depth. This discrepancy further limits the applicability of our setup for assessing subsoil OM mineralization.

The extra disturbed top 20 cm soil was first dried and sieved at 4 mm and visible root fragments were manually removed. Subsequently, the three soils were pre-incubated for one week at 20.8°C at a water content of 0.15, 0.22 and 0.28  $\text{m}^3 \text{m}^{-3}$  for

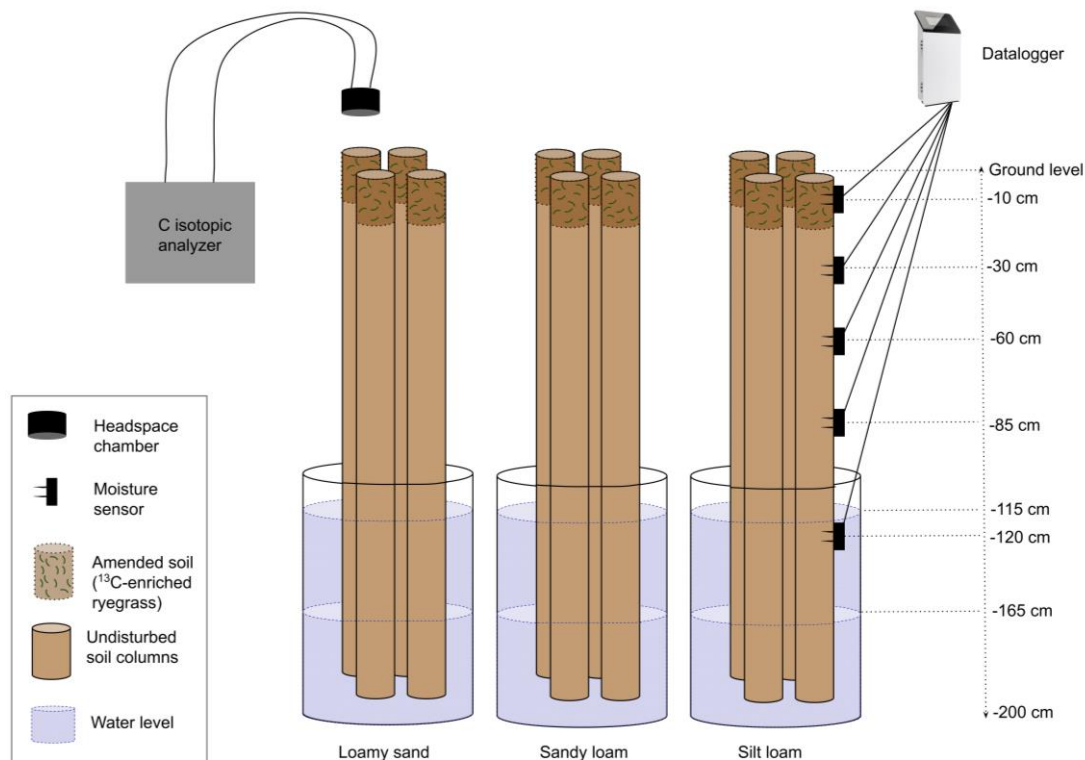
145 the loamy sand, sandy loam and silt loam columns, respectively. The model substrate, i.e.  $^{13}\text{C}$ -labeled ryegrass ( $\delta^{13}\text{C} = +44.93 \pm 1.65 \text{‰}$ ), was added at a dose of 1.5  $\text{g C kg}^{-1}$  dry soil ( $C_{\text{ryegrass}} = 38.74 \pm 0.99 \%$ , C:N = 12.8) and mixed thoroughly. The production of this  $^{13}\text{C}$ -enriched ryegrass is described by Li et al. (2023). To exclude differences in N availability between the various soil texture and GWT depth treatment combinations,  $\text{KNO}_3$  (dissolved in water) was added at a dose equivalent to 100  $\text{kg N ha}^{-1}$ . Each of these soil-grass mixtures for the three soil textures was then gently packed on top of the columns to bulk

150 densities of 1.50, 1.45 and 1.40  $\text{g cm}^{-3}$  for the loamy sand, sandy loam and silt loam columns, respectively. Volumetric water sensors (type EC-5, 5TM, Teros10, Teros12, from Decagon and METER group, USA) were installed at different depths (–10, –30, –60, –85 and –120 cm) by puncturing the sensor rods through the waterproof foil. Prior to use, all sensors were calibrated for the three specific soil textures. Dataloggers, type ZL6 (METER group, USA), were used with a log frequency of one hour. Rainfall was simulated by gently adding 85 or 128 mL over a 30-minute period every 14 to 21 days, equivalent to a dose of

155 25  $\text{mm month}^{-1}$ . With this watering scheme, we simulated a drier than usual (78  $\text{mm month}^{-1}$ ; 30-year Belgian average between the 21<sup>st</sup> of June to 20<sup>th</sup> of September over 1991-2020) local Maritime climate summer, without exceeding the actual measured lowest extreme of 5.2  $\text{mm month}^{-1}$  only observed in July 2022 (Royal Meteorological Institute, 2022). Moisture measurements at –10 cm depth were considered representative for the entire repacked topsoil layer (0 to –20 cm), and therefore suitable for assessing  $^{13}\text{C}$ -labeled ryegrass mineralization within this layer. Simulations in HYDRUS-1D confirmed that moisture had

160 infiltrated to a depth of approximately 20–30 cm, and that within 24–36 hours after water addition, the water content had become nearly uniform throughout the 0–20 cm layer (Fig. A1). Since soil CO<sub>2</sub> efflux measurements (see 2.2.2) were taken then to the earliest after watering events, the –10 cm measurements provided a representative state of the topsoil moisture state. Water levels in the barrels were kept constant daily with the help of a float and a time-of-flight sensor (Adafruit, VL53L0X) combined with a Raspberry Pi (small single-board computer). A plastic grid with a mesh size of 5 mm placed between the  
165 undisturbed soil column and the repacked topsoil allowed its removal after completion of the first incubation batch while preserving the structure and hydraulic contact with the underneath undisturbed columns. Similarly, for the second GWT treatment, fresh topsoil mixed with ryegrass was once again added. At the end of each GWT treatment incubation batch, the packed topsoil was removed and its gravimetric water content was determined. Both initial and final gravimetric water contents were converted into volumetric water content ( $\theta_v$ ) using the applied bulk densities and compared with the sensor values (Table  
170 A1). Deviating measurements were found for three sandy loam columns during the –115 cm GWT treatment, presumably due to air entrapment around the sensor rods after installation. To rectify this discrepancy, a correction was applied using linear regression (Fig. A2).

175



180 **Figure 1: Schematic overview of the laboratory setup.**

### 2.2.2 Soil CO<sub>2</sub> efflux measurements and calculations

Soil CO<sub>2</sub> efflux was regularly measured to record soil C mineralization and infer the progress of the cumulative amount of C<sub>ryegrass</sub> mineralized over time. For CO<sub>2</sub> efflux measurements, a G2201-i Cavity Ring-Down Spectrometer (CRDS) (Picarro, USA) was consecutively connected via tubing to an air tight lid attached on top of the soil columns. The lid contained two sampling ports (gas in- and outlet), a vent tube (Ø: 1 mm) to minimize air pressure differences and a 9V battery-powered fan on the inside to ensure air circulation inside the headspace between soil surface, PVC tube and lid. The headspace volume varied between 0.52 and 0.82 L and covered an area of 73.90 cm<sup>2</sup>. The CRDS recorded changes in the headspace CO<sub>2</sub> concentration and δ<sup>13</sup>C value every 2–3 seconds. CO<sub>2</sub> efflux rates were calculated as the slope of the linearly increasing CO<sub>2</sub> concentration over a 7 to 15 minutes time interval per soil column and were converted to a mass-based unit (mg CO<sub>2</sub>-C kg soil<sup>-1</sup> h<sup>-1</sup>) using the ideal gas law. To determine the δ<sup>13</sup>C (‰) value of emitted CO<sub>2</sub> (δ<sup>13</sup>C·CO<sub>2</sub>, Eq. (1)), the Keeling plot method was applied in which measured δ<sup>13</sup>C values are plotted against the inverse CO<sub>2</sub> emission concentrations and the δ<sup>13</sup>C of emitted CO<sub>2</sub> is obtained from the y-axis intercept of a linear model fitted to the data (Keeling, 1958). Measurements were

made on days 1, 2, 3, 5, 7, 9, 11, 13, 15, 20, 22, 24, 27, 29, 34, 36, 38, 42, 45, 48, 52, 57, 59, 62, 66 and 69 of each of both  
 195 incubation batches. The CRDS was recalibrated at onset of each incubation using two certified standard gases of 400 ppm and  
 2500 ppm CO<sub>2</sub> with δ<sup>13</sup>C values of respectively -8.6 ‰ and -51 ‰. The contrasting δ<sup>13</sup>C values of the added <sup>13</sup>C-labeled  
 ryegrass (+ 44.93 ± 1.65 ‰) and soil organic carbon (- 25.68 ± 0.23 ‰ for loamy sand, - 25.57 ± 0.17 ‰ for sandy loam, and  
 - 24.79 ± 0.11 ‰ for silt loam soils, Table 1) allowed to partition the total CO<sub>2</sub> efflux (CO<sub>2</sub>·C<sub>total</sub>) into a share resulting from  
 ryegrass decomposition (CO<sub>2</sub>·C<sub>ryegrass</sub>) and from native SOC (CO<sub>2</sub>·C<sub>SOC</sub>) (µg CO<sub>2</sub>-C kg<sup>-1</sup> soil) with an isotope mixing model  
 200 following Eq. (1):

$$CO_2 \cdot C_{ryegrass} = \frac{\delta^{13}C \cdot CO_2 - \delta^{13}C \cdot CO_2 \cdot SOC}{\delta^{13}C \cdot CO_2 \cdot ryegrass - \delta^{13}C \cdot CO_2 \cdot SOC} * CO_2 \cdot C_{total} \quad (1)$$

The isotopic signature of CO<sub>2</sub> emitted from either end member, i.e. δ<sup>13</sup>C·CO<sub>2</sub>·ryegrass and δ<sup>13</sup>C·CO<sub>2</sub>·SOC, were analyzed in  
 ancillary soil incubations as in Mendoza et al. (2022). The δ<sup>13</sup>C·CO<sub>2</sub>·SOC was determined in parallel 20 cm packed soil columns  
 205 with no ryegrass added. For δ<sup>13</sup>C·CO<sub>2</sub>·ryegrass, such soil columns were amended with a high dose of ryegrass (3 g C kg<sup>-1</sup> soil;  
 indicated as “high”). The rationale for using smaller columns compared to the main experimental setup was to exclude CO<sub>2</sub>  
 emissions from the underlying soil OC, ensuring a more accurate assessment of δ<sup>13</sup>C·CO<sub>2</sub>·ryegrass. The following Eq. (2) was  
 applied:

$$210 \quad \delta^{13}C \cdot CO_2 \cdot ryegrass = \frac{CO_2 \cdot C_{high} * \delta^{13}C \cdot CO_2 \cdot high - CO_2 \cdot SOC \cdot C_{SOC} * \delta^{13}C \cdot CO_2 \cdot SOC}{CO_2 \cdot C_{high} - CO_2 \cdot C_{SOC}} \quad (2)$$

Emission measurements in these ancillary incubations were made on days 2, 7, 15, 29, and 52.

From ryegrass-derived CO<sub>2</sub> efflux (CO<sub>2</sub>·C<sub>ryegrass</sub> h<sup>-1</sup>) cumulative amounts of mineralized C<sub>ryegrass</sub> (in µg C kg<sup>-1</sup> soil) were  
 calculated by integrating these mineralization rates over time intervals defined as half of the period before the previous  
 215 measurement and half of the period until the next measurement. To describe the kinetics of mineralized ryegrass over time,  
 relative to the added amount of ryegrass in % C<sub>ryegrass</sub>, the following parallel two rate first-order kinetic model was used (Sleutel  
 et al., 2005; Zacháry et al., 2018), Eq. (3):

$$Cumulative C_{ryegrass-min}(t) = C_f * (1 - e^{-k_f * t}) + k_s * t \quad (3)$$

220

where C<sub>f</sub> (% of C<sub>ryegrass</sub>) and k<sub>f</sub> (day<sup>-1</sup>) are parameters representing the easily mineralizable C<sub>ryegrass</sub> pool and the mineralization  
 rate, respectively, while k<sub>s</sub> (% of C<sub>ryegrass</sub> day<sup>-1</sup>) is the mineralization rate constant of a more stable C<sub>ryegrass</sub> pool.



### 2.3 Column analyses: physicochemical soil properties

225 At the end of the experiment, the 200 cm tubes were opened carefully by relieving cable ties, taking off one of both PVC half-pipes and opening the waterproof foil. Then, undisturbed soil samples ( $\emptyset$ : 5 cm, h: 5.1 cm) were taken by pressing Kopecky rings in the soil columns near the moisture sensor locations, i.e. at -15 to -10 cm; -35 to -30 cm; -55 to -50 cm; -85 to -80 cm and -125 to -120 cm depth. For each depth layer a soil-water retention curve was determined by measuring water contents of these ring samples on a silica sand tension table and pressure plates (Eijkelkamp, The Netherlands) at different matric  
230 tensions (-1, -3, -7, -10 and -33, -100, -1500 kPa, respectively). Average water retention curves per texture and depth (Fig. B1) were further used to convert measured mean volumetric water contents in matric potentials, expressed as matric head in units of cm water height (cm WH). The latter were used to calculate hydraulic head differences ( $\Delta H$ ) between two measurement heights, where height was defined to increase in the upward direction, and with hydraulic head the sum of matric head and gravitational head. They were used as an indicator for the water flux direction: positive  $\Delta H$  values indicate a net upward  
235 (capillary) water flux, while negative  $\Delta H$  values signify an overall downward water flux. Soil texture, OC content and  $\text{pH}_{\text{H}_2\text{O}}$  were determined on homogenized subsamples from -20 to -50 cm, -50 to -100 cm, -100 to -150 and -150 to -200 cm layers. Values for  $\delta^{13}\text{C}$  were only determined for the repacked topsoil. Physicochemical properties of the soil columns are listed in Table 1.

### 2.4 Statistical analyses

240 Statistical analyses were made with R Studio statistical software, version 4.1.2 (R Core Team, 2021). Reported values represent means  $\pm$  standard errors. Linear mixed-effect models (R package “nlme”, function “lme”) (Pinheiro and Bates, 2000) in combination with estimated marginal means (R package “emmeans”, function “emmeans”) (Lenth et al., 2024) were used to detect statistical differences in average water content and  $C_{\text{ryegrass}}$  mineralization rates between GWT treatments per texture over the entire incubation period. In this model, the GWT treatment was set as fixed factor, while column replicates ( $n = 4$ )  
245 were added as random intercept to represent the grouped structure of the experimental setup and an autocorrelation factor was included to account for temporal autocorrelation between measurements as well (Schielzeth and Nakagawa, 2013). Diagnostic plots for the linear mixed-effects fit were visually examined (R package “nlme”, function “plot.lme”). Additionally, paired two-tailed t-tests were used to compare  $C_{\text{ryegrass}}$  mineralization rates between GWT treatments per measurement day (after checking assumptions of normality and homoscedasticity). Goodness-of-fit of the parallel two rate first-order kinetic model  
250 was assessed through the Nash–Sutcliffe model efficiency coefficient (NSE) (R package “ie2misc”, function “vnse”) (Embry et al., 2023). To detect any effect of GWT treatment and texture on the kinetic parameters of the two rate first-order C mineralization model ( $C_f$ ,  $k_f$  and  $k_s$ ) and cumulative  $C_{\text{ryegrass-min}}$  at the end of the incubation, once more linear mixed-effect models (R package “lme4”, function “lmer”) (Bates et al., 2015) were applied in combination with estimated marginal means (R package “emmeans”, function “emmeans”). This time, both GWT and texture were set as fixed factors, while the separate

255 columns ( $n = 12$ ) were set as a random effect to allow for a pairwise comparison. The normality assumption for the residuals was tested using a simulation based approach (R package “DHARMA”) (Hartig, 2020).

**Table 1: Physicochemical properties of the undisturbed soil columns (n = 4).**

Location cropland	Depth below the surface from; to (cm)	Soil texture <sup>b</sup>			USDA soil texture class	OC <sup>c</sup> (g kg <sup>-1</sup> )	$\delta^{13}\text{C}$ <sup>d</sup> (‰)	pH <sub>H2O</sub> <sup>e</sup> (-)	Sensor depth (cm)	BD <sup>f</sup> (g cm <sup>-3</sup> )
		Sand (%)	Silt (%)	Clay (%)						
Kruisem	0 ; -20 <sup>a</sup>					11.2 ± 0.3	-25.68 ± 0.23		-10	1.50
	-20 ; -50	86.2 ± 0.3	10.4 ± 0.6	3.3 ± 0.3	Loamy sand	5.0 ± 1.0		7.3 ± 0.0	-30	1.54 ± 0.02
	-50 ; -100	89.5 ± 1.6	8.4 ± 1.4	2.1 ± 0.2	Sand	0.6 ± 0.2		7.3 ± 0.0	-60	1.58 ± 0.01
	-100 ; -150	85.3 ± 3.2	8.1 ± 2.6	6.6 ± 1.4	Loamy sand	0.2 ± 0.1		7.6 ± 0.0	-85	1.52 ± 0.01
	-150 ; -200	76.6 ± 5.7	14.1 ± 5.4	9.3 ± 0.7	Sandy loam	0.5 ± 0.1		7.7 ± 0.1	-120	1.66 ± 0.01
Bottelare	0 ; -20 <sup>a</sup>					10.0 ± 0.4	-25.57 ± 0.17		-10	1.45
	-20 ; -50	60.6 ± 0.8	33.1 ± 0.9	6.3 ± 0.3	Sandy loam	3.6 ± 0.6		7.4 ± 0.0	-30	1.55 ± 0.01
	-50 ; -100	62.8 ± 3.8	26.6 ± 3.6	10.6 ± 1.8	Sandy loam	0.7 ± 0.1		7.6 ± 0.0	-60	1.75 ± 0.02
	-100 ; -150	47.7 ± 1.0	36.7 ± 1.3	15.6 ± 0.4	Loam	0.5 ± 0.1		7.5 ± 0.0	-85	1.65 ± 0.02
	-150 ; -200	66.5 ± 4.6	23.0 ± 3.7	10.5 ± 0.9	Sandy loam	0.2 ± 0.1		7.3 ± 0.0	-120	1.65 ± 0.01
Oosterzele	0 ; -20 <sup>a</sup>					9.8 ± 0.2	-24.79 ± 0.11		-10	1.40
	-20 ; -50	12.2 ± 1.2	68.8 ± 0.5	18.9 ± 0.8	Silt loam	4.3 ± 0.6		7.1 ± 0.1	-30	1.61 ± 0.02
	-50 ; -100	15.6 ± 3.8	66.8 ± 2.9	17.6 ± 0.9	Silt loam	1.4 ± 0.2		7.3 ± 0.2	-60	1.60 ± 0.02
	-100 ; -150	22.5 ± 4.3	60.7 ± 3.3	16.8 ± 1.1	Silt loam	0.9 ± 0.2		7.6 ± 0.2	-85	1.54 ± 0.01
	-150 ; -200	16.6 ± 2.1	66.2 ± 1.8	17.1 ± 0.4	Silt loam	1.8 ± 0.3		7.7 ± 0.0	-120	1.67 ± 0.01

<sup>a</sup> Repacked soil layer.

260 <sup>b</sup> Measured with the pipette-sedimentation method, with fractions: Sand (0.05 mm – 2 mm); Silt (0.002 mm – 0.05 mm) and Clay (< 0.002 mm).

<sup>c</sup> Organic Carbon (OC); Measured by a FORMACS<sup>TM</sup> HT-i TOC/TN analyser (Skalar, The Netherlands).

<sup>d</sup> Measured with a PDZ Europa ANCA-GSL elemental analyser interfaced with a Sercon 20-22 IRMS with SysCon electronics (SerCon, UK) and EA-IRMS EA IsoLink interfaced through a ConFloIV to a delta Q (Thermo Scientific, Germany). All  $\delta^{13}\text{C}$  values are  $^{13}\text{C}/^{12}\text{C}$  ratios expressed relative to the international VPDB (Vienna Pee Dee Belemnite) standard.

265 <sup>e</sup> pH in 1:5 soil:water (volume fraction) suspensions, measured using a glass electrode.

<sup>f</sup> Bulk Density (BD).

### 3 Results

#### 3.1 Soil moisture dynamics in response to GWT treatment

##### 270 3.1.1 Volumetric water content ( $\theta_v$ ) along soil profiles of undisturbed columns

Overall, there was a gradual decrease in  $\theta_v$  with increasing height above the GWT for all GWT and soil texture treatments (Fig. 2). The applied water appeared to primarily affect  $\theta_v$  in the upper 10 cm and not in deeper soil layers.

In the loamy sand columns, moisture levels at  $-85$  cm and  $-60$  cm depth were on average  $0.07$  and  $0.04 \text{ m}^3 \text{ m}^{-3}$  lower ( $P = 0.016$  and  $P = 0.007$ , respectively) for GWT  $-165$  cm than for GWT  $-115$  cm (Table 2). At  $-30$  cm, a less significant  
275 ( $P = 0.067$ ) difference of  $0.03 \text{ m}^3 \text{ m}^{-3}$  was observed, while at  $-10$  cm, GWT treatment did not significantly impact  $\theta_v$  ( $P = 0.294$ ). The  $\theta_v$  at an equivalent height of about  $80$  cm above both GWTs was lower in case of the  $-115$  cm GWT treatment at  $-30$  cm compared to at  $-85$  cm for the  $-165$  cm GWT treatment, which was probably the result of evaporative losses. Conversely, for the GWT  $-165$  cm treatment,  $\theta_v$  was comparable at  $-30$  cm and  $-10$  cm, and this might indicate limited impact of evaporative losses on topsoil moisture.

280 In the sandy loam columns,  $\theta_v$  generally decreased with increasing height above the GWT, aside from lower  $\theta_v$  at  $55$  cm above the  $-115$  cm GWT ( $0.237 \text{ m}^3 \text{ m}^{-3}$ ) compared to that at  $80$  cm above the  $-165$  cm GWT ( $0.282 \text{ m}^3 \text{ m}^{-3}$ ). This inconsistency might be explained by the elevated bulk density at  $-60$  cm ( $1.75 \pm 0.02 \text{ g cm}^{-3}$ ) compared to that at  $-85$  cm ( $1.65 \pm 0.02 \text{ g cm}^{-3}$ ) (Table 1). The  $\theta_v$  differed significantly between both GWT treatments with an effect of  $0.02 \text{ m}^3 \text{ m}^{-3}$  ( $P = 0.012$ ) at  $-85$  cm,  $0.02 \text{ m}^3 \text{ m}^{-3}$  at  $-60$  cm ( $P = 0.028$ ) and  $0.03 \text{ m}^3 \text{ m}^{-3}$  at  $-10$  cm ( $P = 0.026$ ), but surprisingly not at  $-30$  cm ( $0.01 \text{ m}^3 \text{ m}^{-3}$ ,  $P = 0.31$ )  
285 (Table 2).

In the silt loam columns,  $\theta_v$  was comparable (about  $0.310 \text{ m}^3 \text{ m}^{-3}$ ) at depths below  $30$  cm from the surface (Table 2). The surprisingly lower  $\theta_v$  at  $-120$  cm ( $0.270 \text{ m}^3 \text{ m}^{-3}$ ) for the  $-165$  cm GWT treatment might again be explained by the relatively higher BD ( $1.67 \pm 0.01 \text{ g cm}^{-3}$ ) at that depth (Table 1). Between the GWT treatments, there were only marginally significant differences in  $\theta_v$  at  $-85$  cm ( $0.01 \text{ m}^3 \text{ m}^{-3}$ ,  $P = 0.062$ ) and  $-60$  cm ( $0.01 \text{ m}^3 \text{ m}^{-3}$ ,  $P = 0.092$ ), but not at  $-30$  cm ( $P = 0.160$ ). At  $-$   
290  $10$  cm,  $\theta_v$  was lower at GWT  $-165$  cm ( $0.153 \text{ m}^3 \text{ m}^{-3}$ ) than at GWT  $-115$  cm ( $0.200 \text{ m}^3 \text{ m}^{-3}$ ) ( $P = 0.028$ ).

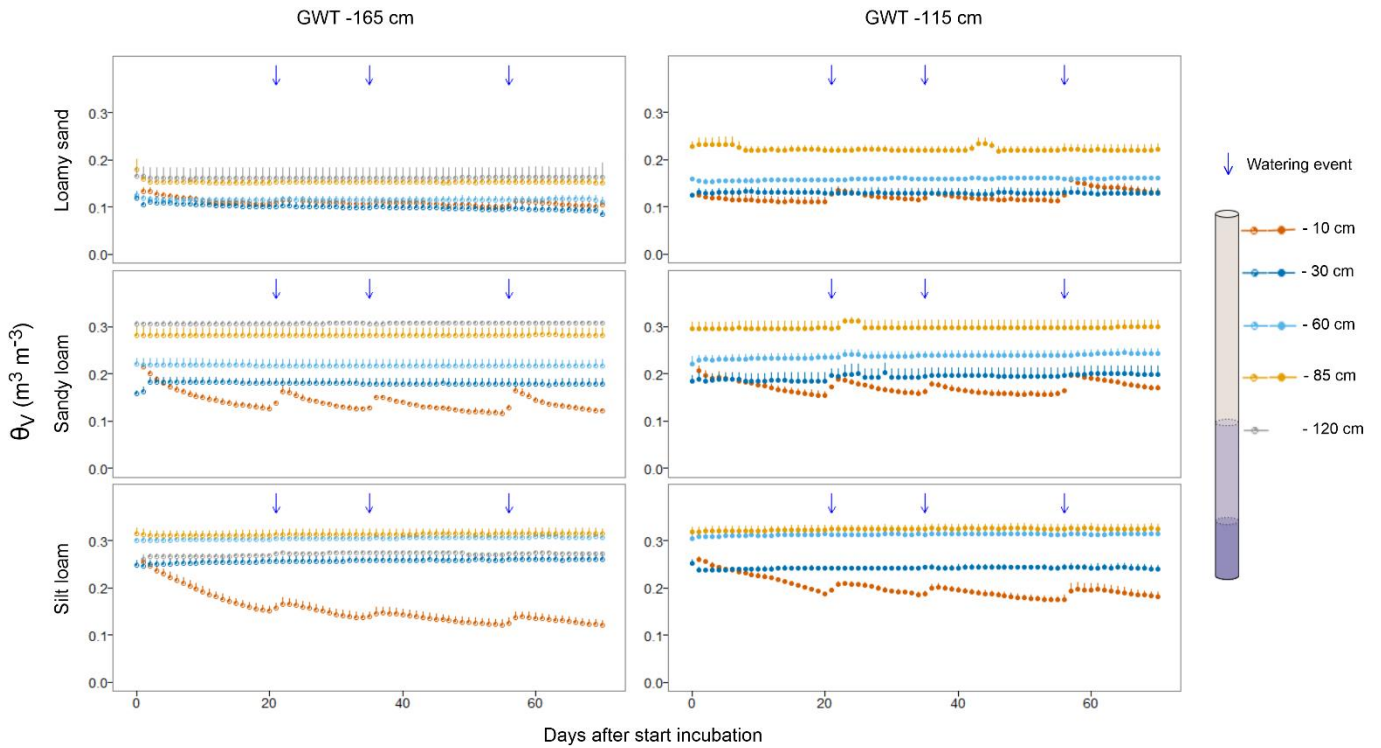


Figure 2: Evolution of soil moisture ( $\theta_v$ ) depth profiles ( $n = 4$ ) over time for two GWT (groundwater table) treatments (depths at  $-165$  and  $-115$  cm) and three textures (loamy sand, sandy loam and silt loam). Note that the GWT treatment  $-115$  cm does not have a sensor installed at  $-120$  cm depth (i.e. below the established GWT).

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**Table 2: Estimated marginal means of water contents ( $\theta_v$ ) measured at different depths as a function of GWT treatment (depths at –165 cm and –115 cm).**

300

	Sensor depth (cm)	Relative position above the GWT (cm)		$\theta_v$ ( $m^3 m^{-3}$ )		
		GWT	GWT	GWT	GWT	
		–165 cm	–115 cm	–165 cm	–115 cm	
305	Loamy sand	–10	155	105	0.109	0.123
		–30	135	85	0.099	0.129 .
		–60	105	55	0.115	0.159 *
		–85	80	30	0.153	0.222 *
		–120	45	/	0.162	/
310	Sandy loam	–10	155	105	0.140	0.172 *
		–30	135	85	0.179	0.193
		–60	105	55	0.217	0.237 *
		–85	80	30	0.282	0.298 *
		–120	45	/	0.307	/
315	Silt loam	–10	155	105	0.153	0.200 *
		–30	135	85	0.257	0.242
		–60	105	55	0.305	0.313 .
		–85	80	30	0.313	0.325 .
		–120	45	/	0.271	/

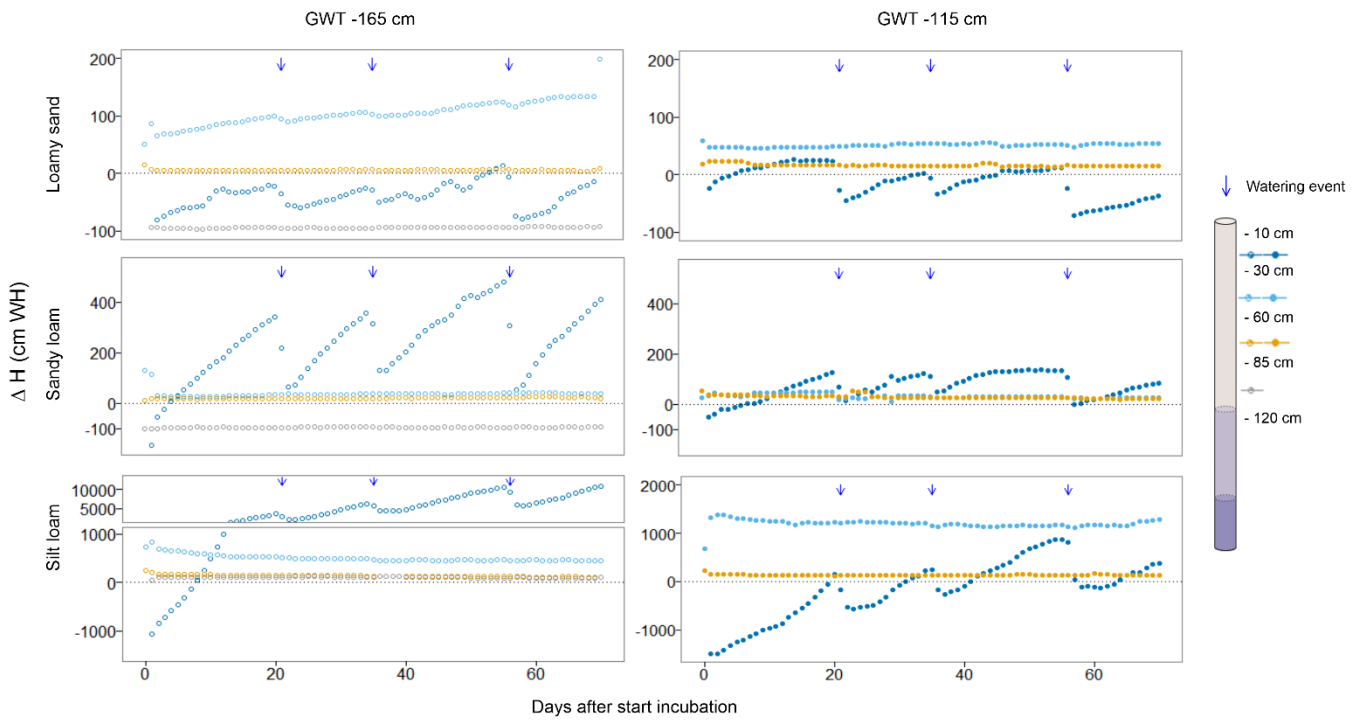
320

Symbols “.” and “\*” indicate that moisture was significantly higher ( $P < 0.1$  and  $P < 0.05$ , respectively) for GWT treatment –115 cm when compared to the deeper –165 cm treatment. Note that GWT treatment –115 cm did not have a sensor installed at –120 cm depth (i.e. under the established GWT).

### 3.1.2 Hydraulic head differences

Across all three textures and both GWT treatments, there was a negative hydraulic head difference ( $\Delta H$ ) between  $-10$  cm and  $-30$  cm during the first few days of the incubation. This indicates gravitational water transport due to wetter repacked topsoil layers at the start of the experiment towards the drier undisturbed soil layers. In the loamy sand columns, the  $\Delta H$  between  $-10$  cm and  $-30$  cm remained mostly negative in case of the  $-165$  cm GWT treatment during the rest of the experiment (Fig. 3). In contrast, between  $-60$  cm and  $-30$  cm,  $\Delta H$  ranged from  $+50$  to  $+198$  cm WH, indicating upward water movement. For the shallower  $-115$  cm GWT, water transport between  $-30$  cm and  $-10$  cm was alternately downward and upward depending on the watering applications (viz.  $\Delta H$  ranging from  $-80$  to  $+30$  cm WH), followed by slight positive and quite constant  $\Delta H$  ( $+50$  cm WH) between  $-60$  cm and  $-30$  cm. For both GWT treatments,  $\Delta H$  between  $-85$  cm and  $-60$  cm remained slightly positive throughout the experiment period. Between  $-120$  cm and  $-85$  cm we found an unforeseen negative  $\Delta H$  of  $\sim -95$  cm WH. In the sandy loam columns, between  $-30$  cm and  $-10$  cm  $\Delta H$  was positive and fluctuated in response to the water applications for both GWT treatments. In the  $-165$  cm GWT treatment, higher  $\Delta H$  maxima were observed as a result of drier topsoil compared to the  $-115$  cm GWT treatment. Both GWT treatments exhibited fairly consistent positive  $\Delta H$  between  $-60$  cm and  $-30$  cm, as well as between  $-85$  cm and  $-60$  cm, with average  $\Delta H$  values of  $\sim +37$  cm WH and  $\sim +20$  cm WH (GWT  $-165$  cm), and  $\sim +32$  cm WH and  $\sim +29$  cm WH (GWT  $-115$  cm), respectively. Surprisingly, like with the loamy sand columns, we measured a negative  $\Delta H$  of about  $-95$  cm WH between  $-120$  cm and  $-85$  cm, for the GWT  $-165$  cm treatment, i.e. close to the GWT.

In the silt loam columns,  $\Delta H$  in the topsoil increased up to  $+10800$  cm WH in case of the  $-165$  cm GWT treatment as a result of topsoil drying out compared to underlying soil. In case of the shallower GWT of  $-115$  cm, the  $\Delta H$  between  $-10$  cm and  $-30$  cm alternated around  $0$  cm WH, with temporary negative values (i.e. downward moisture transport) directly after watering events, then followed by an increase in  $\Delta H$  to positive values after several days (i.e. upward moisture transport). For GWT  $-165$  cm positive  $\Delta H$  values were found in all subsoil layers, which tended to decrease over time from  $+830$  to  $+450$  cm WH,  $+245$  to  $+100$  cm WH,  $+120$  to  $+30$  cm WH and  $+110$  to  $+90$  cm WH between respective depths of  $-60$  cm to  $-30$  cm,  $-85$  cm to  $-60$  cm and  $-120$  cm to  $-85$  cm. For the  $-115$  cm GWT, upward (but rather constant) moisture transport existed as well, with average  $\Delta H$  values of  $+1200$  cm WH and  $+135$  cm WH, for  $-60$  cm to  $-30$  cm and  $-85$  cm to  $-60$  cm, respectively.



350 **Figure 3: Difference in hydraulic head ( $\Delta H$ ) over time for both GWT treatments (-165 cm and -115 cm) measured in loamy sand, sandy loam and silt loam soil columns. A positive (negative)  $\Delta H$  indicates a hydraulic head difference enabling upward (downward) moisture transport. Note that GWT treatment -115 cm did not have a sensor installed at -120 cm depth and therefore no  $\Delta H$  with -85 cm could be shown.**

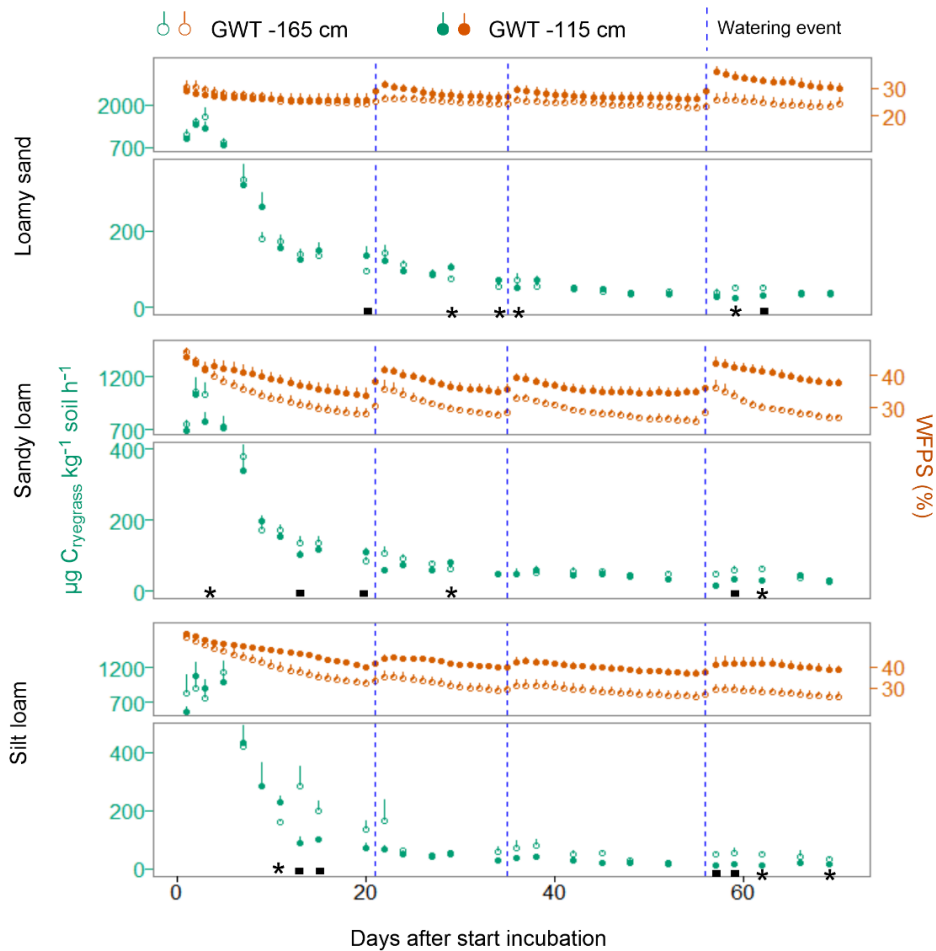


## 3.2 Mineralization of added ryegrass

### 3.2.1 Mineralization rates and moisture in topsoil

355 During the initial five days of the incubation ryegrass mineralization rates were highest with mean maxima of 1643, 1053 and  
1133  $\mu\text{g C}_{\text{ryegrass}} \text{kg}^{-1} \text{soil h}^{-1}$  for loamy sand, sandy loam and silt loam columns, respectively. From day seven onwards, the  
rates decreased gradually over time and after day 30, averaged around 72, 62 and 78  $\mu\text{g C}_{\text{ryegrass}} \text{kg}^{-1} \text{soil h}^{-1}$  for the three  
respective textures (Fig. 4). There was no significant effect of GWT treatment on the mean  $\text{C}_{\text{ryegrass}}$  mineralization rate across  
the entire incubation period per texture, although for some individual measurement days, rates did alternate between the GWT  
360 treatments. After the watering applications, mineralization rates in the drier, -165 cm GWT treatment, soil seemed to be more  
sensitive to the moisture input. Significant differences were observed only in comparison to the -115 cm GWT from the  
second watering application onwards in the loamy sand soil (72 vs 51  $\mu\text{g C}_{\text{ryegrass}} \text{kg}^{-1} \text{soil h}^{-1}$  at day 36), and after the third  
application for the sandy loam (59 vs 32  $\mu\text{g C}_{\text{ryegrass}} \text{kg}^{-1} \text{soil h}^{-1}$  at day 59) and silt loam (51 vs 13  $\mu\text{g C}_{\text{ryegrass}} \text{kg}^{-1} \text{soil h}^{-1}$  at  
day 57) soil.

365

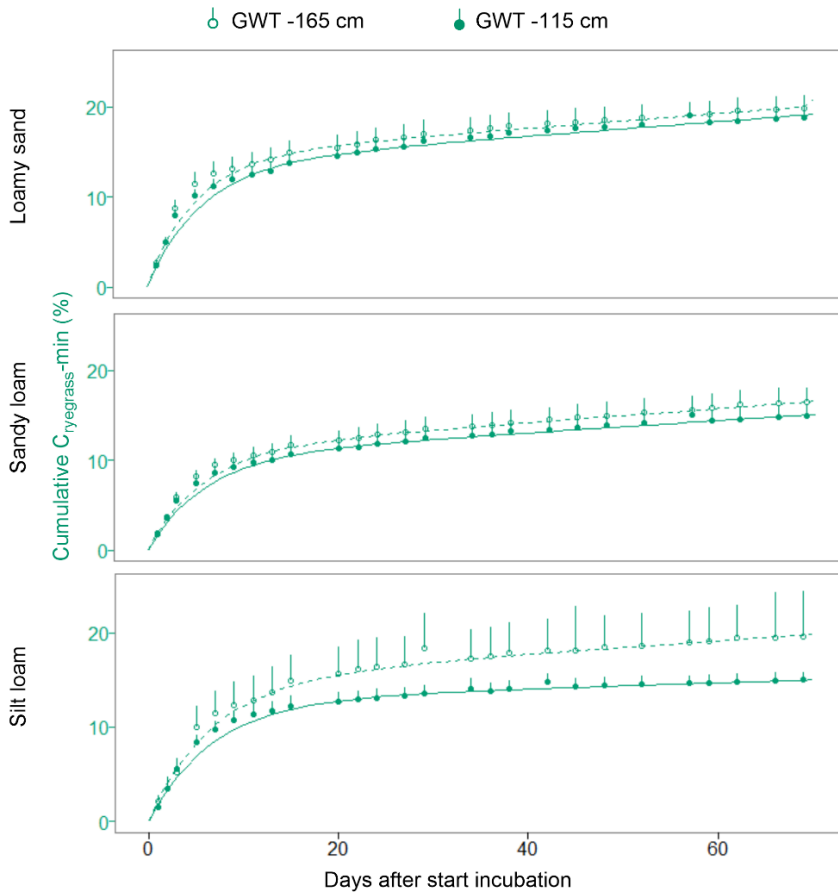


370 **Figure 4: Ryegrass mineralization rates combined with the topsoil moisture expressed in % of Water-Filled Pore Space (WFPS) for both GWT treatments in the loamy sand, sandy loam and silt loam soil columns (n = 4). Symbols “.” and “\*” indicate significant differences for a specific measurement day at P < 0.1 and P < 0.05, respectively.**

### 3.2.2 Cumulative ryegrass mineralization

Overall, 15 – 20 % of the added  $C_{\text{ryegrass}}$  was mineralized over the course of the 70-days incubation period. Cumulative  $C_{\text{ryegrass-min}}$  did not differ between the three soil textures (19.3 %, 15.7 % and 17.4 % for the loamy sand, sandy loam and silt loam, respectively). In contrast, GWT treatment had a marginal significant effect ( $P = 0.051$ ) with lower cumulative  $C_{\text{ryegrass-min}}$  in case of the –115 cm GWT (16.2 %) compared to the –165 cm GWT (18.7 %).

The kinetic parallel two rate first-order mineralization model fitted very closely to the cumulative  $C_{\text{ryegrass-min}}$  with NSE-values  $> 0.98$  (Fig. 5). The estimated size of the easily mineralizable pool ( $C_f$ ) was not different between the texture and GWT depth combinations, with average values between 10.3 % and 15.0 % of the initially added amount of  $C_{\text{ryegrass}}$  (Table 3). The mineralization rate of this fast  $C_{\text{ryegrass}}$  pool ( $k_f$ ) was not different between the GWT treatments, but it was  $0.041 \text{ d}^{-1}$  and  $0.026 \text{ d}^{-1}$  lower for the silt loam compared to the loamy sand ( $P = 0.004$ ) and sandy loam ( $P = 0.049$ ) soils, respectively. After the depletion of the fast  $C_{\text{ryegrass}}$  pool in about 2-3 weeks, the cumulative  $C_{\text{ryegrass-min}}$  further proceeded at a much slower pace following a close to linear course, described by  $k_s$ . This  $k_s$  was significantly lower in case of the –115 cm GWT silt loam soil treatment compared to the other soil texture and GWT depth combinations.



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**Figure 5: Cumulative  $C_{ryegrass-min}$  (%) and fitted parallel two rate first-order kinetic model for both GWT treatments in loamy sand, sandy loam and silt loam soil columns (n = 4).**

390

**Table 3: Parameters of the parallel two rate first-order kinetic model characterizing the cumulative  $C_{ryegrass-min}$  for both GWT treatments in loamy sand, sandy loam and silt loam soil columns.**

	Loamy sand		Sandy loam		Silt loam	
	GWT -165 cm	GWT -115 cm	GWT -165 cm	GWT -115 cm	GWT -165 cm	GWT -115 cm
$C_r$ (%)	14.3 ± 1.5 a	13.5 ± 0.9 a	11.0 ± 1.0 a	10.3 ± 1.0 a	15.0 ± 2.6 a	12.8 ± 1.0 a
$k_r$ (d <sup>-1</sup> )	0.20 ± 0.00 a	0.18 ± 0.01 a	0.18 ± 0.01 a	0.17 ± 0.00 a	0.15 ± 0.02 b	0.15 ± 0.01 b
$k_s$ (% d <sup>-1</sup> )	0.08 ± 0.00 a	0.08 ± 0.01 a	0.08 ± 0.01 a	0.07 ± 0.00 a	0.07 ± 0.02 a	0.03 ± 0.01 b

Letters indicate significant (P < 0.1) differences per parameter between soil texture and GWT depth combinations.

400

## 4 Discussion

With this experiment, we aimed to infer if and how GWT depth (here either at  $-165$  cm and  $-115$  cm) impacts topsoil moisture and C mineralization during simulated dry periods that could realistically occur in North-West Europe. Below we discuss capillary moisture supply as a function of GWT and soil texture combinations (4.1), the impact on OM mineralization (4.2) and consequences for modelling of topsoil carbon on the landscape scale (4.3).

### 4.1 To what extent does groundwater table depth affect moisture during simulated drought?

In the loamy sand columns, with a GWT of  $-165$  cm, moisture of the shallow layers ( $-30$  cm and  $-10$  cm) was consistently low ( $\sim 0.1$  m<sup>3</sup>/m<sup>3</sup>), and thus situated in the “dry” range of the soil water retention curve (Fig. B1). There was clear evidence that capillary moisture supply from deeper soil layers towards the topsoil was insignificant for this deepest GWT treatment. First, although positive hydraulic head differences ( $\Delta H$ ) between  $-60$  cm and  $-30$  cm enabled capillary action, they displayed an increasing trend throughout the experiment (Fig. 3). Hence, the soil was observed to be drying out at  $105$  cm and  $135$  cm above the GWT, indicating clearly that evaporative losses were insufficiently compensated by a capillary water flux. Second, hydraulic head differences between  $-30$  cm and  $-10$  cm depth were even negative, excluding upward moisture transport out of the directly underlying subsoil. In fact, watering events likely caused temporary downward moisture fluxes between these topsoil layers, as indicated by the fluctuating pattern of  $\Delta H$  ( $-30$  cm to  $-10$  cm). Considering the moisture retention curve, it emerges that stronger suction forces than the ones recorded here would also not have readily resulted in marked further soil drying, which explains why moisture at  $-30$  cm remained relatively constant despite temporal changes in  $\Delta H$ . In sum, the absence of a significant upward moisture supply to the loamy sand topsoil at deep GWT is most likely directly attributable to a too limited capillary rise height characteristic of this texture. When the GWT was raised to  $-115$  cm, moisture at  $-30$  cm was higher than at the  $-165$  cm GWT, implying that upward capillary moisture flow markedly impacted soil moisture up to at least  $85$  cm above the GWT, less so beyond  $105$  cm and no more beyond  $135$  cm.

In the sandy loam and silt loam soil columns, GWT depth did clearly affect the topsoil moisture with higher water contents when the GWT was at  $-115$  cm compared to at  $-165$  cm. Hence, it seems likely that upward moisture flow in the sandy loam and silt loam columns by capillary action reached at least up to a height of  $135$  cm. In case of the silt loam soils, water contents were also consistently high ( $\sim 0.310$  m<sup>3</sup> m<sup>-3</sup>) up to  $105$  cm above the  $-165$  cm GWT and so the capillary fringe likely extended beyond  $135$  cm above the GWT.

Our findings are substantiated by the calculated hydraulic head differences, especially with respect to (dis)continuity of evaporation from the topsoil layer. For example negative  $\Delta H$  between  $-30$  cm and  $-10$  cm for the loamy sand during the  $-165$  cm GWT treatment indicated that evaporation ceased, while for the other soil texture and GWT combinations this did not seem to be the case. However,  $\Delta H$  was unexpectedly negative between  $-120$  cm and  $-85$  cm for the  $-165$  cm GWT treatment of the loamy sand and sandy loam columns. These observations imply a downward moisture transport, which could be the case if macropores served as preferential flow pathways. However, as we observed an increase in water content during the shallower

GWT treatments above this soil segment, upward moisture movement would have been the dominant water flow, with the GWT as starting point of the flow path. We believe these unexpected negative  $\Delta H$  values are therefore more likely a result of cumulative errors when converting measured  $\theta_v$  into H using soil water retention curves obtained from drying phases. Due to hysteresis, such curves can be inaccurate for soil wetting (Hillel, 2003), which was the main expected process at the considered deeper depths near the GWT. In retrospect, a better experimental approach would have been to directly measure hydraulic head using compact tensiometers, especially in the undisturbed parts of the soil columns, where following moisture transport was the main objective. However, even for the smallest lab-scale models, their installation would likely have caused significant disturbance to the soil columns, in contrast to the volumetric sensors used in this study, which had very sharp fine rods able to pierce the waterproof foil surrounding the soil columns with minimal disruption.

In sum, our experiment revealed that upward moisture transport from the GWT to the topsoil occurs when the GWT depth is located within specific depth ranges depending on texture, with a larger impact on moisture supply in case of a shallower (closer to the topsoil) depth. For the loamy sand soils, the depth of the GWT to still affect topsoil via capillary moisture supply was estimated at 85 cm below the surface. For the sandy loam, topsoil moisture supply occurred for GWT depths up to 135 cm below the soil surface, while for the silt loam soils, it seemed that capillary moisture supply from the GWT also at deeper depths than tested here would still markedly affect the topsoil. Former conducted laboratory experiments observed capillary moisture supply from the GWT up to heights of 117 cm and 149 cm in case of loamy sand soils, and up to 175 cm and 183 cm in sandy loam soils (Malik et al., 1989; Shaw and Smith, 1927). In another study (Lane and Washburn, 1947), upward moisture transport was seen up to 240 cm for soils with a  $D_{10}$  of 0.02 mm, which should resemble our silt loam soil (Mozaffari et al., 2022). These reported results are based on setups with repacked soil columns which do not reflect the soil structure of *in situ* conditions. In contrast, our undisturbed soil columns included small scale heterogeneities, with e.g. macropores, small stones, and cracks as they would occur in the field (Lewis and Sjöström, 2010), and this probably explains the somewhat lower capillary rise heights found for loamy sand in our experiment. Our setup was located in a temperature-controlled dark room, where environmental conditions do not approach the field situation. Ambient outdoor wind, temperature and relative air humidity determine evaporation from the topsoil and thus indirectly co-drive the upward suction force across the soil profile as well (Huo et al., 2020). But overall, we expect that mainly soil texture, structure and GWT depth predominantly dictate the height of capillary rise. Consequently, as we worked with 2 m undisturbed soil columns and realistic GWT depths, we do expect findings of GWT-dependent capillary moisture supply and topsoil moisture to be representative for the field situation. Indeed, when GWT is deeper than the so-called evaporation characteristic length, hydraulic pathways get disconnected and even high evaporative demands will not lead to notable topsoil moisture supply (Balugani et al., 2018; Shokri and Salvucci, 2011). This was also observed in the lighter textured loamy sand soil in our study.

## 465 4.2 Impact of GWT on topsoil OM decomposition

Soil water content ( $\theta_v$  or % WFPS) determines soil heterotrophic activity and OM mineralization along a bell-shaped relationship (Manzoni et al., 2012; Moyano et al., 2013; Skopp et al., 1990; Yan et al., 2018). Particularly in the intermediate dry range the response of OM mineralization to volumetric soil moisture is strong, while at lower water content, mostly water potential is a better predictor. Given the occurring moisture range and to avoid conversion of measured volumetric moisture through pF curves sensitive to hysteresis, we further used % WFPS as a more directly obtained measure of soil moisture. As average topsoil moisture was significantly higher in the –115 cm GWT compared to the –165 cm GWT treatment for the sandy loam (38 % compared to 31 % WFPS) and silt loam (43 % compared to 33 % WFPS) soils, we accordingly expected promotion of OM mineralization at shallower GWT for these two soil textures. In loamy sand, shallower GWT only slightly increased topsoil moisture (28 % vs. 25 % WFPS), and so a minimal effect on OM decomposition may be expected. Surprisingly however, the GWT treatment induced moisture differences did not hold the expected effect on  $C_{ryegrass}$  mineralization rates (Fig. 4). Moreover, cumulative 70-days  $C_{ryegrass}$ -min proved lower for the shallower –115 cm GWT treatment (Fig. 5). However, these observations need to be interpreted with care as GWT treatment induced topsoil moisture differences only occurred after day 8, while mineralization rates were an order of magnitude greater during the first five days than later on. Notwithstanding this, about half to two thirds of the cumulative  $C_{ryegrass}$ -min occurred early in the first weeks of the experiment. This implies that the effect of GWT treatment on  $C_{ryegrass}$ -min should not be evaluated based on the 70-days cumulative  $C_{ryegrass}$ -min, but rather only after several weeks, with GWT treatment imposed topsoil moisture differences effective by then. From the fitted kinetic model it emerges that the easily mineralizable  $C_{ryegrass}$  pool had already been mineralized around day 14 in case of the loamy sand and sandy loam soil and day 20 for the silt loam soil. Thereafter, cumulative  $C_{ryegrass}$ -min followed a relatively constant course, i.e. it was determined by the mineralization of a more stable  $C_{ryegrass}$  pool, and therefore the evaluation of GWT on topsoil  $C_{ryegrass}$  mineralization should further solely be based on effects on mineralization rate of the more stable  $C_{ryegrass}$  pool ( $k_s$ ). We accordingly expected lower  $k_s$  estimates with deeper GWT. However, there was no effect of GWT on  $k_s$  for the loamy sand and sandy loam soils, while for the silt loam soils, it was even lower for the –115 cm than for the –165 cm GWT treatment (0.03 vs. 0.07 %  $d^{-1}$ , respectively). These results thus lead to reject the hypothesis that a higher GWT-induced topsoil moisture availability would promote topsoil C mineralization.

To interpret these seemingly illogical effects, it is important to consider the complexity of the relationship between soil moisture and C mineralization, especially when moisture fluctuates as it did in our experiment. This is in contrast to typical experiments to infer the bell-shaped  $\theta_v - C$ -min relationship where moisture is held constant. Notably it is well known that rewetting of dry soil triggers a pulse of microbial activity, resulting in a  $CO_2$  flush, and this phenomenon is referred to as the “Birch effect” (Barnard et al., 2020; Birch, 1958). Former studies found that these respiration pulses enlarge with bigger change in soil moisture state upon rewetting, but also with increased drier pre-wetting soil conditions (Fischer, 2009; Harrison-Kirk et al., 2013; Lado-Monserrat et al., 2014; Manzoni et al., 2020; Unger et al., 2010). For example Harrison-Kirk et al. (2013) observed an increased Birch effect in silt loam soils when pre-wetting moisture state was reduced from 33 % to 22 % WFPS.

Indeed particularly shortly after water applications later in our experiment, the rates tended to deviate between both GWT treatments, with a stronger temporary stimulation in the drier pre-wetting, -165 cm GWT (24 %, 27 % and 29 % WFPS) topsoil, when compared to the wetter, shallower, -115 cm GWT treatment (26 %, 35 %, 39 % WFPS for respectively the loamy sand, sandy loam and silt loam soils) (Fig. 4). Accordingly, a potential explanation could be that the drier condition of topsoil with deeper GWT may have amplified the Birch effect, i.e. rewetting C mineralization pulses caused by the watering events. In the light of this, it is possible that the expected enhancement of C mineralization (as represented by  $k_s$ ) due to increased moisture from capillary action under shallower GWT depths was offset in loamy sand and sandy loam soils, and perhaps even overruled in silt loam soils, by a stronger Birch effect in drier soils with less capillary moisture supply. In other words, the reduced mineralization rates observed in silt loam under a shallower GWT ( $k_s$ ) might be explained, at least in part, by a larger capillary moisture supply compared to the other soil texture and GWT combinations, although other factors, such as an intertwined effects between moisture and temperature, could also be at play. As dry-wet cycles are expected to intensify with climate change in Europe, i.e. longer periods of drought followed by intense rainfall events (CEU. JRC., 2022), such GWT-induced control on moisture variations and consequences for the C budget must be carefully considered.

#### 4.3 Consequences for modelling moisture and SOC balances on the larger spatial landscape scale

Based on our findings, it emerges that variation in GWT at relatively shallow depths as seen in a large part of our study area (North-West Europe) will contribute to spatial variation in topsoil moisture during periods of limited rainfall. Along, Meles et al. (2020) adapted the often used Topography Wetness Index by inversely weighing it with the GWT depth, resulting into a more accurate index for low-slope landscapes, such as our study region. Ukkola et al. (2016) further reported that there is a systematic tendency among numerous land surface models to overestimate the consequences of drought. They attributed this to the assumption of a free-draining soil boundary in these models, i.e. no account is taken of a GWT. According to our results, hydrological modules which calculate water fluxes between adjacent layers, but with free-draining lower boundaries, applied in some soil C models, e.g. DAYCENT (Schimel et al., 2001), would be less accurate for simulation of topsoil moisture during periods with limited rainfall, as these models do not incorporate capillary moisture flow in simulating recharge and presuppose that water draining from the soil profile is lost. The discrepancy with real in-soil occurring physical processes becomes even larger for models that employ a simplistic cascade bucket approach, such as DSSAT (Jones et al., 2003), BIOME-BCG (Thornton, P.E and Law, B.E, 2010), CERES (Gabrielle et al., 1995) and CANDY (Franko et al., 1995). Only a limited number of biogeochemical models calculating water fluxes also include bidirectional water flow between the saturated and unsaturated zones by defining or even calculating a dynamic GWT, e.g. LandscapeDNDC (Haas et al., 2013; Liebermann et al., 2018) and DAISY (Abrahamsen and Hansen, 2000). However, the question remains how accurate such models simulate upward moisture supply and relate C mineralization to water content, particularly under dry conditions. With respect to the latter question, Moyano et al. (2013) concluded that the predictive capacity of current models is still questionable and that these models should incorporate physically-based transport mechanisms for solutes, coupled with a more detailed portrayal of biological reactions



to alterations in soil moisture. In order to reproduce respiration patterns caused by phenomena like the Birch effect, Evans et al. (2016) accordingly argued that models should include physicochemical mechanisms linking water content to microbial growth and to diffusion.

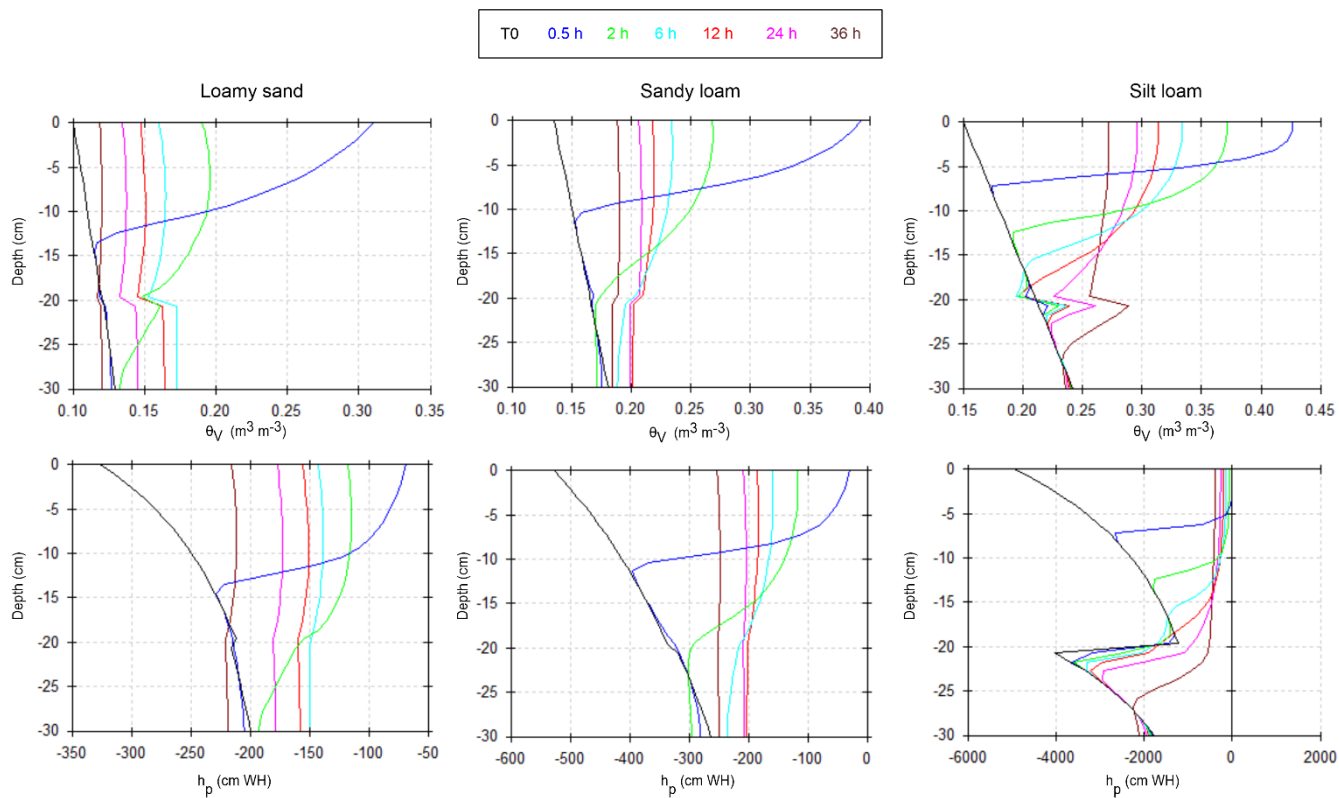
535 Although in our 70-days experiment two GWTs did not suggest a severe impact of GWT on C mineralization, we should not generally conclude that capillary moisture supply is an irrelevant process to be taken along in soil C models. When meteorological droughts extend over longer periods than the simulated period here, the combination of limited moisture supply and increased evaporation might not only lead to soil moisture deficits but it should also diminish groundwater recharge over the longer term (Brauns et al., 2020). This process could then lead to a further reduction of topsoil water content, creating a positive feedback system. As a result, in turn GWT could then deepen further than usually anticipated during summer, which  
540 was in fact also eminently observed over the past years in e.g. Flanders, Belgium (VMM et al., 2022). Especially for croplands in North-West Europe with a GWT close to the evaporation characteristic length, a tipping point in their moisture balance may be reached under future expected prolonged periods of drought in spring or summer. We conclude that soil models that are able to simulate upward moisture supply through capillary action and phenomena such as the Birch effect are better positioned to anticipate soil C trends.

## 545 **5 Conclusion**

Variation in GWT depth, typically to occur in North-West European arable land, was found to significantly impact the soil moisture profile of finer-textured soils during periods with limited rainfall. The expected texture-dependent reach of soil moistening by capillary rise could here be quantified to 85 cm above the GWT for loamy sand soils and minimally to 135 cm for sandy loam and silt loam soils. For situations where the GWT is within these ranges our findings should motivate to include  
550 bidirectional water flow, i.e. drainage and capillary transport, in soil models. Nevertheless, contrary to our hypothesis, a rise of GWT did not enhance decomposition of the added substrate (ryegrass). Moreover, we found that after rewetting, C mineralization pulses were larger for the deepest GWT treatment. We hypothesize that, as soil was drier for the deeper GWT owing to less capillary moisture supply, the imposed rewetting events caused stronger Birch effects. Hence, not just topsoil moisture state itself, but also the extent of its fluctuation over time, probably culminates into the here overall observed net  
555 effect of GWT depth onto C mineralization. To use empirical data from experiments like this to improve soil models, further studies will be needed to deconvolute the effects of soil moisture regimes on soil C mineralization. During prolonged periodic droughts, expected to become more frequent under future climate, correct simulation of the mostly neglected capillary moisture transport may become imperative for reliable simulation of C cycling in agricultural land in North-West Europe.

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## Appendix A

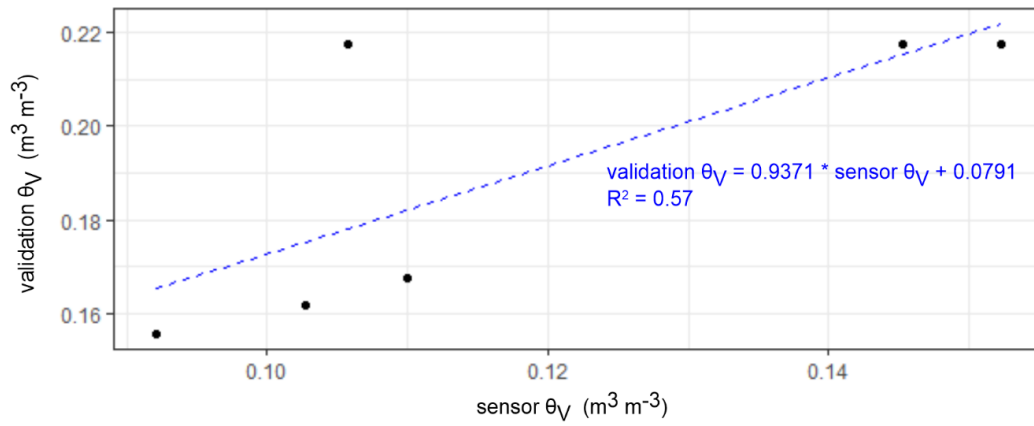


565 **Figure A1: Simulations using HYDRUS-1D to determine when the water, added at T0, reached the lower boundary of the repacked topsoil containing  $^{13}\text{C}$ -labeled ryegrass (at -20 cm depth). A 24-hour period after water addition was found sufficient for all three soil textures (loamy sand, sandy loam, and silt loam) to reach an approximately constant moisture level across the topsoil layer.**

**Table A1: Comparison of volumetric water content measured with sensors at –10 cm and at the start and the end of the incubation of each groundwater treatment (“validation”). Sensor values indicated with “\*” are subjected to a correction via linear regression (see Fig. A2).**

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Location cropland (Texture)	Column replicate	Point in time	$\theta_v$ ( $\text{m}^3 \text{m}^{-3}$ )				
			GWT –165 cm		GWT –115 cm		
			sensor	validation	sensor	validation	
<b>Kruisem</b> (Loamy sand)	1	Start	0.155	0.150	0.132	0.150	
		End	0.092	0.110	0.123	0.164	
	2	Start	0.139	0.150	0.122	0.150	
		End	0.125	0.097	0.126	0.155	
	3	Start	0.122	0.150	0.142	0.150	
		End	0.086	0.093	0.156	0.148	
	4	Start	0.114	0.150	0.103	0.150	
		End	0.099	0.104	0.115	0.182	
	<b>Bottelare</b> (Sandy loam)	1	Start	0.205	0.218	0.106*	0.218
			End	0.122	0.137	0.092*	0.156
		2	Start	0.223	0.218	0.212	0.218
			End	0.132	0.124	0.158	0.176
3		Start	0.205	0.218	0.152*	0.218	
		End	0.109	0.118	0.110*	0.168	
4		Start	0.225	0.218	0.145*	0.218	
		End	0.121	0.117	0.103*	0.162	
<b>Oosterzele</b> (Silt loam)		1	Start	0.250	0.280	0.247	0.280
			End	0.103	0.128	0.211	0.242
	2	Start	0.278	0.280	0.259	0.280	
		End	0.148	0.145	0.170	0.204	
	3	Start	0.241	0.280	0.266	0.280	
		End	0.125	0.146	0.176	0.170	
	4	Start	0.245	0.280	0.272	0.280	
		End	0.109	0.130	0.171	0.171	



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**Figure A2:** Sensors installed at a depth of  $-10$  cm in sandy loam columns 1, 3 and 4 during GWT treatment  $-115$  cm were subjected to a correction via linear regression.

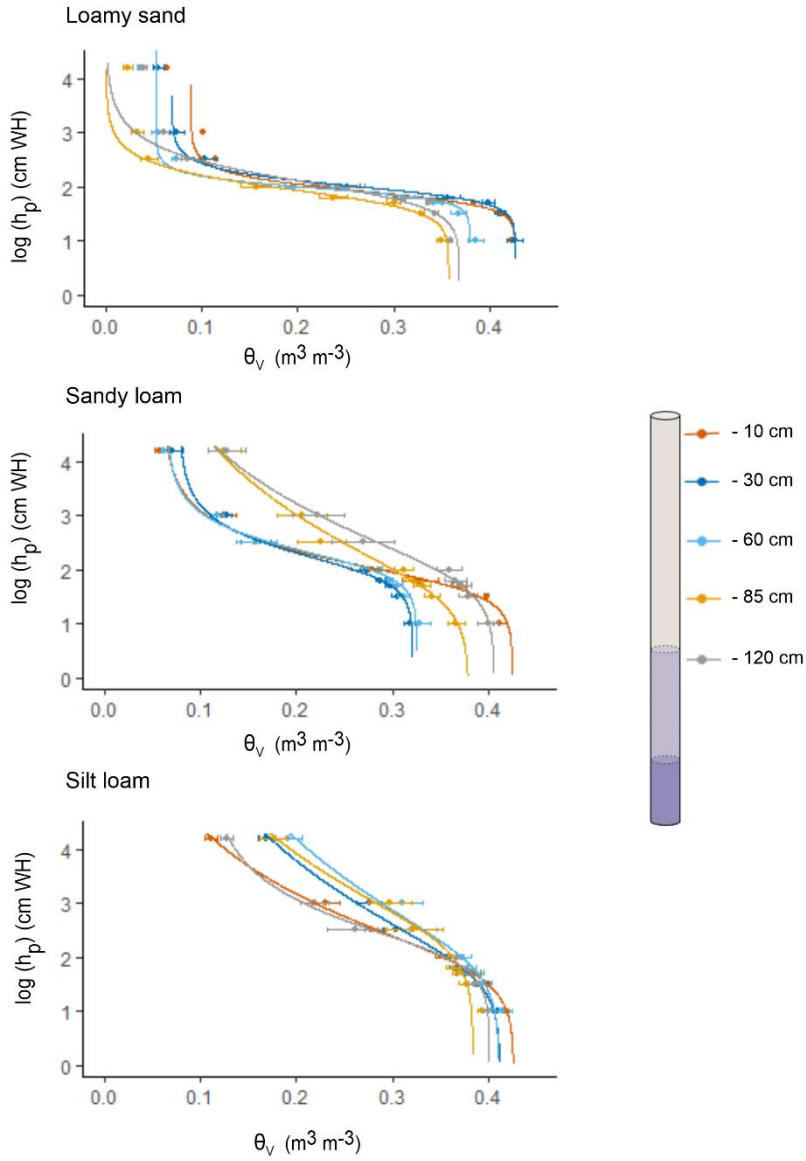


Figure B1: Soil water retention curves for different depths in our soil columns (n=4; except at -10 cm, n = 2).

### **Data / Code availability**

585 Raw data and R scripts will be made available upon request.

### **Author contribution**

Astrid François: Conceptualization, Methodology, Formal analysis, Visualization, Writing – original draft preparation. Orly Mendoza: Visualization, Writing – review & editing. Junwei Hu: Formal analysis, Writing – review & editing. Pascal Boeckx: Funding acquisition, Writing – review & editing. Wim Cornelis: Funding acquisition, Writing – review & editing. Stefaan De Neve: Writing – review & editing. Steven Sleutel: Conceptualization, Methodology, Funding acquisition, Supervision, Writing – review & editing.

### **Competing interests**

Some authors are members of the editorial board of journal SOIL.

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