

# Ground-based contrail observations: comparisons with [reanalysis](#) [weatherflight telemetry](#) and contrail model [simulationsestimates](#)

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**Abstract.** Observations of contrails are vital for improving our understanding of contrail formation and lifecycle, informing models, and assessing contrail mitigation strategies. Ground-based cameras offer a cost-effective method to observe the formation and evolution of young contrails which can be used to assess the accuracy of existing models. Here, we developed a methodology to use ground-based cameras for tracking and analysing young contrails (< 35 minutes) formed under clear sky conditions from ground-based cameras, comparing these observations against reanalysis meteorology and simulations from the contrail cirrus prediction model (CoCIP) with actual flight trajectories. Our ground-based contrail observations consist of 14 h of video footage recorded over five different days over in Central London, capturing a total of 1,582,649 flight waypoints from 2813 unique flights. The simulation correctly predicted contrail formation and absence for around 75% of these waypoints, with incorrect contrail predictions occurring at warmer temperatures than those with true positive predictions (7.8 K vs. 12.8 K below). Our results suggest that the best agreement between the observed and simulated contrail formation occurs at around 35,000–40,000 feet and at temperatures at least 10 K below the Schmidt-Appleman Criterion threshold temperature ( $T_{SAE}$ ). Among all waypoints with contrail observations, 78% of short-lived contrails (observed lifetimes < 2 minutes) formed under ice sub-saturated conditions, while 75% of persistent contrails (observed lifetimes > 10 minutes) formed under ice supersaturated conditions. Conversely, the largest discrepancies occurred when contrails are formed below 30,000 feet and at temperatures within 2.5 K of  $T_{SAE}$ . On average, the simulated contrail geometric width is was around 100 m (17.5% smaller than the observed (visible) geometric width over its observed lifetime, with the mean underestimation reaching up to 280 m within the first five minutes. This discrepancy between the observed and simulated contrail formation, lifetime and widths can be associated with could be caused by uncertainties in reanalysis meteorology due to known model limitations and sub-grid scale variabilities, contrail model simplifications, uncertainties in aircraft performance estimates, and observational challenges the underestimation of sub-grid scale wind shear and turbulent mixing in the simulation, and model representation of the contrail cross-sectional shape, among other possible factors. Overall, these findings this study demonstrates the capability potential of ground-based cameras to create essential observational and benchmark datasets for validating and improving existing inform weather and contrail models development when combined with flight telemetry.

## 1 Introduction

Contrails, ~~line-shaped clouds that~~ form behind an aircraft at altitudes of 8–13 km, ~~occur~~ when conditions in the exhaust plume fulfil the Schmidt-Appleman Criterion (SAC) (Schumann, 1996). Under these conditions, the relative humidity (~~RH~~) in the exhaust plume reaches liquid saturation ~~causing-enabling~~ water vapour to condense onto the surface of soot particles ~~to form~~ water droplets, which subsequently freeze to form contrail ice crystals. These newly formed contrail ice particles are entrained in the aircraft's wake vortices, and in most cases, contrails that are formed disappear within a few minutes as adiabatic heating causes the ice particles to sublimate (Lewellen and Lewellen, 2001; Unterstrasser, 2016). However, a small fraction of contrails can persist beyond a few minutes when the atmosphere is ice supersaturated, i.e., relative humidity with respect to ice (RH<sub>i</sub>) exceeding 100% (Jensen et al., 1998a). According to the definition provided by the World Meteorological Organization (2017), contrails that survive for at least 10 minutes are known as persistent contrails. Over time, persistent contrails tend to spread and mix with other contrails and natural clouds to form contrail cirrus clusters (Haywood et al., 2009) affecting the Earth's radiative balance and producing a net warming effect (Fuglested et al., 2010; Meerkötter et al., 1999). Recent studies suggests that the global annual mean contrail cirrus net radiative forcing (RF) in 2018 and 2019 (best-estimate of between 61 and 72 ~~62-1~~ ~~{34.8, 74.8}~~ mW m<sup>-2</sup> ~~across three studies~~) (Märkl et al., 2024; Quaas et al., 2021; Teoh et al., 2024a) could be around two times greater than the RF from aviation's cumulative CO<sub>2</sub> emissions (34.3 [31, 38] mW m<sup>-2</sup> ~~at a 95% confidence interval~~) (Lee et al., 2021).

Different modelling approaches are available to simulate the contrail properties and climate forcing, including: (i) large-eddy simulations (LES) (Lewellen, 2014; Lewellen et al., 2014; Unterstrasser, 2016); (ii) general circulation models (GCM) (Bier and Burkhardt, 2022; Chen and Gettelman, 2013; Märkl et al., 2024); (iii) Lagrangian models based on parameterised physics, such as the contrail cirrus prediction model (CoCiP) (Schumann, 2012); and (iv) climate change functions (CCFs) and algorithmic climate change functions (aCCFs) (Dietmüller et al., 2023; Grewe et al., 2014). These contrail modelling approaches have been used to estimate the global and regional contrail climate forcing (Bier and Burkhardt, 2022; Chen and Gettelman, 2013; Schumann et al., 2021; Teoh et al., 2022a, 2024a) and explore the effectiveness of different mitigation strategies (Burkhardt et al., 2018; Caiazzo et al., 2017; Grewe et al., 2017; Märkl et al., 2024; Martin Frias et al., 2024; Schumann et al., 2011; Teoh et al., 2020, 2022b).

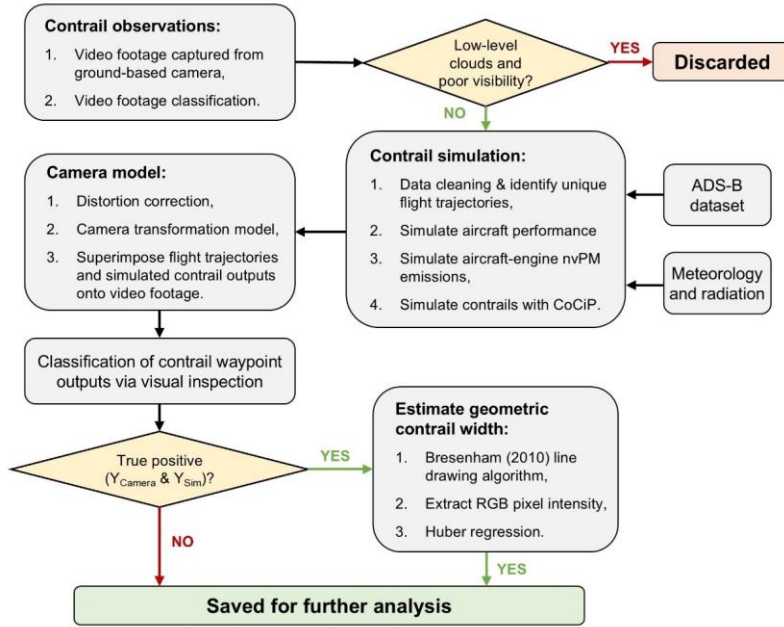
To enhance confidence and ensure that any proposed contrail mitigation solution yields a net climate benefit, it is crucial that ~~these~~ contrail models ~~outputs~~ are extensively validated against measurements and observations. Existing studies have compared the simulated contrail properties from CoCiP relative to in-situ measurements, remote sensing ~~data~~, and satellite observations, ~~where the results and~~ generally ~~show-found~~ a good agreement between the measured and simulated contrail properties at various stages of their lifecycle (Jeßberger et al., 2013; Märkl et al., 2024; Schumann et al., 2017, 2021; Teoh et al., 2024a). However, these ~~studies either focused on comparisons were conducted on an~~ aggregate ~~statistics derived from level,~~ ~~focusing on~~ an ensemble of contrails, ~~or and thus do not provide insights into the evaluation of individual contrails formed by unique flights. While~~ (Jeßberger et al., 2013) ~~has~~ assessed the simulated contrail properties ~~from CoCiP~~ with in-situ

65 measurements of young contrails ~~formed by different passenger aircraft types, these measurements were made~~ at a single point  
in time ~~and the study remains limited to three with a limited number of~~ data points. ~~While~~ Satellite observations, ~~on the other~~  
70 ~~hand,~~ can partially address some ~~of these~~ limitations ~~of in-situ measurements~~ by enabling a large number of contrails to be  
measured, matched with specific flights and tracked over time (Duda et al., 2019; Gryspeerdt et al., 2024; Marjani et al., 2022;  
Tesche et al., 2016; Vázquez-Navarro et al., 2015), ~~they still face challenges in but it remains challenging for satellites to~~  
85 ~~detecting~~ young contrails with sub-pixel width, aged contrail cirrus ~~that has lost its line-shaped structure, eases instances of with~~  
cloud-contrail overlap, and contrails with small optical depths ( $< 0.05$ ) (Kärcher et al., 2010; Mannstein et al., 2010; Meijer et  
al., 2022).

Ground-based instruments, such as lidar and cameras, can ~~complement be used in tandem with~~ in-situ measurements and  
satellite observations in ~~the validation of validating~~ contrail models (Mannstein et al., 2010; Rosenow et al., 2023; Schumann  
95 et al., 2013). ~~Notably in particular,~~ contrail observations from ground-based cameras ~~can provide specific advantages over an~~  
~~address some of the~~ satellites, ~~particularly~~ ~~limitations because they can be set up at a lower relative cost, are effective in~~  
observing ~~the contrail~~ formation and ~~the early stages of their lifecycle evolution of young contrails at very high temporal and~~  
~~spatial resolutions,~~ and ~~are capable of~~ detecting optically thin contrails (Mannstein et al., 2010). However, previous research  
~~that utilised using~~ ground-based instruments ~~has~~ predominantly focused on natural cirrus observations (Feister et al., 2010;  
80 Long et al., 2006; Seiz et al., 2007), ~~and with only~~ two small-scale studies ~~have compared~~ a total of 16 observed contrail  
properties (~~e.g.~~ 3D positions, width, and/or persistence) with model estimates (Rosenow et al., 2023; Schumann et al., 2013).  
Recognising the potential of ground-based cameras, this study aims to: (i) develop a ~~methodology for an algorithm to~~ detecting  
~~and tracking contrails over time and extracting their widths from analyse contrails that are observed by~~ ground-based camera  
90 ~~footages;~~ and (ii) ~~extend the use of camera observations to~~ evaluate ~~the~~ contrail observations against CoCiP simulations,  
85 ~~which are informed by meteorological data from a reanalysis numerical weather prediction (NWP) model, ed-contrail outputs~~  
~~from the CoCiP contrail model~~ on a larger-scale ~~than compared to~~ prior studies.

## 2 Materials and methods

This section describes the contrail observations ~~that were captured provided~~ by the ground-based camera (Section 2.1), the  
workflow that is used to simulate the formation and evolution of contrails (Section 2.2), and the methods used to superimpose  
90 the actual flight trajectories and simulated contrails onto the video footage (Section 2.3) and to compare between the observed  
and simulated contrails properties (Section 2.4). ~~Figure~~ 1 provides an overview of the step-by-step process and datasets used  
to compare the ground-based contrail observations with the simulated contrail outputs.



95 **Figure 1: Overview of the step-by-step process and datasets used to compare the ground-based contrail observations with the simulated contrail outputs from CoCiP.**

### 2.1 Contrail observations

100 Contrail observations were made using a Raspberry Pi Camera Module v2.1 which features an 8 Megapixel sensor (3280 x 2464 pixels), a wide-angle field of view spanning 62.2° horizontally and 48.8° vertically, and a focal length of 3.04 mm (Raspberry Pi, n.d.). The camera was positioned at Imperial College London’s South Kensington Campus (51.4988°N, 0.1788°W) at an elevation of 25 m and pitched at a 25° angle above the horizontal plane. Recordings were taken between October-2021 and April-2022 during daylight hours, and at a temporal resolution of 5 seconds per frame. The captured footage is then filtered to remove the time intervals with low-level clouds and poor visibility (i.e., nighttime and periods with significant glare from direct sunlight) (Appendix A1). This filtering results in a final dataset containing 14 h of video footage collected over 5 different days, and 283 unique flights were observed during these specific time frames.

## 105 2.2 Contrail simulation

The formation and evolution of contrails that were observed by the video footage are simulated using CoCiP (Schumann, 2012). ~~For this study, we use the CoCiP algorithm hosted in the open-source contrail model that can now be accessed via the pycontrails repository v0.52.2 on GitHub~~ (Shapiro et al., 2024). Several datasets and methods are required as inputs to CoCiP, including the: (i) actual flight trajectories; (ii) historical meteorology and radiation fields; and (iii) aircraft performance and emissions estimates.

### 2.2.1 Flight trajectories and waypoint properties

The trajectories for each flight were derived using the raw Automatic Dependent Surveillance – Broadcast (ADS-B) telemetry that was purchased from Spire Aviation (Teoh et al., 2024b). Each ADS-B waypoint contains the unique flight identifier (call sign and flight number) and its corresponding 4D position (longitude, latitude, barometric altitude, and time) provided at time intervals of 40 s, and we filter the dataset to only include waypoints ~~that were broadcasted~~ within a defined spatial bounding box (40 – 60° N and 10° W – 10° E/40°W, 40°N, 10°E, 60°N) that extends ~~approximately~~  $\pm 10^\circ$  in longitude and latitude from camera’s location.

The ~~interpolated temperature and wind vectors are used to estimate the Mach number at each flight waypoint. These meteorological variables are then used as inputs to the~~ Base of Aircraft Data Family 4.2 (BADA 4) aircraft performance model (EUROCONTROL, 2016) ~~is used~~ to estimate the: (i) fuel mass flow rate; (ii) change in aircraft mass, assuming that the initial aircraft mass at the first known waypoint is ~~equal set~~ to the nominal (~~reference~~) mass ~~that is~~ provided by BADA; ~~and~~ (iii) overall efficiency ( ~~$\eta$~~ ); ~~and~~ (iv) engine thrust. ~~We then estimate~~ The aircraft-engine specific non-volatile particulate matter (nvPM) number emissions index (EI<sub>n</sub>), ~~which strongly influences the initial contrail ice crystal properties, is estimated by interpolating the according to~~ Teoh et al. which utilises the  $T_4/T_2$  methodology when the nvPM emissions profile for the specific aircraft-engine type is covered in engine-specific nvPM emissions profile from the ICAO Aircraft Engine Emissions Databank (EDB) (EASA, 2021) ~~relative to the non-dimensional engine thrust settings or the fractal aggregates (FA) model if the engine-specific nvPM data is not available~~ (Teoh et al., 2024b). All flights are assumed to be powered by conventional Jet A-1 fuel.

### 2.2.2 Meteorology

The historical 4D meteorological fields within the defined spatial bounding box (between 40 – 60° N and 10° W – 10° E) were provided by the European Centre for Medium Range Weather Forecast (ECMWF) ERA5 high-resolution realisation (HRES) reanalysis (ECMWF, 2021; Hersbach et al., 2020) at a spatial resolution of 0.25° longitude  $\times$  0.25° latitude over 37 pressure levels and at a 1 h temporal resolution. For each flight waypoint, the local meteorology is estimated from a quadrilinear interpolation across the three space coordinates and time (Schumann, 2012).

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We apply the humidity correction methodology from Teoh et al. (2022a) to ensure that the ERA5-derived RHi has a probability density function that is consistent with in-situ measurements from the In-service Aircraft for a Global Observing System (IAGOS) dataset (Boulangier et al., 2022; Petzold et al., 2015),

$$\text{RHi}_{\text{corrected}} = \begin{cases} \frac{\text{RHi}}{a_{\text{opt}}} & \text{for } \left(\frac{\text{RHi}}{a_{\text{opt}}}\right) \leq 1 \\ \min\left(\left(\frac{\text{RHi}}{a_{\text{opt}}}\right)^{b_{\text{opt}}}, \text{RHi}_{\text{max}}\right) & \text{for } \left(\frac{\text{RHi}}{a_{\text{opt}}}\right) > 1 \end{cases} \quad (1)$$

where  $\text{RHi}_{\text{max}} = 1.65$ ,  $a_{\text{opt}} = 0.9779$  and  $b_{\text{opt}} = 1.635$ . Eq. (1) is expected to be applicable to this study because its coefficients were calibrated using RHi measurements over the North Atlantic (40 – 75° N and 50 – 10° W), which corresponds to the same latitude band as our study domain (40 – 60° N and 10° W – 10° E). While Eq. (1) improves the goodness of fit between the measured and ERA5-derived RHi distribution and corrects for average biases (Teoh et al., 2022a), we note that it does not correct for the RHi errors at specific waypoints (Teoh et al., 2024a). Thus, RHi uncertainties at each waypoint can remain significant.

We note that corrections were applied to the ERA5 HRES humidity fields to ensure that the RHi distribution is consistent with in-situ measurements from the In-service Aircraft for a Global Observing System (IAGOS) dataset each flight waypoint, the local meteorology is estimated from a quadrilinear interpolation across the three-space coordinates and time

### 2.2.3 Aircraft performance and nvPM emissions

#### 2.2.3 Contrail cirrus prediction model

CoCiP assumes that contrails form when the ambient temperature ( $T_{\text{amb}}$ ) at the flight waypoint is below the SAC threshold temperature ( $T_{\text{SAC}}$ ) which is estimated by,

$$T_{\text{SAC}}[\text{K}] = (273.15 - 46.46) + 9.43 \ln(G - 0.053) + 0.72 [\ln(G - 0.053)]^2 \quad (2)$$

where  $G$  is the gradient of the mixing line in a temperature-humidity diagram,

$$G = \frac{E_{\text{H}_2\text{O}} p_{\text{amb}} c_p R_1}{Q_{\text{fuel}} (1-\eta) R_0} \quad (3)$$

$E_{\text{H}_2\text{O}}$  is the water vapour emissions index and assumed to be  $1.237 \text{ kg kg}^{-1}$  for Jet A-1 (Gierens et al., 2016),  $\eta$  is provided by the aircraft performance model (Section 2.2.1),  $p_{\text{amb}}$  is the pressure altitude at each waypoint,  $c_p$  is the isobaric heat capacity of dry air ( $1004 \text{ J kg}^{-1} \text{ K}^{-1}$ ), and  $R_1$  ( $461.51 \text{ J kg}^{-1} \text{ K}^{-1}$ ) and  $R_0$  ( $287.05 \text{ J kg}^{-1} \text{ K}^{-1}$ ) are the gas constant for water vapour and dry air respectively.

Two successive waypoints that satisfy the SAC forms a contrail segment that can either be short-lived or persistent (Schumann, 1996). A parametric wake vortex model is then used to simulate the wake vortex downwash (Holzapfel, 2003), of

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160 which CoCiP assumes that the process is instantaneous and does not resolve the temporal evolution of the wake vortex (Schumann, 2012), and persistent contrails in CoCiP are defined when their post-wake vortex ice water content (IWC) remains above  $10^{-12}$  kg  $\text{kg}^{-1}$ . The persistent contrail width ( $W$ ) and depth ( $D$ ) in CoCiP, defined as the dimensions along the y- and z-axis of a Gaussian plume, are initialised as,

$$165 W_{t=0} = \frac{\pi}{4} S_w \quad (4)$$

$$D_{t=0} = 0.5 \times dZ_{\max} \quad (5)$$

where  $S_w$  is the aircraft wingspan and  $dZ_{\max}$  is the maximum vertical displacement of the contrail mid-point after the wake vortex breakup.

The evolution of these persistent contrail segments different contrail properties is then simulated using a first order Euler method Runge-Kutta scheme with the model time steps ( $dt$ ) of 40 s. More specifically, the change in contrail dimensions over time are estimated as,

$$170 W_t = \sqrt{8\sigma_{yy}} \quad (6)$$

$$D_t = \sqrt{8\sigma_{zz}} \quad (7)$$

where  $\sigma$  is a dispersion matrix that captures the spread of the contrail plume along the y- and z-axes.  $\sigma$  is influenced by various factors such as wind shear, contrail segment length, diffusivity, and  $dZ$  (Schumann, 2012). CoCiP assumes that the contrail segment is sublimated when it's until the ice particle number concentration or optical depth drops below  $10^3 \text{ m}^{-3}$  and  $10^{-6}$ , respectively, or when the mid-point of the contrail plume advects beyond the simulation domain of interest ( $40 - 60^\circ \text{ N}$  and  $10^\circ \text{ W} - 10^\circ \text{ E}$ ). We specifically selected a  $dt$  that is significantly smaller than the typical range that was used in previous studies (1800–3600 s) (Schumann et al., 2015; Teoh et al., 2020a, 2022a) to superimpose the simulated contrail outputs to the video footage and perform a more comprehensive assessment of the early-stage contrail evolution.

### 2.3 Camera transformation model

Before comparing the camera observations with aircraft positions and simulated CoCiP outputs, we first correct any radial and tangential distortion of the video footage using the OpenCV homography method (Bradski, 2000), specifically applying the chessboard calibration technique (Tsai, 1987; Wu et al., 2015) described in Appendix A2. After correcting for distortions, we project the simulated contrail waypoints and dimensions onto the video footage using a camera transformation model which that follows a two-step process: (i) the real-world 3D positions (i.e., ADS-B flight waypoints and the simulated mid-point and edges of the contrail plumes) are mapped to a 3D camera coordinate system ( $X, Y, Z$ ) using an extrinsic (rotation) matrix; followed by (ii) transforming the 3D camera coordinates ( $X, Y, Z$ ) to a 2D pixel coordinate system ( $u, v$ ) using an intrinsic (camera) matrix. Further details of the camera transformation model can be found in Appendix A3. Figures 2 and 3 provides

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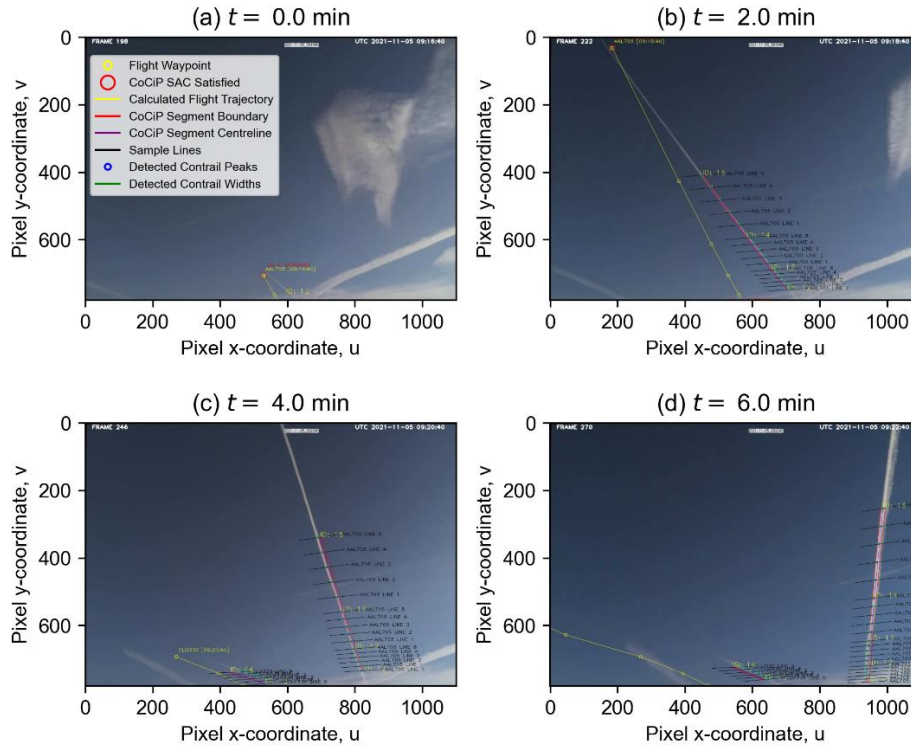
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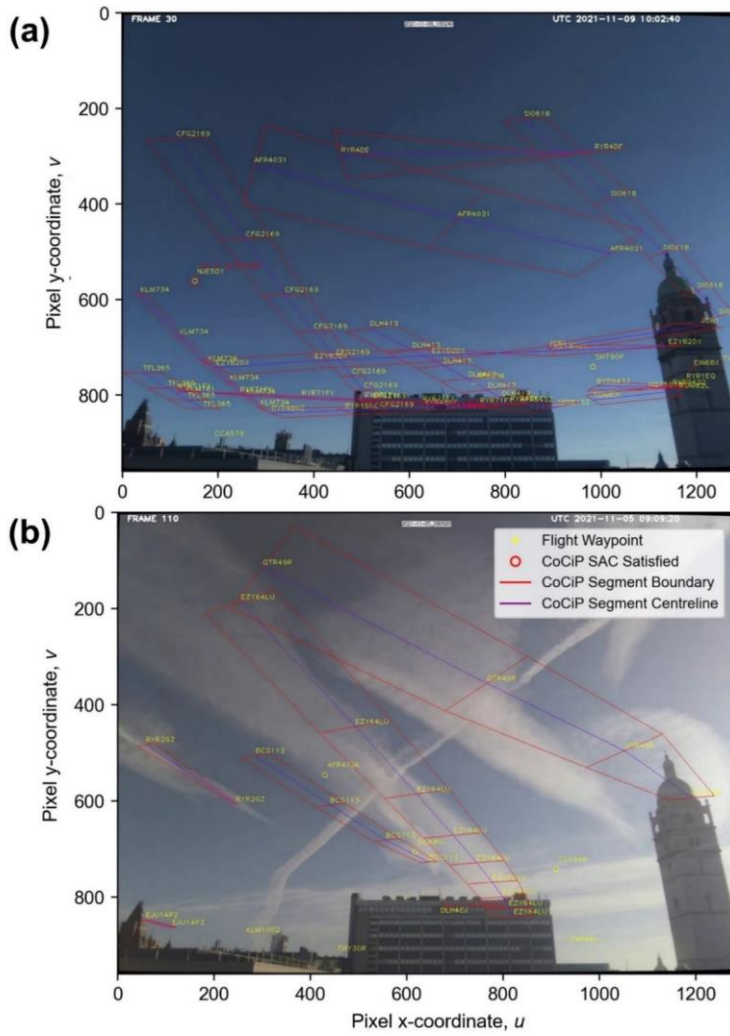
190 an examples of the superimposed flight trajectories and/or simulated contrail properties to the video footage at time intervals of 40 s.



195 **Figure 2:** Example of the flight trajectories and simulated contrail properties-dimensions from CoCiP that are superimposed onto the video footage using the camera transformation model (detailed in Section 2.3)-c.f. Eq. (1) and Eq. (2). The flight trajectories and contrails were observed on 5-Nov-2021 between 09:16:40 and 09:22:40 (UTC). Note that the persistent contrails visible in the top right and lower right of panels (a) and (b) were formed outside the observation domain and subsequently drifted into the camera's field of view, and the absence of labels on these contrails suggests that they were most likely false negative outcomes ( $Y_{camera} \& N_{sim=CoCiP}$ ).

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200 [Figure 3: Examples of the simulated contrails that were initially formed outside the camera's observation domain and subsequently drifted into view on: \(a\) 9-Nov-2021 at 10:02:40 UTC; and \(b\) 5-Nov-2021 at 09:09:20 UTC. The CoCIP-simulated contrail dimensions are superimposed onto the video footage using the camera transformation model \(detailed in Section 2.3\). Note that the](#)

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absence of labels on some of the observed contrails in panel (b) indicates that they were most likely false negative outcomes ( $Y_{\text{Camera}}$  &  $N_{\text{Sim-CoCiP}}$ ).

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#### 2.4 Comparison between contrail observation and simulation

We visually compare the simulated contrail formation with observations and classify each ADS-B waypoint into four groups to quantify the probability of: (i) true positive cases  $P(Y_{\text{Camera}} \& Y_{\text{CoCiPSim}})$ , where the contrails are both formed at that waypoint is observed by the camera ( $Y_{\text{Camera}}$ ) and predicted in the simulation ( $Y_{\text{CoCiPSim}}$ ), i.e., SAC is fulfilled in CoCiP; (ii) true negative cases  $P(N_{\text{Camera}} \& N_{\text{CoCiPSim}})$ , where no contrails are observed ( $N_{\text{Camera}}$ ) and predicted ( $N_{\text{CoCiPSim}}$ ); (iii) false positive cases  $P(N_{\text{Camera}} \& Y_{\text{CoCiPSim}})$ , where contrails are predicted in the simulation but not observed; and (iv) false negative cases  $P(Y_{\text{Camera}} \& N_{\text{CoCiPSim}})$ , where contrails are observed but not predicted in the simulation. More specifically, we evaluate the accuracy of the contrail simulation workflow by first assessing whether it correctly identifies short-lived contrails based on the SAC (i.e.,  $T_{\text{emb}} < T_{\text{SAC}}$ ), noting correct and incorrect predictions as  $Y_{\text{Sim-SAC}}$  and  $N_{\text{Sim-SAC}}$ , respectively. Additionally, we also compare CoCiP's definition of persistent contrail formation (i.e., post wake vortex contrail  $\text{IWC} > 10^{-12} \text{ kg kg}^{-1}$ ) against observations, with accurate and missed predictions denoted as  $Y_{\text{Sim-CoCiP}}$  or  $N_{\text{Sim-CoCiP}}$ , respectively. In instances where multiple observed contrail segments ( $Y_{\text{Camera}}$ ) overlap and/or are closely clustered together, we assign them to the respective ADS-B waypoints through manual visual inspection of preceding frames (Segrin et al., 2007).

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All ADS-B waypoints with  $Y_{\text{Camera}}$  are further classified into three categories based on their observed contrail lifetimes; i.e., defined as the duration during which the contrail is present-observed within by the camera's field of view. The lifetime categories include: (i) short-lived contrails with observed-lifetimes of fewer than 2 minutes; (ii) contrails with observed lifetimes of between 2 and 10 minutes; and (iii) persistent contrails with observed-lifetimes of least 10 minutes (World Meteorological Organization, 2017). We note that the observed contrail lifetime in our study is restricted by the contrail either advecting out of the camera's field of view (see Fig. A2), becoming too small or faint to be visible in the footage, or sublimating within the observation domain.

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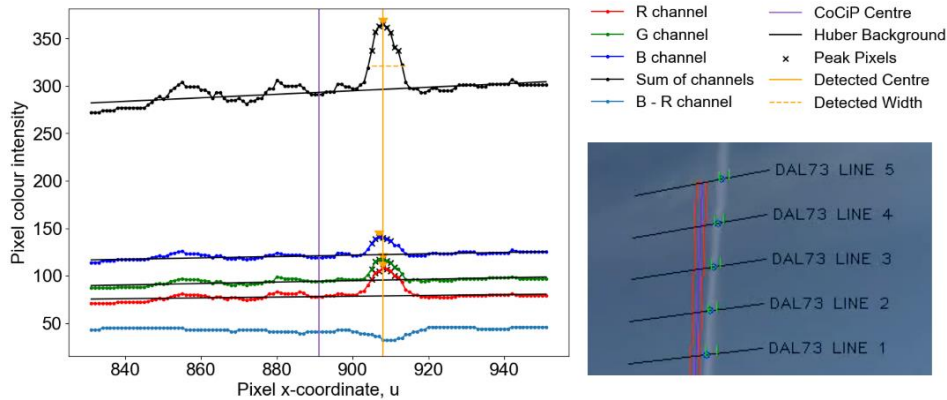


Figure 43: Pixel colour intensity profiles of the contrail waypoint at Line 5 (shown at the bottom right). Linear trendlines (in black) indicate the background colour intensity for each RGB channel. The solid vertical yellow and purple lines represent the mid-point of the observed and simulated contrail plume, respectively, while the dashed (horizontal) yellow line indicates the estimated contrail pixel width.

Additionally, for waypoints with true positive cases ( $Y_{\text{Camera}}$  &  $Y_{\text{Sim=CoCiP}}$ ), we also compare their observed lifetimes and evolving contrail width relative to the simulated CoCiP outputs. To estimate the observed contrail pixel width from the video footage, we apply the Bresenham (2010) line drawing algorithm at each ADS-B waypoint to extract: (i) a line of pixels orthogonal to the flight trajectory; and (ii) the Red-Green-Blue (RGB) colour channel intensity of these pixels (Fig. 43).

Previous studies found that the presence of clouds can be identified by their prominent increase in pixel intensity, especially in the red channel relative to the blue channel, because the sky scatters more blue than red light while clouds scatter both red and blue light equally (Long et al., 2006; Shields et al., 2013). However, due to day-to-day variability in atmospheric conditions, we were unable to consistently identify contrails from the video footage by applying a fixed threshold for the red-blue pixel intensity ratio. Instead, we compare the relative difference between the local pixel intensity ( $P_{u,v}$ ) and the modelled estimated background pixel intensity ( $\hat{P}_{u,v}^B$ ), i.e., the estimated pixel intensity of the background sky assuming that the contrail is absent.

$$\Delta P_{u,v} = P_{u,v} - \hat{P}_{u,v}^B \quad (83)$$

Here, where  $\hat{P}_{u,v}^B$ , represented by the black line of best fit in the RGB plot of Fig. 4, is modelled-estimated using a Huber regression instead of a traditional least squares regression to minimise the regression sensitivity to outliers (Pedregosa et al., 2012). The observed contrail pixel width at each waypoint and time slice is then estimated from the video footage as follows,

$$\Delta P_{u,v} > \overline{\Delta P}_{u,v} + 2\sigma(\Delta P_{u,v}), \quad (94)$$

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where  $\overline{\Delta P_{u,v}}$  and  $\sigma(\Delta P_{u,v})$  are the mean and standard deviations of the line of pixels orthogonal to the flight trajectory respectively, and the mid-point of the observed plume determined by locating the local maximum of  $\Delta P_{u,v}$  (Fig. 43). The reverse camera transformation is then applied to convert the 2D plane pixel width to a geometric width within a 3D space. Notably, due to the lack of depth information from a single camera, we assume that observed contrail altitude is equal to the modelled contrail altitude from CoCiP. This assumption introduces an additional source of error in the observed geometric contrail width when compared to the pixel contrail width, which we discuss in Section 3.3 below.

### 3 Results and discussion

Section 3.1 compares the observed contrail formation with those predicted by the SAC and CoCiP. Section 3.2 evaluates the observed contrail lifetime against the ERA5-derived meteorology and simulated contrail lifetime, while Section 3.3 compares the temporal evolution of contrail width between the observation and simulation. Finally, Section 3.4 briefly explores the potential limitations in detecting contrails from the video footage. Across these sections, we discuss the known and potential factors that may contribute to the discrepancies between the observed and simulated contrail properties, while acknowledging that the list of factors may not be exhaustive.

This section evaluates the simulated contrail formation (Section 3.1), lifetime (Section 3.2), and width (Section 3.3) from CoCiP relative to observations from the video footage. Where possible, we also incorporate additional variables into the analysis, such as the specific aircraft characteristics and local meteorology at each waypoint, to better understand the factors influencing the agreement between the observed and simulated contrail properties.

#### 3.1 Contrail formation

A total of 1,582,619 unique waypoints from 2813 flights were identified across five days of video footage. Contrail formation was observed in 59.6% of these waypoints ( $Y_{\text{Camera}}$ ), 81.6% of these waypoints satisfied the SAC in the simulation ( $Y_{\text{Sim-SAC}}$ ), and 44.2% formed persistent contrails according to CoCiP's definition ( $Y_{\text{Sim-CoCiP}}$ ) (Table 1). Table 1 shows that when evaluated using the SAC, the simulation correctly predicted the contrail formation and absence of contrails for 75.869.3% of the flight waypoints, i.e., true positives  $P(Y_{\text{Camera}} \& Y_{\text{CoCiP-Sim-SAC}} = 58.5\%)$  of 32.9% plus true negatives  $P(N_{\text{Camera}} \& N_{\text{CoCiP-Sim-SAC}} = 17.3\%)$  of 36.4%, of which: (i) true positive waypoints are always formed above 30,000 feet; while (ii) true negative waypoints were always formed below 32,000 feet where warmer temperatures limit contrail formation, or above 40,000 feet where drier stratospheric conditions are more common (Fig. 5a). In contrast, the SAC incorrectly predicted contrail formation in 24.2% of the waypoints, where the false positives ( $N_{\text{Camera}} \& Y_{\text{Sim-SAC}} = 23.1\%$ ) significantly outweigh the false negatives ( $Y_{\text{Camera}} \& N_{\text{Sim-SAC}} = 1.1\%$ ). This overestimation in contrail formation by the SAC may be due to observation challenges, as false positive waypoints were often associated with very low RHi's ( $0.62 \pm 0.38$  at  $1\sigma$ , Fig. 6b) relative to true positive waypoints ( $0.90 \pm 0.30$  at  $1\sigma$ , Fig. 6a), potentially resulting in very short-lived or faint contrails that might not be detected by cameras (Fig. 3a). Other factors that may influence the SAC accuracy include uncertainties in: (i)

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$T_{amb}$  from the ERA5 HRES; (ii)  $T_{SAC}$ , resulting from modelling errors in  $\eta$ , c.f. Eq. (2) and (3), and the assumption of homogenous plume mixing; and (iii) soot activation at  $T_{amb} \approx T_{SAC}$ , which are likely incomplete (Bräuer et al., 2021) and becomes strongly dependent on the soot dry core radius and hygroscopicity that are not accounted for by the SAC (Bier et al., 2022). Indeed, contrails at waypoints with incorrect predictions were generally formed at higher temperatures ( $dT_{SAC} = T_{amb} - T_{SAC} = -7.8 \pm 4.3$  K at  $1\sigma$ ) compared to true positive waypoints ( $dT_{SAC} = -12.8 \pm 3.7$  K at  $1\sigma$ ) (Fig. 5a).

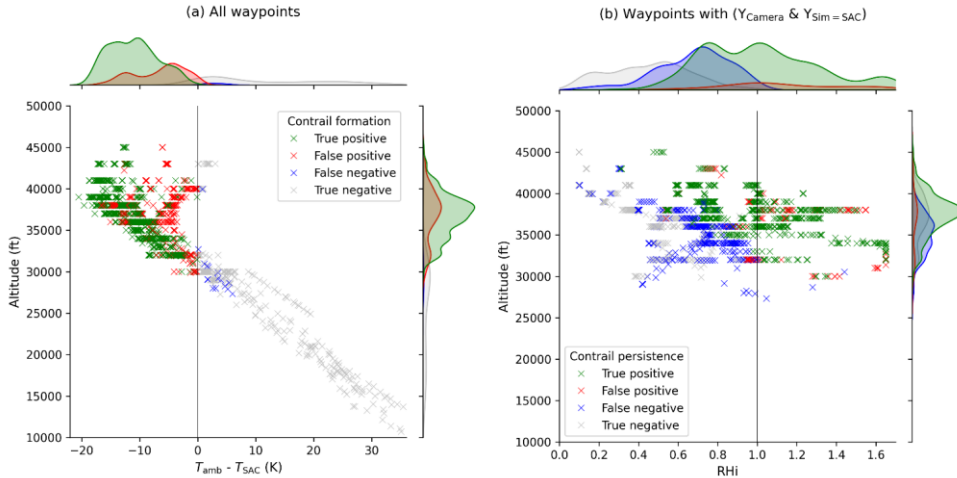


Figure 5: Joint plot of the aircraft barometric altitude versus the: (a) difference between the ambient ( $T_{amb}$ ) and SAC threshold temperature ( $T_{SAC}$ ) across all flight waypoints; and (b) the corrected RH from the ERA5 HRES for waypoints that satisfy the SAC in the simulation and have contrails observed from the camera ( $Y_{Camera} \& Y_{Sim=SAC}$ ). In both figures, green data points represent true positive outcomes ( $Y_{Camera} \& Y_{Sim}$ ), red for false positive outcomes ( $N_{Camera} \& Y_{Sim}$ ), blue for false negative outcomes ( $Y_{Camera} \& N_{Sim}$ ), and grey for true negative outcomes ( $N_{Camera} \& N_{Sim}$ ).

However, the percentage of false negative outcomes,  $P(Y_{Camera} \& N_{CoCIP}) = 25.9\%$ , is 5.4 times larger than the false positive outcome,  $P(N_{Camera} \& Y_{CoCIP}) = 4.8\%$ , which suggests that the simulation exhibits a: (i) specificity of 88.3%, i.e.,  $P(N_{CoCIP} | N_{Camera}) = \frac{P(N_{Camera} \& N_{CoCIP})}{P(N_{Camera} \& N_{CoCIP}) + P(N_{Camera} \& Y_{CoCIP})}$  which is the proportion of actual negatives that is correctly predicted by the model; (ii) precision of 87.3%, i.e.,  $P(Y_{Camera} | Y_{CoCIP}) = \frac{P(Y_{Camera} \& Y_{CoCIP})}{P(Y_{Camera} \& Y_{CoCIP}) + P(N_{Camera} \& Y_{CoCIP})}$  which is the proportion of predicted positives that are true positives; and (iii) sensitivity of 56.0%, i.e.,  $P(Y_{CoCIP} | Y_{Camera}) = \frac{P(Y_{Camera} \& Y_{CoCIP})}{P(Y_{Camera} \& Y_{CoCIP}) + P(Y_{Camera} \& N_{CoCIP})}$  which is the proportion of actual positives that are correctly predicted by the model. In other words, the simulation is more likely to correctly predict the observed outcomes on the presence/absence of contrails (high specificity and precision), but it could underestimate the observed contrail formation (low sensitivity).

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Using CoCiP's definition of persistent contrail formation (i.e., post wake vortex contrail IWC  $\geq 10^{12}$  kg kg<sup>-1</sup>), the overall correct contrail predictions across five days decreased slightly from 75.8% (SAC approach) to 73.1%, with significant variability between individual days (Table 1). Unlike with the SAC, the percentage of false negative waypoints ( $Y_{\text{Camera}}$  &  $N_{\text{Sim-CoCiP}} = 21.2\%$ ) is nearly four times higher than the false positive waypoints ( $N_{\text{Camera}}$  &  $Y_{\text{Sim-CoCiP}} = 5.7\%$ ) (c.f.  $Y_{\text{Camera}}$  &  $N_{\text{Sim-SAC}} = 1.1\%$  vs.  $N_{\text{Camera}}$  &  $Y_{\text{Sim-SAC}} = 23.1\%$ ). This underprediction of persistent contrail formation is most likely due to contrail model simplifications, where adiabatic heating from the wake vortex downwash is assumed to occur instantaneously which can underestimate the simulated contrail lifetime compared to observations for short-lived contrails. False negative waypoints also tend to occur at lower altitudes ( $35100 \pm 2600$  feet at  $1\sigma$ ) and at sub-saturated RH conditions ( $0.68 \pm 0.19$  at  $1\sigma$ ) relative to those with true positive outcomes ( $37500 \pm 2700$  feet and  $1.02 \pm 0.29$ ) (Fig. 5b). Notably, on 14-Jan-2022, correct contrail predictions dropped sharply from 83.8% to 42.9%, with no persistent contrails predicted in the simulation, because the ERA5-derived RH<sub>i</sub> at all waypoints were well below ice supersaturation ( $0.07\text{--}0.79$ , Fig. 6).

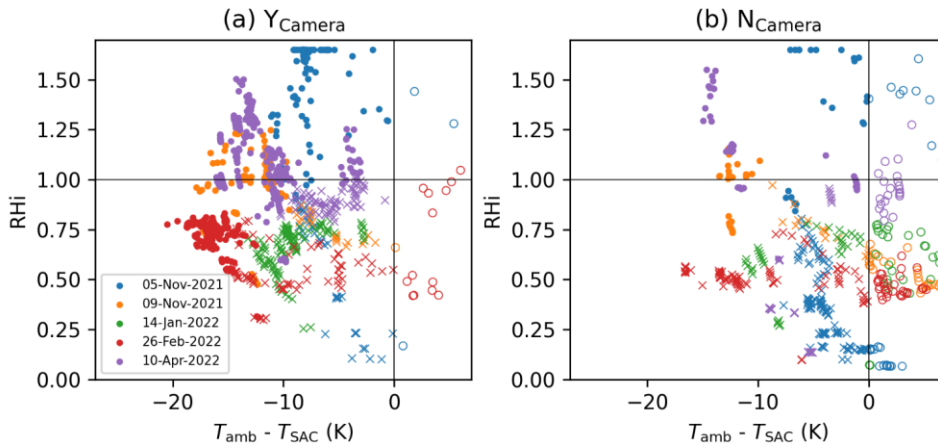


Figure 6: Corrected RH<sub>i</sub> from the ERA5 HRES versus the difference between the ambient ( $T_{\text{amb}}$ ) and SAC threshold temperature ( $T_{\text{SAC}}$ ) for all waypoints across five days: (a) with; and (b) without contrails observed from the video footage. In both plots, data points with no fill (circles) represent waypoints where contrails did not form in the simulation ( $N_{\text{Sim-SAC}}$ ), crosses indicate waypoints that satisfied the SAC in the simulation ( $Y_{\text{Sim-SAC}}$ ), and filled data points denote waypoints where persistent contrails were formed in the simulation ( $Y_{\text{Sim-CoCiP}}$ ).

We evaluate the impact of aircraft cruise altitude on contrail observations and model performance (Fig. 4a). In general, contrails are most likely to be observed by the camera at altitudes between 34,000 and 38,000 ft where  $P(Y_{\text{Camera}}) > 60\%$ . Across all altitudes, the false positive rate,  $P(Y_{\text{CoCiP}}|N_{\text{Camera}}) = \frac{P(Y_{\text{CoCiP}} \& N_{\text{Camera}})}{P(Y_{\text{CoCiP}} \& N_{\text{Camera}}) + P(N_{\text{CoCiP}} \& N_{\text{Camera}})}$ , tends to range between 0% and 25%.

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Two factors likely contribute to this error: (i) the known limitations in the ERA5 HRES humidity fields; and (ii) sub-grid scale RHI variabilities that cannot currently be resolved from the spatiotemporal resolution of the ERA5 HRES (0.25° longitude × 0.25° latitude over 37 pressure levels provided at hourly time intervals). For (i), although corrections were applied to the humidity fields to ensure that the RHI distribution from the ERA5 HRES is consistent with in-situ measurements (Section 2.2.2), we note that the RHI uncertainties and errors remains large at the waypoint level

**Table 1: Summary statistics for each day when contrails were observed by the camera.** For each of the five days, the observed and a comparison of the contrail formation from the video footage is compared with the two different definitions of contrail formation in the simulation, i.e., using the SAC ( $T_{\text{amb}} < T_{\text{SAC}}$ ) and CoCiP's definition of persistent contrail formation (post wake vortex contrail  $\text{IWC} > 10^{-12} \text{ kg kg}^{-1}$ ) predictive accuracy from CoCiP relative to the camera observations for each day. The notation  $Y_{\text{Camera}}$  indicates that the camera observed contrails forming at the flight waypoint,  $N_{\text{Camera}}$  indicates that no contrails at the flight waypoint were observed by the camera,  $Y_{\text{CoCiP}}$  indicates that the CoCiP simulation estimates the formation of contrails at the flight waypoint, while  $N_{\text{CoCiP}}$  indicates that the CoCiP simulation did not predict contrails forming at the flight waypoint.

Date	Hours	Number of flights	Number of waypoints	Waypoints				Correct prediction <sup>*</sup>
				$P(Y_{\text{Camera}} \& Y_{\text{CoCiP}})$	$P(N_{\text{Camera}} \& Y_{\text{CoCiP}})$	$P(Y_{\text{Camera}} \& N_{\text{CoCiP}})$	$P(N_{\text{Camera}} \& N_{\text{CoCiP}})$	
05-Nov-2021	2	62	328	25.3%	7.3%	13.4%	54.0%	79.3%
09-Nov-2021	2	39	227	43.2%	7.9%	18.9%	30.0%	73.2%
14-Jan-2022	4	39	215	0.0%	0.0%	58.1%	41.9%	41.9%
26-Feb-2022	3	73	420	38.6%	0.2%	26.0%	35.2%	73.8%
10-Apr-2022	3	70	429	44.3%	7.9%	23.1%	24.7%	69.0%
<b>TOTAL</b>	<b>14</b>	<b>283</b>	<b>1619</b>	<b>32.9%</b>	<b>4.8%</b>	<b>25.9%</b>	<b>36.4%</b>	<b>69.3%</b>

\* The correct prediction is calculated by  $P(Y_{\text{Camera}} \& Y_{\text{CoCiP}}) + P(N_{\text{Camera}} \& N_{\text{CoCiP}})$ .

Date	05-Nov-2021	09-Nov-2021	14-Jan-2022	26-Feb-2022	10-Apr-2022	TOTAL
Times (UTC)	09:00 – 11:00	09:00 – 11:00	10:00 – 14:00	07:00 – 09:00, 11:00 – 12:00	08:00 – 11:00	-
Hours	2	2	4	3	3	14
Number of flights	62	39	38	73	69	281
Number of waypoints	317	223	210	419	413	1582
$dT_{\text{SAC}}$ , all waypoints (K) <sup>a</sup>	$-3.0 \pm 7.3$	$-7.5 \pm 8.7$	$-3.2 \pm 10.9$	$-8.6 \pm 11.5$	$-6.3 \pm 10.3$	<b><math>-6.0 \pm 10.2</math></b>
RHI, all waypoints <sup>a</sup>	$0.80 \pm 0.56$	$0.85 \pm 0.22$	$0.61 \pm 0.15$	$0.61 \pm 0.17$	$1.0 \pm 0.26$	<b><math>0.78 \pm 0.35</math></b>
<b>Contrail formation<sup>b</sup></b>						
$P(Y_{\text{Camera}} \& Y_{\text{Sim=SAC}})$	38.9%	62.8%	57.1%	61.6%	68.8%	<b>58.5%</b>
$P(N_{\text{Camera}} \& Y_{\text{Sim=SAC}})$	45.3%	17.5%	16.2%	18.9%	16.9%	<b>23.1%</b>
$P(Y_{\text{Camera}} \& N_{\text{Sim=SAC}})$	0.9%	0.4%	0.0%	3.1%	0.0%	<b>1.1%</b>
$P(N_{\text{Camera}} \& N_{\text{Sim=SAC}})$	14.9%	19.3%	26.7%	16.4%	14.3%	<b>17.3%</b>
Correct prediction <sup>d</sup>	53.8%	82.1%	83.8%	78.0%	83.1%	<b>75.8%</b>
<b>Contrail persistence<sup>c</sup></b>						
$P(Y_{\text{Camera}} \& Y_{\text{Sim=CoCiP}})$	26.9%	53.4%	0.0%	44.9%	52.1%	<b>38.4%</b>
$P(N_{\text{Camera}} \& Y_{\text{Sim=CoCiP}})$	7.6%	10.7%	0.0%	0.7%	9.7%	<b>5.7%</b>

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$P(Y_{\text{Camera}} \& N_{\text{Sim=CoCiP}})$	13.0%	9.9%	57.1%	19.8%	16.7%	<b>21.2%</b>
$P(N_{\text{Camera}} \& N_{\text{Sim=CoCiP}})$	52.5%	26.0%	42.9%	34.6%	21.5%	<b>34.7%</b>
<b>Correct prediction<sup>d</sup></b>	<b>79.4%</b>	<b>79.4%</b>	<b>42.9%</b>	<b>79.5%</b>	<b>73.6%</b>	<b>73.1%</b>

<sup>a</sup> Mean and one standard deviation across all waypoints, as derived from the ERA5 HRES. For each of the five days, the ambient meteorological conditions across all flight waypoints are visualised in Fig. 6.

<sup>b</sup> Contrail formation in the simulation is determined by the SAC, where  $Y_{\text{Sim=SAC}}$  denotes that  $T_{\text{amb}} < T_{\text{SAC}}$ , and  $N_{\text{Sim=SAC}}$  denotes that  $T_{\text{amb}} > T_{\text{SAC}}$ .

<sup>c</sup> Contrail persistence in the simulation is determined by CoCiP, where  $Y_{\text{Sim=CoCiP}}$  denotes that the post wake vortex contrail  $\text{IWC} > 10^{-12} \text{ kg kg}^{-1}$  and  $N_{\text{Sim=CoCiP}}$  denotes that the contrail  $\text{IWC} < 10^{-12} \text{ kg kg}^{-1}$ .

<sup>d</sup> The correct prediction is calculated by  $(Y_{\text{Camera}} \& Y_{\text{Sim}}) + (N_{\text{Camera}} \& N_{\text{Sim}})$ .

The false negative rate,  $P(N_{\text{CoCiP}} | Y_{\text{Camera}}) = \frac{P(N_{\text{CoCiP}} \& Y_{\text{Camera}})}{P(N_{\text{CoCiP}} \& Y_{\text{Camera}}) + P(Y_{\text{CoCiP}} \& Y_{\text{Camera}})}$ , exhibits a negative linear relationship with

altitude, where  $P(N_{\text{CoCiP}} | Y_{\text{Camera}})$  is: (i) above 80% at altitudes below 30,000 feet, meaning that a significant fraction of contrails observed at lower altitudes are not being predicted in the simulation; (ii) around 50–80% between 30,000 and 38,000 feet; and (iii) below 30% at altitudes above 38,000 feet (Fig. 4a). These error patterns can most likely be attributed to the warmer temperatures at lower altitudes resulting in  $T_{\text{amb}} \sim T_{\text{SAC}}$  where: (i) small errors in  $T_{\text{amb}}$  and the estimated  $T_{\text{SAC}}$  is likely to have a significant impact on contrail formation predictions; and (ii) the microphysics of soot activation at  $T_{\text{amb}} \sim T_{\text{SAC}}$  becomes strongly dependent on various soot properties such as the geometric mean dry core radius and hygroscopicity, but CoCiP does not currently account for these effects. Indeed, a comparison between the difference in ambient and SAC threshold temperature

( $dT_{\text{SAC}} = T_{\text{amb}} - T_{\text{SAC}}$ ) shows that the false discovery rate,  $P(N_{\text{Camera}} | Y_{\text{CoCiP}}) = \frac{P(N_{\text{Camera}} \& Y_{\text{CoCiP}})}{P(N_{\text{Camera}} \& Y_{\text{CoCiP}}) + P(Y_{\text{Camera}} \& Y_{\text{CoCiP}})}$ , is largest when  $dT_{\text{SAC}} > 2.5 \text{ K}$  (77.2%), and smallest when  $dT_{\text{SAC}} < -10 \text{ K}$  (9.3%) (Fig. 4b).

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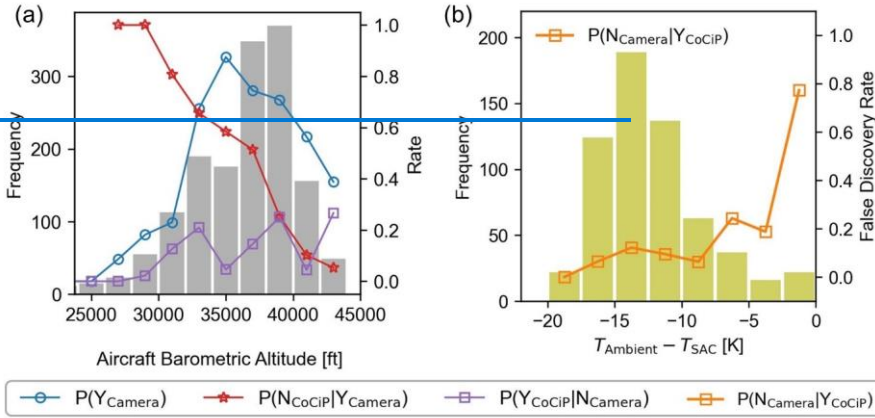


Figure 4: Probability density function of the: (a) aircraft barometric altitude; and (b) difference between the ambient and SAC threshold temperature for ADS-B waypoints with observed and/or simulated contrails. Additional statistics on probability of waypoints with contrail observations,  $P(Y_{Camera})$  (blue line), and conditional probabilities  $P(N_{CoCIP}|Y_{Camera})$  (red line),  $P(Y_{CoCIP}|N_{Camera})$  (purple line), and  $P(N_{Camera}|Y_{CoCIP})$  (orange line) are also included in these figures.

### 3.2 Contrail observed lifetime

Among the 94253 unique waypoints with observed contrails ( $Y_{Camera}$ ), 73.32% of them ~~contrails formed~~ are short-lived with observed lifetimes of less than ( $\ll 2$  minutes). Of these short-lived contrails, 99.3% of them either became too small to be tracked or sublimated within the camera's field of view, while 0.7% advected out of it. Contrails with observed lifetimes ranging ~~10.6% of them are contrails with observed lifetimes of~~ between 2 and 10 minutes made up 12.5% of the observations, with 36% of them drifting beyond the camera's field of view. The remaining and 14.246.6% of contrails them are persistent contrails with had observed lifetimes exceeding 10 minutes, of which 64% of them advected beyond the camera's field of view. For waypoints with  $Y_{Camera}$ , we compared their observed contrail lifetimes against the ERA5-derived meteorology at the time of formation (Fig. 7). Our analysis shows that: (i) 98% of these contrails met the SAC ( $T_{amb} < T_{SAC}$ ) in the simulation; (ii) 78% of short-lived contrails with observed lifetime under 2 minutes were formed under ice sub-saturated conditions ( $RH_i < 100\%$ ); and (iii) 75% of persistent contrails with observed lifetime exceeding 10 minutes were formed in ice supersaturated conditions ( $RH_i > 100\%$ ). The gradual decline in agreement between observations and NWP estimates over longer time periods suggests that the ERA5-derived temperature fields are generally more accurate than the humidity fields, as noted in previous studies (Gierens et al., 2020; Reutter et al., 2020), thereby leading to more accurate predictions of contrail formation compared to contrail persistence.

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370 [Fig. 8](#) shows a poor visual agreement between the observed and simulated contrail lifetime, with the simulation generally underpredicting contrail lifetime when the ERA5-derived RH<sub>i</sub> is below 100% and could overestimate it when the RH<sub>i</sub> exceeds 100%. Several known factors likely contribute to this mismatch. Firstly, the ERA5 HRES humidity fields are known to have limitations, which often produce weakly supersaturated RH<sub>i</sub> estimates (Agarwal et al., 2022; Reutter et al., 2020; Teoh et al., 2022a). Although corrections were applied to ensure that the ERA5-derived RH<sub>i</sub> distribution is consistent with in-situ measurements (Section 2.2.2), the RH<sub>i</sub> uncertainties remain large at the waypoint level (Teoh et al., 2024a). Secondly, the spatial resolution of the ERA5 HRES (0.25° longitude × 0.25° latitude ≈ 18 × 28 km) is insufficient to capture the sub-grid scale RH<sub>i</sub> variabilities (Wolf et al., 2024). Here, we do not evaluate the effects of sub-grid scale RH<sub>i</sub> variabilities because of the small study domain, where the camera's field of view fits within 10 grid boxes of the ERA5 HRES (Fig. A2), and the limited sample size (n = 942 for waypoints with Y<sub>camera</sub> over 14 h). Thirdly, the maximum observed contrail lifetime can be capped by the contrail drifting out of the field of view or becoming too small or faint to be tracked (Fig. 3a).

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380 A further evaluation of these waypoints (Y<sub>camera</sub>) shows a weak negative correlation between dT<sub>SAC</sub> and the observed contrail lifetime (R = 0.168, as shown in Fig. 5). This finding is consistent with previous research, suggesting that contrails forming at lower temperatures tend to have a lower ice water content and smaller ice crystal radius which, in turn, can increase the contrail lifetime.

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385 Fig. 6 shows that the false negative rate,  $P(N_{CoCIP}|Y_{camera})$ , tends to decrease with increasing aircraft cruise altitude and the observed contrail lifetime.  $P(N_{CoCIP}|Y_{camera})$  is: (i) lowest for persistent contrails (observed lifetime > 10 min) forming above 35,000 feet, where  $P(N_{CoCIP}|Y_{camera}) < 5\%$ ; and (ii) largest for short lived contrails (observed lifetimes < 2 min) forming below 35,000 feet, where  $P(N_{CoCIP}|Y_{camera}) > 75\%$ . Consequently, around 92% of all waypoints with a false negative outcome,  $P(N_{CoCIP} \& Y_{camera})$ , are associated with short lived contrails (< 2 min). The contrail simulation also exhibits a low sensitivity,  $P(Y_{CoCIP}|Y_{camera}) = 44.5\%$ , when the observed contrails are short lived (< 2 min), but the sensitivity increases by approximately twofold to 86.5% when contrails have an observed lifetimes of > 2 min.

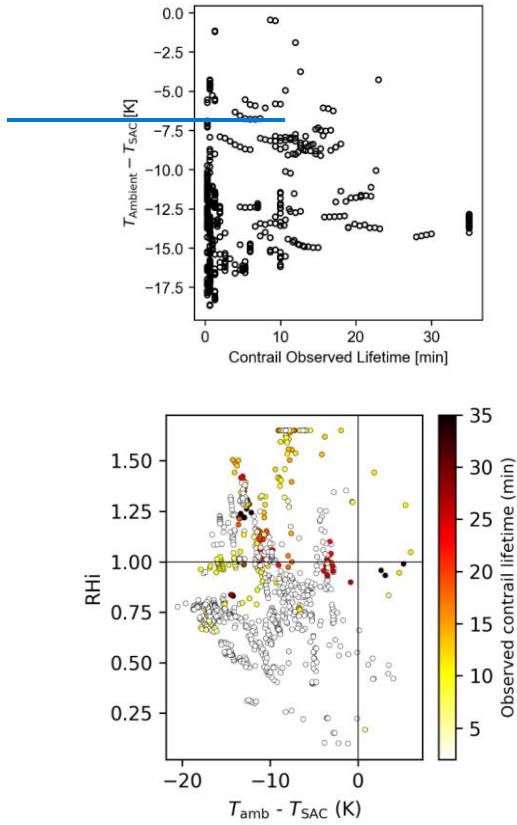


Figure 765: Comparison-Evaluation of the observed contrail lifetime relative to versus the ERA5-derived RHI (y-axis) and the difference between the ambient temperature ( $T_{\text{amb}}$ ) and SAC threshold temperature ( $T_{\text{SAC}}$ ) (x-axis) at the time of contrail formation. This analysis includes all for individual ADS-B flight waypoints with observed contrail true positive cases ( $Y_{\text{Camera}}$  &  $Y_{\text{CoCIP}}$ ).

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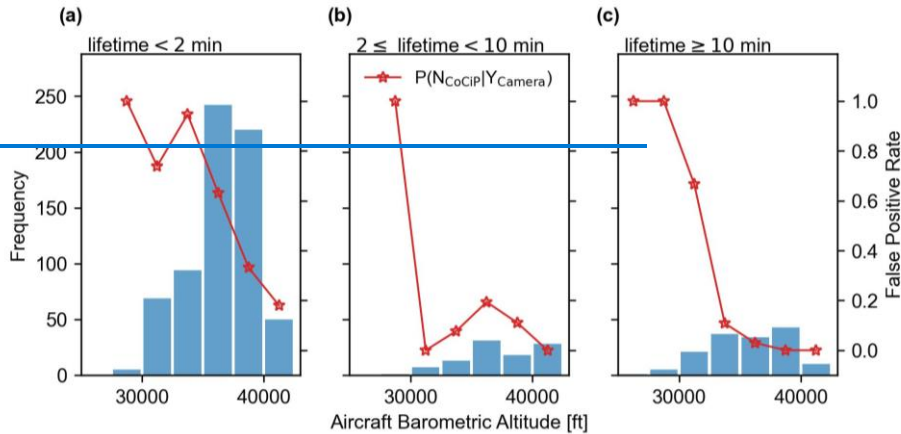


Figure 6: Histogram of the aircraft altitudes for ADS-B waypoints with observed contrails and their respective false positive rates (red lines) at each altitude bins. The waypoints are segmented into three groups based on their observed contrail lifetime: (a) short-lived contrails ( $< 2$  mins); (b) contrails that persist for 2–10 mins; and (c) persistent contrails ( $\geq 10$  mins).

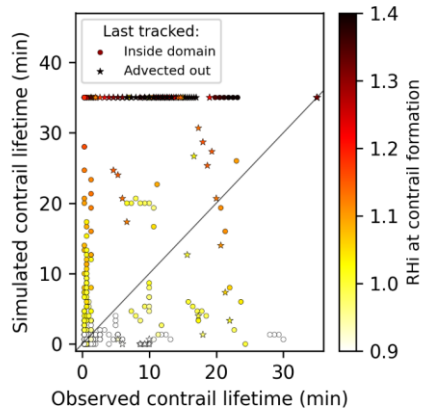


Figure 8: Comparison between the observed and simulated contrail lifetime for waypoints with true positive outcomes ( $Y_{camera} \& Y_{Sim=CoCIPI}$ ). Observed contrails are categorised based on their final known position: circles represent contrails that either sublimated or became too small or faint within the observation domain; while stars indicate that the contrail drifted out of the observation domain and can no longer be tracked. The colour bar represents the corrected ERA5-derived RH<sub>i</sub> at the time of contrail formation. The simulated contrail lifetime in this plot is constrained to 35 minutes to align with the maximum observed contrail lifetime.

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### 3.3 Contrail width

Fig. 2 illustrates the temporal evolution of the observed and simulated contrails that were formed by one flight, while Figure 97 compares the temporal evolution of the observed and simulated contrail pixel and geometric widths relative to the simulated CoCiP outputs for 70533 segments from all waypoints with true positive cases ( $Y_{\text{Camera}}$  &  $Y_{\text{Sim-CoCiP}}$ ) and observed lifetimes greater than 2 minutes. On average, our findings, as assessed by the root mean square error (RMSE) metric, suggest that the simulated contrail geometric widths are around 100 m smaller than the observed widths over the observed contrail lifetime, with the largest underestimations occurring within the first five minutes (-280 m, on average, Fig. 9b), tends to be smaller than the observed pixel width (by -6.8 pixels) and geometric width (by -330 m). These results are consistent with Schumann et al. and The tendency to underestimate the simulated contrail widths is consistent with Schumann et al. (2013) and can be attributed to several known factors, including: (i) uncertainties in could be caused by the: (i) potential underestimation of sub-grid scale wind shear and turbulent mixing, where their sub-grid scale variabilities cannot be resolved from the spatiotemporal resolution of the ERA5 HRES (Hoffmann et al., 2019; Paugam et al., 2010; Schumann et al., 2013); (ii); and (iii) contrail model errors resulting from the CoCiP's use of simplified physics, such as the Gaussian plume assumption which may not adequately represent the contrail cross-sectional area (Jensen et al., 1998b; Sussmann and Gierens, 1999; Unterstrasser and Gierens, 2010), instantaneous wake vortex assumption, and the initialisation of persistent contrail width solely based on the aircraft wingspan, c.f. Eq. (4), without considering wake vortex dynamics and ambient meteorology (Lewellen and Lewellen, 2001; Schumann, 2012); and (iii) Gaussian plume when simulating the evolution of contrails CoCiP's definition of the simulated contrail width (i.e., the length across the y-axis of a Gaussian plume), which is inherently shorter than the maximum possible observed contrail width (i.e., length across the major axis of an inclined ellipse). These factors are among those identified and may not be exhaustive.

In addition to errors in the simulated contrail width, independent error sources in the observed contrail widths also contribute to the poor visual agreement between the observed and simulated contrail widths (Fig. 9a). Firstly, the presence of other contrails and natural cirrus can affect the Huber regression used to identify the contrail edges, c.f., Eq. (9), thereby contributing to errors in the observed contrail pixel width (Fig. 3b). A visual comparison shows that the agreement between the observed and simulated contrail geometric width (Fig. 7b) is lower than the pixel width (Fig. 7a). The higher relative agreement between the observed and simulated contrail pixel width is partially explained by its dependence on the contrail camera distance, i.e., contrails further away have a smaller pixel width, which can be estimated with high accuracy. In contrast Secondly, converting the observed pixel width to geometric width introduces additional errors due to our estimate of the observed geometric width the lack of data on assumes that the: (i) contrail altitude, which we assume that the actual observed contrail altitude is equal to the simulated contrail altitude in CoCiP (Section 2.4); and (ii) inclination angle of the elliptical contrail plume, where parallax errors can contribute to a larger variability in the observed geometric width relative to the pixel width - contrail cross-section is a horizontal ellipse, meaning that the contrail edges are at the same altitude as the contrail mid-point. Assumption (i) is subject to uncertainties in the actual aircraft mass and local meteorology, resulting which can result in additional errors when

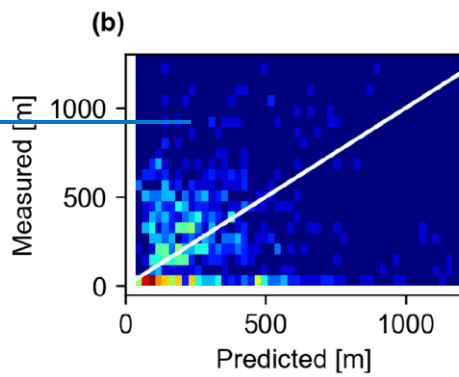
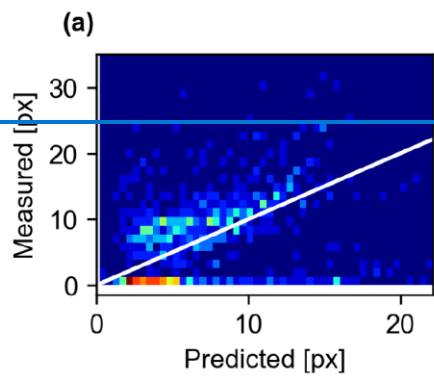
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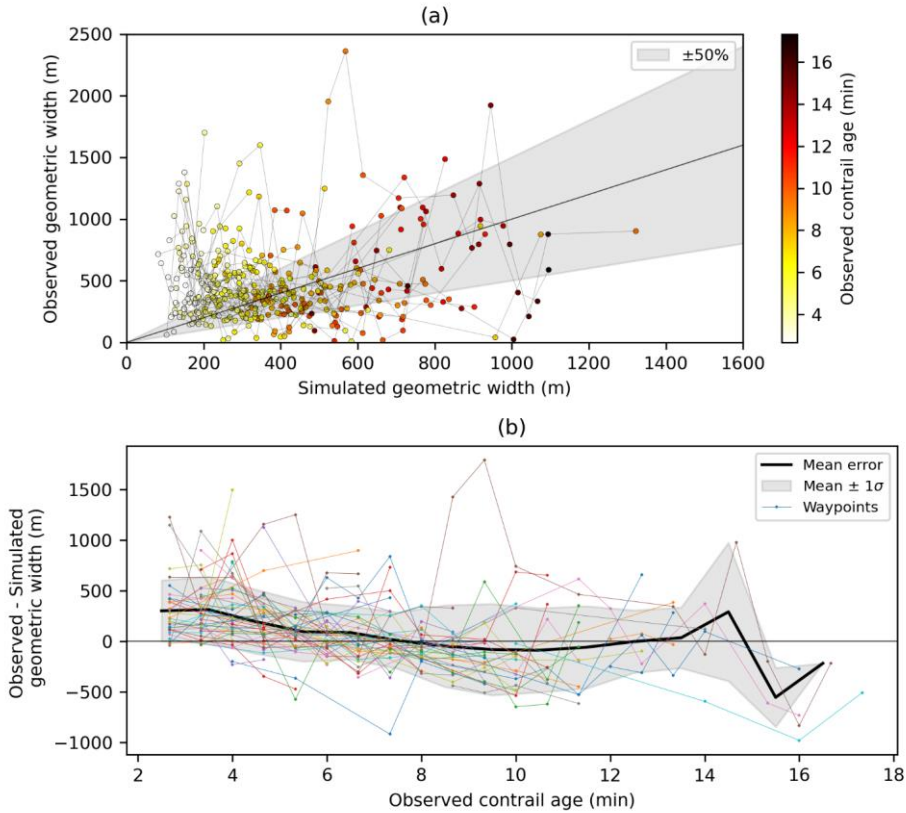
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445 simulating the contrail vertical displacement caused by the wake vortex downwash; ~~while assumption (ii) does not hold in the real world due to local turbulence and wind shear that can deform the contrail cross section into an inclined ellipse. To~~ We evaluate ~~the~~ ~~their~~ ~~impacts, we assess the~~ sensitivity of the observed ~~e~~contrail geometric width ~~to these factors~~ by varying the assumed contrail altitude ~~and the altitude at one of the contrail edges~~ by  $\pm 100$  m ~~for assumption (i), and by  $\pm 100$  m at one of the contrail edges for assumption (ii).~~ Our results indicate that ~~assumption (ii)~~the inclination angle has a significantly greater influence on the observed contrail geometric width ( $\pm 36\%$ ) ~~relative compared to the altitude assumption~~ ~~assumption (i)~~ ( $\pm 0.9\%$ ).





450 **Figure 8: Comparison Kernel density estimate between the observed and simulated contrail- (a) pixel width; and (b) geometric width**  
 for ADS-B waypoints with true positive cases ( $Y_{Camera}$  &  $Y_{Sim=CoIP}$ ) and with observed lifetimes exceeding 2 minutes. Panel (a) shows  
 a parity plot between the observed and simulated widths at single point in time, with the black lines representing the temporal  
 evolution of the contrail width for each waypoint. Panel (b) illustrates the difference between the observed and simulated geometric  
 widths as a function of the observed contrail age, with individual lines representing the temporal evolution of each contrail waypoint.  
 455 The observed contrail pixel width is converted to the observed geometric width using the reverse camera transformation model (see  
 Section 2.3).

### 3.4 Contrail detection limits

We also visually examined contrails that were initially formed outside the spatial-observation domain and were subsequently  
 advected into the camera's field-of-view, where the results yielded mixed outcomes. For instance Firstly, upon visual inspection,

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460 ~~contrails predicted on 5-Nov-2021 the 5<sup>th</sup> of November 2021~~ at 09:09:20 UTC, ~~some predicted contrails aligned well appear to show a reasonable agreement with relative to the~~ observations (Fig. 38b). ~~However, not all observed contrails were predicted by the model, and there were notable differences in the locations of predicted and observed contrails. We note that contrail-contrail and cloud-contrail overlapping further complicated the identification of contrail edges and the extraction of contrail widths.~~

465 ~~Secondly, in contrast, on 9-Nov-2021 the 9<sup>th</sup> of November 2021~~ at 10:02:40 UTC, ~~the we were unable to visually confirm the presence of contrails in the video footage (Fig. 3a), despite the simulation predicting ed the presence of contrail cirrus with a mean optical depth of 0.024 [0.002, 0.056] (5<sup>th</sup> and 95<sup>th</sup> percentile). This suggests~~ **ing** that these contrails ~~could be misclassified as false positive cases ( $N_{\text{Camera}}$  &  $Y_{\text{Sim-CoCIP}}$ ) because their optical depths were~~ **are** below ~~and or~~ close to the lower visibility ~~limit~~ **threshold** ~~limit~~ for ground-based observers (optical depth of < 0.02) (Kärcher et al., 2009). ~~While Although~~ faint white grains were visible in the video footage (Fig. 38a), ~~it remains challenging to determine~~ **discerning** whether these features represented ~~contrail cirrus, natural clouds, or false positive cases ( $N_{\text{Camera}}$  &  $Y_{\text{CoCIP}}$ ) is challenging. Collectively, our results suggest that ground-based cameras generally excel at identifying freshly formed and narrow contrails relative to satellites. This difficulty underscores the challenges that remote sensing methods, including ground-based cameras, have, but they are likely to also encounter difficulties in with~~ detecting optically thin contrails below a ~~yet-to-be determined~~ **threshold** optical depth (Driver et al., 2024; Mannstein et al., 2010; Meijer et al., 2022) ~~that is yet to be determined.~~

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#### 4 Discussion and conclusions

480 Recent estimates suggest that the 2019 global annual mean contrail cirrus net RF ( $62.1 [34.8, 74.8] \text{ mW m}^{-2}$ ) could be two times larger than the RF from aviation's cumulative  $\text{CO}_2$  emissions ( $34.3 [31, 38] \text{ mW m}^{-2}$ ). Ground-based cameras provide a cost-effective way to can observe contrails at a higher spatiotemporal resolution than and unlike satellite imagery, making them potentially valuable for validating their higher relative spatiotemporal resolution enables effective tracking of the formation and evolution of young contrails. Moreover, these ground-based observations can also be used to validate the early contrail lifecycle as simulated by contrail models. specific aspects of existing contrail models, which currently play a crucial role in validating and evaluating the effectiveness of different climate mitigation strategies. In this study, we develop a methodology to track and analyse contrail formation, persistences, and their geometric widths from ground-based video footage, and subsequently compare these observations with contrail simulations. The ground-based Our contrail observations consist of 14 h of video footage recorded on five different days at Imperial College London's South Kensington Campus, and 490 The actual flight trajectories that intersecting with the camera's field of view were obtained from ADS-B telemetry, and contrails formed by these flights were simulated with CoCiP using historical meteorology from the ECMWF ERA5 HRES reanalysis.

In total, we identified 1,582,649 flight ADS-B waypoints from 2813 flights were identified from the video footage, with contrails observed in 60% of these waypoints ( $Y_{\text{Camera}}$ ) under clear sky conditions, and contrails that were formed from these flights were simulated with CoCiP using historical meteorology from the ECMWF ERA5 HRES reanalysis; and estimates of the aircraft fuel consumption and aircraft engine specific nvPM particle number emissions from ADS-B transponder data. The simulation accurately correctly predicted contrail forecasted the formation ( $Y_{\text{Camera}} \& Y_{\text{CoCiP}}$ ) and absence ( $N_{\text{Camera}} \& N_{\text{CoCiP}}$ ) of contrails in for 7669.3% of these ADS-B waypoints when evaluated using the SAC ( $T_{\text{amb}} < T_{\text{SAC}}$ ), and for 73% of waypoints when evaluated using CoCiP's definition of persistent contrail formation (post wake vortex contrail  $\text{IWC} > 10^{12} \text{ kg kg}^{-1}$ ) (Table 1). Among waypoints with incorrect predictions, the SAC overestimates contrail formation, with 23% of waypoints being false positives ( $N_{\text{Camera}} \& Y_{\text{Sim-SAC}}$ ) compared to 1% false negatives ( $Y_{\text{Camera}} \& N_{\text{Sim-SAC}}$ ). In contrast, CoCiP's definition tended to underestimate contrail formation, with 6% of false positives ( $N_{\text{Camera}} \& Y_{\text{Sim-CoCiP}}$ ) versus 21% of false negatives ( $Y_{\text{Camera}} \& N_{\text{Sim-CoCiP}}$ ). A comparison with reanalysis weather data suggests that waypoints with incorrect predictions were often associated with warmer temperatures ( $dT_{\text{SAC}} = -7.8 \pm 4.3 \text{ K}$  at  $1\sigma$ ) and sub-saturated RH conditions ( $0.68 \pm 0.19$  at  $1\sigma$ ) relative to those with true positive outcomes ( $dT_{\text{SAC}} = -12.8 \pm 3.7 \text{ K}$  and  $\text{RH} = 1.02 \pm 0.29$ ) (Fig. 5). Notably, 98% of waypoints with  $Y_{\text{Camera}}$  fulfilled the SAC, 78% of waypoints with short-lived contrails (observed lifetimes  $< 2$  minutes) initially formed at  $\text{RH} < 100\%$ , and 75% of persistent contrails (observed lifetimes  $> 10$  minutes) formed at  $\text{RH} > 100\%$  (Fig. 7). The observed contrail geometric widths tend to be larger than the simulated widths by an average of 100 m over their observed lifetime, with the most significant underestimations (around 280 m) occurring during the first five minutes (Fig. 9).

510 , and the best agreement between the observations and simulations occur when contrails: (i) have an observed lifetime of  $> 2$  min; (ii) were formed between 35,000 and 40,000 feet; and (iii) at temperatures where  $dT_{\text{SAC}} < -10 \text{ K}$  (Fig. 4 and 6). However,

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515 a comparison between the waypoints with false negative and false positive outcomes, i.e.,  $P(Y_{\text{Camera}} \& N_{\text{CoCIP}}) = 25.9\%$  vs.  $P(N_{\text{Camera}} \& Y_{\text{CoCIP}}) = 4.8\%$ , suggests that the simulation underestimates contrail occurrence. Instances where a contrail is observed but not predicted occur five times more often than instances where the model falsely predicts a contrail to form ( $25.9/4.8 = 5.4$ ). Around 92% of waypoints with false negative outcomes,  $P(N_{\text{CoCIP}} \& Y_{\text{Camera}})$ , are associated with short-lived contrails ( $< 2$  min) that were formed at altitudes below 30,000 feet and at temperatures where  $dT_{\text{SAC}} > 2.5$  K (Fig. 4 and 6).

520 Among waypoints with true positive cases,  $P(Y_{\text{Camera}} \& Y_{\text{CoCIP}})$ , we also evaluated the evolving contrail dimensions over time and found that the simulation underestimates the geometric contrail width by an average of 17.5%. This underestimation is most likely caused by two factors: (i) uncertainties in the ERA5 HRES humidity fields; (ii) sub-grid scale variabilities that cannot be captured by the spatiotemporal resolution of existing NWP models; (iii) contrail model assumptions and simplifications; (iv) uncertainties in the simulated aircraft overall efficiency, which influences  $T_{\text{SAC}}$ ; (v) observational challenges (Fig. 3); and (vi) potentially other unidentified factors. (i) the sub-grid-scale variability in wind shear and turbulent mixing that cannot be resolved from the spatiotemporal resolution of numerical weather prediction (NWP) models; and (ii) CoCIP's assumption of a horizontal ellipse as the shape of the contrail cross-section, which may not adequately represent the inclined ellipse observed in real-world conditions.

525 When taken together, these results

530 hold potential significance within the context of contrail mitigation because: (i) contrails forming at very low temperatures ( $dT_{\text{SAC}} < 10$  K) tend to be long-lived and strongly warming and are more likely to be captured by the contrail simulation; while (ii) contrails forming at warmer temperatures ( $dT_{\text{SAC}} > 2.5$  K), where the simulation exhibits a larger relative error, are generally short-lived ( $< 2$  min) with a negligible energy forcing. Nevertheless, we also acknowledge the potential limitations of our study, including such as the: (i) small sample size; and (ii) inherent bias toward selecting contrails formed under high-pressure systems (i.e., clear sky conditions), while excluding contrails formed in low-pressure systems associated with storms and/or overcast weather. This selection bias could be significant, as different synoptic weather conditions could introduce varying error patterns in NWP models, which may lead to differences in the accuracy of the simulated contrail outputs. Additionally, as we specifically selected days with observed contrails, our findings should not be interpreted as representative of the overall likelihood of contrail formation. For limitation (ii), the distinct synoptic weather conditions could lead to different error patterns in the NWP which will propagate to the simulated contrail outputs.

540 Future work can build upon our research by: (i) developing a methodology to estimate the contrail optical thickness from ground-based cameras; (ii) establishing a network of ground-based cameras to observe contrails across a larger set of flights and over a wider domain, while also mitigating and to reduce the sensitivity of camera models' sensitivity to contrail altitude; (ii) conducting a larger-scale comparison between the observed and simulated contrail formation to assess the accuracy of humidity fields provided by NWP models, which is a critical input parameter for contrail models; (iii) combining ground-

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545 based ([i.e., cameras and lidars](#)) and satellite observations to track the whole contrail lifecycle [and beyond cloud free conditions,](#)  
 which can then be used to validate existing contrail models; (iv) [conducting a large-scale comparison between the observed](#)  
 and simulated contrails to establish benchmark datasets, which can be used to validate and improve the accuracy of contrail  
 models and the humidity fields provided by NWP models; and (iv) integrating ground-based observations with contrail  
 forecasts, thereby reducing the uncertainties in the real-time decision making processes for flight diversions to minimise the  
 550 formation of strongly warming contrails.

## Appendix

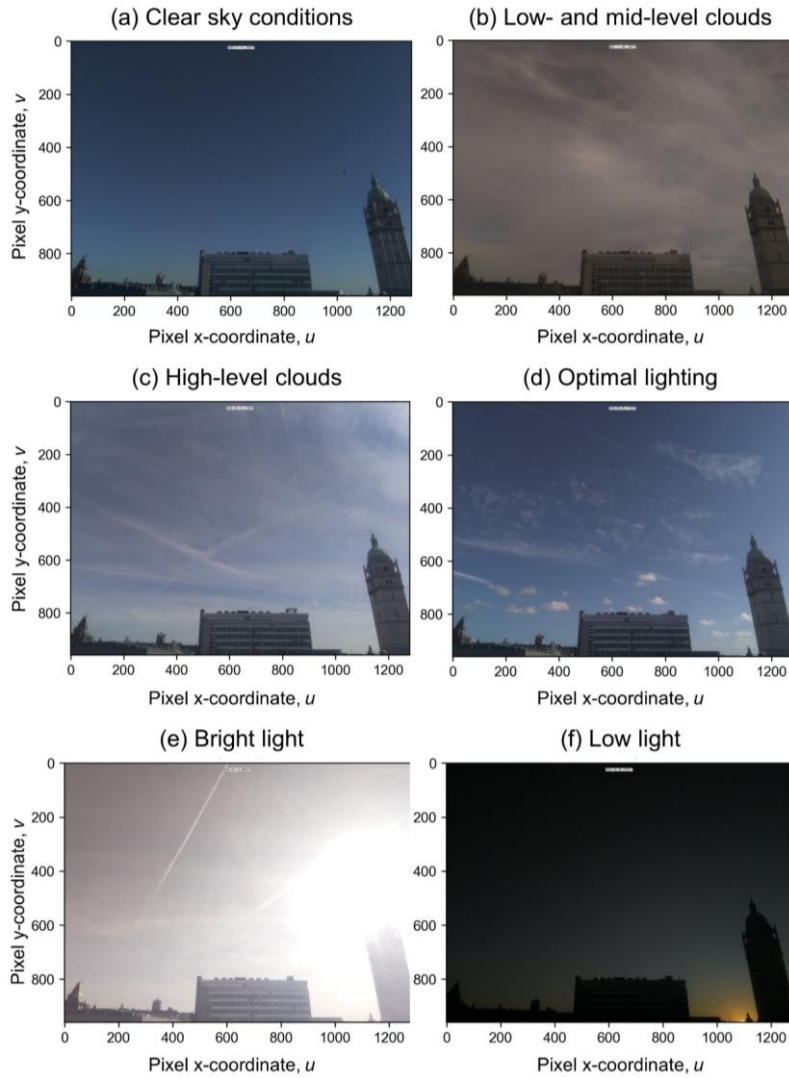
### A1 Video ~~footage~~ classification and camera field of view

Temporal variabilities in weather conditions influence the suitability of the video footage for contrail observations. To filter the video  
 footage that can be used to observe, track, and extract the properties of contrails, we visually inspect each hourly recording~~s~~ and  
 555 classify them based on the background cloud cover (Table A1) and lighting conditions (Table A2). An example of each classification  
 is shown in Fig. A1. The 14 h of video footage that were selected for further analysis have: (i) clear sky conditions; and (ii) optimal  
 lighting with strong color contrast between the (blue) sky and (white) contrails. Following the selection of video footages that are  
 feasible for contrail analysis, we reduced their frame rate to 40 seconds per frame to match the temporal resolution of the ADS-B  
 data and CoCiP outputs. [Figure A2 shows the camera's position and the spatial distribution of observed contrails within its field of](#)  
 560 [view.](#) The camera transformation model, as will be described in Appendix A3, was applied to systematically superimpose ADS-B  
 data and CoCiP outputs onto the video footage.

**Table A1: Classification of the video footage by the extent of background cloud cover.**

Category	Remarks/Implications
<b>Clear</b>	<ul style="list-style-type: none"> <li>• Clear sky conditions (0 oktas)* with an absence of low-, mid- and high-level cirrus.</li> </ul>
<b>Presence of low- and mid-level clouds</b>	<ul style="list-style-type: none"> <li>• Cloud cover with more than 5 oktas* can potentially obscure contrail observations, thereby limiting the opportunities for analysis.</li> </ul>
<b>Presence of high-level clouds</b>	<ul style="list-style-type: none"> <li>• Contrails formed within these clouds may be difficult to identify.</li> <li>• Contrails formed outside and subsequently advected into the camera's field of view may not be easily distinguished from natural cirrus clouds.</li> </ul>

\*: The unit "okta" is used to quantify the extent of cloud cover by dividing the sky into eights. A measurement of 0 oktas denotes a completely clear sky, while 8 oktas imply an entirely overcast sky.

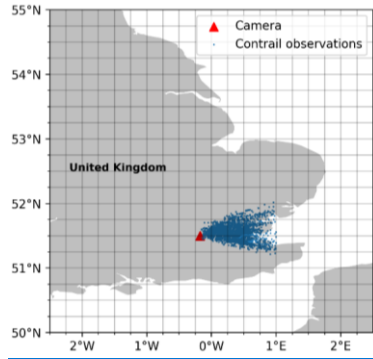


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**Figure A1:** Examples of the different background cloud cover, i.e., (a) clear sky conditions, (b) low-/mid-level clouds, and (c) high-level clouds), and lighting conditions, i.e., (d) optimal lighting, (e) bright-light; and (f) low-light conditions that were described in Tables A1 and A2.

**Table A2:** Classification of the video footage by the ambient lighting levels.

Category	Remarks/Implications
<b>Optimal</b>	<ul style="list-style-type: none"> <li>Strong color and feature contrast between the (blue) sky and contrails, ideal for contrail observations.</li> </ul>
<b>Bright light</b>	<ul style="list-style-type: none"> <li>Limited color contrast between the (white) sky compared to contrails and natural cirrus clouds.</li> <li>If the sun is in direct view of the camera, the solar glare may obscure a portion of the image.</li> </ul>
<b>Low light</b>	<ul style="list-style-type: none"> <li>Adjustments to the typical thresholds used to identify contrails will be necessary due to the reduced color brightness of the contrail against a darker background.</li> </ul>



**Figure A2:** Location of the camera (51.4988°N, 0.1788°W) and the spatial distribution of observed contrails within its field of view ( $n = 942$  for waypoints with  $Y_{\text{Camera}}$ ). The grid boxes represent the spatial resolution of the ERA5 HRES (0.25° longitude  $\times$  0.25° latitude).

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## 575 A2 Corrections to camera distortion

Unlike the ideal pinhole model, camera images contain radial and tangential distortion. Radial distortion occurs due to the bending of light rays near the edge of a lens, causing straight lines to appear curved. Tangential distortion occurs when lens assembly are not directly parallel and centred over the image plane. Distortion coefficients are determined using a chessboard pattern and homography, and an example process can be found in Wu et al. (2015). Using the OpenCV Python package (Bradski, 2000), every pixel is mapped to a corrected position following these steps:

**STEP 1:** The distorted pixel coordinates ( $u_{\text{dist}}, v_{\text{dist}}$ ) are converted to distorted camera coordinates ( $x_{\text{dist}}, y_{\text{dist}}, z_{\text{dist}}$ ) in Eq. (A1) using the inverse of the camera intrinsic matrix ( $K^{-1}$ , see Appendix A3),

$$\begin{bmatrix} x_{\text{dist}} \\ y_{\text{dist}} \\ z_{\text{dist}} \end{bmatrix} = K^{-1} \begin{bmatrix} u_{\text{dist}} \\ v_{\text{dist}} \\ 1 \end{bmatrix}. \quad (\text{A1})$$

**STEP 2:** The distorted camera coordinates are corrected using Eq. (A2) and Eq. (A3), both of which are found in the OpenCV package documentation,

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$$x'' = x'(1 + k_1 r^2 + k_2 r^4 + k_3 r^6) + [2p_1 x' y' + p_2 (r^2 + 2x'^2)], \quad (\text{A2})$$

$$y'' = y'(1 + k_1 r^2 + k_2 r^4 + k_3 r^6) + [2p_2 x' y' + p_1 (r^2 + 2x'^2)], \quad (\text{A3})$$

where  $x' = x_{\text{dist}}/z_{\text{dist}}$  and  $y' = y_{\text{dist}}/z_{\text{dist}}$  are normalised coordinates,  $r = \sqrt{x'^2 + y'^2}$ ,  $k_1 = 0.580$ ,  $k_2 = -2.661$ , and  $k_3 = 4.420$  are radial distortion coefficients, and  $p_1 = 5.803 \times 10^{-1}$  and  $p_2 = -2.576 \times 10^{-3}$  are tangential distortion coefficients.

**STEP 3:** The undistorted pixel coordinates ( $u, v$ ) are recalculated using Eq. (A4),

$$\lambda \begin{bmatrix} u \\ v \\ z_{\text{dist}} \end{bmatrix} = K \begin{bmatrix} x'' \\ y'' \\ z'' \end{bmatrix}. \quad (\text{A4})$$

Figure A32 shows an original frame captured by the camera alongside a corrected frame using the three-step process. While these differences may not be visually discernible, it is crucial to remove distortions to minimise errors when extracting the observed contrail pixel and geometric width from these images. The correction of the minor distortion in the original frame is evident through the added grid lines. All video footage used in the study underwent initial frame-by-frame processing to eliminate distortion before conducting subsequent analysis.

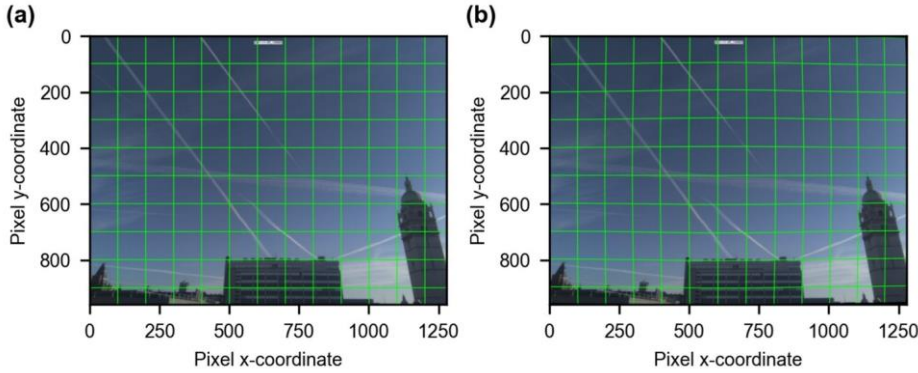


Figure A32: Side-by-side comparison of (a) an original frame captured by the ground-based camera; and (b) the distortion corrected frame by mapping coordinates to their undistorted positions using the OpenCV Python package.

### A3 Camera transformation model

After correcting for distortions, a camera transformation method is used to project the aircraft positions and simulated contrail location, which are provided as three-dimensional (3D) positions, to the camera observations which utilises a two-dimensional (2D) pixel coordinate ( $u, v$ ). A two-step process is used to achieve this:



605 **STEP 1:** The real-world 3D positions relative to the camera is mapped to a 3D camera coordinate system  $(X, Y, Z)$  using an extrinsic (rotation) matrix  $R$ ,

$$R = [R_x][R_y][R_z] = \begin{bmatrix} 0.1434 & -0.1357 & 0.9803 \\ -0.1357 & 0.9785 & 0.1553 \\ -0.9803 & -0.1553 & 0.1219 \end{bmatrix}. \quad (\text{A5})$$

$R$  describes the camera rotation in relation to the world axis, where  $R_x$ ,  $R_y$ , and  $R_z$  are the roll, pitch, and yaw of the camera respectively. The  $R$  coefficients are estimated by minimising the residuals between the computed and measured pixel coordinates of known aircraft positions and landmarks that are visible in the camera frame.

610 **STEP 2:** The 3D camera coordinates is then transformed to a 2D pixel coordinate system  $(u, v)$  using an intrinsic (camera) matrix  $K$ ,

$$K = \begin{bmatrix} f_x & s & x_0 \\ 0 & f_y & y_0 \\ 0 & 0 & 1 \end{bmatrix} = \begin{bmatrix} 708 & 0 & 634 \\ 0 & 708 & 472 \\ 0 & 0 & 1 \end{bmatrix}, \quad (\text{A6})$$

615 where the camera parameters  $f_x$  and  $f_y$  are the focal lengths in pixel units,  $(x_0, y_0)$  is the principal point of the image, and  $s$  represents the axis skew. Fig. 2 in the main text provides an example of the superimposed flight trajectories and simulated contrail properties to the video footage.

#### Author contributions

620 MEJS and EG conceptualised the study. JL, RT, [JP](#), and EG developed the methodology and undertook the investigation. JL, RT, JP, EG, and MS were responsible for software development and data curation. [RT and JL](#) and ~~RT~~ created or sourced the figures. [RT and JL](#) and ~~RT~~ wrote the original manuscript. MEJS, EG, and MS acquired funding. All authors have read, edited, and reviewed the manuscript, and agreed upon the published version of the paper.

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#### 625 Data availability

The ADS-B telemetry that is used to derive the actual flight trajectories in this study was purchased from Spire Aviation and can be made available for scientific research upon reasonable request. The pycontrails repository that contains the CoCiP algorithm has recently been published and publicly available at <https://doi.org/10.5281/zenodo.7776686>. This document used elements of Base of Aircraft Data (BADA) Family 4 Release 4.2 which has been made available by EUROCONTROL to

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use of the Copernicus information. The timelapse videos will be submitted to the Central for Environmental Data Analysis  
635 (CEDA) on acceptance.

### Competing interests

There are no conflicts of interest and all funding sources have been acknowledged. All figures are our own. None of the authors  
has any competing interests.

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