

# Determining optimal sampling conditions in the TSI Nanometer Aerosol Sampler 3089

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**Abstract.** Physicochemical characterisation of airborne particles requires appropriate sampling and deposition methods. The TSI Nanometer Aerosol Sampler 3089 (TSI NAS) has predominantly been used as an electrostatic precipitator for depositing airborne particles, enabling subsequent offline characterization through techniques such as electron microscopy. However, the optimal sampling time of TSI NAS for varying input concentrations has not been thoroughly investigated. This is extremely important as the concentration of particles in different environments differ significantly. This study aimed to establish the appropriate sampling durations of TSI NAS for various input concentrations, or conversely, to determine suitable input concentrations for a fixed sampling duration. We developed an experimental set-up and a linear regression model to predict conditions conducive to efficiently collecting loaded samples, particularly at low concentrations, such as exhaled particles from the human respiratory tract or marine aerosol particles. Experiments were conducted using the TSI NAS 3089 at a flow rate of 1 L·min<sup>-1</sup> and a voltage of -9 kV. Three particle types, nebulized from different solutions at low, medium, and high concentrations, were sampled over durations of 1, 3, and 6 hours. Deposition densities were subsequently analysed using ImageJ software. The findings revealed a linear relationship between deposition density and the product of particle concentration and sampling time, with a recommended density range of 0.015 to 0.1 #·µm<sup>2</sup> for particles with a count median diameter of approximately 100 nm and average circularity of 0.56 ± 0.25. Despite potential factors affecting the accuracy of the model, such as the number of samples, random collisions, and potential overload in high-concentration experiments, it provides a valuable predictive tool for determining optimal sampling times. The suggested linear regression model is applicable across various research areas, enhancing the efficiency and accuracy of airborne particle characterisation.

## 1 Introduction

Aerosol can present significant threats to the atmosphere, climate, and human health, necessitating comprehensive research efforts to understand their multifaceted impacts (Pöschl, 2005; Savage et al., 2017). Extensive experiments have been conducted to sample and characterize various types of aerosols, focusing on their morphology, size distribution, and chemical composition (Mirhoseini et al., 2016; Müller et al., 2011; Groth et al., 2022). One of the primary challenges in sampling these

30 particles lies in their potential presence at low number concentrations, particularly in aerosols emitted during respiratory activities (Groth et al., 2021; Pöhlker et al., 2023).

Microscopy is a valuable method for assessing various features of aerosols, including constructing particle size distributions (PSDs) and determining particle morphology and composition. (Wittmaack et al., 2005; Sobanska et al., 2014; Groth et al., 2023). Various electron microscopy (EM) techniques, including scanning electron microscopy (SEM) and transmission  
35 electron microscopy (TEM), have been widely employed for analysing airborne particles. For example, Wittmaack et al. characterized bioaerosols in ambient air using SEM, revealing their complex morphology and diversity in size and shape (Wittmaack et al., 2005). Similarly, Capannelli et al. evaluated SEM, field emission SEM (FE-SEM), and TEM modes to optimize procedures for analyzing particles on filtering membranes, demonstrating the capabilities of these techniques for direct particle observation (Capannelli et al., 2011). However, obtaining accurate microscopy results requires collecting an  
40 efficiently loaded number of aerosols on a flat, chemically stable, and transportable substrate. This is critical because such substrates prevent chemical interactions and physical deformations that could alter the characteristics of the aerosols, ensuring that the observed characteristics reflect their true nature (Li et al., 2010).

Aerosol loading on a substrate for EM analyses includes inertial, thermophoretic, and electrophoretic techniques, each offering unique advantages for aerosol collection and analysis. Inertial sampling methods rely on the separation of particles based on  
45 their momentum, which depends on their aerodynamic properties, and subsequently collected onto an impaction surface (Hering et al., 1990). Thermophoretic methods utilize temperature gradients to drive aerosol particles towards a cooler surface for collection, allowing for the selective sampling of particles based on their thermal properties (Wasmund et al., 2010). Electrophoretic deposition is a very common method employed for the collection of aerosols based on their electrical mobility diameter. In this process, the particles are first charged and are subsequently directed toward a surface that carries an opposite  
50 electric charge. Aerosols with higher mobility deposit onto the charged surface, while aerosols with lower mobility continue their passage and are expelled through the exhaust. The diameter of the aerosols that ultimately deposit on the surface depends on several factors such as particle charge, surface voltage or electrical fields, and rate of airflow (Kettleson et al., 2009).

The TSI Nanometer Aerosol Sampler 3089 (TSI NAS, Shoreview, MN) is a widely used electrostatic precipitator for collecting airborne particles to facilitate offline analysis, including EM (Lyu et al., 2024; Bauer et al., 2019; Buckley et al., 2017). The  
55 NAS offers two primary advantages: an efficient collection of particles ranging from 2 to 100 nm and fairly uniform deposition on the substrate, allowing a small portion of the sample to accurately reflect the entire sample (Dixkens and Fissan, 1999). The NAS has been employed to investigate the collection efficiency for ultrafine particles (UFPs) across a range of voltages and flow rates to evaluate the optimal sampling conditions within a specific time span (Li et al., 2010). Li et al. found that collection efficiency improved with the decrease in flow rate and increase in voltage. The highest efficiency was measured at  $1 \text{ L} \cdot \text{min}^{-1}$   
60 and  $-9.3 \text{ kV}$ . Thus, there is a direct relationship between particle deposition and voltage, owing to the greater electrical force (Li et al., 2010). The NAS has also been used for collecting atmospheric aerosols for offline particle characterization studies. Barone et al. investigated the morphology of particles with diameters smaller than 100 nm, collected on TEM grids attached to the NAS electrode. They conducted sampling at  $1 \text{ L} \cdot \text{min}^{-1}$  and  $-10 \text{ kV}$  to sample particles on and near major freeways in

Los Angeles, CA, where particles were electrically charged using a bipolar diffusion charger and selectively sized to 50 nm  
65 using a differential mobility analyser. Analysis of the particles selected based on size using TEM allowed them to explore  
changes in the fraction of particles within each morphology class with distance from the major freeway, providing insights  
into the aerosol mechanisms affecting the number-size distribution (Barone and Zhu, 2008).

The samples collected using NAS have also been used to investigate the chemical composition of UFPs, offering valuable  
insights into the nature and origin of the aerosols present in the ambient air near coal-fired power stations (Hinkley et al.,  
70 2008). Hinkley et al. collected particles under 300 nm on TEM grids affixed to the NAS electrode with a flow rate and voltage  
of 1 L·min<sup>-1</sup> and -10 kV, respectively. Prior to the collection by the NAS, aerosols underwent a cascade impactor separation  
and charge neutralization. Subsequently, they were subjected to TEM analysis coupled with energy dispersive X-ray (EDX)  
to determine both chemical composition and morphology. The study investigated the contribution of UFPs from power station  
emissions to ambient aerosol at a near source sampling site (Hinkley et al., 2008). Hinkley et al. reported a table indicating the  
75 suitability of sample loading for TEM analysis based on various particle concentrations and sampling duration. Four out of ten  
experiments were well loaded, while the remaining were categorized as either lightly loaded or overloaded. Overloading could  
lead to inaccuracies in size and shape analysis, introducing bias or errors and reducing the reliability and representativeness of  
the collected data. Verma et al. investigated the effect of fuel oxygen content on morphology and nanostructure characteristics  
of soot particles, utilizing fuels such as diesel, coconut biodiesel and triacetin. They employed a NAS at 1 L·min<sup>-1</sup> flow rate  
80 and 7 kV voltage. Diesel fuel, producing the highest number of particles, was sampled first while the engine operated at 100%  
load. They tried to optimize sampling duration to prevent particle overlap and ensure an adequate number of soot particles for  
morphological analysis. TEM imaging revealed that a sampling time of 3-4 minutes was sufficient for diesel particles. For the  
other fuels, the sampling time was gradually increased to seven minutes to collect enough particles for analysis while still  
avoiding the overlapping of soot agglomerates (Verma et al., 2019).

85 Despite efforts to characterise UFPs using the NAS and determining the efficient operating flow rate and voltage, there haven't  
been comprehensive studies on the optimum sampling time for a given input concentration. This gap is particularly significant  
in low input concentration environments, such as aerosols generated from the human respiratory system, marine aerosols, and  
aerosols present in the free troposphere at high altitudes (Mirhoseini et al., 2016; Facchini et al., 2008; Pöhlker et al., 2011).  
This study aimed to sample three types of aerosols in low, medium, and high input concentration environments over a sampling  
90 duration spanning 1 to 6 hours. The outcome of this study can provide a model for the prediction of optimal sampling conditions  
for the NAS to ensure reliable measurements of the physiochemical properties of collected aerosols.

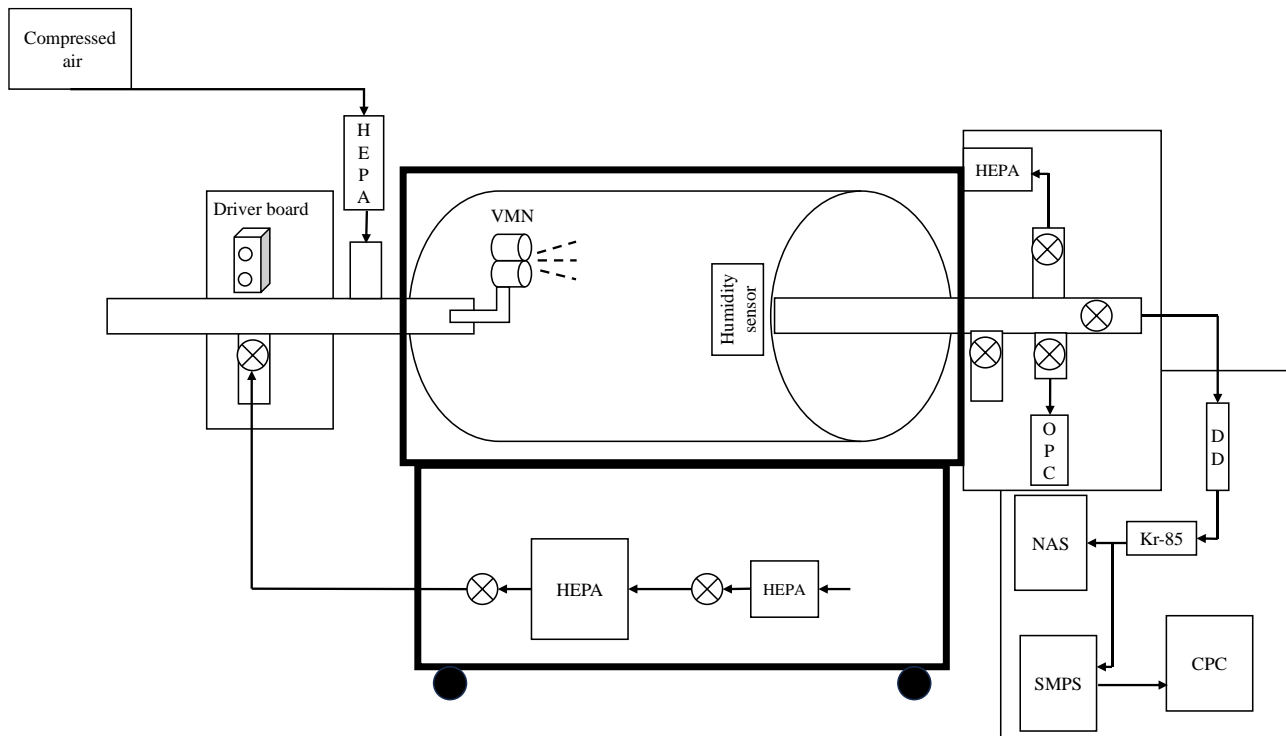
## 2 Methodology

### 2.1 Experimental Arrangement

In this study, the collection density of aerosols generated from phosphate buffered saline (PBS), Dulbecco's Modified Eagle  
95 Medium (DMEM) solutions, as well as human saliva, was evaluated using the TSI NAS with a voltage of up to -10 kV as an

electrostatic precipitator to collect charged aerosols for offline analysis. The PBS, DMEM, and human saliva aerosols were selected as a representative of marine or human respiratory aerosols. PBS, a balanced salt solution used in biological research, contains inorganic compounds including chloride- and phosphate-containing salts and is buffered to maintain physiological pH (Almeida et al., 2013). Consequently, PBS was chosen to represent the complexity of the ionic composition of not only marine aerosols (Nenes et al., 2011; Baker et al., 2006) but also in general other aerosols. DMEM, a widely used cell culture medium, contains amino acids, vitamins, glucose, and salts, providing nutrients for cell growth (Yao and Asayama, 2017). The combination of organic and inorganic components in DMEM tends to produce irregular shapes, contrasting with the relatively regular structures observed in PBS. DMEM may also be representative of respiratory fluid particles. The morphology of human saliva can be complex due to its diverse composition, comprising both inorganic and organic components, such as water, electrolytes, proteins, enzymes, mucins, and cells. The drying process can lead to the formation of heterogeneous structures, including protein aggregates and fibrous structures (Sharma et al., 2011; Bel'skaya et al., 2019). The morphology of the aerosols may influence the NAS deposition due to different dynamic shape factors and agglomeration, where highly agglomerated or non-spherical particles may result in higher particle diffusion coefficients (Moskal and Payatakes, 2006). As the diffusion coefficient increases, aerosols disperse more extensively from the electrode where they are initially deposited, potentially reducing particle concentration near the electrode (Park and Chun, 2002). However, the three selected solutions in this study are expected to show no agglomeration, with particles predominantly spherical or cubic.

Two adjacent vibrating mesh nebulisers (VMN) mounted inside a rotating drum were utilised to produce the aerosols (Johnson et al., 2016; Niazi et al., 2021). These aerosols were then passed through a silica diffusion dryer (DD) and an  $^{85}\text{Kr}$  neutralizer (Kr-85) before being collected on continuous carbon-coated copper grids (200 mesh, Ted Pella, Inc.) fixed on the electrode of the NAS. This ensures that all aerosols were in the same humidity during deposition, and the humidity inside the drum did not affect the deposition density of the NAS. The NAS was operated at a flow rate and voltage of  $1 \text{ L}\cdot\text{min}^{-1}$  and  $-9 \text{ kV}$ , respectively which has been shown to have the highest collection efficiency (Li et al., 2010). A schematic diagram of the NAS is presented in Fig. S1 to highlight airflow patterns, aerosol deposition, and electrical field dynamics. Particle input concentration and size distribution were measured by the TSI 3080 scanning mobility particle sizer (SMPS), using the TSI 3776 butanol-based condensation particle counter (CPC) (TSI, Shoreview, MN). The SMPS had a sheath flow rate of  $3 \text{ L}\cdot\text{min}^{-1}$ , and each scan was conducted for 5 minutes. After scans were performed, the average PSDs were used for comparison with data obtained from SEM micrographs. An AeroTrak Handheld Particle Counter 9306 (OPC) was used to ensure the experimental system was clean and free from any residual particles prior to aerosol injection. Figure 1 shows the schematic diagram of the experimental setup. The summary of the NAS parameters and operating conditions is presented in Table 1.



**Figure 1: Diagram showing the experimental setup used in this study.**

**Table 1: The operating conditions and dimensions of the Nanometer Aerosol Sampler (TSI NAS 3089) employed in this study.**

Operating conditions and dimensions	Values
NAS inlet diameter (mm)	6.5
NAS electrode diameter (mm)	9.5
Rate of inlet airflow ( $L \cdot min^{-1}$ )	1
Voltage applied to the electrode (kV)	-9
Temperature inside the rotating drum ( $^{\circ}C$ )	$22 \pm 1$
Relative Humidity inside rotating drum (%) before introducing particles	$4 \pm 1$
Relative Humidity inside rotating drum (%) after introducing particles	$11 \pm 4$

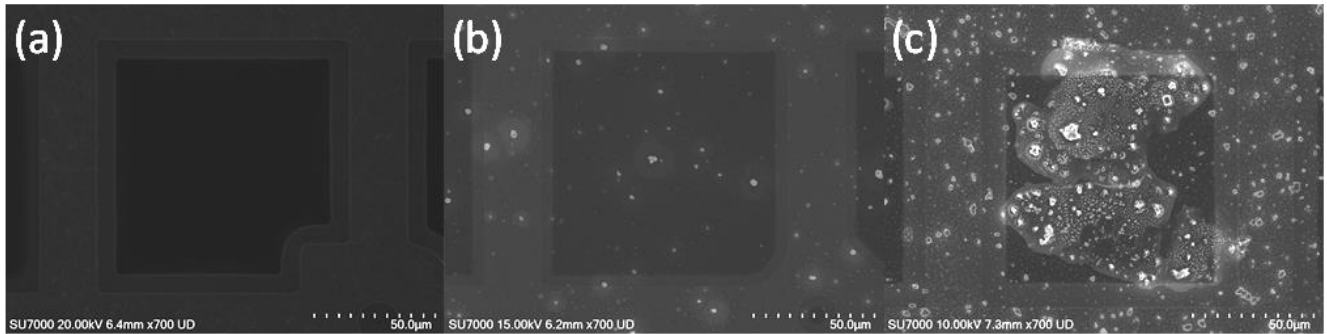
Experiments were conducted at three different concentrations and three sampling durations of 1, 3 and 6 hours. The desired input particle number concentrations for each experiment were achieved by modifying the nebulization time of the VMNs. Specifically, 1.5 mL of the solution was nebulized for 3 seconds in low deposition experiments, 9 seconds for medium deposition experiments, and 20 seconds for high deposition experiments. The number of collected particles was examined by scanning electron microscopy (Hitachi SU 7000 SEM), employing a high-energy electron beam scanned in a raster pattern. Micrographs were captured at an accelerating voltage ranging from 10 to 20 kV and a spot intensity of 30% in secondary

135 electron imaging (SE) mode. To prepare the samples for analysis, they were first coated with a 10 nm carbon layer to avoid  
surface accumulation of electrostatic charge.

## 2.1 Deposition density calculations

140 Figure 2 shows examples of SEM micrographs depicting under loaded, efficiently loaded, and over loaded numbers of  
particles. When particle numbers are too low (Fig. 2a), or excessively high, resulting in clusters or pileups (Fig. 2c), accurate  
size and shape analysis becomes unattainable. Additionally, overlapping particles introduce bias and errors into the data,  
complicating the identification of individual particles and reducing the reliability and representativeness of the collected  
chemical composition information. Conversely, the efficiently loaded sample (Fig. 2b) exhibits an optimal deposition density  
that enhances the reliability and representativeness of morphology, size, and chemical composition characterization.

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**Figure 2: SEM images of phosphate buffered saline (PBS) particles collected in different input concentrations and sampling times: a) low concentration ( $200 \text{ \#}\cdot\text{cm}^{-3}$ ), 1 hour,  $7.52 \times 10^{-4} \text{ \#}\cdot\mu\text{m}^{-2}$ , b) medium concentration ( $500 \text{ \#}\cdot\text{cm}^{-3}$ ), 6 hours,  $2.96 \times 10^{-2} \text{ \#}\cdot\mu\text{m}^{-2}$ , c) high concentration ( $5000 \text{ \#}\cdot\text{cm}^{-3}$ ), 6 hours,  $0.385 \text{ \#}\cdot\mu\text{m}^{-2}$ .**

150 On each sample substrate, multiple grid squares at different locations were randomly investigated, and micrographs of the  
collected particles were captured. Subsequently, image analysis was conducted using ImageJ to determine the deposition  
density of the collected particles (Schneider et al., 2012). A sample of a viewing area processed by ImageJ is presented in Fig.  
3. First, the micrographs were binarized and size-corrected using the image scalebar. The number, perimeter, and area of the  
particles in the image were then measured using the ‘Analyze Particles’ feature. The deposition density of the collected  
155 particles was calculated by dividing the number of detected particles in each grid square by the total area of that grid square.

$$D = \frac{N_{count}}{A_{total}}, \quad (1)$$

Where  $D$  is the deposition density of the collected particles ( $\text{\#}\cdot\mu\text{m}^{-2}$ ),  $N_{count}$  is the number of deposited particles counted using  
SEM ( $\text{\#}$ ), and  $A_{total}$  is the total area of the examined substrate ( $\mu\text{m}^2$ ). The number of particles in each viewing area ( $6.3 \mu\text{m} \times$   
 $4.7 \mu\text{m}$ ) was investigated and calculated for three different types of generated aerosol. The relative standard deviation in the

160 particle count per viewing area was calculated to be below 10% for the efficiently loaded samples, suggesting a relatively uniform deposition. To calculate this, 4500 viewing areas were randomly investigated by SEM. This uniform deposition enables a small sample of the substrate to be analysed as a representative of the entire collection on the TEM grid.

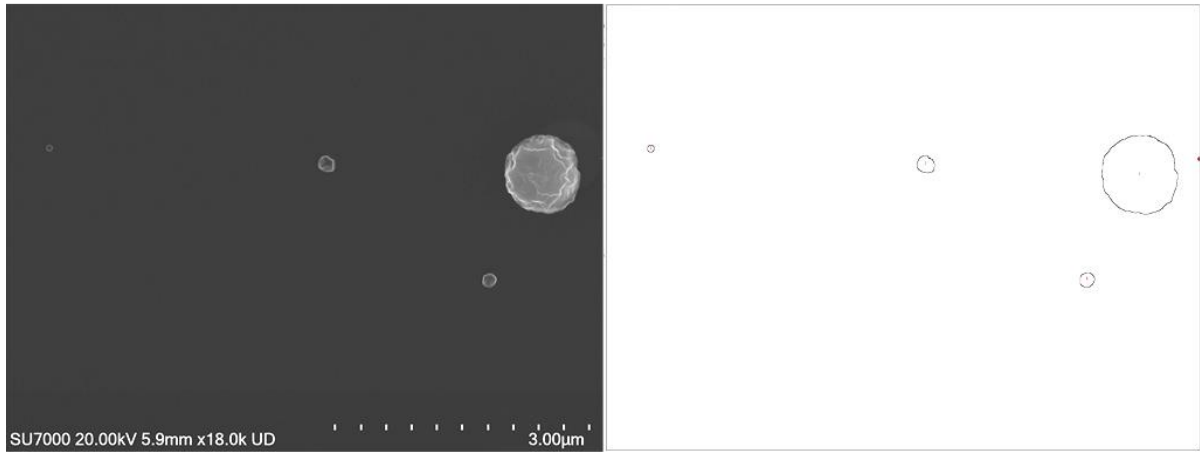


Figure 3: An example of the output of the 'Analyze Particles' feature in ImageJ.

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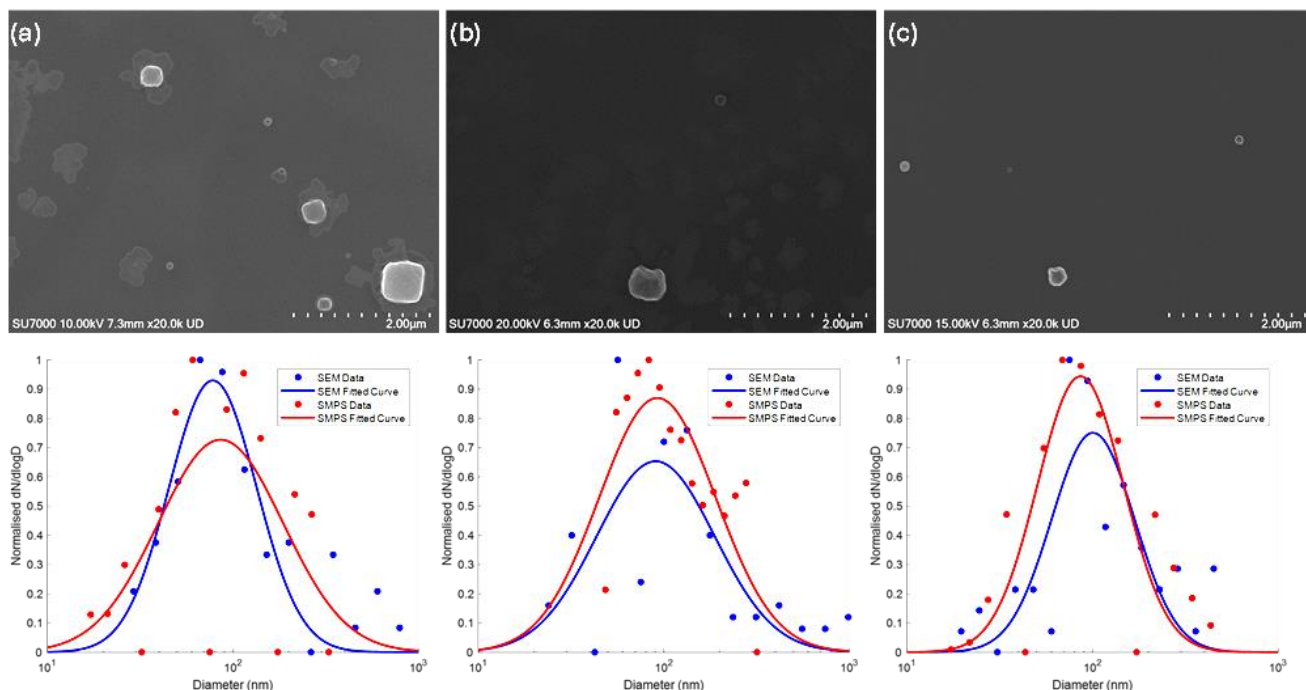
### 3 Results and discussion

#### 3.1 Comparison of SEM analysis with SMPS measurements

Examples of the three different aerosols collected and their PSDs are shown in Fig. 4. Following particle detection using ImageJ, measurements of particles can be conducted, yielding area (A) and perimeter (P) of the collected particles. To correlate  
170 the collected data into size distributions of particles, the area equivalent diameter ( $d_{AE}$ ) can be calculated using Eq. (2).

$$d_{AE} = 2\sqrt{\frac{A}{\pi}}, \quad (2)$$

Furthermore, Fig. 4 illustrates a comparison of the PSD obtained through both SEM analysis of deposited particles using ImageJ and SMPS measurement of airborne particles. This comparison was made for PBS aerosols (Fig. 4a), DMEM aerosols (Fig. 4b), and human saliva aerosols (Fig. 4c). Spherical particle geometry was assumed for consistency between the  
175 measurement techniques. This allowed the electrical mobility diameter from SMPS to be compared with the area-equivalent diameter from SEM without requiring shape factor corrections. Table 2 outlines the average input concentration during the experiment, sampling duration, count median diameters (CMD), and geometric standard deviations (GSD) obtained from both SMPS and SEM for PBS, DMEM, and human saliva aerosols. The PSDs acquired by SEM analysis and SMPS measurements exhibit a good agreement, affirming the validity of the setup for determining the optimal sampling time.



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**Figure 4: SEM images and particle size distributions of (a) phosphate buffered saline (PBS) (b) Dulbecco's Modified Eagle Medium (DMEM), and (c) human saliva. Particle size distributions were normalized to the maximum concentration for easier comparison between SEM and SMPS. Particle size distributions with absolute concentrations are provided in Fig. S2.**

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**Table 2: Properties of dry aerosol generated under different conditions by vibrating mesh nebulizers and measured by scanning electron microscopy (SEM) analysis and scanning mobility particle sizer (SMPS) measurements.**

Solution	Average Concentration ( $\# \cdot \text{cm}^{-3}$ )	Input	Sampling duration (h)	$\text{CMD}_{\text{SMPS}}$ (nm)	$\text{CMD}_{\text{SEM}}$ (nm)	$\text{GSD}_{\text{SMPS}}$	$\text{GSD}_{\text{SEM}}$
PBS	487		3	85.9	77.9	2.2	1.7
DMEM	202		6	92.4	90.4	2.1	2.1
Human saliva	775		3	86.2	100.7	1.7	1.6

### 3.2 Estimating optimal sampling time

The results obtained from the SMPS measurements and SEM image analysis are presented in Table 3, which includes data for experiments conducted at low, medium, and high concentrations of PBS, DMEM, and human saliva aerosols. To compare deposition density ( $D$ ) with sampling time ( $t$ ) and concentration ( $C$ ), a new variable, which is a product between the particle concentration and time of sampling  $C \times t$ , is introduced. This variable is equivalent to the particle exposure of the grids. By applying linear regression analysis to the data and setting the intercept to zero, Eq. (3) defines the relationship between

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deposition density and  $C \times t$ . This equation allows us to determine the ideal sampling time (in hours) for a given particle  
 195 number concentration (in  $\text{cm}^{-3}$ ) or the optimal particle number concentration within a set sampling duration, given a specified  
 optimal deposition density.

$$D = 1.2 \times 10^{-5}(C \times t), \quad (3)$$

Figure 5 illustrates the plot of the linear fit to the data, along with the 95% confidence bands. As the particle number  
 concentration changes for several orders of magnitude, the x-axis has a logarithmic scale. The regression analysis yielded a  
 200 multiple R-value of 0.99, indicating a strong correlation between  $C \times t$  and D. The  $R^2$  value of 0.98 indicates that the regression  
 model effectively explains the variability in the data. With a relative standard error of 2%, the average distance between  
 observed and predicted values is relatively low. Based on qualitative observations during this study, the suggested deposition  
 density falls within the range of 0.015 to 0.1  $\mu\text{m}^{-2}$ . It is important to note that the relationship established in this study was for  
 nebulized aerosols with a CMD of around 100 nm.

205 Certain factors, such as the number of samples, particle diffusion, Brownian motion, random collisions, and potential overload  
 in high-concentration experiments can impact the accuracy of the model. Despite these potential influences, the model provides  
 a robust estimation of particle deposition and enables the determination of the optimal sampling time for a given particle  
 concentration. This ensures the identification and characterization of an adequate number of particles in subsequent research  
 phases. For the particle diameters examined in this study, all particles closely adhere to the derived regression model.

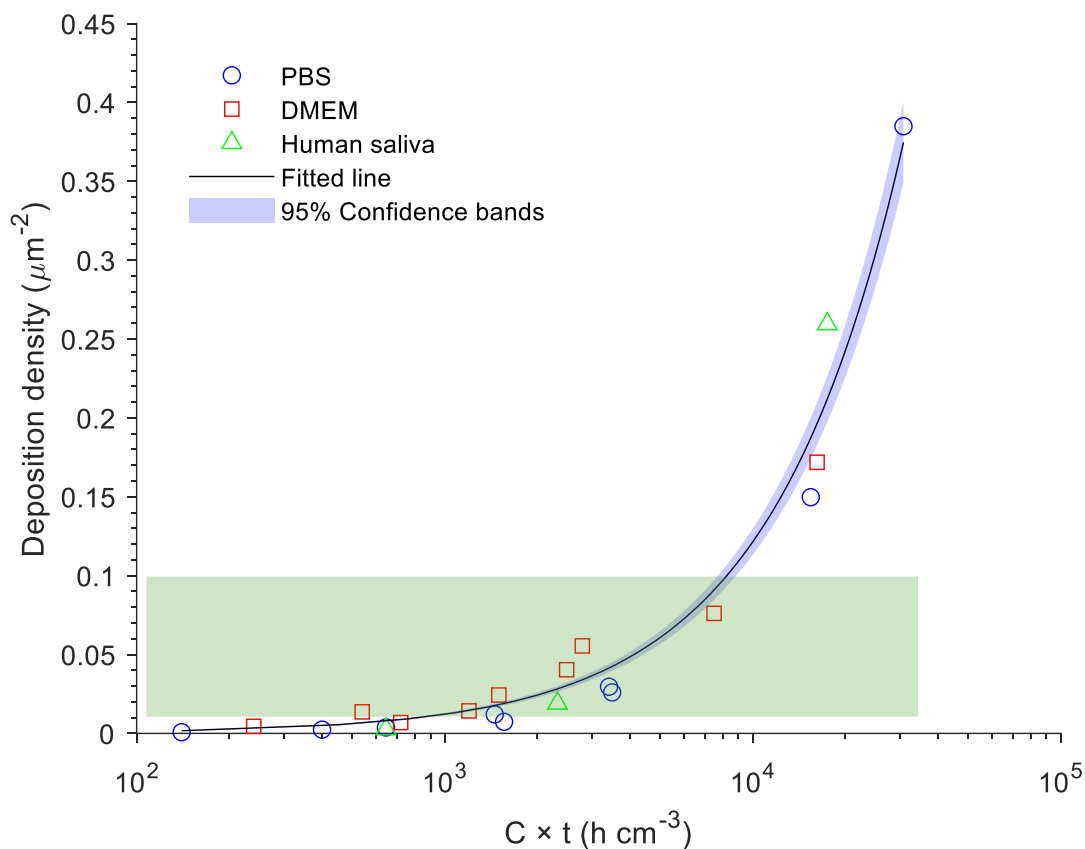
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**Table 3: Values measured by scanning mobility particle sizer (SMPS) and scanning electron microscopy (SEM) images for phosphate buffered saline (PBS), Dulbecco's Modified Eagle Medium (DMEM), and human saliva aerosols.**

Sampling time (h)	Input concentration ( $\#\cdot\text{cm}^{-3}$ )	$C \times t$ ( $\text{h}\cdot\text{cm}^{-3}$ )	Deposition density ( $\#\cdot\mu\text{m}^{-2}$ )
PBS			
1	140	140	$7.52 \times 10^{-4}$
3	215	645	$3.77 \times 10^{-3}$
6	260	1560	$7.34 \times 10^{-3}$
1	400	400	$2.37 \times 10^{-3}$
3	485	1455	$1.20 \times 10^{-2}$
6	570	3420	$2.96 \times 10^{-2}$
1	3500	3500	$2.60 \times 10^{-2}$
3	5150	15450	0.15
6	5150	30900	0.38
DMEM			
1	240	240	$4.47 \times 10^{-3}$

3	240	720	$6.84 \times 10^{-3}$
6	200	1200	$1.43 \times 10^{-2}$
1	540	540	$1.36 \times 10^{-2}$
3	500	1500	$2.43 \times 10^{-2}$
6	415	2490	$4.04 \times 10^{-2}$
1	2800	2800	$5.54 \times 10^{-2}$
3	2500	7500	$7.61 \times 10^{-2}$
6	2700	16200	0.17
Human saliva			
3	215	645	$2.68 \times 10^{-3}$
3	775	2325	$1.90 \times 10^{-2}$
3	5830	17490	0.26

Furthermore, the deposition density of the NAS was found to be relatively consistent with the variations in particle morphology. Particle circularity was calculated using the formula,  $4\pi \frac{[area]}{[perimeter^2]}$ , with both area and perimeter obtained by ImageJ. Circularity values were  $0.51 \pm 0.25$  for DMEM,  $0.57 \pm 0.24$  for PBS, and  $0.67 \pm 0.24$  for human saliva, indicating a range of shapes from irregular to cubic or spherical. These results suggest that Eq. (3) can be used to estimate deposition density across a variety of particle shapes. The comprehensive evaluation of the TSI NAS 3089 instrument is critical not only for the analysis of human respiratory aerosols and their analogues, but also for a variety of applications, including marine aerosol studies (Laskina et al., 2015; Tervahattu et al., 2002), engine emissions (Dallmann et al., 2014), and indoor air quality measurements (Vestlund et al., 2014; Wittmaack et al., 2005). It is recommended that researchers utilize this model as a first order estimate of required sampling time and extend its application to high-concentration experiments.



225 **Figure 5: Regression model derived for phosphate buffered saline (PBS), Dulbecco's Modified Eagle Medium (DMEM), and human saliva aerosols collected by the TSI Nanometer Aerosol Sampler. The green box highlights the suggested range for the deposition density values, ranging from 0.015 to 0.1 μm<sup>-2</sup>**

#### 4 Conclusion

In this study, a linear regression model was developed to predict the optimal sampling time for a given particle number concentration or determine the optimal particle number concentration within a specified sampling duration. This model was constructed for sampling aerosols utilizing a TSI NAS 3089 at a flow rate of 1 L·min<sup>-1</sup> and a voltage of -9 kV, where three different aerosol types were generated at low, medium and high concentrations. These aerosols were subsequently collected on a TEM grid over the duration of 1, 3, and 6 hours. SEM images were post-processed using ImageJ to determine deposition density, revealing a linear relationship between deposition density and the product of particle concentration and time. The recommended deposition density range of 0.015 to 0.1 μm<sup>-2</sup> was found suitable for aerosols with a CMD around 100 nm.

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Notably, this model is effective for aerosols with an average circularity of approximately  $0.56 \pm 0.25$ , regardless of their chemical composition, and that are not agglomerated.

240 It is important to consider factors that may influence the accuracy of the developed linear regression model, including the number of samples, particle diffusion, Brownian motion, random collisions, and potential overload in high-concentration experiments. These considerations require attention in future investigations to refine and enhance the predictive capabilities of the model. In conclusion, the suggested linear regression model provides a valuable tool for predicting the optimal sampling time and offers researchers a reliable estimation of particle behaviour and concentration. Its applicability extends beyond the study of human respiratory aerosols, making it relevant to a wide range of aerosol research areas.

## **5 Data availability**

245 Plots in electronic format and SEM data will be provided upon request.

## **6 Author contribution**

B.A., S.N., R.G., B.M., and Z.R. designed research, B.A., and S.N. performed research, B.A., S.N., R.G., and Z.R. analysed and processed data, B.A., S.N., R.G., B.M., and Z.R. drafted the manuscript.

## **7 Competing interests**

250 The authors declare that they have no conflict of interest.

## **8 Acknowledgement**

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