

1 **Title:** An Autonomous Flow Through Salinity and Temperature Perturbation Mesocosm System  
2 for Multi-stressor Experiments

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4 **Author list:** Miller, C.A.<sup>1,2\*</sup>, Urrutti, P.<sup>1</sup>, Gattuso, J.-P.<sup>1,3</sup>, Comeau, S.<sup>1</sup>, Lebrun, A.<sup>1</sup>, Alliouane<sup>1</sup>  
5 S., Schlegel, R.W.<sup>1</sup>, and F. Gazeau<sup>1</sup>

6  
7 <sup>1</sup>Sorbonne Université, CNRS, Laboratoire d'Océanographie de Villefranche, 181 chemin du  
8 Lazaret, F-06230 Villefranche-sur-Mer, France

9  
10 <sup>2</sup>Present address: Department of Earth Sciences, Geosciences, Utrecht University, Utrecht, The  
11 Netherlands

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13 <sup>3</sup>Institute for Sustainable Development and International Relations, Sciences Po, 27 rue Saint  
14 Guillaume, F-75007 Paris, France

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17 \*Correspondence to: [Cale A. Miller](mailto:c.a.miller@uu.nl) (e-mail: c.a.miller@uu.nl)

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35 **Abstract**

36 The rapid environmental changes in aquatic systems as a result of anthropogenic forcings are  
37 creating a multitude of challenging conditions for organisms and communities. The need to  
38 better understand the interaction of environmental stressors now, and in the future, is  
39 fundamental to determining the response of ecosystems to these perturbations. This work  
40 describes an automated *ex-situ* mesocosm perturbation system that can manipulate several  
41 variables of aquatic media in a controlled setting. This perturbation system was deployed in  
42 Kongsfjorden (Svalbard) where ambient water from the fjord was heated and mixed with  
43 freshwater in a multifactorial design to investigate the response of mixed kelp communities in  
44 mesocosms to projected future Arctic conditions. The system employed an automated dynamic  
45 offset scenario where a nominal temperature increase was programmed as a set value above real-  
46 time ambient conditions in order to simulate future warming. A freshening component was  
47 applied in a similar manner where a decrease in salinity was coupled to track the temperature  
48 offset based on a temperature-salinity relationship in the fjord. The system functioned as an  
49 automated mixing manifold that adjusted flow rates of warmed and chilled ambient seawater,  
50 with unmanipulated ambient seawater and freshwater delivered as a single source of mixed  
51 media to individual mesocosms. These conditions were maintained via continuously measured  
52 temperature and salinity in all 12 mesocosms (1 control and 3 treatments, all in triplicates) for 54  
53 days. System regulation was robust as median deviations from nominal conditions were < 0.15  
54 for both temperature (°C) and salinity across the 3 replicates per treatment. Regulation further  
55 improved during a second deployment that mimicked three marine heatwave scenarios where a  
56 dynamic temperature regulation held median deviations to < 0.036°C from the nominal value for  
57 all treatment conditions and replicates. This perturbation system has the potential to be

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64 implemented across a wide range of conditions to test single or multi-stressor drivers (e.g.,  
65 increased temperature, freshening, high CO<sub>2</sub>) while maintaining natural variability. The  
66 automated and independent control for each experimental unit (if desired) provides a large  
67 breadth of versatility with respect to experimental design.

68

## 69 1 Introduction

70 The persistent burning of fossil fuels since the industrial revolution has radically increased  
71 atmospheric CO<sub>2</sub>. This has led to an enhanced greenhouse effect resulting in a multitude of  
72 changing climatic elements such as increasing sea surface temperature (Bindoff et al., 2019). In  
73 fjord systems, the confluence of increased fluvial inputs, glacier and permafrost meltwater,  
74 stratification and water mass intrusion, as well as increased sea surface temperatures can create  
75 periods of extreme physicochemical conditions for nearshore benthic and pelagic marine  
76 communities (Bhatia et al., 2013; Poloczanska et al., 2016; Divya and Krishnan, 2017; Bindoff et  
77 al., 2019). As ocean changes progress, the need to better understand the effects of combined  
78 stressors (e.g., increased temperature and freshening) on marine communities is essential to  
79 understand how community function and species richness will be affected ~~while ecosystems~~  
80 adjust to ~~these~~ new environmental conditions (Kroeker et al., 2017; Wake, 2019; Orr et al.,  
81 2020). ~~Several methodological approaches have been used to assess and characterize the~~  
82 ~~response of organisms and communities to future ocean changes, such as ex-situ~~  
83 ~~experimentation, the use of natural analogues (e.g., CO<sub>2</sub> vents), and space-for-time substitution~~  
84 ~~(using spatial phenomena to model temporal changes) (Blois et al., 2013; Rastrick et al., 2018;~~  
85 ~~Bass et al., 2021). These approaches, however, can be limited from testing the full range and~~  
86 dynamics of present and future environmental conditions. The use of *ex-situ* experimental

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108 systems that manipulate multiple environmental conditions, such as temperature and salinity, can  
109 therefore provide a valuable tool to assess the response to multi-stressors in a future ocean.

110 The necessity of conducting multi-stressor experiments has become more pressing due to  
111 the increasing interactions of environmental drivers within dynamic systems under a changing  
112 climate (Kroeker et al., 2020). Nearshore regions can experience amplified modulations of  
113 temperature and salinity on short timescales (Evans et al., 2015; Hales et al., 2016; Fairchild and  
114 Hales, 2021). Such instances have been observed in sub-Arctic estuaries where water  
115 temperature at a depth of 10 m decreased by 1.5°C in < 10 h, and in temperate systems where the  
116 magnitude of salinity change driven by high precipitation displayed a decrease of 4 units in < 24  
117 h (Miller and Kelley, 2021; Poppeschi et al., 2021). Changes of this magnitude are particularly  
118 pertinent for Arctic fjords, where the variations in salinity from glacial meltwater can influence  
119 whether a system exhibits net heterotrophic or autotrophic characteristics (Sejr et al., 2022).

120 Recent advances in the ability to modulate several environmental parameters at once  
121 using *ex-situ* mesocosms have been made via the use of modular programmable systems (Wahl  
122 et al., 2015; Pansch and Hiebenthal, 2019). Such systems have demonstrated an ability to apply  
123 programmable environmental scenarios as a multifactorial design, or as a delta-change (offset)  
124 from ambient conditions that mimic the natural variability of an environment. The advantages of  
125 these types of automated systems lie in their ability to overcome the need for capturing and  
126 measuring abundant discrete measurements used to regulate experimental conditions, and  
127 transcend the logistical difficulties of implementing natural variability to experimental designs.  
128 In addition, these systems can reduce the need for constant human observation which may be  
129 required to program new regulatory operations or make rapid adjustments to experimentally  
130 manipulated conditions.

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154 Here, we describe an autonomous salinity and temperature experimental perturbation  
155 mesocosm system (SalTEExPreS) that has the ability to modify, and then regulate, salinity and  
156 temperature in real-time. The SalTEExPreS can perform similar functions as the *ex-situ* mesocosm  
157 systems discussed [above](#) (i.e., Kiel-outdoor and -indoor benthocosms), such as applying  
158 programmable static or dynamic changes to temperature and salinity, or by replicating natural  
159 variability as on offset in real-time, but has the added capability of autonomous control for each  
160 experimental unit (e.g., chamber or mesocosm). In the initial deployment of the SalTEExPreS, we  
161 applied a delta offset (i.e., offset from a measured control) to temperature and salinity as a  
162 fractional-factorial treatment design for a two-month long experiment in KongsFjorden,  
163 Svalbard, that exposed mixed kelp communities to future temperature, salinity, and irradiance.  
164 This study demonstrates the stability and flexibility of the SalTEExPreS as an experimental tool to  
165 be utilized under extreme and dynamic conditions to test the effects of physicochemical multi-  
166 stressors on marine organisms and communities in the context of a multi-month experiment.

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## 168 2 Methods

### 169 2.1 Operational Concept of the Experimental System:

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171 The SalTEExPreS simulates the drivers in a marine or freshwater system such as temperature,  
172 freshening, acidification, or hypoxia as either static or as temporally-variable modifications to a  
173 [reference water source](#). This is accomplished by mixing manipulated source water, whether it is  
174 freshwater or warmed water, with ambient water through automatic flow valves that control the  
175 volume and rate of water delivered. This is regulated by the constant monitoring of the mixed  
176 water conditions in each mesocosm or chamber via a programmable feedback loop that transmits  
177 the opening or closing of the automatic flow valves. The automated ability of the SalTEExPreS is

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182 configured to respond to near instantaneous measurements (several reads per second) to achieve  
183 high frequency regulation of the manipulated drivers based on a measured *in-situ* or control  
184 reference. The programmable **nominal** conditions in each mesocosm are easily controllable  
185 through an intuitive **user** interface.

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## 187 2.2 Site Description and Experimental Design

188 Kongsfjorden is a fjord system on the west coast of Svalbard (Norway) where the West  
189 Spitsbergen Current exchanges warm Atlantic water through sill channels based on differences in  
190 density gradients at the fjord mouth. Over the past two decades, a persistent influx of Atlantic  
191 water has resulted in the reduction of **sea** ice and the melting of **marine**-terminating glaciers  
192 causing enhanced freshwater and fluvial input (Luckman et al., 2015; Tverberg et al., 2019). The  
193 influx of freshwater is highest in summer and is accompanied by an important sediment loading  
194 with the potential to **reduce** the euphotic zone from 30 to 0.3 m depth (Svendsen et al., 2002).  
195 These **climatic** changes in **the Kongsfjorden environment** set a relevant context for the inaugural  
196 **experiment** of the SalTExPreS. **It was placed** on a concrete platform situated ~ 12 m from the  
197 shoreline in Ny-Ålesund, which is located on southwestern shore of Kongsfjorden ~ 11 km from  
198 the fjord mouth.

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199 The SalTExPreS was utilized to implement three treatment scenarios in a fractional-  
200 factorial design to **simulate** expected future conditions in Kongsfjorden for a **54 d** experiment  
201 that **supervised** the productivity, survival, and growth response of mixed kelp communities  
202 **surveyed** at 7 m (**maximum depth of collection**). The treatments were realized by multi-driver  
203 combinations of temperature, freshening, and irradiance, where treatments 1 and 2 differed in the  
204 magnitude of temperature increase, salinity decrease, and irradiance decrease (Table 1). Only

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224 temperature was manipulated for treatment 3. The chosen treatment and salinity perturbations  
225 were applied as offset values from *in-situ* fjord conditions, which were measured at an  
226 underwater observatory fixed at 11 m depth and captured the natural variability of the fjord  
227 system. The applied temperature offsets used for this experiment reflected the projected SSP2-  
228 4.5 and SSP5-8.5 scenarios (Meredith et al., 2019; Overland et al., 2019; Table 1). The chosen  
229 decreases in salinity were based on correlations between *in-situ* temperature and salinity during  
230 summer 2020 in Kongsfjorden (Gattuso et al., 2023), weeks 22 to 35 (Appendix A1 and Fig.  
231 A1). These calculated delta salinity values were applied as offsets in treatments 1 and 2 (Table  
232 1). The third treatment scenario applied a temperature change of + 5.3°C as a way to decouple  
233 the multi-stressor system and evaluate a temperature only stress. The effect of turbidity for  
234 treatments 1 and 2 were simulated as a decrease in surface irradiance (i.e., ~ 25% and ~ 40%  
235 reduction from ambient irradiance at 7 m) by applying a combination of neutral light and spectral  
236 filters (Lee© Filters) placed as static fixtures over the top of the mesocosms. The response of  
237 these kelp community assemblages was determined in part by conducting weekly closed system  
238 incubations and assessing the growth and metabolism of the kelp in each mesocosm—details and  
239 results of this experiment are discussed elsewhere (Lebrun et al. *in review*; Miller et al., *in*  
240 *review*).

241

### 242 **2.3 Experimental System**

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244 Water was pumped from Kongsfjorden at a 10 m depth (300 m offshore) using a submersible

245 pump (NPS© Albatros F13T) that was tapped into an underwater intake pipe and that fed a

246 header tank in the Kings Bay Marine Laboratory in Ny-Ålesund, Svalbard. To prevent clogging

247 from sediment, the pump was situated at a 10 m depth ensuring a safe height above sediment

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253 **resuspension from the floor.** Pumped ambient seawater from the header tank was then split into  
254 three sub-header tanks within the marine lab where ambient water was (1) left unchanged, (2)  
255 chilled to 0°C, or (3) warmed to 15°C. Each sub-header tank was plumbed to supply a maximum  
256 flow of 6 m<sup>3</sup> h<sup>-1</sup> for the ambient, 1 m<sup>3</sup> h<sup>-1</sup> for chilled, and 2 m<sup>3</sup> h<sup>-1</sup> of warmed water which  
257 required a pressure of 0.3 bars for each line to ensure consistent flow rates (Fig. 1). The three  
258 control mesocosms received a mix of chilled and ambient seawater in order to properly simulate  
259 *in-situ* temperatures. The three experimental treatments (nine mesocosms in total) received a mix  
260 of ambient, warmed, and freshwater for treatments 1 and 2, whereas treatment 3 received a mix  
261 of just ambient and warmed water (Fig 1). Freshwater was sourced from the tap which **is** fed by  
262 the Tvillingvann reservoir close to Ny-Ålesund. The total flow-through rate of each mesocosm  
263 was 0.5 m<sup>3</sup> h<sup>-1</sup> (i.e., each mesocosm turned over every 2 h) of post-mixed media delivered in an  
264 open cycle flow-through system, **which was the necessary flow rate needed to maintain the target**  
265 **nominal values.** Continuous flow was maintained throughout the experiment **except for weekly 3**  
266 **h interruptions** (to perform experiments on the community) where the flow to each mesocosm  
267 was shut off. In total, there were twelve circular mesocosms (3 treatments and 1 control, **each**  
268 **with 3** replicates) with a mean diameter of 1.1 m and a volume of 1 m<sup>3</sup>, each equipped with a 12  
269 W wave pump (Sunsun© JVP-132), a temperature-conductivity probe (Aqualabo, PC4E), an  
270 optical oxygen sensor (Aqualabo, PODOC), and an Odyssey© light logger. Fiberglass insulation  
271 **at the outside of each mesocosm reduced unintended changes in treatment water** temperature.

272 Delivery of ambient, chilled, warmed and freshwater first ran through an automated  
273 mixing manifold that regulated the flow of each media type assuring that proper volumetric  
274 proportions passed through the regulator valves to achieve target conditions (Fig. 1). Each  
275 source-water flow line was regulated by an automated 2-way mixing valve (**including the**

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294 incoming freshwater line) which then passed through a 3-way mixing valve that was assigned to  
295 each mesocosm (12 in total, Fig. 1). This style of regulation ensured that the proper proportions  
296 of manipulated media and ambient water were mixed to achieve nominal conditions. Any  
297 temperature variation induced by mixing freshwater was immediately compensated for by  
298 regulating the flow of the warm water line. Details regarding the programmed regulation are  
299 discussed further in the appendix (Section A2). The mixed media then passed through a flow  
300 meter which measured the flow rate to each mesocosm. A hand-crank regulating valve was  
301 placed directly after the flow meter and was used for making minor adjustments and controlling  
302 the overall flow. Measurements by the pressure sensors, the status of open position for the  
303 regulator valves, and flow rates were logged every minute and displayed on the user interface  
304 (Fig. A3).

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## 306 2.4 Nominal Regulation

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308 Nominal temperature conditions of + 3.3, 5.3, and 5.3°C applied to treatments 1, 2, and 3,  
309 respectively, were offsets from the nominal control temperature. The nominal temperature of the  
310 control was updated hourly and programmed to replicate the measured *in-situ* conditions in the  
311 fjord logged by the AWIPEV (Alfred Wegener Institute and Institute Paul Emile Victor)  
312 FerryBox part of the COSYNA underwater observatory (<https://dashboard.awi.de/>) situated at a  
313 depth of 11 m. Each treatment condition (temperature and salinity offset) was set by manually  
314 programming the nominal value of temperature in the software interface (see appendix A3). The  
315 salinity offset was coupled to the nominal temperature via the correlation described in appendix  
316 A1. The measured temperature and salinity observations from inside each mesocosm were  
317 recorded multiple times per minute and used to continuously monitor the regulation of the

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339 conditions inside each mesocosm. This data transmission was used to program the software  
340 controller that performed the automated regulation of mixed media (for details see appendix A2).

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## 341 342 2.5 Software

343 The software application used for the control of the SalTEPreS was developed using Visual  
344 Studio Community (2019 edition) with the vMicro extension and Arduino 1.8.13. The program  
345 application has a user-friendly interface designed to allow real-time monitoring and

346 parameterization of regulation processes (Fig. A3). The main window displays each mesocosm  
347 condition (the parameters measured by a sensor), their piping connections, a connection status  
348 for each Programmable Logic Controller (PLC) informing on proper communication, date and  
349 time of the last received communication packet from the Head PLC, and the status of the

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350 experiment (e.g., started or stopped). The interface also displays the valve opening percentage  
351 along with the nominal pressure and the actual measured value for each main source-water inlet.

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352 In addition, the *in-situ* data (temperature and salinity) received from the FerryBox is displayed  
353 with the time and date of the last logged value utilized to program the real-time nominal value of

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354 the control. Sensor readings of flow rate ( $L\ min^{-1}$ ),  $O_2$  saturation (%), salinity, and temperature  
355 ( $^{\circ}C$ ) are shown for each mesocosm in conjunction with the treatment nominal values (i.e.,  
356 temperature, and salinity when relevant). All measured data are stored through the server

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357 connection to the cloud, however, there is a backup microSD card on the Head PLC that logs  
358 data from all mesocosms every 5 sec. If communication fails between the Head PLC and the  
359 interfaced computer, data will not be retrieved by the PC during the communication break but  
360 will be retained by the microSD card.

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## 361 362 3 Results

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### 3.1 Regulation of the Control

The control was able to simulate the ambient fjord temperature well over the experimental period where the average value across the 3 replicates deviated  $< 0.3^{\circ}\text{C}$  (Table 2, Fig. 2). The overall quality of the regulation was achieved by the ability of the system to interpret and respond to the measured data from the FerryBox (or to follow a manually programmed nominal value when communication with the FerryBox was interrupted). During the experiment, the FerryBox went intermittently offline 24% of the time, ceasing transmission of real-time data that resulted in a break of communication to the PLCs. This somewhat frequent break in communication resulted in an average nominal deviation that was nearly double for the control compared to the treatment conditions (Table 2). The ability to manually program a new nominal value when communication breaks occurred ensured that the control remained robustly regulated. Over the entire period of the SalTexPreS deployment, the mean temperature of the control increased from  $\sim 4$  to  $6.5^{\circ}\text{C}$  from early July to the end of August (Fig. 3a). The coldest mean temperature of the control occurred when a backup pump situated at 90 m depth in the fjord was used from 2021-07-14  $\sim 21:00$  UTC until 2021-07-26 13:49 UTC while the original pump at 10 m depth was repaired. During this period, the control was  $\sim 1.0 - 1.5^{\circ}\text{C}$  cooler than the temperature measured by the FerryBox (Figs. 2, 3). Since a warmed seawater inlet was not supplied to the control, the temperature of the control remained cooler than the measured ambient conditions at the FerryBox. Despite the cooler temperature for the control, regulation of flow rates, mesocosm turnover time, and variability across the control replicates was well maintained by the system.

### 1.2 Temperature and Salinity Regulation

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425 The regulation of temperature and salinity in the different treatment conditions (Trts. 1 – 3) was  
426 maintained by the SalTExPreS for the full planned duration of 54 days (2021-07-03 to 2021-08-  
427 26). For the first 6 days of the SalTExPreS experiment, the treatment conditions were held at the  
428 control (i.e., no applied offset from the control) before the stepwise increase in temperature  
429 began. On 2021-07-10 12:00 UTC a temperature offset of 0.55°C d<sup>-1</sup> was programmed for  
430 treatment 1 while treatment 2 and 3 were programmed to increase by 0.88°C d<sup>-1</sup> (Figs. 2, 3). The  
431 final nominal temperature above the control was reached on 2021-07-15 21:00 UTC. The system  
432 needed 4 h to achieve the new temperature conditions (i.e., homogenize the mesocosm to a  
433 0.88°C increase). A manual override was applied to the salinity regulation for treatments 1 and 2  
434 which resulted in the system achieving the final salinity offset value upon the initial temperature  
435 increase (Fig. 3b, 4). This was done to ensure the maintenance of salinity regulation as the  
436 temperature offsets were applied relative to the control, which was receiving fjord water pumped  
437 from 90 m and was colder than the measured *in-situ* conditions. It took the system 4 h to achieve  
438 the salinity offset for treatment 2 adjusting the value from ~34 to 29.8 (Fig. 3b, 4).

440 The precision of the temperature and salinity regulation across all treatment conditions  
441 was well maintained as the mean difference between the measured value and the nominal value  
442 was < 0.2°C and < 0.36 for salinity across the entire deployment (Table 2). The mean deviations  
443 observed across treatments did not appear to correlate to the degree of offset. Thus, treatment 3  
444 showed the highest precision for temperature regulation, while salinity regulation was the most  
445 robust for treatment 2 compared to treatment 1 (Table 2). During several instances when  
446 communication was interrupted between the FerryBox and the Head PLC, the SalTExPreS  
447 retained the last measured value at the FerryBox as a contingency protocol. This aided in the  
448 ability of the system to maintain a high degree of regulation throughout the entire deployment.

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468 The largest deviation from the nominal value for all treatment conditions occurred during the  
469 single instance in which the last read value from the FerryBox was not retained: this occurred on  
470 2021-08-24 04:47 UTC (Fig. 4). Communication was quickly restored after this incident by  
471 cycling the program code, and the average deviation of temperature (°C) and salinity for  
472 treatment 1 for the remainder of the deployment was < 0.16, and < 0.25 for treatment 2.

473 When adequate flow rates were maintained, the SalTExPreS was able to simultaneously  
474 regulate 12 mesocosms at 4 different conditions to deviations in temperature and salinity that  
475 were < 0.5°C or 0.5 in salinity from the nominal value  $\geq 80\%$  and  $\geq 70\%$  of the time,  
476 respectively (Fig. 5). Due to an erroneous nominal value for the control during the 90 m pump  
477 usage, these times were excluded. If warm water could have been mixed with the ambient water  
478 feeding the control mesocosms, then a proper nominal value could have been maintained. Over  
479 the full duration of the experiment, effective regulation from the nominal temperature and  
480 salinity values were kept to < 1 for all mesocosms 89% of the time for temperature (°C), and  
481 80% for the salinity (excluding the 1<sup>st</sup> replicate for treatment 2).

## 483 Discussion

484  
485 The first application of the fully autonomous SalTExPreS demonstrated the capacity of the  
486 system to successfully manipulate temperature and salinity as an offset value from the control,  
487 thus maintaining, natural, *in-situ* variability for 4 different conditions simultaneously. We  
488 utilized this deployment to test the effects of climate change drivers on Arctic kelp communities  
489 recognizing the feasibility of the system to perform *ex-situ* experiments on organisms or whole  
490 communities (Miller et al., *in review*). The versatility of the system not only allows for the  
491 manipulation of temperature and salinity, but can incorporate other factors such as CO<sub>2</sub> or

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513 hypoxia (Gazeau et al., *in prep*). While this experiment used a control offset approach to produce  
514 treatment conditions, programmable parametrization of various treatment combinations can be  
515 applied depending on the question and design of the experiment. The automated component of  
516 the system reduced the logistical hurdles that can arise when performing high precision  
517 replication and regulation of experimental conditions that track real-time system variability.  
518 While the use of such a system can reduce user oversight and limitations, there is still a need for  
519 diligent operation.

520 Since the initial experiment, we have implemented a number of changes to improve the  
521 performance of the system which have been realized during a second experiment in the summer  
522 of 2022 (Fig. 6). In this experiment, the SalTexPreS was integrated to function with a deployable  
523 heat pump to simulate multiple scenarios of marine heatwave patterns over a nearly month-long  
524 experiment. In this instance, temperature regulation was vastly improved as a result of the  
525 programmable modifications made since the initial experiment. During this second experiment,  
526 the SalTexPreS mimicked 3 marine heatwave scenarios where a dynamic temperature regulation  
527 kept deviations in the 9 different mesocosms at  $< 0.5^{\circ}\text{C}$  for 94% of the time. This was an  
528 improvement to the % time of temperature regulation by  $\sim 15\%$  compared to the first  
529 experiment. During the first experiment, inconsistent flow rates and communication errors  
530 between the FerryBox and the Head PLC were the primary causes of larger deviations ( $> 2.0$   
531 salinity or  $^{\circ}\text{C}$ ) from nominal values. For example, flow rates of  $< 2 \text{ L min}^{-1}$  accounted for  $\sim 20\%$   
532 of the large deviations in temperature and salinity regulation. Simple software modifications  
533 such as 'pop-up' alert windows that warned when a lapse in communication with the FerryBox  
534 occurred (e.g., FerryBox stopped logging), and the addition of contingency coding instructions  
535 (i.e., fail-safe instructions) ensuring that the last received *in-situ* data were maintained solved

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552 most of the issues. Communication errors were easily remedied by cycling the power on a PLC,  
553 which is why pop-up alerts were an improvement to the operation. Other extraneous  
554 circumstances that could impact flow rates, such as pump failure and clogging of the seawater  
555 intake ports, are issues that need to be addressed whenever the SalTEExPreS is used. However,  
556 these are very manageable situations which can be easily mitigated by an operator.

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557 The novelty of the SalTEExPreS lies in its ability to independently regulate experimental  
558 conditions in a single experimental chamber (e.g., mesocosm). The operational data produced  
559 from this deployment are reliable, easily quantifiable, and provide the highest degree of  
560 monitoring frequency for every applied experimental condition. This study has demonstrated the  
561 system's ability to replicate dynamic nearshore environments where temperature and salinity can  
562 vary at high frequency (e.g., tidally). The system's additional capacity to mimic future scenarios  
563 by applying an amplitude offset to the natural dynamics of *in-situ* conditions is an added feature  
564 for conducting manipulative experiments. Wahl et al. (2015) described a system with a similar  
565 capability, but regulated treatment conditions by monitoring source water and adjusting that  
566 media before it was delivered to each experimental chamber. The SalTEExPreS differs in that it  
567 measures the conditions inside each experimental chamber (i.e., mesocosm) and regulates them  
568 independently based on per second measurements. This provides the flexibility to individually  
569 modulate each experimental chamber providing a broad range of versatility. The lack of  
570 infrastructure needed to set up the SalTEExPreS makes it easy to deploy and transport. As long as  
571 there is a sufficient supply of ambient water and manipulated media, there is little limit to the  
572 versatility of automated control for each mesocosm. Many research endeavors and future  
573 implementations by the SalTEExPreS have the potential to conduct a large range of experimental  
574 settings that pertain to environmental perturbations associated with climate change or other

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585 anthropogenic forcings. The operation of such a system in extreme environmental conditions has  
586 shown the durability of the manifold to endure an adverse Arctic summer and still respond  
587 without mechanical failures. With proper operation and user proficiency, this proves to be a  
588 highly sophisticated and powerful tool to be utilized for marine and aquatic perturbation  
589 experiments.

590

### 591 **Acknowledgements**

592 This study is part of the FACE-IT Project (The Future of Arctic Coastal Ecosystems –  
593 Identifying Transitions in Fjord Systems and Adjacent Coastal Areas). The authors thank [Jens](#)  
594 [Terhaar for helping with temperature projection data](#), Philipp Fischer for access to the AWIPEV  
595 data as well as AWIPEV and Kings Bay staff for helping with logistical details, shipping, and  
596 access to [the](#) marine lab facilities.

597

### 598 **Author contributions**

599 C.M. and F.G. conceptualized the frame of the paper while F.G, S.C, and P.U. designed the  
600 experimental system. P.U. programmed the software. C.M. wrote the manuscript, performed the  
601 data analysis, and constructed the figures and tables while P.U. designed [schematic figures](#). All  
602 authors participated in the operation of the system and have, thus, commented, and edited during  
603 writing.

604

### 605 **Financial support**

606 [This study was conducted in the frame of the project FACE-IT \(The Future of Arctic Coastal](#)  
607 [Ecosystems – Identifying Transitions in Fjord Systems and Adjacent Coastal Areas\)](#). FACE-IT

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609 [has received funding from the European Union’s Horizon 2020 research and innovation](#)  
610 [programme under grant agreement No 869154. Logistical and financial support was provided by](#)  
611 IPEV, The French Polar Institute [and the Foundation Prince Albert 2 of Monaco \(project: 3051,](#)  
612 <http://fpa2.org>).

**Deleted:** FACE-IT has received funding from the European Union’s Horizon 2020 research and innovation programme under grant agreement no. 869154. Partial

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#### 614 **Competing interest**

615 The authors declare no competing interests exist.

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720 **Tables**

721 **Table 1.** Experimental treatment conditions with corresponding offsets (as compared to the  
 722 control) for temperature (°C), salinity and photosynthetically active radiation (PAR; expressed as  
 723 a percentage). See section A1 and figure A1 for a full description of the temperature-salinity  
 724 relationship used to calculate salinity offsets.

<i>Treatment</i>	<i>Temperature</i>	<i>Salinity</i>	<i>PAR</i>
1	+ 3.3 °C	- 2.5 – 3.0 - S = 0.546*T + 0.490	- 25% PAR
2	+ 5.3 °C	- 5.0 – 5.5 - S = 0.877*T + 0.089	- 40% PAR
3	+ 5.3 °C	Ambient	Ambient

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<i>Treatment</i>	<i>Temperatur</i>
Cntrl.	Ambient
Trt. 1	+ 3.3 °C
Trt. 2	+ 5.3 °C
Trt. 3	+ 5.3 °C

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756 **Table 2.** Absolute mean difference between measured temperature ( $T_{\text{meas}}$ ; °C) and salinity ( $S_{\text{meas}}$ )  
 757 values against nominal values ( $T_{\text{nominal}}$  and  $S_{\text{nominal}}$ ) plus or minus the corresponding standard  
 758 deviation, in each mesocosm during the experimental period. A weighted average was used for  
 759 treatments 1 – 3 to account for the initial 5-day incremental increase. Triplicate mesocosms per  
 760 condition are expressed as a, b and c. Water mixture indicates the types of media supplied to  
 761 each treatment, denoted with an 'x'.

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Treatment	Mean diff		Water mixture			
	Abs( $T_{\text{meas}} - T_{\text{nominal}}$ )	Abs( $S_{\text{meas}} - S_{\text{nominal}}$ )	Cold	Ambient	Warm	Fresh
Control a	0.275 ± 0.39	–	x	x		
Control b	0.291 ± 0.36	–	x	x		
Control c	0.223 ± 0.36	–	x	x		
Treatment 1a	0.126 ± 0.31	0.116 ± 0.31		x	x	x
Treatment 1b	0.142 ± 0.29	0.148 ± 0.22		x	x	x
Treatment 1c	0.145 ± 0.33	0.171 ± 0.33		x	x	x
Treatment 2a	0.111 ± 0.29	0.357 ± 0.74		x	x	x
Treatment 2b	0.133 ± 0.29	0.149 ± 0.26		x	x	x
Treatment 2c	0.196 ± 0.38	0.128 ± 0.25		x	x	x
Treatment 3a	0.109 ± 0.27	–		x	x	
Treatment 3b	0.112 ± 0.27	–		x	x	
Treatment 3c	0.106 ± 0.28	–		x	x	

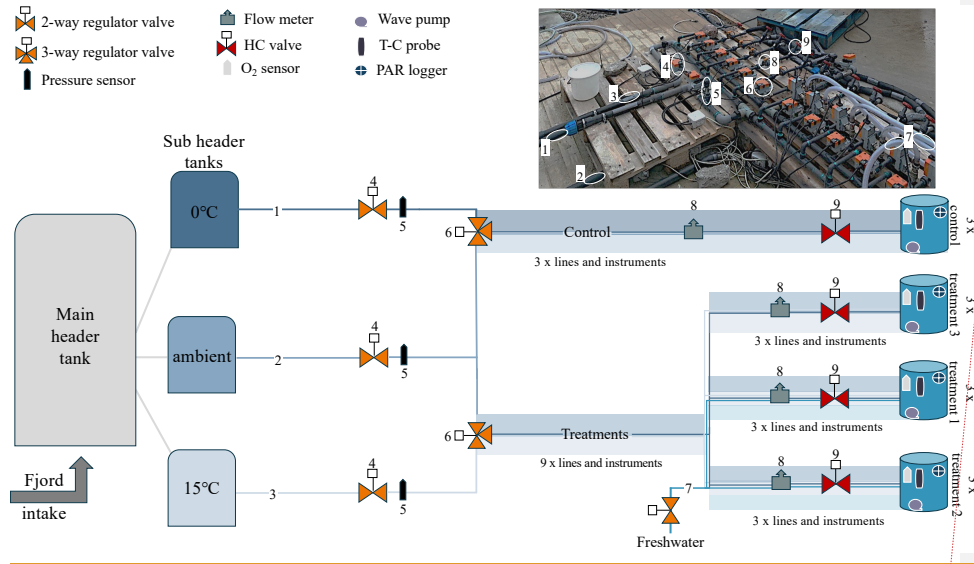
Treatment	Mean diff	
	Abs( $T_{\text{meas}} - T_{\text{set}}$ )	Abs( $S_{\text{meas}} - S_{\text{set}}$ )
Cntrl. a	0.275 ± 0.39	–
Cntrl. b	0.291 ± 0.36	–
Cntrl. c	0.223 ± 0.36	–
Trt. 1a	0.126 ± 0.31	0.116 ± 0.31
Trt. 1b	0.142 ± 0.29	0.148 ± 0.22
Trt. 1c	0.145 ± 0.33	0.171 ± 0.33
Trt. 2a	0.111 ± 0.29	0.357 ± 0.74
Trt. 2b	0.133 ± 0.29	0.149 ± 0.26
Trt. 2c	0.196 ± 0.38	0.128 ± 0.25
Trt. 3a	0.109 ± 0.27	–
Trt. 3b	0.112 ± 0.27	–
Trt. 3c	0.106 ± 0.28	–

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### Figures



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**Figure 1.** Piping schematic of the SaTExPreS which includes the mixing and regulation

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manifold. Items 1 – 3 depict the main seawater inlets from the **chilled, ambient, and warmed** sub-

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header tanks located in the Kings Bay Marine Laboratory. Seawater from each sub-header tank

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moves through a 2-way regulator (4) valve followed by a pressure sensor (5) before splitting into

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individual lines that lead to all 12 3-way regulator valves (6), each assigned to a single

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mesocosm. For treatments 1 and 2, the freshwater inlet (clear tube; item 7) passes through a 2-

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way regulator valve before mixing with the ambient and warmed seawater lines. Flow rates are

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then measured (8) post-mixing, and final flow rates are set using a hand-crank (HC) red valve

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(9). **The shaded regions in the schematic indicate that mixed media lines and instruments occur**

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**3x or 9x times. T-C probe is the temperature-conductivity probe and the PAR logger measures**

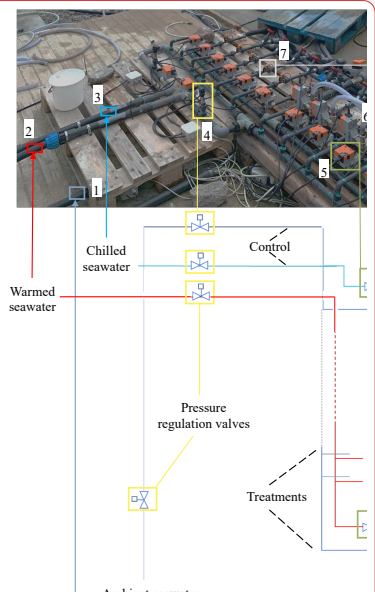
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**the photosynthetically active radiation. Photos of mesocosms and the sensors inside can be found**

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**in the appendix (Fig. A6). Table A1 provides the parts list for the items shown in this figure.**

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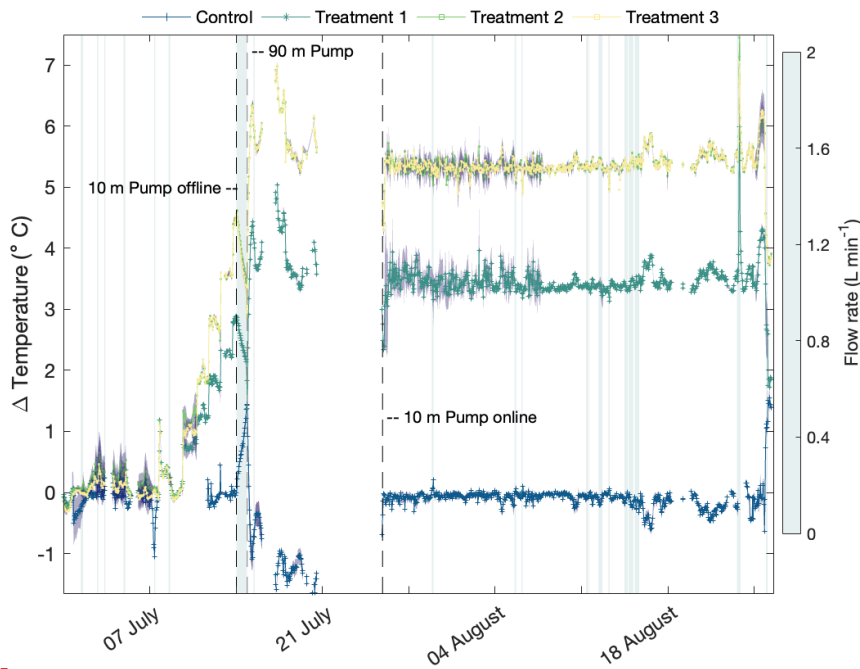
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811 **Figure 2.** The hourly mean (across triplicated mesocosms) temperature offsets of all applied  
 812 conditions. For control mesocosms (in blue), offsets were calculated against *in-situ*  
 813 measurements (FerryBox). For the three experimental treatments (dark green, light green, and  
 814 yellow for treatments 1, 2 and 3, respectively), offsets were estimated against the mean control  
 815 values. The purple shaded region around the mean is the standard deviation. The heatmap  
 816 isoclines (blue-grey shaded regions) are instances when flow rates were  $\leq 2 \text{ L min}^{-1}$  (threshold to  
 817 avoid large deviations  $> 2.0$  salinity or  $^{\circ}\text{C}$ ). Dashed black lines indicate periods when the pump  
 818 at 10 m depth and 90 m depth were used to feed the sub-header tanks. The time presented is the  
 819 duration of the experimental deployment.

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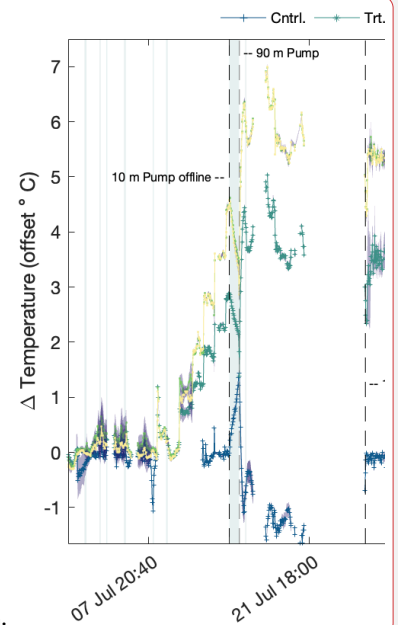
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859 **Figure 3.** Mean (across triplicated mesocosms) temperature (°C; **a**) and salinity (**b**) values  
 860 measured every minute over a 60 d period (including 6 day period before the start of the  
 861 experiment) for the control (blue), and for treatments 1 – 3 (dark green, light green, and yellow,  
 862 respectively).

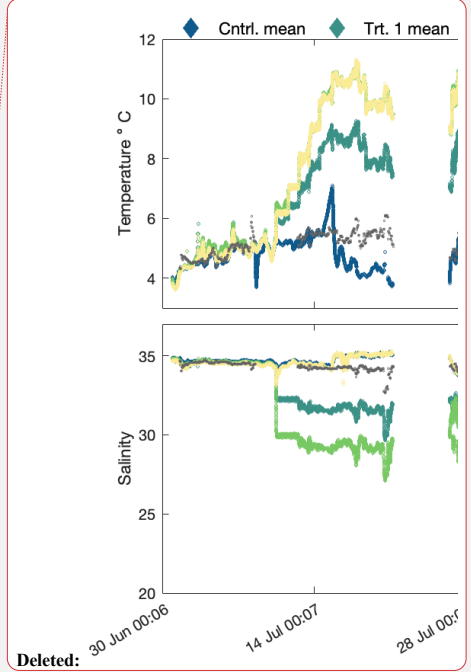
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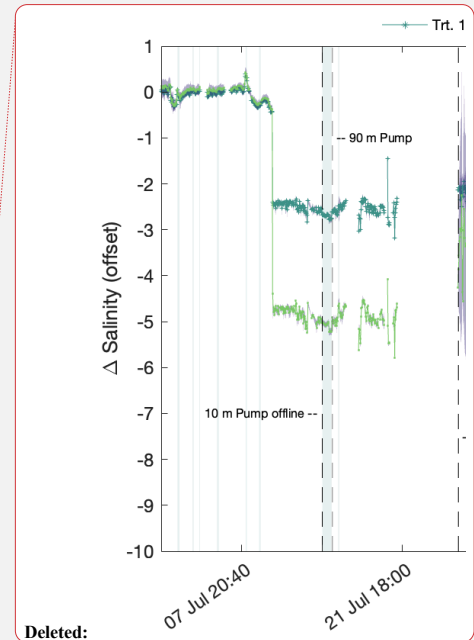
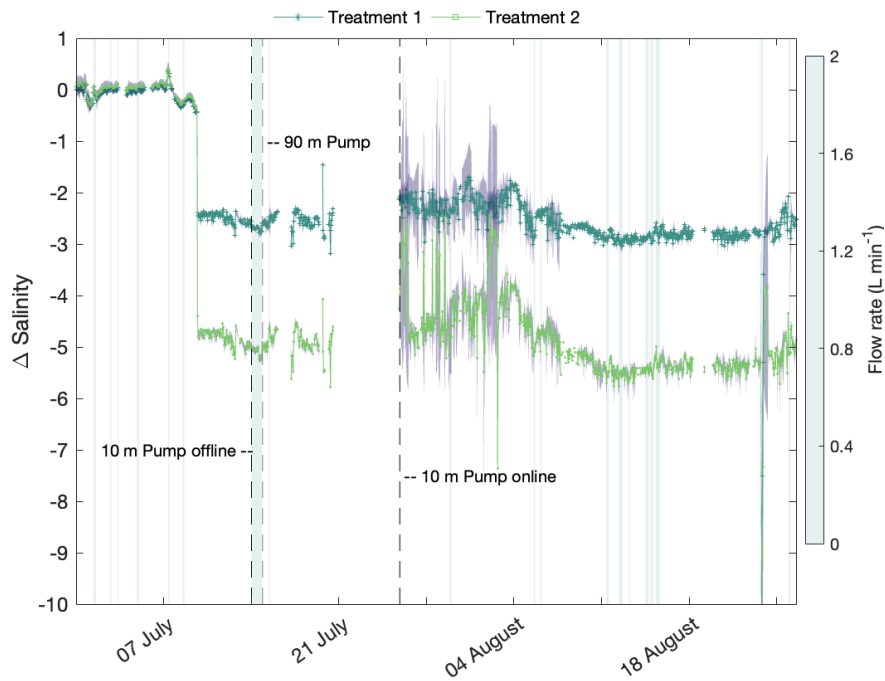
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Deleted: temperature (a) and salinity (b) for all conditions including those from the FerryBox (dark grey circles) for the entire deployment.





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 873 **Figure 4.** The hourly mean (across triplicated mesocosms) salinity offsets for the experimental  
 874 period. Dark green is treatment 1 and light green is treatment 2. The purple shaded region around  
 875 the mean is the standard deviation and the heatmap isoclines (blue shaded regions) are the  
 876 instances when flow rates  $\leq 2 \text{ L min}^{-1}$ . Dashed black lines indicate periods when the pump at 10  
 877 m depth and 90 m depth were used to feed the sub-header tanks.

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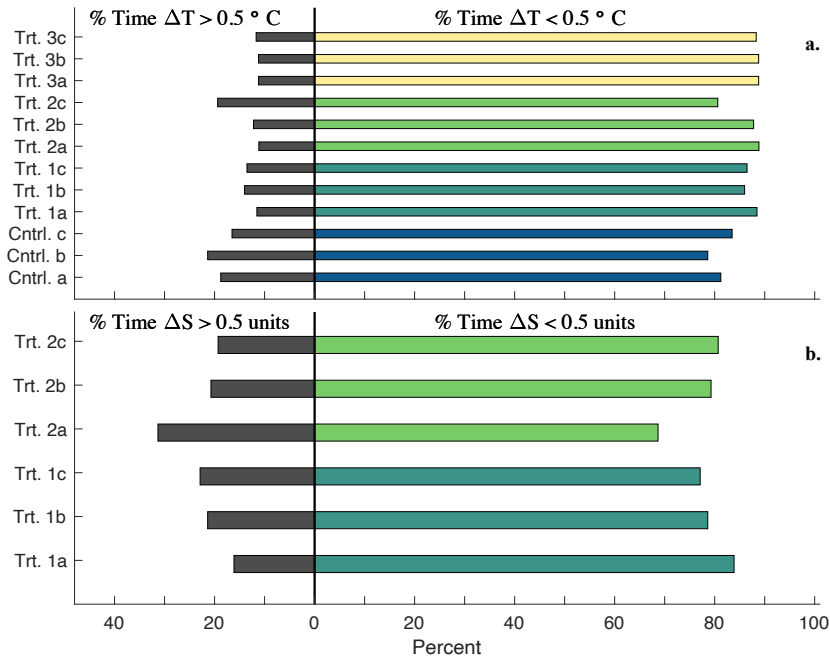
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889 **Figure 5.** Percent time each mesocosm experienced a deviation > (black bars) or < (colored  
890 bars) 0.5°C ( $\Delta T$ ; **a**) or 0.5 in salinity ( $\Delta S$ ; **b**) when flow rates were above 2 L min<sup>-1</sup>. Cntrl. and  
891 Trt. abbreviations are the control and treatments, respectively. This excludes the period when  
892 using the 90 m pump (12 d), but accounts for 42 days out of the 54-day experiment. Bar color  
893 indicates different treatment groups, as shown on the y-axes.

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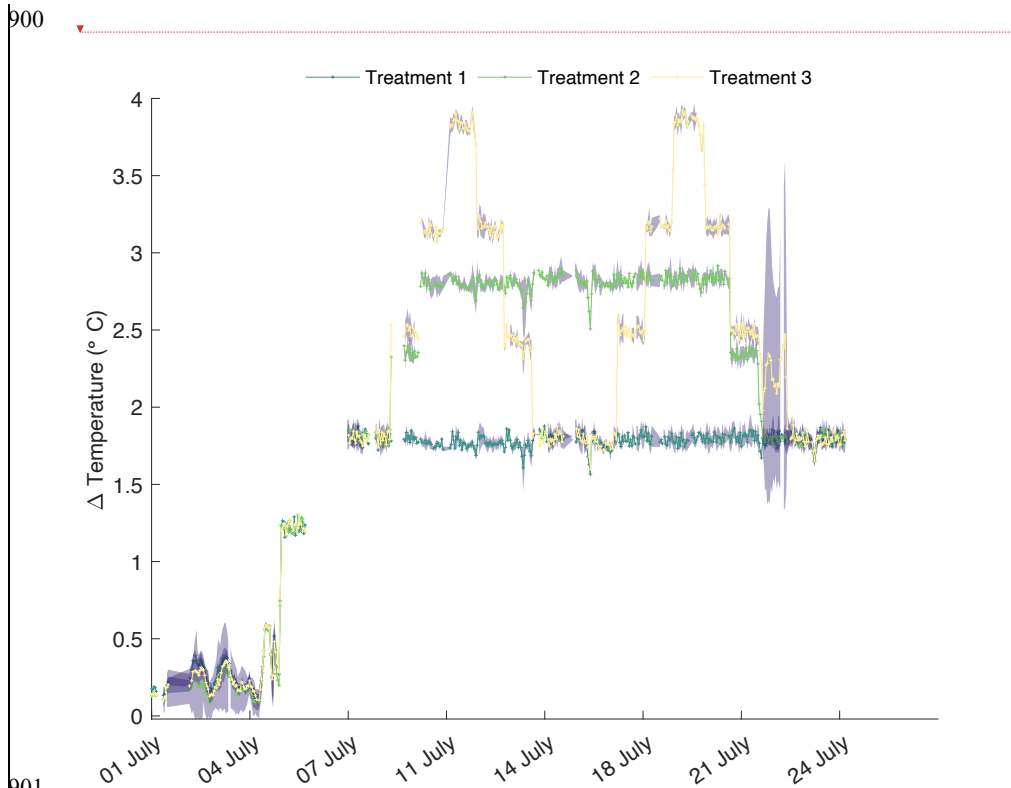
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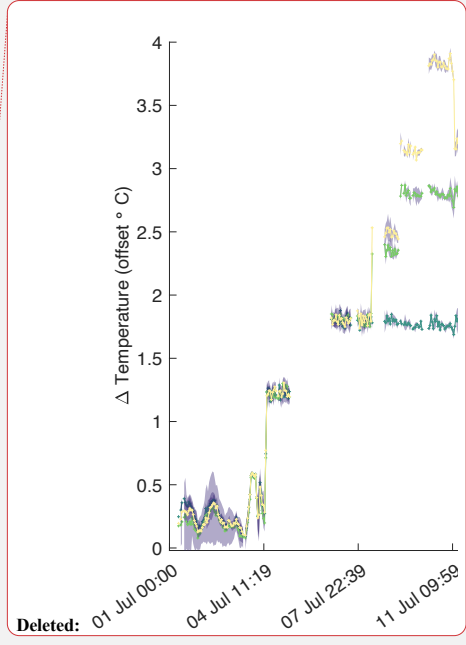
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902 **Figure 6.** The hourly mean temperature offsets ( $\Delta$  Temperature) during the 2<sup>nd</sup> deployment of  
 903 SalTEPreS in the summer of 2022 in Tromsø (Norway) performing a variation of heatwave  
 904 scenarios with three experimental treatments 1 – 3. **Treatment 1 is a constant high temperature (+**  
 905 **1.76°C), treatment 2 is a low frequency (1 heatwave) and medium magnitude offset (+ 2.81°C),**  
 906 **while treatment 3 is a high frequency (2 heatwaves) and magnitude offset (+ 3.86°C).** The purple  
 907 shaded region around the mean is the standard deviation.

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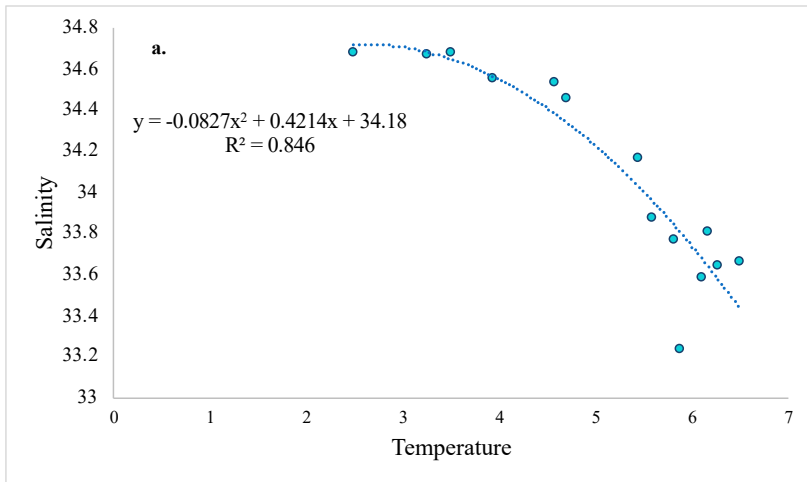
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914 **Appendix**

915 **A1. Calculation of Salinity Offset**

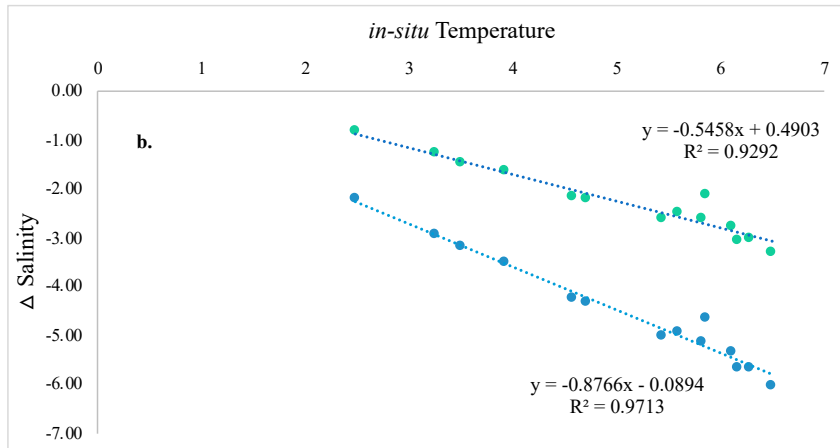
916 In the summer of 2020—weeks 22 to 35—the mean temperature at 11 m displayed a range from  
917 2.48 – 6.28, with salinity values ranging from 34.67 measured at the minimum 2.48°C and 33.63  
918 measured at 6.28°C (Fig. A1a). The correlation was best fit with a 2<sup>nd</sup> order polynomial. To  
919 project the salinity offset at a future temperature based on this 2<sup>nd</sup> order polynomial fit,  
920 temperatures of + 3.3 and 5.3°C (SSP2-4.5 and SSP5-8.5, respectively) were added to *in-situ*  
921 fjord temperatures and salinity was calculated based on the 2<sup>nd</sup> order polynomial. These  
922 estimated salinity values were then subtracted from the mean salinity values observed (y-axis,  
923 Fig. A1a) in summer 2020 in order to calculate a delta salinity value for the SSP2-4.5 and SSP5-  
924 8.5 scenarios. The relationship between these estimated delta salinity values and the mean *in-situ*  
925 temperature (y-axis, Fig. A1a) displayed a robust linear relationship (Fig A1b).



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 933 **Figure A1.** Relationship between temperature and salinity in summer 2020 weeks 22 – 35 in Ny-  
 934 Ålesund, Svalbard (a). Relationship between estimated delta salinity and *in-situ* temperature,  
 935 where delta salinity was calculated as the difference between the current mean salinity and the  
 936 salinity estimated at the temperature increase projected for SSP2-4.5 (green dots) and SSP5-8.5  
 937 (blue dots) scenarios (b).

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**Table A1. Parts list with manufacturer model numbers.**

Group	Item	Supplier/manufacturer	Model / details	Quantity
<b>Hydraulic system</b>				
	Mesocosms	home made	1000 L fiber glass	12
	Seawater pump	NPS, BradFord, UK	Albatros F13T	1
	PVC-U tubing and fittings		20mm, 32mm & 50mm diameter	–
	Insulated flexible hose		19mm diameter	100 m
<b>Sensors</b>				
	Conductivity / temperature	Aqualabo, Champigny sur Marne, France	PC4E	12
	Oxygen	Aqualabo, Champigny sur Marne, France	PODOC	12
	Pressure	Siemens, Munich, Germany	7MF1567-3BE00-1AA1	3
	Flow rate	IFM, Essen, Germany	SV3150	12
<b>Actuators</b>				
	Pressure regulation valves	BELIMO, Hinwil, Switzerland	R2025-10-S2 with LR24A-SR motor	3
	Temperature regulation valves	BELIMO, Hinwil, Switzerland	R3015-10-S2 with LR24A-SR motor	12
	Salinity regulation valves	BELIMO, Hinwil, Switzerland	R2015-10-S2 with LR24A-SR motor	6
<b>Automation cabinet</b>				
	Cabinet	Fibox, Espoo, Finland	FIB8120017N	1
	Security switch	KRAUS-NAIMER, Karlsruhe, germany	KNA002245	1
	12 vdc power supply	TDK Lambda, New York, USA	LAMDRL30-12-1	1
	24vdc power supply	TDK Lambda, New York, USA	LAMDRB240-24-1	1
	PLC	Industrial Shields, Barcelona, Spain	Mduino-42+	4
	Ethernet switch	HIRSCHMANN-INET, Neckartenzlingen, Germany	HIR942132002	1

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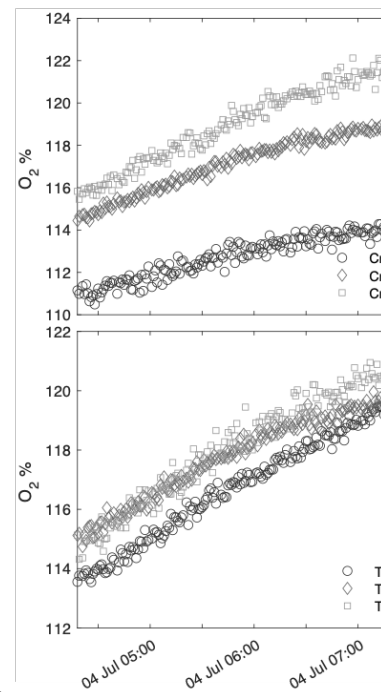
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## A2. Temperature and Salinity Regulation

Accurate temperature and salinity regulation was managed using the software PID (proportional integral derivative) controller on the corresponding Programmable Logic Controller (PLC). The PLC operated in PoE mode (power over ethernet) which builds a local area network (LAN) enabling use of Ethernet data cables to carry electrical power. The PID controller measures the difference between the measured value and the nominal value (i.e., the error). This calculates the position and adjustment of the valve opening by multiplying the error, the integral of this error, and the derivative of the error over time, by previously determined coefficients  $K_p$  (proportional gain),  $K_i$  (integral gain) and  $K_d$  (derivative gain), respectively. These coefficients were obtained experimentally using the empirical method of Ziegler & Nichols (1943). These coefficient values may differ from one condition to another.

### A2.1. Pressure and Flow Regulation

Each sub-header tank inlet line of ambient, chilled and warmed seawater had its own pressure regulation system enabling equivalent pressure levels to be maintained. This regulation process aided in the ability to adjust flow rates for all mesocosms by using the hand-crank valves (Fig. 1). The system consisted of an analog pressure sensor (Siemens© 7MF1567-3BE00-1AA1) and a two-way analog valve (BELIMO© R2025-10-S2 with LR24A-SR motor). The pressure sensors were placed in-line directly after water from each sub-header tank passed through a regulator valve. The sensor ensured that pressure for each line was maintained at 0.3 bars by transmitting data to the system which then regulated the valve opening position of the incoming flow. A nominal pressure for all three sensors was predetermined during flow rate test trials. This



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Figure A2. Oxygen evolution for each mesocosm separated by treatment.

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982 process took place during the setup of the system where the valve opening was adjusted using a  
983 PID regulator (see A2) to maintain the defined nominal pressure.

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## 985 A2.2 Automation

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986 The automation was performed using 4 Industrial Arduino-based PLCs (Industrial shields©

987 Mduino-42+), with an individual PLC regulating the control and each treatment 1 – 3,

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988 respectively. Each PLC was responsible for logging data and regulating a specific experimental

989 condition. The PLC regulating the control—identified as the Head PLC—was the primary device

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990 responsible for communication with the branched PLCs and the monitoring computer (Fig. A2).

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991 All monitoring was performed on a PC Windows application (Section A3) and responsible for:

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992 (1) reading data received from the PLCs, (2) reading *in-situ* data received from the internet, (3)

993 displaying live data, (4) logging data and sending it to an FTP server, and (5) sending settings

994 and commands to the PLCs. Communication between the PLCs and the PC was ensured using

995 http WebSocket protocol on RJ45 ethernet cables. The communication between the PLCs and the

996 conductivity-temperature and oxygen sensors, flow rate sensors, and regulation valves was

997 executed using a half duplex RS485 (2 wires) protocol, with an analog 4-20mA and an analog 0-

998 10V signal, respectively. All PLCs and wired communication lines were housed in an electrical

999 box installed to an IP68 Fibox enclosure with a 400 V (3P+N+E) 32 A security switch (Fig. A6).

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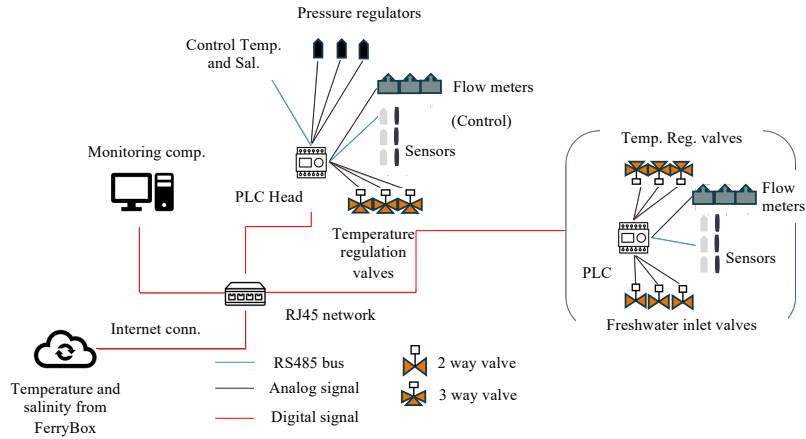
1000 All the automation elements use low tension (12 Vdc or 24 Vdc) through circuit breakers and

1001 fuses. The electrical box was protected with a 220 V socket.

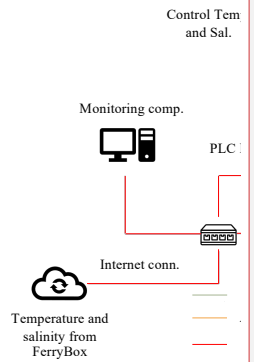
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## Automation Hardware Architecture



## Automation Hardware Architecture



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Figure A2. Diagram and flow-chart of the automation system.

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1026 **A3. Software Development**

1027 The code for the application was written in C/C++. The code uses publicly available Arduino  
1028 libraries (<https://www.arduino.cc/reference/en/libraries/>) as well as originally designed libraries.  
1029 All code is available on Github (<https://github.com/purrutti/FACEIT>). The code is divided into  
1030 two pathways: ‘Master.ino’ for the Head PLC, and ‘Regul\_condition.ino’ for the Branched  
1031 PLCs. A description of the main functions applied in the code for programming the system  
1032 regulation and features are listed in Table A3.

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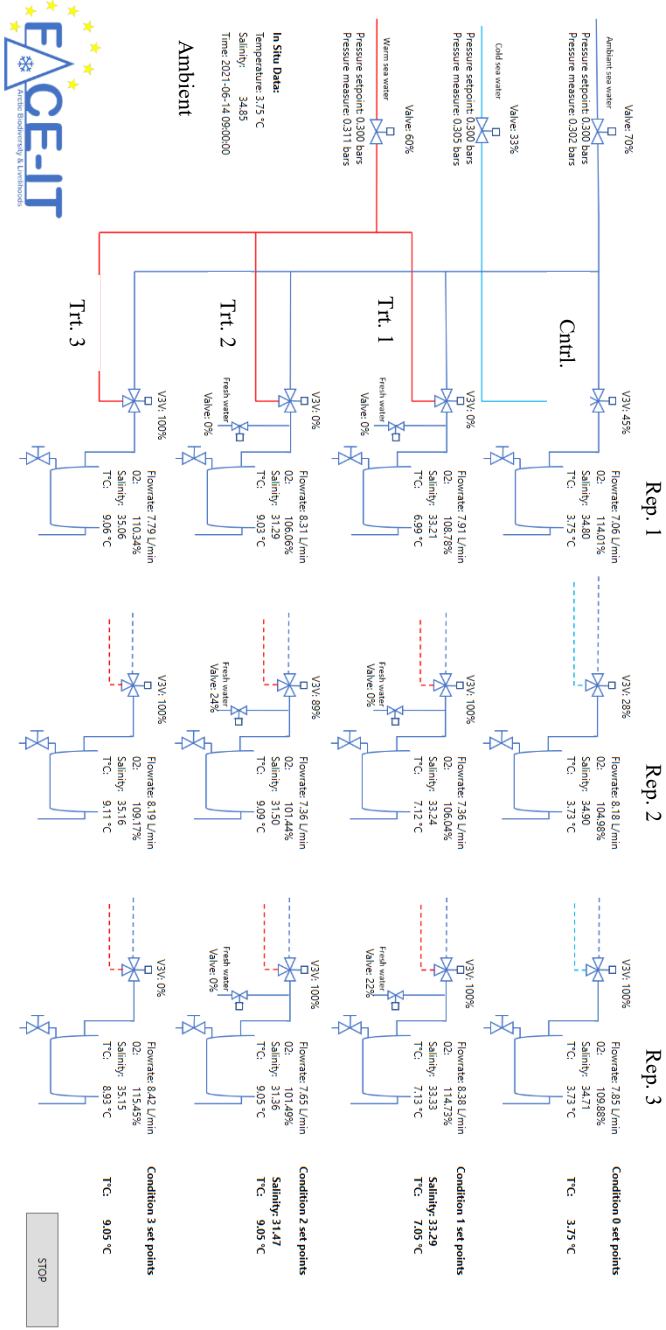
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**Table A3.** Functions used for programming of software.

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Function	Operation	Auxiliary field Sender ID	Auxiliary field Command #
<i>RTC/read()</i>	The PLCs are equipped with a RTC chip and battery to keep track of the date. Once set on commissioning, RTC/read() returns the current date and time.  This function loops through each sensor connected on the RS485 bus. Each Mesocosm has two sensors (O2 and Conductivity/Salinity), so each PLC has 6 sensors connected on its bus.  <i>readMesosensors()</i> - O2 sensors have addresses ranging from 10 to 12, for mesocosms 0 to 2 of the scenario, respectively. - PC4E sensors have addresses ranging from 30 to 32, for mesocosms 0 to 2 of the scenario, respectively. - Sensors are requested individually and in sequence. A request is made every 200 ms.		
<i>webSocketLoop()</i>	This is a callback function responsible for dealing with the WebSocket communication. The master PLC is the WebSocket server. It listens to slave PLCs requests and to the monitoring PC requests. Requests are JSON formatted. They always contain <i>method/field</i> : <i>senderID</i> (ID of the entity sending the request), <i>command</i> (ID of the requested entity), <i>command</i> (command type of the request). They optionally can also contain a « <i>time</i> » field. Unlike the <i>timestamp</i> (number of seconds since 01-01-1970)	Head PLC (ID = 0) Branch PLC (ID = 1-3) Monitoring PC (ID = 4)	Request params: <i>sepspans</i> , <i>PID settings</i> (# = 0) Request data: <i>measurement values</i> , <i>regulation outputs</i> (# = 1) Send Params: response to a « request params » request (# = 2) Send Date: response to a « request data » request (# = 3) Calibrate sensor: request for calibrating sensor to specified value (# = 4) Request Head data: specific data measured by Head PLC (pressure & flow rates ) (# = 5) Send Head data: a response to a « request Head data » request (# = 6)
<i>regulationTemperature()</i>	This function is responsible for the temperature regulation of the mesocosm. It sets the corresponding three-way valve position using a 0-10V analog signal. The function first checks if the regulation is in « manual override » mode. If so, it applies the override setpoint. If not, it reads the temperature measure in the mesocosm, compares it with the setpoint, and uses the PID settings to set the valve position.		
<i>checkMesocosms()</i>	This function loops through every mesocosm every 200 ms and reads analog signals (i.e. flow rates and pressure readings).		
<i>regulationPressure()</i>	This function is responsible for the pressure regulation of the mesocosm. It sets the corresponding three-way valve position using a 0-10V analog signal. The function first checks if the regulation is in « manual override » mode. If so, it applies the override setpoint. If not, it reads the pressure measure in the mesocosm, compares it with the setpoint, and uses the PID settings to set the valve position.		
<i>pinWriteSD()</i>	Master PLC is equipped with a microSD card, on which data from all mesocosms is logged every 5 seconds, in one csv file per day. This is for security only, as the microSD card is not easy to remove from the PLC casing. It should not be removed before the end of the experiment.		
<i>regulationSalinity()</i>	This function is responsible for the salinity regulation of the mesocosm. It sets the corresponding three-way valve position using a 0-10V analog signal. The function first checks if the regulation is in « manual override » mode. If so, it applies the override setpoint. If not, it reads the salinity measure in the mesocosm, compares it with the setpoint, and uses the PID settings to set the valve position.		



1056 **Figure A3.** Application interface displaying real-time monitoring of ambient conditions as well  
1057 and control (Cntrl.), and treatment (Trt.) conditions for each replicate (Rep.) in each mesocosm.

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1080 **A4. Menu bar of PC application**

1081 From the interface, the user sets the temperature condition and associated salinity offset, IP  
1082 address and logging parameters, sensor calibration settings, and **nominal** pressure (Fig. A4).  
1083 Within the menu bar several tabs permit the setup of the project: file, settings, maintenance, and  
1084 data. Under 'file' the system can be manually connected to, or disconnected from, the PLCs.  
1085 Connection is usually maintained automatically. The 'settings' tab displays the application and  
1086 experimental setting options (Fig. A4.1 a – c). All the settings of the project are stored on the  
1087 computer (found in 'application settings') that is running the application, which include:

- 1088 i. *Master IP address*: The IP Address of the Master PLC (centralizing all the data).
- 1089 ii. *Data Query Interval*: Frequency of queries from the application to the master PLC.
- 1090 iii. *Data Log Interval*: Number of minutes between logs to file.
- 1091 iv. *Data Base File Path*: Directory and base filename of the csv data files.
- 1092 v. *FTP Username, Password, Path*: FTP settings for sending the data file every hour.
- 1093 vi. *InfluxDB Settings*: For Live Monitoring and local storage of the data.

1094 Under 'experimental settings', the programmed specificities and regulation of the treatment  
1095 conditions can be adjusted. This includes programming the **nominal** pressure (all main inflow  
1096 lines), temperature and the salinity-temperature relational equation (on a different tab selected  
1097 from dropdown), as well as adjusting the  $K_p$ ,  $K_i$  &  $K_d$  coefficients for the regulation (see section  
1098 2.3.1). The **nominal** temperature is provided by the data received from the ferry-box, however  
1099 this can be overridden if needed. The « Save to PLC » button sends the values to the  
1100 corresponding PLC and saves the data, while the « Load from PLC » button loads the settings  
1101 from the PLC. For the purposes of this experiment, the **nominal** salinity was calculated based on  
1102 a delta salinity for treatments 1 and 2 which were derived from the linear relationship with

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1108 temperature (see section 2.3.1). This can also be overridden if needed by selecting the manual  
1109 override box.

1110         The ‘maintenance’ tab is where sensor calibration and communication ‘Debug’  
1111 operations can be executed (Fig. A4 d, e). Calibration can be performed for each sensor deployed  
1112 in each mesocosm, and uses a 2-point calibration for temperature and % oxygen. The salinity  
1113 calibration is done by setting the conductivity value corresponding to a temperature of 25°C  
1114 rather than the *in situ* measured temperature. The conductivity value is programmed as  $\mu\text{S cm}^{-1}$ .  
1115 The communication process for sensor calibration is between 5 to 10 seconds. The final option in  
1116 the menu is the ‘data’ tab which displays the historical and live data. The historical data can be  
1117 interfaced to an html site if desired.  
1118

Experiment Settings

Number of Address: 16 (KES, 0)  
 Control Channel: 1

Control Channel: 5  
 Control Channel Name: ControlChannel, Mod, Dev

IP: 192.168.1.100  
 Username: root@kali:root  
 Password: root@kali:root  
 FTP Directory Path: /usr/bin/nc

Website: http://www.102401.org/nc/nc64bit/nc64bit.exe  
 Host: 192.168.1.100  
 Port: 4444  
 User: root  
 Pass: root

Save Cancel

Experiment Settings

Control Condition: v

Pressure regulation

Pressure setpoint: 0.00

Temperature regulation

Temperature setpoint: 3.75

Kp: 0.00  
 Ki: 0.00  
 Kd: 0.00

Manual Override: 0 %

Load from PLC Save to PLC Cancel

Experiment Settings

Condition 1

Salinity regulation

delta Salinity = [-0.54158] \* Ambient TC + [0.4903]

Update

delta Salinity setpoint: -1.56  
 Salinity setpoint: 33.29

Temperature regulation

delta TC setpoint: 3.30  
 Temperature setpoint: 7.05

Kp: 10.00  
 Ki: 50.00  
 Kd: 0.00

Manual Override: 0 %

Load from PLC Save to PLC Cancel

Experiment Settings

Communication Being

Request sent: [Command: "cond?0,read?0"]

Response received: [Response: "3,cond:0,read:0,dev:1,198015,uspb?0,35,temps?0,pc:10,pc:10,13,54611"]

Request: [Request: "temp:3,171,171,cond:55892,26,cal:124,67,268,now:7,289924,uspb?0,pc:10,pc:10"]

Response: [Response: "temp:3,171,171,cond:55892,26,cal:124,67,268,now:7,289924,uspb?0,pc:10,pc:10"]

Experiment Settings

Calibration

Measurement: 32.7 °C

Calibration standard 1: Set Offset  
 Calibration standard 2: Set Slope

Request sent: [Command: "cond?0,read?0"]

Response received: [Response: "3,cond:0,read:0,dev:1,198015,uspb?0,35,temps?0,pc:10,pc:10,13,54611"]

Experiment Settings

Calibration

Measurement: 32.7 °C

Calibration standard 1: Set Offset  
 Calibration standard 2: Set Slope

Request sent: [Command: "cond?0,read?0"]

Response received: [Response: "3,cond:0,read:0,dev:1,198015,uspb?0,35,temps?0,pc:10,pc:10,13,54611"]

Experiment Settings

Calibration

Measurement: 32.7 °C

Calibration standard 1: Set Offset  
 Calibration standard 2: Set Slope

Request sent: [Command: "cond?0,read?0"]

Response received: [Response: "3,cond:0,read:0,dev:1,198015,uspb?0,35,temps?0,pc:10,pc:10,13,54611"]

Experiment Settings

Calibration

Measurement: 32.7 °C

Calibration standard 1: Set Offset  
 Calibration standard 2: Set Slope

Request sent: [Command: "cond?0,read?0"]

Response received: [Response: "3,cond:0,read:0,dev:1,198015,uspb?0,35,temps?0,pc:10,pc:10,13,54611"]

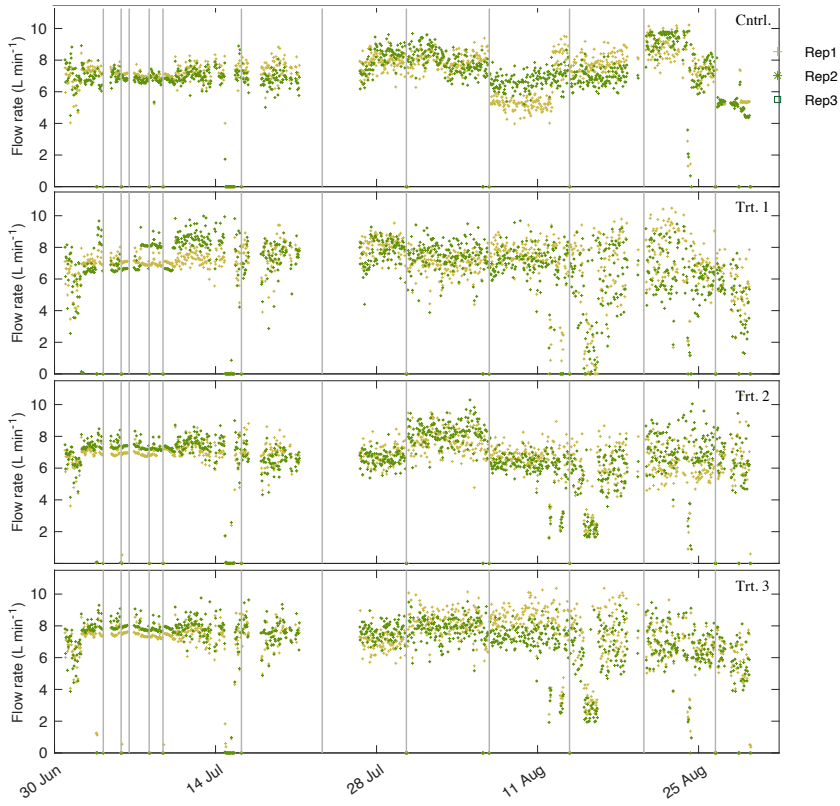


1120 **Figure A.4.** Operation windows for the application and experimental settings (a-c). These  
1121 windows are found under the 'settings' tab. Operation windows for sensor calibration and  
1122 debugging (d, e). These are found under the 'maintenance' tab.

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1146 **Figure A5.** Flow rates for control and treatments 1-3 for the entirety of the system deployment.

1147 Black vertical lines are when incubations were performed and the system shut-off for a period of  
1148 3 h. Flow rates went to zero at these times.

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1156 **Figure A6.** All 12 mesocosms are displayed (upper left photo) with the inside of one mesocosm  
1157 (right photo) showing the oxygen (silver) and temperature/conductivity sensors along with the  
1158 photosynthetically active radiation (PAR) logger (bottom right photo).

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1166 **Figure A7.** Electrical cabinet used for SalTExPreS

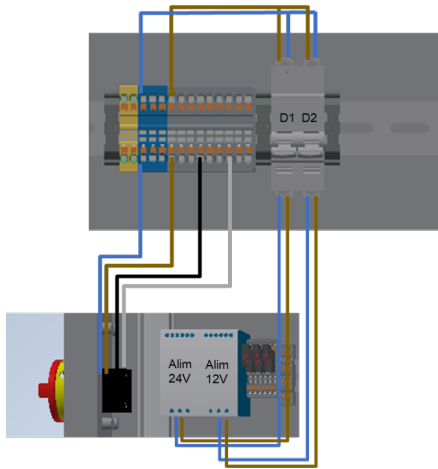
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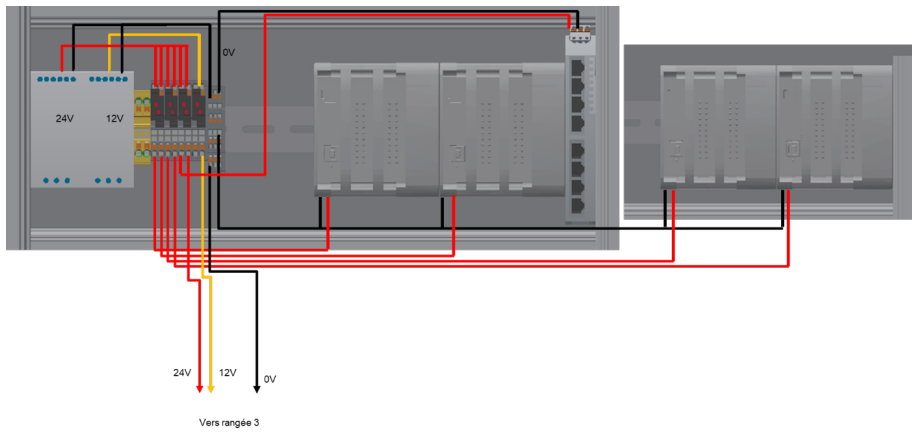
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D1: Alim 24Vdc  
D2: Alim 12Vdc

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1174 **Figure A8.** Electrical schematic for wiring within the electrical box.

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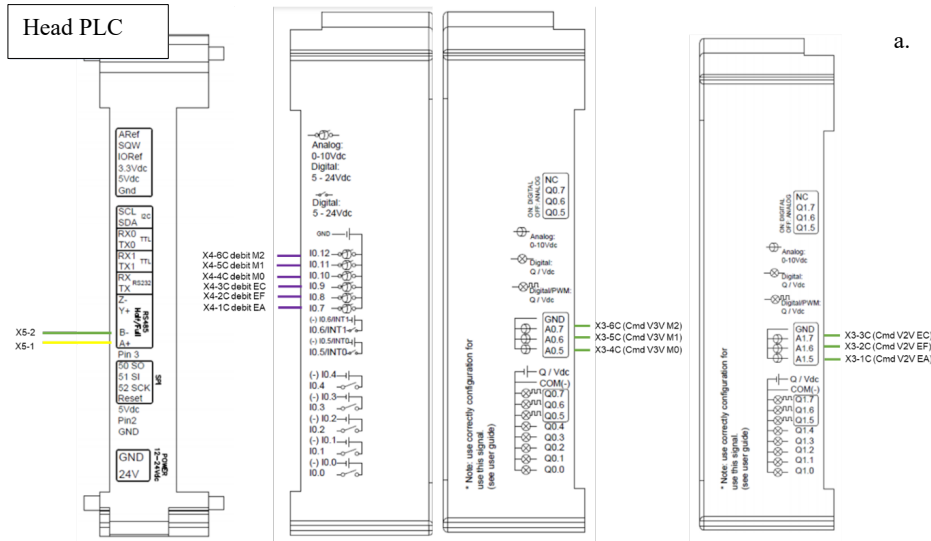
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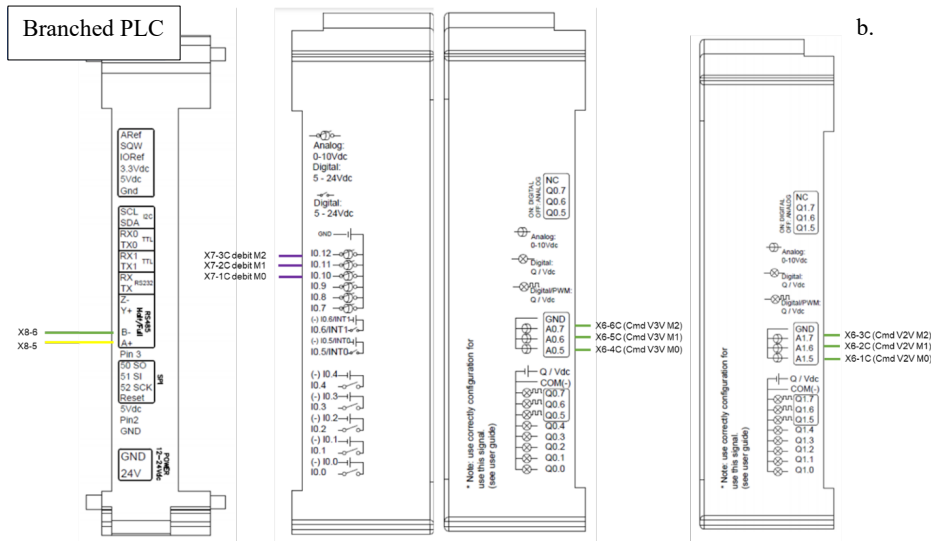
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1183 **Figure A9.** PLC controller diagram for Head (a) and Branched (b) operations.

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Moved up [2]: Table A2. Parts list with manufacturer model numbers.

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Group	Item	Supplier/man
<b>Hydraulic system</b>		
	Mesocosms	home r
	Seawater pump	NPS BradForc
	PVC-U tubing and fittings	
	Insulated flexible hose	
<b>Sensors</b>		
	Conductivity / temperature	Aquala Champigny s Franc
	Oxygen	Aquala Champigny s Franc
	Pressure	Sieme Munich, G
	Flow rate	IFM Essen, Ge
<b>Actuators</b>		
	Pressure regulation valves	BELIM Hinwil, Swi
	Temperature regulation valves	BELIM Hinwil, Swi
	Salinity regulation valves	BELIM Hinwil, Swi
<b>Automation cabinet</b>		
	Cabinet	Fiboy Espoo, Fi
	Security switch	KRAUS-N Karlsruhe, g
	12 vdc power supply	TDK Lar New York
	24vdc power supply	TDK Lar New York
	PLC	Industrial S Barcelona
	Ethernet switch	HIRSCHMAN Neckartenz Germa

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