

Author's response to Anonymous Referee 1 Comment 1

June 27, 2023

1 General Comment

[I think that this manuscript has the potential to be a useful contribution to the (slowly) growing body of literature on the relationship between thermodynamics and sliding. However, I think that this manuscript needs quite a bit of work to be publishable. My criticism is not generally aimed at the science, but rather at the presentation which reads more like a set of internal notes than a manuscript. In particular the organization does not proceed in a logical manner, and I struggle to find a narrative that relates adjacent sections. In addition, the manuscript includes difficult-to-remember jargon and sometimes dubious interpretations of referenced material. There are far too many tables; it is very difficult to make sense of tabular numbers appearing in columns that reference one of many difficult to differentiate experiments. Perhaps most critically, some of the most important figures - many of which are referenced frequently and are essential to the paper's conclusions - are relegated to supplemental material or appear in one of the authors' previous papers. I do not suggest any new experiments or analysis here. However, I do suggest that the authors revise this manuscript with a keen eye for the fact that it will, ultimately and hopefully, be read by others.]

We thank the referee for their constructive comments. We have addressed all the referee's comments and revised the text accordingly. A point-by-point reply is reported below, with referee comments in orange (line references refer to the old manuscript version) and our replies in black.

We agree that the readability of the paper benefits from a general restructuring and focusing on the key takeaways (Numerical Model Error Estimates (MNEEs) must be considered when numerically modeling ice stream surge cycles, surge characteristics are sensitive to the basal sliding activation criterion, resolution dependency can be reduced by incorporating a resolution-dependent basal sliding activation criterion). To streamline the paper, we grouped the 11 research questions into three main themes: 1) determine the 'MNEEs' as a metric to determine the significance of a change in model configuration (note that we use the MNEEs because we are not able to determine the model error; we provide more details on this issue in our replies below), 2) using the MNEEs, determine the sensitivity of the surge characteristics (number of surges, mean surge periodicity, mean surge duration, and mean ice volume change during a surge) to model aspects with a physical relevance (particular focus on the basal sliding activation criterion), and 3) perform a convergence study based on the results of 1) and 2). We also added a short paragraph describing the narrative of the sensitivity experiments in 2) (see our reply to comment *Sec 1.1* below).

Additionally, we replaced most of the tables in the results section with the two new figures 6 and 7. These figures summarise the sensitivities of the surge characteristics of all model components with a significant effect in a concise way. In terms of model components analyzed, we are now focusing only on model components that have significant effects on the surge characteristics in order to reduce the burden on the reader, as suggested by the reviewer. Additional model components that we showed to have no influence were moved to the supplement and are only briefly summarized in the main manuscript. Figure S18 showing the definition of the surge

characteristics (previously situated in the supplement) has been moved to the main manuscript (Figure 3).

Where possible, we changed the jargon to phrases that are easier to interpret and remember (e.g., 'numerical noise estimates' to 'Numerical Model Error Estimates (MNEEs)', 'base setup' to 'reference setup', 'event'/'surge event' to 'surge', 'event characteristics' to 'surge characteristics').

We reworked the summary and conclusions section to remove the dubious interpretations of referenced material and give a more extensive and accurate comparison to the existing literature (e.g., added comparison to the EISMINT temperature spokes).

2 Detailed comments

[Title - The title should be shortened to something like 'Numerical issues in modeling binge-purge behavior in ice streams.' No other instabilities are addressed and 'binge-purge', 'cyclic', and 'surging' are all redundant.] In order to streamline the title, we changed it from: *Numerical issues in modeling ice sheet instabilities such as binge-purge type cyclic ice stream surging*

to: *Numerical issues in modeling thermally and hydraulically driven ice stream surge cycling.*

We kept the term 'surge cycling' because 'surging' alone could also refer to just a single surge, and the analysis of multiple surges per run is a key aspect of this study.

[L1 - Delete 'as in any environmental system'.] Agree and done.

[L20 - I think it is strange to lead with validation as a means of motivating the current manuscript, when no validation occurs here. Validation is not the same as sensitivity testing.]

This part was indeed misleading and we change it from: *The use of Ice Sheet Models (ISMs) has grown at least an order of magnitude over the last two decades. The relevance of such modeling studies to the actual physical system can be unclear without careful consideration and testing of numerical components and implementations. Model validation is particularly important when modeling highly non-linear ice sheet instabilities, for which it is hard to distinguish between numerical noise and physical phenomena. In addition, there are a number of numerical choices, such as for thermal activation of basal sliding, for which no model to date has documented sensitivities.*

to: *The use of Ice Sheet Models has grown at least an order of magnitude over the last two decades. The relevance of such modeling studies to the actual physical system can be unclear without careful consideration and testing of numerical aspects and implementations. This is especially true when modeling the highly non-linear ice sheet surge instability, which has significant implications not only for the ice sheet itself but also for the climate. In fact, it is often difficult to assess whether model results are physically significant (effects of physical system processes), a consequence of model-specific numerical choices, or a combination of both. This is especially important in the case of abrupt changes. Whether ice sheet instabilities observed in numerical simulations are the result of physical instabilities of the underlying continuum models or spurious effects of the discretization and numerical implementation of said models has long been debated [e.g., Payne et al., 2000, Hindmarsh, 2009] and is a consequential matter. The present study is concerned with characterizing the impact of model physics, numerical choices, and numerical errors on ice stream surge cycling.*

[...]

As a result of the involved physics and expected behaviors, modeling of ice stream surge cycling is challenging. The challenges entail, among others, rapid surge onset, high ice velocities, and non-linear (thermo-viscous, hydraulic, and thermo-frictional) feedbacks. In addition to the physical complexity, further challenges arise in the numerical modeling of ice stream surge cycling, whether in terms of model choices (e.g., choice of mechanical model, thermal modeling of the substrate, accounting for sub-glacial hydrology) and/or in terms of their numerical implementation (e.g., grid and time step size, convergence under grid refinement, etc.).

Our focus here is on the challenges arising from numerical modeling, both those related to the modeling choices and those related to the implementation. Numerical challenges have received limited attention in studies examining ice sheet surging. The few studies to date that do examine numerical aspects of surge cycling suggest strong sensitivities in model response to implementation choices such as grid size [e.g., Calov et al., 2010, Roberts et al., 2016, Ziemen et al., 2019]. However, the effects of different approximations of the Stokes equations have been previously addressed [e.g., Brinkerhoff and Johnson, 2015], and are therefore not discussed here.

[...]

In terms of different numerical choices, the impact on model results is usually determined by calculating the model error to the exact analytical solution. However, the theory behind the surge instability is not fully developed (no analytical solution exists), especially in the context of a spatially extended 3D system, thus precluding systematic benchmarking of numerical models.

To overcome this issue and provide at least a minimum estimate of the numerical model error, we first determine 'Minimum Numerical Error Estimates' (MNEEs). This is a new metric that aims to minimally resolve whether a change in surge characteristics due to changes in the model configuration is significant (see Sec. 2.3 for details).

The corresponding part in Sec. 2.3 states: We compute the new 'Minimum Numerical Error Estimates' (MNEEs) metric by examining the model response to changes in the model configuration that are not part of the physical system. The MNEEs are defined as the percentage differences in surge characteristics when applying a stricter (than default) numerical convergence in the GSM and adjusting the matrix solver used in PISM (changing the number of processor cores used). They are then used as a threshold to determine if model sensitivities to changes in the model configuration that affect the physical system (e.g., the inclusion of a bed thermal model or sliding dependence on effective pressure from basal hydrology) are above the level of background noise induced by iterative numerical solvers in the model. We refrain from drawing conclusions about the effects of a change in model configuration with physical relevance when the model sensitivities in question are smaller than the MNEEs. In these cases, the actual physical response of the model might be hidden within the numerics.

While the MNEEs are useful to our purpose, we wish to emphasize that they can not replace proper model verification and validation and are missing uncertainties due to, e.g., different approximations of the Stokes equations and other physical processes not included in the models. Nonetheless, they provide a minimum estimate of the numerical model error, which is still a significant improvement over ignoring this issue entirely.

[L26 - What is 'numerical noise'? Something random? Pseudo-randomness in a chaotic system? Numerical error? This is a critical consideration but it's not really clear what it means in this paper here and elsewhere.] We agree that the concept of 'numerical noise' needed clarification. We changed the term 'numerical noise estimates' to 'Numerical Model Error Estimates (MNEEs)'. Refer to our answer to comment L20 - I think it is strange to lead with validation as a means of motivating the current manuscript, when no validation occurs here. Validation is not the same as sensitivity testing. for the details that have been added to the revised draft.

[L38 - Define 'meaningful'] 'Meaningful' in the sense of 'physically meaningful', i.e., that the modeled surges are not just due to numerical instabilities. However, the sentence works just fine without this phrase, and we, therefore, chose to remove it for clarity.

[L44 - The quote from Soucek and Martinec is relevant, but it misses the fact that there are a great many approximations that appear in, for example, the solution of the Stokes' equations. Why the emphasis on numerical rather than model error?] We agree that one is ultimately interested in the model rather than the numerical error. However, the analytical solution for the here used 3D thermo-mechanically coupled models with hybrid SIA/SSA ice dynamics is not fully developed, and it is not the goal of this study to progress the theory. Note that this is also the case for other ice sheet models with different approximations, e.g., BISICLES (sliding everywhere, minimal heat treatment at the bed (just a vertical flux, which in temperate regions

produces water)) or ELMER ice (too expensive for ensembles needed). Therefore, the model error cannot be determined in this context.

To provide at least some uncertainty estimates, we determine the MNEEs in the models by changing purely numerical model components (no physical relevance). Additionally, uncertainties associated with the numerical aspects of a model have received limited attention (compared to the effect of different approaches to the Stokes equations).

See also our answer to comment *L20 - I think it is strange to lead with validation as a means of motivating the current manuscript, when no validation occurs here. Validation is not the same as sensitivity testing.* for a revised version of this paragraph. Note that the quote from Souček and Martinec [2011] is now situated later in the text.

[L60–72 - While I recognize that this paper focuses on the ISMIP-HEINO setup, it would be worthwhile to try to contextualize this work with respect to the EISMINT-F experiments as well. There is a great deal of insight there regarding thermal sliding instabilities and the circumstances under which they appear.] The EISMINT-F experiment has an air temperature 15 K cooler than the reference experiment A but otherwise the same boundary conditions. Due to this colder air temperature, almost all examined models show cold ice spokes in the basal temperature fields extending into the melt zone. These spokes break the radial symmetry of the model results. While the effects are most pronounced in the temperature fields, the spoked pattern also exists in the ice velocity, flow factor, and ice thickness fields.

Our work is similar in that we use a comparable experimental design with respect to the boundary conditions, especially for the PISM experiments, but different because of the sediment distribution and the ice dynamics used in the models (SIA in EISMINT vs. hybrid SIA/SSA here). Bueler et al. [2007] show that when the derivative of the strain-heating term to the temperature field is horizontally smoothed, the spokes can be eliminated. They also discuss the possibility that the inclusion of membrane stresses provides a physical mechanism for this smoothing. Additionally, Bueler and Brown [2009] hypothesize that the spokes occurring in EISMINT experiment H (basal slip where the basal ice is at the melting point vs. no basal slip in Experiment A and F), are caused by a velocity discontinuity introduced by traditional SIA sliding laws.

While it is true that there is a lot that can be learned from the EISMINT-F and H experiments, we do not see basal temperature spokes in our experiments. Nevertheless, this is an interesting comparison, and we added the following paragraph to the conclusions: *Basal temperature spokes, such as the ones modeled in the EISMINT-F and H experiments [Payne et al., 2000], are not apparent in the PISM experiments. The GSM runs show some warm-based areas at the margins interspersed by colder regions, but this is likely due to a steep surface slope leading to a large driving stress, high velocity, and then consequently, a basal temperature increase. Therefore, neither the PISM nor GSM instabilities discussed here are comparable to the EISMINT temperature spokes. The absence of basal temperature spokes is likely due to the inclusion of membrane stresses in the ice dynamics of both models [Bueler et al., 2007, Bueler and Brown, 2009].*

[Sec 1.1 - I find the organization of the paper according to research question to be quite challenging to follow, perhaps mostly because there are so many (11) research questions. I think it would be better to group these into open questions rather than yes/no, and this might make for more comprehensible themes. For example, Q1,11 could be grouped as ‘what aspects of simulated surges are due to numerical considerations?’, while Q2–6,9 could be grouped as ‘what modeling and solution choices influence surging?’ and Q7,8,10 as ‘what parameterizations of basal physics leads to the most robust conclusions?’ or something similar.] We agree that the manuscript needed some restructuring to make it more accessible for the reader. To increase the readability, we grouped the individual research questions into the following main themes: 1) MNEEs (Q1), 2) sensitivity experiments with (previous Q2, Q3, Q4, Q5, Q7, Q8; now Q2, Q3, Q5, Q6, Q7, Q8) and without a significant effect on the results (previous Q6, Q9, Q10; now Q4, Q9, Q10), and 3) convergence study (Q11). As suggested by the second reviewer,

the sensitivity experiments without a significant effect will be only briefly summarised, with the details moved to the supplement. Since the results of the convergence study depend on previous experiments, this aspect is discussed last.

Within the above mentioned 3 main themes, and counter to the request of the reviewer, we decided to keep the specific research questions, but added the following paragraph to better link the different research questions within the sensitivity experiment section: *Here we aim to determine the significance of different model configurations on the surge characteristics. We are particularly interested in model configurations affecting the basal temperature and thus the surge behavior. Therefore, we first discuss the change in surge characteristics due to a bed thermal model (Q_2) and modeling choices affecting the basal temperature at the grid cell interface where the ice velocities are calculated (Q_3 and Q_4), including the basal sliding thermal activation criterion (Q_5). Previous studies examining the effects of ice stream behavior are often based on an idealized basal topography and sediment distribution and do not consider sub-glacial hydrology [e.g., Calov et al., 2010, Brinkerhoff and Johnson, 2015]. Therefore, we determine the change in surge characteristics due to these aspects in Q_6 , Q_7 , Q_8 , and Q_9 , respectively. Since thermally and hydraulically driven ice stream surges are not exclusive, we also investigate the differences between the two mechanisms when used as the primary smoothing mechanism at the warm/cold-based transition zone (Q_{10}).*

We believe that this organization allows the reader to jump right to the parts they are most interested in, now without detracting from the readability of the manuscript. Anyways, should the Referee find that our preferred paper organization is still challenging to follow, we are open to eliminating the research question structure altogether.

[L166 and elsewhere - I don't find it helpful to reference a manuscript that is 'in preparation' because such manuscripts are not readable and sometimes fail to ever get published. Is there some source code that could be referenced instead? An instruction manual? An older manuscript from which the ideas in the in prep manuscript are adapted?] We agree that referencing a manuscript 'in preparation' is not ideal. We hoped this manuscript would be available as a preprint by now, which is not the case. Therefore, we removed this reference.

The source code of the model version used in this manuscript can be found in the supplementary material [Tarasov et al., 2023] as stated in the Code and data availability section. Additionally, we have added this reference to the GSM description section. Older manuscripts on which the current GSM version is based on are also mentioned in this section [e.g., Pollard and DeConto, 2012, Tarasov et al., 2012, Bahadory and Tarasov, 2018].

[L198 - I am deeply skeptical of a model that 'activates' stress terms based on a heuristic that in turn depends on whether the bed is soft or hard (whatever that means). Does it not seem that such an obviously non-physical choice could lead to just as much variability in surging behavior as any of these other mechanisms? Validation is mentioned in the introduction, but what about verification? How does the reader know (especially given that there is no current reference to the model description) that this model converges to the true solution of some physically and mathematically justified system of equations under discretization refinement?] Thanks for raising this point. First of all, there was a mistake in the GSM description. The model version used within this paper does not differentiate between soft (100 % sediment cover) and hard (0 % sediment cover) beds for the SSA activation criteria. However, different SSA activation criteria are available in the GSM and we add a table showing the model sensitivity to this choice to the revised supplement, including a model setup with active SSA everywhere (Sec. S1.2).

The reference to the hybrid SIA/SSA ice dynamics of the GSM is [Pollard and DeConto, 2012]. See also our answer to comment L20 - *I think it is strange to lead with validation as a means of motivating the current manuscript, when no validation occurs here. Validation is not the same as sensitivity testing.* for a discussion about the difficulties regarding model verification and validation.

[L215 - I don't know what 'legacy' means here.] Changed to 'values used in previous GSM

modeling studies [e.g., Bahadory and Tarasov, 2018]’.

[Eq. 5 - Is this supposed to be $F_{T_{ramp}}$? Otherwise F_{warm} is defined twice. Also, I think it’s really awkward (ignoring subscripts) to have F depend on T, which depends on a different F. Maybe consider different notation?] We compare our definition of F_{warm} to the one used by Fowler [1986], Mantelli et al. [2019], so F_{warm} is correct here. To make this clearer, we changed: *A temperature ramp similar to the one suggested by Fowler [1986] and later Mantelli et al. [2019] [...]*

to: *For comparison, a temperature ramp similar to the one suggested by Fowler [1986] and later Mantelli et al. [2019] [...]*

We agree that the previous notation was confusing and replaced $F_{T_{ramp}}$ by $P_{T_{ramp}}$.

[Sec. 2.1.2 - I generally find the phrase ‘vector’ to be unhelpful here. I think it would be better to describe how the ensemble is created (i.e. by selecting different values for each of eight parameters) and then referring to different members of the ensemble as, well, ‘ensemble members’.] For precision/accuracy and lack of alternatives, we prefer to stick to the phrase ‘parameter vector’. Note that a parameter vector and ensemble member are not the same (e.g., multiple ensemble members can have the same parameter vector).

[Sec. 2.1.2 - It takes quite a bit of flipping around to understand why we’re talking about ensembles at all. I think this section could use a clear explanation of the fact that you’re running each subsequent experiment with multiple different parameter settings.] Note that the benefits of an ensemble are explained earlier in the text: *‘To partly address potential non-linear dependencies of surge cycling on model parameters, we use a high variance subset of 5 base GSM parameter vectors (each comprising 8 model input parameters) for our numerical experiments’.*

To make it clearer that each experiment is run with all parameter vectors, we updated this part to: *‘In order to partly address potential non-linear dependencies of surge cycling on model parameters, we run each of our numerical experiments with a high variance ensemble of 5 GSM parameter vectors (each comprising 8 model input parameters) and 9 PISM parameter vectors (each comprising 6 model input parameters).’*

We have also added the following sentence as an introduction to section 2.1.2: *‘Each GSM experiment is run with an ensemble based on 5 input parameter vectors.’* Furthermore, we added *‘Each PISM experiment is run with an ensemble based on these 9 input parameter vectors.’* to section 2.2.2.

[Sec. 2.1.3 I think that ‘reference simulation’ might be more clear than ‘base setup’.] We agree that the word ‘reference’ is easier to interpret than ‘base’. However, a ‘reference simulation’ and ‘base setup’ are not the same thing. In this study, there are 5 reference simulations (one for each parameter vector) but only one base setup. To avoid potential confusion, we are now using ‘reference setup’.

[Sec. 2.1.3 - I think that the very frequent referencing to future sections is not very helpful.] The forward referencing was meant to guide the reader and allow them to skip sections they are not interested in. However, this is better suited at the end of the introduction and was removed here.

[Sec. 2.1.3 and elsewhere - There are far too many references to supplementary information in this manuscript. SI is intended for things that either cannot appear in the manuscript itself due to medium (e.g. code or videos) or that offer additional insight or detail into some aspect of the work but that is not essential to the results. In this case, the mass balance forcing (the single most important thing in determining long term ice sheet extent) is relegated to the supplement, but really should be in the main text.] We agree that the climate forcing is an important detail and changed the text from: *‘The GSM is run with an idealized down-scaled North American geometry (Fig. 1, modified after the ISMIP-HEINO setup [Calov and Greve, 2006]) and simplified climate representation. The temperature forcing is defined by a domain wide surface temperature (rT_{north} , Tab. 1) and a specified vertical temperature gradient (atmospheric lapse rate (lapsr in Tab. 1)). The surface temperature forcing is asymmetric in time (Fig. S1), enabling the analysis of the timing of cycling onset and termination under*

different physical and numerical conditions (a comparison of ice stream ice volume evolution under constant and asymmetric temperature forcing is shown in Fig. S2 for one parameter vector).

to: The GSM is run with an idealized down-scaled North American geometry (Fig. 1, modified after the ISMIP-HEINO setup [Calov and Greve, 2006]) and simplified climate representation. The surface temperature forcing in the GSM is given by

$$T_{\text{surf}} = rT_{\text{surf}} + \text{lapsr} \cdot H + T_{\text{asym}}, \quad (1)$$

where rT_{surf} and lapsr are input parameters for the domain-wide surface temperature constant and atmospheric lapse rate, respectively (Table 1), H the ice sheet thickness, and T_{asym} the asymmetric (in time) temperature forcing (maximum difference of 10°C , orange line in Fig. S1) calculated according to

$$T_{\text{asym}} = \left| \left(\frac{t}{200 \text{ kyr}} \cdot 3 + 2 \right) - 1 \right| \cdot 5^\circ\text{C}, \quad (2)$$

where t is the model time ranging from -200 kyr to 0 kyr (instead of 0 kyr to 200 kyr). The asymmetric temperature forcing enables the analysis of the timing of cycling onset and termination under different physical and numerical conditions (a comparison of ice stream ice volume evolution under constant and asymmetric temperature forcing is shown in Fig. S2 for one parameter vector).

The surface mass balance forcing is then determined by

$$M_{\text{tot}} = M_{\text{acc}} - M_{\text{melt}}, \quad (3)$$

where M_{acc} and M_{melt} are the surface accumulation and melt, respectively. The surface accumulation is defined by

$$M_{\text{acc}} = \text{precRef} \cdot \exp(\text{hpre} \cdot T_{\text{surf}}), \quad (4)$$

where precRef and hpre are the precipitation coefficient input parameters. Surface melt is calculated according to a Positive Degree Day (PDD) approach:

$$M_{\text{melt}} = r\text{PDDmelt} \cdot \max(0.0, \text{POSdays} \cdot (T_{\text{surf}} + 10.0^\circ\text{C})), \quad (5)$$

where $r\text{PDDmelt}$ is the input parameter for melt per PDD and the PDD constant POSdays is set to 100 days yr^{-1} . Note that we set $T_{\text{surf}} = 0.1^\circ\text{C}$ and $M_{\text{tot}} = -100 \text{ m yr}^{-1}$ for ocean grid cells, and $T_{\text{surf}} = 0.1^\circ\text{C}$ and $M_{\text{tot}} = -200 \text{ m yr}^{-1}$ at the boundaries of the model domain.

However, Fig. S1 only shows the asymmetric aspect of the temperature forcing (atmospheric lapse rate and parameter vector dependency are not considered). Due to the simplicity of the plot, we do not deem it important enough to be in the main manuscript.

Generally speaking, we moved information to the supplement when we suspected most readers would not be interested in reading about it. In all of these cases, we added a reference to the corresponding part in the supplement to ensure the reader is aware that additional information is available and where to find it. Where possible, we replaced the references to the supplement with references to the two new Fig. 6 and 7.

However, the information in the supplement is not essential to understanding the paper. Following this logic, we prefer to keep the remaining references to the supplement.

[2.2.1 - It's strange to imply that PISM is not also optimized for computational speed. It's the parallel ice sheet model, after all.] Thanks for bringing this up. It was not the intent of this statement to imply that PISM is not optimized. While both models are optimized, the optimizations are not for the same contexts. The idea behind using two different models is to minimize the possibility that drawn conclusions are solely a result of the used optimization schemes. Furthermore, the GSM is optimized for computational resource use to enable large ensembles over paleo timescales and therefore not parallelized (not the case for PISM).

To make this clearer, we have adjusted: *'The GSM is an ice sheet model developed specifically for glacial cycle ensemble modeling. The GSM is therefore numerically optimized for computational speed.'*

to: *'In contrast to the GSM, the Parallel Ice Sheet Model (PISM) is not specifically developed for glacial cycle ensemble modeling. Therefore, the two models use distinct sets of numerical optimizations for computational speed.'*

[L303–310 - I think it would be helpful not to mix units of measurement (m/a and m/d). What is a 'stable solution of the numerical matrix solver' ? Is 'observed range' the heuristic from Cuffey and Paterson?] Agree and done.

Given the varying meanings of 'stable', we removed *'[...], indicating a stable solution of the numerical matrix solver even for runs with very high velocities.'*

Yes, the corresponding part in K.M. Cuffey and W.S.B. Paterson. [2010] is: *'Speeds and displacements also vary widely. High velocities are about 100 m/day for short periods, and 5 km/yr maintained for one or two years. Low velocities are only several tens to a few hundred meters per year, values typical of many nonsurging glaciers'*. However, we now use the more appropriate comparison to Jakobshavn Isbræ: *For comparison, observed outlet glacier velocities at Jakobshavn Isbræ (Greenland) approach 20 km yr⁻¹ [Joughin et al., 2012, 2014].*

The paragraph: *Excluding runs that show maximum sliding velocities > 50 km yr⁻¹ from the analysis yields similar results to the full 10-member ensemble (Sec. S6 and Fig. S10), indicating a stable solution of the numerical matrix solver even for runs with very high velocities. In addition, the 50 km yr⁻¹ is exceeded no more than 7 times per 200 kyr run (100 yr output) and the maximum sliding velocities are generally within the observed range (Fig. S10).* was removed from the revised draft because we now impose a maximum sliding velocity of 40 km/yr for all PISM runs (same as for the GSM). The analysis for higher velocities is, therefore, no longer needed.

[L318 - 'event' and 'HE' seem to be used interchangeably in the manuscript. I think it would be better to just use 'HE'.] They are not interchangeably. The term HE should be exclusively used when referring (to at least some extent) to the ocean sediment records/IRD layers. The abbreviation 'HE' and most instances of the term 'Heinrich Event' were removed. The term 'event' was replaced by the more precise term 'surge'.

[L330 - This is another circumstance where including the supplemental figure in the main manuscript would be very helpful.] Agree and done.

[L341–342 'ice-free when no surge occurs.' I'm not sure it's possible to ascribe a date to when something doesn't happen.] Agreed. We changed: *'a large fraction of the pseudo-Hudson Strait area is ice-free when no surge occurs'*

to: *'a large fraction of the pseudo-Hudson Strait area is only ice-covered when a surge occurs'*

[3.1.1 What about PISM? Can surges be understood similarly to those in GSM?] This was indeed missing from the manuscript and will help the reader to better understand later sections. We added a plot and the following short description of the PISM surges to the revised draft (Sec. 3.1.1 and Fig. 5): *Surges in the PISM originate at the ice sheet margin in the soft-bedded pseudo-Hudson Strait (exact position varies between runs) and propagate towards the center of the pseudo-Hudson Bay ($x = 1300$ km, $y = 1500$ km, Fig. S8 and 5). The ice near the margin is already flowing downstream before the start of the surge ($t = 89.36$ kyr). However, the basal temperature is below the pressure melting point, and the ice velocities are low (< 100 m yr⁻¹). As the ice sheet upstream of the margin thickens, the warm-based area extends further downstream, particularly along the 100 % soft-bedded contour line (magenta line in Fig. 5). Once the warm-based area connects with the margin ($t = 89.42$ kyr), the ice velocities increase beyond 100 m yr⁻¹, activating the SSA (Sec. 2.2.1). Similar to the surges in the GSM, the sliding velocities then increase rapidly, quickly extending the warm-based area ($t = 89.43$ kyr and $t = 89.433$ kyr). The surge propagates upstream into the pseudo-Hudson Bay and the ice is transported along the pseudo-Hudson Strait into regions with increasingly negative surface mass balance rates ($t = 89.435$ kyr to $t = 89.45$ kyr, Fig. S7). The ice sheet*

thins, the basal temperature at the margin falls below the pressure melting point, blocking parts of the upstream ice stream, and the surge ceases at $t = 89.47$ kyr (~ 100 yr surge duration). The ice volume in the surge-affected area continues to decrease for, on average, another 2.5 kyr due to the large amounts of ice in the negative surface mass balance regions. In contrast to the GSM, the PISM results remain symmetrical about $y = 1500$ km throughout the surge.

[3.1.2 - I'm not sure it's reasonable to try to state a specific justification for why the time scales of this highly idealized and not-observationally-constrained experiment are dissimilar to geological records: many different factors may be in play here (some improving the fit, some to its detriment) and (as an example) saying that the period mismatch is just the result of domain size seems like its missing a broader set of possibilities.] While it is true that several factors influence the period (e.g., bed thermal model, basal temperature ramp, basal hydrology, ...), the domain size seems to be the controlling one here. Previous experiments with a non-downscaled model domain (but otherwise identical experimental setup) yielded results within the limits of geological records. We changed this part from: *Due to the downscaled GSM domain, the mean modeled GSM period is shorter than the observed period of, on average, 7 kyr [K.M. Cuffey and W.S.B. Paterson., 2010].*

to :*'The mean modeled GSM period is shorter than the observed period of, on average, 7 kyr [K.M. Cuffey and W.S.B. Paterson., 2010]. However, exploratory GSM runs with a dimensionally accurate (not downscaled) model domain (but otherwise identical experimental setup) yielded periods within the range of geological inferences.'*

[3.1.3 - I again struggle with the notion of 'numerical noise'; the paper would be well served by having a much more in-depth description of what is meant by this and where it comes from. With respect to the latter, in most modelling exercises, the numerical error is something that can be well quantified through comparison to exact solutions or by a theoretical analysis of the interpolation properties of numerical method. Yet here, what we're effectively measuring is the system's sensitive dependence to small perturbations. In that sense, it doesn't necessarily follow that stricter convergence criteria (in the case of GSM) would necessarily lead to any less 'noise'. Could an equivalent result be achieved by just adding white noise to the initial conditions?] To avoid repetition, please refer to our reply to comment L20 - *I think it is strange to lead with validation as a means of motivating the current manuscript, when no validation occurs here. Validation is not the same as sensitivity testing.* for a discussion about the difficulties regarding the determination of the model error.

The main idea behind using stricter convergence criteria was not to decrease the overall noise level, especially since we do not know the exact solution and, therefore, can not determine the noise level. Instead, we want to show (by changing purely numerical model components) that small differences in the surge characteristics between different model setups do not necessarily have a physical origin and might just be due to numerical errors. We added the following paragraph to the revised draft: *Note that the goal of these experiments is not necessarily to decrease the model error, especially since we do not know the exact solution and, therefore, can not determine the model error. Instead, we aim to show (by changing purely numerical aspects) what the minimum numerical errors are for each surge characteristic..* Furthermore, we have added *Surge cycling is sensitive to numerical aspects (e.g., numerical solver error).* as an introduction to the MNEE research question.

Model experiments with noise added to the surface temperature are shown in section '3.2.1 Adding surface temperature noise' (3.1.4 in the old manuscript). The differences in surge characteristics are generally smaller than for the experiments with a stricter numerical convergence criterion.

[3.1.5 - This section on implicit coupling is so vague as to be useless. What even is 'implicit coupling' in this context? Is this the same as implicit time stepping, i.e. Backward-Euler?] Implicit coupling (in contrast to the default explicit time step coupling) refers to the coupling between the thermodynamics and ice dynamics part of the model. To make this clearer in the text, we changed: *'The GSM has a default explicit time step coupling between the thermody-*

namics and ice dynamics but also includes an optional implicit coupling scheme'

to: 'As is standard for thermo-mechanically coupled glaciological ice sheet models, the GSM has a default explicit time step coupling between the thermodynamics and ice dynamics but also includes an optional implicit coupling scheme (c.f. Sec. 3.2.2).'

and: 'we test the impact of implicit coupling (via an iterative implementation) between the thermodynamics and ice dynamics'.

to: 'we test the impact of approximate implicit time step coupling via an iteration between the two calculations for each time step.'

[3.2.3 - I can't figure out what TpmTrans, TpmInt, or any other Tpm thing are. If they are described earlier, such a description needs to be here instead or also. If they are not, they need to be defined (and not in the supplement).] Since it is the most concise way, we embedded the equations describing the three approaches (previously in the supplement) into section 3.3.2 (3.2.3 in the old manuscript). Following this suggestion, we have also added the equations for the local basal hydrology to section 3.3.6 (3.2.6 in the old manuscript). Should the Referee find this too detailed, we are open to moving the equations back to the supplement and working on another solution.

[3.2.4 - It's not my preference, but if you prefer to have the actual equations describing GSM in the supplement, I suppose that's fine. However we need at least a little bit of a qualitative description of what these different 'weights' imply. What is the context for understanding why these different choices should yield different surging behaviors?] Due to the restructuring of the paper, this entire section has been moved to the supplement (no significant effect on the surge characteristics, now section S8.1). Although the equations and analysis are in the same document now, we restructured and slightly adjusted this section from: *Here we compare the event characteristics for three different weights when calculating the basal interface temperature in the GSM (Eq. (S5)): no consideration of adjacent minimum basal temperature ($W_{Tb,min} = 0.0$), basal temperature at the interface depends to 50 % on the adjacent minimum basal temperature at the grid cell center (base setup, $W_{Tb,min} = 0.5$), and basal temperature at the interface is equal to the adjacent minimum basal temperature at the grid cell center ($W_{Tb,min} = 1.0$).*

Depending on the location of the adjacent minimum grid cell center basal temperature, either the ice flow (when the adjacent minimum basal temperature is downstream) or upstream propagation of the surge should be affected. For the large-scale surges, the adjacent minimum basal temperature is almost exclusively located upstream (e.g., video 02 of Hank [2023]). Changing the weight, therefore, affects the surge propagation rather than blocking parts of the ice flow.

to: 'Depending on the location of the adjacent minimum grid cell center basal temperature, either the ice flow (when the adjacent minimum basal temperature is downstream) or upstream propagation of the surge should be affected (decreasing basal interface temperature with increasing weight). For the large-scale surges, the adjacent minimum basal temperature is almost exclusively located upstream (e.g., video 02 of Hank [2023]). Changing the weight of the adjacent minimum basal temperature, therefore, affects the surge propagation rather than blocking parts of the ice flow.'

Here we compare the effect of three different weights on the GSM event characteristics (Eq. (S1)): no consideration of adjacent minimum basal temperature ($W_{Tb,min} = 0.0$), basal temperature at the interface depends to 50 % on the adjacent minimum basal temperature at the grid cell center (base setup, $W_{Tb,min} = 0.5$), and basal temperature at the interface is equal to the adjacent minimum basal temperature at the grid cell center ($W_{Tb,min} = 1.0$).'

[Fig. 7 - I honestly can't figure out what this figure is trying to convey. Part of this is that I also can't figure out what the part of the text that references it is trying to convey either (L534-540). Please try to make this a little bit more clear.] Fig. 7 (Fig. 10 in the revised draft) shows the results of the upscaling experiment. The reasoning behind this figure is described in L523-530 (old manuscript): 'We complement the above analysis by upscaling the 3.125 km base runs. For example, a 25x25 km grid cell contains a patch of 64 3.125x3.125 km grid cells. The scatter plot of the warm-based fraction (basal temperature with respect to the pressure melting

point at 0 °C) and the mean basal temperature with respect to the pressure melting point of the patch can be used to estimate the parameters T_{ramp} and T_{exp} of the basal temperature ramp (Eq. (3)). [...] Consequently, this estimate for the basal temperature ramp should be a lower bound to the points in the scatter plot. [...]'. The scatter plot described here is what is shown in Fig. 7. To make this clearer, Fig. 7 is now referenced right after the first 'scatter plot'.

Additionally, we have added: *For example, an upscaled 25 km patch (containing 64 3.125 km grid cells) with 32 3.125 km grid cells at the pressure melting point and 32 3.125 km grid cells at -1°C with respect to the pressure melting point has a warm-based fraction of 50 % and a mean basal temperature of -0.5°C .* to the figure caption.

[3.3 - Brinkerhoff and Johnson, 2015 suggest that the inclusion of membrane stresses leads to convergence under spatial grid refinement, whereas without them, the SIA does not lead to convergence. Can you place those results in the context of this section? Are the relatively weak convergence results here a result of GSM and PISM velocity solvers being insufficiently 'higher-order'?] There is a possibility that the velocity-dependent switch between pure SIA and a membrane stress approximation used in both the GSM and PISM is insufficiently 'higher-order'. To test this, we ran additional GSM resolution scaling experiments with the SSA active everywhere. The differences in surge characteristics between the different resolutions are comparable to the results with the velocity-dependent SSA activation criteria. Therefore, we conclude that the velocity solvers are not the only reason for the strong resolution dependence. We added the following paragraph to the summary section: *Even though the studies are not directly comparable, the results of Brinkerhoff and Johnson [2015] offer some insight relevant to this study. For example, they suggest membrane stresses are necessary for convergence under horizontal grid refinement. The hybrid SIA/SSA ice dynamics used in the GSM and PISM might be insufficiently 'higher-order' and lead to a stronger resolution dependence than the schemes used in Hindmarsh [2009], Brinkerhoff and Johnson [2015]. However, GSM experiments with the SSA active everywhere show a resolution dependence comparable to the velocity-dependent SSA activation criteria (Table S24 and S18, respectively), indicating that the hybrid SIA/SSA ice dynamics are not the sole reason for the strong resolution dependence.*

Note that an analysis of GSM sensitivity to different SIA/SSA switching rules was added to the revised draft (Sec. S1.2).

[Sec. 4 If you maintain these research questions as an organizing principle, I would like to see them revisited as they are resolved by the experiments rather than all at once at the end.] We transformed this section into a 'Results Summary and Discussion' to make it a more standalone section. However, we suspect that not every reader will be interested in every detail of the results section. The new 'Results Summary and Discussion' section provides an easy way to get the most important information and allows the reader to then jump to individual results for more details. Therefore, we would like to answer the research questions in this revised section.

[L738–746 - I think that this section is kind of weird: none of the results presented in this work actually refute the resolution dependency conclusions of Hindmarsh (2009) or Brinkerhoff and Johnson (2015), yet the paragraph is written as if they did. As mentioned before, it seems just as reasonable to assert that those works saw more robust numerical convergence due to the use of more consistent membrane stress resolution schemes rather than because they fortuitously (or nefariously) made parameter choices that suppressed resolution effects.] We agree that this paragraph was confusing. We added it with the intention of providing possible explanations for the different conclusions, not to refute the conclusions of Hindmarsh [2009] or Brinkerhoff and Johnson [2015]. While the fact that different parameter choices can yield very different results remains, we want to clarify that we do not accuse the authors of making parameter choices that suppress resolution effects.

We have updated: *'Event characteristics in both the GSM and PISM show a strong resolution dependence for all sensitivity tests (Table 13+14 and 15). This is in contrast to the findings of other studies examining thermally induced ice streaming Hindmarsh [2009], Brinkerhoff and*

Johnson [2015]. However, both of these studies analyze just one parameter vector, and it is relatively easy to find a parameter vector for which, e.g., the GSM exhibits only a minor resolution dependence. While Hindmarsh [2009] considers sub-temperate sliding, his model allows sliding far below the pressure melting point (order of $\delta = 1$ compared to $\delta = 0.01$ within this study, Eq. (5) and focuses on steady ice streams, not binge-purge-type surges. Over 200 kyr, even minor differences at the beginning of a run can slowly accumulate and yield overall different surge characteristics (e.g., Fig. S31). Furthermore, Brinkerhoff and Johnson [2015] examine ice stream statistics over the whole domain and not a specific soft-bedded region. Neither Hindmarsh [2009] nor Brinkerhoff and Johnson [2015] consider a bed thermal model.’

to: ‘Surge characteristics in both the GSM and PISM show a strong resolution dependence for all sensitivity tests (Table S18+S22 and S25). While other studies examining thermally induced ice streaming do not find a strong resolution dependence [Hindmarsh, 2009, Brinkerhoff and Johnson, 2015], these studies are not directly comparable. The different results are likely due to differences in the experimental design. For example, neither Hindmarsh [2009] nor Brinkerhoff and Johnson [2015] consider a bed thermal model. While Hindmarsh [2009] considers sub-temperate sliding, his model allows sliding far below the pressure melting point (order of $\delta = 1$ compared to $\delta = 0.01$ within this study, Eq. (10)) and focuses on steady ice streams, not ice stream surge cycling. Over 200 kyr, even minor differences at the beginning of a run can slowly accumulate and yield overall different surge characteristics (e.g., Fig. S30). Furthermore, Brinkerhoff and Johnson [2015] examine ice stream statistics over the whole domain and not a specific soft-bedded region. Additionally, both of these studies analyze just one parameter vector, and there are some parameter vectors for which, e.g., the GSM exhibits only a minor resolution dependence.’

and the paragraph outlined in our response to comment 3.3 - Brinkerhoff and Johnson, 2015 suggest that the inclusion of membrane stresses leads to convergence under spatial grid refinement, whereas without them, the SIA does not lead to convergence. Can you place those results in the context of this section? Are the relatively weak convergence results here a result of GSM and PISM velocity solvers being insufficiently ‘higher-order’?

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Author's response to Anonymous Referee 2 Comment 1

June 27, 2023

1 General Comment

[The goal of this study is a worthy one, and though the general topic of simulating thermal oscillations in ice sheet models has received considerable attention over three decades, a systematic study of the dependence of oscillation characteristics on choices in the numerical implementation has not been done. The main issue I see is that the manuscript in its current form is very challenging to read. It is organized more like a reference guide to a large number of simulations, rather than a discussion of the link between real physical processes, numerical choices and clear recommendations for how to remedy these issues in future simulations. In order to be publishable in a form that will be usable by other researchers, the manuscript needs substantial re-organization, reduction in length and re-writing in places. Below the major issues are listed in more detail (I will wait to comment on minor issues in a subsequent revision):]

We thank the referee for their constructive comments. We have addressed all the referee's comments and revised the text accordingly. A point-by-point reply is reported below, with referee comments in orange and our replies in black.

We agree that the readability of the paper benefits from a general re-organization and focusing on the key takeaways (Numerical Model Error Estimates (MNEEs) must be considered when numerically modeling ice stream surge cycles, surge characteristics are sensitive to the basal sliding activation criterion, resolution dependency can be reduced by incorporating a resolution-dependent basal sliding activation criterion). To streamline the paper, we grouped the 11 research questions into three main themes: 1) determine the 'MNEEs' as a metric to determine the significance of a change in model configuration (note that we use the MNEEs because we are not able to determine the model error; we provide more details on this issue in our replies below), 2) using the MNEEs, determine the sensitivity of the surge characteristics (number of surges, mean surge periodicity, mean surge duration, and mean ice volume change during a surge) to model aspects with a physical relevance (particular focus on the basal sliding activation criterion), and 3) perform a convergence study based on the results of 1) and 2).

We also reworked the 'Results Summary and Discussion' section to provide a more extensive and accurate comparison to the existing literature (e.g., added comparison to the EISMINT temperature spokes) and to discuss the link between real physical processes and numerical choices. We also added recommendations for what key model components should be used when modeling ice stream surge cycling.

2 Detailed comments

[1. Currently, the organization of the manuscript feels like a laundry list of simulations completed and a description of the results, without prioritizing the most important and revealing simulations and little discussion for what the results mean and how they relate to other studies. The study also seems to currently have about 10-15 areas of focus, making it challenging to see which end up actually being important. My recommendation would be to take all the description of simulations where numerical choices don't appear to have much influence on the results

and move them into a supplement. They can be summarized in a few sentences perhaps at the end of the results section, but right now they add too much extra to the manuscript making it longer and hard to get through. This includes the sediment-hard bed transition, basal hydrology, basal hydrology instead of temperature ramp and the max time step.] While discussing numerical choices that do not significantly affect the results is important, we agree that these details can be moved to the supplement to make the manuscript more accessible to the reader. Following this suggestion, we grouped the individual research questions into the following main themes: 1) MNEEs (Q1), 2) sensitivity experiments with (previous Q2, Q3, Q4, Q5, Q7, Q8; now Q2, Q3, Q5, Q6, Q7, Q8) and without a significant effect on the results (previous Q6, Q9, Q10; now Q4, Q9, Q10), and 3) convergence study (Q11). The sensitivity experiments without a significant effect will be only briefly summarised in the main manuscript. Since the results of the convergence study depend on previous experiments, this aspect is discussed last.

[2. The way the results are currently described and presented also contributes to the challenge of reading through this manuscript. There are 15 tables, and it is difficult to understand what all the numbers in the tables mean. Figures 8 and 6 seem like a more intuitive way to present this information (though all the markers and line and shading in Figure 6 need explicit descriptions in the caption and perhaps a legend to be interpretable). There really shouldn't be more than a few tables in the main text of this manuscript, the rest should be relegated to a supplement.] We agree that there were too many tables in the main manuscript. To increase the readability, we replaced most of the tables in the results section with the two new figures 6 and 7 (same plot idea as the previous figure 6). These figures summarise the sensitivities of the surge characteristics of all model components with a significant effect in a concise way. In terms of model components analyzed, we are now focusing only on model components that have significant effects on the surge characteristics in order to reduce the burden on the reader.

Most information necessary to interpret the previous figure 6 (figure 9 in the revised draft) was already in the caption. However, to make it even clearer, we slightly updated the caption from:

Percentage differences in event characteristics compared to the GSM base setup ($T_{ramp} = 0.0625$, $T_{exp} = 28$) for different basal temperature ramps at 3.125 km horizontal grid resolution. The ramps are sorted from widest (first row) to sharpest (last row, see Fig. S25 for a visualization of all ramps). The shaded pink regions mark the numerical noise estimates (Tab. 5) and the black numbers in the title of each subplot represent the mean values of the base setup. No runs crashed and all runs had more than 1 surge event. The first 20 kyr of each run are treated as a spin-up interval and are not considered in the above. The x-axis is logarithmic. The exact values are given in Tab. S5.

to

Percentage differences in event characteristics compared to the GSM base setup ($T_{ramp} = 0.0625$, $T_{exp} = 28$) for different basal temperature ramps at 3.125 km horizontal grid resolution (average of the 5 parameter vectors). The ramps are sorted from widest (first row) to sharpest (last row, see Fig. S24 for a visualization of all ramps). Otherwise same as Fig. 6. No runs crashed and all runs had more than 1 surge event. The exact values are given in Tab. S10.,

where the caption in figure 6 states

[...] The different colors were added for visual alignment of the individual model setups, the stars are the ensemble mean percentage differences, and the horizontal bars represent the ensemble standard deviations. The shaded pink regions mark the MNEEs (Table 5) and the black numbers in the title of each subplot represent the mean values of the reference setup. The 3 small numbers between the first two columns represent the number of crashed runs (nC), the number of runs without a surge ($nS0$), and the number of runs with only one surge ($nS1$), respectively. The first 20 kyr of each run are treated as a spin-up interval and are not considered in the above. The x-axis is logarithmic. [...]

Note that figures in the form of figure 8 (now figure 12) were not suitable to replace the tables because they only show the results of one parameter vector.

[3. The "such as" in the title of the paper is misleading. The only type of ice sheet instability discussed and tested in this paper is a thermal oscillatory instability (or B-P). A more accurate title would be simpler: "Numerical issues in modeling binge-purge type cyclic ice stream surging"] In order to give a more accurate description of the content of the manuscript, we changed the title from: *Numerical issues in modeling ice sheet instabilities such as binge-purge type cyclic ice stream surging*

to: *Numerical issues in modeling thermally and hydraulically driven ice stream surge cycling.*

[4. Related to #3 and throughout - the term "binge-purge" oscillations has largely fallen out of favor in the ice sheet modeling community. These are more commonly called thermal oscillations or ice stream activation-stagnation cycles. It is OK to mention in the introduction that these have historically been referred to as binge-purge, but it isn't in keeping with the field to continue to refer to them as such throughout.] Thanks for bringing this up. Except for historical contexts, we now use *ice stream surge cycling* instead of *binge-purge cycling*. Note that we were not aware of such a development [e.g., Roberts et al., 2016, Feldmann and Levermann, 2017, Ziemen et al., 2019, Schannwell et al., 2023, still use 'binge-purge']

[5. I am quite confused over how numerical noise is defined in this manuscript. It seems in section 3.1.3 that to quantify numerical noise that different solver choices are used. However, depending on the number of iterations occurring between the different tolerances (and the details of how the solver works) it would seem that this method could yield strongly different estimates for the "noise". Additionally, it is unclear why this is the correct bar for determining whether a change is "important", instead of a more physically meaningful quantity. Additionally, the rationale behind the set of simulations detailed in Table 6 is confusing. In a bitwise reproducible code, I don't see why the number of cores used in a simulation should have any influence on the simulations. This makes me concerned about the robustness of other simulations if the number of cores has such an important influence on the results. How reproducible are these results by other researchers? If the same setup is run on a different cluster architecture would the results be different?]

We agree that the concept of 'numerical noise' needed clarification. We changed the term 'numerical noise' to 'minimum numerical error estimates' and updated the first part of the introduction from: *The use of Ice Sheet Models (ISMs) has grown at least an order of magnitude over the last two decades. The relevance of such modeling studies to the actual physical system can be unclear without careful consideration and testing of numerical components and implementations. Model validation is particularly important when modeling highly non-linear ice sheet instabilities, for which it is hard to distinguish between numerical noise and physical phenomena. In addition, there are a number of numerical choices, such as for thermal activation of basal sliding, for which no model to date has documented sensitivities.*

to: *The use of Ice Sheet Models has grown at least an order of magnitude over the last two decades. The relevance of such modeling studies to the actual physical system can be unclear without careful consideration and testing of numerical aspects and implementations. This is especially true when modeling the highly non-linear ice sheet surge instability, which has significant implications not only for the ice sheet itself but also for the climate. In fact, it is often difficult to assess whether model results are physically significant (effects of physical system processes), a consequence of model-specific numerical choices, or a combination of both. This is especially important in the case of abrupt changes. Whether ice sheet instabilities observed in numerical simulations are the result of physical instabilities of the underlying continuum models or spurious effects of the discretization and numerical implementation of said models has long been debated [e.g., Payne et al., 2000, Hindmarsh, 2009] and is a consequential matter. The present study is concerned with characterizing the impact of model physics, numerical choices, and numerical errors on ice stream surge cycling.*

[...]

As a result of the involved physics and expected behaviors, modeling of ice stream surge cycling is challenging. The challenges entail, among others, rapid surge onset, high ice velocities,

and non-linear (thermo-viscous, hydraulic, and thermo-frictional) feedbacks. In addition to the physical complexity, further challenges arise in the numerical modeling of ice stream surge cycling, whether in terms of model choices (e.g., choice of mechanical model, thermal modeling of the substrate, accounting for sub-glacial hydrology) and/or in terms of their numerical implementation (e.g., grid and time step size, convergence under grid refinement, etc.).

Our focus here is on the challenges arising from numerical modeling, both those related to the modeling choices and those related to the implementation. Numerical challenges have received limited attention in studies examining ice sheet surging. The few studies to date that do examine numerical aspects of surge cycling suggest strong sensitivities in model response to implementation choices such as grid size [e.g., Calov et al., 2010, Roberts et al., 2016, Ziemen et al., 2019]. However, the effects of different approximations of the Stokes equations have been previously addressed [e.g., Brinkerhoff and Johnson, 2015], and are therefore not discussed here.

[...]

In terms of different numerical choices, the impact on model results is usually determined by calculating the model error to the exact analytical solution. However, the theory behind the surge instability is not fully developed (no analytical solution exists), especially in the context of a spatially extended 3D system, thus precluding systematic benchmarking of numerical models.

To overcome this issue and provide at least a minimum estimate of the numerical model error, we first determine 'Minimum Numerical Error Estimates' (MNEEs). This is a new metric that aims to minimally resolve whether a change in surge characteristics due to changes in the model configuration is significant (see Sec. 2.3 for details).

The corresponding part in Sec. 2.3 states: We compute the new 'Minimum Numerical Error Estimates' (MNEEs) metric by examining the model response to changes in the model configuration that are not part of the physical system. The MNEEs are defined as the percentage differences in surge characteristics when applying a stricter (than default) numerical convergence in the GSM and adjusting the matrix solver used in PISM (changing the number of processor cores used). They are then used as a threshold to determine if model sensitivities to changes in the model configuration that affect the physical system (e.g., the inclusion of a bed thermal model or sliding dependence on effective pressure from basal hydrology) are above the level of background noise induced by iterative numerical solvers in the model. We refrain from drawing conclusions about the effects of a change in model configuration with physical relevance when the model sensitivities in question are smaller than the MNEEs. In these cases, the actual physical response of the model might be hidden within the numerics.

While the MNEEs are useful to our purpose, we wish to emphasize that they can not replace proper model verification and validation and are missing uncertainties due to, e.g., different approximations of the Stokes equations and other physical processes not included in the models. Nonetheless, they provide a minimum estimate of the numerical model error, which is still a significant improvement over ignoring this issue entirely.

The above description should clarify our intentions behind using the MNEEs instead of a physically meaningful quantity (we are unsure how a physically meaningful quantity could determine whether the modeled result is due to numerical errors or a true physical phenomenon). However, we have tested the effect of different tolerances and added the following short statement to the revised draft: The differences in surge characteristics between different numbers of cores can be minimized by decreasing the relative Picard tolerance in the calculation of the vertically-averaged effective viscosity (10^{-4} to 10^{-7}) and the relative tolerance for the Krylov linear solver used at each Picard iteration (10^{-7} to 10^{-12} , Table S5 and Fig. S19). However, this leads to an unreasonable increase in model run time ($\sim 300\%$) that is not feasible for an ensemble-based approach (more than 50% of all runs did not finish within the time limit of the computational cluster). Intermediate decreases in the relative tolerances still lead to significant differences in surge characteristics while increasing the model run time and are, therefore, not used in the PISM reference setup.

When dealing with non-linear transitions such as surge onset and shutdown, small differences

can accumulate and lead to a somewhat different result at the end of the model run. These small differences can be caused by, e.g., a different number of cores (see [online PETSc-FAQ link](#)). PETSc is used by PISM. So the results might be somewhat different on a different cluster. However, the whole point of introducing the MNEE threshold is to identify what characteristics and relations are likely to be robust.

[6. In section 4 I see the summary of results, but very little discussion of what they mean (in some cases but not others). This seems to me to be the main missing piece of the manuscript to be useful to other researches, a discussion of how these results relate to the theory of thermal oscillations (from Schiavi, Mantelli, Robel, MacAyeal, etc.) and how they might relate to other ice sheet models.] Where possible, we added a more in-depth discussion to the revised draft (see below). However, a comparison to the existing theory is not straightforward because the theory in the context of 3D thermo-mechanically coupled models with hybrid SIA/SSA ice dynamics is not fully developed.

Q_1 - MNEEs: *We expect other ice sheet models with a comparable experimental design and ice dynamics to show similar levels of MNEEs. To minimize the possibility of interpreting numerical errors as a physical response to a change in model setup, it is crucial to determine MNEEs (or a comparable metric).*

Q_3 - interface temperature: *The additional heat transfer to the grid cell interface is comparable to spreading 50 % of the basal heating effect from sliding in a grid cell to the surrounding grid cells used in mPISM (latest version based on PISM v0.7.3) [e.g., Ziemen et al., 2014, 2019, Schannwell et al., 2023]. This spreading of basal heating warms the grid cells adjacent to an ice stream and was necessary to model Heinrich Event-like surges (Florian Ziemen, personal communication). While no additional heat transfer was added to PISM v2.0.2 used within this study, the till friction angles had to be reduced to model surges.*

Q_5 - basal temperature ramp: *To account for observational and experimental evidence of sub-temperate sliding [Barnes et al., 1971, Shreve, 1984, Echelmeyer and Zhongxiang, 1987, Cuffey et al., 1999, McCarthy et al., 2017], avoid an abrupt onset of sliding at the warm/cold-based transition that causes refreezing on the warm-based side [Mantelli et al., 2019], and minimize resolution dependencies, a basal temperature ramp (or similar mechanism) should be implemented in all ice sheet models for contexts where surge onset/termination are important.*

Q_6 - abrupt sediment transition: *Since the sediment cover can change within a few kilometers [e.g., Andrews and MacLean, 2003], we conclude that, despite the minor differences, an abrupt transition between soft and hard beds is a reasonable simplification, especially considering horizontal grid cell dimensions of 25 km or larger.*

Q_7 - bed topography: *In agreement with previous modeling studies [e.g., Winsborrow et al., 2010, and references within], the topography is a key aspect of ice stream modeling. When interested in a comparison with observational data or proxy reconstructions, a more realistic topography (in contrast to the idealized flat topography) should be used.*

Q_{11} - convergence study: *Even though the studies are not directly comparable, the results of Brinkerhoff and Johnson [2015] offer some insight relevant to this study. For example, they suggest membrane stresses are necessary for convergence under horizontal grid refinement. The hybrid SIA/SSA ice dynamics used in the GSM and PISM might be insufficiently 'higher-order' and lead to a stronger resolution dependence than the schemes used in Hindmarsh [2009], Brinkerhoff and Johnson [2015]. However, GSM experiments with the SSA active everywhere show a resolution dependence comparable to the velocity-dependent SSA activation criteria (Table S24 and S18, respectively), indicating that the hybrid SIA/SSA ice dynamics are not the sole reason for the strong resolution dependence.*

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