

1 **Title:** An Autonomous Flow through Salinity and Temperature Perturbation Mesocosm System
2 for Multi-stressor Experiments

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34 **Abstract**

35 The rapid environmental changes in aquatic systems as a result of anthropogenic forcings are
36 creating a multitude of challenging conditions for organisms and communities. The need to
37 better understand the interaction of environmental stressors now, and in the future, is
38 fundamental to determining the response of ecosystems to these perturbations. This work

39 describes an automated ex-situ mesocosm perturbation system that can manipulate several

40 variables of aquatic media in a controlled setting on land. This perturbation system was deployed

41 in Kongsfjorden, (Svalbard) where ambient water from the fjord was heated and mixed with

42 freshwater in a multifactorial design to investigate the response of mixed kelp communities in

43 mesocosms to projected future Arctic conditions. The system employed an automated dynamic

44 offset scenario where a nominal temperature increase was programmed as a set value above real-

45 time ambient conditions in order to simulate future warming. The freshening component was

46 applied in a similar manner where the decrease in salinity was coupled to track the temperature

47 offset based on a temperature-salinity relationship in the fjord. The system functioned as an

48 automated mixing manifold that adjusted flow rates of warmed and chilled ambient seawater,

49 with unmanipulated ambient seawater and freshwater delivered as a single source of mixed

50 media to individual mesocosms. These conditions were maintained via continuously measured

51 temperature and salinity in all 12 mesocosms (1 ambient-control and 3 treatments, all in

52 triplicates) for 54 days. System regulation was robust as median deviations from setpoint

53 conditions were < 0.15 for both temperature (°C) and salinity across the 3 replicates per

54 treatment. Regulation further improved during a second deployment that mimicked 3 marine

55 heatwave scenarios where a dynamic temperature regulation held median deviations to < 0.036

56 °C from the setpoint for all treatment conditions and replicates. This perturbation system has the

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77 potential to be implemented across a wide range of conditions to test single or multi-stressor
78 drivers (e.g., increased temperature, freshening, high CO₂) while maintaining natural variability.
79 The automated and independent control for each experimental unit (if desired) provides a large
80 breadth of versatility with respect to experimental design.

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82 1 Introduction

83 The persistent burning of fossil fuels since the industrial revolution has radically increased
84 atmospheric CO₂. This has led to an enhanced greenhouse effect resulting in a multitude of
85 changing climatic elements such as increasing sea surface temperature (Bindoff et al., 2019). In
86 fjord systems, the confluence of increased fluvial inputs, glacier and permafrost meltwater,
87 stratification and water mass intrusion, as well as increased sea surface temperatures can create
88 periods of extreme physicochemical conditions for nearshore benthic and pelagic marine
89 communities (Bhatia et al., 2013; Poloczanska et al., 2016; Divya and Krishnan, 2017; Bindoff et
90 al., 2019). As ocean changes progress, the need to better understand the effects of combined
91 stressors (e.g., increased temperature and freshening) on marine communities is essential to
92 understand how community function and species richness will be affected as assemblages adjust
93 to new environmental conditions (Kroeker et al., 2017; Wake, 2019; Orr et al., 2020).
94 Methodological approaches to assessing and characterizing the response of organisms and
95 community assemblages to future ocean change is often pursued by conducting *ex-situ*
96 experiments, utilizing natural analogues (e.g., CO₂ vents), or performing space-for-time
97 substitution (when spatial phenomena are used to model temporal changes); however, this can
98 limit the ability to test the range and dynamics of present and future environmental conditions
99 (Blois et al., 2013; Rastrick et al., 2018; Bass et al., 2021). The use of *ex-situ* experimental

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118 systems that manipulate multiple environmental conditions such as temperature and salinity can,
119 thus, be a valuable tool to assess the response to multi-stressors in a future ocean.

120 The recognition of conducting multi-stressor experiments has become increasingly
121 relevant due to the interaction of environmental drivers in dynamic systems under a changing
122 climate (Kroeker et al., 2020). Nearshore regions such as fjord systems and estuaries can
123 experience an amplified modulation of temperature and salinity on short timescales (Evans et al.,
124 2015; Hales et al., 2016; Fairchild and Hales, 2021). Such instances have been observed in sub-
125 Arctic estuaries where water temperature at a depth of 10 m decreased by 1.5 °C in < 10 h, and
126 in temperate systems where the magnitude of salinity change driven by high precipitation
127 displayed a decrease of 4 units in < 24 h (Miller and Kelley, 2021; Poppeschi et al., 2021).
128 Changes of this magnitude are particularly pertinent for Arctic fjords where recent evidence
129 found that changes in salinity from glacial meltwater were capable of directing whether a system
130 is net heterotrophic or autotrophic (Sejr et al., 2022). In this system, the salinity dynamics were
131 observed as a temporal decrease from 31 to 28 over a few days, or as a spatial modification
132 where values changed by 5 units over a 5 – 10 km distance.

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133 Recent advances in the ability to modulate several environmental parameters at once
134 using *ex-situ* mesocosms has been presented via the use of a modular programmable system
135 (Wahl et al., 2015; Pansch and Hiebenthal, 2019). Such systems have demonstrated an ability to
136 apply programmable environmental scenarios as a multifactorial design, or as a delta-change
137 (offset) from ambient conditions that mimic the natural variability of an environment. The
138 advantages of these types of automated systems lie in their ability to overcome the need for
139 capturing and measuring abundant discrete measurements used to regulate experimental
140 conditions, and transcend the logistical difficulties of implementing natural variability to

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142 experimental designs. In addition, these systems can reduce the need for constant human
143 observation which may be required to program new regulatory operations or make rapid
144 adjustments to experimentally manipulated conditions.
145 Here, we describe an autonomous salinity and temperature experimental perturbation
146 mesocosm system (SalTEPreS) that has the ability to modify, and then regulate, salinity and
147 temperature in real-time. The SalTEPreS can perform similar functions as the *ex-situ* mesocosm
148 systems discussed previously (i.e., Kiel-outdoor and -indoor benthocosms), such as applying
149 programmable static or dynamic changes to temperature and salinity, or by replicating natural
150 variability as on offset in real-time, but has the added capability of autonomous control for each
151 experimental unit (e.g., chamber or mesocosm). In this initial deployment of the SalTEPreS, we
152 applied a delta offset (i.e., offset from a measured control) to temperature and salinity as a
153 multifactorial treatment design for a two-month long experiment in Kongsfjorden, Svalbard, that
154 exposed mixed kelp communities to future temperature, salinity, and irradiance conditions in the
155 fjord. This study demonstrates the stability and flexibility of the SalTEPreS as an experimental
156 tool to be utilized under extreme and dynamic conditions to test the effects of physicochemical
157 multi-stressors on marine organisms and communities in the context of a multi-month
158 experiment.

160 2 Methods

161 2.1 Operational Concept of the Experimental System:

162 The SalTEPreS simulates the drivers in a marine or freshwater system such as temperature,
163 freshening, acidification, or hypoxia as either static or as temporally-variable modifications to
164 ambient seawater. This is accomplished by mixing manipulated source water, whether it be
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A principal challenge of conducting an *ex-situ* multi-stressors experiment lies within the ability to consistently modulate, replicate, and regulate the experimental conditions in real-time. To date, the majority of experiments conducted on marine organisms and communities have implemented only static changes to physical stressors with a limited capacity to induce variability by either manually changing conditions at set time points or using coarse automation with static setpoints and thresholds (Olariaga et al., 2014; Pansch and Hiebenthal, 2019; Kroeker et al., 2020). Often, this can fail to capture the high frequency variability of *in-situ* conditions. When considering the dynamics of physicochemical conditions in nearshore systems that can notably change within tidal cycles (Evans et al., 2015; Hales et al., 2016; Miller and Kelley, 2021; Fairchild and Hales, 2021), replication of these environmental scenarios necessitates the development of an autonomous system in order to properly conduct experiments over various periods of time. The advantages of implementing an automated system are that it can overcome the need for capturing and measuring the abundant discrete measurements used to regulate the experimental conditions. This can also remove the need for constant human observation which may not be feasible in the long-term, but may be required to program new regulatory operations and make rapid adjustments to the experimentally manipulated conditions.

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211 freshwater or warmed water, with ambient water through automatic flow valves that control the
212 volume and rate of water delivered. This is regulated by the constant monitoring of the mixed
213 water conditions in each mesocosm or chamber via a programmable feedback loop that transmits
214 the opening or closing of the automatic flow valves. The automated ability of the SalTExPreS is
215 configured to respond to near instantaneous measurements (several reads per second) to achieve
216 high frequency regulation of the manipulated drivers based on a measured *in-situ* or control
217 reference. The programmable setpoint conditions in each mesocosm are easily controllable
218 through an intuitive computer interface application.

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220 **2.2 Site Description and Experimental Design**

221 Kongsfjorden is a fjord system on the west coast of Svalbard where the West Spitsbergen
222 Current exchanges warm Atlantic water through trough channels regulated by density gradients
223 at the fjord mouth. Over the past 2 decades, a persistent influx of Atlantic water has resulted in
224 the reduction of land-fast ice and the melting of sea terminating glaciers causing enhanced
225 freshwater and fluvial input (Luckman et al., 2015; Tverberg et al., 2019). The influx of
226 freshwater is highest in summer and is accompanied by an important sediment loading with the
227 potential to shoal the euphotic zone from 30 m to a 0.3 m depth (Svendsen et al., 2002). These
228 advancing climatic changes in Kongsfjorden set a relevant context for the inaugural deployment
229 of the SalTExPreS on a concrete platform situated ~ 12 m from the shoreline in Ny-Ålesund,
230 which is located on southwestern shore of Kongsfjorden ~ 11 km from the fjord mouth.

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231 The SalTExPreS was utilized to implement three treatment scenarios in a multifactorial
232 design to represent expected future conditions in Kongsfjorden for an experiment that examined
233 the productivity, survival, and growth response of mixed kelp communities found at 7 m for 54

243 d. The response of these kelp community assemblages was determined in part by conducting
 244 weekly closed system incubations and assessing the growth and metabolism of the kelp in each
 245 mesocosm—the details and results of this experiment are discussed elsewhere (Miller et al., *in*
 246 *prep*). The treatments were realized by multi-driver combinations of temperature, freshening, and
 247 irradiance, where treatments 1 and 2 differed in the magnitude of temperature increase, salinity
 248 decrease, and irradiance decrease (Table 1). Only temperature was manipulated for treatment 3.
 249 The chosen treatment and salinity perturbations were applied as offset values from measured *in-*
 250 *situ* fjord conditions at 11 m which captured the natural variability of the fjord system. The
 251 applied temperature offsets used for this experiment reflected the projected, SSP2-4.5 and SSP5-
 252 8.5 scenarios (Meredith et al., 2019; Overland et al., 2019; Table 1). The chosen decreases in
 253 salinity were based on correlations between *in-situ* temperature and salinity during summer 2020
 254 in Kongsfjorden (Gattuso et al., 2023), weeks 22 to 35 (Appendix A1 and Fig. A1). These
 255 calculated delta salinity values were applied as offsets in treatments 1 and 2 (Table 1). The third
 256 treatment scenario applied a temperature change of + 5.3 °C as a way to decouple the multi-
 257 stressor system and evaluate a temperature only stress. The effect of turbidity for treatments 1
 258 and 2 were simulated as a decrease in surface irradiance (i.e., ~ 25% and ~ 40% reduction from
 259 ambient irradiance at 7 m) by applying a combination of neutral light and spectral filters (Lee©
 260 Filters) placed as static fixtures overtop the mesocosms.

262 2.3 Experimental System

263 Water was pumped from Kongsfjorden at a 10 m depth (300 m offshore) using a submersible
 264 pump (NPS© Albatros F13T) that was tapped into an underwater intake pipe that fed a header
 265 tank in the Kings Bay Marine Laboratory in Ny-Ålesund, Svalbard. Pumped ambient seawater

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340 from the header tank was then split into 3 sub-header tanks within the marine lab where ambient
341 water was (1) left unchanged, (2) chilled to 0 °C, or (3) warmed to 15 °C. Each sub-header tank
342 was plumbed to supply a maximum flow of 6 m³ h⁻¹ for the ambient, 1 m³ h⁻¹ for chilled, and 2
343 m³ h⁻¹ of warmed water which required a pressure of 0.3 bars for each line to ensure consistent
344 flow rates (Fig 1). The 3 control mesocosms received a mix of chilled and ambient seawater in
345 order to properly simulate *in-situ* temperatures. The three experimental treatments (9 mesocosms
346 in total) received a mix of ambient, warmed, and fresh water for treatments 1 and 2, whereas
347 treatment 3 received a mix of just ambient and warmed water (Fig 1). Freshwater was sourced
348 from the tap which was fed by the Tvillingvann reservoir close to Ny-Ålesund. The total flow-
349 through rate of each mesocosm was 0.5 m³ h⁻¹ (i.e., each mesocosm turned over every 2 h) of
350 post-mixed media delivered in an open cycle flow-through system, where flow rates of 7 – 8 L
351 min⁻¹ were maintained as target setpoints. Continuous flow was maintained throughout the
352 experiment with the exception of weekly 3 h incubations (to perform experiments on the
353 community) where flow to each mesocosm was shut off. In total, there were twelve circular
354 mesocosms (3 treatments and 1 control, 3x replicates) with a mean diameter of 1.1 m and a
355 volume of 1 m³, each equipped with a 12 W wave pump (Sunsun© JVP-132), a temperature-
356 conductivity probe (Aqualabo, PC4E), an optical oxygen sensor (Aqualabo, PODOC), and an
357 Odyssey© light logger. Fiberglass insulation was placed on the outside of each mesocosm to
358 increase insulation in order to reduce any potential change in temperature.

359 Delivery of ambient, chilled, warmed, and freshwater first ran through an automated
360 mixing manifold that regulated the flow of each media type assuring that proper volumetric
361 proportions passed through the regulator valves to achieve target conditions (Fig. 1). Each
362 source-water flow-line was regulated by an automated 3-way mixing valve (2-way mixing valve

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394 for incoming freshwater) which then passed through another mixing valve (12 in total) that was
395 assigned to each mesocosm (Fig. 1) This style of regulation ensured that the proper proportions
396 of manipulated media and ambient water were mixed to achieve setpoint conditions. Any
397 temperature variation induced by mixing freshwater was immediately compensated for by
398 regulating the flow of the warm water line. Details regarding the programmed regulation are
399 discussed further in the appendix (Section A2). The mixed media then passed through a flow
400 meter to measure the flow rate to each mesocosm which was regulated by a manual hand-crank
401 valve used to make minor adjustments to the valve opening position. This regulates the flow to
402 each mesocosm. Measurements by all the pressure sensors, the status of open position for the
403 regulator valves, and flow rates were logged ever minute and projected to the user interface via a
404 computer application (Fig. A3).

406 **2.4 Setpoint Regulation**

407 Setpoint temperature conditions + 3.3, 5.3, and 5.3 °C applied to treatments 1, 2, and 3,
408 respectively, were offsets from the control temperature setpoint. The temperature setpoint of the
409 control condition was updated hourly and programmed to replicate the measured *in-situ*
410 conditions in the fjord logged by the AWIPEV (Alfred Wegener Institute and Institute Paul
411 Emile Victor) FerryBox part of the COSYNA underwater observatory
412 (<https://dashboard.awi.de/>) situated at a depth of 11 m. Each treatment condition (temperature
413 and salinity offset) was set by manually programming the setpoint value of temperature in the
414 software interface (see appendix A3). The salinity offset was coupled to the temperature setpoint
415 via the correlation described in appendix A1. The measured temperature and salinity
416 observations from inside each mesocosm were recorded multiple times per minute and used to

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2.3 Parameter Regulation

2.3.1 Temperature and Salinity

The control from which temperature and salinity regulation were automated was based on hourly *in-situ* readings from the

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442 continuously monitor the regulation of the conditions inside each mesocosm. This data
443 transmission was used to program the software controller that performed the automated
444 regulation of mixed media (for details see appendix A2).

445 2.5 Software

446 The software application used for the control of the SalTExPreS was developed using Visual
447 Studio Community (2019 edition) with the vMicro extension and Arduino 1.8.13. The program
448 application has a user-friendly interface designed to allow real-time monitoring and
449 parameterization of regulation processes (Fig. A3). The main window displays each mesocosm
450 condition (sensor measured parameters), their piping connections, a connection status for each
451 PLC informing proper communication, date and time of the last received communication packet
452 from the Head PLC, and the status of the experiment (e.g., started or stopped). The interface also
453 displays the valve-open percentage along with the pressure setpoints and the actual measured
454 value for each main source-water inlet. In addition, the in-situ data (temperature and salinity)
455 received from the FerryBox is displayed with the time and date of the last logged value utilized
456 to program the real-time setpoint of the control condition. Sensor readings of flow rate ($L \text{ min}^{-1}$),
457 O_2 concentration (% saturation), salinity, and temperature ($^{\circ}C$) are shown for each mesocosm in
458 conjunction with the treatment setpoints (i.e., temperature, and salinity when relevant). All
459 measured data is stored through the server connection to the cloud, however, there is a backup
460 microSD card on the Head PLC that logs data from all mesocosms every 5 sec. If
461 communication fails between the Head PLC and the interfaced computer, data will not be
462 retrieved by the PC during the communication break, but will be retained by the microSD card.

463 Results

Deleted: The program automatically calculated the salinity offset based on the preset temperature offsets (Table 1). Regulation was maintained via regulation flow valves utilizing minutely measurements of temperature and salinity inside each mesocosm making instantaneous adjustments. This was accomplished using an analog three-way mixing valve for temperature and two-way valve for salinity (BELIMO© R3015-10-S2 with LR24A-SR motor). Each valve was plumbed within the manifold and applied to each mesocosm flow line where its open-position was adjusted (using a PID regulator) to reach the temperature and salinity setpoint value.

Moved down [2]: Accurate temperature and salinity regulation was obtained using a software PID controller on the corresponding Programmable Logic Controller (PLC), in PoE mode (proportional on error). The PID controller measures the difference between the measure and the setpoint (i.e., the error), and calculates how the valve opening should be adjusted by multiplying the error, which is the integral of the error and the derivative of the error, by previously determined coefficients K_p (proportional gain), K_i (integral gain) and K_d (derivative gain), respectively. These coefficients were obtained experimentally using the empiric method of Ziegler & Nichols (1943), and may differ from one condition to another.

2.3.2 Pressure and Flow Regulation

Each main inflow line of ambient, cold and warmed seawater had its own pressure regulation system established to

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3.1 Regulation of the control condition

The control condition was able to simulate the ambient fjord temperature well over the experimental period deviating < 0.3 °C on average across the 3 replicates (Table 2, Fig. 3). The overall quality of the regulation was based on the ability of the system to read the measured data from the FerryBox, or to follow a manually programmed setpoint when communication with the FerryBox was interrupted. During the experiment, the FerryBox went intermittently offline, 24 % of the time ceasing transmission of real-time data that resulted in a break of communication to the PLCs. This somewhat frequent break in communication resulted in an average setpoint deviation that was nearly double for the control compared to the treatment conditions (Table 2). The ability to manually program a new setpoint when communication breaks occurred ensured that the control condition was still robustly regulated. Over the entire period of the SalTExPreS deployment, the mean temperature of the control condition increased from ~ 4 to 6.5 °C from early July to the end of August (Fig. 3a). The coldest mean temperature of the control condition occurred when a backup pump situated at 90 m was used from 2021-07-14 ~21:00 UTC until 2021-07-26 13:49 UTC while the original pump at 10 m was repaired due to a motor malfunction. During this period, the control condition was $\sim 1.0 - 1.5$ °C cooler than the temperature measured by the FerryBox (Figs. 2, 3). Since a warmed seawater inlet was not supplied to the control condition, the temperature of the control condition remained cooler than the measured ambient conditions at the FerryBox. Despite the cooler temperature for the control, regulation of flow rates, mesocosm turnover time, and variability across the control condition replicates was well maintained by the system.

2.6 Temperature and salinity regulation

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Deleted: There were two main disruptions in the regulation of the control conditions resulting from the main seawater pump failure and a disconnection from the FerryBox. On 2021-07-14 ~21:00 UTC the pump deployed in the fjord suffered a motor malfunction causing a spike in ambient temperatures due to suspended incoming flow of water to the main header tank (Figs. A5, A6). An alternative deep-water pump (90 m) was used as a replacement until the pump at 10 m depth could be repaired on 2021-07-26 13:49 UTC. During this period, the control condition was colder than the target fjord temperature at 7 to 10 m depth by > 1 °C (Figs. 3, 4) until the proper pump depth was reestablished. The average deviation (Table 2) excluded this period as the control condition was unable to be warmed as only cold and ambient water lines were plumbed to the control condition (see section 2.2). The other instance occurred on 2021-08-24 04:47 UTC when setpoint values did not retain the last FerryBox reading and dropped to 0 °C. This issue was quickly resolved (< 8 h) by resetting the PLC.

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710 The regulation of temperature and salinity in the different treatment conditions (Trts. 1 – 3) was
711 maintained for 54 days (2021-07-03 – 2021-08-26) by the SalTEXPreS: the entirety of the
712 planned experiment. For the first 6 days of the SalTEXPreS deployment, the treatment conditions
713 were held at control conditions (i.e., no applied offset from the control) before the stepwise
714 increase in temperature began. On 2021-07-10 12:00 UTC a temperature offset of $0.55\text{ }^{\circ}\text{C d}^{-1}$
715 was programmed for treatment 1 while treatment 2 and 3 were programmed to increase by 0.88
716 $^{\circ}\text{C d}^{-1}$ (Figs. 2, 3). The final temperature setpoint above the control condition was reached on
717 2021-07-15 21:00 UTC. The system needed 4 h to achieve the new temperature conditions (i.e.,
718 homogenize the mesocosm to a plus $0.88\text{ }^{\circ}\text{C}$ increase) after the final incremental increase was
719 programmed. To avoid potential discrepancies with the regulation of salinity for treatments 1 and
720 2, a manual override was applied resulting in the system to realize the final salinity offset value
721 upon the initial temperature increase (Fig. 3b, 4). It took the system 4 h to achieve the salinity
722 offset for treatment 2 adjusting the value from ~ 34 to 29.8 (Fig. 3b, 4).
723 The precision of the temperature and salinity regulation across all treatment conditions
724 was well maintained as the mean difference between the measured value and the setpoint was $<$
725 $0.2\text{ }^{\circ}\text{C}$ and < 0.36 for salinity across the entire deployment (Table 2). The mean deviations
726 observed across treatments did not appear to correlate to the degree of offset. Thus, treatment 3
727 showed the highest precision for temperature regulation, while salinity regulation was the most
728 robust for treatment 2 compared to treatment 1 (Table 2). During the several instances where
729 communication broke with the FerryBox and the Head PLC, the SalTEXPreS retained the last
730 measured value at the FerryBox as a contingency protocol. This aided in the ability of the system
731 to maintain a high degree of regulation throughout the entire deployment. The largest deviation
732 from the setpoint value for all treatment conditions occurred during the single instance in which

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Deleted: Due to technical issues with the incoming FerryBox data, the final salinity offset values for treatments 1 and 2 were reached immediately with the first incremental temperature increase on 2021-07-10 12:00 UTC because the programmed setpoint based on the linear relationship with temperature was set as a manual override

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765 the last read value from the FerryBox was not retained: this occurred on 2021-08-24 04:47 UTC
766 (Fig. 4). Communication was quickly restored after this incident by cycling the program code,
767 and the average deviation of temperature and salinity for treatment 1 for the remainder of the
768 deployment was < 0.16 and < 0.25 for treatment 2.

769 When adequate flow rates were maintained, the SalTExPreS was able to simultaneously
770 regulate 12 mesocosms at 4 different conditions to deviations in temperature and salinity that
771 were ≤ 0.5 °C or 0.5 in salinity from the setpoint value ≥ 80 % and ≥ 70 % of the time,
772 respectively (Fig. 5). Due to an erroneous setpoint for the control condition during the 90 m
773 pump usage, these times were excluded. When considering the % of time deviations from a
774 temperature setpoint were held to ≤ 1 °C, all mesocosms were regulated accordingly 89 % of the
775 time and 80 % for the salinity treatments (i.e., < 1 unit deviation), with the exception of the 1st
776 replicate for treatment 2.

778 Discussion

779
780 The inaugural application of the fully autonomous SalTExPreS demonstrated the capacity of the
781 system to successfully manipulate temperature and salinity as an offset value from control
782 conditions, thus maintaining natural *in-situ* variability for 4 different conditions simultaneously.
783 We utilized this deployment to test the effects of climate change drivers on Arctic kelp
784 communities recognizing the feasibility of the system to perform *ex-situ* experiments on
785 organisms or whole communities (Miller et al. in prep/submitted). The versatility of the system
786 not only permits the manipulation of temperature and salinity, but could incorporate other factors
787 such as CO₂ or hypoxia (Gazeau et al., in prep). While this experiment used a control offset
788 approach to produce treatment conditions, programmable parametrization of various treatment

Deleted: is programmed to automatically retain the last value read. Thus, regulation would be maintained based on this last *in-situ* temperature, unless a manual value was programmed as an override.

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Moved down [10]: when connection with the FerryBox was interrupted, the last value was not retained and resulted in strong deviations in the regulation until a manual value could be implemented (Fig. A5). This happened on only one

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924 combinations can be applied depending on the question and design of the experiment. The
925 automated component of the system reduced the logistical hurdles that can arise when,
926 performing high precision replication and regulation of experimental conditions that track real-
927 time system variability. While the use of such a system can reduce user oversight and limitations,
928 there is still a need for diligent operation.

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930 Since this initial deployment we have implemented several changes which have improved
931 the performance of the system that have been realized during a second deployment in the
932 summer of 2022 (Fig. 6). In this experiment, the SalTExPreS was integrated to function with a
933 deployable heat pump to simulate multiple scenarios of heatwave patterns over a nearly month-
934 long experiment. In this instance, temperature regulation was vastly improved as a result of the
935 programmable modifications made since the initial deployment. During this deployment the
936 SalTExPreS mimicked 3 marine heatwave scenarios where a dynamic temperature regulation
937 held deviations to < 0.5 °C for 94 % of the time in 9 different mesocosms. This was an
938 improvement to the % time of temperature regulation by ~ 15 % compared to the first
939 deployment. In the first deployment, inconsistent flow rates and communication errors between
940 the FerryBox and the Head PLC were the primary causes of large deviations (> 2.0 salinity or
941 °C) from setpoint values. For example, flow rates < 2 L min⁻¹ accounted for ~ 20 % of the large
942 deviations in temperature and salinity regulation. Simple modifications such as ‘pop-up’ alert
943 windows that warned when a lapse in communication with the FerryBox occurred (FerryBox
944 stopped logging), and the addition of contingency coding instructions (fail-safe instructions)
945 ensuring that the last received *in-situ* data were maintained are the types of modifications that
946 resolved most of the issues. Communication errors were easily remedied by cycling the power on

949 a PLC which is why pop-up alerts were an improvement to the operation. Other extraneous
950 circumstances that could impact flow rates such as pump failure and clogging from the use of
951 raw seawater are conditions that would need to be assessed whenever the SalTEXPathS is used.
952 However, these are very manageable situations which can be easily mitigated by an operator.
953
954 The novelty of the SalTEXPathS lies in its ability to independently regulate an experimental
955 condition in a single experimental chamber (e.g., mesocosm). The operational data produced
956 from this deployment are reliable, easily quantifiable, and provide the highest degree of
957 monitoring frequency for every applied experimental condition. This study has demonstrated its
958 ability to replicate dynamic nearshore systems where temperature and salinity can vary at high
959 frequency (e.g., tidally), but further enhances these conditions to mimic a future scenario by
960 applying an amplitude offset to the natural dynamics of *in-situ* conditions. Wahl et al. (2015)
961 described a system with a similar capability, but regulated treatment conditions by monitoring
962 source water and adjusting that media before it was delivered to each experimental chamber. The
963 SalTEXPathS differs here as it measures the conditions inside each experimental chamber (i.e.,
964 mesocosm) and regulates based on per second measurements made inside each mesocosm. This
965 provides the flexibility to individually modulate each experimental chamber providing a broad
966 range of versatility. The lack of infrastructure needed to set up the SalTEXPathS makes it easy to
967 deploy and transport. As long as there is a sufficient supply of ambient water and manipulated
968 media, there is little limit to the versatility of automated control for each mesocosm. Many
969 research endeavors and future implementations by the SalTEXPathS have the potential to conduct
970 a large range of experimental settings that pertain to environmental perturbations associated with
971 climate change or other anthropogenic forcings. The operation of such a system in extreme

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Some of the operational challenges encountered during the 2-month experiment in Svalbard were able to be mitigated or resolved henceforth. The use of pop-up alert windows when a lapse in connection occurred, or when data is not logging, along with secondary coding instructions (as fail-safe instructions) ensuring that the last received *in-situ* data were maintained are examples how improvements made during the experiment facilitate a more robust deployment for the future. These improvements are now incorporated into the available code for programming of the SalTEXPathS. These new editions were implemented during a second deployment that occurred in the summer of 2022 under a similar experimental design, and resulted in fewer lapses and frequencies of mis-regulation (Fig. 6). Further, we forewent attempting to regulate the control condition (i.e., mixing chilled seawater with ambient to account for unintended warming during transit from fjord to header tank to mesocosm) during this second deployment as transit time and distance from pumped fjord water was substantially less than this first application. The result of this decision was the complete resolution of connection issues that regulate the control setpoint. As for some of the more common disruptions that can occur during long-term experimental setups using raw seawater such as pump failure and clogging, both of which impacted the performance of the SalTEXPathS, were extraneous instances that are not relevant to its direct performance. Other issues such as a sudden glitch in the programming which resulted in a sudden freshening on 2021-08-03 07:30 UTC, or the persistent miscommunication with the treatment 2 branched-PLC from 2021-07-26 to 2021-08-03 UTC, could have been reduced by more fastidious monitoring of the SalTEXPathS regulation. We note that some of these issues were easily resolvable by resetting the Head PLC or cycling the power of the system. In short, efficient user operation could further reduce deviations and increase the accuracy of the SalTEXPathS regulation. ¶ This first and initial deployment of the SalTEXPathS used to conduct a multi-stressor experiment provided robust results for determining mixed kelp community metabolic responses to future Arctic conditions (Miller et al., *in prep*).

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1019 environmental conditions has shown the durability of the manifold to endure an adverse Arctic
1020 summer and still respond without mechanical failures. With proper operation and user
1021 proficiency, this proves to be a highly sophisticated and powerful tool to be utilized for aquatic
1022 perturbation experiments.

1023

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1028 logistical details, shipping, and access to marine lab facilities.

1029

1030 **Author contributions**

1031 C.M. and F.G. conceptualized the frame of the paper while F.G, S.C, and P.U. designed the
1032 experimental system. P.U. programmed the software. C.M. wrote the manuscript, performed the
1033 data analysis, and constructed the figures and tables while P.U. designed the diagram and
1034 schematic figures. All authors revised, commented, and edited during revision.

1035

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1040

1041 **Competing interest**

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1044 The authors declare no competing interests exist.

1045

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Tables

Table 1. Experimental treatment conditions with corresponding positive temperature offsets and the calculated negative salinity offsets. See section A1 and figure A1 for a full description of the T-S relationship used to calculate salinity offsets. PAR offsets are the approximate mean value across replicates. Cntrl. is the control and Trt. is treatment.

<i>Treatment</i>	<i>Temperature</i>	<i>Salinity</i>	<i>PAR</i>
Cntl.	Ambient	Ambient	Ambient
Trt. 1	+ 3.3 °C	$\Delta 2.5 - 3.0$ $\Delta S = 0.546 * T + 0.490$	~ 25% decrease from ambient
Trt. 2	+ 5.3 °C	$\Delta 5.0 - 5.5$ $\Delta S = 0.877 * T + 0.089$	~ 40% decrease from ambient
Trt. 3	+ 5.3 °C	Ambient	Ambient

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<i>Treatment</i>	<i>Temperature</i>
Control	Ambient
Trt 1	+ 3.3 °C
Trt 2	+ 5.3 °C
Trt 3	+ 5.3 °C

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Table 2. Absolute mean difference between measured temperature and salinity values against

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setpoints plus or minus the standard deviation. A weighted average was used for treatments 1 – 3

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to account for the 5-day incremental increase. Cntrl. is the control and Trt. is treatment 1 – 3 with

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replicates a – c.

Treatment	Mean diff		Manipulated water			
	Abs($T_{meas} - T_{set}$)	Abs($S_{meas} - S_{set}$)	Cold	Ambient	Warm	Fresh
Cntrl. a	0.275 ± 0.39	–	x	x		
Cntrl. b	0.291 ± 0.36	–	x	x		
Cntrl. c	0.223 ± 0.36	–	x	x		
Trt. 1a	0.126 ± 0.31	0.116 ± 0.31		x	x	x
Trt. 1b	0.142 ± 0.29	0.148 ± 0.22		x	x	x
Trt. 1c	0.145 ± 0.33	0.171 ± 0.33		x	x	x
Trt. 2a	0.111 ± 0.29	0.357 ± 0.74		x	x	x
Trt. 2b	0.133 ± 0.29	0.149 ± 0.26		x	x	x
Trt. 2c	0.196 ± 0.38	0.128 ± 0.25		x	x	x
Trt. 3a	0.109 ± 0.27	–		x	x	
Trt. 3b	0.112 ± 0.27	–		x	x	
Trt. 3c	0.106 ± 0.28	–		x	x	

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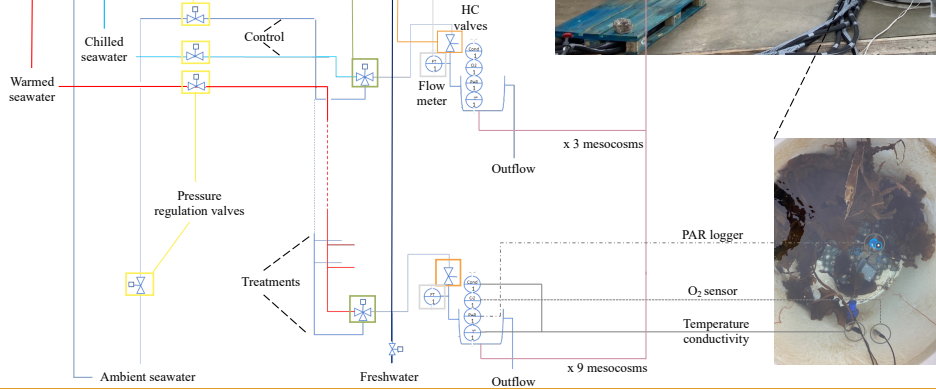
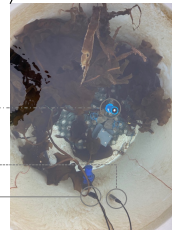
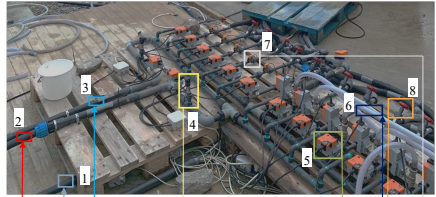
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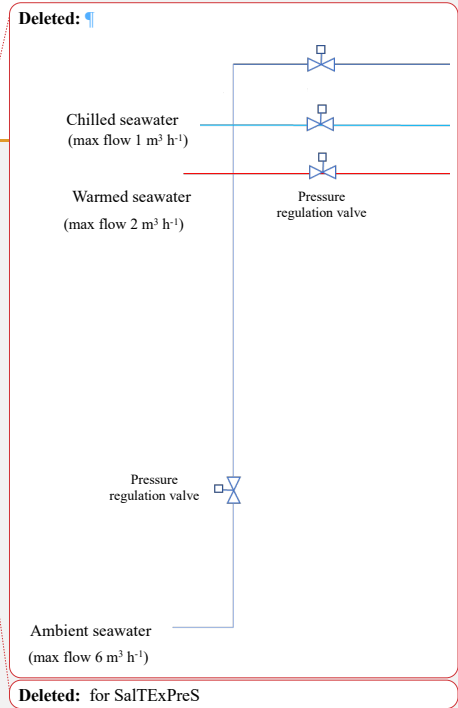
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1210 **Figures**



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1213 **Figure 1.** Piping schematic of the SalTExPreS which includes the mixing and regulation
 1214 manifold. **Items 1 – 3** depict the main seawater inlets from the ambient, warmed, and chilled sub-
 1215 header tanks located in the Kings Bay Marine Laboratory. Seawater from each sub-header tank
 1216 moves through a 2-way regulator valve followed by a pressure sensor (4) before splitting into
 1217 individual lines that lead to all 12 regulator valves (5), each assigned to a single mesocosm. For
 1218 treatments 2 and 3, the freshwater inlet (clear tube; item 6) passes through a 2-way regulator
 1219 valve before mixing with the ambient and warmed seawater lines. Flow rates are then measured
 1220 (7) post-mixing, and final flow rates are set using a hand-crank red valve (8). All 12 mesocosms
 1221 are displayed (upper right photo) with the inside of one mesocosm showing the oxygen and

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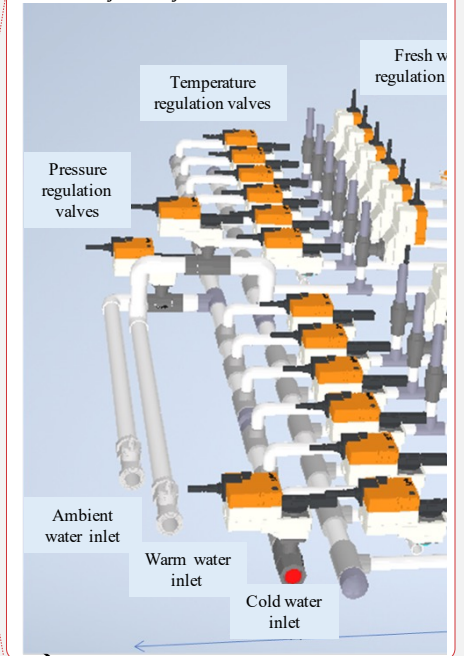
1233 conductivity sensors along with the PAR logger (bottom right photo). Table A2 provides the
1234 parts list for the items show in this figure. ▼

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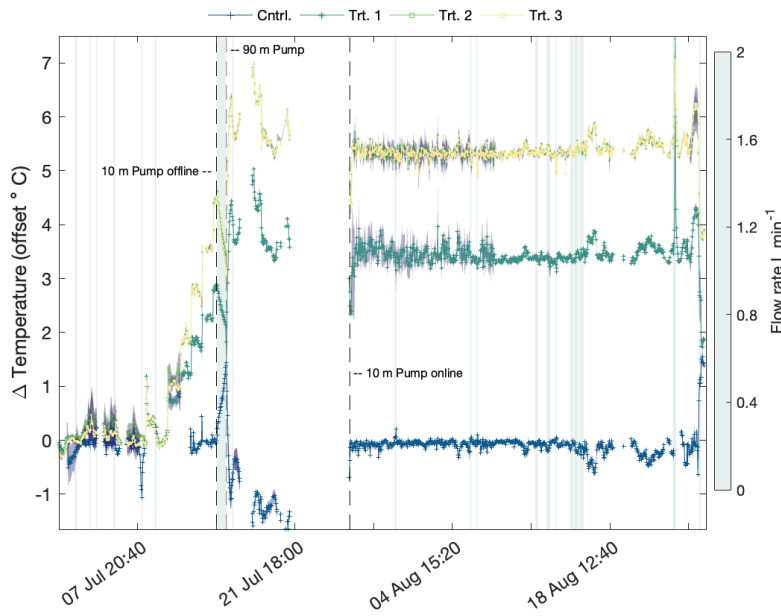
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Figure 2.



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1258 **Figure 2.** Regulation of the mean temperature offset for all conditions, including the control
 1259 offset from the FerryBox, and the three treatment offset values from the control condition. The
 1260 purple shaded region around the mean is the standard deviation and the heatmap isoclines (blue-
 1261 grey shaded regions) are instances when flow rates were $\leq 2 \text{ L min}^{-1}$ (threshold to avoid large
 1262 deviations > 2.0 salinity or $^{\circ}\text{C}$). Dashed black lines indicate periods when the pump at 10 m
 1263 depth and 90 m depth were used to feed the sub-header tanks. The time period presented is the
 1264 duration of the experimental deployment.

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Figure 3. Mean temperature (a) and salinity (b) for all conditions including those (dark grey circles) from the FerryBox for the entire deployment.

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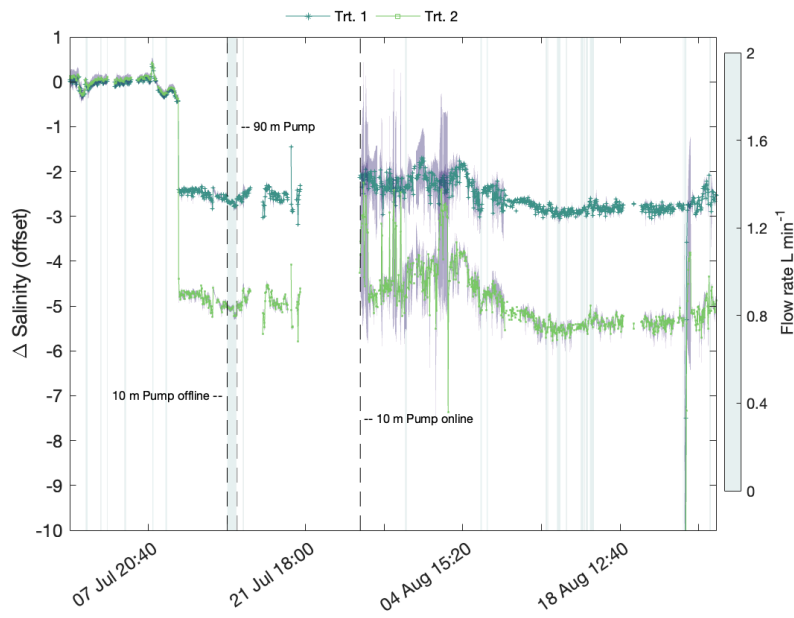
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1281 **Figure 4.** Regulation of the mean salinity offset (Δ salinity) during the experimental period for
 1282 treatments 1 and 2. The purple shaded region around the mean is the standard deviation and the
 1283 heatmap isoclines (blue-grey shaded regions) are the instances when flow rates $\leq 2 \text{ L min}^{-1}$.
 1284 Dashed black lines indicate periods when the pump at 10 m depth and 90 m depth were used to
 1285 feed the sub-header tanks.

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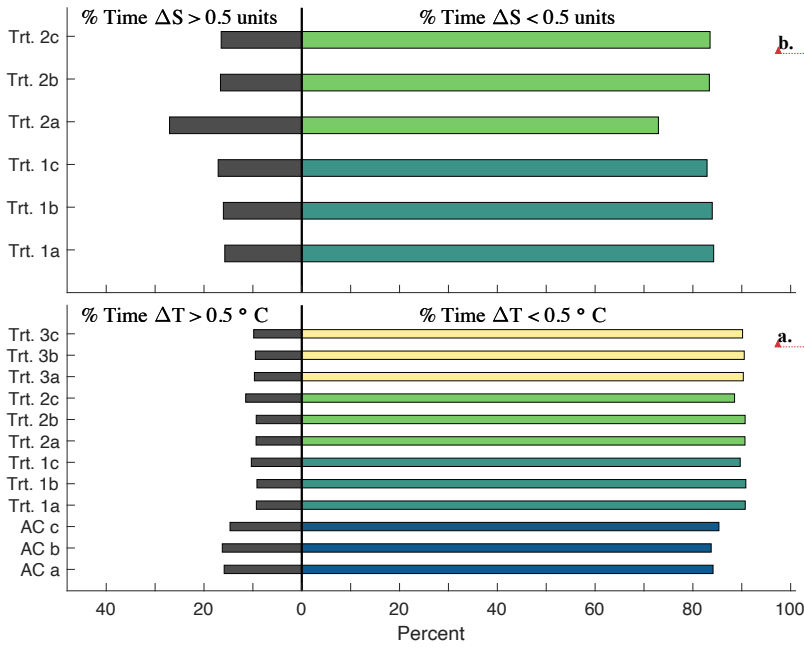
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Figure 5. Percent time each mesocosm experienced a deviation > (black bars) or < (colored) 0.5

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°C (ΔT; **a**) or 0.5 in salinity (ΔS; **b**) when flow rates were above 2 L min⁻¹. This excludes the

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period when using the 90 m pump (12 d) but accounts for 42 days out of the 54 day experiment.

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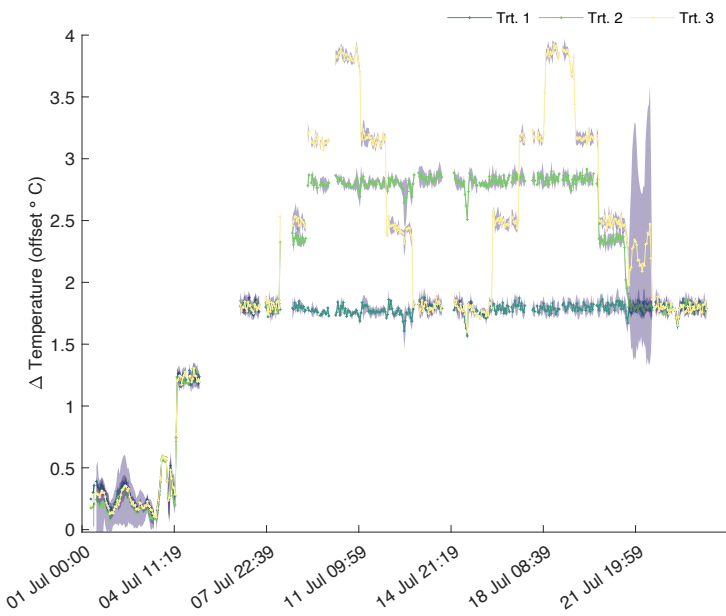
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Deleted: excluding the time when using the 90 m pump as regulation setpoints were invalid due to an erroneous control.



1314
 1315 **Figure 6.** Regulation of the mean temperature offset (Δ temperature) during the 2nd deployment
 1316 of SalTExPreS in the summer of 2022 in Tromsø (Norway) performing a variation of heatwave
 1317 scenarios with three experimental treatments 1 – 3. The purple shaded region around the mean is
 1318 the standard deviation.

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1327 **Appendix**

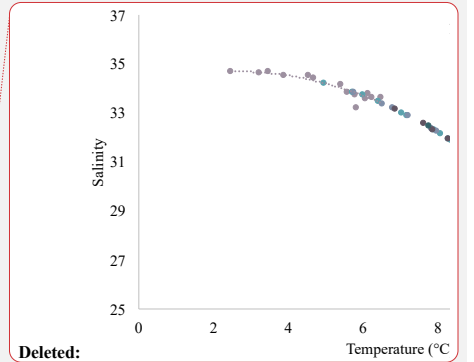
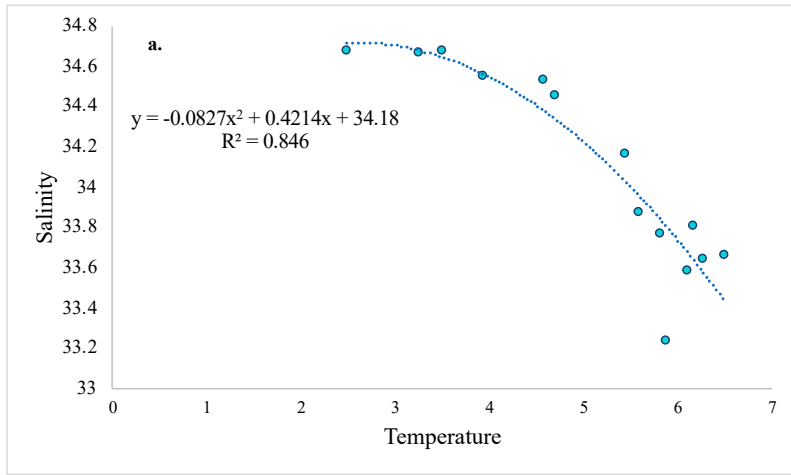
1328 **A1. Calculation of Salinity Offset**

1329 In the summer of 2020—weeks 22 to 35—the mean temperature at 11 m displayed a range from
1330 2.48 – 6.28, with salinity values ranging from 34.67 measured at the minimum 2.48 °C and 33.63
1331 measured at 6.28 °C (Fig. A1a). The correlation was best fit with a 2nd order polynomial. To
1332 project the salinity offset at a future temperature based on this 2nd order polynomial fit,
1333 temperatures of + 3.3 and 5.3 °C (SSP-245 and SSP-545, respectively) were added to *in-situ*
1334 fjord temperatures and salinity was calculated based on the 2nd order polynomial. These
1335 estimated salinity values were then subtracted from the mean salinity values observed (y-axis,
1336 Fig. A1a) in summer 2020 in order to calculate a delta salinity value for the SSP-245 and SSP-
1337 545 scenarios. The relationship between these estimated delta salinity values and the mean *in-*
1338 *situ* temperature (y-axis, Fig. A1a) displayed a robust linear relationship (Fig A1b).

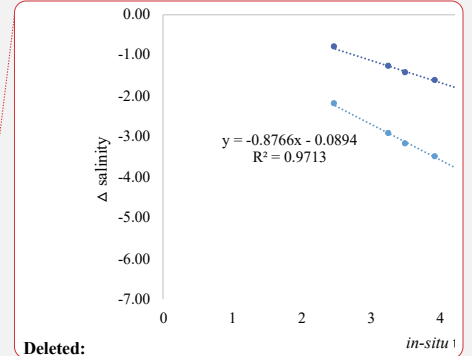
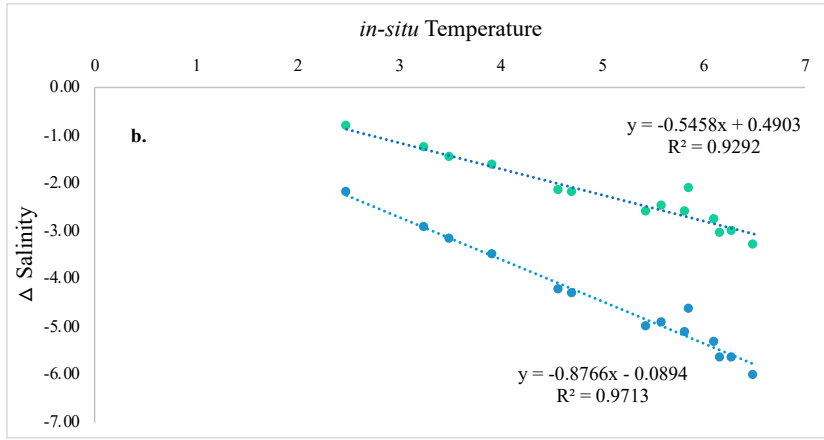
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1349 **Figure A1.** Relationship between temperature and salinity in summer 2020 weeks 22 – 35 in Ny-

1350 Ålesund, Svalbard **(a)** Relationship between estimated delta salinity and *in-situ* temperature,
 1351 where delta salinity was calculated as the difference between the current mean salinity and the
 1352 salinity estimated at the temperature increase projected for SSP-245 (blue dots) and SSP-545
 1353 (green dots) scenarios **(b)**.

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Deleted: Applied salinity offsets based on relationship with temperature used for treatments 1 and 2 (Table 1).

1371 **A2. Temperature and Salinity Regulation**

1372 Accurate temperature and salinity regulation was managed using the software PID (proportional
1373 integral derivative) controller on the corresponding Programmable Logic Controller (PLC). The
1374 PLC operated in PoE mode (power over ethernet) which builds a local area network (LANs)
1375 enabling use of Ethernet data cables to carry electrical power. The PID controller measures the
1376 difference between the measured value and the nominal value (i.e., the error). This calculates the
1377 position and adjustment of the valve opening by multiplying the error, the integral of this error,
1378 and the derivative of the error over time, by previously determined coefficients Kp (proportional
1379 gain), Ki (integral gain) and Kd (derivative gain), respectively. These coefficients were obtained
1380 experimentally using the empirical method of Ziegler & Nichols (1943). These coefficient values
1381 may differ from one condition to another.

1383 **A2.1. Pressure and Flow Regulation**

1384
1385 Each sub-header tank inlet line of ambient, chilled and warmed seawater had its own pressure
1386 regulation system enabling equivalent pressure levels to be maintained. This regulation process
1387 aided in the ability to adjust flow rates for all mesocosms by using the hand-crank valves (Fig.
1388 1). The system consisted of an analog pressure sensor (Siemens© 7MF1567-3BE00-1AA1) and
1389 a two-way analog valve (BELIMO© R2025-10-S2 with LR24A-SR motor). The pressure
1390 sensors were placed in-line directly after water from each sub-header tank passed through a
1391 regulator valve. The sensor ensured that pressure for each line was maintained at 0.3 bars by
1392 transmitting data to the system which then regulated the valve opening position of the incoming
1393 flow. A pressure setpoint for all three sensors was predetermined during flow rate test trials. This

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1415 process took place during the setup of the system where the valve opening was adjusted using a
1416 PID regulator (see A2) to maintain the defined pressure setpoint.

1418 A2.2 Automation

1419 The automation was performed using 4 Industrial Arduino-based PLCs (Industrial shields©
1420 Mduino-42+), with an individual PLC regulating the control condition and each treatment 1 – 3
1421 respectively. Each PLC was responsible for logging data and regulating a specific experimental
1422 condition. The PLC regulating the control condition—identified as the Head PLC—was the
1423 primary device responsible for communication with the branched PLCs and the monitoring
1424 computer (Fig. A2). All monitoring was performed on a PC Windows application (Section A3)
1425 and responsible for: (1) reading data received from the PLCs, (2) reading in-situ data received
1426 from the internet, (3) displaying live data, (4) logging data and sending it to an FTP server, and
1427 (5) sending settings and commands to the PLCs. Communication between the PLCs and the PC
1428 was ensured using http WebSocket protocol on RJ45 ethernet cables. The communication
1429 between the PLCs and the conductivity-temperature and oxygen sensors, flow rate sensors, and
1430 regulation valves was executed using a half duplex RS485 (2 wires) protocol, with an analog 4-
1431 20mA and an analog 0-10V signal, respectively. All PLCs and wired communication lines were
1432 housed in an electrical box installed to an IP68 Fibox enclosure with a 400 V (3P+N+E) 32 A
1433 security switch (Fig. A6). All the automation elements use low tension (12 Vdc or 24 Vdc)
1434 through circuit breakers and fuses. The electrical box was protected with a 220 V socket.

Deleted: (Kp, Ki, Kd in software interface) was applied to adjust the valve opening in order to regulate the pressure to the defined setpoint. Each water line with post-mixed seawater flowing to each mesocosm was then manually adjusted and controlled with a hand-crank valve. An analog flow rate sensor (IFM© SV3150) was placed in-line with the piping going to each mesocosm located directly before each hand-crank valve. This provided up-to-date logged flow rate values (updating every 30 sec), which could then be monitored to set incoming flow to each mesocosm.

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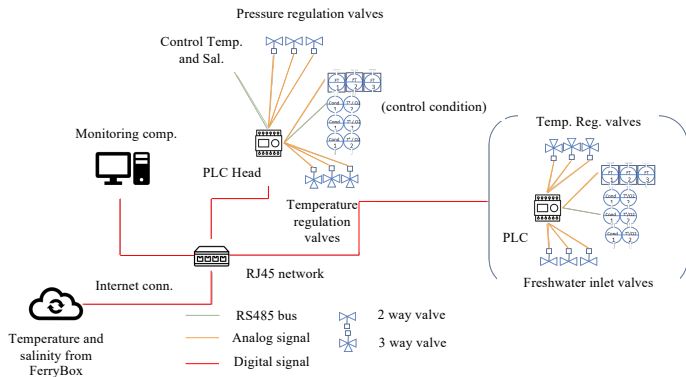
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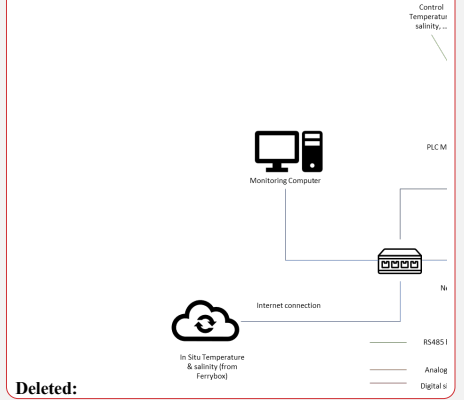
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Automation Hardware Architecture



Automation Hardware architecture



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1458 **Figure A2.** Diagram and flow-chart of the automation system.

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1472 **A3. Software Development**

1473 The code for the application was written in C/C++. The code uses publicly available Arduino

1474 libraries (<https://www.arduino.cc/reference/en/libraries/>) as well as originally designed libraries.

1475 All code is available on Github (<https://github.com/purrutti/FACEIT>). The code is divided into

1476 two pathways: 'Master.ino' for the Head PLC, and 'Regul_condition.ino' for the Branched

1477 PLCs. A description of the main functions applied in the code for programming the system

1478 regulation and features are listed in Table A3.

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<code>cmdID (ID of the requested entry), command (command type of the request). They optionally can also contain a « time » field: Unix-like timestamp (number of seconds since 01-01-1970)</code>	Monitoring PC (ID = 4)	Request Head data: specific data measured by Head PLC (pressure & flow rates) (ID = 5)
<code>regulationTemperature()</code>	This function is responsible for the temperature regulation of the mesocosm. It sets the corresponding three-way valve position using a 0-10V analog signal. The function first checks if the regulation is in « manual override » mode. If so, it applies the override setpoint. If not, it reads the temperature measure in the mesocosm, compares it with the setpoint, and uses the PID settings to set the valve position.	Send Head data: a response to a « request Head data » request (ID = 6)
<code>deAkkosozsmst()</code>	This function is responsible for the pressure regulation of the mesocosm. It sets the corresponding three-way valve position using a 0-10V analog signal. The function first checks if the regulation is in « manual override » mode. If so, it applies the override setpoint. If not, it reads the pressure measure in the mesocosm, compares it with the setpoint, and uses the PID settings to set the valve position.	
<code>printSD()</code>	Master PLC is equipped with a microSD card, on which data from all mesocosms is logged every 5 seconds, in one csv file per day. This is for security only, as the microSD card is not easy to remove from the PLC casing. It should not be removed before the end of the experiment.	
<code>Only for Head PLC</code>	This function is responsible for the salinity regulation of the mesocosm. It sets the corresponding three-way valve position using a 0-10V analog signal. The function first checks if the regulation is in « manual override » mode. If so, it applies the override setpoint. If not, it reads the salinity measure in the mesocosm, compares it with the setpoint, and uses the PID settings to set the valve position.	
<code>Only for Branched PLC</code>		

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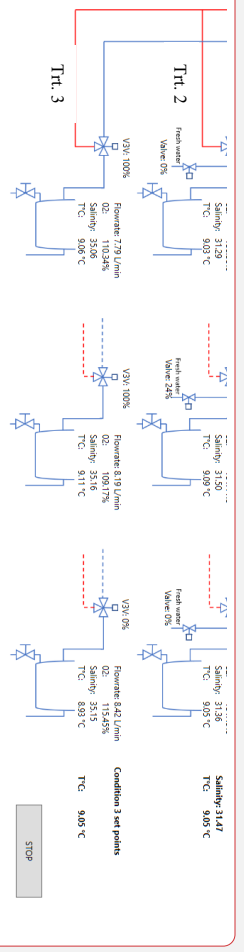


Function	Operation	Auxiliary field Sender ID	Auxiliary field Command #
<i>RTC/read()</i>	The PLCs are equipped with a RTC chip and battery to keep track of the date. Once set on commissioning, RTC read/Write status can be read and time-related on the RS485 bus. Each Mesocosm has two sensors (O2 and Conductivity/salinity), so each PLC has 6 sensors connected on its bus.		
<i>readAllSensors()</i>	- O2 sensors have addresses ranging from 10 to 12, for mesocosms 0 to 2 of the scenario, respectively. - PC4E sensors have addresses ranging from 30 to 32, for mesocosms 0 to 2 of the scenario, respectively. - Sensors are requested individually and in sequence. A request is made every 200 ms.		
<i>webSocketLoop()</i>	This is a callback function responsible for dealing with the WebSocket communication. The master PLC is the WebSocket server. It listens to slave PLCs requests and to the monitoring PC requests. Requests are JSON formatted. They always contain <i>url/path/fields</i> : sender ID (ID of the entity sending the request), comID (ID of the requested entity, command (command type of the request). They optionally can also contain a « time » field. Unix-like timestamp (number of seconds since 01-01-1970)	Head PLC (ID = 0) Branched PLCs (ID = 1-3) Monitoring PC (ID = 4)	Request params: seipoints, PID settings (# = 0) Request data: measurement values, regulation outputs (# = 1) Send Params: response to a « request params » request (# = 2) Send Data: response to a « request data » request (# = 3) Calibrate sensor: request for calibrating sensor to specified value (# = 4) Request Head data specific data measured by Head PLC (pressure & flowmeters) (# = 5) Send Head data: response to a « request Head data » request (# = 6)
<i>regulationTemperture()</i>	This function is responsible for the temperature regulation of the mesocosm. It sets the corresponding three-way valve position using a 0-10V analog signal. The function first checks if the regulation is in « manual override » mode. If so, it applies the override seipoint. If not, it reads the temperature measure in the mesocosm, compares it with the seipoint, and uses the PID settings to set the valve position.		
<i>checkMesocosms()</i>	This function loops through every mesocosm every 200 ms and reads analog signals (i.e., flowrates and pressure readings).		
<i>regulationPressure()</i>	This function is responsible for the pressure regulation of the mesocosm. It sets the corresponding three-way valve position using a 0-10V analog signal. The function first checks if the regulation is in « manual override » mode. If so, it applies the override seipoint. If not, it reads the pressure measure in the mesocosm, compares it with the seipoint, and uses the PID settings to set the valve position.		
<i>printTASD()</i>	Master PLC is equipped with a temperature sensor, on which data from all mesocosms is logged every 5 seconds, in one csv file per day. This is for security only, as the temperature sensor is not easy to remove from the PLC casing. It should not be removed before the end of the experiment.		
<i>regulationSalinity()</i>	This function is responsible for the salinity regulation of the mesocosm. It sets the corresponding three-way valve position using a 0-10V analog signal. The function first checks if the regulation is in « manual override » mode. If so, it applies the override seipoint. If not, it reads the salinity measure in the mesocosm, compares it with the seipoint, and uses the PID settings to set the valve position.		

Table A3. Functions used for programming of software.

In Situ Data:
 Temperature: 32.75 °C
 Salinity: 34.85
 Time: 2021-06-14 09:00:00

Ambient

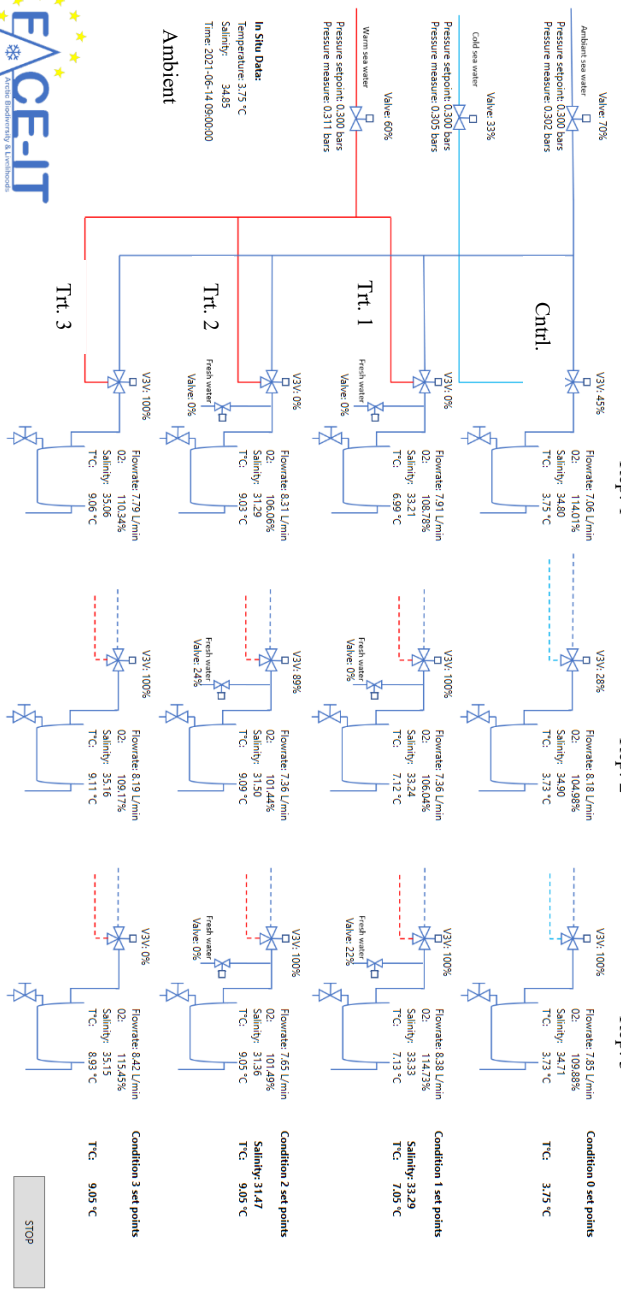


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1505 **Figure A3.** Application interface displaying real-time monitoring of ambient conditions as well
1506 and control (Cntl.), and treatment (Trt.) conditions for each replicate (Rep.) in each mesocosm.

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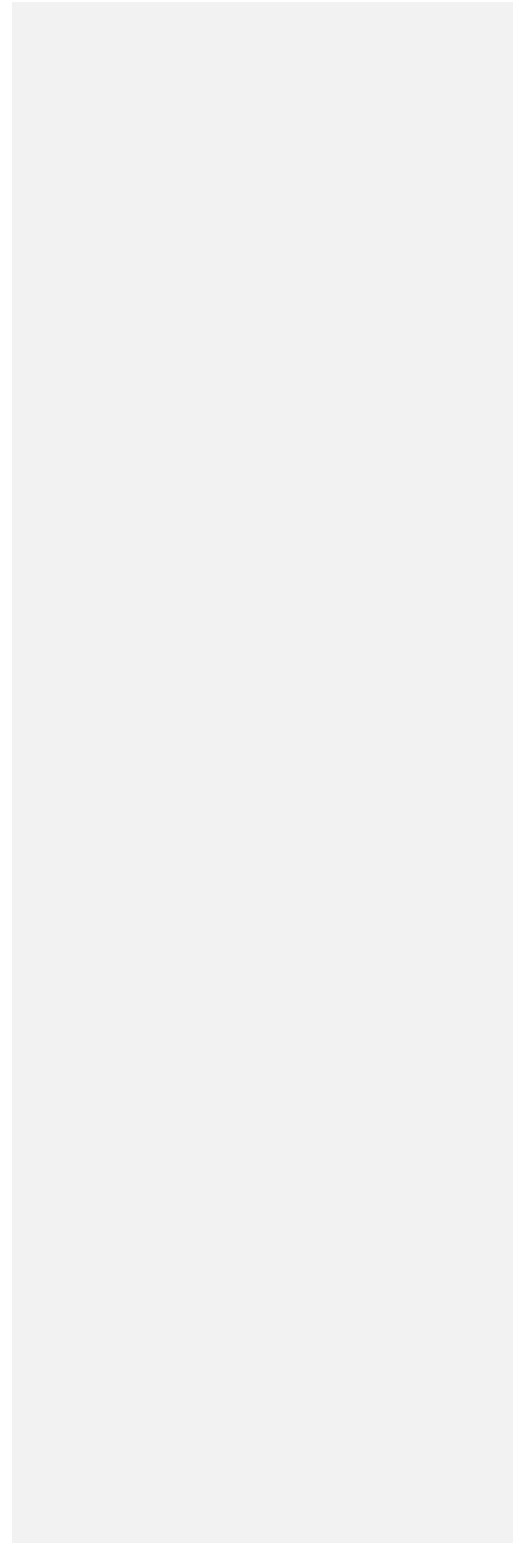
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1528 **A3.1. Menu bar of PC application**

1529 From the interface, the user sets the temperature condition and associated salinity offset, IP
1530 address and logging parameters, sensor calibration settings, and pressure setpoints (Fig. A4).
1531 Within the menu bar several tabs permit the setup of the project: file, settings, maintenance, and
1532 data. Under ‘file’ the system can be manually connected to, or disconnected from, the PLCs.
1533 Connection is usually maintained automatically. The ‘settings’ tab displays the application and
1534 experimental setting options (Fig. A4 a – c). All the settings of the project are stored on the
1535 computer (found in ‘application settings’) that is running the application, which include:

- 1536 i. *Master IP address*: The IP Address of the Master PLC (centralizing all the data).
- 1537 ii. *Data Query Interval*: Frequency of queries from the application to the master PLC.
- 1538 iii. *Data Log Interval*: Number of minutes between logs to file.
- 1539 iv. *Data Base File Path*: Directory and base filename of the csv data files.
- 1540 v. *FTP Username, Password, Path*: FTP settings for sending the data file every hour.
- 1541 vi. *InfluxDB Settings*: For Live Monitoring and local storage of the data.

1542 Under ‘experimental settings’, the programmed specificities and regulation of the treatment
1543 conditions can be adjusted. This includes programming the setpoints for pressure (all main
1544 inflow lines), temperature and the salinity-temperature relational equation (on a different tab
1545 selected from dropdown), as well as adjusting the Kp, Ki & Kd coefficients for the regulation
1546 (see section 2.3.1). The temperature setpoint is provided by the data received from the ferry-box,
1547 however this can be overridden if needed. The « Save to PLC » button sends the values to the
1548 corresponding PLC and saves the data, while the « Load from PLC » button loads the settings
1549 from the PLC. For the purposes of this experiment, the salinity setpoint was calculated based on
1550 a delta salinity for treatments 1 and 2 which were derived from the linear relationship with

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1551 temperature (see section 2.3.1). This can also be overridden if needed by selecting the manual
1552 override box.

1553 The 'maintenance' tab is where sensor calibration and communication 'Debug'
1554 operations can be executed (Fig. A4 d, e). Calibration can be performed for each sensor deployed
1555 in each mesocosm, and uses a 2-point calibration for temperature and % oxygen. The salinity
1556 calibration is done by setting the conductivity value corresponding to a temperature of 25 °C
1557 rather than the *in situ* measured temperature. The conductivity value is programmed as $\mu\text{S cm}^{-1}$.
1558 The communication process for sensor calibration is between 5 to 10 seconds. The final option in
1559 the menu is the 'data' tab which displays the historical and live data. The historical data can be
1560 interfaced to an html site if desired.

1561

Experiment Settings

Header ID Address: 171.16.2.110
 Data Store Method: 1

Delta T (K) Input: 5
 Delta T Unit: Kelvin
 Delta T Unit Label: Celsius/DeltaT/Kelvin, Same, Delta

RP: 1
 Universal: 0
 RP Factory path: /

Metadata:
 Name: /
 Title: /
 Author: /
 Date: /
 Cfg: /

Buttons: Save, Cancel

Experiment Settings

Control Condition: v

Pressure regulation

Pressure setpoint: 0.00
 Kp: 0.00
 Ki: 0.00
 Kd: 0.00

Temperature regulation

Temperature setpoint: 31.75
 Kp: 0.00
 Ki: 0.00
 Kd: 0.00

Manual Override: 0 %

Buttons: Load from PLC, Save to PLC, Cancel

Experiment Settings

Condition 1: v

Salinity regulation

delta Salinity: Δ -0.5458 x Ambient T°C + 0.4503 1
 Update

delta Salinity setpoint: -1.56
 Salinity setpoint: 33.29

Temperature regulation

delta T°C setpoint: 3.30
 Temperature setpoint: 7.05

Kp: 10.00
 Ki: 50.00
 Kd: 0.00

Manual Override: 0 %

Buttons: Load from PLC, Save to PLC, Cancel

Calibration

CO: 160
 Temperature: 31.75
 Measurement: 31.75

Calibration method 1:
 Calibration method 2:

Buttons: Factory reset

Request for update: The calibration of your sensor has been updated. If you require a full calibration after 20 seconds, please recheck the calibration of your sensor. (Temperature: 31.75°C)

Request sent: /
 Response received: /

Buttons: OK, Cancel

1563 **Figure A4.** Operation windows for the application and experimental settings (a-c). These
1564 windows are found under the 'settings' tab. Operation windows for sensor calibration and
1565 debugging (d, e). These are found under the 'maintenance' tab.

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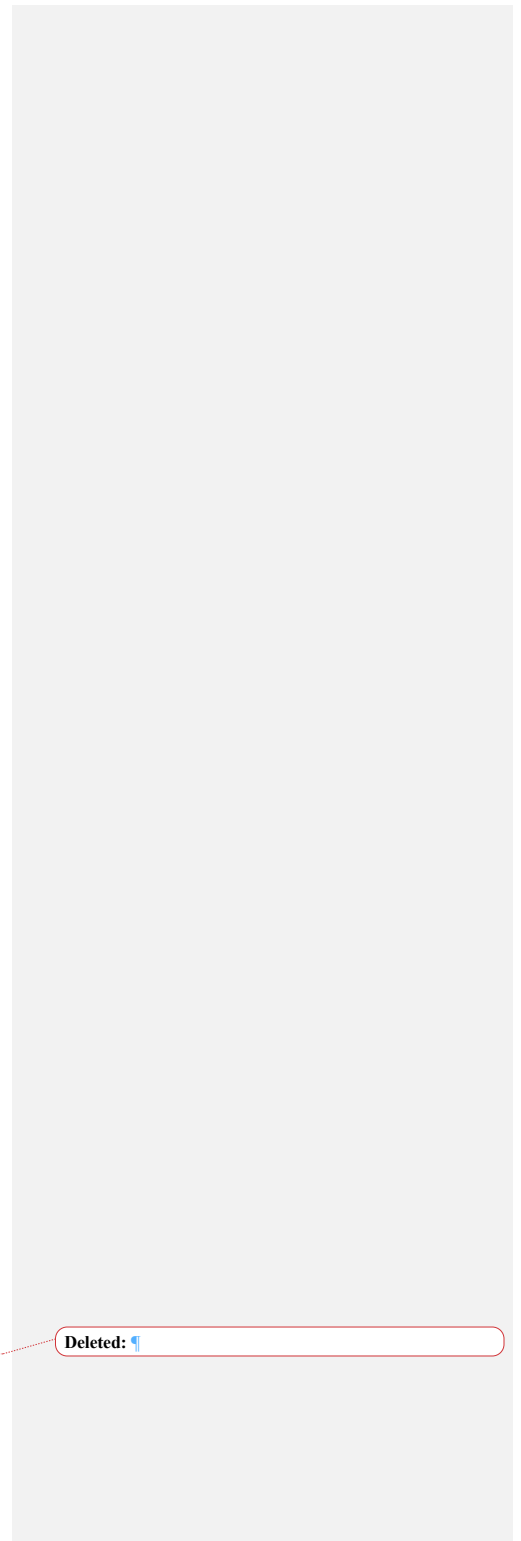
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1613 **Figure A.6.** Electrical cabinet used for SalTExPreS

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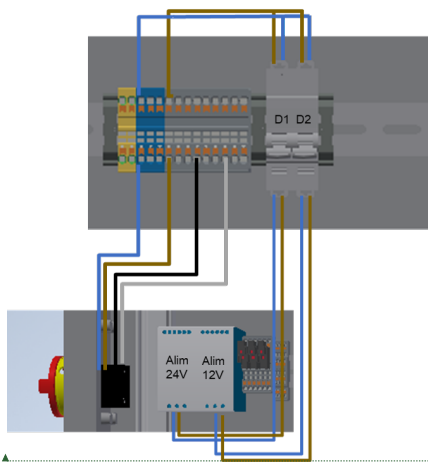
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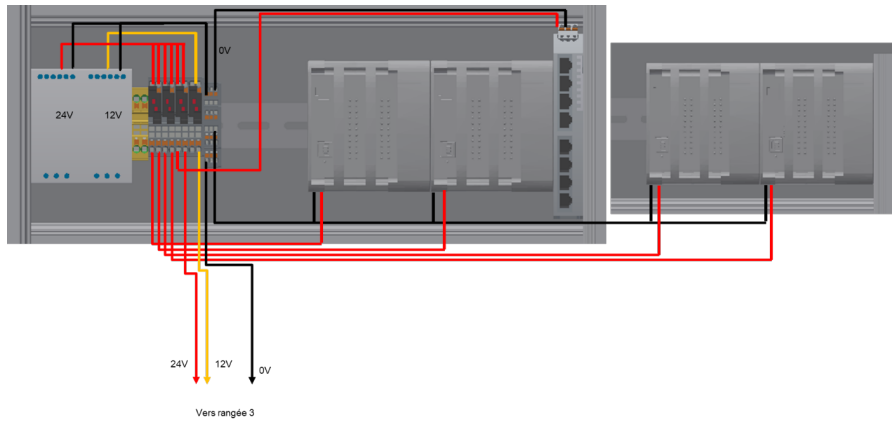
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D1: Alim 24Vdc
D2: Alim 12Vdc

Moved down [11]: Figure A8. Electrical schematic for wiring within the electrical box.

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Figure A7. Electrical schematic for wiring within the electrical box.

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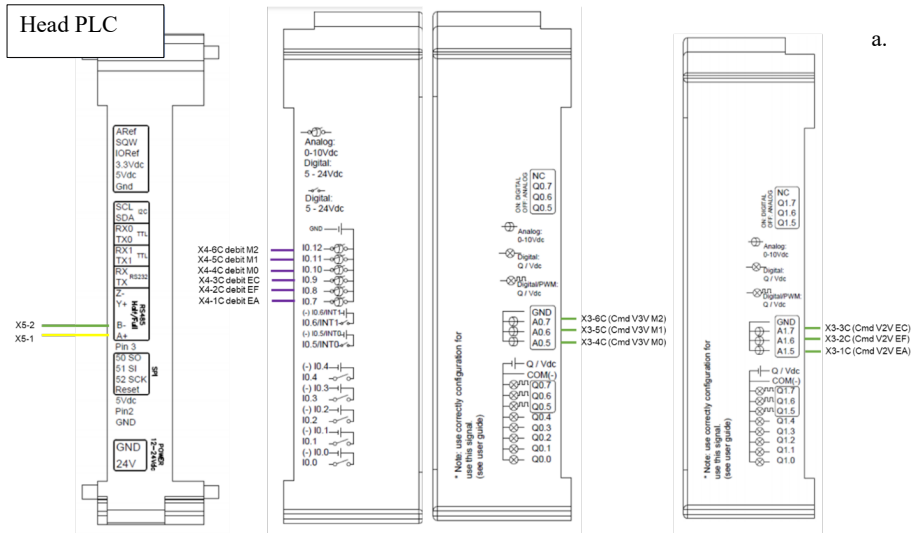
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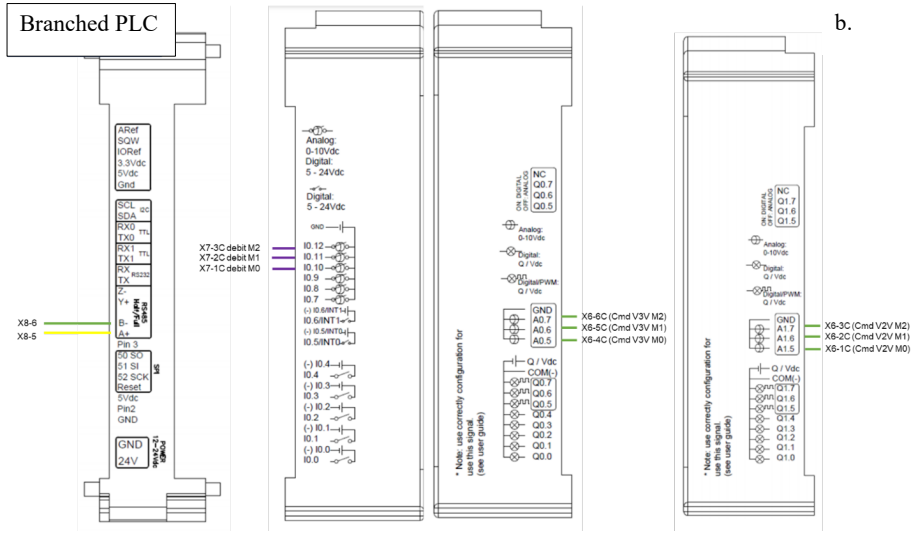
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1632 **Figure A8.** PLC controller diagram for Head (a) and Branched (b) operations.

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1636 **Table A2. Parts list with manufacturer model numbers.**

Group	Item	Supplier/manufacturer	Model / details	Quantity
Hydraulic system				
	Mesocosms	home made	1000 L fiber glass	12
	Seawater pump	NPS	Albatros F13T	1
	PVC-U tubing and fittings		20mm, 32mm & 50mm diameter	–
	Insulated flexible hose		19mm diameter	100 m
Sensors				
	Conductivity / temperature	Aqualabo	PC4E	12
	Oxygen	Aqualabo	PODOC	12
	Pressure	Siemens	7MF1567-3BE00-1AA1	3
	Flow rate	IFM	SV3150	12
Actuators				
	Pressure regulation valves	BELIMO	R2025-10-S2 with LR24A-SR motor	3
	Temperature regulation valves	BELIMO	R3015-10-S2 with LR24A-SR motor	12
	Salinity regulation valves	BELIMO	R2015-10-S2 with LR24A-SR motor	6
Automation cabinet				
	Cabinet	Fibox	FIB8120017N	1
	Security switch	KRAUS-NAIMER	KNA002245	1
	12 vdc power supply	Lambda	LAMDRL30-12-1	1
	24vdc power supply	Lambda	LAMDRB240-24-1	1
	PLC	Industrial shields	Mduino-42+	4
	Ethernet switch	HIRSCHMANN-INET	HIR942132002	1

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