



# Measurement report: In-flight and ground-based measurements of nitrogen oxide emissions from latest generation jet engines and 100% sustainable aviation fuel

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**Abstract.** Nitrogen oxides, emitted from air traffic, are of concern due to their impact on climate by changing atmospheric ozone and methane levels. Using the DLR research aircraft Falcon, total reactive nitrogen (NO<sub>y</sub>) measurements were carried out at high altitudes to characterize emissions in the fresh aircraft exhaust from the latest generation Rolls-Royce Trent XWB-84 engine aboard the long-range Airbus A350-941 aircraft. The impact of different engine thrust settings, monitored in terms of combustor inlet temperature, pressure, and engine fuel flow, was tested for two different fuel types: Jet A-1 and for the first time a 100% sustainable aviation fuel (SAF) under similar atmospheric conditions. During ground emission measurements, a range of combustor temperatures and an additional blended SAF were tested. We confirm that the NO<sub>x</sub> emission index increases with increasing combustion temperature, pressure and fuel flow. We find that as expected, the fuel type has no measurable effect on the NO<sub>x</sub> emission index. These measurements are used to compare to cruise NO<sub>x</sub> emission index estimates from three engine emission models. Our measurements thus help to understand the ground to cruise correlation of current emission models while serving as input for climate modelling, and extending the extremely sparse data set on in-flight aircraft NO<sub>x</sub> emissions to newer engine generations.

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## 35 1 Introduction

Aviation is a steadily growing transport sector (Lee et al., 2021), even despite the short-term drop during the COVID-19 pandemic (Le Quéré et al., 2020; Schumann et al., 2021; Voigt et al., 2022). As a result, emissions from air traffic are also expected to increase continuously and higher aircraft and engine efficiencies are surpassed by the overall air traffic growth. The exhaust of an aircraft engine burning conventional kerosene is constituted on average of ~3.16 kg carbon dioxide (CO<sub>2</sub>) and ~1.23 kg water vapour (H<sub>2</sub>O) per kg of fuel burned (Lee et al., 2021). Further emissions depend on the engine type, power settings, combustor technology and fuel composition and include nitrogen oxides (NO<sub>x</sub>) as the sum of nitric oxide (NO) and nitrogen dioxide (NO<sub>2</sub>), carbon monoxide (CO), unburnt hydrocarbons (C<sub>x</sub>H<sub>y</sub>), sulphur dioxide (SO<sub>2</sub>) and soot (or non-volatile particulate matter, nvPM).

Most recent estimates (Lee et al., 2021) state that aviation since its historical beginnings contributes with +100.9 (55-145) mW m<sup>-2</sup> to about 4 to 5% to total anthropogenic effective radiative forcing (ERF) (Grewe et al., 2019; Lee et al., 2021). Thus, air traffic emissions have a warming effect on climate. Contrail cirrus hereby represent the largest share of aviation ERF with ~57%, followed by CO<sub>2</sub> (~34%) and NO<sub>x</sub> emissions (~17%; (Lee et al., 2021)). NO<sub>x</sub> emissions from aviation contribute indirectly to anthropogenic ERF via a short-term warming and a long-term cooling effect (Brasseur et al., 1996; IPCC, 1999; Köhler et al., 2008; Lee et al., 2010; Dahlmann et al., 2011; Grewe et al., 2019; IPCC, 2021; Lee et al., 2021; Skowron et al., 2021; Terrenoire et al., 2022). The net ERF from NO<sub>x</sub>, in sum, is however positive with 17.5 (0.6/29) mW m<sup>-2</sup> (Lee et al., 2021). Other studies indicate that the contribution of NO<sub>x</sub> in aviation ERF may be even higher due to simplifications in the methodology of previous estimates (Grewe et al., 2019). In the future, aviation NO<sub>x</sub> emissions may have a net negative ERF, as the effect of emission of aircraft NO<sub>x</sub> depends strongly on background emissions (Skowron et al., 2021).

Up to now, there is a lack of experimental measurements of NO<sub>x</sub> emissions at cruise altitudes from state-of-the-art jet engines. Thus, in the joint ECLIF3 (Emission and CLimate Impact of alternative Fuels 3) project, direct (NO<sub>x</sub>, CO, nvPM, H<sub>2</sub>O) and indirect aircraft emissions (ice particles, vPM) were measured at high altitudes to understand and assess the impact of modern air traffic on the atmosphere, see also Märkl et al. (2023) and previous related projects as in Voigt et al. (2021). In this paper, we present a comprehensive set of NO<sub>y</sub> emission measurements performed in the exhaust of the Airbus A350-941 with Rolls-Royce Trent XWB-84 engines. We derive emission indices from airborne measurements and compare them to ground-based measurements and three different engine emission prediction methods. We further investigate the effect of the Airbus aircraft burning 100% sustainable aviation fuel (SAF). Replacing conventional kerosene with SAF is one promising approach to reduce engine soot emissions, ice crystal number concentrations in contrails and the related climate impact, all in addition to a potential reduction of the CO<sub>2</sub> footprint in the life cycle analysis (Voigt et al., 2011; Moore et al., 2017; Kleine et al., 2018; Bräuer et al., 2021b; Bräuer et al., 2021a; Voigt et al., 2021).



## 65 2 Materials and Methods

### 2.1 NO<sub>x</sub> and CO<sub>2</sub> measurements

The DLR-operated research aircraft Falcon (reg. D-CMET, Dassault Falcon 20-E5), a twin-engine jet, was used as the airborne measurement platform. The in situ instrumentation consisted of several cabin-mounted trace gas (NO<sub>y</sub>, CO, CO<sub>2</sub>, H<sub>2</sub>O) and aerosol instruments with their sample inlets located on the upper fuselage, see Figure 1b. Also, cloud particle probes were  
70 mounted in underwing pods to measure ice particle number concentrations and size distributions in ambient conditions (Märkl et al., 2023). Here, we focus on the NO<sub>y</sub> and CO<sub>2</sub> measurement instruments as they are needed to derive the respective NO<sub>x</sub> emission indices.

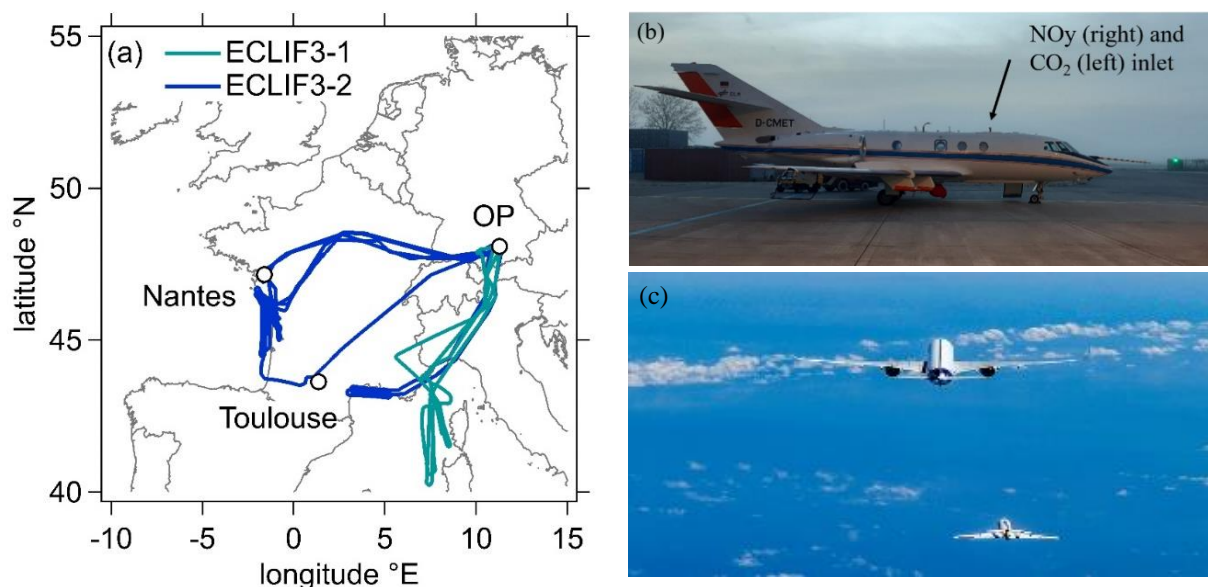
A well-established technique for measuring reactive nitrogen species, as employed in the present paper, includes their catalytic conversion to NO and subsequent detection using chemiluminescence technique. In general, chemiluminescence detectors  
75 (CLD) are widely used in atmospheric monitoring because they are sensitive with a detection limit as low as a few parts per trillion (ppt). In CLD, a sample of air passes through a reactor where NO is excited to NO<sub>2</sub><sup>\*</sup> by the reaction with high concentrations of O<sub>3</sub> produced by an ozone generator (Ridley and Howlett, 1974; Drummond et al., 1985). When returning to its ground state, the light emitted by the chemiluminescence reaction is proportional to the concentration of NO in the sample. By using selective converters directly upstream of the measurement chamber different reactive nitrogen species are converted  
80 to NO and subsequently detected by the CLD (Bollinger et al., 1983; Fahey et al., 1985). Within DLR, different types of CLD detectors have been used for atmospheric background measurements (Schlager et al., 1997; Ziereis et al., 2000; Schmitt, 2003; Stratmann et al., 2016; Ziereis et al., 2022) as well as in-plume detections (Schulte and Schlager, 1996; Schlager et al., 1997; Roiger et al., 2015). Aboard the Falcon a heated gold converter (T = 290 °C) with hydrogen (H<sub>2</sub>) as reducing agent catalytically reduces all NO<sub>y</sub> compounds to NO. NO<sub>y</sub> is the sum of NO<sub>x</sub> and all reactive nitrogen species as e.g. nitric acid,  
85 peroxyacetylnitrate (PAN) etc. The time resolution of the instrument is ~1 Hz with a detection limit of ~0.5 ppb. Under normal operating conditions the detector runs into saturation above mixing ratios of ~1000 ppb or ~1e6 counts per seconds. In order to measure at higher concentrations as expected in the exhaust plumes, a dilution system was integrated supplying zero air to the sample air in a ratio of 1/1 prior to the measurement. The NO<sub>y</sub> measurement accuracy ranges between ~5 ppb near the detection limit and ~490 ppb at highest detected mixing ratios of ~4 ppm. It includes the following uncertainty parameters  
90 typical for CLD instruments, for details see (Stratmann, 2013): the sensitivity of the instrument (841 ± 95 counts/ppb), the efficiency of the NO<sub>y</sub> converter (98.7 ± 1.5% at low and ± 30% at high concentrations), the instrumental interferences due to desorption processes and dark current (36 ± 118 counts), the statistical uncertainty of count rates (150-1600 counts), the uncertainty in the calibration standard (1% as stated by the manufacturer), the uncertainty due to the dilution system (7-21%) and due to a second instrument stage above 1e6 counts per seconds (i.e. 300 ppb).

95 A high frequency (~10 Hz) non-dispersive infrared gas analyser (LI-7000, LI-COR Biosciences) was used aboard the Falcon for in-plume CO<sub>2</sub> detections to be able to capture the small-scale variability of the plume. The LI-7000, uniquely modified in-house for aircraft deployment, uses two measurement chambers to detect CO<sub>2</sub>: one is constantly flushed with dry zero air, the



other is supplied with ambient air. The difference in absorption of infrared radiation passing through both cells is used to determine the absolute absorption and the absolute CO<sub>2</sub> mixing ratio (LI-COR, 2007). In the post processing, the CO<sub>2</sub> mixing ratio is corrected for dilution effects (LI-COR, 2003) and reported as dry air mole fraction. The CO<sub>2</sub> accuracy of the LI-7000 is independent with respect to the measured mixing ratios and is around 0.2 ppm. This includes the reproducibility of the calibration standards (0.08 ppm), the precision (0.08 ppm) and the uncertainty of water vapour measurement and thus the dilution correction (0.16 ppm). An occurring trend of the instrument response with instrument temperature and time is compensated by frequent zero measurements every 30 minutes during the flight. Absolute CO<sub>2</sub> mixing ratios and background values were cross checked with a second instrument aboard the Falcon, a cavity ring-down spectrometer (CRDS, Picarro G2401-m), due to its stable instrument performance (Fiehn et al., 2020; Klausner et al., 2020; Klausner, 2020). Airborne measurements are complemented by in-field ground measurements. The CO<sub>2</sub> concentration was monitored via a LI-7200RS (LI-COR Biosciences) and the nitrogen oxide concentration was monitored via a CLD64 (ecophysics) chemiluminescence monitor. Both instruments were calibrated with certified calibration gases before each test run.

## 110 2.2 Emission sampling strategy



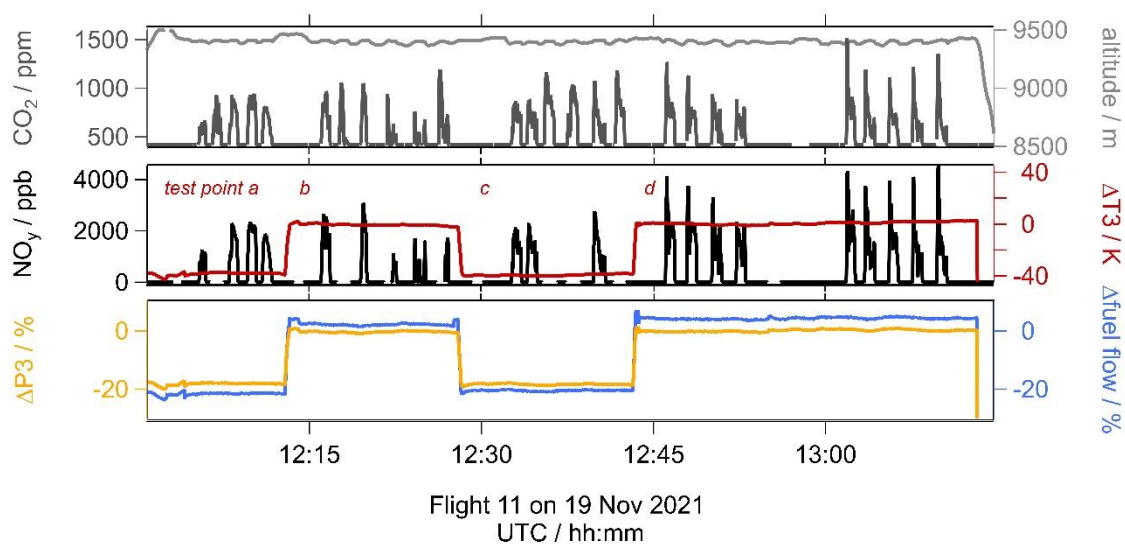
**Figure 1: (a) Map of the Falcon flight routes, (b) inlet positions for trace gas sampling aboard the Falcon and (c) Falcon aircraft catching up to the Airbus A350 to perform emission measurements, © Airbus 2021, photo by S. Ramadier.**

In-flight measurements at high altitudes were carried out under the framework of ECLIF3 in April 2021 (referred to as ECLIF3-1) and in November of 2021 (referred to as ECLIF3-2). This joint project was led by DLR and Airbus with Rolls-Royce, Neste, the University of Manchester and the National Research Council Canada (NRC) as partners. The objective of these flight campaigns was to characterize emissions behind an Airbus A350-941 (reg. F-WXWB) with Rolls-Royce Trent XWB-84 engines (ECLIF3-1: engine number 21004, ECLIF3-2: engine number 21012). This twin-engine aircraft is used for long-range

distances by many operators since it is more fuel efficient than a four-engine long-range aircraft and older two-engine aircraft.

120 During the mission flights, the Airbus aircraft was able to feed the engines from separate fuel tanks. Hence, measurements with two different fuels could be performed within single measurement flights which allowed probing of emissions at similar atmospheric conditions. As reference fuel, conventional Jet A-1 was used and provided by the local fuel supplier TotalEnergies. As sustainable aviation fuel, a 100% HEFA-SPK (Hydroprocessed Esters and Fatty Acids Synthetic Paraffinic Kerosene) made from sustainably sourced renewable waste and residues such as used cooking oil and other waste fat was provided by the project partner Neste.

125 Emission measurements were performed as close as possible to the Airbus aircraft at distances between 65 to 470 m (mean of 260 m), resulting in young plume ages of 0.3 to 3.5 s (mean of 0.8 s) in order to sample the fresh emissions before they undergo chemical processing in the atmosphere. Furthermore, it was aimed to study the emissions for various fuels at different combustor inlet parameters (temperature T3, pressure P3, engine fuel flow / fuel-to-air ratio) by varying the engine power settings and flight altitudes in defined but variable test point sequences. In total, six emission chase flights were performed along the western and southern French coast in temporary reserved air space, as shown in Figure 1a. The Falcon was mainly based in Oberpfaffenhofen (OP), Germany, and for a 5-day period in Toulouse, France, to minimize transfer flight times to the Airbus test area. With a take-off from OP, the Falcon had to be refueled in Nantes prior to the measurement flights along the Atlantic coast.



**Figure 2: Emission measurement sampling sequence during the flight on 19 Nov 2021. Trace gases ( $\text{CO}_2$ ,  $\text{NO}_y$ ) and flight altitude as measured aboard the Falcon. Change in Airbus aircraft engine parameters (delta fuel flow, delta T3 temperature, delta P3 pressure) indicate different engine test points.**

135 An example of an emission time series is shown in Figure 2. Measurements took place in the near field with the Falcon aircraft flying behind the Airbus aircraft under non- or only short-lived contrail-formation conditions. Usually, emissions were sampled from the right-hand side engine which was operated at different, well-defined cruise combustor inlet temperature conditions.



The Falcon is the slower flying aircraft with a maximum cruise speed of  $\sim 200 \text{ m s}^{-1}$ . To ensure that both aircraft speeds match in order to maintain the close distance, the Airbus aircraft had to adjust its speed by operating the left engine at a lower thrust. Hence, the test conditions probed in this study are not fully representative of typical cruise conditions. In addition, the Airbus aircraft also typically flies at higher altitudes (above FL350) compared to the altitudes which were sampled within this project (FL180 to 360). Generally speaking, this means that, at fixed T3 and DISA (Delta International Standard Atmosphere), the EIs measured at the lower test altitudes tend to be higher than the actual EIs at typical cruise altitudes (due to higher P3 at lower altitudes). Nevertheless, we assume that above FL300, this effect is small and the measurements can be directly compared to predictions at test conditions.

To ensure that the ceiling with the trace gas inlets is directly located in the exhaust plumes, the Falcon approached the exhaust trail from slightly lower altitudes. This position was held for  $\sim 50 \text{ s}$ , then the Falcon dropped down to measure atmospheric background conditions for  $\sim 30 \text{ s}$ . This alternating sequence was repeated 3-5 times for each test point with fixed engine parameters. Large enhancements ( $\Delta$ ) of  $\text{CO}_2$  and  $\text{NO}_y$  were clearly visible with values typically between 100-800 ppm ( $\Delta\text{CO}_2$ ) and 500-4000 ppb ( $\Delta\text{NO}_y$ ) above mean atmospheric background values of 414-419 ppm and 0.6-4 ppb, respectively.

Ground measurements were performed in October 2021 in Toulouse, France. Sampling was performed with a stainless-steel probe at a height of 2.6 m and a distance of 24.5 m between the right-hand side engine exit plane and probe inlet. The exhaust was transported via a 40 m heated stainless-steel line to a manifold that allowed even distribution of air to the different measuring instruments.

### 2.3 Emission index calculation and plume definition

In order to quantify exhaust emissions from aircraft, the most common metric is the so-called emission index (EI), i.e. an emission quantity per mass of burned fuel. The  $\text{NO}_x$  emissions index ( $\text{EI}(\text{NO}_x)$ ) is defined by convention in mass units of  $\text{NO}_2$  (ICAO, 2008; Voigt et al., 2012; ICAO, 2023), hence the sum of NO and  $\text{NO}_2$  in ambient air is calculated as if all NO was in the form of  $\text{NO}_2$ . Several studies discuss the composition of the different nitrogen species in the engine exhaust. E.g. (Kärcher et al., 1996; Tremmel et al., 1998; Bradshaw et al., 2000; Wormhoudt et al., 2007; Voigt et al., 2012) agree that at high engine power settings  $\text{NO}_x$  in the exhaust is dominated by NO ( $>80\%$ ). With growing plume age, the NO and  $\text{NO}_2$  ratio is determined by an equilibrium of the reaction of NO and  $\text{O}_3$ , forming  $\text{NO}_2$  and the photolysis of  $\text{NO}_2$  (Tremmel et al., 1998). In addition, small amounts of  $\text{HNO}_2$  and  $\text{HNO}_3$  are formed in the ageing plume from the  $\text{NO}_x$  emissions. Hence, by measuring  $\text{NO}_y$  aboard the Falcon all reactive nitrogen species in the exhaust can be detected and related to the initial  $\text{NO}_x$  emissions. For each individual plume encounter  $\text{EI}(\text{NO}_x)$  is derived based on the inert dilution tracer  $\text{CO}_2$  via Eq. (1) following Schulte et al. (1997):

$$\text{EI}(\text{NO}_x) = \frac{\int \Delta\text{NO}_y}{\int \Delta\text{CO}_2} * \text{EI}(\text{CO}_2) * \frac{M(\text{NO}_2)}{M(\text{CO}_2)}, \quad (1)$$

where  $\int \Delta\text{NO}_y$  and  $\int \Delta\text{CO}_2$  is the integrated enhancement above an atmospheric background level;  $\text{EI}(\text{CO}_2)$  is the emission index of  $\text{CO}_2$  dependent on the fuel used (see Table 1); and  $M(\text{NO}_2)$  and  $M(\text{CO}_2)$  are the molar masses of  $\text{NO}_2$  ( $46.0055 \text{ g mol}^{-1}$ ) and  $\text{CO}_2$  ( $44.0095 \text{ g mol}^{-1}$ ).



170 An individual plume encounter denotes a plume crossing in a time series where enhancements of  $\text{NO}_y$  and  $\text{CO}_2$  start exceeding  
background level variations, denoting the plume beginning, and the subsequent return to atmospheric background level,  
denoting the plume end. Between plume beginning and end a minimum 7 second plume length threshold was chosen to exclude  
accidental plume encounters. Further plumes were rejected due to Airbus aircraft engine instability (e.g. variability of T3  
greater than  $\pm 2$  K) and/or low correlation between  $\text{CO}_2$  and  $\text{NO}_y$  measurements ( $R < 0.7$ ). The individual plume crossings of  
175 the background-corrected mixing ratios of each species are integrated over time (and hence, over the horizontal extent of the  
plume) to account for the inlet positions (about 30 cm difference in the horizontal direction), tubing lengths and different  
instrument response times. Due to the variable position of the Falcon aircraft within the turbulent exhaust plume and thus  
variable plume dilution values, it is necessary to normalize  $\text{NO}_y$  mixing ratios to the measured  $\text{CO}_2$  concentration.  $\text{CO}_2$  hereby  
acts as a chemically inert species to determine the dilution of the engine emissions at the measurement point.  $\text{CO}_2$  emission  
180 indices are a fuel-dependent metric and are derived from the hydrogen and carbon content of the fuel under the assumption  
that it is completely burnt and all available carbon is converted to  $\text{CO}_2$ . The emission index  $\text{EI}(\text{CO}_2)$  can then be calculated via  
Eq. (2) following Moore et al. (2017):

$$\text{EI}(\text{CO}_2) = \frac{RT}{pV_m} * \frac{M(\text{CO}_2)}{M(\text{C}) + \alpha M(\text{H})} \quad (2)$$

where  $R$  is the ideal gas constant ( $8.31 \text{ J mol}^{-1} \text{ K}^{-1}$ );  $T$  and  $p$  are the temperature (273.15 K) and pressure (101325 Pa) at  
185 standard conditions;  $V_m$  is the molar volume at standard conditions ( $0.0224 \text{ m}^3 \text{ mol}^{-1}$ );  $M(\text{C})$  and  $M(\text{H})$  are the molar masses  
of carbon ( $12.01 \text{ g mol}^{-1}$ ) and hydrogen ( $1.01 \text{ g mol}^{-1}$ ); and  $\alpha$  is the hydrogen-to-carbon molar ratio of the fuel (as calculated  
based on Table 1). As the batches of the fuel supplier varied between the two measurement campaigns, also the fuel properties  
slightly varied. Their characteristic hydrogen and carbon contents are listed in Table 1 together with the calculated emission  
index of  $\text{CO}_2$ . The hydrogen content was measured via low resolution nuclear magnetic resonance spectrometry (ASTM D3701  
190 with a repeatability of 0.09% and reproducibility of 0.11%). The carbon content is assumed to add up to 100 mass% with the  
hydrogen content and sulphur content (not listed), and was cross checked via ASTM D5291 (which has a repeatability of  
0.94% and reproducibility of 2.42%).

195 **Table 1: Hydrogen and carbon content of Jet A-1 and HEFA-SPK during the two airborne measurement projects.  $\text{EI}(\text{CO}_2)$  is  
estimated following Moore et al. (2017). For the ground measurements also the HEFA-SPK blend is listed.**

Project	Fuel type	Hydrogen content / mass%	Carbon content / mass%	$\text{EI}(\text{CO}_2)$ / $\text{g kg}^{-1}$
<b>ECLIF3-1</b>	Jet A-1	14.08	85.90	3149
	HEFA-SPK	15.11	84.89	3111
<b>ECLIF3-2 (ground and flight)</b>	Jet A-1	14.25	85.74	3142
	HEFA-SPK	15.18	84.82	3108
	HEFA-SPK blend	14.39	85.56	3137

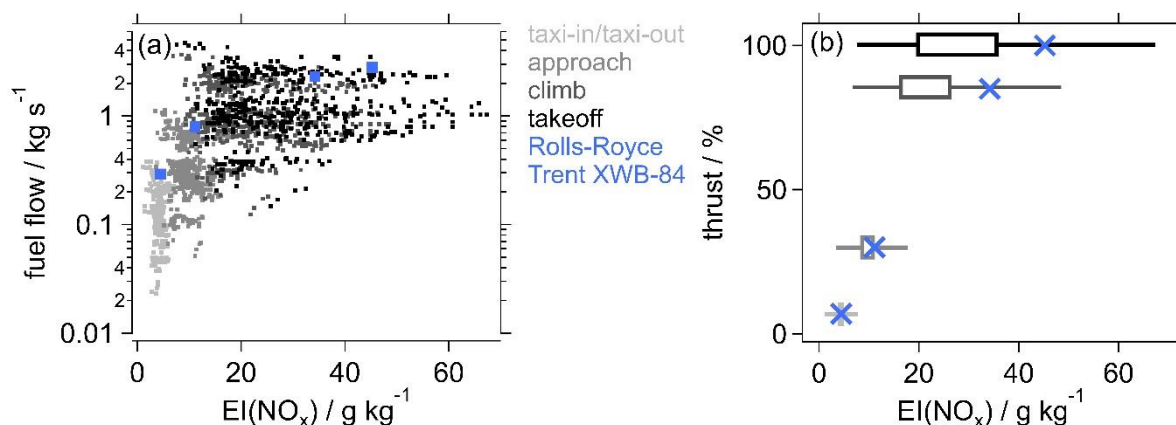


## 2.4 ICAO Aircraft Engine Emissions Databank

The reporting of emissions in the vicinity of airports is mandatory for engine manufacturers during certification processes for individual engine types and reports are voluntarily made publicly available at the International Civil Aviation Organization (ICAO) Aircraft Engine Emissions Databank (EEDB). For that, a landing and takeoff (LTO) cycle is defined to derive emissions during taxi-out/taxi-in, approach, climb and takeoff in a consistent manner (ICAO, 2008). While varying the engine power settings, and thus the fuel flow rate at a test stand, emissions at sea level conditions are measured. Thrust levels of 7%, 30%, 85% and 100% hereby correspond to taxi-in/taxi-out, approach, climb and takeoff conditions.

As  $\text{NO}_x$  emissions highly depend on temperature and pressure in the engine combustor, they are derived for different thrust settings related to different flight phases at certification ground test for International Standard Atmosphere (ISA) conditions. In general,  $\text{NO}_x$  emissions increase with increasing power and increasing fuel flow, see Figure 3. Thermal NO formation, first described by Zeldovich in 1946 and therefore also referred to as Zeldovich mechanism, is one of the main sources of nitrogen oxides in combustion dominating at high pressure and temperature conditions typical for a jet engine (Lavoie et al., 1970). However, as chemical equilibrium of the thermal NO formation route is not reached within typical timescales of a combustor, total formed  $\text{NO}_x$  in a modern rich burn combustor is strongly dependent on the quick quenching and mixing of the hot streams of the primary combustion zone. Combustor design optimised for  $\text{NO}_x$  emissions aims for enhanced mixing and reducing residence time in areas of high temperature. For a given combustor design,  $\text{NO}_x$  emissions depend on operating conditions as pressure temperature and local air-to-fuel ratio in the combustor.  $\text{NO}_x$  in a gas turbine combustor, i.e. at high pressure and temperature, is predominantly formed via thermal NO pathway. Thermal  $\text{NO}_x$  formation rate increases exponentially with temperature and further depends on pressure (Gokulakrishnan and Klassen, 2013). In comparison to all ~560 engine types covered by the EEDB (depicted in grayish/black; (EEDB, 2021)),  $\text{NO}_x$  emissions from the Rolls-Royce Trent XWB-84 engine (depicted in blue) are rather at the upper limit when considering the thrust settings, but typical for a modern large engine powering the long range planes. This engine is specifically designed for a modern long-range aircraft being the most fuel-efficient large aero-engine in revenue service, and therefore it operates at high pressure ratios and combustor exit temperatures to deliver the required thrust at high fuel efficiency. Therefore,  $\text{NO}_x$  emissions tend to be higher than for engines operating at lower overall pressure ratio (OPR).





225 **Figure 3: EI(NO<sub>x</sub>) based on the entire ICAO Aircraft Engine Emissions Databank v28B (EEDB, 2021). Panel (a) shows the dependency on fuel flow, panel (b) on thrust. The Rolls-Royce Trent XWB-84 engine, which was the focus during ECLIF3, is highlighted in blue.**

The certification engine emission data cover a standardised LTO cycle intended to cover local air quality. To predict EIs of the whole flight envelope, different modelling approaches exist, which use ground test data and correct them to atmospheric conditions at the respective flight level, flight phase and engine thrust setting, as e.g. done when applying the Rolls- Royce model or Fuel Flow correlation methods as described in the next section.

### 230 2.5 P3T3 and Fuel Flow methods

Based on the set of emissions data determined during the engine certification process, one can derive emission indices over various flight profiles using engine performance and emission models. A modern high-bypass turbofan engine in general follows a Brayton or Joule Cycle, where, after a fan, two air streams are separated: in the core of the engine, pressurized air and fuel are burned (temperature is increased by the heat release in the combustion chamber), and passed through a turbine, and together with the larger bypass air, propulsion thrust is produced. The subsequent positions are characterized and defined by total temperature and pressure regions: T2/P2 at the fan inlet, T24/P24 at the low-pressure compressor outlet, T3/P3 at the high-pressure compressor outlet and T5/P5 at the low-pressure turbine outlet. However, input data such as e.g. P3 and T3 are proprietary and thus not publicly available.

240 Engine performance data or models can be used to directly predict emissions at altitude, which is called P3T3 method (DuBois and Paynter, 2006). Manufacturers thus have developed their own prediction methods for non-LTO conditions based on correlations derived from empirical rig data to correct for the effect of a change in combustor inlet pressure (P3) and combustor Air Fuel Ratio (AFR) at a fixed combustor inlet temperature (T3). These correlations are typically referred to as P3T3 methods as often the AFR exponent may be set to zero. However, as NO<sub>x</sub> sensitivity to AFR depends on the stoichiometric distribution within the combustion zones of a rich burn combustor, it may also be set to some small number to reflect more EI(NO<sub>x</sub>) at



245 richer AFRs (towards higher power), as done for this comparison where AFR is set to 0.5. The validation of these methods has proven to be accurate within 10%.

The EI NO<sub>x</sub> must further be corrected to the lower pressure at altitude compared to sea-level static ( $P_{3_{\text{sealevel}}}/P_{3_{\text{altitude}}}$ )<sup>y</sup>. The exponent y is unique for every engine and derived by the manufacturers, but commonly ranges between 0.2 to 0.5 with typically 0.5 for a rich burn combustor being used. In addition, NO<sub>x</sub> emissions are also dependent on the ambient humidity as the  
250 additional heat capacity of the water reduces combustion temperature, and thus the NO<sub>x</sub> formation rate. Either actual humidity measurements are needed or a reference humidity of 60% is assumed (ISO 5878). In-flight measurements of relative humidity in the ECLIF3 test areas show values between 30 and 70%, hence the reference value is a reasonable assumption. However, this relative humidity at cold ambient temperature at altitude relates to a much lower absolute humidity by mass compared to  
255 ground reference condition of 6.34 g/kg. Based on the certification humidity correction formula for EI(NO<sub>x</sub>), cruise predictions must include a humidity correction of around +12%.

The direct P3T3 method requires proprietary engine data, which are not available for modelers. Simplified methods were developed to estimate NO<sub>x</sub> emissions relating in flight fuel flow at altitude to publicly available fuel flow data and corresponding EI(NO<sub>x</sub>) in the ICAO emissions databank. Such fuel flow methods (FFM) provide corrections to the different flight conditions such as altitude, humidity and Mach number (Deidewig et al., 1996; Döpelheuer and Lecht, 1999; DuBois  
260 and Paynter, 2006). The ground-based values, as reported by the ICAO Aircraft Engine Emissions Databank, are logarithmically fitted with respect to fuel flow. For EI(NO<sub>x</sub>), a power function fit leading to linear relations in a log-log plot is used between two points. Previously published comparisons with in situ NO<sub>x</sub> observations of older engines have shown that predictions based on fuel flow models and in-flight measurements agreed on average within ±12% (Schulte et al., 1997). For conventional rich burn combustors fuel flow methods like Boeing FFM2 (DuBois and Paynter, 2006) are able to predict altitude  
265 emissions within 10% compared to the full proprietary P3T3 method (Norman, 2003; SAE, 2009).

In this paper we use the calculated EI(NO<sub>x</sub>) of three different prediction methods and compare them to the in flight measurements: (a) the Boeing Fuel Flow Method2 (BFFM2) with which Rolls-Royce estimated EI(NO<sub>x</sub>) at the tested operating conditions; (b) a method based on the Fuel Flow Method2 (DuBois and Paynter, 2006) adapted and improved by DLR (aptFFM2) as described in Teoh et al. (2022); and (c) the Rolls-Royce in-house P3T3 method. For the fuel flow, actual  
270 observational data and the EI(CO<sub>2</sub>), according to Table 1, served as input. Differences between aptFFM2 and BFFM2 models are that the aptFFM2 method uses total pressure and temperature, therefore calculating the effect of aircraft speed, while the BFFM2 method uses ambient pressure and Mach number (Schaefer and Bartosch, 2013).

\* as coded in December 2022 in python by Roger Teoh and Marc Stettler at Imperial College and converted in 2022 to Fortran by our team at DLR.



## 275 3 Results and Discussion

In-flight measurements aboard the DLR research aircraft Falcon were carried out in the framework of the ECLIF project in 2021. Based on these in situ measurements at high altitudes we quantify exhaust emissions by inferring emission indices of  $\text{NO}_x$  valid for the young exhaust of a long-range A350-941 aircraft with latest generation Rolls-Royce Trent XWB-84 engines. For the first time, the Airbus aircraft was fuelled with 100% SAF (Airbus, 2021b, a; Rolls-Royce, 2021). The aircraft was able  
 280 to switch between Jet A-1 and SAF during the flight mission, hence, the impact of fuel effects could be measured in comparable atmospheric conditions. Furthermore, different engine power settings, e.g. compressor exit temperatures and pressure, as well as engine fuel flows / fuel-to-air ratio, were studied at high altitudes. Due to the confidential nature of detailed aircraft and engine parameters, we do not relate the derived emission indices to absolute values of engine sensitive parameters, but use a delta notation ( $\Delta$ ) to a representative observed value of the flight mission.

### 285 3.1 In-flight $\text{NO}_x$ emissions

The emitted  $\text{NO}_x$  of an aircraft engine is dependent on actual thrust and resulting combustor conditions as inlet temperature  $T_3$  and pressure  $P_3$ , as well as local air-to-fuel ratio. Hence, we present  $\text{EI}(\text{NO}_x)$  values depending on different source engine parameters, as listed in Table 2.

290 **Table 2: Normalisation of source engine parameters.**

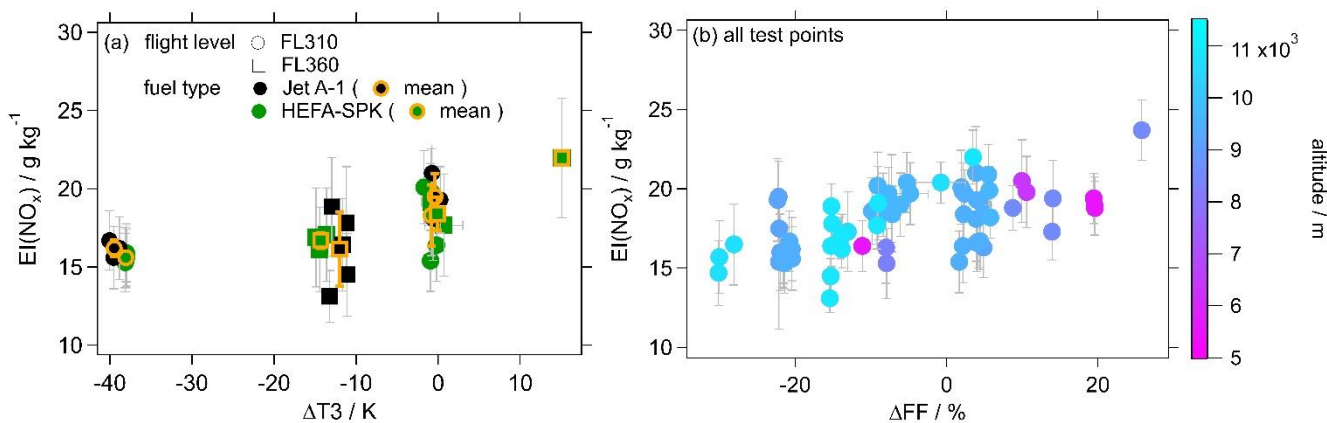
Abbreviation	Parameter	Unit	State within individual test points
$\Delta T_3$	total temperature at HPC exit relative change to a representative mission value	K	controlled adjustment
$\Delta P_3$	total pressure at HPC exit relative change to a representative mission value	%	changes with $T_3$ adaptations
$\Delta FF$	fuel flow rate per engine relative change to a representative mission value	%	changes with $T_3$ adaptations
<b>Mach</b>	Mach number ratio of true air speed (TAS) and local speed of sound	-	constant
<b>T2</b>	Total temperature at fan intake	%	constant

Since the temperature at the exit of the high-pressure compressor (HPC),  $T_3$ , is one of the major parameters affecting emissions, engine throttle was set in order to achieve various levels of  $T_3$  in the cruise range (low, mid and high-power cruise). This led to a different  $P_3$  and fuel flow levels, while Mach number and  $T_2$  were held roughly constant during different test  
 295 points by adjusting the second engine.



The dots in Figure 4a show emission indices derived from near field measurements on 19<sup>th</sup> of November 2021 at flight level (FL) 310 for varying  $\Delta T3$ . Two different T3 settings and fuel types (Jet A-1 and 100% HEFA-SPK) were probed during that flight. The flight altitude ( $9465 \pm 10$  m), Mach number ( $0.62 \pm 0.003$ ) and T2 ( $\pm 1\%$ ) were held constant within the different test points, while T3 was increased by  $\sim 40$  K. This led to a simultaneous increase in P3 by  $\sim 19\%$  and fuel flow by  $\sim 26\%$ . First, at  $\Delta T3$  of approx.  $-40$  K the mean EI from Jet A-1 ( $16.2 \pm 0.3$  g kg<sup>-1</sup>) and HEFA-SPK ( $15.6 \pm 0.2$  g kg<sup>-1</sup>) agree within their error estimates. Hence, no statistically significant impact of fuel type on EI(NO<sub>x</sub>) can be detected. This is within expectation, since it is assumed that the usage of different fuel types do not alter stoichiometric distribution within the combustion chamber. Second, the mean EI for Jet A-1 increases over the T3 range by  $\sim 20\%$  (to  $19.1 \pm 0.4$  g kg<sup>-1</sup>), the mean EI for HEFA-SPK by  $\sim 17\%$  (to  $18.3 \pm 1.7$  g kg<sup>-1</sup>). Therefore, it can also be concluded that both fuels show similar sensitivities to combustion conditions as temperature and pressure as expected.

The squares in Figure 4a represent measurements on 14<sup>th</sup> and 16<sup>th</sup> of April 2021 at FL360 to underline the two observations above with additional measurement points on a different day and at different flight altitude. At the  $\Delta T3$  setting of approx.  $-15$  K the mean EI(NO<sub>x</sub>) for Jet A-1 and HEFA-SPK again are in agreement within expected uncertainties. HEFA-SPK, in addition, was probed at two higher T3 settings (approx.  $0$  K and approx.  $15$  K) and shows also an increasing trend in mean EI(NO<sub>x</sub>) from  $16.7 \pm 0.5$  to  $18.4 \pm 1$  and  $22.0$  g kg<sup>-1</sup>.



**Figure 4:** EI(NO<sub>x</sub>) as calculated from in-flight measurements behind the A350 with Rolls-Royce Trent XWB-84 engines (a) versus  $\Delta T3$  at constant conditions at FL310 and FL360, (b) versus  $\Delta$ fuel flow; color coded by altitude for all acquired data points.

Figure 4b presents all data points acquired during the ECLIF3 campaign plotted against fuel flow range and color coded by flight altitude. Despite the scattered data, the expected increase in NO<sub>x</sub> emissions with increasing fuel flow can be recognized. Due to the multi-dimensional dependency of EI(NO<sub>x</sub>) on more than one engine parameter we cannot further assess the relative importance of individual engine parameter changes. However, we do not observe differences for the different flight altitudes where the measurements took place.

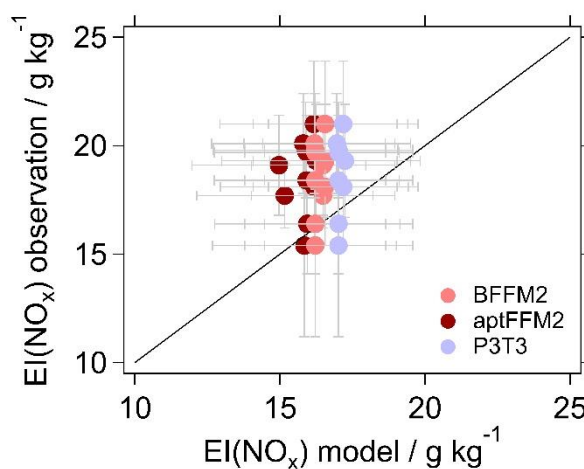
The spread of individual EIs in Figure 4a may be due to sensitivity of NO<sub>x</sub> to ambient conditions. The standard deviations from the means in  $\Delta T3$  EIs on 19 November 2021 (dots) are between 3-8% for Jet A-1 and around 2-11% for HEFA-SPK.



The standard deviations from the means for  $\Delta T_3$  EIs on 14 and 16 April 2021 (squares) are up to 15 % for Jet A-1 and 3-6 % for HEFA-SPK. However, these internal variabilities are still smaller than the increasing trend of the mean values with  $T_3$ .

### 3.2 Comparison with engine emission models

- 325 In this section we compare our near field in-flight measurements with model predictions. Please note that all ECLIF3-1 and -2 test points were analysed using BFFM2 and aptFFM2, whereas P3T3 model results are only available for ECLIF3-2. The model uncertainty for BFFM2 is around 10% for conventional rich burn (DuBois and Paynter, 2006), for aptFFM2 ~20% (ICAO, 2020; Teoh et al., 2022), for P3T3 around 10 to 15% (SAE, 2009) and for the observational EIs ~14% as derived from emission index uncertainty analysis below.
- 330 In general, the observation to model agreement is good with a correlation coefficient ( $R^2$ ) of 0.3 to 0.4. For aptFFM2 / BFFM2 / P3T3 roughly 40 / 50 / 75 % of data points agree within a difference of  $\pm 3 \text{ g kg}^{-1}$  and are thus well within the combined errors of model results and measurements. Deviations between the models are within the error limits. However, predicted EIs tend

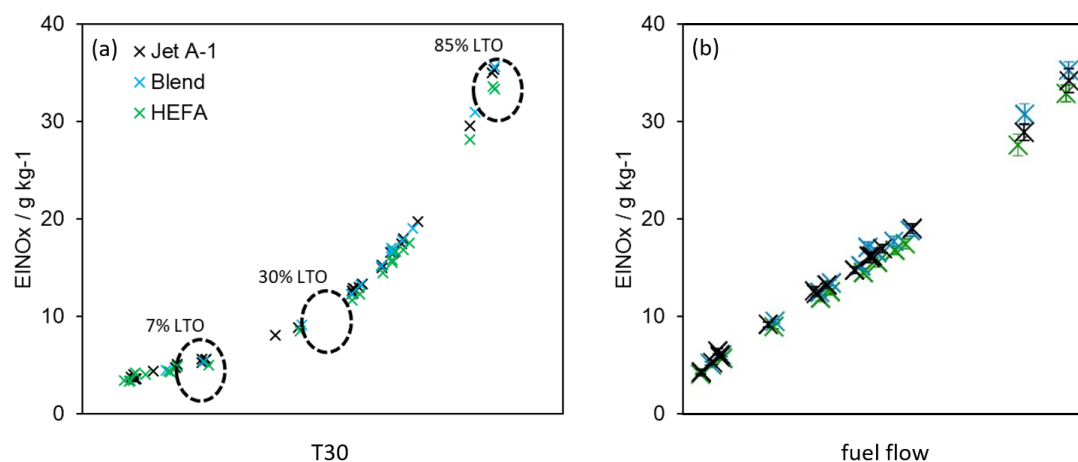


**Figure 5: EI(NO<sub>x</sub>) from observations and three model estimates for the 0 K  $\Delta T_3$  setting at FL310 and FL360. The black line marks the 1:1 agreement.**

- to be on average ~15% (aptFFM2, P3T3) to ~20% (BFFM2) lower than calculated EIs from the in-flight measurements in near field conditions. Figure 5 shows, analogous to Figure 4a, only data points for constant flight conditions at FL310 and FL360 with a focus on the  $\Delta T_3$  setting of 0 K. This subset focuses on a set of conditions for which the DISA was quite similar, hence the atmospheric temperature conditions do not affect the emission indices. Still, the model predictions tend to show smaller EIs than determined by the in-flight measurements of the engines at cruise at slightly lower Mach numbers compared to typical cruise conditions. In order to investigate in flight engine performance at typical cruise conditions we compare model predictions to far field measurements in the next section. Furthermore, to reduce effects of engine-to-engine variability we use
- 340 ground measurements at the same engine instead of predictions from the data base.

### 3.3 Ground-based NO<sub>x</sub> emissions

The ground-based engine tests were performed on two days at similar ambient temperatures. The reference measurements with fossil Jet A-1 were performed on 22 October 2021 (temperature: 12.2°C - 14.4°C; relative humidity: 87% - 81% during test run). The neat HEFA-SPK and an additional SAF blend (HEFA-SPK blended with a different Jet A-1) were tested on 23 October 2021 (temperature: 9.1°C - 15.2°C; relative humidity: 47% - 96% during test run). The hydrogen and carbon content by mass% of the SAF blend are 14.39% and 85.61% respectively (see Table 1). Four test points with Jet A-1 were repeated on the second day in order to identify any biases from changes in environmental conditions or different probe alignment. The engine was operated at several different power settings ranging from idle conditions to maximum climb. Each test point was stabilised for a few minutes and after reaching a stable T3, sampling was performed for 5-6 minutes. In case of the highest thrust settings, the sampling time was reduced to 2-3 minutes. During the ground measurements a large T3 temperature range was covered. Thus, the ground measurements allow the detection of the EI(NO<sub>x</sub>) curve over a larger range of T3 and fuel flows.



**Figure 6: EI(NO<sub>x</sub>) from ground measurements behind the A350 with Rolls-Royce Trent XWB-84 engines versus desensitized T3 (referenced to 60% RH, (a)) and  $\Delta$ fuel flow (b) for Jet A-1, HEFA-SPK and Blend. Black circles indicate LTO points.**

The NO<sub>x</sub> emission curve shows a continuous increase with higher thrust, and corresponding increasing T3, P3 and fuel flow. These dependencies are recognizable from Figure 6, where NO<sub>x</sub> is plotted over T3 and fuel flow. As expected and discussed above, NO<sub>x</sub> emissions are not significantly affected by the fuel composition. The observed emission indices are within estimated error margins. These findings are in line with results of ground-based measurements behind an Airbus A320-232 with IAE V2527-A5 engines in 2018 using fossil Jet A-1 fuels as well as blends of HEFA-SPK and Jet A-1 as discussed by Schripp et al. (2022). They also found an independence of NO<sub>x</sub> emissions on fuel type, and similar sensitivities to combustion temperature ( $\Delta T3 \sim 40K$ ,  $\Delta EI(NO_x) \sim 4 \text{ g kg}^{-1}$ ). Bulzan et al. (2010) also presented and discussed NO<sub>x</sub> results of a ground-based campaign in 2009 targeting the CFM56-2C1 engine of the NASA DC-8 aircraft burning pure fossil fuels (JP-8) as well as



blends with Fischer-Tropsch fuels based on natural gas and coal. They found an increase of EIs with fuel flow by about  $\sim 6$  g  $\text{kg}^{-1}$  per  $\sim 100\%$  more burned fuel, which is in line with the measurements performed in this study.

Figure 7 shows predictions using the ground measurements during the ECLIF3-2 campaign with the identical Rolls-Royce engine as input (see Figure 6) for engine emission model predictions to cruise altitudes and conditions. Although the lower absolute humidity should increase  $\text{NO}_x$  by 12%, in general, lower  $\text{NO}_x$  levels compared to the ground measurements are expected due to the lower pressure at altitude. The predictions are compared to far field measurements of the Falcon, obtained within the same project, but with both aircraft flying at typical cruise conditions and Mach numbers. The two engine models agree well with the measurements at cruise altitudes within the estimated uncertainties. The BFFM2 predictions are typically 10% higher compared to P3T3 methods which has been found before for this type of combustor, but are still within the  $\Delta T_3$  ranges. The agreement between the models and the in flight measurements is significantly improved by using the ground based  $\text{EI}(\text{NO}_x)$  measurements on the same engine instead of using emission data from the engine emission data base used for Figure 5. The use of ground measurement data on the same engine takes into account a potential slight change in engine performance of well-maintained in operation engines. The comparison to in-flight measurements at typical cruise conditions in terms of  $T_3$ ,  $P_3$ , AFR and Mach number also ensures a better comparability of the predictions well within the range tested in rig tests.

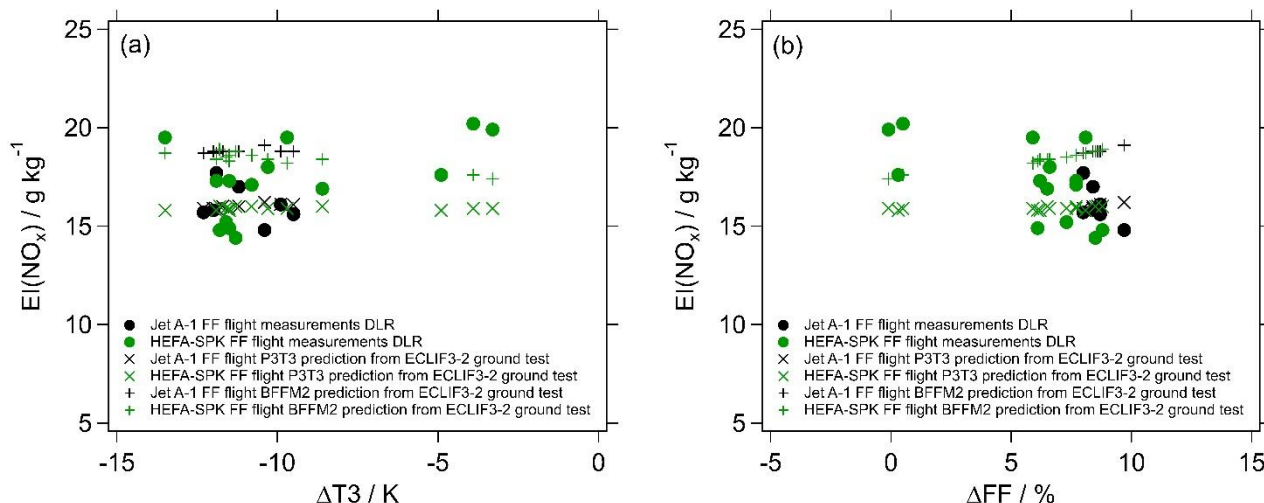


Figure 7:  $\text{EI}(\text{NO}_x)$  (dots) from in flight measurements for different fuels at typical cruise Mach numbers in the far field at flight level 320 and FL350 from ECLIF3-2 behind the A350 with Rolls-Royce Trent XWB-84 engines versus desensitized  $T_3$  (a) and desensitized fuel flow (b). Modelled  $\text{EI}(\text{NO}_x)$  for the far field measurement conditions from the P3T3 model (cross) and the Boeing Fuel Flow Method2 (plus) calculated based on ECLIF3 ground measurements shown in Figure 6.

### 3.4 In-flight emission index uncertainty analysis

Here, we present an in-depth analysis of different aspects contributing to the uncertainty of each individual inferred emission index (see Eq. (1)) with respect to the in-flight measurements. The EI uncertainty consists of several individual errors: (a) the uncertainty of the enhancement above an atmospheric background level ( $\partial(\Delta \text{NO}_y)$  and  $\partial(\Delta \text{CO}_2)$ ), which can be subdivided into (a.a) the absolute accuracy of the measured species ( $\partial \text{NO}_{y\_acc}$ ,  $\partial \text{CO}_{2\_acc}$ ) and (a.b) the uncertainty related to the atmospheric

background determination ( $\partial\text{NO}_{y\_bgr}$ ,  $\partial\text{CO}_2\_bgr$ ); (b) the uncertainty in  $\text{EI}(\text{CO}_2)$ ; and (c) the uncertainty in the molar masses of  $\text{NO}_2$  and  $\text{CO}_2$ . The total uncertainty ( $\partial$ ) is then estimated using Gaussian error propagation following Eq. (3):

$$\begin{aligned}
 390 \quad \partial\text{EI}(\text{NO}_x) = \pm & \sqrt{\left(\frac{\partial\text{EI}(\text{NO}_x)}{\partial\text{NO}_y} \partial\text{NO}_{y\_acc}\right)^2 + \left(\frac{\partial\text{EI}(\text{NO}_x)}{\partial\text{NO}_y} \partial\text{NO}_{y\_bgr}\right)^2 + \left(\frac{\partial\text{EI}(\text{NO}_x)}{\partial\text{CO}_2} \partial\text{CO}_{2\_acc}\right)^2 + \left(\frac{\partial\text{EI}(\text{NO}_x)}{\partial\text{CO}_2} \partial\text{CO}_{2\_bgr}\right)^2 +} \\
 & + \left(\frac{\partial\text{EI}(\text{NO}_x)}{\partial\text{EI}(\text{CO}_2)} \partial\text{EI}(\text{CO}_2)\right)^2 + \left(\frac{\partial\text{EI}(\text{NO}_x)}{\partial M(\text{NO}_2)} \partial M(\text{NO}_2)\right)^2 + \left(\frac{\partial\text{EI}(\text{NO}_x)}{\partial M(\text{CO}_2)} \partial M(\text{CO}_2)\right)^2} \\
 (3)
 \end{aligned}$$

The individual uncertainty terms and the total EI uncertainty for  $\text{EI}(\text{NO}_x)$  are listed in Table 3. For  $\text{EI}(\text{NO}_x)$  the mean uncertainty from all in-flight plume encounters sums up to ~14%. Figure 8 further depicts the relative contribution of the individual terms to the total uncertainty for each plume encounter. It is evident that the most important uncertainty term for  $\text{EI}(\text{NO}_x)$  is the  $\text{NO}_y$  accuracy. For future aircraft campaigns we plan to implement a different dilution approach and suggest flying in a larger distance to the aircraft of interest to prevent the instrument from running into saturation effects.

**Table 3: Individual contributions to total  $\text{EI}(\text{NO}_x)$  uncertainty for all in-flight exhaust encounters. The table denotes mean values; however the uncertainty is estimated for each individual plume encounter individually.**

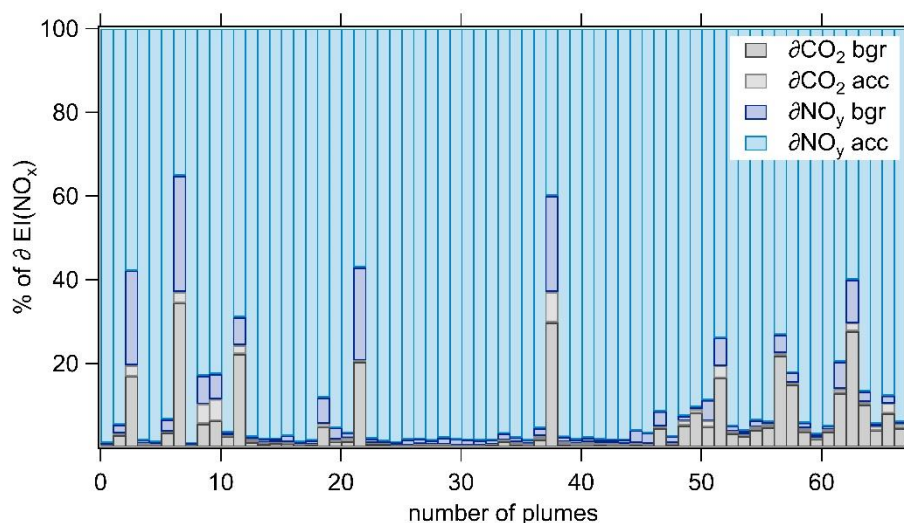
Uncertainty term for $\text{EI}(\text{NO}_x)$	Mean uncertainty estimate / %
$\partial\text{NO}_y$ acc	13
$\partial\text{NO}_y$ bgr	<1
$\partial\text{CO}_2$ acc	<1
$\partial\text{CO}_2$ bgr	1
$\partial\text{EI}(\text{CO}_2)$	0.1
$\partial M(\text{NO}_2)$	0.002
$\partial M(\text{CO}_2)$	0.003
<b>Total uncertainty <math>\partial\text{EI}(\text{NO}_x)</math></b>	<b>14</b>

The percentage contribution of the individual accuracy is generally higher (lower) when the encountered mixing ratio enhancement was low (high). The uncertainty of  $\text{EI}(\text{CO}_2)$ , as well as of the molar masses, are negligible. The measurement uncertainties, i.e. the measurement accuracies for  $\text{NO}_y$  and  $\text{CO}_2$  were described in the Materials and Method Section, including errors from the individual instruments, measurement techniques and calibration procedures. These absolute measurement accuracies (in ppb and ppm) are then translated into a relative accuracy (in %) based on the maximum mixing ratio enhancement observed during each exhaust plume encounter. The mean relative accuracy for  $\text{CO}_2$  is <1% (0.1-2.5%) and for  $\text{NO}_y$  13% (9-23%), see Table 3. The atmospheric background mole fraction needs to be determined for each individual plume encounter individually to account for horizontal, vertical as well as temporal gradients in the ambient atmosphere. However,





410 the typical atmospheric background variation of  $\text{NO}_y$  ( $\Delta 4$  ppb) and  $\text{CO}_2$  ( $\Delta 5$  ppm) is not sensitive to the high mixing ratios encountered ( $\Delta \text{NO}_y \sim 500\text{-}4000$  ppb,  $\Delta \text{CO}_2 \sim 100\text{-}800$  ppm). The atmospheric background itself is estimated based on the following assumption. Primarily, prior to and after the plume encounter the probed air mass needs to be free of engine exhaust. Due to the natural dynamics of the troposphere, the atmospheric background for the long-lived gases  $\text{CO}_2$  is not always as obvious as in the short-lived  $\text{NO}_y$ , hence,  $\text{NO}_y$  is taken as the main focus for this determination. If prior and after the encounter  
415 the mole fractions are identical, this value is taken for the atmospheric background. If the mole fractions are different, the atmospheric background is set in between these values. The mean difference from the mixing ratio at the start and end of the individual plume encounter to the respective atmospheric background estimate is considered in the uncertainty of the atmospheric background estimate. Moreover, the standard deviation ( $1\sigma$ ) of an atmospheric background-like sequence is taken into account.



420 **Figure 8: Stacked individual uncertainties for  $\text{EI}(\text{NO}_x)$  for in-flight plume encounters.**

## Conclusion

In conclusion, we presented the first  $\text{EI}(\text{NO}_x)$  in-flight measurements for a modern long-range aircraft and engines since 1995 (Schulte et al., 1997). We showed that the measurements and methodology are adequate to infer  $\text{EI}(\text{NO}_x)$  emissions from  
425 aircraft at high altitudes. As expected from previous ground engine tests, the fuel type, even a 100% SAF, has no statistically significant effect on the  $\text{NO}_x$  emission index.  $\text{EI}(\text{NO}_x)$  increases with increasing combustion temperature, pressure, and fuel flow for the measured cruise T3 range conditions. Furthermore, the in-flight in situ measurements generally agree with predictions from three different engine emission prediction methods within combined uncertainties when using data sets from the emission data base release as input, with a slight trend towards modelled lower emission indices. In order to take into  
430 account performance variations of the operational engines during maintenance cycles and to avoid engine to engine performance variations we performed ground measurements behind the same engine over a wide T3 range. The ground



measurements show an increase in  $EI(NO_x)$  with increasing thrust, as explained by higher combustor temperatures. The ground measurements were then used as input to predict  $EI(NO_x)$  at cruise altitudes for typical cruise conditions using current engine models. The models generally agree better with the measured  $EI(NO_x)$  for in flight observations at typical cruise conditions with respect to P3, T3, AFR and Mach number. These campaigns present the first in-flight measurements targeting  $NO_x$  emissions of latest-generation engines at high altitudes and thus provide a valuable data set of  $EI(NO_x)$  cruise measurements for the evaluation of state-of-the art engine models. The observations thereby enhance the sparse existing data set of cruise emissions of older generation engines.

### Data Availability

440 The  $CO_2$  and  $NO_y$  flight measurement data are released at <https://doi.org/10.5281/zenodo.10646359> (Harlass et al., 2024).

### Author Contribution

TH analyzed the  $NO_y$  and  $CO_2$  measurement data and wrote the manuscript with inputs from all co-authors. TH, RD, RM, DS, MS, SK and PSt performed the Falcon measurements. TS, TG and LB performed the ground-based measurements. CV and CR conceived and designed the aircraft campaigns. US, MJ, DL, DA and PM performed the model simulations. All authors contributed to the interpretation of the data, reviewed the manuscript and have given approval to its final version.

### Competing Interests

CR and MG are employed by Airbus Operations SAS; MJ, DL, PM and Psw are employed by Rolls-Royce plc. 725 and DA by Rolls-Royce Deutschland; RS is employed by Neste Corporation. All other authors declare that they have no conflict of interest.

### 450 Funding Sources

TB was funded by the Deutsche Forschungsgemeinschaft (DFG, German Research Foundation) under project nr 510826369 and CV by DFG SPP 1294 HALO under project nr VO1504\_9 and by European Union under Grant Agreement No 101101999 and No 101114613.

### Acknowledgments

455 The authors especially thank DLR-FX for the campaign cooperation. This involves not only our pilots Michael Grossrubatscher, Thomas von Marwick, Philipp Weber and Roland Welsler, but also the management Georg Dietz and Oliver Paxa and the group of Martin Zöger, Andreas Giez, Vladyslav Nenakhov, Christoph Grad, Marina Schimpf, Christian Mallaun,

David Woudsma, Alexander Wolf, Frank Probst, Stefan Hempe and many more. We also thank the flight test team of Airbus for the great coordination of the aircraft on ground as well as in the test areas. Great recognition is dedicated to the Rolls-  
460 Royce Technical Support team in Toulouse. And a special thanks is dedicated to all other ECLIF3 partners for their helpful cooperation. We would also like to thank Roger Teoh and Mark Stettler, who provided the source code for modelling emission indices.

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