

1 **Evolution of Cloud Droplet Temperature and Lifetime in**  
2 **Spatiotemporally Varying Subsaturated Environments with**  
3 **Implications for Ice Nucleation at Cloud Edges**  
4

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12 **Abstract.** Ice formation mechanisms in generating cells near stratiform cloud-tops, where mixing and entrainment  
13 occurs in the presence of supercooled water droplets, remain poorly understood. Supercooled cloud droplet  
14 temperature and lifetime may impact heterogeneous ice nucleation through contact and immersion freezing; however,  
15 modeling studies normally assume droplet temperature to be spatially uniform and equal to the ambient temperature.  
16 Here, we present a first-of-its-kind quantitative investigation of the temperature and lifetime of evaporating droplets,  
17 considering internal thermal gradients within the droplet as well as thermal and vapor density gradients in the  
18 surrounding air. Our approach employs solving the Navier-Stokes and continuity equations, coupled with heat and  
19 vapor transport, using an advanced numerical model. For typical ranges of cloud droplet sizes and environmental  
20 conditions, the droplet internal thermal gradients dissipate quickly ( $\leq 0.3$  s) when droplets are introduced to new  
21 subsaturated environments. However, the magnitude of droplet cooling is much greater than estimated from past  
22 studies of droplet evaporation, especially for drier environments. For example, for an environment with pressure of  
23 500 hPa, and ambient temperature far from the droplet of  $-5^{\circ}\text{C}$ , the droplet temperature reduction can be as high as  
24 24, 11, and  $5^{\circ}\text{C}$  for initial ambient relative humidities of 10%, 40%, and 70% respectively. Droplet lifetimes are found  
25 to be tens of seconds longer compared to previous estimates due to weaker evaporation rates because of lower droplet  
26 surface temperatures. Using these new end-of-lifetime droplet temperatures, the enhancement in activation of ice-  
27 nucleating particles predicted by current ice nucleation parameterization schemes is discussed.

## 30 **1 Introduction**

31  
32 Ice formation often occurs near cloud tops of stratiform clouds where ice-generating cells (AMS 2024) are frequently  
33 found in a variety of cold, cloudy environments (Plummer et al., 2014; Ramelli et al., 2021). These cells play a crucial  
34 role in primary ice nucleation and growth (Tessendorf et al., 2015). Evidence of mixing and entrainment and the  
35 presence of supercooled liquid water within and between the highly turbulent cells has been observed (Plummer et al.,  
36 2014; Wang et al., 2020; Zaremba et al., 2024). Within regions of entrainment and mixing at cloud boundaries, cloud  
37 droplets are exposed to subsaturated environments and undergo evaporation that leads to droplet temperatures that  
38 could be several degrees lower than that of the ambient environment (Kinzer and Gunn, 1951; Watts, 1971; Roy et  
39 al., 2023). However, in modeling cloud microphysical processes, the difference in temperature between the cloud  
40 droplets and their environment is generally assumed to be negligible (Pruppacher and Klett, 1997), i.e., the droplets'  
41 temperatures are approximated to be the same as that of their ambient environment. This assumption is reasonable for  
42 cloud droplets inside the cloud but breaks down within entrainment and mixing zones at cloud boundaries and may  
43 lead to uncertainties in the numerical simulations of microphysical processes. Cloud droplet temperatures affect the  
44 calculated droplet diffusional growth or evaporation rates (Roach 1976; Srivastava and Coen 1992; Marquis and  
45 Harrington 2005; Roy et al., 2023), and droplet lifetimes (Roy et al., 2023), radiative effects via temperature-dependent  
46 refractive indices (Rowe et al. 2020), and ice formation via pathways that require supercooled liquid water droplets,  
47 such as contact nucleation (Young, 1974), immersion freezing (Szakáll et al., 2021), and homogeneous nucleation  
48 (Khvorostyanov and Sassen, 1998; Khain and Pinsky, 2018). These uncertainties can propagate into microphysical  
49 parameterization schemes, leading to possible inadequate representation of mixed-phase cloud properties across  
50 various scales (e.g., Large Eddy Simulations (LES), Cloud Resolving Models (CRM), Climate Models), impacting  
51 predictions of precipitation or climate change.

52  
53 Several studies have highlighted the special importance of the air-water interface of the water droplet during ice  
54 nucleation. Many experimental and theoretical studies have suggested that ice initiation occurs at the droplet surface  
55 (Tabazadeh et al., 2002a; Tabazadeh et al., 2002b; Djikaev et al., 2002; Satoh et al. 2002; Shaw et al., 2005) and the  
56 interface thermodynamically favors the contact mode over the immersion freezing mode (Djikaev and Ruckenstein,  
57 2008). Based on their laboratory observations, Tabazadeh et al., (2002a) suggested that homogeneous nucleation of  
58 nitric acid dihydrate (NAD) and nitric acid trihydrate (NAT) particles within aqueous nitric acid droplets primarily  
59 occurs at the droplet surface. This leads to the hypothesis that phase transformations in atmospheric aerosols may  
60 predominantly be surface-based (Tabazadeh et al., 2002b), challenging the traditional theory of homogeneous  
61 crystallization where freezing begins inside the volume of the droplet (Volmer, 1939). Satoh et al. (2002) studied  
62 cooling and freezing in water droplets due to evaporation in an evacuated chamber and found that droplets rapidly  
63 froze with significant supercooling, with the freezing initiated from the droplet surface. Studies employing molecular  
64 dynamics simulations (Chushak et al., 1999, 2000) and thermodynamic calculations (Djikaev et al., 2002) additionally  
65 corroborate that a crystalline nucleus preferentially forms at the droplet surface rather than within the bulk droplet  
66 volume. Laboratory observations from Shaw et al., (2005) reveal that freezing temperatures are 4-5 K higher when an

67 ice-forming nucleus is closer to the surface of a supercooled water droplet compared to when it's immersed within the  
68 droplet. They found that the nucleation rate at the water surface is significantly higher (by a factor of  $10^{10}$ ) than in the  
69 bulk droplet, indicating that the free energy required for critical ice germ formation decreases when near the air-water  
70 interface, and the jump frequency of molecules from the liquid to the solid phase may be significantly enhanced at the  
71 interface. Lü et al., (2005) conducted ice nucleation experiments with acoustically levitated supercooled water  
72 droplets. Using statistical analyses of nucleation rates, they found that ice nucleation predominantly initiates in the  
73 vicinity of the droplet surface. Therefore, given the importance of the droplet surface in ice nucleation and since  
74 evaporation is a surface phenomenon, in the quest to better understand the physical mechanisms responsible for  
75 primary ice nucleation, it is important to accurately investigate the thermal evolution of the evaporating droplet surface  
76 as well as the internal thermal gradients within the supercooled droplet, as ice nucleation is highly temperature  
77 dependent.

78  
79 Droplet condensation or evaporation results from vapor density gradients between the surface of the droplet and the  
80 ambient environment. The solution to determine the rate of droplet growth or decay was first derived by Maxwell  
81 (1890), with an alternative approximate solution presented by Mason (1971) which has since appeared in several  
82 textbooks (e.g. Eq. 7.18 of Rogers and Yau, 1989; Eq. 13-28 of Pruppacher and Klett, 1997). The vapor density at the  
83 droplet surface is a sensitive function of the temperature at the drop surface. For simplicity, cloud models, while  
84 computing the growth/decay rates of cloud droplets, eliminate the use of droplet temperature from the equations by  
85 assuming the saturation vapor density difference as a linear function of temperature difference between the droplet  
86 and ambient environment (e.g. Vaillancourt et al., 2001, Chen et al., 2020). This quasi-steady approximation is  
87 applicable for droplet growth where the supersaturation is typically less than 1% and the difference between the droplet  
88 temperature and ambient air is negligible. For evaporation, where vapor deficits can occur over a wide range of relative  
89 humidities, the approximation breaks down as the droplet temperature can deviate significantly from the ambient  
90 environment (Srivastava and Coen, 1992; Roy et al., 2023).

91  
92 Few studies in the cloud microphysics literature have carried out explicit numerical estimations and evolutions of  
93 supercooled, evaporating cloud droplet temperatures and lifetimes for a wide range of environmental conditions. Roy  
94 et al., (2023) provides a comprehensive review of past theoretical, numerical, or experimental studies of droplet  
95 evaporation. Most of these studies examined the evaporation of raindrops for above  $0^{\circ}\text{C}$  temperatures (Kinzer and  
96 Gunn, 1951; Watts 1971; Watts and Farhi, 1975), either assuming steady-state expressions (Beard and Pruppacher,  
97 1971) or simplifying assumptions of linear dependence of saturation vapor density on temperature (Kinzer and Gunn,  
98 1951; Watts 1971; Watts and Farhi, 1975). Srivastava and Coen (1992) assumed the heat storage term in the droplet  
99 heat budget to be negligible, and investigated the evaporation of isolated, stationary hydrometeors by iteratively  
100 solving the steady-state solutions, using saturation vapor pressure relations from Wexler (1976) to calculate the  
101 saturation vapor density. Roy et al., (2023), by including the heat storage term and solving for time-dependent heat  
102 and mass transfer between single, stationary cloud droplets evaporating in infinitely large, prescribed ambient  
103 environments, demonstrated that the temperatures of the cloud droplets (initial radii between  $30\text{-}50\ \mu\text{m}$ ) reach steady-

104 state quite quickly (within  $<0.5$  s). They considered a wide range of environmental conditions and found that  
105 evaporating droplet temperatures can typically be 1-5 K colder than that of the environment, with values as low as  
106  $\sim 10$  K for low relative humidity, and low-pressure conditions with near  $0^{\circ}\text{C}$  environments. Their steady-state droplet  
107 temperatures agreed well with those of Srivastava and Coen (1992). They showed that the droplet temperature during  
108 evaporation can be approximated by the thermodynamic wet-bulb temperature of the ambient environment. For most  
109 subsaturated conditions, radiative cooling in cloud-top environments was found to play a negligible role in altering  
110 evaporating droplet temperatures, except for larger droplets in environments close to saturation.

111  
112 However, two main issues have not yet been accounted for in the aforementioned studies. Firstly, water droplets were  
113 considered to have a uniform bulk droplet temperature, based on the assumption of infinite thermal heat conductivity  
114 of water, thus ignoring the added complexity of simulating the internal thermal gradients within the droplet. (Kinzer  
115 and Gunn, 1951; Watts, 1971; Srivastava and Coen, 1992, Roy et al., 2023). As several studies suggest that the droplet  
116 surface plays a special role in nucleating ice and evaporation being a surface phenomenon, accurate modeling of the  
117 evolution of droplet surface temperature and internal thermal gradients within the droplet volume is required to  
118 correctly predict the ice nucleation rates. Secondly, to date, none of these studies considered the spatiotemporally  
119 evolving effects of thermal and moisture feedback between the droplet and its immediate environment. The rationale  
120 for justifying the usage of constant ambient conditions far away from the droplet was mostly based on studies where  
121 ambient conditions were defined by prescribed temperature and moisture fields far away from a droplet (Sedunov,  
122 1974; Eq. 7.7 of Rogers and Yau, 1989; Srivastava and Coen, 1992). A correction to the ambient conditions at a radius  
123 similar to the mean distance between droplets ( $\sim 1$  mm) was shown to lead to minimal modifications for typical cloud  
124 conditions (Fukuta, 1992). Thus, this assumption holds for droplets distributed homogeneously in space. Concerning  
125 numerically simulating the growth and decay of a droplet population, Grabowski and Yang (2013) stated: “Cloud  
126 droplets grow or evaporate because of the presence of moisture and temperature gradients in their immediate vicinity,  
127 and these gradients are responsible for the molecular transport of moisture and energy between the droplet and its  
128 immediate environment. One may argue that these gradients need to be resolved to represent the growth accurately.  
129 Elementary considerations demonstrate that the moisture and temperature gradients in the droplet vicinity are  
130 established rapidly [i.e., with a characteristic timescale of milliseconds or smaller (e.g., Vaillancourt et al. 2001, and  
131 references therein)]; thus, the steady-state droplet growth equation is accurate enough. More importantly, the volume  
132 affected by these gradients has a radius of approximately 10 to 20 droplet radii.... One can simply neglect molecular  
133 transport processes in the immediate droplet vicinity and simulate droplet growth using the Maxwellian approach, that  
134 is, by applying the supersaturation predicted by the mean (over the volume occupied by the droplet) temperature and  
135 moisture fields...(see Vaillancourt et al. 2001, appendix).”

136  
137 Here, we quantitatively revisit these arguments within the context of an evaporating supercooled cloud droplet. We  
138 use high-resolution modeling to resolve the spatiotemporally evolving unsteady thermal and vapor density gradients  
139 in the vicinity of the droplet as well as include internal heat transfer within the droplet, relaxing the assumption of  
140 infinite thermal heat conductivity of water. Using an advanced numerical model, our framework employs the finite-

141 element method to solve the Navier-Stokes and continuity equations, coupled with heat and vapor diffusion, with  
142 appropriate boundary conditions. The results from this study extend the findings from Roy et al. (2023) that an  
143 evaporating droplet can exist at a temperature lower than that of the ambient environment, and that the temperature  
144 deviation increases from the steady-state value under certain environmental conditions. This may lead to significant  
145 enhancement in ice nucleation by increasing the predicted number concentrations of activated ice-nucleating particles  
146 (INPs) either immersed within or externally contacting the supercooled droplet. The current study advances the  
147 numerical approach presented in Roy et al. (2023) by including the impact of internal heat gradients within the droplet  
148 and spatiotemporally varying heat and mass transfer between the droplet and its immediate environment. We also  
149 provide droplet lifetime comparisons with estimates from Roy et al. (2023) and pure diffusion-limited evaporation  
150 calculations. The implications of the evaporating supercooled cloud droplet temperatures and lifetimes on ice  
151 nucleation at cloud boundaries are discussed.

152

## 153 **2 Numerical Methodology**

### 154 **2.1 Description of COMSOL**

155

156 The simulation of the spatiotemporally varying droplet temperature and radius of an evaporating cloud droplet  
157 embedded in a gaseous domain is difficult to solve analytically because of the moving and shrinking boundary at the  
158 surface of the evaporating droplet. These kinds of moving boundary problems are known as Stefan problems. To  
159 model this process, we have used an advanced numerical solver, COMSOL (Version 6.0), which employs a finite  
160 element method to solve partial differential equations (PDEs). The COMSOL Multiphysics software simultaneously  
161 uses spatial, material, and mesh coordinate systems described as the spatial frame, material frame, and mesh frame,  
162 respectively. The spatial frame is a fixed, global, Euclidean coordinate system, which in 2D has spatial cartesian  
163 coordinates  $(r, z)$  with the center of the droplet at  $(r, z) = (0,0)$  (Fig. 1). The material frame specifies the material  
164 substance, in this case, water or air. The mesh frame is a coordinate system used internally by the finite element  
165 method.

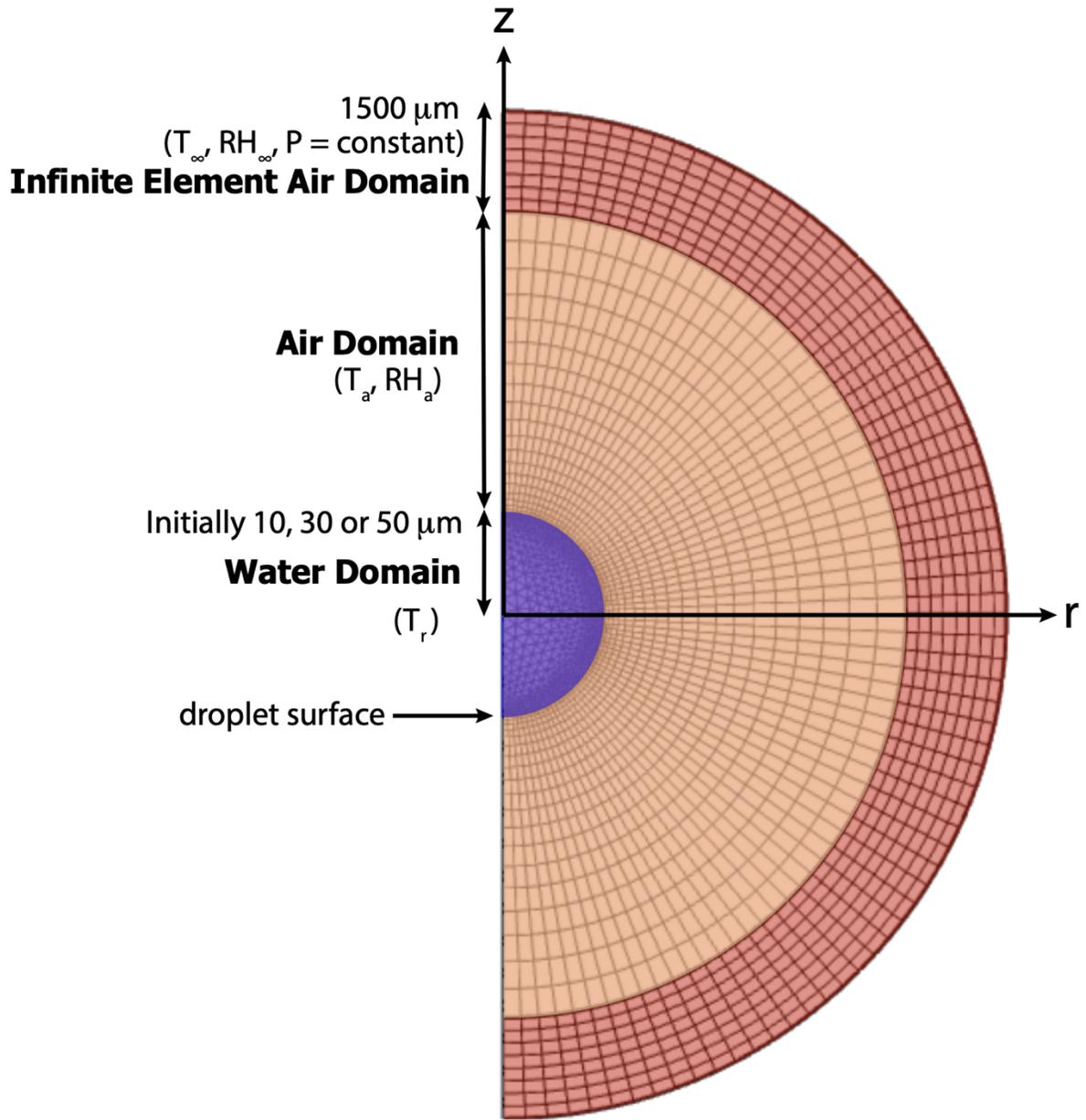
166

167 The Navier-Stokes and Fick's second law of diffusion equation, which follows from the continuity equation, along  
168 with appropriate boundary conditions (see Sec. 3) are solved to conserve mass and momentum in the whole system.

169 The following physics interfaces in COMSOL were used to simulate droplet evaporation: (1) *Two-Phase Laminar*  
170 *Fluid Flow*, which includes a moving mesh to track the shrinking water-air interface of the evaporating water droplet  
171 and fluid-fluid interface that incorporates evaporative mass flux; (2) *Transport of Diluted Species* to track water vapor  
172 diffusion through the air domain and predict the evaporation rate at the droplet surface; and (3) *Heat Transfer in Fluids*  
173 which accounts for the non-isothermal flow within the computational domain, temperature-dependent saturation vapor  
174 density at the droplet interface, and a boundary heat source to account for the latent heat of evaporation. The  
175 computational domain also includes an infinite element air domain (COMSOL 2023b) to specify and maintain  
176 boundary conditions far away from the droplet. The physics modules are coupled through non-isothermal flow

177 between heat transfer and fluid flow, and mass transport at the fluid–fluid interface between fluid flow and species  
178 transport.

179  
180 A non-uniform moving mesh was created by breaking down the computational domain into numerous fine elements  
181 of variable sizes, using the Arbitrary Lagrangian-Eulerian technique (Yang et al., 2014) to accurately track the moving  
182 air-water interface at the droplet surface. In the ALE technique, the spatial cartesian coordinate system  $(r, z)$  is fixed,  
183 while the coordinates of the material  $(R, Z)$  and the mesh  $(R_m, Z_m)$  nodes are functions of time as the droplet evaporates.  
184 However, the material and mesh node coordinates are always fixed in their respective frames. Initially, the spatial,  
185 material and mesh frames are all identical. As the simulation starts, the material and mesh frames deform as the moving  
186 boundary of the droplet shrinks during evaporation. After each time step, the deformed nodes are mapped to the spatial  
187 frame, where calculations are performed. In this study, we have used triangular mesh elements (COMSOL 2023c)  
188 within the droplet and quadrilateral mesh elements (COMSOL 2023d) for the rest of the domain as shown in Fig. 1.  
189 The triangular mesh allows a higher resolution at the droplet surface, and both meshes adjust continually as the droplet  
190 surface shrinks during evaporation. Finally, to simulate the water droplet evaporating in ambient air system, with  
191 appropriate initial and boundary conditions, the discretized PDEs are numerically solved with adaptive time steps ( $\leq$   
192 0.01 s) to maintain numerical stability and obtain the solution (the temporal evolution of droplet temperature and  
193 radius) for a range of conditions.



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 196  
 197  
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 201  
 202  
 203

Figure 1: Schematic depicting the evaporating droplet, embedded in the air domain. The spatial frame  $(r, z)$  and the initial mesh frame (triangular elements within the droplet and quadrilateral elements outside the droplet) are shown (not to scale).

## 204 2.2 Justification for choice of environmental parameters in the simulations

205

206 Probing the evolution of the droplet and its immediate environment under a wide swath of conditions was  
207 computationally too expensive, thus, certain choices regarding the parameter selection were made. The assumption  
208 behind the computational set-up is that the supercooled droplet is suddenly introduced to a subsaturated environment  
209 with ambient temperature,  $T_\infty = 273.15$  K, 268.15 K, or 263.15 K, as might happen when the droplets are near cloud  
210 boundaries such as those occurring in cloud-top generating cells. These temperatures are the ones where activation of  
211 INPs is thought to be least effective. Calculations presented in Sec. 4 consider three different environments having  
212 ambient relative humidity,  $RH_\infty = 10, 40, \text{ and } 70\%$ , and two different ambient pressures,  $P = 500, \text{ and } 850$  hPa, and  
213 initial cloud droplet radii,  $r_0$ , of 10, 30, and 50  $\mu\text{m}$ . The pressure levels were chosen based on the occurrence of 273.15  
214 K, 268.15 K, and 263.15 K in standard atmospheric profiles for tropical latitudes and middle latitudes under warm  
215 and cool season conditions (Standard Atmosphere, 2021). Overall, 90 numerical experiments were performed using  
216 various combinations of initial  $RH_\infty$ ,  $T_\infty$ ,  $P$ , and  $r_0$  to obtain a better understanding of the relationships between the  
217 evolution of droplet temperatures and radii, and environmental variables. Of these, the results of 54 experiments are  
218 reported in detail herein. The results of these experiments are later summarized in Figs. 3-10 and Tables 1-2. The  
219 specific combinations of environmental parameters and initial droplet radii used in this study were also selected to  
220 enable easy comparison with results from a previous study of droplet evaporation (Roy et al., 2023). Also, to be noted,  
221 the effect of radiation in this study was neglected based on Roy et al. (2023), which demonstrated the negligible role  
222 played by radiation in modifying evaporating droplet temperatures under most subsaturated conditions ( $RH < 80\%$ ).

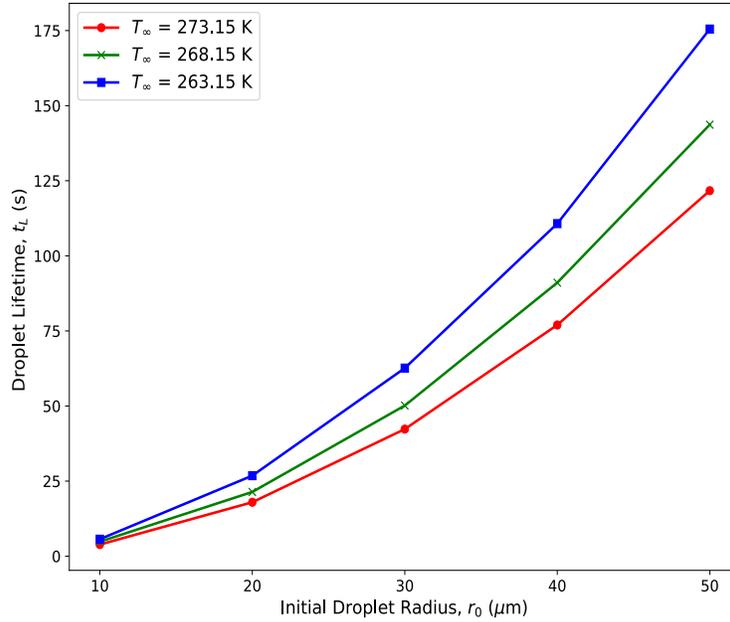
223

## 224 2.3 Justification for choice of droplet lifetime cut-off

225

226 For each experiment, the computational time rose exponentially to maintain numerical stability as the droplet radius  
227 decreased during evaporation and the grid sizes needed to be smaller. To avoid exceptionally long computation time,  
228 the cut-off radius for the simulations was set to be when the volume of the droplets decreased by 99.5% to reach 0.5%  
229 of the initial droplet volume. For  $r_0 = 10, 20, 30, 40, 50$   $\mu\text{m}$ , the cutoff radii of the droplets are 1.71, 3.42, 5.13, 6.84,  
230 and 8.55  $\mu\text{m}$ , respectively. Note that due to the Raoult effect, for a solution droplet with a mass of dissolved and  
231 ionized  $\text{NaCl} = 10^{-13}$  g, the reduction in the evaporation rate ( $dr/dt$ ) from that of a pure water droplet is about 1% for  
232 a 1  $\mu\text{m}$  radius droplet and 4% for a 0.7  $\mu\text{m}$  droplet. As all cut-off radii considered here are  $> 1$   $\mu\text{m}$ , the solute effect  
233 can be neglected. From the Kelvin equation, the equilibrium vapor pressure over a curved surface of pure water  
234 approaches the value of equilibrium vapor pressure over a flat surface of pure water for a radius  $> 0.01$   $\mu\text{m}$ . Thus,  
235 curvature effects were also neglected. For simplicity, we will refer to the cutoff time as the *droplet lifetime*, although  
236 the droplets will survive for a longer time before complete evaporation. The droplet lifetime increases with the initial  
237 droplet radius, higher atmospheric pressure, and higher  $RH_\infty$  (Fig. 2).

238



239  
 240 **Figure 2: Droplet lifetimes,  $t_L$  in seconds, for droplets with varying initial droplet radii,  $r_0 = 10, 20, 30, 40$  and  $50 \mu\text{m}$ ,**  
 241 **evaporating in an initial ambient environment with three different ambient temperatures,  $T_\infty = 273.15$  ( $0^\circ\text{C}$ ),  $268.15$  ( $-5^\circ\text{C}$ )**  
 242 **and  $263.15$  ( $-10^\circ\text{C}$ ) K, with relative humidity,  $RH_\infty = 70\%$ , with pressure,  $P = 850$  hPa.**  
 243

244 **2.4 Sensitivity to domain size**

245  
 246 It was important to ensure that the spatiotemporally varying thermal and vapor density gradients in the ambient air in  
 247 the vicinity of the evaporating droplet don't interfere with the constant ambient conditions ( $RH_\infty$  and  $T_\infty$ ) at the external  
 248 boundary of the computational domain. Sensitivity tests with different air domain sizes of 10, 30, and 50 times the  
 249 initial droplet radius were carried out to determine the droplet temperature and radial dependence on domain size. It  
 250 was found that the evolution of droplet temperature and radius was not sensitive to domain sizes larger than 10 times  
 251 the droplet radius considered. Based on the sensitivity analysis, the maximum size of the computational domain for  
 252 all experiments was fixed at  $1500 \mu\text{m}$ , 30 times the largest droplet considered.

253  
 254 **3 Theory**

255  
 256 **3.1 Assumptions**

257  
 258 The framework of the numerical model assumes that an isolated, stationary, spherical, pure water droplet is suspended  
 259 within a 2D axisymmetric ambient air domain with constant ambient temperature ( $\leq 0^\circ\text{C}$ ) and relative humidity  
 260 ( $<100\%$ ) at a sufficiently far distance away from the droplet that the droplet evaporation does not influence the far  
 261 environment. The water droplet and air are considered to be Newtonian fluids, with the assumption that no internal  
 262 circulation occurs within the droplet and that there is no ventilation, no radiative heat transfer, and negligible buoyancy  
 263 effects due to gravity. This computational approach is an advanced form of the one described in Roy et al., (2023),

264 but also includes the effect of internal droplet heat transfer and spatiotemporal gradients in temperature and vapor  
 265 density between the droplet and the environment (see discussion in Sec. 5).

### 267 3.2 Governing Equations

268  
 269 Based on the above assumptions, the following are the equations governing the system during droplet evaporation in  
 270 the ambient air.

271  
 272 (1) Fluid flow: The *Laminar Flow* interface models the weakly compressible form of the Navier-Stokes equation,  
 273 along with the continuity equation in the water and air domains,

$$274 \quad \rho \frac{\partial \mathbf{u}}{\partial t} + \rho(\mathbf{u} \cdot \nabla) \mathbf{u} = \nabla \cdot [-p\mathbf{I} + \boldsymbol{\tau}] + \mathbf{F} \quad (1)$$

$$275 \quad \boldsymbol{\tau} = \mu(\nabla \mathbf{u} + (\nabla \mathbf{u})^T) - \frac{2}{3} \mu(\nabla \cdot \mathbf{u})\mathbf{I} \quad (2)$$

$$276 \quad \frac{\partial \rho}{\partial t} + \nabla \cdot (\rho \mathbf{u}) = 0 \quad (3)$$

277  
 278 where  $t$  is time,  $\rho$  is the fluid density ( $\text{kg/m}^3$ ),  $\mathbf{u}$  is the fluid velocity vector ( $\text{m/s}$ ),  $p$  is pressure (Pa),  $\mathbf{I}$  is the identity  
 281 tensor,  $\boldsymbol{\tau}$  is the viscous stress tensor (Pa),  $\mathbf{F}$  is the external volume force vector ( $\text{N/m}^3$ ), which is assumed to be  
 282 negligible here, and  $\mu$  is the fluid dynamic viscosity. For water below 273.15 K, the dynamic viscosity can be  
 283 approximated as 1.79 mPa s. For air, COMSOL uses an empirical equation that produces values equivalent to

284 Sutherland's law (White, 2006),  $\mu = \mu_0 \left(\frac{T}{T_0}\right)^{\frac{3}{2}} \left(\frac{T_0 + S_\mu}{T + S_\mu}\right)$  where  $\mu_0 = 1.716 \times 10^{-5} \text{ N s m}^{-2}$ ,  $T_0 = 273 \text{ K}$ , and  $S_\mu = 111 \text{ K}$   
 285 for air. The empirical equation is given as:

$$286 \quad \mu = -8.38278 \times 10^{-7} + 8.35717342 \times 10^{-8}T - 7.69429583 \times 10^{-11}T^2 + 4.6437266 \times 10^{-14}T^3 -$$

$$287 \quad 1.06585607 \times 10^{-17}T^4 \quad (4)$$

288  
 289 (2) Heat Transport: The *Heat Transfer in Fluids* interface models heat transfer in all domains (air, water, infinite  
 290 element domain) using the following version of the heat equation:

$$291 \quad \rho C_p \frac{\partial T}{\partial t} + \rho C_p \mathbf{u} \cdot \nabla T + \nabla \cdot \mathbf{q} = 0 \quad (5)$$

$$292 \quad \mathbf{q} = -k \nabla T \quad (6)$$

293  
 294 where  $\rho$  ( $\text{kg/m}^3$ ) is the fluid density,  $C_p$  ( $\text{J}/(\text{kg} \cdot \text{K})$ ) is the fluid heat capacity at constant pressure,  $T$  is the temperature,  
 296  $k$  ( $\text{W}/(\text{m} \cdot \text{K})$ ) is the fluid thermal conductivity,  $\mathbf{u}$  ( $\text{m/s}$ ) is the fluid velocity field from the Laminar Flow interface,  $\mathbf{q}$   
 297 ( $\text{W}/\text{m}^2$ ) is the heat flux by conduction. We chose the value of  $k$  for supercooled water at  $0.56 \text{ W m}^{-1} \text{ K}^{-1}$  based on Fig.  
 298 3 of Biddle et al., (2013) where the thermal conductivity of supercooled water is very close to  $0.56 \text{ W}/(\text{m K})$  for the

299 range of temperatures used in this study. Based on Beard and Pruppacher (1971), the thermal conductivity of air, given  
 300 by  $k_a = 0.004184[5.69 + 0.017(T - 273.15)]$  ( $\text{W m}^{-1} \text{K}^{-1}$ ), has very weak dependence on temperature over the  
 301 temperature range used in this study. For both  $T = 273.15 \text{ K}$  and  $253.15 \text{ K}$ , the value of  $k_a$  is  $0.02 \text{ W m}^{-1} \text{K}^{-1}$ . Hence,  
 302 we have used a constant value of  $0.02 \text{ W m}^{-1} \text{K}^{-1}$ .

303

304 (3) Mass transport: The *Transport of Diluted Species* interface models water vapor transport through Fick's laws of  
 305 diffusion, solving the mass conservation equation for vapor transfer in all domains except within the cloud droplet:

306

$$307 \quad \frac{\partial c}{\partial t} + \nabla \cdot \mathbf{J} = 0 \quad (7)$$

$$308 \quad \mathbf{J} = -D\nabla c \quad (8)$$

309

310 where  $c$  is the concentration of water vapor ( $\text{mol/m}^3$ ),  $D$  denotes the diffusion coefficient ( $\text{m}^2/\text{s}$ ), and  $\mathbf{J}$  is the mass flux  
 311 diffusive flux vector ( $\text{mol}/(\text{m}^2 \cdot \text{s})$ ).  $D$  is calculated following Hall and Pruppacher (1976) and defined as follows:  $D =$   
 312  $0.0000211 \frac{P_0}{P} \left[ \frac{T}{T_0} \right]^{1.94}$  ( $\text{m}^2 \text{ s}^{-1}$ ) with reference pressure,  $P_0 = 1013.25 \text{ hPa}$ , reference temperature,  $T_0 = 273.15 \text{ K}$ ,  
 313 atmospheric temperature,  $T$ , and pressure,  $P$ . In this study, values of  $P$  are either fixed at 500 or 850 hPa to determine  
 314 the effect of ambient air pressure on droplet evaporation.  $\mathbf{J}$  is obtained from the Laminar Flow interface through  
 315 coupling between these interfaces.

316

### 317 3.3 Initial conditions

318 The initial velocity components in the  $r$ , and  $z$  directions are assumed to be  $0 \text{ m/s}$  in both air and water domains. The  
 319 initial fluid pressure is  $p = P_{0,air}$  (Pa), specified either at 500 or 850 hPa in the air domain, and in the water domain,  $p$   
 320  $= P_{0,water} = \frac{2\sigma}{r_0}$  Pa, where surface tension,  $\sigma = 70 \times 10^{-3} \text{ (N/m)}$ . For the heat transfer module, all domains are assumed  
 321 to be at a prescribed initial ambient temperature,  $T_0$ , which is the same as that of a point at a far distance away from  
 322 the droplet,  $T_\infty$ .

323 For the vapor transfer interface, except within the droplet, all domains are at an initial vapor concentration of  $c_{0,air}$   
 324 which is again assumed to be the same as that of the constant ambient concentration value far from the droplet,  $c_\infty$ ,  
 325 calculated as follows:

$$326 \quad c_\infty = \frac{RH_\infty \times e_{sT_\infty}}{R_{univ} \times T_\infty} \text{ where, } RH_\infty \text{ is set at a constant ambient relative humidity far from the droplet, } R_{univ} = 8.3145$$

327 (J/mol/K),  $T_\infty$  is in K. The saturation vapor pressure is calculated as,  $e_{sT_\infty} = 610.94 * \exp\left(\frac{17.625 * T_\infty}{T_\infty + 243.04}\right)$  (in Pa, with

328  $T_\infty$  in  $^\circ\text{C}$ ) following Alduchov and Eskridge (1996).

329

330

### 3.4 Model Constraints and Boundary Conditions

332

333 1. Within the droplet and throughout the domain, the following conditions are applicable:

334 
$$\mathbf{u} \cdot \mathbf{n} = 0 \quad (9)$$

335 
$$[-p\mathbf{I} + \boldsymbol{\tau}] \cdot \mathbf{n} = 0 \quad (10)$$

336 
$$\mathbf{q} \cdot \mathbf{n} = -k\nabla T \cdot \mathbf{n} = 0 \quad (11)$$

337 
$$-D\nabla c \cdot \mathbf{n} = 0 \quad (12)$$

338 where  $\mathbf{n}$  is the normal to an outward-pointing vector from the center of the droplet. This constraint limits water  
339 mass, water vapor and heat flow to the direction normal to the droplet surface.

340

341 2. At the fluid-fluid interface i.e., droplet-air boundary, the droplet surface is assumed to be at vapor saturation  
342 throughout its lifetime. Hence, saturated vapor concentration at the shrinking droplet boundary, using the ideal gas

343 law, is given by,  $c_{sat}(T_{sf}) = \frac{e_s(T_{sf})}{R_{univ} \times T_{sf}}$  where  $T_{sf}$  is the surface temperature, in K. The saturation vapor pressure  $e_s(T_{sf})$

344 is estimated as  $e_s(T_{sf}) = 610.94 * \exp\left(\frac{17.625 * T_{sf}}{T_{sf} + 243.04}\right)$  (in Pa, with  $T_{sf}$  in °C) again following Alduchov and Eskridge  
345 (1996).

346

347 The local evaporative mass flux at the interface is given by diffusion of water vapor across the water-air interface,  $M_J$   
348 (kg/ m<sup>2</sup> s)

349 
$$\mathbf{M}_J = M_w \mathbf{n} \cdot (-D\nabla c) \quad (13)$$

350

351 where the molecular weight of water,  $M_w = 0.018$  (kg/mol). Although the temperature is continuous across the droplet-  
352 air boundary, there is a discontinuity in heat flux across the interface due to the evaporation of water. Thus, the latent  
353 heat of evaporation  $L$ , defined as  $L = [2501 - 2.44T_r]$  kJ kg<sup>-1</sup> with droplet surface temperature,  $T_r$  in °C, is  
354 incorporated as a boundary heat sink as  $-M_J L$  (W/m<sup>2</sup>).

355

356 The mass balance at the water-vapor boundary at the droplet surface, and the velocity of the moving mesh  $\mathbf{u}_{mesh}$ , at  
357 the shrinking water-air interface, are expressed by the following equations, based on Scardovelli and Zaleski, (1999):

358

359 
$$\mathbf{u}_w = \mathbf{u}_v + M_J \left( \frac{1}{\rho_w} - \frac{1}{\rho_v} \right) \mathbf{n} \quad (14)$$

360

361 
$$\mathbf{u}_{mesh} = (\mathbf{u}_w \cdot \mathbf{n} - \frac{M_J}{\rho_w}) \mathbf{n} \quad (15)$$

362

363 where the subscripts  $w$  and  $v$  represent water and vapor respectively.

364

365 The stresses are balanced at the water-vapor interface by the following conditions, based on Yang et al., (2014):

366

367

$$\mathbf{n} \cdot (\mathbf{S}_w - \mathbf{S}_v) = \sigma(\nabla_\sigma \cdot \mathbf{n})\mathbf{n} - \nabla_\sigma \sigma \quad (16)$$

368

$$\mathbf{S} = [-p\mathbf{I} + \boldsymbol{\tau}] \quad (17)$$

369

370 where  $\mathbf{S}$  is the total stress tensor and  $\nabla_\sigma$  is the surface gradient operator defined by

371

$$\nabla_\sigma = (\mathbf{I} - \mathbf{n} \cdot \mathbf{n}^T)\nabla \quad (18)$$

372

373 In the normal direction of the boundary, the force is balanced by,

374

$$\mathbf{n} \cdot (\mathbf{S}_w - \mathbf{S}_v) = \frac{\sigma}{r_c} \cdot \mathbf{n} \quad (19)$$

375

376 where  $r_c$  is the curvature radius.

377

378 3. The external air domain boundary is open with the following condition:

379

$$[-p\mathbf{I} + \boldsymbol{\tau}]\mathbf{n} = -f_0\mathbf{n}, \quad (20)$$

380

381 where normal stress,  $f_0 = 0 \text{ N/m}^2$ .

382

383 4. The infinite element domain consists of air and is considered to be an ideal gas. The temperature, relative humidity, and concentration far from the droplet i.e., at the inner boundary of the infinite element domain, are fixed at  $T_\infty$  and  $c_\infty$ , respectively.

384

### 385 3.5 Coupling between the COMSOL interfaces

386

387 To numerically model the evaporating droplet embedded in the air domain, intercoupling between the three physics interfaces - laminar two-phase flow (formulated within the Arbitrary Lagrangian-Eulerian framework), the heat transfer in fluids, and the transport of diluted species within the air medium are established through the following mechanisms: (i) the local evaporative mass flux at the droplet-air interface, which is related to the mesh velocity for the laminar flow, is estimated by the diffusion of water vapor in the air domain; (ii) saturated vapor concentration at the droplet-air interface, which serves as a boundary condition for the vapor diffusion, is calculated using the local temperature at the droplet interface; and (iii) the evaporative heat flux at the droplet-air interface acts as a heat sink boundary condition for the heat transfer in fluids module.

388

## 389 4 Results

390

391 Since evaporation is a surface phenomenon, with the evaporative cooling at the droplet surface acting as a heat sink, the temperature of the evaporating droplet surface should be lower than the center of the droplet. In all simulations,

392

403 the center to surface temperature gradient within the droplet forms almost instantaneously as evaporative cooling at  
404 the droplet surface occurs extremely fast. The time required for the droplet to reach internal thermal equilibrium  
405 depended slightly on the initial size of the droplet and the ambient  $RH_\infty$ , with larger droplets and drier environments  
406 leading to more time required by the droplets to reach equilibrium. However, generally, for typical cloud droplet sizes  
407 and environmental conditions considered here ( $r_0 = 10, 30, 50 \mu\text{m}$ ), the internal thermal gradients dissipate and the  
408 temperatures throughout the droplets become uniform in  $\leq 0.3$  s, consistent with Fick's laws of diffusion with a  
409 diffusive timescale of  $r^2/D$ , where  $r$  is the length scale and  $D$  is the thermal diffusivity of water. For this study, we  
410 have simulated internal droplet heat transfer for the entirety of the droplet lifetime and will be reporting the average  
411 droplet temperatures as "droplet temperatures" in the results, unless noted otherwise.

412  
413  
414  
415

#### 4.1 Droplet Thermal and Radial Evolution: Influence of Initial Droplet Size and Environmental Factors

416 Figures 3 and 4 depict the early evolution of the droplet average temperatures and radii ( $r_0 = 10, 30$  and  $50 \mu\text{m}$ ) for  
417 the first few seconds of their lifetimes (as defined in Sec. 2c), for different environments with constant ambient  
418 conditions ( $T_\infty, RH_\infty$ , and  $P$ ) far from the droplet. Tables 1 and 2 provide the final temperature values and total lifetimes  
419 of the droplets. Figures 3 and 4 also state the droplet temperatures at the end of their lifetimes ( $T_L$ ) and the total  
420 lifetimes of the droplets ( $t_L$ ). For all numerical experiments, the evaporating droplet temperature decreases sharply,  
421 within  $< 0.5$  s, to a certain temperature defined here as the transition point,  $T_i$ , where the slope of the curve changes.  
422 After reaching  $T_i$ , the decrease in droplet temperature is relatively more gradual as can be seen from Figs. 3 and 4. For  
423 example, in Fig. 3(c), for  $P = 500$  hPa,  $T_\infty = 268.15$  K ( $-5^\circ\text{C}$ ),  $RH_\infty = 10\%$ , a droplet with  $r_0 = 10 \mu\text{m}$ , takes about 0.03  
424 s to reach  $T_i$  at 260.98 K (a decrease of 7.17 K from initial temperature). In contrast, a 30  $\mu\text{m}$  droplet takes about 0.12  
425 s to reach  $T_i$  at 260.85 K (a decrease of 7.3 K from initial temperature), and a 50  $\mu\text{m}$  droplet takes about 0.33 s to  
426 reach  $T_i$ . Finally, the 10  $\mu\text{m}$  droplet reaches the end of its lifetime in 1.05 s i.e.  $t_L = 1.05$  s with temperature,  $T_L =$   
427 244.12 K after reaching  $T_i$ , while for the 30  $\mu\text{m}$  droplet,  $t_L = 11.4$  s with  $T_L = 244.31$  K, and  $t_L = 32.76$  s for the 50  $\mu\text{m}$   
428 droplet with  $T_L = 244.29$  K after reaching  $T_i$ .

429

430 The evaporation process in these experiments starts in a condition that is far from equilibrium. The coupled air- droplet  
431 system attempts to evolve towards a steady-state where the thermal energy towards the droplet compensates for  
432 evaporative cooling at the droplet surface. In this process, the droplet initially rapidly cools to the thermodynamic  
433 wet-bulb temperature of the initial environment similar to what has been shown in Roy et al., (2023). However, under  
434 low relative humidity conditions, the thermal and vapor diffusion are not yet near equilibrium. As the system attempts  
435 to achieve a steady-state, the imbalance in the heat fluxes associated with vapor and thermal diffusion in the immediate  
436 vicinity of the drop leads to a gradual reduction in the wet-bulb temperature of the immediate droplet environment  
437 leading to a continued slow decrease in the droplet temperature as the droplet continues to evaporate.

438

439 In general, we can see that a higher ambient  $T_\infty$ , and lower  $RH_\infty$  and  $P$  leads to a larger reduction in droplet temperature  
440 from its initial temperature. Therefore, drier, relatively warmer (closer to  $0^\circ\text{C}$ ), and lower-pressure environments lead

441 to the strongest evaporative cooling of the droplets. Also, due to evaporative cooling, the droplets survive longer as  
442 compared to the pure diffusion-limited evaporation approach where the decreases in evaporating droplet temperature  
443 have not been considered (see Sec. 5). However, drier, relatively warmer (close to  $0^{\circ}\text{C}$ ), and lower-pressure  
444 environments lead to smaller droplet lifetimes as compared to more humid environments, with lower ambient  
445 temperatures and higher pressures.

446

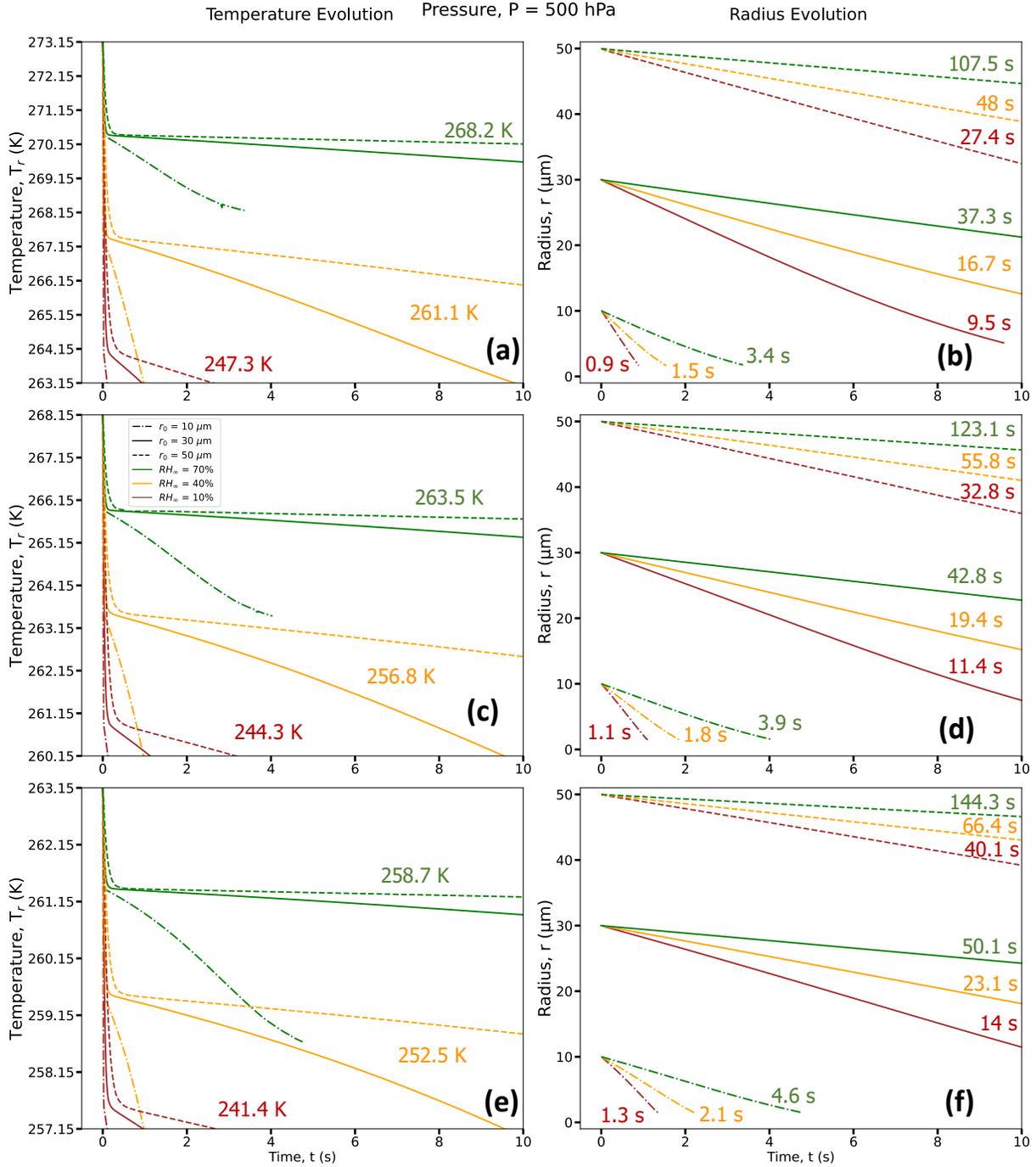
#### 447 **4.2 Environmental Evolution: Evolution of Temperature, Relative Humidity, and Wet-Bulb Temperature in** 448 **the air domain near the droplet**

449

450 Figures. 5-7 (a, d) show radial cross sections of the computational domain, starting from the center of the droplet at  
451  $(r, z) = (0, 0)$ , along the  $r$  axis to the edge of the domain at  $r = 1500 \mu\text{m}$ , while Figs. 5-7 (b, e) expand the dashed box  
452 regions of Figs. 5-7 (a, d), and Figs. 5-7 (c, f) further expand the dashed box regions of Figs. 5-7 (b, e). All panels  
453 show the spatiotemporal evolution of temperature (Fig. 5), relative humidity (Fig. 6), thermodynamic wet-bulb  
454 temperature (Fig. 7), and droplet radius for a droplet with initial radius,  $r_0 = 50 \mu\text{m}$ , introduced to an initial environment  
455 with pressure,  $P = 500 \text{ hPa}$ , ambient temperature,  $T_{\infty} = 268.15 \text{ K}$  ( $-5^{\circ}\text{C}$ ), with two different relative humidities,  $RH_{\infty}$   
456  $= 10\%$  and  $70\%$ . The evolution of temperature within the droplet is left of the dashed black line, which denotes the  
457 droplet radius.

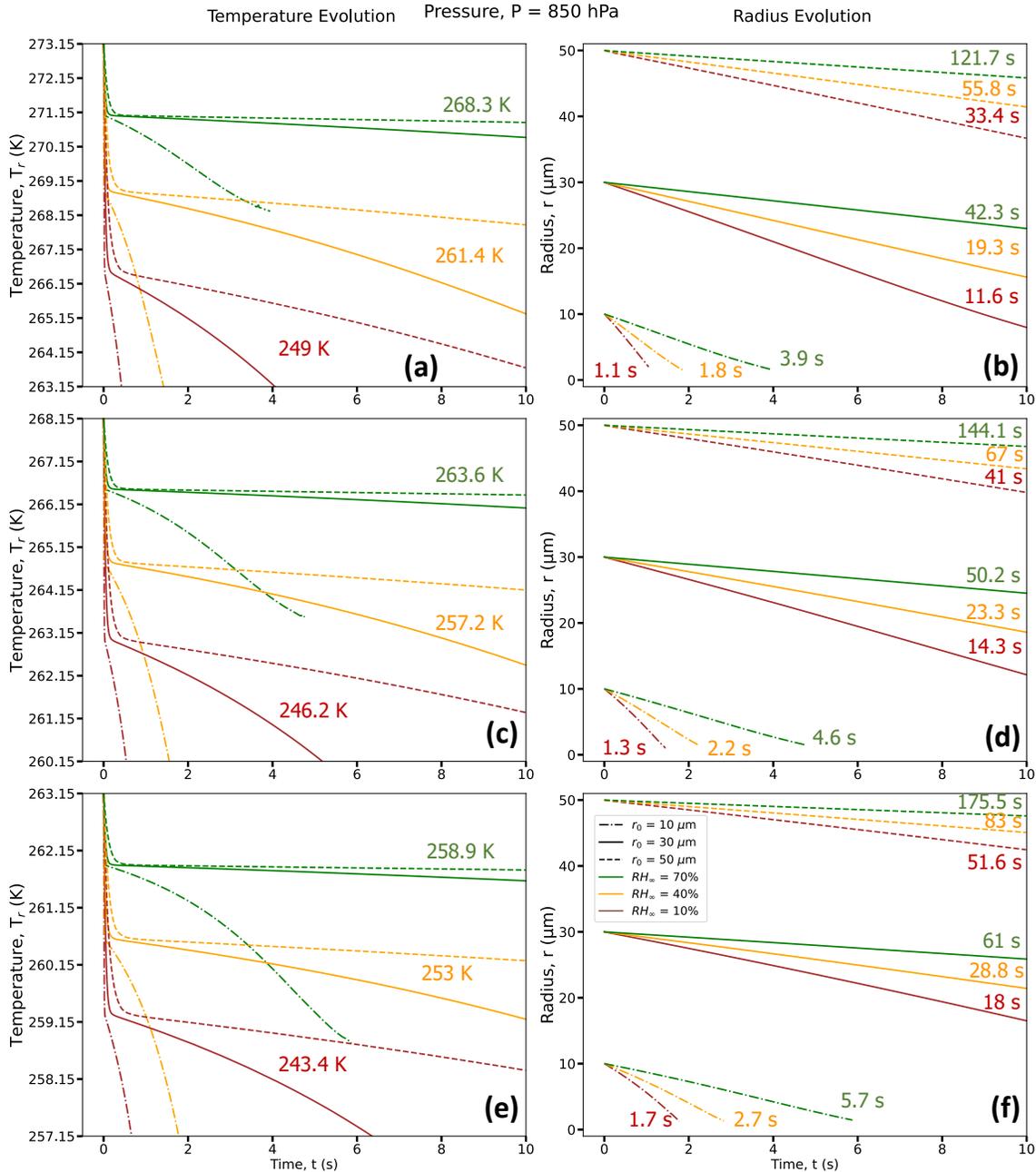
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459 As the droplet evaporates in the subsaturated domain, evaporative cooling occurs at the droplet surface, leading to  
460 heat transfer both from within the warmer droplet and the surrounding air to balance the cooling at the droplet surface.  
461 Since the droplet has no constant internal heat source, the internal thermal gradients dissipate quite fast (within  $0.3 \text{ s}$ )  
462 and the average droplet temperatures continue to decrease as the droplet evaporates. Due to heat exchange between  
463 the droplet surface and the ambient air in its vicinity, transient thermal gradients in the ambient air develop and lead  
464 to a decrease in the air temperature near the droplet. As the droplet shrinks in size along with cooling further, the  
465 colder envelope of air surrounding the droplet shrinks as well and the ambient air far from the droplet, at a constant  
466 temperature, acts as a heat source and supplies heat to the rest of the domain to attempt to equilibrate the air  
467 temperature. Comparing Fig. 5 (a) and (d), at the lower  $RH_{\infty}$ , the magnitude of evaporative cooling is much higher.  
468 For example, the average temperature of the  $50 \mu\text{m}$  droplet decreases by  $\sim 10 \text{ K}$  in  $9 \text{ s}$  when  $RH_{\infty} = 10\%$ , while the  
469 decrease is  $\sim 5 \text{ K}$  in  $120 \text{ s}$ , when  $RH_{\infty} = 70\%$ .



470  
471

472 **Figure 3: Droplet temperature evolution (left column) and radius evolution (right column) for three different  $RH_\infty$  ( $RH_\infty =$**   
 473  **$10\%$  (brown curves),  $40\%$  (orange curves) and  $70\%$  (green curves)), three different  $r_0$  ( $r_0 = 10 \mu\text{m}$  (dot-dashed lines),  $30$**   
 474  **$\mu\text{m}$  (solid lines) and  $50 \mu\text{m}$  (dashed lines)), with three different  $T_\infty = 273.15$  K ( $0^\circ\text{C}$ ) (a, b),  $268.15$  K ( $-5^\circ\text{C}$ ) (c, d) and  $263.15$**   
 475 **K ( $-10^\circ\text{C}$ ) (e, f), for  $P = 500$  hPa. For each  $RH_\infty$ , the average droplet temperature at the end of the lifetimes of the three**  
 476 **droplets with different  $r_0$  ( $T_L$ , in K) is given in (a,c,e) and the time taken to reach the end of its lifetime ( $t_L$ , in s) is given in**  
 477 **(b, d, f). Exact values of final temperature for each  $r_0$  are given in Table 1.**

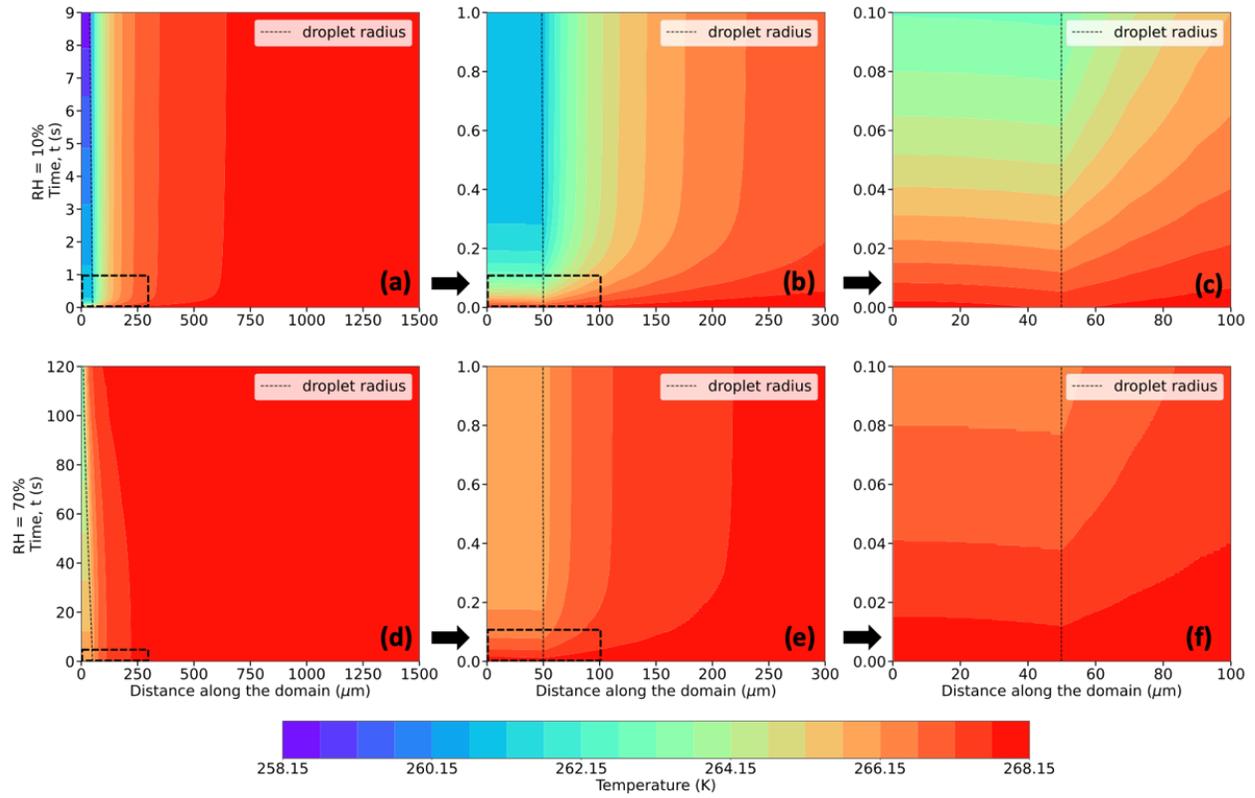


478

479 **Figure 4: Same as Fig. 3 but for  $P = 850$  hPa.**

480

481 In these simulations, the air in contact with the droplet surface is saturated with respect to water, i.e.,  $RH = 100\%$  (Fig.  
 482 6, a-f), consistent with assumptions of isolated, stationary evaporating droplets (Kinzer and Gunn, 1951; Srivastava  
 483 and Coen, 1992). As the water vapor from the evaporating droplet surface diffuses into the surrounding environment,  
 484 with an initial  $RH$  (same as  $RH_\infty$ ) of say 10%, vapor density gradients, similar to the thermal gradients, appear and  
 485 impact the immediate environment of the droplet. These spatiotemporally varying thermal and vapor density gradients  
 486 play an important role in affecting the droplet temperatures, evaporation rates, and in turn, droplet lifetimes.



487

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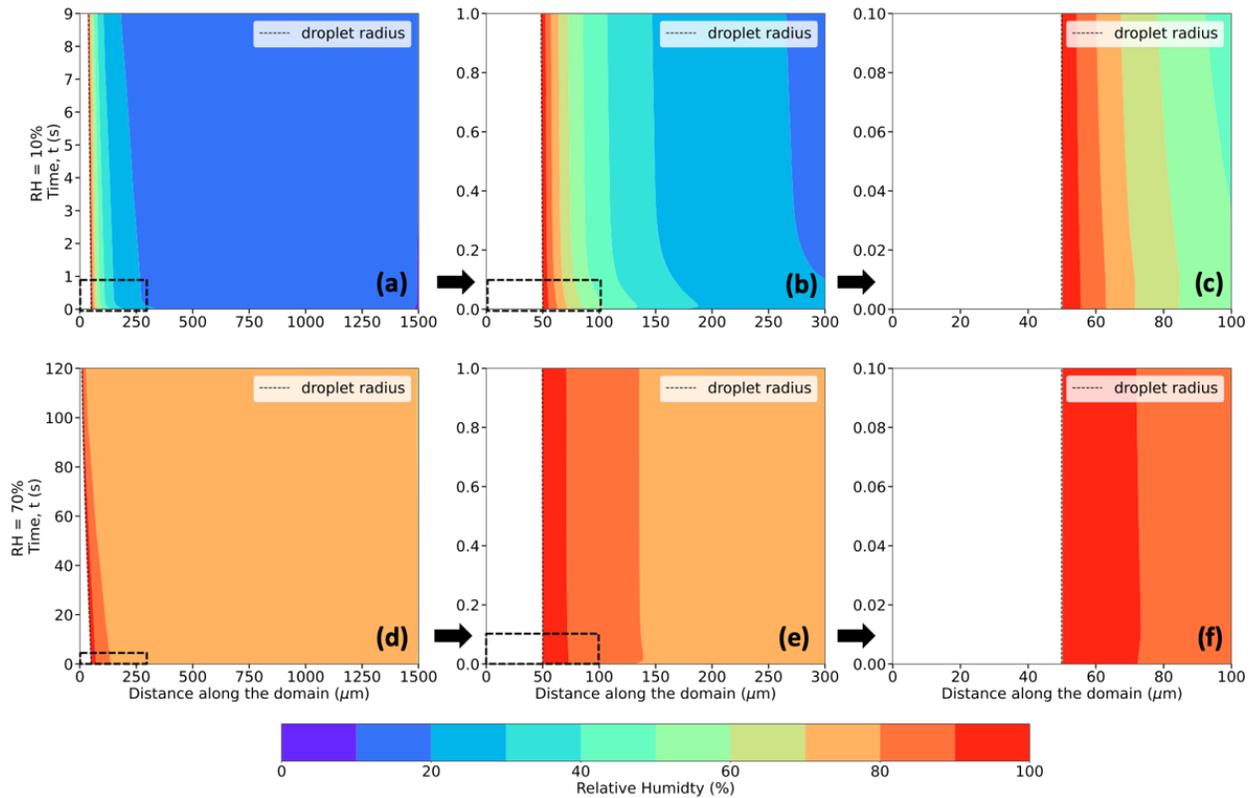
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492

**Figure 5: Evolution of temperature (in K, shaded contours), and droplet radius (in  $\mu\text{m}$ , dashed black trace) for a  $50 \mu\text{m}$  droplet, immersed in an environment with  $T_\infty = 268.15 \text{ K}$  ( $-5^\circ\text{C}$ ),  $P = 500 \text{ hPa}$ , and  $RH_\infty = 10\%$  (top row) and  $70\%$  (bottom rows). Bottom left corner of each plot refers to the center of the droplet at  $(r, z) = (0, 0)$ . Distance along the domain refers to the radial distance from the center of the droplet. Figures denoted as (b) and (e), and (c) and (f) present zoomed-in plot areas marked by the dashed boxes in (a) and (d), and (b) and (e), respectively.**

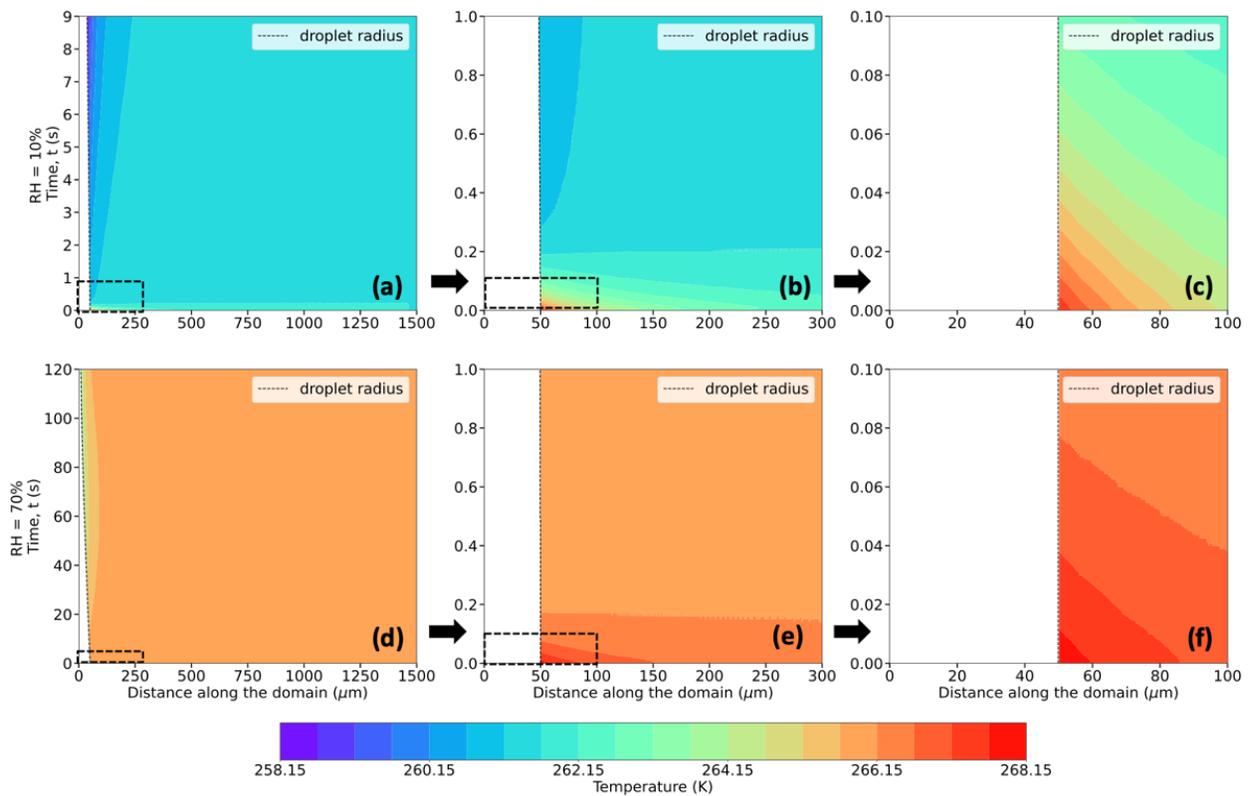


494

495 **Figure 6: Same as Figure 5, but for Relative Humidity (in %, shaded contours), instead of Temperature.**

496

497 Roy et al. (2023) has shown that an evaporating cloud droplet temperature can be well-approximated by the  
 498 thermodynamic wet-bulb temperature of the environment, especially at higher relative humidities and pressures, and  
 499 lower ambient temperatures. Following the iterative procedure used in Roy et al. (2023) to calculate the  
 500 thermodynamic wet-bulb temperature ( $T_{WB}$ ), Fig. 7 (a-f) depicts the evolution of  $T_{WB}$  of the surrounding environment.  
 501 Unlike previous studies (Srivastava and Coen, 1992; Roy et al., 2023), the ambient environment in this study is not  
 502 assumed to be spatiotemporally invariant. Hence, as the thermal and vapor density gradients evolve in the ambient air,  
 503 the  $T_{WB}$  of the environment evolves as well, depending on the temperature, relative humidity, and pressure, with the  
 504 droplet surface temperature the same as that of the  $T_{WB}$  of its immediate environment at all times. Of interest, the  
 505 droplet temperature decreases very quickly to  $T_i$  within  $< 0.5$  s (Figs. 3 and 4), which agrees very well with the initial  
 506  $T_{WB}$  of the surrounding environment and the constant value of the thermodynamic wet bulb temperature far from the  
 507 droplet ( $T_{WB\infty}$ ). For example, in Fig. 7 (a-c),  $T_\infty = 268.15$  K,  $P = 500$  hPa,  $RH_\infty = 10\%$ ,  $T_{WB\infty} = 261.64$  K, and in Fig. 7  
 508 (d-f), for  $RH_\infty = 70\%$ ,  $T_{WB\infty} = 266.13$  K. Fig. 7 shows the two phases of the evolution of  $T_{WB}$  of the immediate  
 509 environment for two  $RH_\infty$  environments – initially, there is a very fast decrease of the air temperature at the droplet  
 510 surface to  $T_{WB\infty}$  typically within  $< 0.3$  s, and then a more gradual decrease of  $T_{WB}$  at the droplet surface as the thermal  
 511 and vapor density gradients in the ambient air become relatively steadier and more established for a period of time,  
 512 and as their spheres of influence start shrinking as the droplet starts getting smaller in size.



513  
 514 **Figure 7: Same as Figure 5, but for thermodynamic wet-bulb temperature (in K, shaded contours).**

515  
 516 **4.3 Influence of initial droplet size and ambient environmental factors on the thermal evolution of the droplet**  
 517 **and its surrounding environment**

518  
 519 The overall results spanning the parameter space of the simulations are summarized in Tables 1-2 for the 54 numerical  
 520 experiments using various combinations of ambient conditions ( $RH_\infty$ ,  $T_\infty$ , and pressure,  $P$ , and  $r_0$ ) specified at a  
 521 distance far away from the droplet.

522  
 523 **4.3.1 Effect of Ambient Relative Humidity,  $RH_\infty$**

524  
 525 The decrease in droplet temperature is larger when the  $RH_\infty$  is lower due to higher evaporation rates and stronger  
 526 evaporative cooling under drier conditions. For instance, as shown in Table 1 and Fig. 8 (a, b, c), 30 μm droplets reach  
 527 ~ 247.3 K (a decrease of 25.8 K from the initial temperature of 273.15 K) for  $RH_\infty = 10\%$ , ~ 261.1 K (a decrease of  
 528 12.1 K) for  $RH_\infty = 40\%$  and ~ 268.2 K (a decrease of ~ 5 K) for  $RH_\infty = 70\%$ . The droplet lifetimes vary depending on  
 529  $RH_\infty$ , with lifetimes increasing with an increase in humidity. For example, the droplet lifetimes for the 30 μm droplet  
 530 are ~ 9.5 s, 16.7 s, and 37.3 s for environments with  $RH_\infty = 10\%$ , 40% and 70%, respectively (Table 2). The decrease  
 531 in droplet temperature and increase in droplet lifetime show similar dependence with increasing  $RH_\infty$  for 10 and 50  
 532 μm droplets as well.

### 533 4.3.2 Effect of Initial Droplet Size, $r_0$

534

535 From Figs. 8-10, for a given initial environmental condition ( $RH_\infty$  and  $T_\infty$ ), the droplet temperatures at the end of their  
536 lifetimes are independent of the initial droplet sizes. For example, from Table 1 and Fig. 9 (a-i) at  $P = 500$  hPa, 10,  
537 30 and 50  $\mu\text{m}$  droplets reach  $\sim 244$  K (a decrease of  $\sim 24$  K from the initial temperature of 268.15 K) for  $RH_\infty = 10\%$ ,  
538  $\sim 256.8$  K for  $RH_\infty = 40\%$ , and  $\sim 263.5$  K for  $RH_\infty = 70\%$ . On the other hand, the droplet lifetime strongly depends on  
539 the initial droplet size, as the larger droplets take more time to evaporate as compared to the smaller ones. For  
540 environments with  $RH_\infty = 10\%$ , 40% and 70%, the droplet lifetimes for the 10  $\mu\text{m}$  droplet are  $\sim 1.1$  s, 1.8 s, and 3.9 s,  
541 while for the 30  $\mu\text{m}$  droplet are  $\sim 11.4$  s, 19.4 s, and 42.8 s, and for the 50  $\mu\text{m}$  droplet are  $\sim 32.8$  s, 55.8 s, and 123.1  
542 s, respectively (Table 2). For a higher pressure of  $P = 850$  hPa (Table 1), at the same  $T_\infty$ , irrespective of  $r_0$ , the decrease  
543 in droplet temperatures is slightly smaller as compared to  $P = 500$  hPa, with values of 22 K, 11 K, and 4.6 K. The  
544 radial dependence of the thermal gradients in the ambient air also depends on the initial droplet size, decreasing with  
545 a decrease in  $r_0$ .

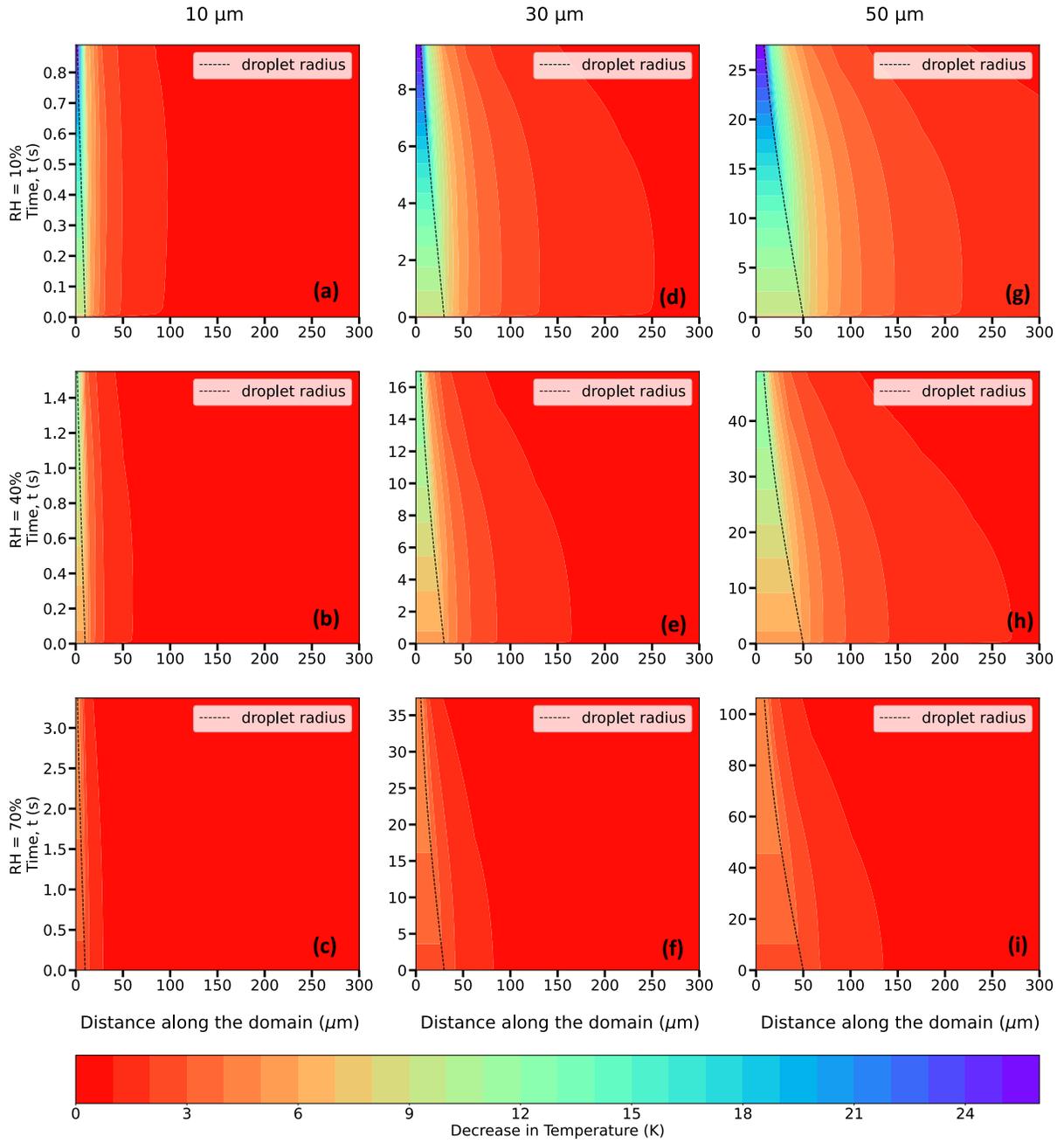
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### 547 4.3.3 Effect of Ambient Temperature, $T_\infty$

548

549 To determine the effect of a lower ambient temperature on droplet temperatures and lifetimes, Figs. 9 and 10  
550 demonstrate similar plots as shown in Fig. 8, but for  $T_\infty = 268.15$  K ( $-5^\circ\text{C}$ ) and 263.15 K ( $-10^\circ\text{C}$ ), respectively. The  
551 decrease in droplet temperatures and increase in droplet lifetimes depict similar relationships with  $RH_\infty$  and  $r_0$ .  
552 Droplets, irrespective of their initial size, cool to a lower temperature depending on the ambient  $RH_\infty$ , with the  
553 magnitude of the cooling being inversely proportional to the subsaturation of the ambient environment. For instance,  
554 for 10, 30 and 50  $\mu\text{m}$  droplets, from an initial temperature of 268.15 K, the droplet temperatures approximately  
555 decrease by 24 K, 11.4 K, and 4.7 K, for environments with  $RH_\infty = 10\%$ , 40%, and 70%, respectively (Table 1). The  
556 droplet lifetimes for the 10  $\mu\text{m}$  droplet are  $\sim 1.1$  s, 1.8 s, and 3.9 s, while for the 30  $\mu\text{m}$  droplet are  $\sim 11.4$  s, 19.4 s,  
557 and 42.8 s, and for the 50  $\mu\text{m}$  droplet are  $\sim 32.8$  s, 55.8 s, and 123.1 s, for  $RH_\infty = 10\%$ , 40% and 70%, respectively  
558 (Table 2). Comparing these values with those of  $T_\infty = 273.15$  K ( $0^\circ\text{C}$ ), it can be noted that a lower ambient temperature  
559 leads to a smaller decrease in droplet temperatures and a slight increase in droplet lifetimes in a spatiotemporally  
560 evolving environment, for the same  $RH_\infty$ ,  $r_0$  and  $P$ . Fig. 10 and Table 1 depict that for  $T_\infty = 263.15$  K ( $-10^\circ\text{C}$ ), the  
561 reduction in droplet temperatures is slightly smaller,  $\sim 21.8$  K, 10.7 K, and 4.5 K for environments with  $RH_\infty = 10\%$ ,  
562 40%, and 70%, respectively, and droplet lifetimes are longer relative to the higher ambient temperatures of 273.15 K  
563 and 268.15 K (Table 2). This is because at a lower ambient temperature, the vapor diffusivity into the ambient air is  
564 lower, leading to a weaker evaporation rate with slightly reduced cooling, and extended droplet lifetime, relative to  
565 those in an environment with a higher ambient temperature.

566



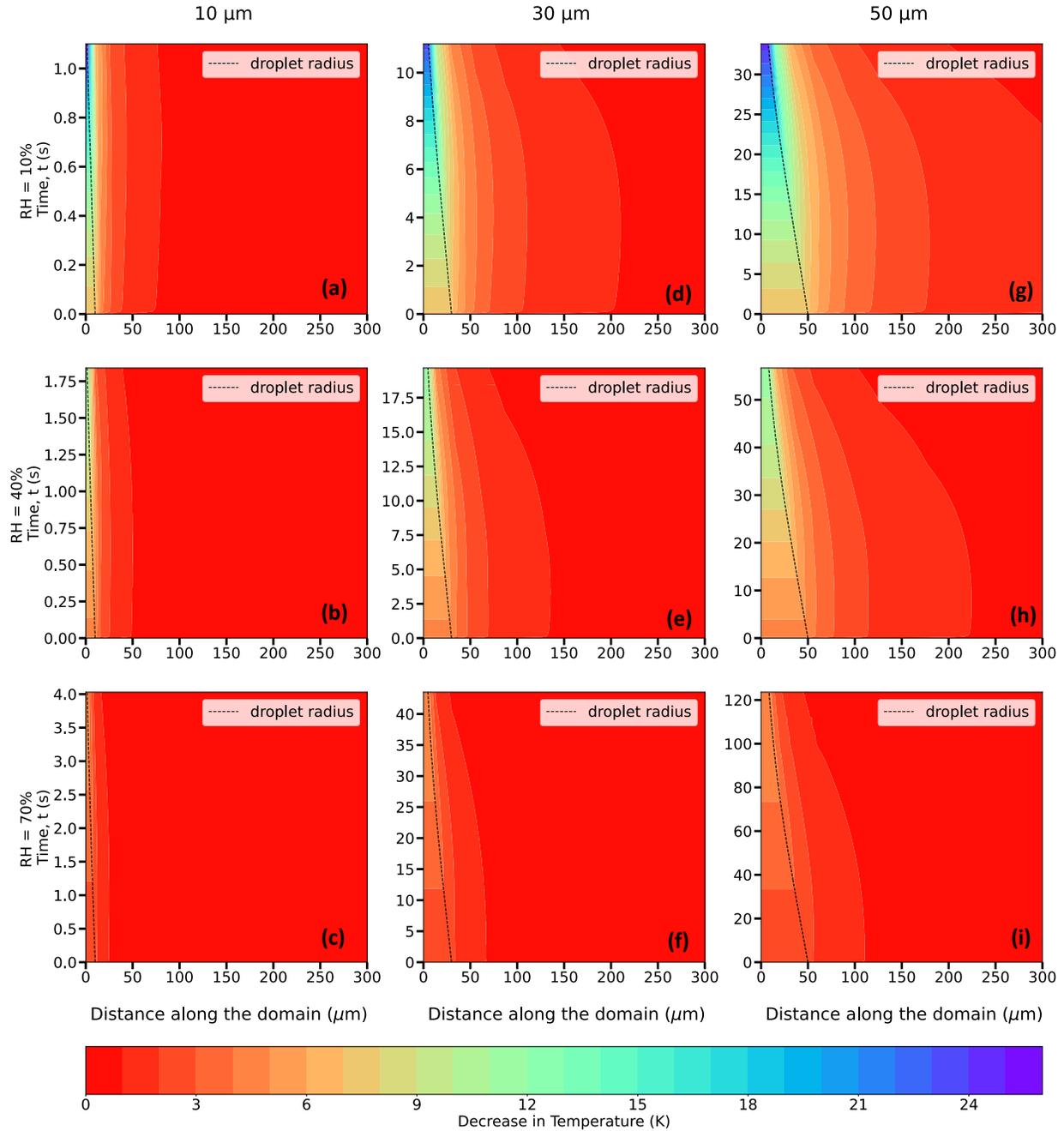
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**Figure 8: Evolution of the decrease in temperature (in K, shaded contours) from the initial temperature of the domain = 273.15 K (0°C), and of the droplet radius (in μm, dashed black trace) for 10 (a,b,c), 30 (d,e,f), and 50 (g,h,i) μm droplets, immersed in an environment with  $T_{\infty} = 273.15$  K (0°C),  $P = 500$  hPa, and  $RH_{\infty} = 10\%$ , 40% and 70%.**

$T_{\infty}$ (K)	$r_0$ ( $\mu\text{m}$ )	$RH_{\infty}$ (%)	$P = 500 \text{ hPa}$					$P = 850 \text{ hPa}$				
			$T_{WB\infty}$ (K)	$T_{RRD}$ (K)	$T_i$ (K)	$T_L$ (K)	$T_{\infty} - T_L$ (K)	$T_{WB\infty}$ (K)	$T_{RRD}$ (K)	$T_i$ (K)	$T_L$ (K)	$T_{\infty} - T_L$ (K)
273.15 (0°C)	10	10	264.94	264.06	264.15	247.15	26	267.20	266.49	266.35	249.03	24.12
		40	267.95	267.41	267.35	261.09	12.06	269.30	268.85	268.95	261.40	11.75
		70	270.67	270.43	270.35	268.21	4.94	271.28	271.07	271.10	268.29	4.86
	30	10	264.94	264.06	264.15	247.33	25.82	267.20	266.49	266.37	249.01	24.14
		40	267.95	267.41	267.35	261.08	12.07	269.30	268.85	268.95	261.43	11.72
		70	270.67	270.43	270.45	268.20	4.95	271.28	271.07	271.15	268.26	4.89
	50	10	264.94	264.06	264.15	247.31	25.84	267.20	266.49	266.37	249.04	24.11
		40	267.95	267.41	267.36	261.09	12.06	269.30	268.85	268.95	261.45	11.7
		70	270.67	270.43	270.45	268.20	4.95	271.28	271.07	271.15	268.29	4.86
268.15 (-5°C)	10	10	261.64	260.90	260.98	244.12	24.03	263.57	263.01	263.15	246.32	21.83
		40	263.96	263.50	263.48	256.77	11.38	265.16	264.79	264.82	257.17	10.98
		70	266.13	265.91	265.9	263.47	4.68	266.68	266.51	266.65	263.57	4.58
	30	10	261.64	260.90	260.85	244.31	23.84	263.57	263.01	263.06	246.18	21.97
		40	263.96	263.50	263.46	256.76	11.39	265.16	264.79	264.69	257.18	10.97
		70	266.13	265.91	265.92	263.47	4.68	266.68	266.51	266.56	263.58	4.57
	50	10	261.64	260.90	260.85	244.29	23.86	263.57	263.01	263.06	246.21	21.94
		40	263.96	263.50	263.47	256.76	11.39	265.16	264.79	264.72	257.16	10.99
		70	266.13	265.91	265.92	263.46	4.69	266.68	266.51	266.56	263.56	4.59
263.15 (-10°C)	10	10	258.14	257.55	257.53	241.38	21.77	259.73	259.28	259.28	243.49	19.66
		40	259.89	259.51	259.65	252.46	10.69	260.90	260.60	260.65	252.97	10.18
		70	261.56	261.38	261.4	258.73	4.42	262.04	261.90	261.90	258.88	4.27
	30	10	258.14	257.55	257.62	241.36	21.79	259.73	259.28	259.28	243.27	19.88
		40	259.89	259.51	259.56	252.47	10.68	260.90	260.60	260.54	252.99	10.16
		70	261.56	261.38	261.39	258.73	4.42	262.04	261.90	261.91	258.88	4.27
	50	10	258.14	257.55	257.62	241.37	21.78	259.73	259.28	259.28	243.48	19.67
		40	259.89	259.51	259.56	252.47	10.68	260.90	260.60	260.56	252.99	10.16
		70	261.56	261.38	261.39	258.73	4.42	262.04	261.90	261.91	258.87	4.28

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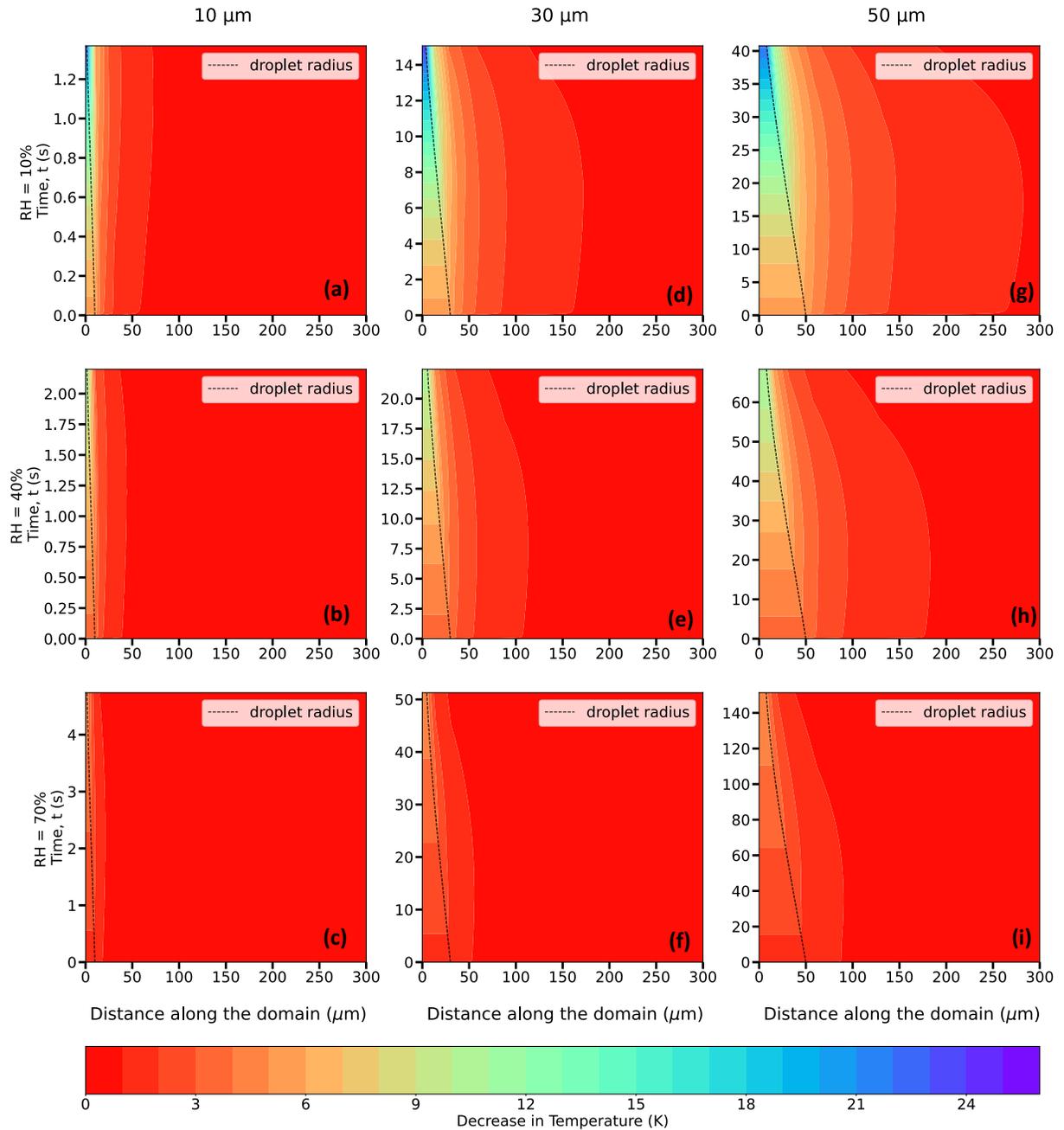
**Table 1. Comparison between thermodynamic wet bulb temperatures in the environment far away from the droplet ( $T_{WB\infty}$ ), simulated droplet steady-state temperatures from Roy et al., (2023) ( $T_{RRD}$ ), slope transition point temperatures ( $T_i$ ), and droplet temperatures at the end of their lifetimes from this study ( $T_L$ ), in K, for initial droplet radii,  $r_0 = 10, 30$  and  $50 \mu\text{m}$ , relative humidities,  $RH_\infty = 10, 40, 70\%$ , and pressures,  $P = 500$  and  $850$  hPa, and ambient temperature,  $T_\infty = 273.15$  K ( $0^\circ\text{C}$ ),  $268.15$  K ( $-5^\circ\text{C}$ ) and  $263.15$  K ( $-10^\circ\text{C}$ ).**



585  
586

**Figure 9: Same as Fig. 8 but for  $T_\infty = 268.15$  K ( $-5^\circ\text{C}$ ).**

587



588  
589 **Figure 10:** Same as Fig. 8 but for  $T_\infty = 263.15$  K ( $-10^\circ\text{C}$ ).

590  
591 **4.3.4 Effect of Ambient Pressure,  $P$**

592 The spatiotemporal evolution of the temperature and droplet radius of an evaporating droplet were also investigated  
593 for a higher ambient pressure,  $P = 850$  hPa. For a higher pressure, the corresponding decreases in droplet temperatures  
594 are smaller and droplet lifetimes are longer. Under the same environmental conditions but with an increase in ambient  
595 pressure, water vapor diffusivity decreases, leading to a decreased evaporation rate, reduced cooling, and extended  
596  
597

$T_{\infty}$ (K)	$r_0$ ( $\mu\text{m}$ )	$RH_{\infty}$ (%)	$P = 500 \text{ hPa}$				$P = 850 \text{ hPa}$			
			$t_{LC}$ (s)	$t_{RRD}$ (s)	$t_L$ (s)	$\frac{t_L - t_{LC}}{t_{LC}} \times 100\%$	$t_{LC}$ (s)	$t_{RRD}$ (s)	$t_L$ (s)	$\frac{t_L - t_{LC}}{t_{LC}} \times 100\%$
273.15 (0°C)	10	10	0.26	0.56	0.87	234.62	0.44	0.77	1.11	152.27
		40	0.39	0.89	1.51	287.18	0.66	1.18	1.79	171.21
		70	0.78	1.86	3.36	430.77	1.33	2.43	3.87	190.98
	30	10	2.34	5.02	9.54	307.69	3.98	6.84	11.63	192.21
		40	3.51	7.94	16.68	375.21	5.97	10.59	19.33	223.79
		70	7.03	16.73	37.26	430.01	11.95	21.83	42.30	253.97
	50	10	6.51	13.95	27.43	321.35	11.06	19.06	33.35	201.54
		40	9.76	22.08	48.04	392.21	16.59	29.45	55.78	236.23
		70	19.52	46.46	107.45	450.46	33.18	60.64	121.70	266.79
268.15 (-5°C)	10	10	0.38	0.72	1.05	176.32	0.65	1.01	1.32	103.08
		40	0.58	1.12	1.77	205.17	0.98	1.54	2.15	119.39
		70	1.15	2.31	3.91	240	1.96	3.14	4.60	134.69
	30	10	3.45	6.42	11.40	230.43	5.87	9.03	14.27	143.10
		40	5.18	10.01	19.35	273.55	8.81	13.83	23.32	164.70
		70	10.36	20.81	42.79	313.03	17.61	28.25	50.15	184.78
	50	10	9.59	17.88	32.76	241.61	16.31	25.15	40.99	151.32
		40	14.39	27.86	55.76	287.49	24.46	38.48	67.02	173.99
		70	28.78	57.80	123.10	327.73	48.92	78.48	144.07	194.50
263.15 (-10°C)	10	10	0.57	0.95	1.29	126.34	0.98	1.37	1.68	71.43
		40	0.86	1.45	2.13	147.67	1.47	2.08	2.68	82.31
		70	1.72	2.98	4.60	167.44	2.93	4.21	5.66	93.17
	30	10	5.17	8.47	13.95	169.83	8.80	12.28	17.99	104.43
		40	7.76	13.05	23.08	197.42	13.19	18.67	28.83	118.57
		70	15.52	26.79	50.12	222.94	26.39	37.85	61.04	131.29
	50	10	14.37	23.59	40.11	179.12	24.43	34.19	51.59	111.17
		40	21.56	36.30	66.42	208.07	36.65	51.93	82.53	125.18
		70	43.12	74.43	144.33	234.72	73.30	105.16	175.50	139.43

598

599

600 **Table 2: Comparison between different timescales (in sec) in this and other studies, all for the cut off radii used in this**  
601 **study. These include droplet lifetimes using the Maxwellian diffusion-limited evaporation approach ( $t_{LC}$ ), the bulk droplet**  
602 **approach in Roy et al., (2023) ( $t_{RRD}$ ), and as calculated from this study ( $t_L$ ), for initial droplet radii ( $r_0 = 10, 30$  and  $50 \mu\text{m}$ ),**  
603 **relative humidities ( $RH_\infty = 10, 40, 70\%$ ), and pressures ( $P = 500$  and  $850$  hPa), and ambient temperature,  $T_\infty = 273.15$  K**  
604 **( $0^\circ\text{C}$ ),  $268.15$  K ( $-5^\circ\text{C}$ ) and  $263.15$  K ( $-10^\circ\text{C}$ ).**  
605

606 droplet lifetimes. For example, for an environment with  $T_\infty = 273.15$  K ( $0^\circ\text{C}$ ),  $P = 850$  hPa,  $10, 30$  and  $50 \mu\text{m}$  droplets  
607 reach  $249.0$  K,  $261.4$  K, and  $268.3$  K for  $RH_\infty = 10\%$ ,  $40\%$  and  $70\%$ , respectively, which are slightly higher as  
608 compared to the corresponding droplet temperatures ( $247.3$  K,  $261.1$  K, and  $268.2$  K) for  $P = 500$  hPa (Table 1). For  
609 higher ambient pressures, droplet lifetimes are also increased due to reduced evaporation rate, with  $50 \mu\text{m}$  droplets  
610 now surviving for  $33.4$  s,  $55.8$  s, and  $121.7$  s at  $P = 850$  hPa, instead of  $27.4$  s,  $48.0$  s,  $107.5$  s for  $P = 500$  hPa for  $RH_\infty$   
611  $= 10\%$ ,  $40\%$  and  $70\%$ , respectively (Table 2). Similar trends can also be observed for lower ambient temperatures,  
612  $268.15$  K and  $263.15$  K, as shown in Table 2.

613

## 614 **5 Discussion**

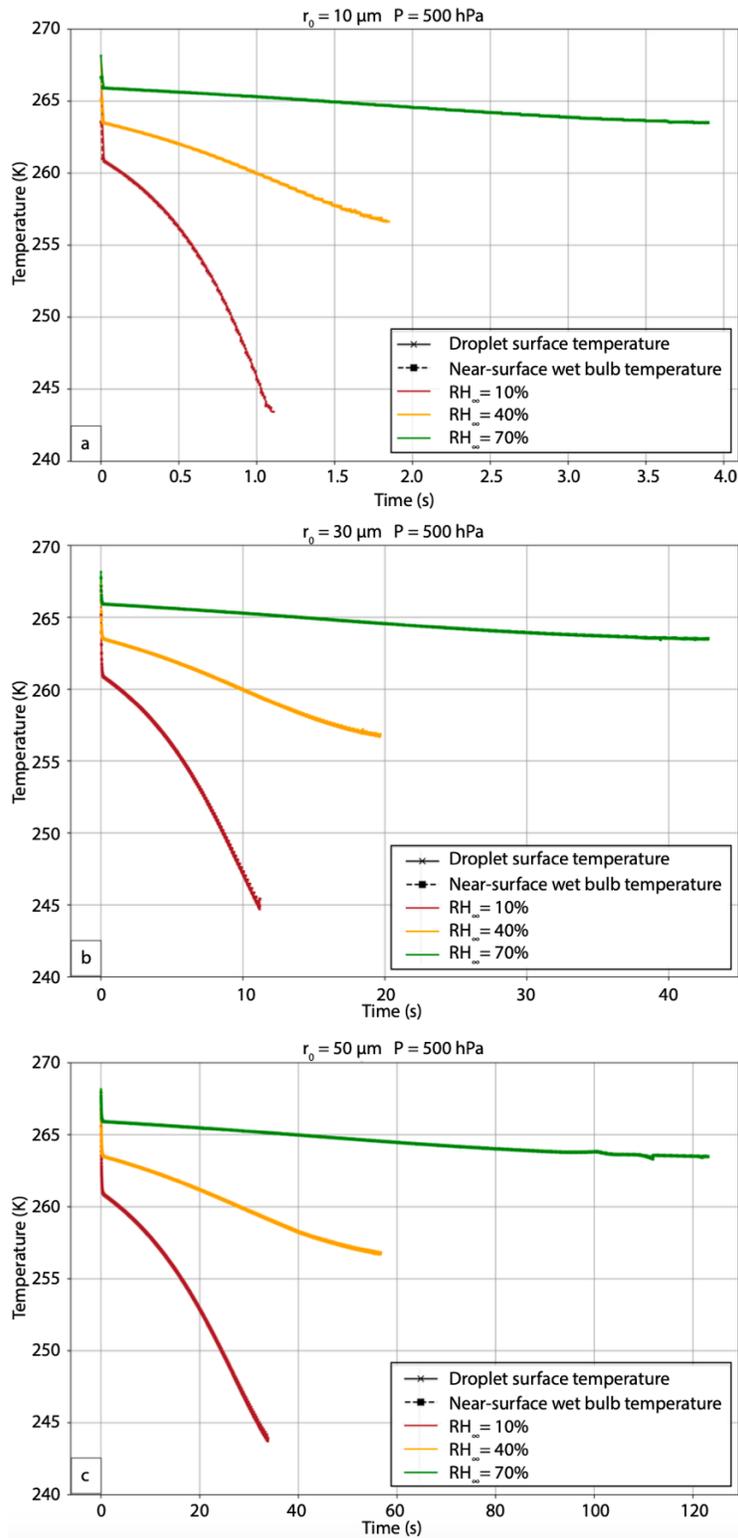
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### 616 **5.1 Droplet Temperature Sensitivities and Relationship to Thermodynamic Wet-bulb Temperature**

617

618 In these experiments, the droplet temperature initially rapidly decreases to the thermodynamic wet-bulb temperature  
619 of the far environment. The novel finding from this study is that the droplet temperature continues to decrease beyond  
620 the thermodynamic wet-bulb temperature of the far environment because of the non-equilibrium condition of the  
621 thermal and vapor fields during the evaporation process (Fig. 11). The droplet temperature continues to conform to  
622 the wet-bulb temperature directly adjacent to the droplet surface, which is lower than the wet-bulb temperature of the  
623 far environment. Note that the dependence on  $T_\infty$  and  $P$  is much smaller than that on  $RH_\infty$ . The strong dependence on  
624  $RH_\infty$  compared to temperature results from the initial conditions. The droplet temperature initially is in thermal  
625 equilibrium with its environment (the droplet has the same temperature as that of the far environment), but the vapor  
626 field is far from equilibrium, especially for low relative humidity environments. As a result, the vapor diffusion rate  
627 (which depends on the vapor density gradient) far exceeds the thermal diffusion rate (which depends on the  
628 temperature gradient). Because the cloud droplets are small, and the relative humidity gradients are large, the droplets  
629 never come to an equilibrium state before evaporating completely into the subsaturated air. The water vapor flux into  
630 the larger subsaturated environment maintains a vapor density near the droplet surface that approaches but never  
631 reaches saturation. As a result, the wet-bulb temperature near the droplet surface continues to fall but at a slower rate  
632 that depends on  $RH_\infty$  (Fig. 11). The pressure affects both the moisture and temperature diffusion fluxes, so these scale  
633 with each other, resulting in pressure not having a strong effect compared to that of the moisture gradient.

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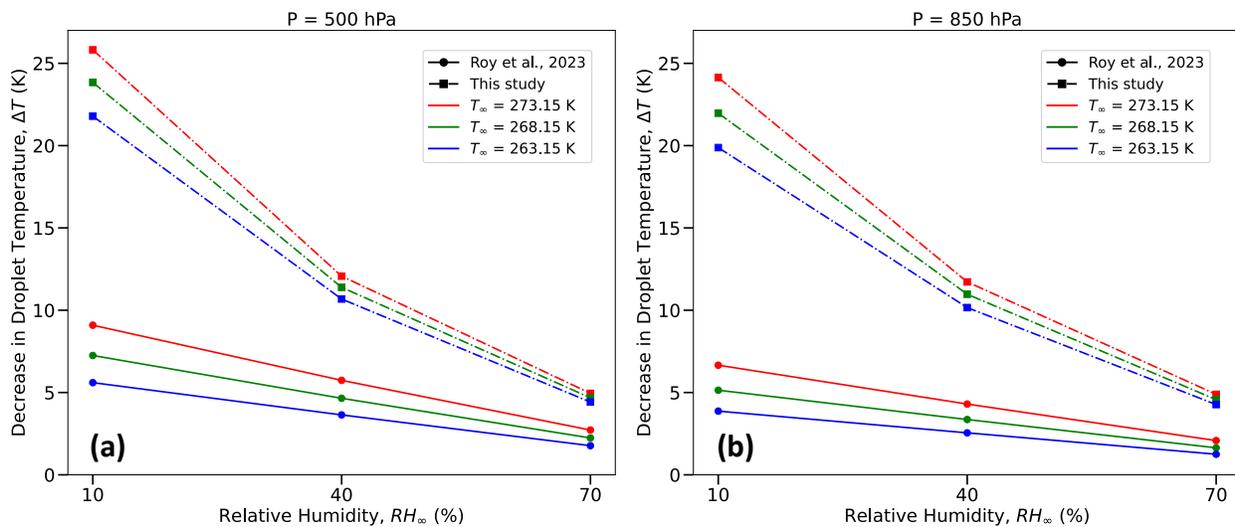
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Figure 11: Evolution of droplet surface temperature (in K, solid lines with cross symbols), and near-surface thermodynamic wet-bulb temperature (in K, dashed lines with square symbols) for (a) 10, (b) 30 and (c) 50  $\mu\text{m}$  droplet, immersed in an environment with  $T_\infty = 268.15$  K ( $-5^\circ\text{C}$ ),  $P = 500$  hPa, and three different  $RH_\infty$ . The lines representing droplet surface temperature and near-surface thermodynamic wet-bulb temperature essentially overlap.

## 641 5.2 Droplet Temperature and Lifetime Comparison with Previous Studies

642

643 As noted in the introduction, not many studies in the cloud microphysics literature have taken a close look at the  
 644 explicit numerical estimation of supercooled, evaporating cloud droplet temperatures for a wide range of  
 645 environmental conditions. Previously, a study by Srivastava and Coen (1992) investigated the evaporation of isolated,  
 646 stationary droplets by iteratively solving the steady-state solutions, using saturation vapor pressure relations from  
 647 Wexler (1976) to calculate saturation vapor density, and assumed the heat storage terms in the droplet heat budget to  
 648 be negligible. Roy et al., (2023), solving for time-dependent heat and mass transfer between single, stationary cloud  
 649 droplets evaporating in infinitely large, prescribed ambient environments, demonstrated that the temperatures of the  
 650 cloud droplets reach steady-state quite quickly ( $< 0.3$  s). Their steady-state droplet temperatures agreed well with those  
 651 of Srivastava and Coen (1992) and could be approximated by the thermodynamic wet-bulb temperature of the ambient  
 652 environment. The current study advances the idealized framework of droplet evaporation as described in Roy et al.,  
 653 (2023) by including the impact of internal heat gradients within the droplet and resolving the spatiotemporally  
 654 evolving thermal and vapor density gradients between the droplet and its immediate environment to estimate the  
 655 evaporating droplet temperature and lifetime with higher accuracy.

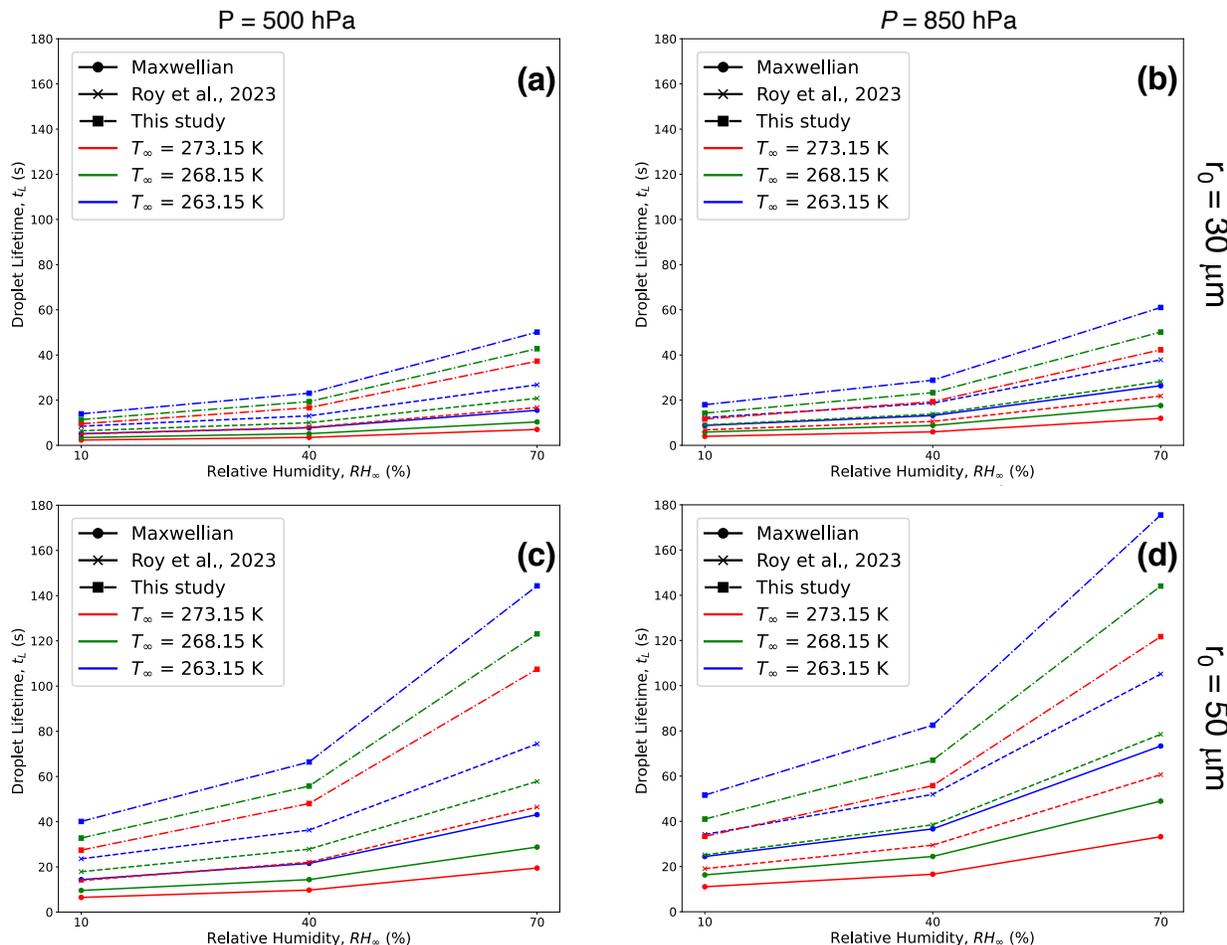


656

657 **Figure 12: Comparison between the decrease in droplet temperatures (in K) from an initial temperature the same as  $T_\infty$ ,**  
 658 **calculated using the bulk droplet model from Roy et al., (2023) (dashed lines), and this study (dashed-dotted lines), for**  
 659 **initial droplet radii,  $r_0 = 10, 30$  or  $50$   $\mu\text{m}$ , relative humidities ( $RH_\infty = 10, 40, 70$  %), and pressures,  $P = 500$  hPa (left column),**  
 660 **and  $850$  hPa (right column), and  $T_\infty = 273.15$  K ( $0^\circ\text{C}$ , red),  $268.15$  K ( $-5^\circ\text{C}$ , green) and  $263.15$  K ( $-10^\circ\text{C}$ , blue).**

661 Table 1 provides a comparison between thermodynamic wet bulb temperatures of the initial environment ( $T_{WB\infty}$ ),  
 662 simulated droplet steady-state temperatures from Roy et al. (2023) ( $T_{RRD}$ ), and droplet temperatures at the end of their  
 663 lifetimes from this study ( $T_L$ ), in K for several environments. Interestingly, the temperatures at the slope transition  
 664 point,  $T_i$ , as defined in Sec. 3e, are in excellent agreement with  $T_{WB\infty}$  and  $T_{RRD}$ . In the current study, the droplet  
 665 temperature continues to decrease almost steadily as the immediate environment in the vicinity of the droplet cools,  
 666 finally reaching  $T_L$ , unlike the evaporating droplet achieving a steady-state temperature in a prescribed ambient  
 667 environment far away from the droplet in Roy et al., (2023). The evaporating droplet temperature essentially keeps

668 adjusting to the thermodynamic wet-bulb temperature of its immediate changing environment. Therefore, the more  
 669 realistic simulations of evaporating cloud droplets that include the effect of spatiotemporally varying ambient air  
 670 thermal and vapor density gradients, as shown in this study, reveal that droplets can potentially achieve even lower  
 671 temperatures than previously known or estimated from past studies (Srivastava and Coen, 1992; Roy et al., 2023). The  
 672 decrease in droplet temperatures from their initial temperatures can be much larger, especially for drier environments,  
 673 as much as 25.8 K for  $RH_\infty = 10\%$  and 5.0 K for  $RH_\infty = 70\%$ , for an environment with  $P = 500$  hPa, and  $T_\infty = 273.15$   
 674 K (Table 1 and Fig. 12a). As shown in Fig. 12, the magnitude of reduction in droplet temperatures decreases with  
 675 higher ambient  $RH_\infty$  and  $P$ , and lower  $T_\infty$ , similar to previous studies (Srivastava and Coen, 1992; Roy et al., 2023).



676  
 677 **Figure 13: Comparison between droplet lifetimes (as defined in this study) calculated using the Maxwellian diffusion-limited**  
 678 **evaporation approach (solid lines), bulk droplet model from Roy et al., (2023) (dashed lines), and this study (dashed-dotted**  
 679 **lines), for initial droplet radii,  $r_0 = 30 \mu\text{m}$  (upper panel), and  $50 \mu\text{m}$  (lower panel), relative humidities ( $RH_\infty = 10, 40, 70\%$ ),**  
 680 **and pressures,  $P = 500$  hPa (left column), and  $850$  hPa (right column), and ambient temperature,  $T_\infty = 273.15$  K ( $0^\circ\text{C}$ , red),**  
 681  **$268.15$  K ( $-5^\circ\text{C}$ , green) and  $263.15$  K ( $-10^\circ\text{C}$ , blue).  $10 \mu\text{m}$  droplets (not shown here) have much smaller lifetimes compared**  
 682 **to  $30$  and  $50 \mu\text{m}$  droplets.**

683 Table 2 and Fig. 13 provide comparisons between  $10, 30$  and  $50 \mu\text{m}$  droplet lifetimes (as defined earlier in Sec. 3a)  
 684 using the Maxwellian pure-diffusion-limited evaporation approach ( $t_{LC}$ ), which ignores evaporative cooling at the  
 685 droplet surface (Maxwell, 1890; Eq 13-10 of Pruppacher and Klett, 1997), the “bulk” droplet approach as described  
 686 in Roy et al., (2023) ( $t_{RRD}$ ), which ignores internal droplet heat transfer and spatiotemporally varying thermal and

687 moisture gradients in the ambient air, and results from this study ( $t_L$ ). The magnitude of  $t_L$  is greater than the  
688 corresponding values of  $t_{LC}$  and  $t_{RRD}$ . This is because the droplet temperatures in this study never reach steady-state,  
689 and are much lower than the corresponding droplet temperatures from the diffusion-limited approach ( $\sim T_\infty$ ), and Roy  
690 et al., (2023) ( $\sim T_{RRD}$ ). The greater decrease in evaporating droplet temperature leads to a greater reduction in saturation  
691 vapor pressure at the droplet surface. This results in a slower droplet evaporation rate, therefore increasing the droplet  
692 lifetime. As shown in Fig. 13, the increase in droplet lifetime depends on the environmental subsaturation, ambient  
693 temperatures, and pressures, with a greater increase for more humid, higher pressure, and lower ambient temperature  
694 environments. The increase in droplet lifetimes can potentially enhance ice nucleation by increasing the chances of  
695 activation of ice nucleating particles (INPs) within the supercooled cloud droplets (see Sect. 5.3).

696

### 697 **5.3 Implications for ice nucleation**

698

699 Ice nucleation rates are influenced by temperature (Wright and Petters, 2013; Kanji et al., 2017) and time (Vali, 1994).  
700 There are two theories in ice nucleation modeling: the time-independent "singular hypothesis," which suggests  
701 instantaneous ice formation, and the time-dependent "stochastic hypothesis," which proposes that ice clusters in  
702 embryos form and vanish continually, with a frequency that depends on temperature. Supercooled cloud droplet  
703 temperatures and their lifetimes are potential contributing factors for the enhancement of ice formation within  
704 evaporating regions of clouds such as cloud-tops and edges. As discussed in Roy et al., (2023), evaporative cooling  
705 of supercooled cloud droplets in subsaturated environments can enhance ice nucleation near cloud boundaries in two  
706 ways: by instantly increasing ice-nucleating particle activation due to lower droplet temperatures (consistent with the  
707 singular hypothesis) and/or by extending supercooled droplet lifetimes, allowing more time for nucleation events  
708 (consistent with the stochastic hypothesis). Based on limited laboratory investigations available on time dependency  
709 of heterogeneous ice nucleation, conducted between temperatures -14 and -30 °C, varying fractions of the droplets  
710 were reported to freeze within a range of 1 s to 500 s (Welti et al., 2012; Broadley et al., 2012; Murray et al., 2012;  
711 Jakobsson et al., 2022).

712

713 Droplet freezing events can potentially occur within the time frame when the evaporating cloud droplets reach lower  
714 temperatures due to evaporative cooling before they completely dissipate into the subsaturated air. This can be seen  
715 by comparing the values in Table 2 and Fig. 13 with reported droplet freezing timescales available from experimental  
716 studies. Droplet lifetimes as estimated from both approaches ( $t_{RRD}$  and  $t_L$ ), which include droplet evaporative cooling,  
717 are longer as compared to the Maxwellian diffusion-limited evaporation approach ( $t_{LC}$ ), allowing more time for  
718 potential occurrence of an ice nucleation event. For temperatures between -5 °C and -10 °C, for the three different  
719 subsaturated environments ( $RH_\infty = 10, 40, \text{ and } 70\%$ ) examined in this analysis,  $t_{RRD}$  typically ranged from 0.7 - 4.2 s  
720 for 10  $\mu\text{m}$ , 6-38 s for 30  $\mu\text{m}$  and 18-105 s for 50  $\mu\text{m}$  initial radius of droplets, respectively. For similar environments,  
721  $t_L > t_{RRD} > t_{LC}$ , with  $t_L$  typically ranging from 1.1-5.7 s for 10  $\mu\text{m}$ , 11-61 s for 30  $\mu\text{m}$  and 33-176 s for 50  $\mu\text{m}$  initial  
722 radii droplets, respectively. For larger droplets, say 30 and 50  $\mu\text{m}$ , the droplets survive much longer as compared to  
723 10  $\mu\text{m}$  droplets, likely enhancing the chances of an ice nucleation event.

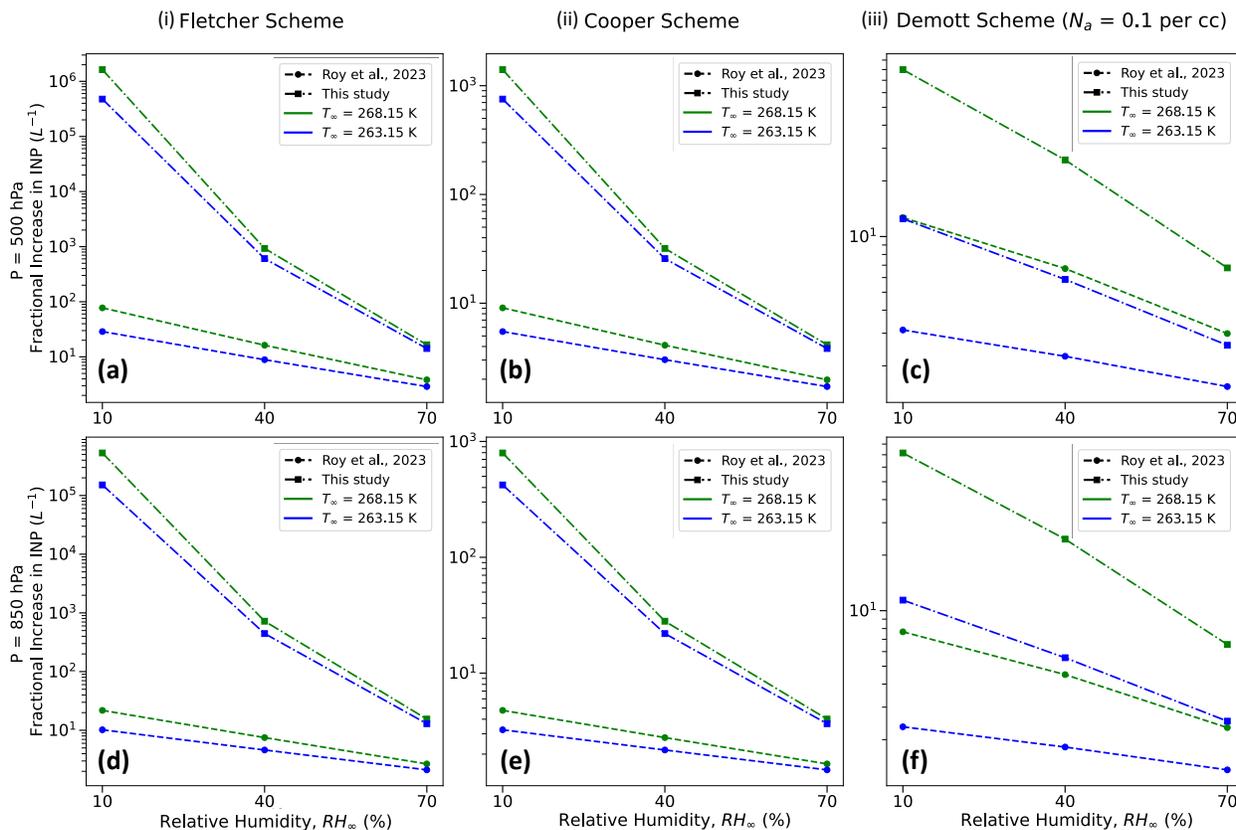
724  
725 Results from this study further strengthen evidence of the hypothesized mechanism of enhancement of ice nucleation  
726 via droplet evaporation. Together with the consistent observation of supercooled water in cloud-top generating cells  
727 (Plummer et al., 2014; Zaremba et al., 2024), these results contribute to explaining the observations of the prodigious  
728 production of ice particles produced in generating cells at the cloud-tops of winter storms and other clouds (e.g.,  
729 Plummer et al., 2015, Wang et al., 2020). Rauber et al. (1986), Plummer et al. (2015), and Tessorf et al. (2024)  
730 have shown that cloud droplet concentrations at the generating cell level near cloud-tops are of the order of  $30\text{-}50\text{ cm}^{-3}$ ,  
731 while ice-particle concentrations in the plumes of ice particles falling beneath generating cells are of the order of  
732  $0.01\text{ cm}^{-3}$ . Based on these values, if less than one frozen cloud droplet in 1000 survive sublimation after freezing and  
733 fall back into the cloud, that would be sufficient to create the ice-particles observed falling from a generating cell.

734  
735 Due to the observational evidence of a higher dependency of ice nucleation on temperature than time (Wright and  
736 Petters, 2013), and the increased difficulty of representing time-dependent stochastic nucleation in numerical models,  
737 the simpler and more widely used approach is to use the time-dependent singular hypothesis framework to simulate  
738 ice initiation processes. Drawing from theoretical insights, laboratory experiments, and field campaigns, numerous  
739 parameterization methods for modeling heterogeneous ice nucleation in cloud and climate models have been created  
740 over the years (Fletcher, 1962; Cooper, 1986; Meyers et al., 1992; DeMott et al., 1998; Khvorostyanov and Curry,  
741 2000; Phillips et al., 2008). Most of the conventionally used schemes (Fletcher, 1962; Cooper, 1986; Demott et al.,  
742 2010) share a common feature, which is the utilization of the ambient air temperature for estimating activated INPs,  
743 as opposed to relying on the droplet temperature, even for primary ice-nucleation modes such as immersion freezing  
744 and contact nucleation.

745  
746 Similar to Roy et al. (2023), we investigate the maximum enhancement in activated INP concentrations that can occur  
747 due to evaporative cooling of supercooled water droplets in a spatiotemporally varying environment, assuming that  
748 the activation in the parameterization schemes (Fletcher, 1962; Cooper, 1986; Demott et al., 2010) is related to the  
749 droplet temperatures towards the end of their lifetimes ( $T_L$ ) rather than the ambient temperature. Fig. 14 presents a  
750 comparison between Roy et al. (2023), and the current study in terms of the highest fractional increase in activated  
751 ice-nucleating particles (INPs), as projected through the Fletcher, Cooper, and Demott schemes (considering ambient  
752 aerosol concentration,  $N_a$ , with diameters greater than  $0.5\text{ }\mu\text{m}$ ). Owing to even lower droplet temperatures during  
753 evaporation, the fractional increase in activated INPs is higher as calculated from this study, with several orders of  
754 magnitude increase for drier environments. For example, the Fletcher Scheme predicts an enhancement in activated  
755 INPs by a factor of  $\sim 10^6$  for  $RH_\infty = 10\%$ ,  $T_\infty = 268.15\text{ K}$ ,  $P = 500\text{ hPa}$  based on droplet temperatures from this study,  
756 while the corresponding number from Roy et al. (2023) is  $\sim 100$  (Fig. 14a). The fractional increases are slightly smaller  
757 for higher pressure environments due to lower evaporative cooling of the droplets under such conditions (compare  
758 Figs. 14a, d, b,e, and c,f). Consistent with previous results from Roy et al. (2023), compared to the Fletcher Scheme,  
759 the Cooper and Demott schemes demonstrate relatively lower enhancement in activated INPs. For the same

760 environment stated earlier, the corresponding activated INP enhancement factor values for Cooper and Demott  
 761 schemes are  $\sim 10^3$  and 80, respectively (Figs. 14b and c).

762  
 763 Therefore, results from the current study further corroborate the hypothesized ice nucleation enhancement mechanism  
 764 through evaporative cooling of supercooled droplets (Mossop et al., 1968; Young, 1974; Beard, 1992; Roy et al.,  
 765 2023), providing much higher estimates of activated INP concentrations from previous analyses (Roy et al., 2023).  
 766 This potential increase in INP concentrations in subsaturated environments near cloud tops and edges, particularly at  
 767 higher sub-freezing temperatures, may partially help resolve the several orders of magnitude discrepancy between  
 768 predicted INP and observed ice particle concentrations in such regions of the cloud. To evaluate the effectiveness of  
 769 the potential ice-nucleation enhancement mechanism through evaporation, future modeling experiments within a  
 770 robust dynamical model setup, considering a population of both freezing and evaporating droplets, along with their  
 771 lifetimes, droplet-droplet interaction, different species of INPs, and the impact of turbulence and other feedbacks, are  
 772 required.



773  
 774 **Figure 14: Comparison between the maximum fractional increase in INPs as estimated by Roy et al., (2023) and this study**  
 775 **for three different parameterization schemes: (i) Fletcher (1962) (ii) Cooper (1986), and (iii) Demott et al., (2010), for three**  
 776 **different environmental relative humidities ( $RH_\infty = 10, 40$  and  $70\%$ ), and two ambient temperatures ( $T_\infty = 268.15$  K ( $-5^\circ\text{C}$ )**  
 777 **and  $263.15$  K ( $-10^\circ\text{C}$ )) and two different pressures ( $P = 500$  and  $850$  hPa).**

778  
 779  
 780

## 781 **6 Conclusions**

782

783 In this study, we presented a quantitative investigation of the temperature and lifetime of an evaporating droplet,  
784 considering internal thermal gradients within the droplet as well as resolving spatiotemporally varying unsteady  
785 thermal and vapor density gradients in the surrounding ambient air. The computational approach involved solving the  
786 Navier-Stokes and continuity equations, coupled with heat and vapor diffusion equations, using an advanced  
787 numerical model that employs the finite element method. This is the first simulation of the spatiotemporal evolution  
788 of droplet temperature, radius, and its environment for an isolated, stationary, and supercooled cloud droplet  
789 evaporating in various subsaturated environmental conditions. Various ambient pressure ( $P$ ), temperature ( $T_\infty$ ),  
790 relative humidity ( $RH_\infty$ ), and initial droplet radii ( $r_0$ ) were considered. The motivation behind this study was to provide  
791 more exacting calculations to support the hypothesized ice nucleation enhancement mechanism due to the evaporation  
792 of supercooled cloud droplets at cloud boundaries, such as cloud-top ice-generating cells, and for ambient temperatures  
793 between  $0^\circ\text{C}$  and  $-10^\circ\text{C}$  where ice nucleation is least effective.

794

795 The numerical simulations show for typical cloud droplet sizes ( $r_0 = 10, 30, 50 \mu\text{m}$ ) and environmental conditions  
796 considered here, the internal thermal gradients dissipate quite quickly ( $\leq 0.3 \text{ s}$ ) when the droplet is introduced to a new  
797 subsaturated environment. Thus, spatial thermal gradients within the droplet can be reasonably ignored. Hence, one  
798 can potentially ignore the extra computational expense of simulating conductive heat transfer within the droplet for  
799 timescales  $> 1 \text{ s}$ .

800

801 The results from this study are similar to findings from the literature that an evaporating supercooled cloud droplet  
802 can exist at a temperature lower than that of the ambient atmosphere and that the tendencies of the dependence of  
803 decrease in droplet temperatures on environmental factors and initial droplet sizes (Srivastava and Coen, 1992; Roy  
804 et. al, 2023). The novelty of this study lies in demonstrating that the magnitude of droplet cooling can be much higher  
805 than estimated from past studies of droplet evaporation, especially for drier environments. For example, a droplet  
806 evaporating in an environment with  $P = 500 \text{ hPa}$ ,  $T_\infty = 268.15 \text{ K}$  ( $-5^\circ\text{C}$ ),  $RH_\infty = 10\%$ , Roy et al., (2023) estimated a  
807  $7.3 \text{ K}$  decrease in droplet temperature, while this study shows that there can be as much as a  $23.8 \text{ K}$  decrease in droplet  
808 temperature. This is because previous studies assumed prescribed ambient environments at all distances from the  
809 droplet, while this analysis shows that as a droplet evaporates and cools, the air in the vicinity of the droplet cools as  
810 well, giving rise to spatiotemporally varying thermal and vapor density fields in the immediate environment  
811 surrounding the droplet. Here, the net conductive warming from the environmental air enveloping the droplet is lower  
812 as compared to Roy et al., (2023), effectively leading to a much lower droplet temperature. At a particular time, the  
813 strength and radial dependence of these gradients depend on the subsaturation of the air medium and the magnitude  
814 of droplet cooling due to evaporation, with the largest cooling at lower  $RH_\infty$ . In this study, the temperature and vapor  
815 density in the ambient air continually evolve, thus affecting the transfer of heat and vapor between the droplet surface  
816 and the environment far away from the droplet. This affects the temperature evolution and decay rates of the

817 evaporating droplet to a greater degree than shown in previous studies for a similar environment (Srivastava and  
818 Cohen, 1992; Roy et al. 2023).

819  
820 This study also demonstrated that the lifetimes of the evaporating droplets are longer compared to Roy et al. (2023)  
821 because as the droplet temperature gets lower, the saturation vapor pressure at the droplet surface reduces, leading to  
822 a weaker evaporation rate. For an environment with  $P = 500$  hPa,  $T_{\infty} = 268.15$  K ( $-5^{\circ}\text{C}$ ),  $RH_{\infty} = 10\%$ , a  $50\ \mu\text{m}$  droplet  
823 reaches the end of its lifetime, as defined in this study, in 32.8s, while the corresponding values for the diffusion-  
824 limited evaporation approach as estimated from Roy et. al, (2023) are 9.6 s and 17.9 s, respectively. The rates of  
825 evaporation tend to be lower in this study due to even lower droplet temperatures as well as spatiotemporally varying  
826 vapor density gradients around the droplets. As the droplet evaporates, the envelope of air surrounding the droplet is  
827 colder, has lower values of diffusivity leading to lower evaporation rates, and has higher vapor concentration than the  
828 ambient air, thus decreasing the evaporation rates.

829  
830 To summarize, if one considers the more realistic case of droplet evaporation, including the spatiotemporally varying  
831 thermal and vapor density gradients in the vicinity of the water droplet, the evaporating droplet can experience a  
832 substantial reduction in temperatures by several degrees, strongly dependent on the ambient relative humidity and  
833 weakly dependent on ambient pressure and temperature. Similar to the case of an isolated, stationary droplet  
834 evaporating in a prescribed ambient environment, the droplet almost immediately reaches its slope transition point  
835 temperature, which can be well-approximated by the thermodynamic wet-bulb temperature of the initial ambient  
836 environment around the droplet. Droplet temperatures then continue to steadily decrease as they adjust to the evolving  
837 thermodynamic wet-bulb temperature of the surrounding air. In more humid environments, the droplets may not  
838 experience a larger droplet cooling, but their lifetimes, as defined in this study, get extended by tens of seconds as  
839 compared to the Maxwellian estimation which neglects droplet cooling.

840  
841 The current analysis also demonstrates that lower evaporating droplet temperatures would lead to an enhancement of  
842 activated INPs from three widely used INP parameterization schemes, further corroborating the hypothesized ice  
843 nucleation enhancement mechanism through evaporative cooling of supercooled droplets. Notably, the estimates of  
844 activated INP concentrations from this study are higher than previous analyses, as the droplet temperatures are much  
845 lower towards the end of their lifetimes, with several orders of magnitude increase in activated INPs for drier  
846 environments. The Fletcher Scheme predicts the greatest enhancement in activated INPs by a factor of  $\sim 10^6$  for  $RH_{\infty}$   
847  $= 10\%$ ,  $T_{\infty} = 268.15$  K,  $P = 500$  hPa, while the corresponding enhancement factor values for Cooper and Demott  
848 schemes are  $\sim 10^3$  and 80, respectively.

849  
850 This study suggests a need for a more in-depth examination of supercooled cloud droplet temperatures and their  
851 lifetimes in subsaturated environments, especially when simulating heterogeneous ice nucleation processes that  
852 require the presence of supercooled water droplets. This is crucial because the concentration of activated ice-  
853 nucleating particles (INPs) is influenced by both droplet temperature and how long evaporating droplets persist.

854 Additionally, the findings from this investigation may also partially help understand disparities between observed ice  
855 particle concentrations and activated INPs, especially at relatively higher sub-0°C temperatures. Including the effect  
856 of droplet evaporative cooling on droplet temperatures and lifetimes, while modeling cloud microphysical processes  
857 in subsaturated environments, will also lead to improved accuracy of the evolution of the droplet size distribution as  
858 well as primary ice nucleation mechanisms.

859

860 **Author contribution:** PR, RMR and LDG conceptualized the problem and numerical experiments. PR designed and  
861 performed the simulations, analyzed the data, and prepared the first draft of the manuscript. RMR and LDG reviewed  
862 and edited the manuscript. RMR and LDG acquired required funding for the project.

863

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865

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869

870 **Code/Data availability:** This modeling analysis used the proprietary COMSOL Multiphysics version 6.0 software  
871 package which can be licensed through <https://www.comsol.com/>.

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