Coupling the urban canopy model TEB (SURFEXv9.0) with the radiation model SPARTACUS-Urbanv0.6.1 for more realistic urban radiative exchange calculation

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Abstract. The urban canopy model TEB is coupled with the radiation model SPARTACUS-Urban to improve both the urban geometry simplification and the radiative transfer calculation. SPARTACUS-Urban assumes that the probability density function of wall-to-wall and of ground-to-wall distances follows a decreasing exponential. This better matches the distributions in real cities than the infinitely-long street canyon employed by the classical TEB. SPARTACUS-Urban solves the radiative transfer equation using the discrete ordinate method. This allows to take into account physical processes such as the interaction of radiation with the air in the urban canopy layer, the spectral dependence of urban material reflectivities or specular reflections. Such processes would be more difficult to account for with the radiosity method used by the classical TEB. With SPARTACUS-Urban, the mean radiant temperature, a crucial parameter for outdoor human thermal comfort, can be calculated from the radiative fluxes in the vertical and horizontal directions incident on the human body in an urban environment. TEB-SPARTACUS is validated by comparing the solar and terrestrial urban radiation budget observables with those simulated by the Monte-Carlo-based HTRDR-Urban reference model for procedurally-generated urban districts that mimic the Local Climate Zones. Improvement is found for almost all radiative observables and urban morphologies for direct solar, diffuse solar, and terrestrial infrared radiation. The TEB Mean Radiant Temperature diagnostic for a person in the urban environment is also improved with TEB-SPARTACUS compared with the classical TEB. Based on these results, TEB-SPARTACUS could lead to more realistic results for building energy consumption, outdoor human thermal comfort, or the urban heat island effect.

1 Introduction

Radiative exchange is a crucial physical process for the urban climate. Multiple reflections of solar radiation in the 3-D urban geometry result in a lower effective reflectivity (albedo) of a city compared to a flat surface (Krayenhoff et al., 2014). At night, downwelling terrestrial infrared radiation at the surface is higher in urban areas than in open rural areas. This is due to the emission of infrared radiation towards the ground from buildings or urban trees, which have a higher surface temperature than the radiative temperature of the sky. Radiative exchange contributes to the higher (night-time) air temperature in urban areas compared with the surrounding rural areas (the urban heat island effect, Oke (1982)), although it is not the main cause.

Shading and multiple reflection of radiation by complex geometries of buildings and vegetation alter the radiation received by buildings and humans in the urban environment compared to an open rural environment. This is relevant to the energy consumption of buildings (Strømann-Andersen and Sattrup, 2011; Frayssinet et al., 2018), and human thermal comfort (Fröhlich and Matzarakis, 2020; Dissegna et al., 2021; Geletič et al., 2022).

Urban Canopy Models (UCMs) such as the Town Energy Balance (TEB, Masson (2000)) or the Building Effect Parametrisation (BEP, Martilli et al. (2002)) that calculate the urban surface energy balance in mesoscale or global atmospheric models (Grimmond et al., 2010, 2011) strongly simplify both urban geometry and radiative transfer physics. The most commonly used UCM geometry is the infinitely-long street canyon; the radiosity method is common for radiative exchange calculation (Schoetter et al., 2023). It assumes that radiation is reflected isotropically (Lambertian surfaces), that there is vacuum in between the buildings, and that there is no wavelength dependence of material reflectivity (broadband materials).

Hogan (2019a) found that radiative transfer in the urban canopy layer (UCL) is governed by the probability density functions of the wall-to-wall (p_{ww}) and ground-to-wall (p_{gw}) distances as these determine the probability that radiation passing through the UCL will be intercepted by buildings or the ground. Hogan (2019a) and Stretton et al. (2022) investigated p_{ww} and p_{gw} for districts in real cities and found systematic differences between them and the distribution that is implicitly assumed in the use of the infinitely-long street canyon geometry. This leads to incorrect mean rates of solar and thermal infrared radiation exchange between the sky, walls, and the ground. Instead, a decreasing exponential function fits p_{ww} and p_{gw} in real cities. For urban districts where this decreasing exponential function of p_{ww} and p_{gw} applies, the attenuation of radiation by buildings can be described by the Beer-Lambert law in the same way as for radiation passing through the turbid atmosphere.

In light of these findings, Hogan (2019b) adapted the SPARTACUS (SPeedy Algorithm for Radiative TrAnsfer through CloUd Sides; Schäfer et al. (2016), Hogan et al. (2016)) atmospheric radiation model representing the 3-D radiative interactions between clouds to the UCL (SPARTACUS-Urban). SPARTACUS-Urban is part of the land surface radiation model SPARTACUS-Surface. It is based on the 1-D discrete ordinate method and divides the UCL into the built, the urban tree, and the clear air regions. In the vertical direction, SPARTACUS-Urban can subdivide the urban canopy into several layers, which allows for a variety of building and tree heights at each grid point. It can model physical processes such as specular reflections, or the interaction of radiation with air, aerosols or clouds in the UCL, which are difficult to account for with the radiosity method. It can also more realistically represent the interaction of radiation with trees by representing them as cylinders, thus preserving their contact surface area with air and buildings.

Hogan (2019b) validated SPARTACUS-Urban with Monte-Carlo reference simulations for the specific case of forest sites without buildings. Stretton et al. (2022) evaluated the solar radiation budget simulated by SPARTACUS-Urban for urban geometries of different complexity including real cities with simulations using the obstacle-resolving radiation model Discrete Anisotropic Radiative Transfer (DART; Gastellu-Etchegorry (2008); Gastellu-Etchegorry et al. (2015)). They find a very good performance of SPARTACUS-Urban as long as the assumption of the decreasing exponential function for p_{ww} and p_{gw} holds. Otherwise, larger biases appear, but the overall performance is still good. Stretton et al. (2023) successfully evaluated SPARTACUS-Urban against DART for terrestrial radiation in a central London domain for both homogeneous and heterogeneous skin surface temperature of urban facets.

Coupling SPARTACUS-Urban with UCMs promises to improve the realism of urban geometry and radiative transfer physics in these models. Furthermore, the benefits of some climate change adaptation measures (e.g. street trees or building materials with specific spectral reflectivities) can be better quantified with SPARTACUS-Urban than with the radiation schemes used by most urban canopy models. This study presents the coupling of SPARTACUS-Urban with the UCM TEB (TEB-SPARTACUS). TEB is used to simulate the energy balance of the urban surface as a function of the meteorological conditions at the top of the urban roughness sublayer (2-5 times the characteristic building height, Roth (2000)). The original TEB, hereafter referred to as TEB-Classical, represents the city as an infinitely-long street canyon. It solves the energy budget separately for the roof, the walls, and the ground. TEB can solve the 1-D prognostic equations for wind speed, air temperature, humidity, and turbulence kinetic energy for the air in the UCL (surface boundary layer scheme SBL) (Hamdi and Masson, 2008). Ground in-canyon vegetation was added by Lemonsu et al. (2012), vertically-extended in-canyon vegetation by Redon et al. (2017, 2020). The urban trees are represented by a turbid layer filling the entire street canyon between the height of the trunk and the height of the tree. A building energy model (Bueno et al. (2012), Pigeon et al. (2014)) solves the energy budget of a representative building at district scale, taking into account human behaviour related to the energy consumption of the buildings (Schoetter et al., 2017). TEB is used as lower boundary condition for cities in mesoscale atmospheric models such as Meso-NH (Lac et al., 2018), numerical weather prediction models such as AROME (Seity et al., 2011), or regional climate models such as CNRM-ALADIN (Daniel et al., 2019), and CNRM-AROME (Lemonsu et al., 2023).

This study is structured as follows. The technical aspects of the coupling between TEB and SPARTACUS-Urban are described in Section 2, the methodology of the TEB-SPARTACUS validation in Section 3, and the validation results in Section 4. Conclusions are drawn in Section 5.

2 Technical aspects of the TEB and SPARTACUS-Urban coupling

In TEB, the outdoor radiative transfer is computed at each time step before the energy balance of the different urban facets is solved (Figure 1a). The outdoor radiative transfer routines take as input the downwelling solar and terrestrial radiation at the top of the UCL, the urban and vegetation morphology parameters, the albedo, emissivity, and prognostic skin surface temperature of the urban facets. They calculate the upwelling solar and terrestrial radiation for the coupling with the atmospheric model, the solar and terrestrial radiation incident on the different urban facets, and the radiative fluxes at ground level for the calculation of the Mean Radiant Temperature. The modular structure of TEB allows to introduce an option to calculate outdoor radiative transfer with SPARTACUS-Urban instead of the Classical radiosity method, leaving the other routines of TEB unchanged.

2.1 TEB-SPARTACUS geometry

The original TEB (Masson, 2000) is a single layer UCM. This means that the roof of the building is at the surface level of the atmospheric model; the walls and the road are below the surface. Schoetter et al. (2020) added the option to couple TEB with the atmospheric model on multiple levels; With the multi-layer TEB the buildings are immersed in the atmosphere . With both the single and multi-layer TEB, there is only one average building (H_{build}) and tree (H_{tree}) height at each grid point.

Furthermore, the radiation received and absorbed by the building walls and the trees is calculated at a single node; No vertical discretisation is performed. TEB-SPARTACUS would allow to consider a variety of building and tree heights at each grid point, and to calculate a vertical profile of the radiation received and absorbed by the walls. However, this would require modification of the input parameters of SURFEX-TEB and also other physical routines, which is left for future development. In this article, except for the assumption of the decreasing exponential function for p_{ww} and p_{gw} inherent to SPARTACUS-Urban, the geometric complexity of TEB is not changed.

2.2 Vertical levels of SPARTACUS-Urban when used by TEB

The vertical levels used by SPARTACUS-Urban for radiative transfer calculation in TEB (hereafter the TEB-SPARTACUS vertical levels) have to be defined. A maximum extension ($\Delta z_{\text{SPTS,max}}$) is defined for the TEB-SPARTACUS vertical levels. Its default value is 1 m. The TEB-SPARTACUS vertical levels are defined as a function of $\Delta z_{\text{SPTS,max}}$, H_{build}, and H_{tree} such that one level is either completely vertically intersected by trees and/or buildings, or completely free of them (Figure 1bc). With this approach, no vertical interpolation of the geometric parameters of buildings and trees is required that could lead to physical inconsistencies. For a grid point with $H_{\text{build}} > H_{\text{tree}}$, vertical levels with the extent $\Delta z_{\text{SPTS,max}}$ are defined starting from the ground. The extent of the level, which would be higher than H_{tree}, is reduced so that its height is equal to H_{tree} ($k_{\text{SPTS}} = 2$ in Figure 1b). The TEB-SPARTACUS vertical levels below H_{tree} contain a built, tree, and clear air region. Above H_{tree}, further vertical levels with the extension $\Delta z_{\text{SPTS,max}}$ are defined. The extent of the level that would be higher than H_{build} is reduced to match H_{build} ($k_{\text{SPTS}} = 3$ in Figure 1b). The levels defined between H_{tree} and H_{build} contain only buildings and clear air. A layer of clear air is placed above the buildings for numerical reasons. For a grid point with $H_{\text{build}} < H_{\text{tree}}$, the TEB-SPARTACUS vertical levels are set in a similar way (Figure 1c).

The TEB-SPARTACUS vertical levels are different from the vertical levels used for the meteorological variables in the SBL scheme. The SBL grid is defined to have a high resolution near the surface (Figure 1bc), because the meteorological parameters computed by the SBL scheme, such as air temperature and wind speed have the strongest gradients close to the surface. For SPARTACUS-Urban, this does not make sense because the radiation fields are relatively homogeneous close to the surface, especially since most buildings are higher than 3 m, there is little variation in building density with height in the lowest metres.

(a)

| Calculation of the prognostic TEB-SBL variables |

Input parameters for outdoor urban radiative transfer:
- Parameters characterising urban and tree morphology
- Downwelling solar and terrestrial radiation at the top of the UCL
- Albedo, emissivity, and skin surface temperature of urban facets

Calculation of outdoor radiative transfer with the radiosity method (TEB-Classical) or with SPARTACUS-Urban (TEB-SPARTACUS)

Output parameters from outdoor urban radiative transfer:
- Upwelling solar and terrestrial radiation at the top of the UCL
- Solar and terrestrial radiation incident on different urban facets
- Radiative fluxes at ground level for Mean Radiant Temperature

Calculation of the energy balance of roof, wall, road, in-canyon vegetation
Calculation of Mean Radiant Temperature, Universal Thermal Climate Index

Figure 1. (a) Outdoor radiative transfer calculation in the TEB model and TEB-SPARTACUS vertical levels for (b): a grid point with the buildings (grey) higher than the trees (green) ($H_{\text{build}} > H_{\text{tree}}$) and (c): a grid point with the buildings lower than the trees ($H_{\text{build}} < H_{\text{tree}}$). The k_{SBL} display the centre of the TEB Surface Boundary Layer (SBL) mass levels, the k_{SPTS} the TEB-SPARTACUS vertical levels (continuous lines). Urban facet properties such as albedo (α), emissivity (ϵ), and skin surface temperature (T), which may show intra-facet variation in TEB (e.g. due to a part of the roofs covered by green roofs (de Munck et al., 2013)) are aggregated before their use in SPARTACUS-Urban. The x-axis represents the horizontal extent of buildings (λ_p), urban trees (λ_{tree}), and clear air ($1 - \lambda_p - \lambda_{\text{tree}}$) in the urban canopy layer.

2.3 SPARTACUS-Urban input and output parameters when used in TEB

The SPARTACUS-Urban input parameters when used in TEB are listed in Table A1, the SPARTACUS-Urban output parameters used by TEB in Table A2. Some of the input parameters are exactly the same as in TEB. This is indicated by "TEB variable" in Table A1. However, SPARTACUS-Urban requires some input parameters that are not present in TEB; these have to be calculated based on the TEB variables or specified, which is explained in the following. The characteristic building diameter D is calculated assuming cylindrical buildings (Eq. 3) by combining the equations defining the plan area building density (λ_p; Eq. 1) and the exterior wall area density (λ_w; Eq. 2).

$$\lambda_p = \frac{\pi D^2}{4A_{\mathrm{ref}}} \tag{1}$$

$$\lambda_w = \frac{\pi D H_{\mathrm{build}}}{A_{\mathrm{ref}}} \tag{2}$$

$$D = \frac{4\lambda_p H_{\mathrm{build}}}{\lambda_w} \tag{3}$$

A_{ref} is the surface area of the grid point.

As the TEB SBL levels are different from those of the TEB-SPARTACUS (Figure 1bc), the air temperature values from the SBL vertical levels are linearly interpolated to the centre of the TEB-SPARTACUS vertical levels.

TEB can take into account a variety of surface coverings per type of urban facet. The roofs of the buildings can be covered with the native roofing material, snow, solar panels (Masson et al., 2014), or green roofs (de Munck et al., 2013). The ground may be covered by roads, bare ground, low vegetation, or snow. The building walls consist of the wall exterior material and possibly windows. In order to keep the SPARTACUS-Urban code independent of its use by TEB, it uses aggregated radiative properties for each facet. After the call of SPARTACUS-Urban, the radiation absorbed by the different surface coverings on each facet is calculated. For a facet consisting of two surface coverings (an example for the roof is shown in Figure 1bc) with fractional covers f_1 and f_2, albedos α_1 and α_2, emissivities ϵ_1 and ϵ_2, and surface temperatures T_1 and T_2, the aggregated values of albedo (α_{agg}), emissivity (ϵ_{agg}), and radiative surface temperature (T_{agg}) used by SPARTACUS-Urban are calculated as follows:

$$\alpha_{\mathrm{agg}} = \frac{f_1\alpha_1 + f_2\alpha_2}{f_1 + f_2} \tag{4}$$

$$\epsilon_{\mathrm{agg}} = \frac{f_1\epsilon_1 + f_2\epsilon_2}{f_1 + f_2} \tag{5}$$

$$T_{\mathrm{agg}} = \left(\frac{f_1\epsilon_1\sigma T_1{}^4 + f_2\epsilon_2\sigma T_2{}^4}{(f_1 + f_2)\sigma\epsilon_{\mathrm{agg}}} \right)^{0.25} \tag{6}$$

145 SPARTACUS-Urban calculates the average solar (SW_{inc}) and infrared (LW_{inc}) radiation incident on a facet. The solar (SW_{abs}) and infrared (LW_{abs}) radiation absorbed by the two surface coverings is calculated as follows

$$SW_{abs,1} = (1 - \alpha_1)SW_{inc} \quad SW_{abs,2} = (1 - \alpha_2)SW_{inc} \tag{7}$$

$$LW_{abs,1} = \epsilon_1(LW_{inc} - \sigma T_1{}^4) \quad LW_{abs,2} = \epsilon_2(LW_{inc} - \sigma T_2{}^4) \tag{8}$$

150 SPARTACUS-Urban represents the radiative exchanges between trees, walls, and the clear air with more detail than TEB, taking into account a more realistic shape of trees with a characteristic diameter D_{tree}, and a potential variability of the optical depth of trees (FSD_{tree}). These parameters are currently specified in the code; future work could investigate whether it would be possible to link them to physiographic input variables (such as land cover) or to specify them via databases. The fraction of tree surface in contact with walls (FC_{tree}) is calculated from the fraction of tree surface cover (λ_{tree}) assuming a random

155 positioning of trees in the urban canyon, as follows

$$FC_{tree} = \frac{\lambda_{tree}}{1 - \lambda_p} \tag{9}$$

The air temperature in the vegetation canopy ($T_{air,veg}$) is assumed to be equal to the air temperature in the clear air region (T_{air}). SPARTACUS-Urban allows to consider the scattering and absorption of solar radiation in the urban canopy. This is specified by the extinction coefficients ($k_{ext,air,sw}$, $k_{kext,air,lw}$) and the single scattering albedo of the air for solar ($\alpha_{ssa,air,sw}$)

160 and terrestrial radiation ($\alpha_{ssa,air,lw}$). These coefficients are currently set to 0, but could be calculated as a function of air temperature, humidity, liquid water content, and aerosol concentration by coupling to an atmospheric radiation scheme.

The single-scattering albedo for solar radiation of a leaf ($\alpha_{ssa,tree,sw}$) is assumed to be 0.4, which corresponds to a value integrated over the solar spectrum. This differs from the bulk vegetation albedo in the original TEB, as this parameter corresponds to an effective albedo after multiple reflections. The single scattering albedo for the terrestrial radiation of a leaf ($\alpha_{ssa,tree,lw}$)

165 is calculated from the value of the tree emissivity (ϵ_{tree}) in TEB as follows

$$\alpha_{ssa,tree,lw} = 1 - \epsilon_{tree} \tag{10}$$

The tree extinction coefficient ($k_{ext,tree}$) is calculated from the vertical profile of the Leaf Area Density (LAD), assuming an isotropic orientation of the leaves:

$$k_{ext,tree} = 0.5 \, LAD \tag{11}$$

170 SPARTACUS-Urban allows to take into account the fraction of specular reflections from the walls ($f_{ref,specular}$). It is set to 0 here, but could be linked to the glazing ratio and properties of the wall and window materials.

2.4 Calculation of the Mean Radiant Temperature

The Mean Radiant Temperature (MRT) is a crucial input parameter for outdoor human thermal comfort indices such as the Universal Thermal Climate Index (UTCI, Blazejczyk et al. (2012)). With the original TEB radiation scheme, it is calculated via

175 the radiosity method using the shape factors between the human body and the different urban facets (road, walls, windows, and vegetation); the detailed equations are given in the supplementary material of Kwok et al. (2019). With TEB-SPARTACUS, the MRT is calculated differently. The flux densities of the diffuse solar and infrared upwelling and downwelling radiation ($SW_{up,diff,gr}$, $SW_{down,diff,gr}$, $LW_{up,gr}$, $LW_{down,gr}$) at the ground level are known. In addition, the diffuse solar and terrestrial fluxes incident on a vertical plane at the ground level ($SW_{hor,diff,gr}$, $LW_{hor,gr}$) can be diagnosed with TEB-SPARTACUS.

180 The vertical and horizontal fluxes are weighted according to Thorsson et al. (2007) to obtain the average diffuse radiative flux density absorbed by the human body:

$$R_{bd,diff} = (1 - \alpha_{bd})(0.88\ SW_{hor,diff,gr} + 0.06\ SW_{up,diff,gr} + 0.06\ SW_{down,diff,gr})$$
$$+\epsilon_{bd}(0.88\ LW_{hor,gr} + 0.06\ LW_{up,gr} + 0.06\ LW_{down,gr}) \tag{12}$$

where α_{bd} (0.3) and ϵ_{bd} (0.97) are the standard (Thorsson et al., 2007) albedo and emissivity of the human body, respectively. The fluxes in the horizontal direction have a higher weight than the fluxes in the vertical direction, because the human body is

185 assumed to be in an upright position.

The average total (diffuse and direct) radiative flux density absorbed by the human body when fully exposed to solar radiation is calculated as follows

$$R_{bd,sun} = R_{bd,diff} + (1 - \alpha_{bd})SW_{dir,bd} \tag{13}$$

with the mean direct solar radiative flux density incident on the human body ($SW_{dir,bd}$) given by Di Napoli et al. (2020) as

190 follows

$$SW_{dir,bd} = 0.308 \frac{SW_{down,dir,gr}}{max(0.05, sin(\beta))} cos\left(\beta(1 - \frac{\beta^2}{14.744})\right) \tag{14}$$

$SW_{down,dir,gr}$ is the direct solar radiation reaching the ground and β is the solar elevation angle. Based on these fluxes, the MRT for a human body exposed to diffuse solar radiation only (MRT_{shade}) and a human body fully exposed to direct solar radiation (MRT_{sun}) are calculated as follows

195 $$MRT_{sun} = \left(\frac{R_{bd,sun}}{\epsilon_{bd}\sigma}\right)^{0.25} \tag{15}$$

$$MRT_{shade} = \left(\frac{R_{bd,diff}}{\epsilon_{bd}\sigma}\right)^{0.25} \tag{16}$$

The radiative fluxes are taken at ground level because the vertical profiles of the diffuse solar and terrestrial fluxes incident on a vertical plane are not outputs of the current version of SPARTACUS-Urban. It would be a bit more accurate to calculate them

200 at 1 m above the ground, as this would better represent their average effect on the human body. The difference between the fluxes at ground level and 1 m above ground is currently neglected. By taking into account the fluxes from vertical building walls, TEB-SPARTACUS allows for a more realistic estimation of MRT in urban areas from weather models and reanalysis data than previous work considering only flat ground (Di Napoli et al., 2020).

3 Methodology for TEB-SPARTACUS validation

Validation of TEB-SPARTACUS with observations of radiative and turbulent fluxes in real cities like those presented by Lipson et al. (2022) is not a promising strategy since the differences between the simulated and observed fluxes may be due to differences in the urban morphology, building material parameters, or anthropogenic heat fluxes between the real city and the simplified representation of the city in TEB. Moreover, observations themselves are uncertain. It would therefore be difficult to attribute any potential improvement in the fluxes simulated by TEB-SPARTACUS to the better representation of urban geometry or radiative transfer physics. For this reason, in this study, the radiative observables simulated by TEB are evaluated with the Monte-Carlo-based HTRDR-Urban reference model (Caliot et al., 2022). HTRDR-Urban takes the actual complex 3D building and tree geometries into account and is used to quantify the errors due to the use of a simplified morphology in the UCM TEB. The comparison of the TEB-Classical and TEB-SPARTACUS errors allows to quantify the potential benefits of TEB-SPARTACUS compared to TEB-Classical. All urban radiation models take into account the solar shading of trees by buildings, and buildings by trees. They also account for the mutual terrestrial radiation interactions between trees and buildings. Only the way how the urban and tree geometry, and the radiative transfer physics is represented changes between the models.

3.1 HTRDR-Urban reference model of urban radiative transfer

HTRDR-Urban uses a backward Monte-Carlo algorithm with the null-collision technique (Galtier et al., 2013; El Hafi et al., 2021) and accelerating grids (Villefranque et al., 2019) to solve the Radiative Transfer Equation (RTE) for solar and terrestrial radiation. It takes into account the interaction between radiation and the atmosphere with non-grey absorption, emission, and anisotropic scattering. 3-D absorption and scattering coefficient data, and scattering phase functions characterise the spectral and directional radiative properties of gases, liquid droplets, and solid particles. At the Top Of the Atmosphere (TOA), the observed solar spectrum irradiance averaged for 2020 from Coddington et al. (2015) is prescribed. At the Earth's surface, opaque surfaces consisting of vegetation and buildings, described by triangles in a wavefront (.obj) file are prescribed. They can be specular or Lambertian reflectors, with a potentially wavelength-dependent reflectivity. Measured spectral Lambertian reflectivities included in the Spectral Library of impervious Urban Materials (SLUM) available from the London Urban Micromet data Archive (LUMA) (Kotthaus et al., 2013, 2014) are distributed with HTRDR-Urban. The surface triangles are assigned a constant surface temperature. The MRT in HTRDR-Urban is calculated under the assumption that the human body is a cylinder with a height of 1 m and a radius of 0.14 m centred 1.1 m above the ground (Schoetter et al., 2023).

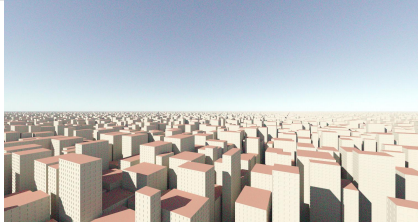
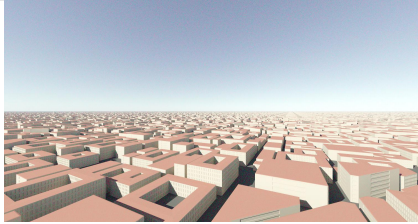
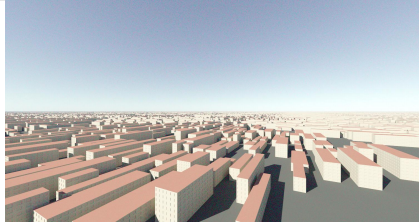
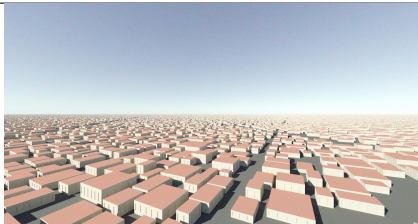
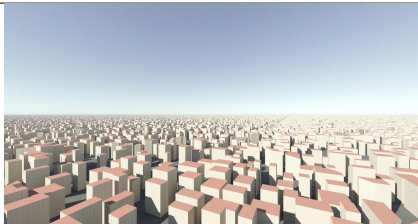
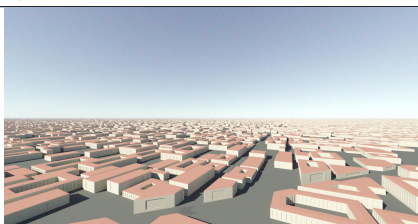
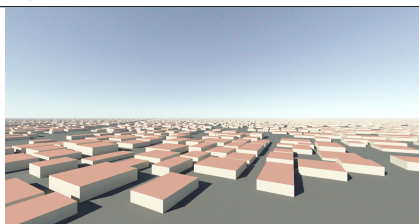
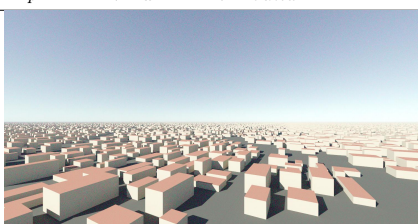
3.2 Procedurally-generated urban morphologies

Exactly the same urban morphologies as described in Section 4 of Schoetter et al. (2023) and Nagel et al. (2023) are investigated (Table 1). They were created with a procedural city generator, their spatial extent is 800 m x 800 m, and they mimic homogeneous urban districts covered by a type of Local Climate Zone (LCZ; Stewart and Oke (2012)). For example, the sparsely built LCZ9 district consists only of detached houses. However, like a real LCZ9 district, they are not all exactly the same height or size. Tornay et al. (2017)'s inventory of common urban morphologies in France has shown that the standard LCZ2 (compact

mid-rise) and LCZ6 (open low-rise) comprises two relatively different morphologies: buildings forming blocks with an internal courtyard or buildings forming rows. Similar results are likely to be found in other European countries. As wind circulation and radiative transfer may be different between the block and row morphologies, the blocks of compact midrise (LCZ2a) and rows of compact midrise (LCZ2b) as well as blocks of open lowrise (LCZ6a) and rows of open lowrise (LCZ6b) are distinguished. LCZ7 is not studied because it differs from LC3 only in terms of construction materials.

For each district, a representative street canyon with the same λ_p, λ_w, and average building height (H_{mean}) than the actual district is created. The morphologies LCZ2a, LCZ2b, LCZ3, LCZ5, LCZ6a, LCZ6b, and LCZ9 will in many cases have pitched roofs. Since pitched roofs cannot be accurately represented in TEB-Classical, TEB-SPARTACUS or SPARTACUS-Urban, the analysis for these morphologies is performed with and without pitched roofs. The evaluation for the morphologies with flat roofs allows for a rigorous quantification of potential TEB-SPARTACUS shortcomings, while the results for the morphologies with the pitched roofs give an additional indication of how TEB-SPARTACUS performs for districts where pitched roofs occur. Potential overhanging roofs, which may also occur in real cities are not considered.

A copy of the LCZ2a, LCZ4, LCZ5, and LCZ9 morphologies with trees represented by trunks, branches, and individual leaves is created. All trees have the same height (10 m), diameter (10.55 m), and leaf area index ($\mathrm{LAI} = 2.24$). As the trees do not intersect the buildings, more trees can be placed in the low density morphologies than in the high density morphologies. There are 64 trees for LCZ2a, 963 for LCZ4, 869 for LCZ5, and 1045 for LCZ9. The values of λ_{tree} are 0.01 for LCZ2a, 0.13 for LCZ4, 0.12 for LCZ5, and 0.14 for LCZ9, respectively.

A disadvantage of using procedurally-generated districts is that they may not be sufficiently representative of real districts. However, for the procedurally-generated districts, it is possible to perfectly control the building geometries and to know exactly which surfaces belong to the buildings roofs, walls or the ground. It is also possible to simplify the morphologies to exclude for example orographic effects, pitched roofs or overhanging roofs. Schoetter et al. (2023) investigated the p_{ww} and p_{gw} for the procedurally-generated districts and found a good agreement with the decreasing exponential function assumed by SPARTACUS-Urban. Therefore, the radiative transfer in the procedurally-generated districts may be close to that in real geometries, for which the assumption of a decreasing exponential distribution of p_{ww} and p_{gw} is correct.

3.3 Radiative boundary conditions

The UCL solar radiation budget consists of the downwelling and reflected solar radiation flux densities at the top of the UCL ($\dot{Q}_D$ and $\dot{Q}_U$), the flux density absorbed by the roofs ($\dot{Q}_R$), the walls including the windows ($\dot{Q}_W$), the ground ($\dot{Q}_G$), the urban trees ($\dot{Q}_T$), and the air ($\dot{Q}_{\mathrm{air}}$). The UCL terrestrial radiation budget consists of the terrestrial radiation exchanged (absorbed minus emitted) by the sky, the roofs, the walls including the windows, the ground, the trees, and the air ($\dot{E}_{\mathrm{sky}}$, $\dot{E}_R$, $\dot{E}_W$, $\dot{E}_G$, $\dot{E}_T$, and $\dot{E}_{\mathrm{air}}$). In this study, vacuum radiative properties are assumed for the air in the UCL, hence $\dot{Q}_{\mathrm{air}} = 0$ and $\dot{E}_{\mathrm{air}} = 0$. The following boundary conditions for downwelling radiation are considered:

LCZ1: Compact high-rise	**LCZ2a: Blocks of compact mid-rise**	**LCZ2b: Rows of compact mid-rise**
$\lambda_p = 0.46$; $\lambda_w = 6.6$; $H_{build} = 91.83$ m	$\lambda_p = 0.53$; $\lambda_w = 1.21$; $H_{build} = 17.2$ m	$\lambda_p = 0.35$; $\lambda_w = 0.97$; $H_{build} = 18.4$ m
LCZ3: Compact low-rise	**LCZ4: Open high-rise**	**LCZ5: Open mid-rise**
$\lambda_p = 0.40$; $\lambda_w = 0.58$; $H_{build} = 6.2$ m	$\lambda_p = 0.23$; $\lambda_w = 1.83$; $H_{build} = 50.3$ m	$\lambda_p = 0.32$; $\lambda_w = 1.18$; $H_{build} = 16.7$ m
LCZ6a: Blocks of open low-rise	**LCZ6b: Rows of open low-rise**	**LCZ8: Large low-rise**
$\lambda_p = 0.38$; $\lambda_w = 0.58$; $H_{build} = 7.1$ m	$\lambda_p = 0.25$; $\lambda_w = 0.29$; $H_{build} = 6.3$ m	$\lambda_p = 0.31$; $\lambda_w = 0.27$; $H_{build} = 7.3$ m
LCZ9: Sparsely built	**LCZ10: Heavy industry**	
$\lambda_p = 0.11$; $\lambda_w = 0.23$; $H_{build} = 6.2$ m	$\lambda_p = 0.25$; $\lambda_w = 0.6$; $H_{build} = 14.0$ m	

Table 1. Rendering in the visible part of the solar spectrum of the urban morphologies.

- Purely direct downwelling solar radiation at the top of the UCL is achieved in HTRDR-Urban by setting the radiative properties of the atmosphere to those of a vacuum. As a result, there is no downwelling scattered radiation at the top of the UCL. Simulations are performed for solar elevation angles (γ) of $1°$, $5°$, $10°$, $20°$, $30°$, $45°$, $60°$, $75°$, and $90°$. No particular solar azimuth angle is considered; for each Monte-Carlo realisation, the solar azimuth angle is randomly sampled with a uniform distribution between $0°$ and $360°$. Schoetter et al. (2023) found that the number of Monte-Carlo realisations (N) must be larger for lower values of γ than for higher ones to achieve a given accuracy of the radiative observables. For this reason, N is specified as follows

$$N_\gamma = min\left(10N_{\text{zen}}, \text{int}\left(\frac{N_{\text{zen}}}{\sin(\gamma)}\right)\right). \tag{17}$$

The number of Monte-Carlo realisations for $\gamma = 90°$ (zenith) is $N_{\text{zen}} = 10^6$. int denotes rounding to the nearest integer. The values of N_γ are $1.0e{+}6$, $1.035e{+}6$, $1.155e{+}6$, $1.414e{+}6$, $2.0e{+}6$, $2.924e{+}6$, $5.759e{+}6$, $1.0e{+}7$, and $1.0e{+}7$ for γ values of $90°$, $75°$, $60°$, $45°$, $30°$, $20°$, $10°$, $5°$, and $1°$, respectively.

- Purely diffuse downwelling solar radiation at the top of the UCL is achieved in HTRDR-urban by setting the atmospheric radiative properties to vacuum ones and specifying a sky model with isotropic downwelling solar radiation, resulting in a flux density of $\dot{Q}_D = 1 \text{ W m}^{-2}$.

- For the terrestrial radiation simulations, a 1-D atmospheric profile consisting of mid-latitude summer (MLS) conditions is used in HTRDR-Urban. For this profile, the near-surface air temperature is 294.2 K.

The downwelling direct solar, diffuse solar, and terrestrial radiation at the top of the UCL simulated by HTRDR-Urban are used as radiation forcing for HTRDR-Urban, TEB-Classical, and TEB-SPARTACUS.

3.4 Numerical tests and uncertainty quantification

The following numerical tests are performed with HTRDR-Urban, SPARTACUS-Urban, TEB-Classical, and TEB-SPARTACUS:

- For the urban geometries without trees, simulations are made for purely direct and purely diffuse downwelling solar radiation using a uniform urban facet albedo of 0.3, which is characteristic of common building materials such as concrete or brick, although there is a wide variety of impervious urban material albedo values (Kotthaus et al., 2014). The same albedo value is chosen for all surfaces in the scene, because the objective is to investigate only the effect of the changed urban geometry assumptions. An additional simulation is performed with HTRDR-Urban for the representative street canyon geometry.

- For the urban geometries with trees, simulations with HTRDR-Urban, TEB-Classical, and TEB-SPARTACUS are made for direct and diffuse solar radiation using a uniform urban facet albedo of 0.4, which corresponds to the broadband single scattering albedo of a leaf. For simplicity, the albedos of the other urban facets are set to the same value.

- For all urban geometries, simulations are performed for terrestrial radiation using a uniform urban facet emissivity of 0.9, a value close to the observed emissivities for a variety of impervious urban surface materials (Kotthaus et al., 2014).

In five sensitivity tests, the skin surface temperature (T_{surf}) of all urban facets including tree leaves is set such that the difference to the near-surface air temperature of 294.2 K is -10 K ($T_{\text{surf}} = 284.2$ K), 0 K ($T_{\text{surf}} = 294.2$ K), 10 K ($T_{\text{surf}} = 304.2$ K), 20 K ($T_{\text{surf}} = 314.2$ K), and 30 K ($T_{\text{surf}} = 324.2$ K). These values span the range of plausible differences between skin surface temperature and air temperature near the surface with -10 K corresponding to a nocturnal situation with clear sky and a negative surface energy balance leading to a skin surface temperature lower than the air temperature and 30 K a situation with strong solar radiation leading to much higher skin surface temperature than the air temperature. No distinction is made in the skin surface temperature between sunlit and shaded surfaces. This simplifies the complexity compared to a realistic situation. This simplication allows to investigate the isolated effect of the changed urban geometry.

The SPARTACUS-Urban simulations use a vertical grid with a resolution of 1 m; the half levels of the nth grid point are located at $z_{\text{spu},n} = n - 0.5$ m $\forall\ n\ in\ [1, \text{int}(H_{max}) + 1]$. H_{max} is the maximum building height in the district. On this vertical grid, the plan area building ($\lambda_p(z_n)$) and the tree density ($\lambda_{\text{tree}}(z_n)$) at the nth level are defined as follows

$$\lambda_p(z_n) = \sum_{i=1}^{N_{\text{build}}} \begin{cases} \frac{A_{\text{build},i}}{A_{\text{district}}}, & \text{if } H_{\text{build},i} \geq z_{\text{spu},n} \\ 0, & \text{otherwise} \end{cases} \tag{18}$$

$$\lambda_{\text{tree}}(z_n) = \sum_{i=1}^{N_{\text{tree}}} \begin{cases} \frac{A_{\text{tree},i}}{A_{\text{district}}}, & \text{if } H_{\text{tree},i} \geq z_{\text{spu},n} \\ 0, & \text{otherwise} \end{cases} \tag{19}$$

N_{build} and N_{tree} are the number of buildings and trees in the district. $A_{\text{build},i}$, $H_{\text{build},i}$ and $A_{\text{tree},i}$, $H_{\text{tree},i}$ are the footprint area and height of the ith building and tree. A_{district} is the area of the district.

The normalised building perimeter ($np_{\text{build}}(z_n)$) and tree perimeter ($np_{\text{tree}}(z_n)$) is calculated as follows

$$np_{\text{build}}(z_n) = \sum_{i=1}^{N_{\text{build}}} \begin{cases} \frac{p_{\text{build},i}}{A_{\text{district}}}, & \text{if } H_{\text{build},i} \geq z_{\text{spu},n} \\ 0, & \text{otherwise} \end{cases} \tag{20}$$

$$np_{\text{tree}}(z_n) = \sum_{i=1}^{N_{\text{tree}}} \begin{cases} \frac{p_{\text{tree},i}}{A_{\text{district}}}, & \text{if } H_{\text{tree},i} \geq z_{\text{spu},n} \\ 0, & \text{otherwise} \end{cases} \tag{21}$$

where $p_{\text{build},i}$ and $p_{\text{tree},i}$ are the perimeters of the ith building and tree respectively.

The characteristic scale of the building ($D(z_n)$ and tree ($D_{\text{tree}}(z_n)$) scale at the nth level is then calculated assuming cylindrical buildings and trees:

$$D(z_n) = \frac{4\,\lambda_p(z_n)}{np_{\text{build}}(z_n)} \tag{22}$$

325
$$D_{\text{tree}}(z_n) = \frac{4 \, \lambda_{\text{tree}}(z_n)}{np_{\text{tree}}(z_n)} \qquad (23)$$

With this setup, the SPARTACUS-Urban simulations take into account the variety of building heights.

The uncertainties of the radiative observables are quantified as follows:

– For the direct solar radiation, the simulated radiative observables are plotted as a function of γ for selected urban morphologies. The normalised mean absolute error ($\bar{\Gamma}$, Eq. 24) is defined to quantify the uncertainty of a radiative observable over different values of γ. Uncertainty is defined here as the difference between the TEB observable ($O_{\text{TEB},\gamma}$) and the HTRDR-Urban observable ($O_{\text{HTRDR},\gamma}$).

$$\bar{\Gamma} = \frac{\sum_\gamma \dot{Q}_{D,\gamma} |O_{\text{TEB},\gamma} - O_{\text{HTRDR},\gamma}|}{\sum_\gamma \dot{Q}_{D,\gamma}} \qquad (24)$$

– For the diffuse solar radiation and the terrestrial infrared radiation, the absolute error (Γ) of the radiative observable is defined as

335
$$\Gamma = |O_{\text{TEB}} - O_{\text{HTRDR}}| \qquad (25)$$

3.5 Validation of Mean Radiant Temperature

TEB-Classical and TEB-SPARTACUS calculate an outdoor district-average MRT value for a person in the shade (MRT_{shade}, Equation 15) and exposed to the sun (MRT_{sun}, Equation 16). HTRDR-Urban allows to calculate the spatial distribution of MRT within the district. It is therefore possible to compare the distribution of MRT values simulated by HTRDR-Urban and 340 the MRT_{sun} and MRT_{shade} values simulated by TEB. This is done here for the example of the LCZ4 district, with $\gamma = 30°$, the mid-latitude summer atmospheric profile with a near-surface air temperature of 294.2 K, and uniform surface temperatures of $T_{\text{surf}} = 314.2$ K. All surfaces have a solar albedo of 0.3 and a terrestrial infrared emissivity of 0.9. HTRDR-Urban is used to calculate a 1 m resolution MRT map. It is also used to calculate the downwelling direct solar, diffuse solar, and terrestrial radiation at the top of the UCL. These radiative fluxes are used for the meteorological forcing of TEB. The solar azimuth angle 345 used by HTRDR-Urban is $337.5°$ from north, clockwise, whereas TEB assumes a uniform street orientation with respect to the solar azimuth.

4 Results

4.1 Solar radiation, urban morphologies without trees

The results for the direct-only downwelling solar radiation and the LCZ2a, LCZ4, and LCZ9 morphologies are shown in 350 Figure 2. The results for the other morphologies are shown in Figures B1 to B3. For LCZ9, with its low λ_p and λ_w, most of the downwelling solar radiation ($\dot{Q}_D$) is absorbed by the ground ($\dot{Q}_G$) or reflected ($\dot{Q}_U$), except for low values of γ,

when the walls absorb ($\dot{Q}_W$) most of the $\dot{Q}_D$. This is captured by TEB-Classical and TEB-SPARTACUS. However, for TEB-Classical, $\frac{\dot{Q}_W}{\dot{Q}_D}$ is overestimated and $\frac{\dot{Q}_G}{\dot{Q}_D}$ is underestimated for γ between $5°$ and $20°$. This is because the infinitely-long street canyon geometry used by TEB-Classical leads to too low shading of building walls by other buildings (Schoetter et al., 2023).

355 TEB-SPARTACUS corrects this shortcoming of TEB-Classical almost perfectly, because the cube-like LCZ9 morphology respects well the SPARTACUS-Urban assumption of a decreasing exponential function for p_{ww} and p_{gw} (Stretton et al., 2022). Similar to the results of Caliot et al. (2022), the TEB-Classical results are almost identical to the HTRDR-Urban results for the infinitely-long street canyon, which is due to the analytical solution of the radiosity method under these conditions (vacuum and Lambertian surfaces). For γ below $5°$, the fraction of solar radiation absorbed by the roofs ($\frac{\dot{Q}_R}{\dot{Q}_D}$) is underestimated by both

360 TEB-Classical and TEB-SPARTACUS, because with a uniform H_{build}, the shading of the roofs by higher buildings cannot be represented. This shortcoming of TEB-SPARTACUS could be overcome by introducing a variety of building heights at each grid point in TEB, which is demonstrated by the almost perfect agreement between SPARTACUS-Urban and HTRDR-Urban. For LCZ2a, TEB-Classical overestimates $\frac{\dot{Q}_W}{\dot{Q}_D}$ and underestimates $\frac{\dot{Q}_G}{\dot{Q}_D}$ for γ between $20°$ and $75°$ for the same reason as for LCZ9. This problem is improved by TEB-SPARTACUS, but there are still small biases of $\frac{\dot{Q}_W}{\dot{Q}_D}$ and $\frac{\dot{Q}_G}{\dot{Q}_D}$, because the selected

365 LCZ2a with street canyons and building courtyards has p_{ww} and p_{gw} which deviate more from the decreasing exponential function than for LCZ9. For LCZ2a, the SPARTACUS-Urban results are also slightly different from the HTRDR-Urban results, which could be due to the deviation of p_{ww} and p_{gw} from the decreasing exponential distribution.

For LCZ4, TEB-SPARTACUS improves $\frac{\dot{Q}_W}{\dot{Q}_D}$ and $\frac{\dot{Q}_G}{\dot{Q}_D}$ over TEB-Classical for γ above $20°$. For lower γ, deficiencies of TEB-SPARTACUS remain because it does not represent the heterogeneous building height. The results for SPARTACUS-Urban

370 show that the inclusion of a variety of building heights in TEB could significantly improve the results for the LCZ4 morphology consisting of blocks without internal courtyards.

Figure 3 shows $\bar{\Gamma}$ for all urban morphologies and radiative observables. For both TEB-Classical and TEB-SPARTACUS, the highest $\bar{\Gamma}$ values are found for $\frac{\dot{Q}_W}{\dot{Q}_D}$ and $\frac{\dot{Q}_G}{\dot{Q}_D}$, while $\frac{\dot{Q}_U}{\dot{Q}_D}$ and $\frac{\dot{Q}_R}{\dot{Q}_D}$ have lower $\bar{\Gamma}$. The $\bar{\Gamma}$ values are highest for the high-rise LCZ1 and LCZ4 morphologies and lowest for the low-rise LCZ3, LCZ6, LCZ8, and LCZ9 morphologies. No difference between

375 TEB-Classical and TEB-SPARTACUS of $\bar{\Gamma}$ is found for $\frac{\dot{Q}_R}{\dot{Q}_D}$, because both do not consider a variety of building heights at each grid point. TEB-SPARTACUS leads to a significant improvement of the other radiative observables for most urban geometries. TEB-SPARTACUS reduces $\bar{\Gamma}$ for $\frac{\dot{Q}_W}{\dot{Q}_D}$ compared to TEB-Classical by 50% to 90% for all morphologies except for LCZ1 (-16%), LCZ2a (-34%) and LCZ2a with flat roofs (-19%). For LCZ1, the large variety of building heights leads to a lower improvement due to TEB-SPARTACUS whereas for LCZ2 it is the prevalence of courtyards and street canyons that leads to

380 deviations from the decreasing exponential distribution assumption for p_{ww} and p_{gw}. With TEB-SPARTACUS, the $\bar{\Gamma}$ values for $\frac{\dot{Q}_G}{\dot{Q}_D}$ are reduced by 40% to 70% compared to TEB-Classical, again with the exception of LCZ1 (-13%), LCZ2a (-11%), and LCZ2a with flat roofs (-35%). TEB-SPARTACUS reduces the $\bar{\Gamma}$ values for $\frac{\dot{Q}_U}{\dot{Q}_D}$ by 35% to 62%, except for LCZ1, LCZ2a, and LCZ6a where it increases. However, this result must be modulated since $\frac{\dot{Q}_U}{\dot{Q}_D}$ is probably only well simulated by TEB-Classical due to error compensation. The comparison of the results for pitched and corresponding flat roof morphologies shows that

385 TEB-SPARTACUS reduces the uncertainties of the radiative observables for pitched roof morphologies to a comparable extent as for flat roof morphologies.

Figure 4 shows the Γ values obtained for TEB-Classical and TEB-SPARTACUS for the purely diffuse downwelling solar radiation. The results are similar to those obtained for direct downwelling solar radiation. For $\frac{\dot{Q}_R}{\dot{Q}_D}$, the Γ values are the same for TEB-Classical and TEB-SPARTACUS, because both do not take into account the variety of building heights. The Γ values for $\frac{\dot{Q}_W}{\dot{Q}_D}$ are reduced by 50% to 95% for all morphologies except LCZ1 and LCZ2a with flat roofs where they are increased by 40%. The Γ values for $\frac{\dot{Q}_G}{\dot{Q}_D}$ are reduced by 50% to 95% with the noted exceptions of LCZ1 (increase of 23%), LCZ2a (decrease of only 11%), and LCZ9 with pitched roofs (increase of 2%). However, for LCZ9 with flat roofs, Γ is reduced by 84% with TEB-SPARTACUS compared to TEB-Classical. Schoetter et al. (2023) has shown that not considering pitched roofs can worsen the UCM results for low-rise urban morphologies. The result here shows that at least in some cases also the benefits of TEB-SPARTACUS compared to TEB-Classical due to neglecting the pitched roofs. The Γ for $\frac{\dot{Q}_U}{\dot{Q}_D}$ is reduced by 25% to 97% with TEB-SPARTACUS compared to TEB-Classical, except for LCZ1 and LCZ2a where it increases, but starting from very low values in TEB-Classical, which could be due to error compensation.

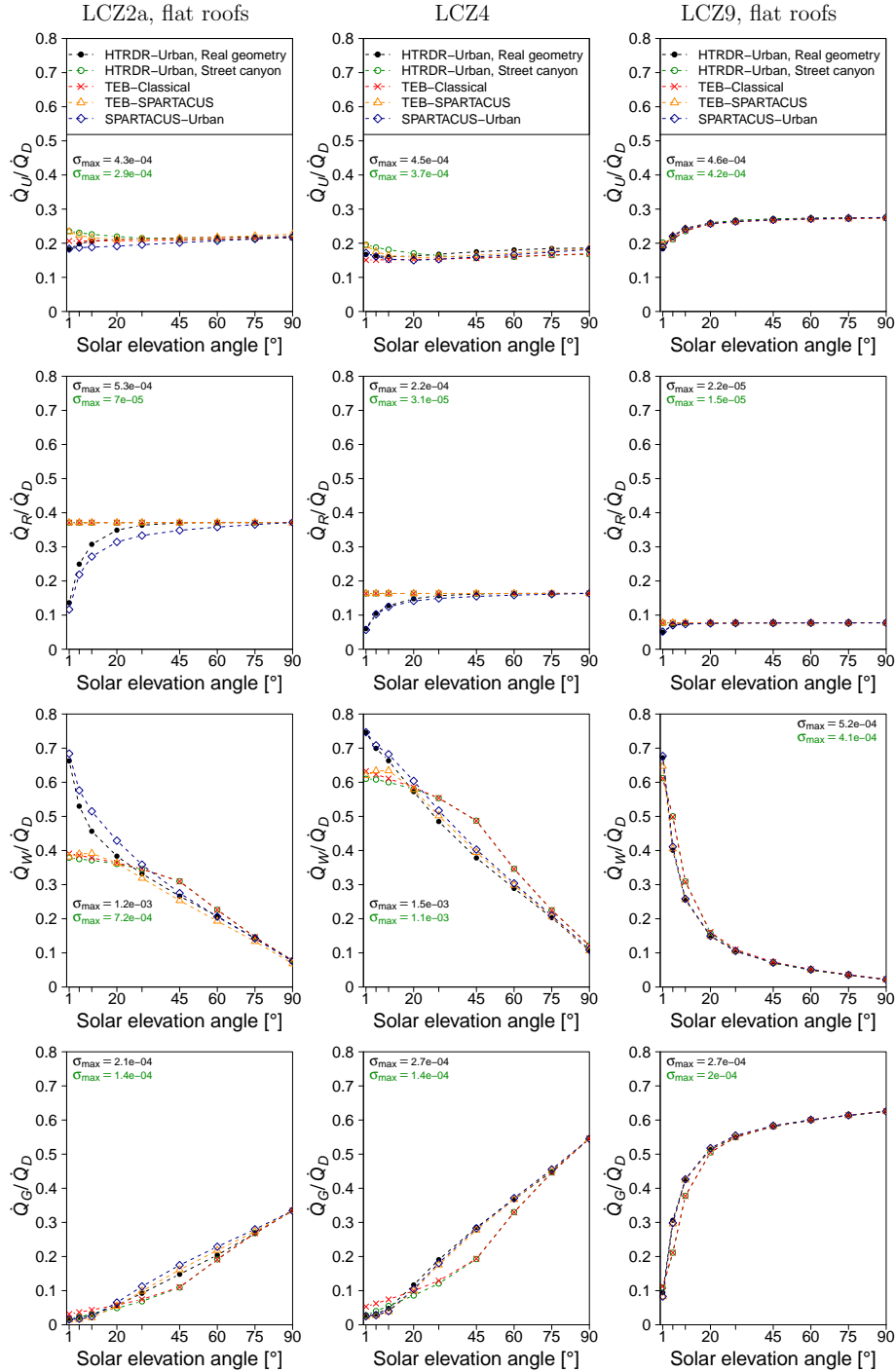



Figure 2. Fraction of the downwelling direct solar radiation ($\dot{Q}_D$) that is reflected by the city ($\dot{Q}_U$), absorbed by the roofs ($\dot{Q}_R$), the walls ($\dot{Q}_W$), or the ground ($\dot{Q}_G$) simulated by the reference model Monte-Carlo model HTRDR-Urban, the urban radiation model SPARTACUS-Urban, and the urban canopy model TEB with the Classical and the SPARTACUS-Urban radiation scheme. The values of $\sigma_{\max}$ indicate the maximum value of the standard deviation of the radiative observable obtained from the Monte-Carlo simulations for all values of solar elevation angle.

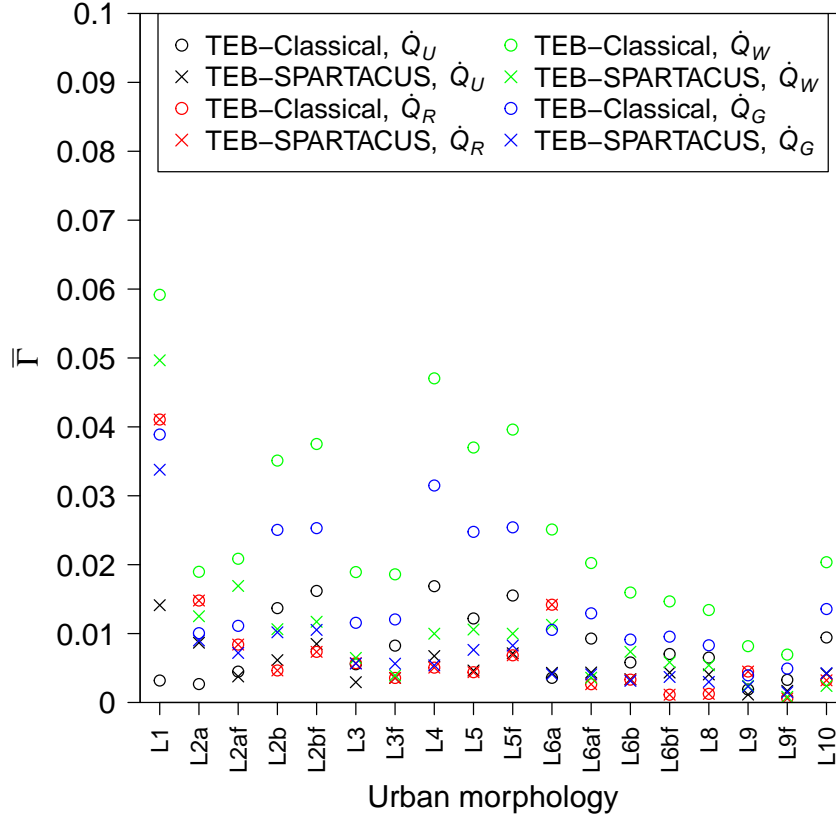



Figure 3. Normalised mean absolute error ($\bar{\Gamma}$, Eq. 24) of the direct solar radiation that is reflected by the city ($\dot{Q}_U$), absorbed by the roofs ($\dot{Q}_R$), the walls ($\dot{Q}_W$), or the ground ($\dot{Q}_G$) when simulated by TEB with the Classical (TEB-Classical) and the SPARTACUS-Urban (TEB-SPARTACUS) radiation scheme. L1 is LCZ1, L2af is LCZ2a with flat roofs, and so on.

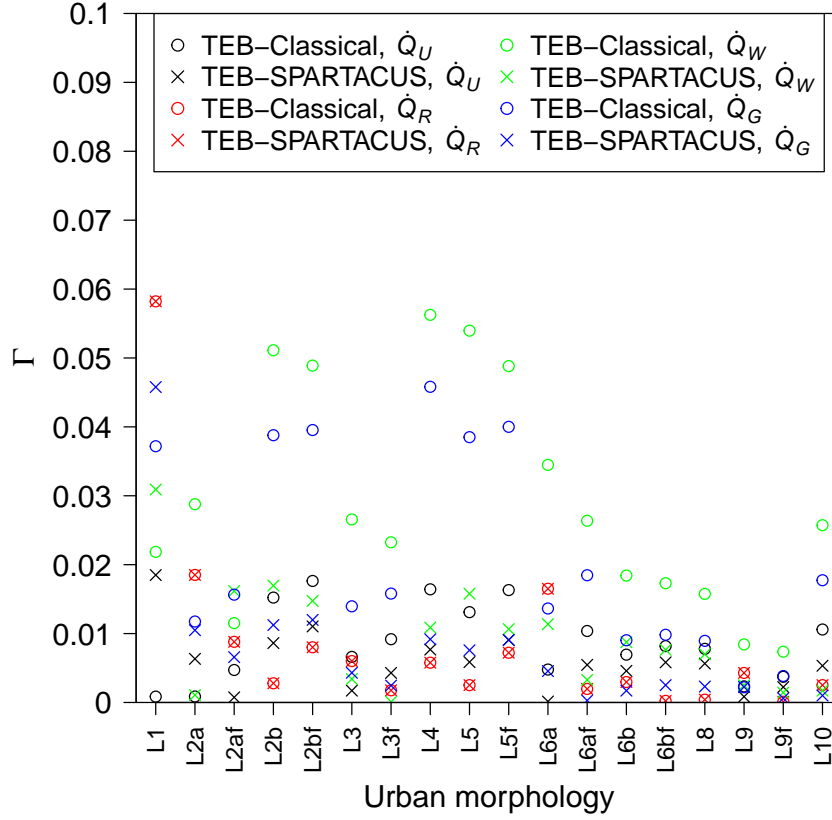



Figure 4. Absolute error (Γ, Eq. 25) of the fraction of diffuse solar radiation that is reflected by the city ($\frac{\dot{Q}_U}{\dot{Q}_D}$), absorbed by the roofs ($\frac{\dot{Q}_R}{\dot{Q}_D}$), the walls ($\frac{\dot{Q}_W}{\dot{Q}_D}$), or the ground ($\frac{\dot{Q}_G}{\dot{Q}_D}$) when simulated by TEB with the Classical (TEB-Classical) and the SPARTACUS-Urban (TEB-SPARTACUS) radiation scheme. L1 is LCZ1, L2af is LCZ2a with flat roofs, and so on.

4.2 Solar radiation, urban morphologies with trees

For direct downwelling solar radiation, Figure 5 shows the results for the LCZ5 and LCZ9 districts with flat roofs and 10 m
high trees. The detailed results for the LCZ2a and LCZ4 districts with flat roofs and trees are shown in Figure C1. Figure 6
shows the $\bar{\Gamma}$ values for all radiative observables and all districts with trees. The LCZ9 district is particular in the way that
the trees are quite large ($H_{\text{tree}} = 10$ m) compared to the low-rise buildings ($H_{\text{mean}} = 6.2$ m). As a consequence, the fraction
of downwelling solar radiation absorbed by the trees ($\frac{\dot{Q}_T}{\dot{Q}_D}$) increases from below 0.1 for γ above $45°$ to above 0.5 for a γ
of $1°$. TEB-Classical represents the trees as a turbid layer that fills the entire street canyon between the trunk and the tree
height without taking into account the individual tree borders. It therefore does not capture the increase in $\dot{Q}_T$ for low values
of γ. As a result, $\frac{\dot{Q}_T}{\dot{Q}_D}$ is slightly underestimated by TEB-Classical for γ above $45°$ and strongly underestimated for lower γ.
TEB-SPARTACUS simulates $\frac{\dot{Q}_T}{\dot{Q}_D}$ well. The other terms of the solar radiation budget are also improved with TEB-SPARTACUS
compared to TEB-Classical. $\frac{\dot{Q}_W}{\dot{Q}_D}$ is significantly reduced for γ below $20°$ with TEB-SPARTACUS due to the enhanced shading
of walls by trees compared to TEB-Classical. $\frac{\dot{Q}_G}{\dot{Q}_D}$ is reduced for γ below $60°$ with TEB-SPARTACUS, because there is more
shading from trees; it matches better with the reference HTRDR-Urban. The $\frac{\dot{Q}_U}{\dot{Q}_D}$ is lower for all γ with TEB-SPARTACUS,
because there are more multiple reflections of solar radiation, leading to a lower probability of reflection towards the sky. Sim-
ilar to the LCZ9 district without trees, an overestimation of $\frac{\dot{Q}_R}{\dot{Q}_D}$ is found for TEB-SPARTACUS, because it neglects the variety
of building heights. The results for SPARTACUS-Urban show that this can be corrected to achieve near perfect results by
taking the variety of building heights into account. Similar improvements of the radiative observables with TEB-SPARTACUS
compared to TEB-Classical are found for LCZ9 with pitched roofs.

For LCZ5 with flat (pitched) roofs, TEB-SPARTACUS reduces the $\bar{\Gamma}$ for $\frac{\dot{Q}_W}{\dot{Q}_D}$ by 76% (68%), by 63% (65%) for $\frac{\dot{Q}_G}{\dot{Q}_D}$, and by
16% (20%) for $\frac{\dot{Q}_T}{\dot{Q}_D}$. For $\frac{\dot{Q}_R}{\dot{Q}_D}$, there is no difference because the buildings are higher than the trees. The $\bar{\Gamma}$ values for $\frac{\dot{Q}_U}{\dot{Q}_D}$ are
higher for TEB-SPARTACUS than for TEB-Classical, but this could be due to the fact that for TEB-Classical the $\frac{\dot{Q}_U}{\dot{Q}_D}$ is well
simulated due to error compensation. SPARTACUS-Urban almost perfectly simulates all radiative observables of the LCZ5
morphology with trees.

For LCZ4, the $\bar{\Gamma}$ values are reduced by 79% for $\frac{\dot{Q}_W}{\dot{Q}_D}$ and $\frac{\dot{Q}_T}{\dot{Q}_D}$, by 74% for $\frac{\dot{Q}_G}{\dot{Q}_D}$, and by 25% for $\frac{\dot{Q}_U}{\dot{Q}_D}$ with TEB-SPARTACUS
compared to TEB-Classical, and are unchanged for $\frac{\dot{Q}_R}{\dot{Q}_D}$. SPARTACUS-Urban simulates almost perfectly all radiative observ-
ables of the LCZ4 morphology with trees.

For LCZ2a with flat (pitched) roofs, TEB-SPARTACUS reduces $\bar{\Gamma}$ by 10% (19%) for $\frac{\dot{Q}_W}{\dot{Q}_D}$, and by 24% (1%) for $\frac{\dot{Q}_G}{\dot{Q}_D}$. The $\frac{\dot{Q}_T}{\dot{Q}_D}$
values are low because not much radiation reaches the few trees in this dense mid-rise morphology; the $\bar{\Gamma}$ for $\frac{\dot{Q}_T}{\dot{Q}_D}$ is almost
unchanged between TEB-SPARTACUS and TEB-Classical. For $\frac{\dot{Q}_U}{\dot{Q}_D}$, TEB-SPARTACUS leads to higher values of $\bar{\Gamma}$ than TEB-
Classical, which could be due to error compensation leading to good performance of TEB-Classical. SPARTACUS-Urban has
similar shortcomings as for LCZ2a without trees, which is due to the deviation of p_{ww} and p_{gw} from the decreasing exponential
function.

Figure 7 shows the Γ of the radiative observables for diffuse downwelling solar radiation and the urban morphologies with
trees. The results are similar to those for direct solar radiation. The Γ values for $\frac{\dot{Q}_T}{\dot{Q}_D}$ are reduced by 50% to 90% with TEB-

SPARTACUS. For $\frac{\dot{Q}_W}{Q_D}$, the Γ values are reduced by 73% to 97% with TEB-SPARTACUS with the notable exception of LCZ2a with flat roofs (67% increase). This could be because TEB-Classical gives good results for the wrong reason due to error compensation. The Γ values for $\frac{\dot{Q}_G}{Q_D}$ are reduced by 48% to 98% for TEB-SPARTACUS, except for LCZ2a where they increase by 24%. For $\frac{\dot{Q}_U}{Q_D}$ there is no clear result. There is a decrease of the Γ values for LCZ4 and LCZ9, but an increase for LCZ2a and LCZ5.

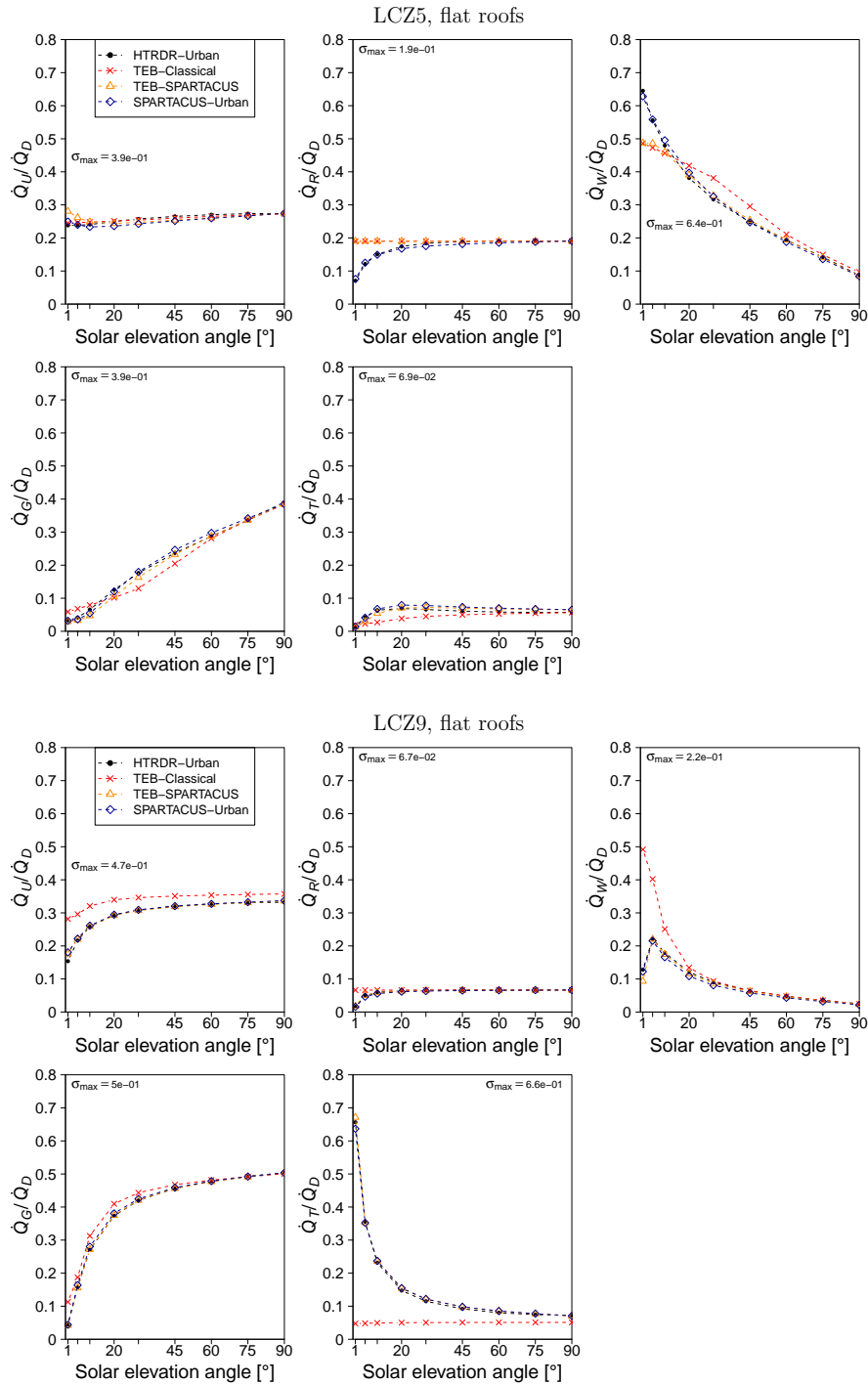



Figure 5. Fraction of the direct downwelling solar radiation ($\dot{Q}_D$) that is reflected ($\dot{Q}_U$), absorbed by the roofs ($\dot{Q}_R$), the walls ($\dot{Q}_W$), the ground ($\dot{Q}_G$), or urban trees ($\dot{Q}_T$) simulated by the reference Monte-Carlo model HTRDR-Urban, the urban radiation model SPARTACUS-Urban, and the urban canopy model TEB with the Classical (TEB-Classical) and the SPARTACUS-Urban (TEB-SPARTACUS) radiation scheme for the LCZ5 and LCZ9 districts with trees. The values of σ_{max} indicate the maximum value of the standard deviation of the radiative observable obtained from the Monte-Carlo simulations for all values of solar elevation angle.

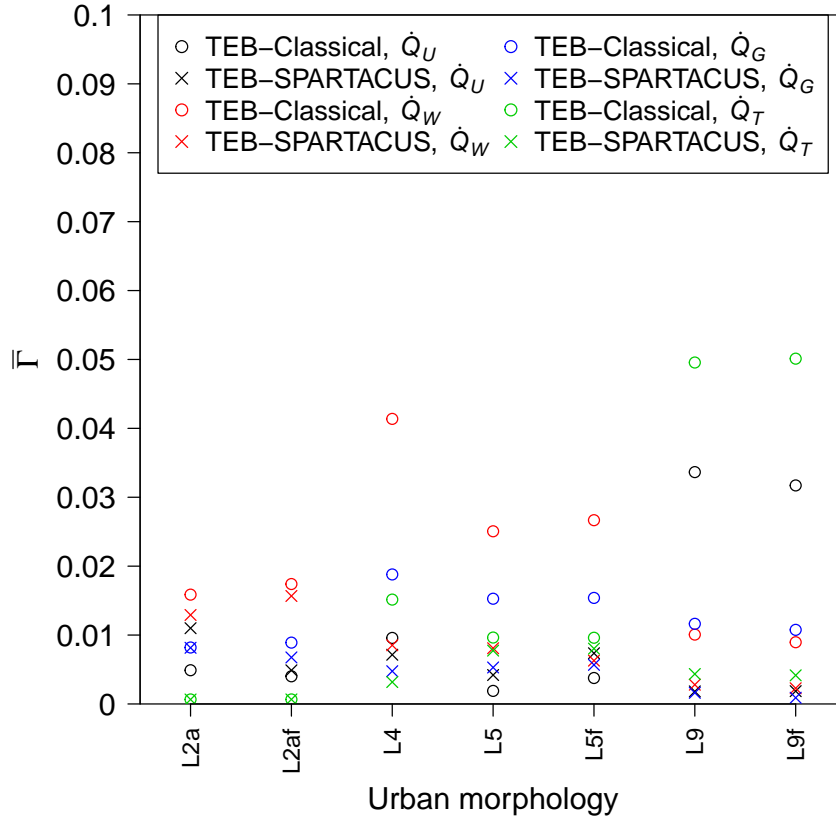



Figure 6. Normalised mean absolute error ($\bar{\Gamma}$, Eq. 24) of the direct solar radiation radiation that is reflected by the city ($\dot{Q}_U$), absorbed by the walls ($\dot{Q}_W$), the ground ($\dot{Q}_G$), or urban trees ($\dot{Q}_T$) when simulated by TEB with the Classical (TEB-Classical) and the SPARTACUS-Urban (TEB-SPARTACUS) radiation scheme for all urban morphologies with trees. The results for the direct solar radiation absorbed by the roofs ($\dot{Q}_R$) are not shown, because the differences between TEB-Classical and TEB-SPARTACUS are very small. L2a is LCZ2a, L2af is LCZ2a with flat roofs, and so on.

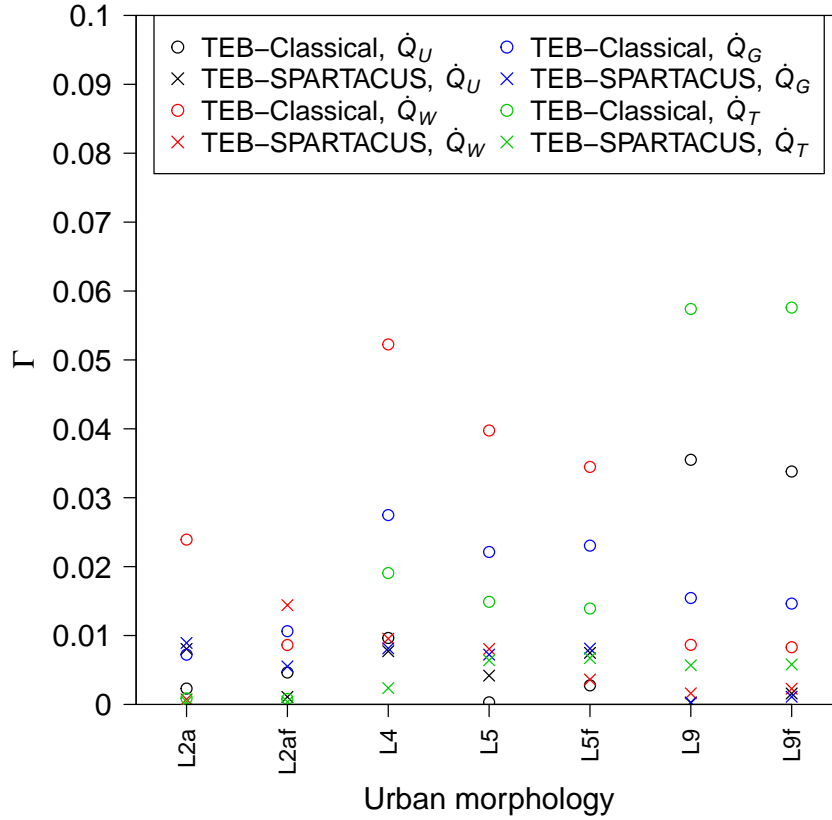



Figure 7. Absolute error (Γ, Eq. 25) of the fraction of diffuse solar radiation that is reflected by the city ($\frac{\dot{Q}_U}{\dot{Q}_D}$), absorbed by the walls ($\frac{\dot{Q}_W}{\dot{Q}_D}$), the ground ($\frac{\dot{Q}_G}{\dot{Q}_D}$), or the urban trees ($\frac{\dot{Q}_T}{\dot{Q}_D}$) when simulated by TEB with the Classical (TEB-Classical) and the SPARTACUS-Urban (TEB-SPARTACUS) radiation scheme. The results for the fraction of radiation absorbed by the roofs are not shown, because they differ only little between TEB-Classical and TEB-SPARTACUS. L1 is LCZ1, L2af is LCZ2a with flat roofs, and so on.

4.3 Terrestrial radiation

Figure 8 shows the Γ of the terrestrial radiation radiative observables or TEB-Classical and TEB-SPARTACUS and the urban morphologies without trees. The Γ values for the terrestrial radiation exchanged by the roofs ($\dot{E}_R$) are very small, except for LCZ1, because the variety in building heights is not taken into account. For $\dot{E}_R$, there is no difference in Γ between TEB-SPARTACUS and TEB-Classical.

For the terrestrial radiation exchanged by the walls ($\dot{E}_W$), the Γ values for TEB-Classical are larger for the mid- and high-rise morphologies and when T_{surf} is greater than the near-surface air temperature of 294.2 K. For $T_{\mathrm{surf}} = 284.2\ K$, TEB-SPARTACUS reduces Γ by about 10%, except for the low-rise LCZ9, LCZ8, and LCZ6b and the high-rise LCZ1. So there is only a small improvement for the case where the skin surface temperature is 10 K lower than the air temperature near the surface. For $T_{\mathrm{surf}} = 294.2\ K$, Γ is reduced by about 30% except for the low-rise LCZ9, LCZ8, and LCZ6b for which it is almost unchanged, and the LCZ1 and (LCZ2 with flat roofs) for which it decreases by 85% (80%). The results for $T_{\mathrm{surf}} = 304.2\ K$, $T_{\mathrm{surf}} = 314.2\ K$, and $T_{\mathrm{surf}} = 324.2\ K$ are similar those for $T_{\mathrm{surf}} = 294.2\ K$. Γ is reduced by 40% to 80% for most morphologies, but the Γ reduction is lower or absent for LCZ9, LCZ8, and LCZ6a.

The results for the Γ values of the terrestrial radiation exchanged by the ground ($\dot{E}_G$) are similar to those for $\dot{E}_W$. For $T_{\mathrm{surf}} = 284.2\ K$, TEB-SPARTACUS reduces Γ by 20% to 30% except for LCZ9, LCZ8, and LCZ6b for which it is reduced by only 10% to 15%. For $T_{\mathrm{surf}} = 284.2\ K$, Γ is reduced by 30% to 80%, with the lowest reductions found for the low-rise morphologies mentioned above. For $T_{\mathrm{surf}} = 304.2\ K$, $T_{\mathrm{surf}} = 314.2\ K$, and $T_{\mathrm{surf}} = 324.2\ K$, Γ is reduced between 55% and 99% for all morphologies, except for LCZ1.

For the terrestrial radiation exchanged with the sky ($\dot{E}_{\mathrm{sky}}$), the Γ values for TEB-Classical are very small for $T_{\mathrm{surf}} = 284.2$ K and increase for higher values of T_{surf}. TEB-SPARTACUS reduces the Γ values for $\dot{E}_{\mathrm{sky}}$ by 50% to 99% for $T_{\mathrm{surf}} = 294.2\ K$, $T_{\mathrm{surf}} = 304.2\ K$, $T_{\mathrm{surf}} = 314.2\ K$, and $T_{\mathrm{surf}} = 324.2\ K$. For $T_{\mathrm{surf}} = 284.2\ K$, TEB-SPARTACUS does not reduce the Γ values for the LCZ9, LCZ8, and LCZ6b, for the other districts it is reduced by 50% to 98%.

Figure 9 shows the Γ values for the terrestrial radiation radiative observables and the urban morphologies with trees. The Γ values for the terrestrial radiation exchanged by the trees ($\dot{E}_T$) are reduced by 45% to 97% with TEB-SPARTACUS compared to TEB-Classical with the notable exception of LCZ9 with $T_{\mathrm{surf}} = 284.2\ K$. The Γ values for $\dot{E}_W$ are lower for TEB-SPARTACUS than for TEB-Classical, except for LCZ2a with flat roofs and $T_{\mathrm{surf}} > T_{\mathrm{air}}$. The Γ reduction is about 15% for $T_{\mathrm{surf}} = 284.2\ K$, 40% for $T_{\mathrm{surf}} = 294.2\ K$, 50% to 70% for $T_{\mathrm{surf}} = 304.2\ K$, 58% to 86% for $T_{\mathrm{surf}} = 314.2\ K$, and 62% to 92% for $T_{\mathrm{surf}} = 324.2\ K$. The Γ values for $\dot{E}_G$ are reduced with TEB-SPARTACUS for all urban morphologies except the LCZ9 ones. The reduction is 20% to 30% for $T_{\mathrm{surf}} = 284.2\ K$, 46% to 78% for $T_{\mathrm{surf}} = 294.2\ K$, 55% to 99% for $T_{\mathrm{surf}} = 304.2\ K$, 60% to 99% for $T_{\mathrm{surf}} = 314.2\ K$, and 64% to 92% for $T_{\mathrm{surf}} = 324.2\ K$. TEB-SPARTACUS reduces the Γ values of $\dot{E}_{\mathrm{sky}}$ by 50% to 96% for $T_{\mathrm{surf}} = 284.2\ K$, by 88% to 96% for $T_{\mathrm{surf}} = 294.2\ K$, by 91% to 96% for $T_{\mathrm{surf}} = 304.2\ K$, and by 91% to 97% for $T_{\mathrm{surf}} = 314.2\ K$ and $T_{\mathrm{surf}} = 324.2\ K$.

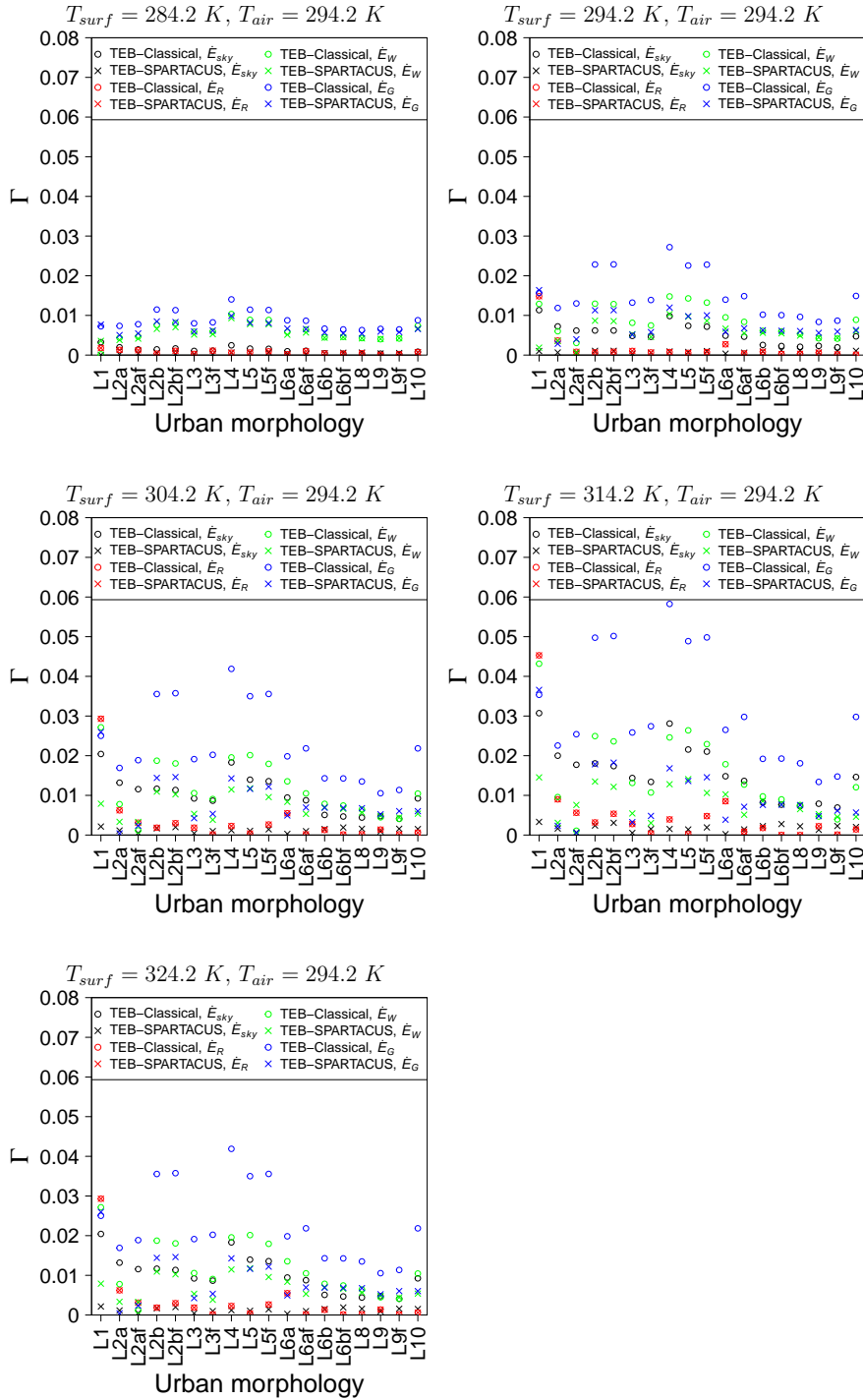



Figure 8. Absolute error (Γ, Eq. 25) of the terrestrial radiation that the city exchanges with the sky ($\dot{E}_{sky}$) and that is exchanged by the roofs ($\dot{E}_R$), the walls ($\dot{E}_W$), and the ground ($\dot{E}_G$) when simulated by TEB with the Classical (TEB-Classical) and the SPARTACUS-Urban (TEB-SPARTACUS) radiation scheme. $\dot{E}_R$ is not shown because its Γ does not differ between TEB-Classical and TEB-SPARTACUS. L1 is LCZ1, L2af is LCZ2a with flat roofs, and so on.

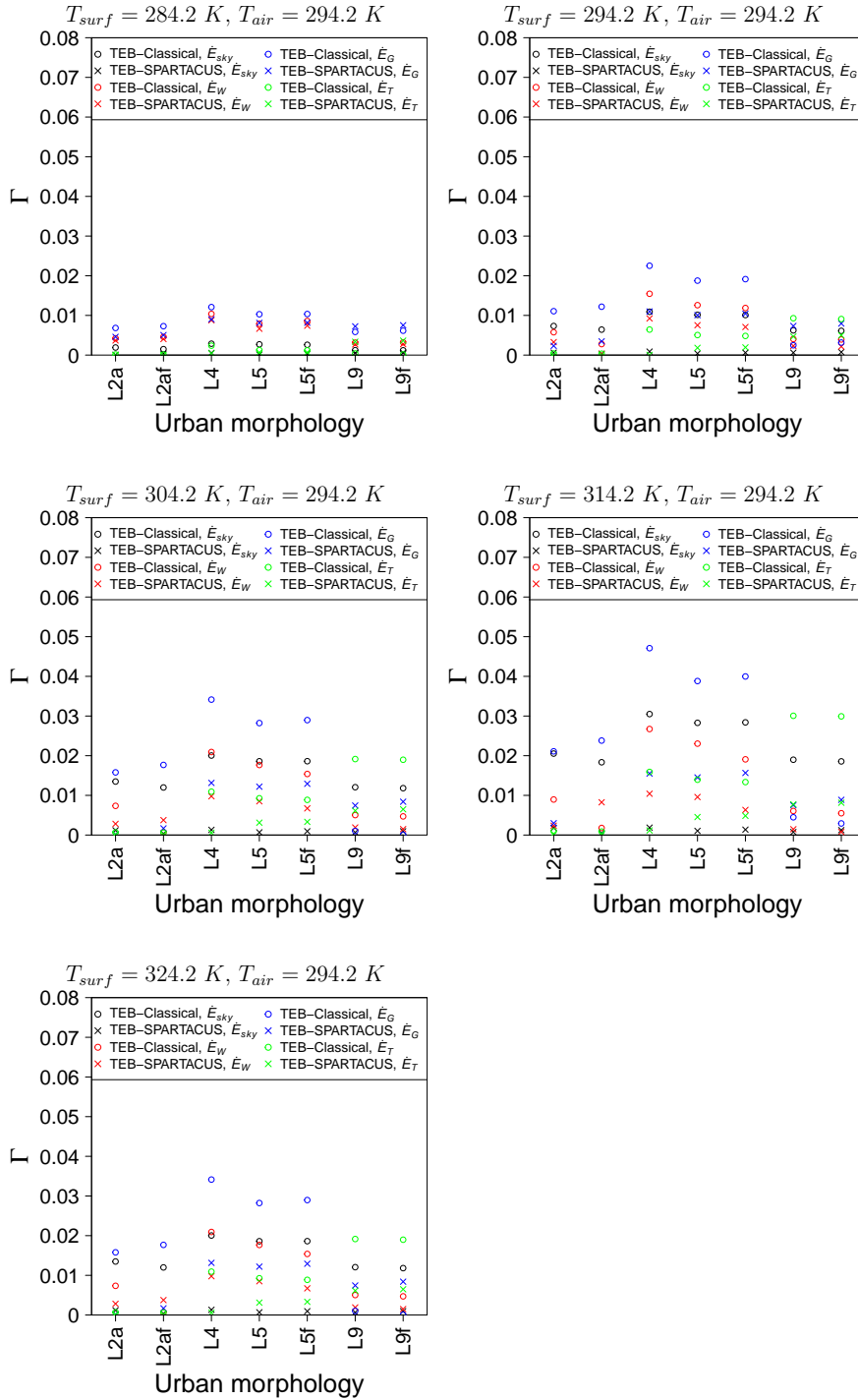



Figure 9. Absolute error (Γ, Eq. 25) of the terrestrial radiation that the city exchanges with the sky ($\dot{E}_{\mathrm{sky}}$) and that is exchanged by the walls ($\dot{E}_W$), the ground ($\dot{E}_G$), and the trees ($\dot{E}_T$) when simulated by TEB with the Classical (TEB-Classical) and the SPARTACUS-Urban (TEB-SPARTACUS) radiation scheme. L2a is LCZ2a, L2af is LCZ2a with flat roofs, and so on.

4.4 Mean Radiant Temperature

470 The spatial distribution of MRT simulated by HTRDR-Urban in the LCZ4 district (Figure 10a) is strongly influenced by the shading from buildings. Its probability density (Figure 10b) shows that the MRT values lie between 34°C and 42°C in the shaded areas and between 60°C and 70°C in the sunlit areas. The highest MRT values are near the walls, which are exposed to the sun because of the reflected solar radiation. There are almost no MRT values between 42°C and 60°C, which means that the TEB approach to providing a diagnostic for MRT_{sun} and MRT_{shade} is useful in this case. TEB-Classical simulates

475 a too high value for both MRT_{sun} and MRT_{shade}. The TEB-SPARTACUS values for MRT_{sun} and MRT_{shade} are 2.5°C lower than the values simulated by TEB-Classical. The MRT_{sun} value simulated by TEB-SPARTACUS agrees very well with the most frequent MRT values simulated by HTRDR-Urban in the sunlit areas. The MRT_{shade} value simulated by TEB-SPARTACUS is still 4°C higher than the most frequent MRT values simulated by HTRDR-Urban in the shaded areas. The general overestimation of MRT_{shade} by TEB could be due to the consideration of the diffuse downwelling solar radiation

480 as isotropic, whereas in reality a part of it comes from a direction close to the sun. In the reference model HTRDR-Urban, this is represented leading to lower MRT values in the shaded areas because the circumsolar diffuse radiation does not reach the human body. As shown in Figure 2, for LCZ4 and $\gamma = 30°$, with TEB-Classical, not enough direct solar radiation reaches the ground and too much reaches the walls. The MRT_{sun} value is therefore too high in TEB-Classical, because too much solar radiation reflected by the walls reaches the human body, which is assumed to be in the sun. The MRT_{shade} value is too

485 high in TEB-Classical for the same reason. TEB-SPARTACUS corrects this problem for both MRT_{sun} and MRT_{shade}. The uncertainty of MRT_{shade} arising from the use of the radiative fluxes at ground level instead of 1 m above ground level has been estimated to be 0.6 K. Since the sensitivity of thermal comfort indicators such as the UTCI to MRT is about 0.25 K (Schoetter et al., 2013), this uncertainty of MRT leads to an uncertainty of 0.15 K of such indicators. Additional output diagnostics could be added in future SPARTACUS-Urban versions to eliminate this uncertainty.

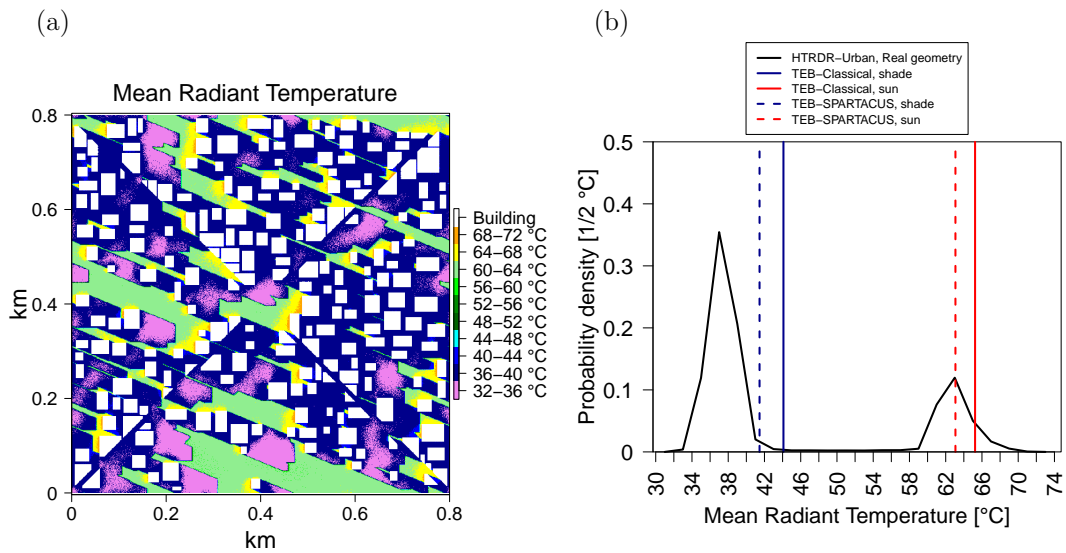



Figure 10. (a) Spatial distribution at 1 m horizontal resolution of the Mean Radiant Temperature simulated by HTRDR-Urban in the LCZ4 district with $\gamma = 30°$ and a solar azimuth angle of $337.5°$ from north, clockwise. (b) Probability density of Mean Radiant Temperature simulated by HTRDR-Urban and the MRT_{sun} and MRT_{shade} values simulated by TEB-Classical and TEB-SPARTACUS.

5 Discussion

The validation of TEB-SPARTACUS with the Monte-Carlo-based reference model HTRDR-Urban shows improvements in radiative observables related to solar and terrestrial radiation over a variety of urban morphologies.

TEB-SPARTACUS corrects a major shortcoming of the infinitely-long street canyon assumption of TEB-Classical, which was documented by Schoetter et al. (2023). This shortcoming consists in too high (too low) absorption of direct solar radiation by the building walls (the ground) due to the wrong distribution of wall-to-wall distances. This improvement can be of the order of 10% of the downwelling direct solar radiation, thus potentially improving the simulated energy balance of buildings or ground vegetation, and outdoor human thermal comfort.

For direct downwelling solar radiation and averaged over all solar elevation angles, TEB-SPARTACUS simulates almost all radiative observables with a higher accuracy than TEB-Classical. The error is reduced by 50% to 90% for block-like urban morphologies such as LCZ3, LCZ4, LCZ5, LCZ8, LCZ9, and LCZ10. For these morphologies, the decreasing exponential function assumption for the distribution of wall-to-wall and ground-to-wall distances made by SPARTACUS-Urban holds. But also for the other morphologies, the radiative observables are simulated more accurately with TEB-SPARTACUS than with TEB-Classical. For the diffuse downwelling solar radiation, the results are very similar to those for the direct downwelling solar radiation when averaging over different values of the solar elevation angle. TEB-SPARTACUS reduces the error of the radiative observables by 50% to 95% with the exception of the compact high-rise LCZ1 and the dense mid-rise LCZ2.

TEB-SPARTACUS improves the solar radiation absorbed by urban trees because of its representation of trees as cylinders, conserving the tree surface area in contact with the air and buildings. This contact area is underestimated by TEB-Classical, which treats urban trees as a homogeneous turbid layer that fills the entire street canyon in the horizontal directions and between the trunk and the tree height in the vertical direction. TEB-SPARTACUS can also represent trees higher than buildings, leading to improved results for such urban districts. As a result of the improved simulation of the interaction of radiation with urban trees, the other radiative observables are also improved. The improved representation of the radiation absorbed by urban trees could potentially improve the results of simulated evapotranspiration, photosynthesis, or CO_2 uptake by trees.

Uncertainties of the direct solar radiation observables for low values of the solar elevation angle are found with TEB-SPARTACUS for the high-rise districts, which is due to the neglect of the variety of building heights. These uncertainties could become more relevant in urban districts with heterogeneous building types, i.e. consisting of a mixture of LCZs. The results obtained when simulating the districts with SPARTACUS-Urban and a 1 m resolution vertical discretisation of building density and characteristic diameter show that SPARTACUS-Urban is well suited to handle such a variety of building heights. The consideration of a variety of building heights on a district scale is therefore a logical next step in the development of TEB.

Schoetter et al. (2023) found that the effective urban albedo ($\frac{\dot{Q}_U}{\dot{Q}_D}$) is an observable that is not strongly influenced by the simplifications of urban morphology such as the assumption of an infinitely-long streetcanyon. The results of the present study are consistent with these earlier findings, since only little or no improvement in the simulated effective urban albedo is found when using TEB-SPARTACUS instead of TEB-Classical.

TEB-SPARTACUS leads to a reduction in the uncertainties of simulated radiative observables for terrestrial infrared radiation.

The improvement is particularly high (50% to 99%) when the skin surface temperature is higher than the near-surface air temperature, which is often the case in urban areas. The improvement is found for all urban morphologies except for LCZ1, where the variety of building heights must be taken into account to obtain good results. TEB-SPARTACUS reduces the error of the simulated absorption of terrestrial infrared radiation by urban trees by 45% to 97% and consequently also the other radiative observables in urban districts with trees.

The validation of the Mean Radiant Temperature simulated by TEB-Classical and TEB-SPARTACUS for an open high-rise district has shown that, given the bimodal distribution of MRT in the district, the strategy used in TEB of providing one MRT value for a person in the shade and one for a person in the sun is useful. Furthermore, the MRT values for shade and sun simulated by TEB-SPARTACUS are closer to the most frequent values in the shaded and sunlit areas simulated by HTRDR-Urban than those simulated by TEB-Classical. This is because the amount of solar radiation reflected by the building walls on the human body is better simulated by TEB-SPARTACUS than by TEB-Classical.

The present study has several limitations. Only urban districts with one building type and morphology were studied. In real cities, there is often a variety of building types in one district, leading, for example, to a greater variety of building heights than in the districts investigated in this study. As TEB-SPARTACUS does not represent the variety of building heights, it may predict radiative observables with less accuracy in such districts. Furthermore, no variety of urban material albedo, emissivity, or skin surface temperature were investigated. TEB-SPARTACUS may have a different performance for heterogeneous districts than for the homogeneous ones that were investigated in this study. Also, only one type of urban tree with homogeneous height and diameter was investigated. Urban districts with a variety of tree types and tree characteristics should be analysed to investigate whether the results of this study still apply to them.

In real cities, overhanging and pitched roofs are common. Simulations with HTRDR-Urban (not shown) show that such features can strongly change the direct solar radiation budget (e.g. the partitioning between the radiation absorbed by the roofs or the walls). Neither TEB-Classical nor TEB-SPARTACUS represent such features. The accuracy of the simulated radiative observables reported here may therefore be too high compared to real cities.

The Mean Radiant Temperature simulated by TEB has only been analysed for one urban district and one solar zenith and azimuth angle. Further research is required to quantify how well the TEB diagnostics of MRT in shade and sun compare with the actual distribution of MRT in a variety of urban districts and with a variety of solar positions.

6 Conclusions

The TEB urban canopy model has been coupled with the urban radiation model SPARTACUS-Urban, which uses a decreasing exponential for the probability density function of the wall-to-wall and ground-to-wall distances. This is more realistic than the assumption of an infinitely-long street canyon used by the original TEB. While the original TEB uses the radiosity method to calculate the radiative exchanges, SPARTACUS-Urban solves the RTE using the discrete ordinate method. This allows to take into account many additional physical processes such as specular reflections, wavelength-dependent albedo of urban materials, and the interaction of radiation with the air, aerosols, or fog in the UCL. SPARTACUS-Urban also represents urban trees in a

more realistic way, in particular as cylinders that represent the contact surface between trees, air, and building walls.

The TEB-SPARTACUS coupling has been made in a very simple way, preserving the geometric complexity of the original TEB, i.e. there is no variation in building height at each grid point. Furthermore, the urban material albedo and emissivities in TEB are still independent of the wavelength, and atmospheric scattering and absorption are not considered in TEB-SPARTACUS. The difference between TEB-Classical and TEB-SPARTACUS is therefore only due to the changed assumptions about the urban and tree geometry and the replacement of the radiosity method by the discrete ordinate method to calculate the radiative exchanges. With TEB-SPARTACUS, the outdoor Mean Radiant Temperature for a cylindrical human body can be diagnosed based on the radiative fluxes in the vertical and horizontal directions using the discrete ordinate method instead of the radiosity method in TEB-Classical.

TEB-SPARTACUS has been validated against a Monte-Carlo-based reference model (HTRDR-Urban) for procedurally-generated urban morphologies that mimic the Local Climate Zones. The urban morphologies are homogeneous as there is no variety of LCZ, albedo, emissivity, or skin surface temperature at the scale of the district. A significant improvement over TEB-Classical of the key radiative observables, i.e. the direct and diffuse solar, and terrestrial radiation exchanged by the roofs, the walls, the ground, urban trees, and the sky is found when using TEB-SPARTACUS. This could improve the simulated building energy balance (e.g. the heating and air-conditioning energy consumption), outdoor human thermal comfort, urban vegetation evapo-transpiration and CO_2 uptake, and even the urban heat island effect.

The next step in the development of TEB-SPARTACUS is to consider a variety of building heights at each grid point, as this will improve radiative observables in high-rise districts and districts with heterogeneous building heights. Also, an atmospheric radiation scheme could be used by TEB-SPARTACUS to calculate the scattering and absorption of radiation in the UCL. This can improve the simulated terrestrial radiation (Hogan, 2019b; Schoetter et al., 2023). Furthermore, TEB-SPARTACUS can be used in urban climate simulations when TEB is coupled with an atmospheric model such as Meso-NH (Lac et al., 2018) to investigate its impact on the urban heat island effect.

Code availability. The software archive on Zenodo (https://zenodo.org/records/11244064) contains the exact model version used in this article, and a user manual describing the TEB-SPARTACUS namelist and how to install the model, run and plot the validation simulations to reproduce the figures in this article. TEB-SPARTACUS is also included in the free and open-source SURFEXv9.0 (http://www.umr-cnrm.fr/surfex/spip.php?article387) that is under a CeCILL-C license.

Appendix A: Input and output parameters for SPARTACUS-Urban when used in TEB

Table A1 describes how the SPARTACUS-Urban input parameters are specified when it is used within TEB, Table A2 how the output of SPARTACUS-Urban is used by TEB.

Table A1. Input parameters for SPARTACUS-Urban when called by TEB.

Symbol	Parameter	Unit	Provenance
α_{agg}	Aggregated albedo of roof, wall, ground	1	Eq. 4
$\alpha_{\mathrm{ssa,air,lw}}$	Single-scattering albedo of terrestrial radiation with air	1	Set to 0
$\alpha_{\mathrm{ssa,air,sw}}$	Single-scattering albedo of solar radiation with air	1	Set to 0
$\alpha_{\mathrm{ssa,tree,lw}}$	Single-scattering albedo of terrestrial radiation with a leaf	1	Eq. 10
$\alpha_{\mathrm{ssa,tree,sw}}$	Single-scattering albedo of solar radiation with a leaf	1	Set to 0.4
D	Characteristic building diameter	m	Eq. 3
D_{tree}	Characteristic tree diameter	m	Set to 5 m
ϵ_{agg}	Aggregated emissivity of roof, wall, ground	1	Eq. 5
$f_{\mathrm{ref,specular}}$	Fraction of specular reflections from the walls	1	Set to 0
FC_{tree}	Fraction of trees in contact with walls	1	Eq. 9
$\mathrm{FSD}_{\mathrm{tree}}$	Fractional standard deviation of tree optical depth	1	Set to 0
$k_{\mathrm{ext,air,lw}}$	Terrestrial radiation extinction coefficient of air	m^{-1}	Set to 0
$k_{\mathrm{ext,air,sw}}$	Solar radiation extinction coefficient of air	m^{-1}	Set to 0
$k_{\mathrm{ext,tree}}$	Extinction coefficient of urban trees	m^{-1}	Eq. 11
λ_p	Plan area building density	1	TEB variable
λ_{tree}	Plan area tree density	1	TEB variable
T_{agg}	Aggregated skin surface temperature of roof, wall, ground	K	Eq. 6
T_{air}	Temperature of the clear-air region	K	Interpolated from TEB SBL levels
$T_{\mathrm{air,veg}}$	Air temperature of the vegetation region	K	Equal to T_{air}
$T_{\mathrm{surf,tree}}$	Skin surface temperature of the leaf	K	TEB variable

Table A2. Output parameters of SPARTACUS-Urban used by TEB.

Symbol	Parameter	Unit	Destination
$\alpha_{\text{town,diff,sw}}$	Diffuse solar albedo of city	1	Coupling with atmospheric model
$\alpha_{\text{town,dir,sw}}$	Direct solar albedo of city	1	Coupling with atmospheric model
$\text{frac}_{\text{gr,sunlit}}$	Fraction of sunlit ground	1	Diagnostic for human thermal comfort quantification
LW_{abs}	Terrestrial radiation absorbed by urban facet	Wm^{-2}	TEB prognostic equation of facet temperature
$\text{LW}_{\text{down,gr}}$	Downwelling terrestrial radiation at ground level	Wm^{-2}	Calculation of MRT (Eq. 12)
$\text{LW}_{\text{hor,diff,gr}}$	Terrestrial radiation at ground level on vertical plane	Wm^{-2}	Calculation of MRT (Eq. 12)
LW_{inc}	Terrestrial radiation incident on urban facet	Wm^{-2}	TEB prognostic equation of facet temperature
$\text{LW}_{\text{up,gr}}$	Upwelling terrestrial radiation at ground level	Wm^{-2}	Calculation of MRT (Eq. 12)
SW_{abs}	Solar radiation absorbed by urban facet	Wm^{-2}	TEB prognostic equations of facet temperature
$\text{SW}_{\text{down,diff,gr}}$	Downwelling diffuse solar radiation at ground level	Wm^{-2}	Calculation of MRT (Eq. 12)
$\text{SW}_{\text{down,dir,gr}}$	Downwelling direct solar radiation at ground level	Wm^{-2}	Calculation of MRT (Eq. 14)
$\text{SW}_{\text{hor,diff,gr}}$	Diffuse solar radiation at ground level on vertical plane	Wm^{-2}	Calculation of MRT (Eq. 12)
SW_{inc}	Solar radiation incident on urban facet	Wm^{-2}	TEB prognostic equation of facet temperature
$\text{SW}_{\text{up,diff,gr}}$	Upwelling diffuse solar radiation at ground level	Wm^{-2}	Calculation of MRT (Eq. 12)

Appendix B: Results for direct-only downwelling solar radiation without trees

The follwing figures display the solar radiation budget for all urban morphologies with flat roofs and direct downwelling solar radiation.

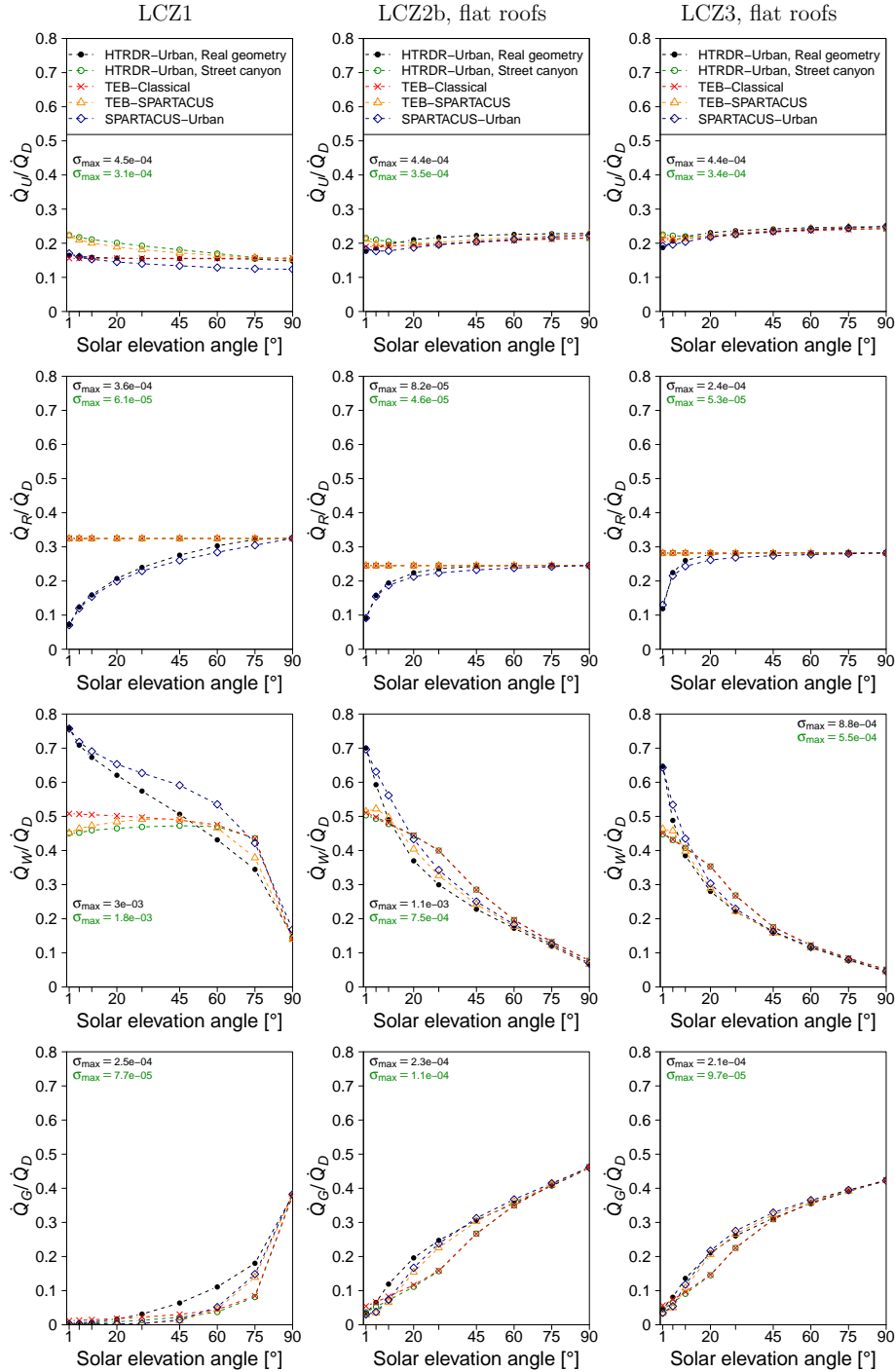



Figure B1. Fraction of the downwelling direct solar radiation ($\dot{Q}_D$) that is reflected by the city ($\dot{Q}_U$), absorbed by the roofs ($\dot{Q}_R$), the walls ($\dot{Q}_W$), or the ground ($\dot{Q}_G$) simulated by the reference model Monte-Carlo model HTRDR-Urban, the urban radiation scheme SPARTACUS-Urban, and the urban canopy model TEB with the Classical and the SPARTACUS-Urban radiation scheme. The values of σ_{max} indicate the maximum value of the standard deviation of the radiative observable obtained from the Monte-Carlo simulations for all values of solar elevation angle.

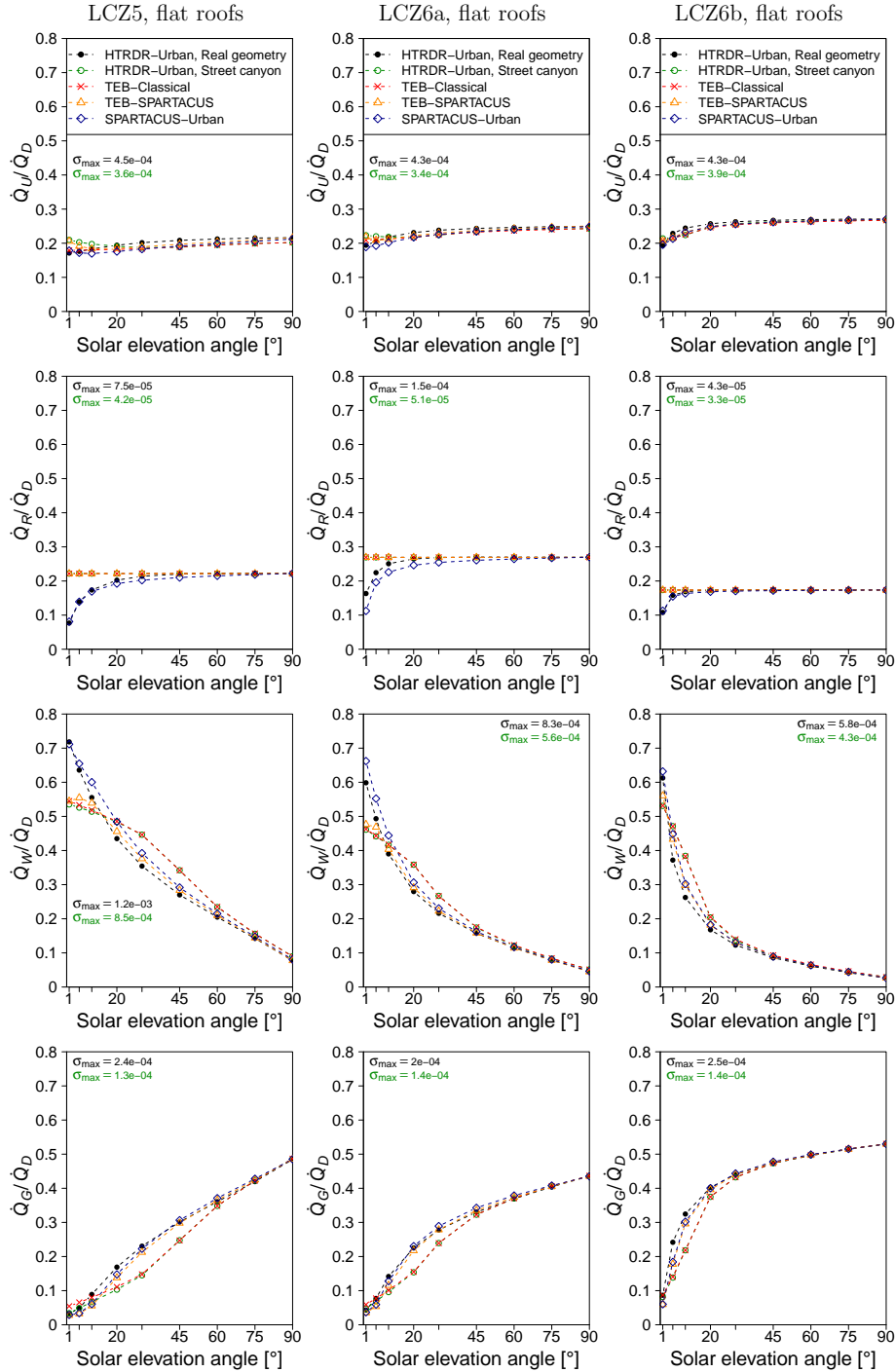



Figure B2. Fraction of the downwelling direct solar radiation ($\dot{Q}_D$) that is reflected by the city ($\dot{Q}_U$), absorbed by the roofs ($\dot{Q}_R$), the walls ($\dot{Q}_W$), or the ground ($\dot{Q}_G$) simulated by the reference model Monte-Carlo model HTRDR-Urban, the urban radiation model SPARTACUS-Urban, and the urban canopy model TEB with the Classical and the SPARTACUS-Urban radiation scheme. The values of σ_{max} indicate the maximum value of the standard deviation of the radiative observable obtained from the Monte-Carlo simulations for all values of solar elevation angle.

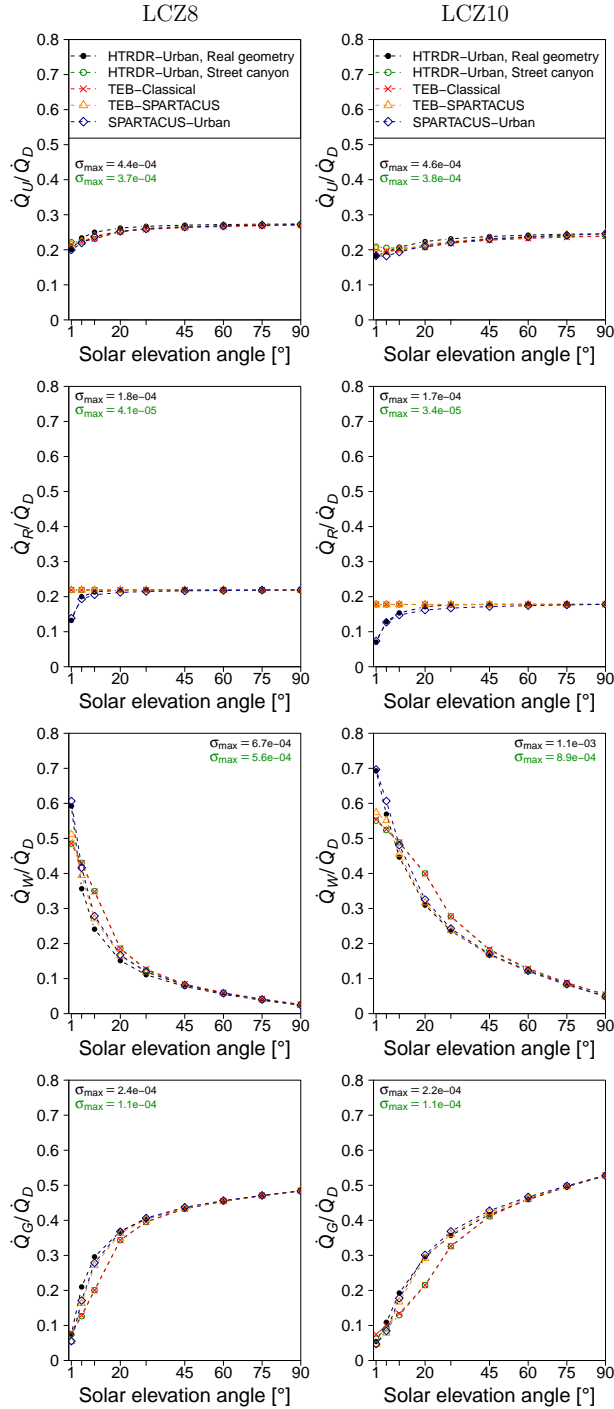



Figure B3. Fraction of the downwelling direct solar radiation ($\dot{Q}_D$) that is reflected by the city ($\dot{Q}_U$), absorbed by the roofs ($\dot{Q}_R$), the walls ($\dot{Q}_W$), or the ground ($\dot{Q}_G$) simulated by the reference model Monte-Carlo model HTRDR-Urban, the urban radiation model SPARTACUS-Urban, and the urban canopy model TEB with the Classical and the SPARTACUS-Urban radiation scheme. The values of $\sigma_{\max}$ indicate the maximum value of the standard deviation of the radiative observable obtained from the Monte-Carlo simulations for all values of solar elevation angle.

Appendix C: Results for direct-only downwelling solar radiation with trees

590   The follwing figure displays the solar radiation budget for the LCZ2a and LCZ4 morphologies with trees and direct down-welling solar radiation.

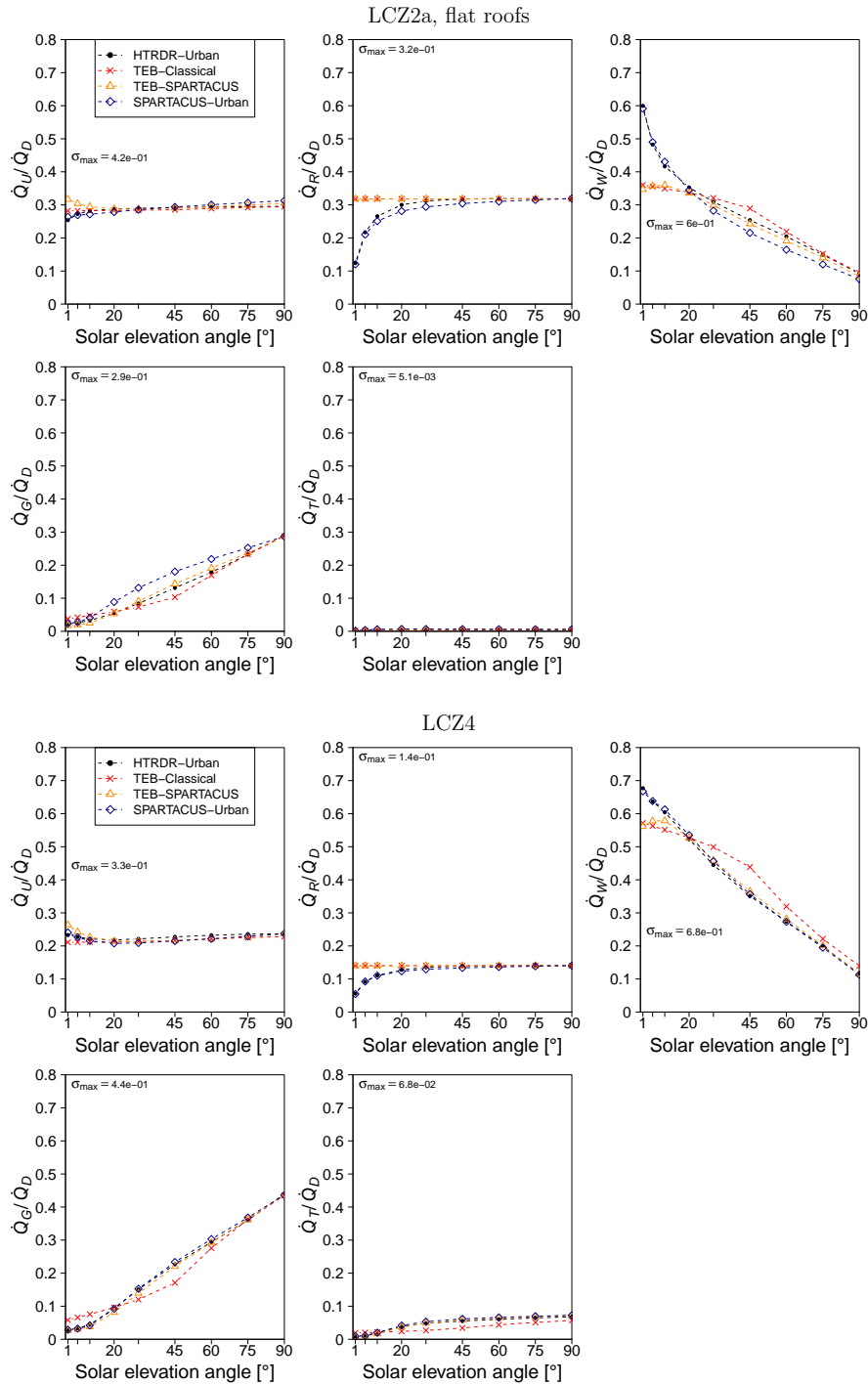



Figure C1. Fraction of the downwelling direct solar radiation ($\dot{Q}_D$) that is reflected by the city ($\dot{Q}_U$), absorbed by the roofs ($\dot{Q}_R$), the walls ($\dot{Q}_W$), the ground ($\dot{Q}_G$), or the urban trees ($\dot{Q}_T$) simulated by the reference model Monte-Carlo model HTRDR-Urban, the urban radiation model SPARTACUS-Urban, and the urban canopy model TEB with the Classical and the SPARTACUS-Urban radiation scheme. The values of $\sigma_{\max}$ indicate the maximum value of the standard deviation of the radiative observable obtained from the Monte-Carlo simulations for all values of solar elevation angle.

Author contributions. Robert Schoetter did the TEB and SPARTACUS-Urban coupling, the execution and analysis of the HTRDR-Urban reference simulations, and the majority of the writing. Robin Hogan prepared SPARTACUS-Urban for its coupling with TEB, provided guidance on the use of Monte-Carlo reference simulations for radiative transfer, and supervised the TEB-SPARTACUS validation. Cyril Caliot lead the HTRDR-Urban reference model development and supervised the TEB-SPARTACUS validation. Valéry Masson supervised the TEB-SPARTACUS coupling. All co-authors have read the entire manuscript and helped to improve the original draft.

Competing interests. The authors declare no competing interests

Acknowledgements. Simone Kotthaus is acknowledged for sharing the Spectral Library of Impervious Urban Materials, and Vincent Eymet for his help with the creation of the optical properties files. This work received financial support from the French Agency for Ecological Transition ADEME (project MODRADURB-1917C001) and from the French National Research Agency through Grant ANR-21-CE46-0013.

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