



1 **ECOMAN: an open-source package for geodynamic and** 2 **seismological modeling of mechanical anisotropy.**

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12 **Abstract.** Mechanical anisotropy related to rock fabrics is a proxy for constraining the Earth's deformation patterns. However,
13 the forward and inverse modelling of mechanical anisotropy in 3D large-scale domains has been traditionally hampered by the
14 intensive computational cost and the lack of a dedicated, open-source computational framework. Here we introduce ECOMAN,
15 a software package for modelling strain-/stress-induced rock fabrics and testing the effects of the resulting elastic and viscous
16 anisotropy on seismic imaging and mantle convection patterns.

17 Differently from existing analogous software, the modelling of strain-induced fabrics has been extended to all mantle levels
18 and it has been optimised to run across multiple CPUs, yielding strong scaling efficiency. In addition, shape preferred
19 orientation (SPO)-related structures can be modelled and superimposed over lattice/crystallographic preferred orientation
20 (LPO/CPO) fabrics, which allows the consideration of the mechanical effects of fluid-filled cracks, foliated/lineated grain-
21 scale fabrics and rock-scale layering.

22 One of the most important innovations is the Platform for Seismic Imaging (PSI), a set of programs for performing forward
23 and inverse seismic modelling in isotropic/anisotropic media using real or synthetic seismic datasets. The anisotropic inversion
24 strategy is capable of recovering parameters describing a tilted transversely isotropic (TTI) medium, which is required to
25 reconstruct 3D structures and mantle strain patterns and to validate geodynamic models.

26 **1 Introduction**

27 The study of the Earth's interior has been traditionally based on seismological and geodynamic modelling, the former providing
28 important information about its present-day structure, composition and state (Chang et al., 2015; French and Romanowicz,
29 2015; Schaeffer et al., 2016; Debayle et al., 2020), and the latter about its dynamics and compositional evolution (Davies et



30 al., 2012; Cramer and Tackley, 2014; Müller et al., 2022). Seismological and geodynamical modelling are very often
31 conducted independently, which creates mechanical and geometrical inconsistencies across the models, hampers the
32 interpretation of seismic observations in terms of geodynamic processes, and exacerbates the non-uniqueness of geodynamic
33 model predictions. An alternative approach is combining computational seismology and geodynamics with mineral physics,
34 which provides a comprehensive understanding of the Earth's interior processes, seismic behaviour, and material properties.
35 This multidisciplinary methodology has been used in previous studies to post-process geodynamic flow calculations with
36 thermodynamically self-consistent models of mantle mineralogy and converting thermal structure into isotropic elastic
37 parameters. The obtained seismic mantle structure can then be used in simulations of global wave propagation, such that
38 specific hypotheses on mantle dynamics can be tested directly against seismic data (Styles et al., 2011; Schubert et al., 2012;
39 Maguire et al., 2018). The inverse procedure consists in converting seismic anomalies into density anomalies driving mantle
40 flow models and is typically employed to quantify dynamic topography and mantle viscosity structure, and to reproduce large-
41 scale mantle flow patterns (e.g., Bunge et al., 2003; Steinberger and Calderwood, 2006; Rudolph et al., 2015). However,
42 isotropic seismic imaging provides limited information regarding local-/regional-scale dynamical processes (Fraters and
43 Billen, 2021), and a better way to couple the geodynamic evolution and seismological structure of the Earth's interior is by
44 accounting for the strain-/stress-induced mechanical anisotropy of crustal and mantle rocks.

45 Mechanical anisotropy refers to the directional dependence of mechanical properties in a material, and is well known to affect
46 both elastic and viscous deformational behaviour. Mechanical anisotropy depends on several factors, including the lattice or
47 crystal preferred orientation (LPO, CPO) of intrinsically anisotropic minerals, and extrinsic mechanisms related to the shape
48 preferential orientation (SPO) of melt, fluid, or air-filled fractures and non-spherical pores, and grain- or rock-scale
49 compositional layering. Most micro- and macro-scale fabrics are acquired as a function of the cumulative deformation and
50 material mechanical properties, and as such they constitute an important source of information about the Earth's dynamical
51 behaviour.

52 Elastic anisotropy is directly connected to seismic anisotropy, which is a phenomenon in which the seismic wave speed varies
53 as a function of the propagation direction. It is mainly observed in the crust, mantle boundary layers, and inner core (Almqvist
54 and Mainprice, 2017; Karato, 1998; Kendall, 2000; Long and Becker, 2010; Deuss, 2014). Understanding and modelling
55 seismic anisotropy is crucial for determining long-term deformational patterns and the present-day stress field in the crust, and
56 constraining geodynamic modelling predictions (Jadamec and Billen, 2010; Hu et al., 2017; Zhou et al., 2018; Lo Bue et al.,
57 2022). In addition, the ability to account for anisotropic effects can improve the quality of subsurface imaging. Indeed, it has
58 been demonstrated that, because of the uneven seismic ray coverage, failing to account for seismic anisotropy may generate
59 strong artefacts that substantially bias our understanding of mantle structures and dynamics in different tectonic settings
60 (Bezada et al., 2016; VanderBeek and Faccenda, 2021; VanderBeek et al., 2023; Faccenda and VanderBeek, 2023).
61 Considering the widespread presence of seismic anisotropy, anisotropic seismic models provide a more realistic representation
62 of the Earth's subsurface compared to isotropic models.



63 Viscous anisotropy modelling refers to the study and simulation of materials that exhibit varying degrees of viscosity
64 (resistance to viscous deformation) in different directions. Although viscous anisotropy has been traditionally associated with
65 the mechanical behaviour of multi-layered media (Mühlhaus et al., 2002; Kocher et al., 2006), it has been also observed in
66 experimentally-deformed mica-rich and olivine crystal aggregates (Shead and Kronenberg, 1993; Hansen et al., 2012).
67 Previous numerical studies demonstrated that viscous anisotropy can potentially stabilise long-wavelength convective patterns
68 (Christensen, 1987; Mühlhaus et al., 2004) and more generally affect processes such as plate motion (Király et al., 2020), post-
69 glacial rebound (Han and Wahr, 1997), lithospheric shear zone reactivation (Tommasi et al., 2009) and dripping (Lev and
70 Hager, 2008).

71 Over the last few years a few attempts have been made to integrate micro-mechanical modelling of fabric evolution with large-
72 scale geodynamic models using either directors (Lev et al., 2008; Halter et al., 2022), the CPO model D-REX (Kaminski et
73 al., 2004; Becker et al., 2006; Jadamec and Billen, 2010; Faccenda and Capitanio, 2013; Faccenda, 2014; Ito et al., 2014; Hu
74 et al., 2017; Zhou et al., 2018; Fraters and Billen, 2021), or the CPO model Visco-Plastic Self Consistent (VPSC; Tommasi et
75 al., 2009; Li et al., 2014). However, each of these methodologies has its own limitations mainly associated with either the
76 accuracy of the estimates, the large computational burden or software accessibility, which have impeded a more widespread
77 diffusion in the geodynamic community. At the same time, the recovery of 3D seismic anisotropy patterns has been
78 traditionally considered intractable due to the highly underdetermined nature of the inverse problem, and only recently a
79 theoretical background and computational algorithms have been developed to invert for body wave seismic anisotropy in 3D
80 anisotropic media (VanderBeek and Faccenda, 2021; Rappisi et al., 2022; Wang and Zhao, 2022; VanderBeek et al., 2023;
81 Del Piccolo et al., 2023). Yet, to date there is no freely-available software capable of modelling seismic anisotropy related to
82 arbitrarily oriented structures.

83 In this contribution we present the new and open-source software package ECOMAN (Exploring the **CO**nsequences of
84 **M**echanical **AN**isotropy) that enables linking seismology and geodynamics by providing a set of computationally optimised
85 programs for (i) estimating rock mechanical anisotropy as a function of the geodynamic model deformation history, and
86 compositional, rheological, stress, pressure, temperature, fields, and (ii) solving forward/inverse seismological problems
87 accounting for seismic anisotropy. In the next sections, we first describe the different ECOMAN modules, after which we
88 discuss the advantages and limitations of the software package, and the roadmap for future developments.

89

90 Table 1. Abbreviations and their description. Units are indicated for dimensional physical properties.

Abbreviation	Description	
UM	Upper mantle	
UTZ	Upper mantle transition zone	



L TZ	Lower mantle transition zone	
LM	Lower mantle	
LPO/CPO	Lattice/crystal preferred orientation	
SPO	Shape preferred orientation	
FSE	Finite Strain Ellipsoid, defined by the eigenvalues and eigenvectors of LS	
STILWE	Smoothed Transversely Isotropic Long-Wavelength Equivalent	
DEM	Differential Effective Medium	
VPSC	Visco-Plastic Self Consistent	
MDM	Modified Director Method	
		Units
ρ	Density	kg/m ³
P	Pressure	Pa
T	Temperature	K
F _d	Fraction of dislocation creep deformation	-
V , V _i	Velocity vector and its components	m/s
F , F _{ij}	2 nd -order deformation gradient tensor and its components	-
LS , LS _{ij}	2 nd -order left stretch tensor and its components	-
C , C _{αβ}	4 th -order elastic tensor and its components in Voigt notation	GPa
η , η _{αβ}	4 th -order normalised viscous tensor and its components in Voigt notation	-

91

92 **2 Software package structure**

93 ECOMAN includes several programs that are complementary and can be grouped into three main categories (Fig. 1):

94



- 1) programs that estimate strain/stress-induced rock fabrics (LPO and SPO) and their elastic and viscous anisotropic mechanical properties (D-REX_S, D-REX_M, EXEV);
- 2) programs that post-process the simulated rock fabrics for visualisation of their isotropic/anisotropic mechanical properties and deformational history (VIZTOMO, VIZVISC), and format the elastic tensors generating input files for seismological synthetics (VIZTOMO);
- 3) programs that test the elastic response of anisotropic media by performing seismological forward/inverse modelling and, in particular, isotropic and anisotropic seismic tomographies on synthetic and real seismic datasets (SKS-SPLIT, PSI).

Most of the code modules are written in the Fortran programming language, except for the PSI program that is written in Julia. Visualisation of the output is done through the MATLAB MTEX toolbox (Mainprice et al., 2011) for single aggregate fabrics, and ParaView (Ahrens et al., 2005) for 2D and 3D simulations.

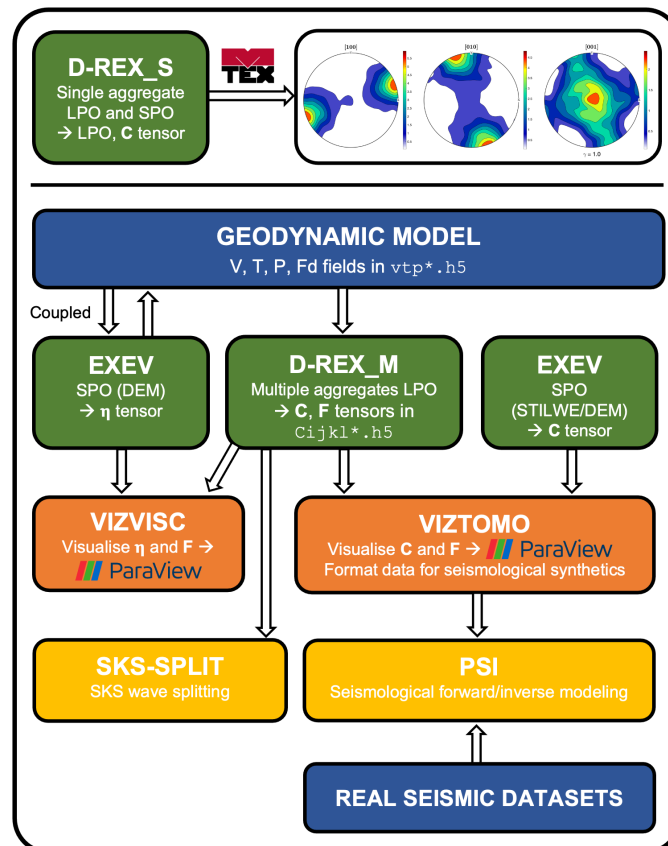


Figure 1. ECOMAN structure and flow chart. Coloured boxes denote programs that compute rock fabrics (green), post-process the elastic (C), viscous (η) and deformation gradient (F) tensors for visualisation and/or data formatting for seismological synthetics (orange), and perform seismological forward/inverse modelling on synthetic or real datasets (yellow). Input data are from geodynamic modelling or real



112 seismic datasets (blue). Visualisation of the mechanical properties and LPO can be done with the MTEX MATLAB toolbox for single crystal
113 aggregates or the software ParaView for large-scale simulations.

114

115 **2.1 Rock fabrics and mechanical properties simulations**

116 The evolution of the strain-induced LPO can be simulated for a single (D-REX_S) or multiple (D-REX_M) two-mineral phase
117 mantle aggregates. Five two-mineral phases mantle aggregates can be defined as a function of depth or density ρ (see Table 1
118 for a list of abbreviations and physical properties):

119

- 120 1) **olivine + enstatite**, for the upper mantle (UM: 0-410 km or $3000 < \rho \leq 3650 \text{ kg/m}^3$);
- 121 2) **wadsleyite** + majoritic garnet, for the upper mantle transition zone (UTZ: 410-520 km or $3650 < \rho \leq 3870 \text{ kg/m}^3$);
- 122 3) ringwoodite + majoritic garnet, for the lower mantle transition zone (LTZ: 520-660 km or $3870 < \rho \leq 4150 \text{ kg/m}^3$);
- 123 4) **bridgmanite** + ferropericlase, for the lower mantle (LM: 660-2900 km or $\rho > 4150 \text{ kg/m}^3$);
- 124 5) **post-perovskite** + ferropericlase, for the bottom of the lower mantle according to the phase boundary from Oganov
125 and Ono (2004).

126

127 The strain-induced LPO is computed for the phases in bold, while other major phases such as garnet, ringwoodite and
128 ferropericlase are considered to be isotropic and their distribution is set to be random. Thus, no LPO is computed for the LTZ,
129 such that (minor) anisotropy arises only when SPO modelling due to compositional layering is active (section 2.1.3; Faccenda
130 et al., 2019). The full elastic tensor is then calculated according to the crystal orientation, volume fraction, phase abundance,
131 P-T conditions, bulk rock composition, and using Voigt-Reuss-Hill averaging schemes (see section 2.1.2 for more details).

132 The elastic properties related to strain/stress-induced SPO fabrics can instead be calculated at the grain- or rock-scale and for
133 layered or two-phase (matrix-ellipsoidal inclusions) systems using the isotropic elastic moduli of the different (fluid, mineral,
134 rock) components (EXEV).

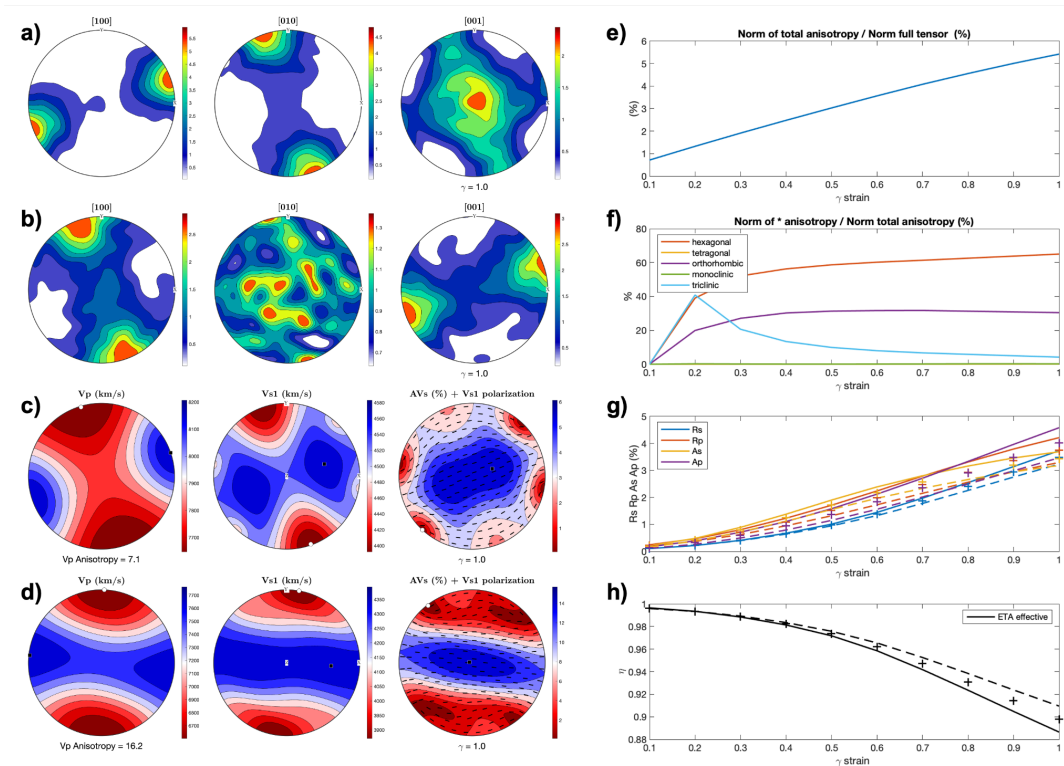
135 The elastic properties and density of the aggregates characterised by LPO and/or SPO fabrics are estimated at relevant mantle
136 P-T conditions using the single crystal elastic moduli and their P-T derivatives for the main mineral phases and compiled from
137 different mineral physics studies, together with lookup tables of the isotropic elastic moduli, density and mineral phase volume
138 fraction generated with MMA_EoS (Chust et al., 2017) for five bulk rock compositions (dunite, harzburgite, pyrolite, MORB,
139 pyroxenite) and in the $T = 300 : 50 : 4500 \text{ K}$, $P = 0 : 0.1 : 140 \text{ GPa}$ range.

140 **2.1.1 D-REX_S**

141 D-REX_S is a program designed for modelling the evolution of strain-induced LPO fabrics and related elastic properties of a
142 single, two-mineral phases mantle aggregate, as a function of the imposed flow field, amount of strain, crystal plasticity, P-T



143 conditions and additional effects related to SPO fabrics. It builds on the original D-REX software (Kaminski et al., 2004) for
 144 modelling the strain-induced LPO, and it includes MATLAB scripts to generate pole figures of the LPO and
 145 isotropic/anisotropic seismic properties with the MTEX software (Mainprice et al., 2011) (Fig. 2a-d), together with the
 146 possibility to display the evolving fabric strength (M-index, J-index) and the fraction of different anisotropy components
 147 (obtained via tensor decomposition; Browaeys et al., 2004; Fig. 2e-h).
 148 D-REX_S is particularly useful for those users who are not familiar with LPO modelling, and more in general, to anyone
 149 interested in performing parameter sensitivity tests on different mantle mineral aggregates before launching large-scale
 150 simulations. In addition, the microstructures generated with D-REX_S can be used in the D-REX_M 2D-3D simulations to
 151 impose pre-existing (e.g., fossil) fabrics on multiple crystal aggregates located within a specific subdomain (see section 2.1.2).
 152



153
 154 **Figure 2.** D-REX_S output for an upper mantle aggregate (Ol:Opx=70:30) subjected to a simple shear deformation of 1. Pole figures of the
 155 olivine (a) and orthopyroxene (b) crystallographic axes; (c) pole figures of Vp, Vs1, AVs = $200(Vs1 - Vs2)/(Vs1 + Vs2)$ with superimposed
 156 Vs1 polarisation directions evaluated from the elastic tensor of the two phase aggregate. (d) same as (c) but with the superimposed effect of
 157 an SPO fabric due to 5% melt-filled cracks aligned at -30° from the principal stress (i.e., at 15° from the horizontal plane); (e) fraction of
 158 total anisotropy relative to the full elastic tensor and (f) contribution of 5 anisotropic classes relative to the total anisotropy; (g) P- and S-
 159 wave radial and azimuthal anisotropy and (h) eta parameter = $F/(A-2L)$ for the elastic tensors computed with the Voigt (continuous lines),
 160 Reuss (dashed lines) and Hill (crosses) averaging schemes, respectively.

161



162 2.1.2 D-REX_M

163 D-REX_M is a program that computes the evolution of the LPO and related elastic properties of multiple, two-mineral phases
164 mantle aggregates, as a function of the single crystal plastic and elastic properties, and of the flow field, deformation
165 mechanisms and P-T conditions resulting from 2D-3D geodynamic simulations. It builds on the original D-REX software,
166 which estimates the strain-induced LPO and elastic properties (i) for upper mantle polycrystalline aggregates only, (ii) using
167 single crystal elastic tensors derived at room P-T conditions and averaged using a Voigt scheme, (iii) in a 2D cartesian domain,
168 (iv) assuming steady-state flow, and (v) whereby the whole deformation is considered to be accommodated by dislocation
169 creep assisted by grain-boundary sliding (Kaminski et al., 2004). D-REX_M additionally models:

- 170 • fabrics relevant to the mid and lowermost mantle (Faccenda, 2014), including those with post-perovskite. Phase
171 transitions can be set to occur at predefined depths (e.g., 410 km, 660 km). Density crossovers (which allow modelling
172 the deflection of phase boundaries with a non-null Clapeyron-slope; Fig. 5), and parameterized phase boundaries as
173 for the case of post-perovskite (Oganov and Ono, 2004) are also included;
- 174 • elastic properties and density as a function of the bulk rock composition and local P-T conditions (Faccenda, 2014,
175 Chang et al., 2016, Ferreira et al., 2019). The isotropic component of the elastic tensors and density are taken from
176 the lookup tables generated by MMA-EoS for a given mantle lithology, and the anisotropic component from the
177 mineral single crystal elastic moduli and their pressure and temperature derivatives. This strategy ensures a gradual
178 transition of the seismic properties at phase boundaries where phase transformations occur. Voigt-Reuss-Hill
179 averaging schemes of the elastic moduli are included;
- 180 • non steady-state flows in 2D/3D cartesian and polar grids (Faccenda and Capitanio, 2012, 2013, Hu et al., 2017; Zhou
181 et al., 2018; Lo Bue et al., 2022; Faccenda and VanderBeek, 2023). The global-scale models are spatially discretized
182 using the so-called Yin-Yang grids (Kageyama and Sato, 2004). Several examples (cookbooks) are provided on how
183 to use the software in different coordinate systems and in steady-state or time-dependent flow conditions;
- 184 • fabric evolution in the presence of multiple creep mechanisms. At any time step, the fraction of deformation
185 accommodated by dislocation creep in a given point of the geodynamic model defines the fraction of time spent for
186 intracrystalline deformation assisted by grain-boundary sliding. The remaining time is used to apply, when present,
187 fluid deformation rotation to the whole crystal aggregate (e.g., Hedjazian et al., 2017);
- 188 • a pre-existing (fossil) fabric (pre-computed with D-REX_S) within a subdomain, typically the lithosphere. This is
189 often the case for geodynamic models where the lithosphere accretion is not modelled, and its geometry is initially
190 prescribed;

191

192 The D-REX_M input files should contain information about the geodynamic model evolution. Critical information are the
193 components of the velocity vector \mathbf{V} field, and, for time-dependent flow models, the total elapsed time and timestep. These are



194 used to compute the velocity gradient tensor, and the LPO evolution and advection of the crystal aggregates. Additional fields
195 defined on the cartesian/spherical grid that can be included in the input files are:

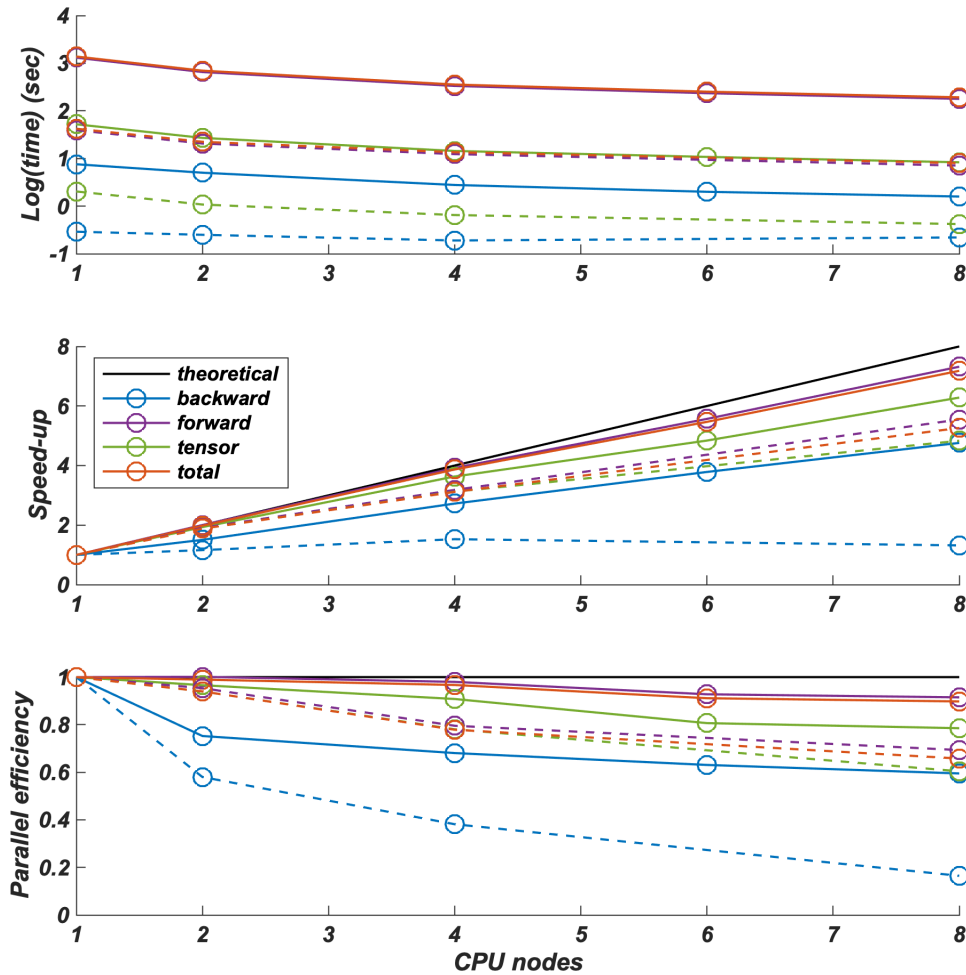
- 196 • when the geodynamic model is thermo-mechanical, the temperature T and total pressure P fields, which can be used
197 to compute the single crystal elastic tensor and aggregate phase transitions as a function of the local P - T conditions;
- 198 • when the rheological model of the geodynamic simulation is based on multiple visco-plastic deformation
199 mechanisms, the fraction of deformation accommodated by dislocation creep $F_d = \eta_{\text{disl}}/\eta_{\text{eff}}$, where $0 \leq F_d \leq 1$,
200 η_{disl} is the viscosity calculated with the dislocation creep flow law, η_{eff} is the effective viscosity calculated with the
201 harmonic average of each of the viscosities representing a different deformation mechanism.

202

203 Summarising, the time and the velocity field \mathbf{V} are essential information, while the P , T , F_d fields are optional and depend on
204 the type of (mechanical vs. thermomechanical) geodynamic and (single vs. multiple visco-plastic deformation mechanisms)
205 rheological models.

206 While the \mathbf{V} , P , T , F_d fields are defined on the Eulerian grid, the distribution, size, modal composition and mechanical
207 properties of mantle aggregates are defined on the Lagrangian particles. After initialising the Eulerian grid and Lagrangian
208 particles, the entire run consists of three main steps: (i) backward advection of the particles; (ii) forward advection and update
209 of the LPO and deformation gradient tensor \mathbf{F} ; (iii) computation of the full elastic tensor and creation of the output file. The D-
210 REX_M output file(s) includes, for each mineral aggregate, the elastic tensor \mathbf{C} , density, and the deformation gradient tensor
211 \mathbf{F} . These properties can be then processed and visualised with the software VIZTOMO (section 2.2.1).

212 D-REX_M is parallelized using a hybrid MPI and OpenMP scheme to take advantage of multiple CPUs architectures of
213 modern HPC clusters. Runtime is obviously affected by the number of crystal aggregates, number of crystals per aggregate
214 and of active slip systems per crystal, and number of timesteps (Fig. 3, top). The parallel efficiency ranges 70-90%, and the
215 update of the LPO and \mathbf{F} tensor during forward advection is the most time-consuming part of the run (Fig. 3, centre, bottom).
216 The small performance degradation is due to the initialization of the Eulerian/Lagrangian grids and arrays, and to I/O operations
217 which are executed serially within each process. As a result, the efficiency of the time-dependent flow models is lower than
218 that of steady-state models, as the latter only require a single velocity (and P , T , F_d) field to be loaded and processed.



219
220

221 **Figure 3.** Runtime (top), speedup (centre) and parallel efficiency (bottom) of D-REX_M for initial backward advection of aggregates
 222 (“backward”), forward advection and updating of the LPO and \mathbf{F} tensor (“forward”), full elastic tensor computation and output file creation
 223 (“tensor”), and entire run (“total”). Results are shown for two models included in the cookbooks: the 3Dspherical_global model (steady-
 224 state flow, 96 timesteps, 1327606 aggregates, LPO computed only for 260474 upper mantle aggregates) and the 3Dspherical_sinkingslab
 225 model (dashed lines; time-dependent flow, 20 timesteps, 38509 aggregates, LPO computed for 25177 upper mantle and 6587 upper mantle
 226 transition zone aggregates). Runs performed on a HPE Superdome Flex (8 CPUs, 28 cores Intel Xeon(R) PLATINUM 8180 @ 2.50GHz)
 227 using from 1 to 8 nodes.

228

229 2.1.3 EXEV

230 EXEV includes routines to compute the EXtrinsic Elastic and Viscous anisotropy using Effective Medium Theory modelling
 231 for a multi-component layered system (Smoothed Transversely Isotropic Long-Wavelength Equivalent, STILWE; Backus,
 232 1962) or a two-component system with similar ellipsoidal inclusions in a uniform background matrix (Differential Effective
 233 Medium, DEM; e.g., Mainprice, 1997).



234 The elastic tensor \mathbf{C} due to SPO fabrics can be either estimated independently or, when using the DEM approach, superimposed
235 on that obtained from the strain-induced LPO modelling. SPO fabrics that can be modelled are those related to rock- or grain-
236 scale layering (e.g., Faccenda et al., 2019), or to the presence of preferentially aligned ellipsoidal inclusions (e.g., melt-/fluid-
237 filled cracks). The user then needs to specify:

- 238 • for grain-scale layered fabrics, a dominant ultramafic or mafic lithology. In this case the mineral phase proportions
239 from the MMA-EoS lookup tables define the mixture for the STILWE model;
- 240 • for rock-scale layered fabrics, the relative abundance of the five available ultramafic-mafic lithologies (dunite,
241 harzburgite, pyrolite, basalt and pyroxenite) defining the mixture for the STILWE model;
- 242 • for matrix-inclusion fabrics, the elastic tensors of the two components and the inclusion's shape and volume fraction
243 as required by the DEM modelling. The matrix elastic tensor can be replaced with that from the LPO modelling in
244 order to estimate the combined effect of LPO and SPO fabrics.

245 The SPO fabrics can then be oriented at any angle relative to the principal Finite Strain Ellipsoid (FSE) axis or, in case of
246 cracks, the local principal stress obtained from the “present-day” (i.e., last) velocity field.

247 Summarising, SPO fabric modelling requires one or more of the following: \mathbf{F} and/or \mathbf{C} obtained from D-REX_M; \mathbf{P} , \mathbf{T} and/or
248 \mathbf{V} and/or fluid/melt fraction fields for the “present-day” state of the geodynamic model. Consequently, this modelling is
249 performed when post-processing the D-REX_M output with the software VIZTOMO (see section 2.2.1).

250 The total or deviatoric component of the viscous tensor $\boldsymbol{\eta}$ due to SPO fabrics is estimated for two-phase systems with ellipsoidal
251 weak/hard inclusions using the DEM theory, and the parametrization of the viscous tensor evolution and orientation as a
252 function of the cumulated deformation (\mathbf{F}) obtained following de Montserrat et al. (2022). Indeed, most if not all, mantle levels
253 are composed of two main mineral phases that control both the elastic and viscous properties. The case of a multi-component
254 layered medium is not considered because its viscous tensor can be either approximated with flat inclusions, or more simply
255 computed using the Voigt and Reuss averages of the layers' isotropic viscosity.

256 The first modelling phase requires running subprogram DEMviscous to generate a database of viscous tensors for a range of
257 inclusion shapes and volume fractions, and inclusion-matrix viscosity contrasts. The latter implies that the viscous moduli are
258 dimensionless and can therefore be interpreted as scaling factors with respect to an isotropic effective viscosity of the bulk
259 rock or most abundant mineral phase. Subsequently, the database can be exploited by large-scale geodynamic simulations to
260 either (i) return the viscosity tensor $\boldsymbol{\eta}$ from a look-up table for every point of the computational domain, which can be
261 superimposed on the isotropic effective viscosity computed from flow laws (coupled mechanical simulations), or (ii) estimate
262 $\boldsymbol{\eta}$ (uncoupled mechanical simulation) and/or visualise its anisotropic viscous properties for the “present-day” state of the
263 geodynamic model with the software VIZVISC (section 2.2.2).

264



265 2.2 Visualisation of the mechanical properties and data formatting in preparation for seismological synthetics

266 2.2.1 VIZTOMO

267 VIZTOMO processes the D-REX_M output for the visualisation of the aggregates' elastic and deformational history properties.
268 Estimation of extrinsic anisotropy effects via the EXEV routines is possible at this stage. The properties of the **C** and **F** tensors
269 can be determined either at the position of the Lagrangian mantle aggregates, or, in case of the elastic properties and density,
270 interpolated to a structured (tomographic) grid. In the latter case the grid can be saved in a format suitable for generating
271 synthetic seismic datasets via the PSI_D package (see section 2.3.2) or for 3D waveform simulations in SPECFEM
272 (Komatitsch and Tromp, 1999).

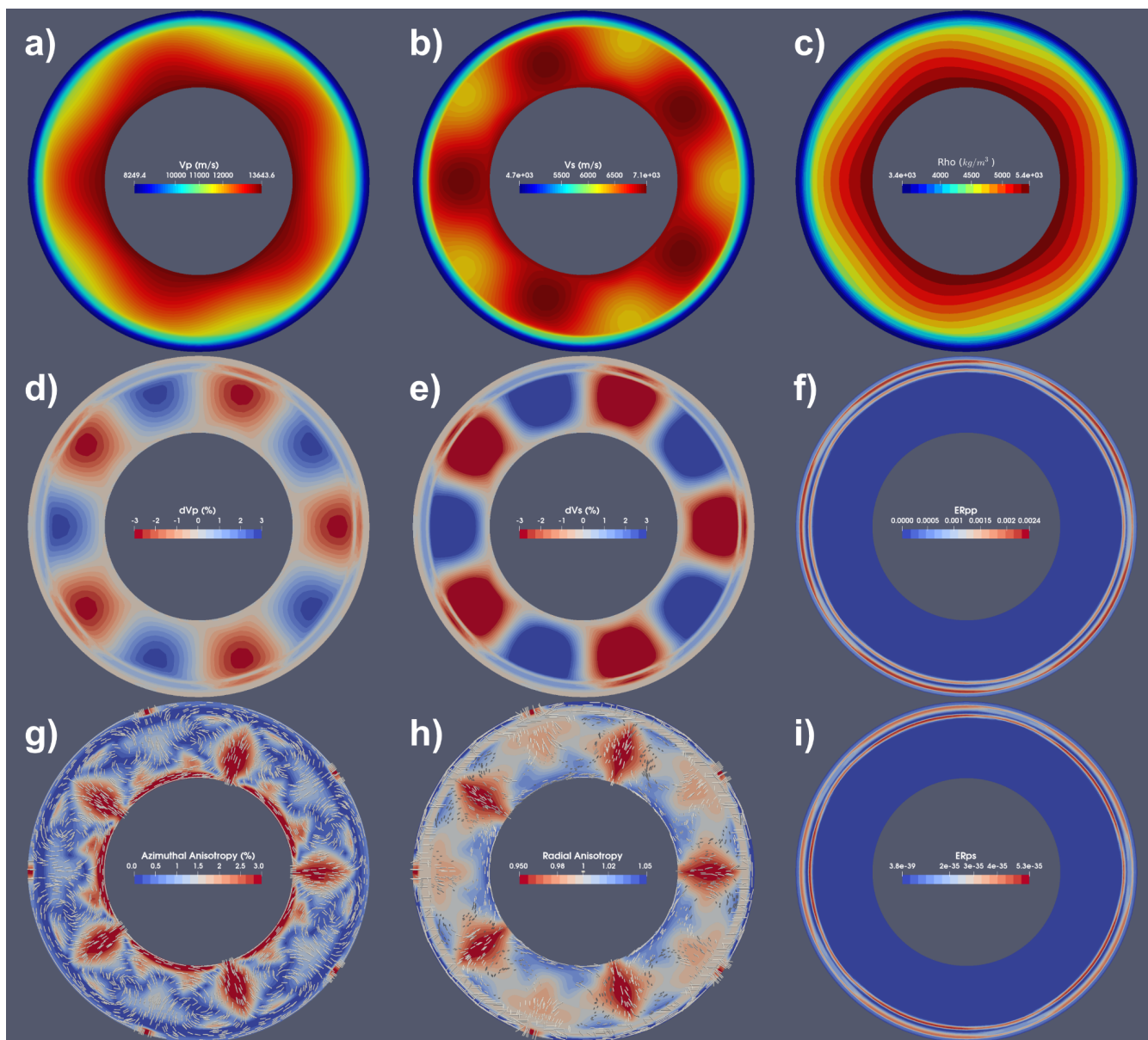
273 Several properties of the elastic tensor **C** can be visualised:

- 274 • Isotropic or ray-path dependent velocity anomalies and anisotropic elastic properties of body-waves (i.e., P-wave
275 anisotropy and direction of maximum P-wave velocity; direction and magnitude of maximum S-wave splitting delay
276 time; S-wave radial and azimuthal anisotropy);
- 277 • reflection/transmission energies resulting from the whole range of P-S conversions occurring at discontinuities (useful
278 for studies based on receiver function analysis);
- 279 • the fraction of the elastic tensor anisotropic component relative to the total and the relative contributions of five
280 different anisotropy classes (hexagonal, orthorhombic, tetragonal, monoclinic, triclinic) obtained through elastic
281 tensor decomposition (Browaeys et al., 2004);
- 282 • the orientation of the hexagonal symmetry axis (already present in the original D-REX).

283 The deformation history stored in **F** can be visualised in terms of the FSE shape and orientation and/or length or orientation of
284 its minimum and maximum semi axes.

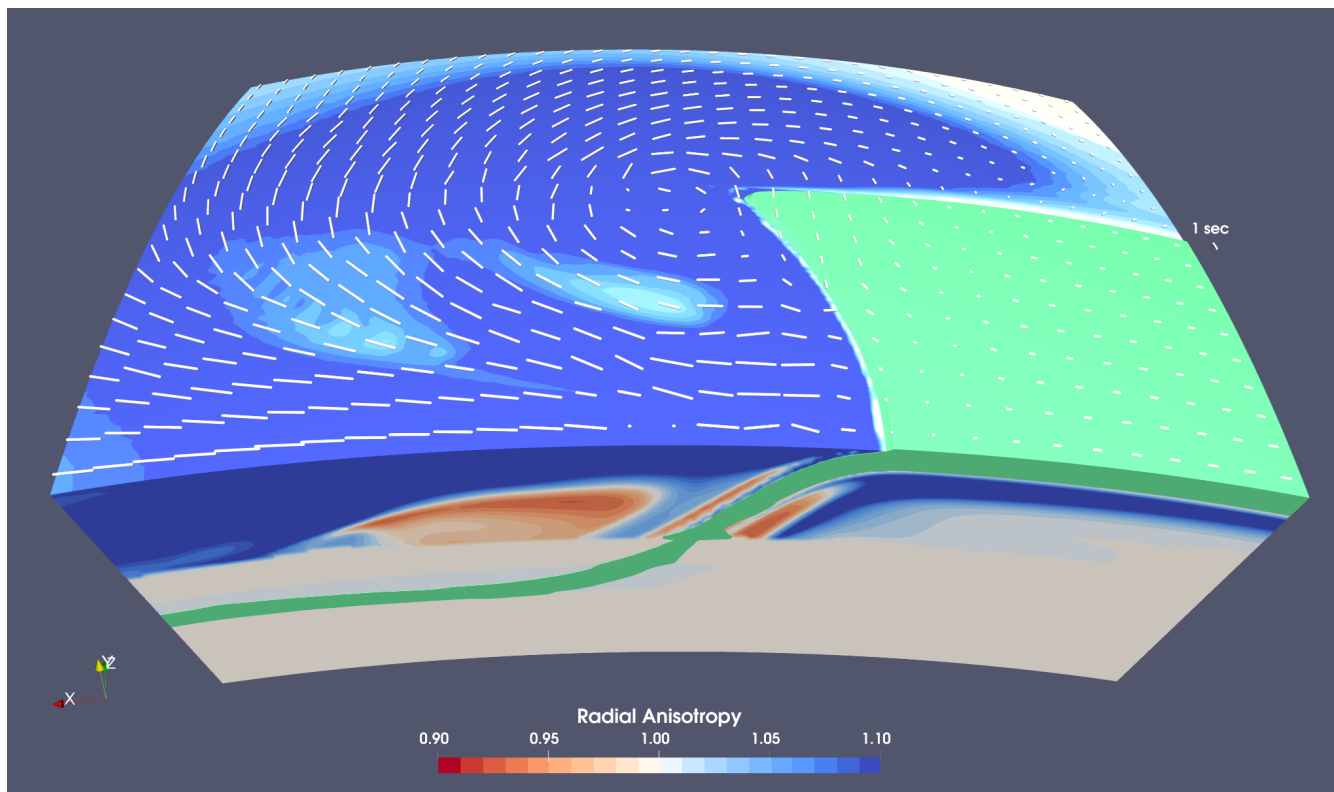
285 The different fields are saved in specific file formats which can be imported by the open source ParaView software (Ahrens et
286 al., 2005) for visualisation. Figures 4, 5, 6, 7 display some of these fields computed for different geodynamic models.

287



288

289 **Figure 4.** VIZTOMO output for the model 2Dpolar_convection available in the cookbooks. (a,b) isotropic Vp and Vs (m/s); (c) density;
290 (d,e) isotropic P- and S-wave anomalies; (g) azimuthal anisotropy and FSE semi-axis (white bars); (h) radial anisotropy and TTI axis (white
291 bars); (f,i) P-P and P-S reflection energy for waves propagating upward.



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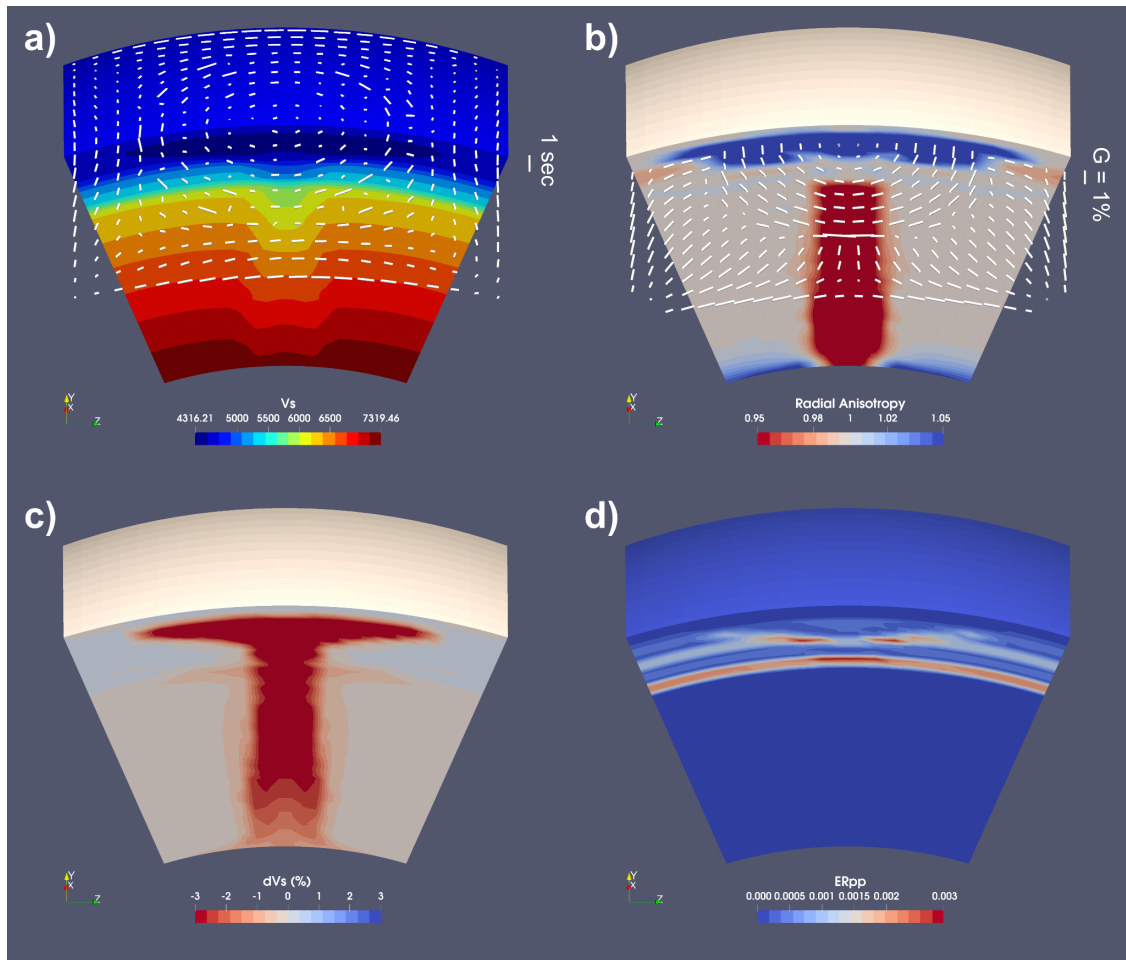
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Figure 5. VIZTOMO output for a 3D model of oceanic plate subduction and roll back in spherical coordinates. Fabrics computed with D-REX_M for only upper mantle aggregates. A fossil A-type olivine fabric with the fast axis parallel to plate motion and computed with D-REX_S is initially defined within the oceanic plate volume. The colour scale indicates radial anisotropy in the upper mantle, and the white bars the SKS splitting computed with SKS-SPLIT. The volume in green encloses material with a +2% P-wave anomaly (i.e., the oceanic plate). Note the apparently thicker slab portion around the 410 km depth discontinuity, due to the upwelling of the olivine-spinel phase transition. The model domain extends from 0-1000 km along the radial direction, 85°-115° along longitude, and 70-90° along colatitude.

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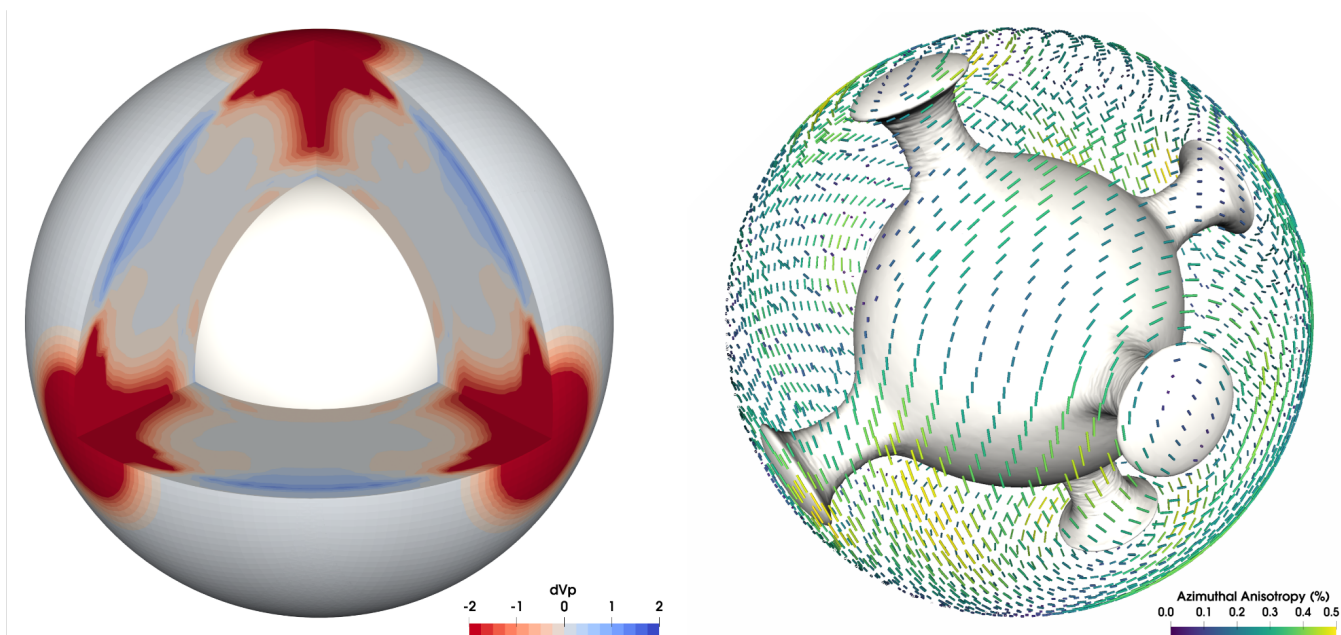
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Figure 6. VIZTOMO output for an upwelling plume toy model in spherical coordinates. a) absolute V_s (m/s) and SKS splitting computed with SKS-SPLIT (white bars); b) radial anisotropy (colour scale) and azimuthal anisotropy at 200 km depth (white bars); c) isotropic V_s anomaly; d) P-P reflection energy for a wave propagating upward. The model domain extends from 0-2900 km along the radial direction, 70° - 110° along longitude, and 70° - 110° along colatitude.



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Figure 7: VIZTOMO output for the model 3Dspherical_global available in the cookbooks. Isotropic P-wave anomaly (left) and azimuthal anisotropy at 200 km depth (right). The grey surface encloses material hotter than the surrounding.

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311 2.2.1 VIZVISC

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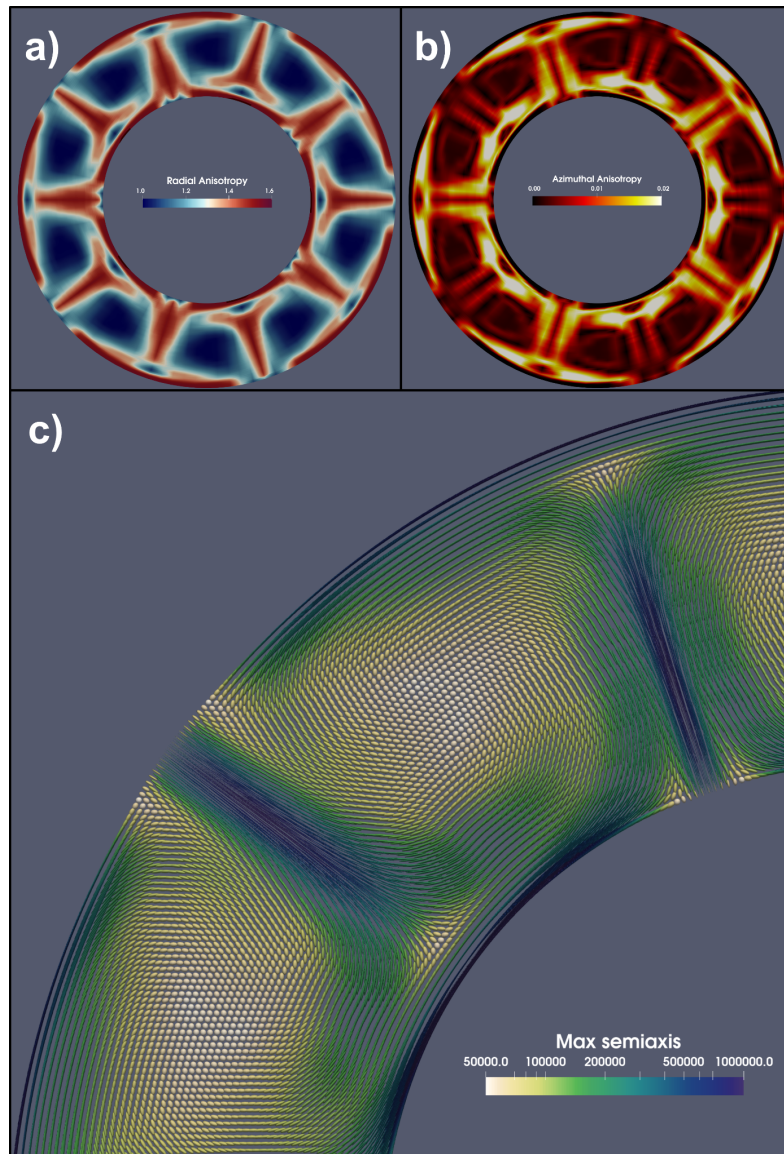
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VIZVISC processes the D-REX_M output for the visualisation of the aggregate properties such as the viscous anisotropy and related deformational history (in terms of the FSE) in ParaView. The deviation from isotropy is evaluated by computing the radial and azimuthal components of viscous anisotropy in a similar way as for the elastic tensor. More in detail, radial viscous anisotropy is defined as $\xi = N/L$, while azimuthal viscous anisotropy is defined by the magnitude $G = \sqrt{Gc^2 + Gs^2}$ and azimuth $\phi = \tan^{-1}(Gs, Gc)$, where $N = \frac{1}{8}(\eta_{11} + \eta_{22}) - \frac{1}{4}\eta_{12} + \frac{1}{2}\eta_{66}$, $L = \frac{1}{2}(\eta_{44} + \eta_{55})$, $Gc = \frac{1}{2}(\eta_{55} - \eta_{44})$, $Gs = \eta_{45}$. Radial and azimuthal viscous anisotropy are evaluated in the FSE (and thus inclusions) reference frame, whereby the minor semi axis is oriented along the vertical direction, and the intermediate and major semi axes are in the horizontal plane. As such, radial anisotropy is always ≥ 1 . Figure 8 displays some of these fields computed for a 2D steady-state model of mantle convection with periodic upwellings and downwellings.



321

322 **Figure 8.** VIZVISC output for the model 2Dpolar_convection available in the cookbooks. (a) Radial viscous anisotropy; (b) azimuthal
323 viscous anisotropy; (c) FSE shape coloured by the length of its major semi-axis upscaled by a factor of 50 km.

324

325 2.3 Seismic forward and inverse modelling

326 2.3.1 SKS-SPLIT

327 SKS-SPLIT estimates the SKS splitting at a grid of virtual seismic stations placed at the top of the D-REX_M model as a
328 function of the back-azimuth using the Fortran routines included in FSTRACK (Schulte-Pelkum and Blackmann, 2003; Becker



329 et al., 2006). The routines have been adapted to load the D-REX_M output, stack the elastic tensors and densities in an upper
330 mantle rock column beneath each virtual seismic station (Faccenda and Capitanio, 2013), and run in parallel using MPI. The
331 averaged fast azimuth scaled by the delay time can then be visualised in ParaView as shown in Figures 5 and 6a.

332 2.3.2 PSI

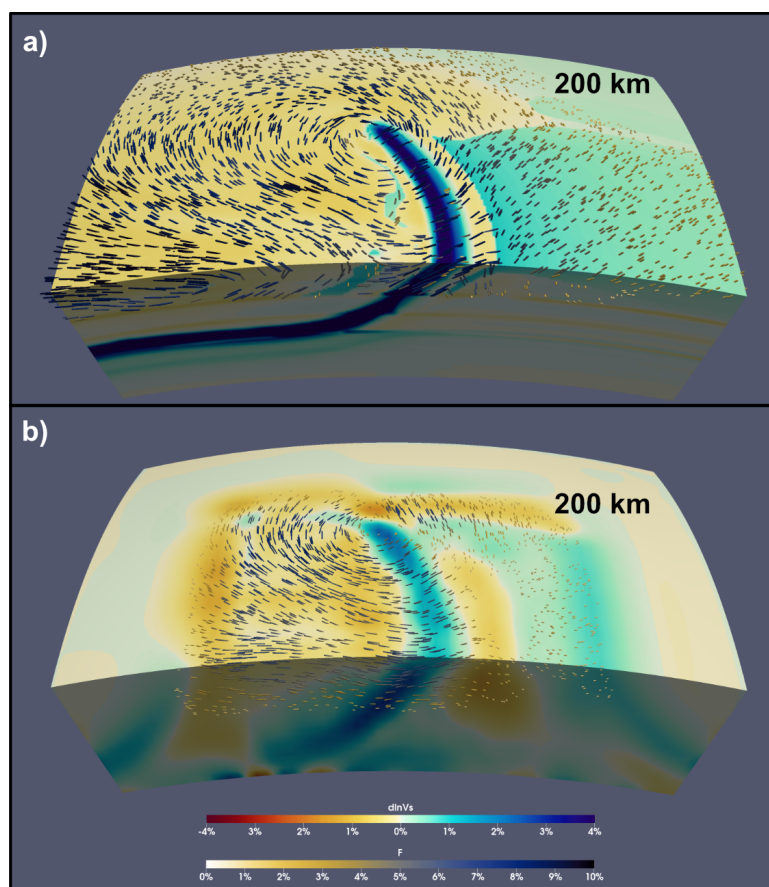
333 PSI (Platform for Seismic Imaging) is a Julia package for performing tomographic inversion of both real and synthetic seismic
334 datasets. In the context of the ECOMAN software, it's a useful tool for exploring how features in high-resolution geodynamic
335 simulations are mapped into lower resolution seismic tomography models; this is a critical step if one aims to evaluate
336 geodynamic results against existing tomographic images.

337 PSI can be used to forward model P and S travel-times, splitting intensity (Chevrot, 2000), and shear wave splitting parameters
338 (i.e. the fast-polarisation azimuth and the delay time between the fast- and slow-polarised waveforms). Forward modelling of
339 these seismic observables is supported for three different model parameterizations: (1) isotropic P- and S-wavespeeds, (2)
340 hexagonally anisotropic media defined by the 5 Thomsen parameters and the azimuth and elevation of the symmetry axis, and
341 (3) fully anisotropic models defined by the density-normalised 21-component elastic tensor which can be generated from D-
342 REX_M + VIZTOMO (sections 2.1.2 and 2.2.1). Seismic phase velocities are computed following Thomsen (1986) for
343 hexagonally anisotropic models while the Christoffel equations are solved when the elastic tensor parameterization is used.
344 Anisotropic travel-times and splitting intensities for arbitrarily polarised S-waves are computed following VanderBeek et al.
345 (2023) using a long-wavelength approximation in which the accumulated delay time between fast- and slow-polarised qS-
346 waves is less than their dominant period. Lastly, splitting parameters are predicted using the matrix propagation method of
347 Rumpker and Silver (1998). In this initial release of PSI, all predictions are made via integration along ray paths traced through
348 a user-defined 1D reference velocity model using the TauP Toolkit (Crotwell et al. 1998). The 3D model properties are
349 subsequently interpolated to these paths before computing the seismic observables. We anticipate releasing an update to the
350 package that includes both 3D anisotropic ray tracing and finite-frequency kernels that are currently under development.

351 Travel-time and splitting intensity datasets can be inverted individually and jointly either for isotropic (V_p and V_s) or
352 hexagonally anisotropic model parameters. Hexagonal anisotropy is defined by up to five free parameters, the isotropic (1) P-
353 and (2) S-velocity, (3) anisotropic magnitude, and the (4) azimuth and (5) elevation of the hexagonal symmetry axis. Only a
354 single anisotropic magnitude parameter is required because the strength of P and S anisotropy is strongly correlated (e.g.,
355 Becker et al., 2006). Consequently, the ratios between the three Thomsen parameters (ϵ , δ , γ ; Thomsen 1986) and the inverted
356 anisotropic magnitude parameter must be chosen *a priori* and can be spatially variable. Source and receiver statics for each
357 observation and seismic phase type may also be included as free parameters. The tomographic model is obtained by iteratively
358 solving a system of linearized equations relating the perturbations in the inversion parameters to the data residuals augmented
359 with damping and smoothing constraints. The solution is obtained via the LSQR algorithm (Paige & Saunders, 1982). Full
360 details on the tomographic method can be found in VanderBeek and Faccenda (2021) and VanderBeek et al. (2023). The final
361 tomographic solution is written to a VTK file to be visualised in ParaView. Tomographic inversions can be run from a



362 workstation. For problems consisting of $\sim 1e4$ observations and $\sim 1e5$ parameters, solutions can be obtained within ~ 10 minutes
363 (less for isotropic inversions).
364 The PSI inversion methodology has been tested on synthetic models of oceanic plate subduction, intra-oceanic upwelling
365 plume, spreading oceanic ridge, and Central-Eastern Mediterranean subduction (VanderBeek and Faccenda, 2021; Lo Bue et
366 al., 2022, VanderBeek et al., 2023; Faccenda and VanderBeek, 2023), and applied to the isotropic and anisotropic imaging of
367 the Central Mediterranean (Rappisi et al., 2022) and of the Mt. Etna volcanic field (Lo Bue et al., 2023). In Figure 9, we
368 illustrate results obtained from a synthetic inversion of direct teleseismic P- and S-wave relative travel-times computed through
369 the subduction zone shown in Figure 5. Synthetic data were computed using the full 21-component elastic tensor while the
370 inversion was performed for the best-fit hexagonal anisotropic parameters. We considered an array of 770 receivers extending
371 from $\pm 7.5^\circ$ in longitude and $\pm 11.5^\circ$ in latitude (~ 75 km spacing) that recorded 16 events; 8 at a range 50° and another 8 at 80°
372 from the origin of the subduction zone model and equally distributed in back-azimuth. This example is included in the PSI
373 package.



374
375 **Figure 9.** Synthetic tomography results obtained from PSI. (a) Target anisotropic model generated from VIZTOMO. (b) Recovered
376 anisotropic model obtained by inverting synthetic teleseismic P and S (relative) delay times computed from the model in (a). In both panels,
377 the isotropic S-wave velocity perturbations are computed with respect to the far-field 1D velocity profile. Quivers parallel the hexagonal



378 symmetry axis and are scaled and coloured by the anisotropic strength. The top surface shown is located at 200 km depth while the full
379 model extends from 0-1000 km along the radial direction, 85°-115° along longitude, and 0-20° along latitude.

380 **3 Discussion**

381 **3.1 Software advantages**

382 When compared to other similar software, ECOMAN (i) aims at being a more versatile package suitable for any geodynamic
383 simulations (2D and 3D; cartesian and polar coordinate systems; regional and global settings), (ii) takes into account the time-
384 dependent deformational history of the mantle (which is usually not steady-state, especially close to plate boundaries), (iii)
385 predicts the strain-induced fabric and elastic tensor of different mantle layers (i.e., not only the upper mantle), (iv) includes
386 Effective Medium Theories (STILWE, DEM) and a parametrization of the fabric evolution of two-phase composites to predict
387 elastic and viscous extrinsic anisotropy, (v) generates realistic grid structure distributions of mantle elastic properties to be
388 used for forward/inverse seismological modelling (e.g., PSI, SPECFEM3D), and (vi) performs synthetic seismic inversions
389 (e.g., P- and S-wave travel-time tomographies, S-wave splitting intensities) within the computational domain, which facilitates
390 the comparison with other tomographic models and the estimation of apparent anomalies (artefacts) due to, for example,
391 unaccounted-for elastic anisotropy (Bezada et al., 2016; VanderBeek and Faccenda, 2021; VanderBeek et al., 2023) and/or
392 regularisation.

393 **3.2 Software (real or potential) limitations**

394 D-REX_S and D-REX_M compute the strain-induced LPO for the most abundant and highly anisotropic mineral phases, while
395 assuming random orientation for several secondary phases that instead could contribute substantially to the aggregate
396 anisotropic properties. For example, cubic ferropericlase is relatively abundant (< 20%) and becomes highly anisotropic in the
397 lower half of the lower mantle ($A_{vs} = 30\text{-}50\%$), such that it could dominate seismic anisotropy at these depths (Marquardt et
398 al., 2009). Davemaoite (Ca-perovskite) is also a highly anisotropic mineral with cubic symmetry ($AV_s = 25\text{-}15\%$, Kawai and
399 Tsuchiya, 2015) but its model abundance is quite low (< 10%). Recently, micromechanical simulations of strain-induced LPO
400 in aggregates with a pyrolite mantle composition have shown that the bulk aggregate seismic anisotropy is controlled by
401 bridgmanite and post-perovskite, while the cubic secondary phases appear to only slightly reduce the amplitude of anisotropy
402 (Chandler et al., 2021). The latter effect can thus be well approximated by randomising the orientation of the cubic phases as
403 assumed here.

404 A main limitation of ECOMAN is that it does not include yet the modelling of viscous anisotropy due to the intrinsic
405 mechanical anisotropy of crystals. Tommasi et al. (2009), have used VPSC simulations to show that olivine CPO in the
406 lithosphere can control the reactivation of fossil faults misoriented with respect to the stress field. Kiraly et al (2020), employed
407 the modified director method (MDM) and estimated up to 1 order of magnitude of intrinsic viscous anisotropy in olivine
408 aggregates, which can control the kinematics and dynamics of tectonic plates. Both the VPSC and MDM approaches are



409 computationally expensive and appear to be prohibitive for the number of mantle aggregates required to discretize the mantle
410 domain of large-scale 3D simulations. An alternative approach which minimises the computational time is therefore desired.
411 A minor limitation is that the different code modules are based on different programming languages (Fortran, Julia), libraries
412 (OpenMP, MPI, HDF5) and software (MATLAB, ParaView), whose installation on local devices might discourage potential
413 users. There are a few main reasons for this. First of all, the original D-REX software was written in Fortran, thus its
414 modifications into D-REX_S and D-REX_M software was more straightforward by maintaining the same programming
415 language. Fortran has high performance standards on HPC clusters, often if not always higher than other high-level
416 programming languages (e.g., MATLAB or Python). Given the large-scale computational power needed for the D-REX_M
417 simulations, especially those with 100.000s or millions of crystal aggregates, and considering that the required compilers and
418 libraries are routinely installed in most (if not all) HPC clusters, the usage of the ECOMAN's Fortran-based applications in
419 high-performance environments is warranted. In contrast, the visualisation of the Fortran-based applications' output in
420 MATLAB and ParaView can be performed on local devices. In particular, the MTEX software is a MATLAB toolbox for
421 visualisation of the LPO and elastic tensor pole figures which should be downloaded ([https://mtex-
422 toolbox.github.io/download](https://mtex-toolbox.github.io/download)) and installed along with MATLAB only when using D_REX_S. Seismic forward/inverse
423 modelling with PSI can be performed on either a HPC cluster or local devices upon installation of the Julia package. Julia was
424 chosen because it's an open-source and high-level language that offers a number of performance benefits over other popular
425 scientific computing languages such as Python or Matlab. It is important to stress that for any of these applications the user
426 only needs to modify input text files, and thus no particular prerequisite or computational skill is required.
427 Finally, running D-REX_M requires allocating ~ 160 GB of memory per million of crystal aggregates with 1000 x 2 crystals
428 each. This potential problem can be addressed by distributing the computational and memory load over several CPUs, which
429 is possible thanks to the hybrid MPI and OpenMP parallelization scheme.

430 **4 Conclusions and outlook**

431 ECOMAN is an open-source software package for estimating strain/stress-induced fabrics in mantle aggregates, their
432 mechanical properties, and how mechanical anisotropy affects the geodynamic evolution and seismic imaging of the Earth's
433 interior. Programs included in ECOMAN are portable across different HPC and local device systems (provided the Julia
434 package and Fortran compilers are available), and are applicable to any 2D-3D geodynamic simulation. Computationally
435 expensive programs such as D-REX_M are parallelized, offering a nearly perfect scaling with an increasing number of cores.
436 As a result, the strain-induced fabrics of millions of mantle aggregates can now be estimated with a reasonable amount of time
437 and computational resources.

438 **As ongoing developments, we are seeking to include in ECOMAN micromechanical modelling**
439 **methods that are capable of estimating the strain-induced LPO and/or the intrinsic viscous**
440 **anisotropy at computational speeds that are orders of magnitude faster than current ones.**



441 For instance, Ribe et al. (2019), have proposed an analytical finite-strain parameterization
442 for texture evolution in deforming olivine polycrystals that is $\approx 10^7$ times faster than full
443 homogenization approaches such as the second-order self-consistent model. When implemented in ECOMAN, preliminary
444 tests indicate that this new method outperforms D-REX by 1-2 orders of magnitude (Ribe et al., 2023).
445 In addition, in the near future the PSI software will be updated to include trans-dimensional Bayesian Monte Carlo sampling
446 methods that, in contrast to deterministic approaches, address the consequences of under-determination in seismic imaging
447 (Del Piccolo et al., 2023). Isotropic and anisotropic seismic imaging with PSI is currently feasible using body wave information
448 such as travel-times and S-wave splitting intensity. However, when local deep seismicity is absent, as is the case in warm
449 subduction zones or at spreading ridges and intraplate settings, the retrieved isotropic and anisotropic mantle structures are
450 only partially recovered and often affected by smearing (e.g., Faccenda and VanderBeek, 2023). Consequently, we are
451 planning to complement body wave information with surface waves data to improve the seismic ray coverage and the resolving
452 power of tomographic models. Lastly, to improve the prediction of seismic observables, 3D anisotropic ray tracing and finite-
453 frequency kernels are planned for a future release.

454 **Code availability**

455 ECOMAN is freely available at <https://github.com/ecoman-geos>.

456 **Data availability**

457 The software package contains the input files to generate the synthetic models and datasets discussed in this manuscript. No
458 data has been produced for this work.

459 **Author contributions**

460 MF and BPV developed the software package, with important contributions from AdM and JY. MF wrote the manuscript draft.
461 MF acquired the funding supporting the research activities. All authors have contributed to the discussion and manuscript
462 editing.

463 **Competing interests**

464 The authors declare that they have no conflict of interest.



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