

1 *Supplement to*
2 **Impact of HO₂/RO₂ ratio on highly oxygenated α -pinene photooxidation**
3 **products and secondary organic aerosol formation potential**

4

5

6 Yarê Baker et al.

7

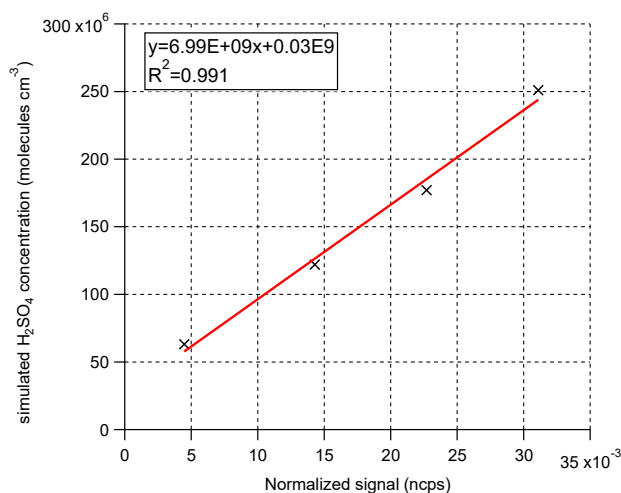
8 *Correspondence to:* Thomas F. Mentel (t.mentel@fz-juelich.de)

9 S1 Sulfuric acid calibration for MION-API-LTOF

10 The calibration source setup used by us was described in detail by Kürten et al. (2012) and was recently applied to a newer
11 model of the MION chemical ionization inlet by He et al. (2023). In short H_2SO_4 is produced via the reaction of SO_2 with
12 OH in a calibration source directly in front of the instrument. OH is produced via the photolysis of water from a humidified
13 N_2 flow and the H_2SO_4 concentration is varied by variation of the humidified inflow.

14 The expected H_2SO_4 concentration is calculated with an open-source python library provided by Shen and He (2023). The
15 model simulates the necessary gas phase chemistry based on a set of differential equations and uses two-dimensional
16 convection-diffusion-reaction equations to take into account the losses of H_2SO_4 in the tubing. All that is needed for this
17 calculation is the dimensions of the exact calibration setup. Details about the model can be found in He et al. (2023).

18 For the analyte signal we used the signal sum of the detected product ions HSO_4^- , $\text{H}_2\text{SO}_4(\text{NO}_3)^-$ and $\text{H}_2\text{SO}_4(\text{HNO}_3\text{NO}_3)^-$ and
19 normalized the signal with the sum of the NO_3^- ion and $(\text{HNO}_3\text{NO}_3)^-$ cluster. The resulting calibration curve can be found in
20 **Figure S1**. The calibration yielded a calibration factor of $7.0 \cdot 10^9$ molecules $\cdot\text{cm}^{-3}\cdot\text{ncps}^{-1}$, which is in the range of calibration
21 factors reported before for different NO_3^- -MION inlets, for comparison see Rissanen et al. (2019)
22 ($1.4 \cdot 10^9$ molecules $\cdot\text{cm}^{-3}\cdot\text{ncps}^{-1}$) and He et al. (2023) ($1.3 \cdot 10^{10}$ molecules $\cdot\text{cm}^{-3}\cdot\text{ncps}^{-1}$).



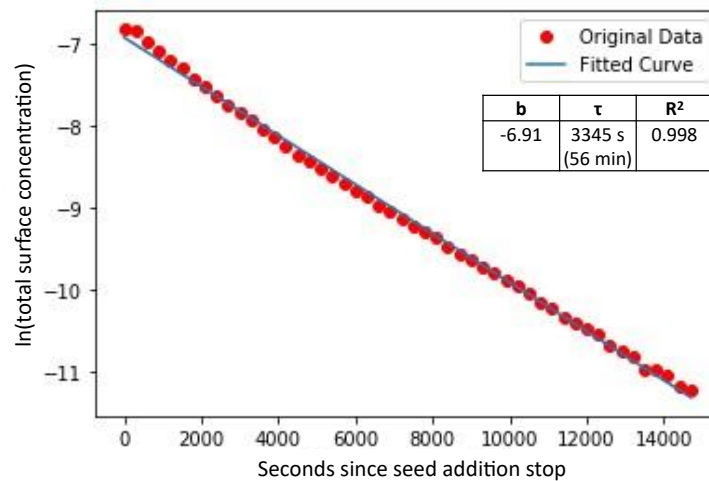
23
24 **Figure S1: Calibration curve NO_3^- -MION-CIMS for H_2SO_4 calibration set-up**

25 S2 Particle loss rate constant determination in SAPHIR STAR

26 The particle loss rate in the SAPHIR STAR chamber was determined by observation of the seed concentration decay in the
27 chamber after stop of the particle addition. The exponential decay was fitted logarithmic as shown in **Eq. (S1)** and the
28 lifetime $\tau_{particle}$ ($k_{particleLoss} = \frac{1}{\tau_{particle}}$) was determined. t is the time since start of the decay (time since seed addition
29 stop) and τ and b are fitted for.

$$\ln(\text{normalized signal}) = -\frac{1}{\tau} * t + b \quad (\text{S1})$$

30 Exemplary the result of the fit for the total surface concentration measured in the SMPS is shown in **Figure S2**. The
 31 determination via AMS sulfate and ammonium signal as well as the number concentration measurement gave similar results.
 32 Therefore, the average determined particle lifetime in the chamber of 54 minutes was used. The residence time in the
 33 chamber was 63 minutes which shows that the seed particles are lost only slightly faster than the flush out rate due to some
 34 deposition.



35
 36 **Figure S2: Logarithmic fit of particle surface decay timeseries to determine particle lifetime in the chamber**

37 S3 Box model input parameters

38 The input parameters into the model are defined by the flows into the reactor and consist of the flows themselves, their
 39 humidity and the contained α -pinene, O₃ and CO concentration. Additional inputs are the temperature, pressure, and J(O¹D).
 40 The UVC light is characterized by an on/off switch and the gap opening of the shielding. In separate experiments J(O¹D) was
 41 calculated from O₃ loss as a function of the gap opening. Other necessary input parameters are the OH background reactivity
 42 (loss of OH without VOC present) and the wall loss of the RO₂ and HO₂ species in the STAR chamber. It is assumed that the
 43 product species in the MCM are too volatile to be lost on the walls, but that the radical species are lost upon wall collision.
 44 An OH background reactivity measurement (kOH instrument, see Lou et al. (2010), Fuchs et al. (2017) for more detailed
 45 information) was performed in the empty, very clean chamber at the same humidity as in the experiments. This yielded a
 46 reactivity of 3 s⁻¹. The background reactivity was adapted to represent the α -pinene consumption in the photooxidation phase
 47 correctly, resulting in a maximum $k_{OH \text{ Background}} = 5 \text{ s}^{-1}$. A possible reason for the discrepancy is that the background
 48 reactivity determination was done in a very clean chamber while during the experiment series small residual contaminations,
 49 resisting flushing over > 6 residence times, may have contributed to the background reactivity.

50 For the estimation of the maximum wall loss the following experiment was performed twice: In a gas phase α -pinene
51 photooxidation steady state the light was turned off and the decay of HOM product signals were observed in the NO₃-MION-
52 CIMS. This approach was used before by Ehn et al. (2014) and Sarrafzadeh et al. (2016) to determine the maximum loss in
53 the JPAC chamber.

54 Only products showing a clear single exponential decay were considered and it is assumed that the chosen HOMs are no
55 longer produced after light off and lost on wall contact. Their timeseries is used to calculate an individual lifetime τ by
56 fitting the decay curve to the function shown in **Eq. (S1)**. From the observation of the decay of C10 products an average
57 lifetime of $\tau=171$ s is determined.

58 The derived wall loss rate for HOM was also applied to describe the wall loss of RO₂ radicals, and therefore, $k_{RO_2\ wall}$ is set
59 as $1/170$ s⁻¹. The lifetime is correlated to the transport through the diffusion layer of the chamber thus should scale with the
60 inverse of the square root of the molar mass (under the assumption of perfect mixing of the chamber core). It is therefore
61 expected that the smaller HO₂ radical is lost faster due to its faster transport. Additionally, the removal efficiency for HO₂
62 and RO₂ radicals might differ further as RO₂ are not lost necessarily on every collision with the wall. The specific RO₂
63 removal efficiency depends on the radical's molecular structure (Miyazaki, 2012).

64 To estimate a value for the HO₂ wall loss, the expected diffusion constant for a HOM-Mon, HOM-Acc and HO₂ are
65 calculated by the parametrization developed by Fuller et al. (1966) and recently reviewed by Tang et al. (2015). The results
66 can be found in **Table S1**.

67 **Table S1. Calculated diffusion coefficients of an exemplary HOM-Mon, exemplary HOM-Acc and HO₂**

Compound	Diffusion constant at 1 bar (cm ² s ⁻¹)
C ₁₀ H ₁₅ O ₆ (HOM-Mon proxy)	0.053
C ₂₀ H ₃₀ O ₁₀ (HOM-Acc proxy)	0.038
HO ₂	0.202

68
69 If the wall loss is only dependent on the diffusion to the wall (i.e. 100 % loss on wall contact), the lifetime should inversely
70 scale with the diffusion speed. To verify this assumption, the ratio of the average lifetimes of HOM-Mon and HOM-Acc
71 were compared to the ratio of their diffusion constants: The HOM-Acc proxy's diffusion constant is 0.71 of the monomer
72 proxy's diffusion constant. The observed accretion products decay resulted in average lifetime of $\tau=202$ s, leading to
73 $k_{HOM-Acc\ wall} / k_{HOM-Mon\ wall} = 0.85$. Within the uncertainties of the diffusion constants calculation and the lifetime
74 determination, the wall loss seems to depend indeed on the diffusion to the surface layer, thus on the diffusion constant.
75 Therefore, considering the diffusion constant of HO₂, $k_{HO_2\ wall} = 1/50$ s⁻¹ is chosen.

76 To study the sensitivity of the modelled HO₂/RO₂ ratio to the assumed wall loss rates, a sensitivity study was performed by
 77 varying the rate coefficients for wall losses. The RO₂ wall loss was varied within 1σ of the determined HOM product wall
 78 loss. The HO₂ wall loss was varied in a wider range to cover the case that not all collision with the wall lead to loss of HO₂.
 79 Therefore, the lifetime of HO₂ was either set as 50 s or to a maximum lifetime of 170 s as determined by HOM monomer
 80 loss. The resulting HO₂/RO₂ ratios of the sensitivity study for the Exp1 experiment are displayed in **Table S2** as an example.

81 **Table S2. Box model HO₂/RO₂ ratio results at varying RO₂ and HO₂ wall loss at low HO₂/RO₂ (left) and high HO₂/RO₂ (right in**
 82 **the Exp1 experiment**

$\tau(\text{HO}_2) \backslash \tau(\text{RO}_2)$	low HO ₂ /RO ₂		high HO ₂ /RO ₂	
	<u>50 s</u>	<u>170 s</u>	<u>50 s</u>	<u>170 s</u>
<u>145 s</u>	6.8E-3	7.5E-3	0.7	1.0
<u>170 s</u>	6.4E-3	7.0E-3	0.6	0.9
<u>195 s</u>	6.1E-3	6.7E-3	0.6	0.9

83
 84 The sensitivity study shows that independent of the assumed wall loss rate the HO₂/RO₂ ratio is around 0.007 and near one
 85 in the low and high HO₂/RO₂ case, respectively. In any case, the modelling results are only used to qualify the change of
 86 chemical regime and not to yield absolute values.

87

88 S4 Peaklist of oxidation products identified in NO₃-MION-CIMS

89 Table S3. Peaklist NO₃-MION-CIMS. All compounds were detected as clusters with (NO₃). The table is sorted into fragments,
 90 monomers, and accretion products. Some compounds were just assignable in certain experiments, this is indicated by the
 91 superscript, no superscript indicated that the compound was assigned in all experiments.

Fragments		Monomers	Accretion products				
C ₅ H ₆ O ₄ ^{E1}	C ₈ H ₁₀ O ₆	C ₁₀ H ₁₄ O ₅	C ₁₄ H ₂₀ O ₉	C ₁₇ H ₂₄ O ₇	C ₁₉ H ₂₆ O ₈ ^{E1,E2}	C ₂₀ H ₂₈ O ₉	
C ₅ H ₆ O ₅	C ₈ H ₁₀ O ₇	C ₁₀ H ₁₄ O ₆	C ₁₄ H ₂₂ O ₁₀	C ₁₇ H ₂₄ O ₉	C ₁₉ H ₂₈ O ₇	C ₂₀ H ₂₈ O ₁₁	
C ₅ H ₆ O ₆	C ₈ H ₁₀ O ₁₀ ^{E1}	C ₁₀ H ₁₄ O ₇	C ₁₄ H ₂₂ O ₁₁ ^{E1,E2}	C ₁₇ H ₂₄ O ₁₀ ^{E1,E2}	C ₁₉ H ₂₈ O ₈	C ₂₀ H ₃₀ O ₆	
C ₅ H ₆ O ₇	C ₈ H ₁₂ O ₅ ^{E1,E2}	C ₁₀ H ₁₄ O ₈	C ₁₄ H ₂₆ O ₁₁	C ₁₇ H ₂₄ O ₁₁	C ₁₉ H ₂₈ O ₉	C ₂₀ H ₃₀ O ₇	
C ₅ H ₆ O ₈ ^{E2}	C ₈ H ₁₂ O ₆	C ₁₀ H ₁₄ O ₉		C ₁₇ H ₂₄ O ₁₃ ^{E1,E2}	C ₁₉ H ₂₈ O ₁₀	C ₂₀ H ₃₀ O ₈	
C ₅ H ₇ O ₈	C ₈ H ₁₂ O ₇	C ₁₀ H ₁₄ O ₁₀	C ₁₅ H ₂₀ O ₁₄ ^{E1}	C ₁₇ H ₂₆ O ₈	C ₁₉ H ₂₈ O ₁₁	C ₂₀ H ₃₀ O ₉	
C ₅ H ₈ O ₇	C ₈ H ₁₂ O ₈	C ₁₀ H ₁₄ O ₁₁	C ₁₅ H ₂₂ O ₉	C ₁₇ H ₂₆ O ₉	C ₁₉ H ₂₈ O ₁₂ ^{E1,E2}	C ₂₀ H ₃₀ O ₁₀	
	C ₈ H ₁₂ O ₉		C ₁₅ H ₂₂ O ₁₀	C ₁₇ H ₂₆ O ₁₀	C ₁₉ H ₂₈ O ₁₃	C ₂₀ H ₃₀ O ₁₁	
C ₆ H ₆ O ₄ ^{E1,E3}	C ₈ H ₁₃ O ₈	C ₁₀ H ₁₅ O ₅	C ₁₅ H ₂₂ O ₁₁	C ₁₇ H ₂₆ O ₁₁	C ₁₉ H ₂₈ O ₁₄ ^{E1,E2}	C ₂₀ H ₃₀ O ₁₂	
C ₆ H ₁₀ O ₅	C ₈ H ₁₃ O ₉	C ₁₀ H ₁₅ O ₆	C ₁₅ H ₂₂ O ₁₂ ^{E1,E2}	C ₁₇ H ₂₆ O ₁₂	C ₁₉ H ₂₈ O ₁₅ ^{E1}	C ₂₀ H ₃₀ O ₁₃	
C ₆ H ₁₀ O ₆	C ₈ H ₁₄ O ₅	C ₁₀ H ₁₅ O ₇	C ₁₅ H ₂₂ O ₁₃ ^{E1}	C ₁₇ H ₂₆ O ₁₃ ^{E1,E2}	C ₁₉ H ₂₈ O ₁₆ ^{E1,E2}	C ₂₀ H ₃₀ O ₁₄	
C ₆ H ₁₀ O ₇	C ₈ H ₁₄ O ₆	C ₁₀ H ₁₅ O ₈	C ₁₅ H ₂₂ O ₁₄ ^{E1}	C ₁₇ H ₂₆ O ₁₄ ^{E1,E2}	C ₁₉ H ₃₀ O ₆	C ₂₀ H ₃₀ O ₁₅	
	C ₈ H ₁₄ O ₇	C ₁₀ H ₁₅ O ₉	C ₁₅ H ₂₄ O ₁₃ ^{E1,E2}	C ₁₇ H ₂₈ O ₈	C ₁₉ H ₃₀ O ₇	C ₂₀ H ₃₀ O ₁₆	
C ₇ H ₈ O ₅ ^{E3}	C ₈ H ₁₄ O ₈	C ₁₀ H ₁₅ O ₁₀	C ₁₅ H ₂₆ O ₁₀ ^{E1,E2}	C ₁₇ H ₂₈ O ₉	C ₁₉ H ₃₀ O ₈	C ₂₀ H ₃₀ O ₁₈	
C ₇ H ₈ O ₆ ^{E3}	C ₈ H ₁₄ O ₉	C ₁₀ H ₁₅ O ₁₁		C ₁₇ H ₂₈ O ₁₀	C ₁₉ H ₃₀ O ₉	C ₂₀ H ₃₂ O ₆	
C ₇ H ₈ O ₇		C ₁₀ H ₁₅ O ₁₂	C ₁₆ H ₂₂ O ₉ ^{E1,E2}	C ₁₇ H ₂₈ O ₁₁	C ₁₉ H ₃₀ O ₁₀	C ₂₀ H ₃₂ O ₇	
C ₇ H ₈ O ₈	C ₉ H ₁₂ O ₅		C ₁₆ H ₂₄ O ₉	C ₁₇ H ₂₈ O ₁₂	C ₁₉ H ₃₀ O ₁₁	C ₂₀ H ₃₂ O ₈	
C ₇ H ₁₀ O ₅ ^{E1,E3}	C ₉ H ₁₂ O ₆	C ₁₀ H ₁₆ O ₄	C ₁₆ H ₂₄ O ₁₀		C ₁₉ H ₃₀ O ₁₂	C ₂₀ H ₃₂ O ₉	
C ₇ H ₁₀ O ₆	C ₉ H ₁₂ O ₇	C ₁₀ H ₁₆ O ₅	C ₁₆ H ₂₄ O ₁₁	C ₁₈ H ₂₆ O ₉	C ₁₉ H ₃₀ O ₁₃	C ₂₀ H ₃₂ O ₁₀	
C ₇ H ₁₀ O ₇	C ₉ H ₁₂ O ₈	C ₁₀ H ₁₆ O ₆	C ₁₆ H ₂₄ O ₁₂ ^{E1,E2}	C ₁₈ H ₂₆ O ₁₀	C ₁₉ H ₃₀ O ₁₄ ^{E1,E2}	C ₂₀ H ₃₂ O ₁₁	
C ₇ H ₁₀ O ₈	C ₉ H ₁₂ O ₉	C ₁₀ H ₁₆ O ₇	C ₁₆ H ₂₆ O ₈	C ₁₈ H ₂₆ O ₁₁	C ₁₉ H ₃₀ O ₁₅ ^{E1,E2}	C ₂₀ H ₃₂ O ₁₂	
C ₇ H ₁₀ O ₉ ^{E1,E2}	C ₉ H ₁₂ O ₁₂ ^{E2}	C ₁₀ H ₁₆ O ₈	C ₁₆ H ₂₆ O ₉	C ₁₈ H ₂₆ O ₁₅ ^{E1}	C ₁₉ H ₃₀ O ₁₆ ^{E1}	C ₂₀ H ₃₂ O ₁₃	
C ₇ H ₁₀ O ₁₀	C ₉ H ₁₃ O ₉	C ₁₀ H ₁₆ O ₉	C ₁₆ H ₂₆ O ₁₀	C ₁₈ H ₂₈ O ₆	C ₁₉ H ₃₂ O ₇	C ₂₀ H ₃₂ O ₁₄	
C ₇ H ₁₄ O ₅ ^{E1,E2}	C ₉ H ₁₃ O ₁₀	C ₁₀ H ₁₆ O ₁₀	C ₁₆ H ₂₆ O ₁₁	C ₁₈ H ₂₈ O ₈	C ₁₉ H ₃₂ O ₈	C ₂₀ H ₃₂ O ₁₅	
C ₇ H ₁₄ O ₆	C ₉ H ₁₄ O ₄	C ₁₀ H ₁₆ O ₁₁	C ₁₆ H ₂₆ O ₁₂	C ₁₈ H ₂₈ O ₉ ^{E1}	C ₁₉ H ₃₂ O ₉	C ₂₀ H ₃₄ O ₆	
	C ₉ H ₁₄ O ₅		C ₁₆ H ₂₆ O ₁₃ ^{E2}	C ₁₈ H ₂₈ O ₁₀	C ₁₉ H ₃₂ O ₁₀	C ₂₀ H ₃₄ O ₇	
	C ₉ H ₁₄ O ₆	C ₁₀ H ₁₇ O ₆	C ₁₆ H ₂₈ O ₁₈ ^{E1,E2}	C ₁₈ H ₂₈ O ₁₁	C ₁₉ H ₃₂ O ₁₁	C ₂₀ H ₃₄ O ₈	
	C ₉ H ₁₄ O ₇	C ₁₀ H ₁₇ O ₇		C ₁₈ H ₂₈ O ₁₂ ^{E1,E2}	C ₁₉ H ₃₂ O ₁₂	C ₂₀ H ₃₄ O ₉	
	C ₉ H ₁₄ O ₈	C ₁₀ H ₁₇ O ₈		C ₁₈ H ₂₈ O ₁₃	C ₁₉ H ₃₂ O ₁₃ ^{E1}	C ₂₀ H ₃₄ O ₁₀	
	C ₉ H ₁₄ O ₉	C ₁₀ H ₁₇ O ₉		C ₁₈ H ₂₈ O ₁₄ ^{E1,E3}	C ₁₉ H ₃₂ O ₁₄ ^{E1,E2}	C ₂₀ H ₃₄ O ₁₁	
	C ₉ H ₁₄ O ₁₀	C ₁₀ H ₁₇ O ₁₀ ^{E1,E3}		C ₁₈ H ₂₈ O ₁₅ ^{E1}	C ₁₉ H ₃₂ O ₇	C ₂₀ H ₃₄ O ₁₂	
	C ₉ H ₁₆ O ₅	C ₁₀ H ₁₇ O ₁₁ ^{E3}		C ₁₈ H ₂₈ O ₁₆ ^{E1,E3}	C ₁₉ H ₃₂ O ₈	C ₂₀ H ₃₄ O ₁₃	
	C ₉ H ₁₆ O ₆			C ₁₈ H ₃₀ O ₇	C ₁₉ H ₃₂ O ₉		
	C ₉ H ₁₆ O ₇	C ₁₀ H ₁₈ O ₄		C ₁₈ H ₃₀ O ₈	C ₁₉ H ₃₂ O ₁₀		
	C ₉ H ₁₆ O ₈	C ₁₀ H ₁₈ O ₅		C ₁₈ H ₃₀ O ₉	C ₁₉ H ₃₂ O ₁₁		
		C ₁₀ H ₁₈ O ₆		C ₁₈ H ₃₀ O ₁₀	C ₁₉ H ₃₂ O ₁₂		
		C ₁₀ H ₁₈ O ₇		C ₁₈ H ₃₀ O ₁₁	C ₁₉ H ₃₂ O ₁₃ ^{E1,E3}		
		C ₁₀ H ₁₈ O ₈		C ₁₈ H ₃₀ O ₁₂	C ₁₉ H ₃₂ O ₁₄ ^{E1,E2}		
		C ₁₀ H ₁₈ O ₉		C ₁₈ H ₃₀ O ₁₃			
				C ₁₈ H ₃₀ O ₁₄ ^{E1}			

92 **S5 Estimation of change in peroxy radical steady state concentration between low and high HO₂/RO₂**

93 Starting from the balance equation **Eq. (S2)**, we derived an equation for the steady state concentration (indicated by subscript
 94 SS) of an [RO₂]_i (**Eq. (S3)**). The equations assume a primary production term *Pri_i* for [RO₂]_i, as well as only three
 95 significant loss pathways: The reaction with the pool of available [RO₂] with a bulk reaction rate constant *k_{RO2RO2}*, the
 96 reaction with [HO₂] with a reaction rate of *k_{RO2HO2}*=1.85·10⁻¹¹ cm³·s⁻¹ at 20 °C as defined in the MCM (Jenkin et al., 1997;
 97 Saunders et al., 2003) and the wall loss. A wall loss rate coefficient of 1/170 s was used, as determined by our measurements
 98 for HOM products (see supplement section Fehler! Verweisquelle konnte nicht gefunden werden.). The rate coefficient
 99 *k_{RO2RO2}* was varied in a range 1.0-5.0·10⁻¹² cm³·s⁻¹, typical values expected for substituted organic peroxy radicals (Jenkin et
 100 al., 2019), to determine what bulk rate coefficient would be reconcilable with our observations. To compare directly to the
 101 measured ratio of HOM-RO₂ signal, we calculated the RO₂ concentration ratio at high to low HO₂/RO₂ applying **Eq. (S4)**. In
 102 **Eq. (S4)** the primary production term *Pri_i* could be eliminated as the primary production was same at high and low
 103 HO₂/RO₂ in our experiments.

$$\frac{d[RO_2]_i}{dt} = Pri_i - k_{RO2RO2}[RO_2][RO_2]_i - k_{HO2}[HO_2][RO_2]_i - k_{wall}[RO_2]_i \quad (\text{S2})$$

$$[RO_2]_{i,SS} = \frac{Pri_i}{k_{RO2RO2}[RO_2] + k_{HO2}[HO_2] + k_{wall}} \quad (\text{S3})$$

$$\frac{[RO_2]_{i,SS,highHO2}}{[RO_2]_{i,SS,lowHO2}} = \frac{k_{RO2RO2}[RO_2]_{SS,lowHO2} + k_{HO2}[HO_2]_{SS,lowHO2} + k_{wall}}{k_{RO2RO2}[RO_2]_{SS,highHO2} + k_{HO2}[HO_2]_{SS,highHO2} + k_{wall}} \quad (\text{S4})$$

105 S6 Calculation of condensation rate constant k_{cond}

106 The condensation rate constant k_{cond} of each compound was calculated as shown in **Eq. (S5)**. Here α is the accommodation
107 coefficient and is set to 1. \bar{v} is the mean molecular speed calculated from the molar mass of the compound and S_{Ptot} is the
108 total particle surface measured in the chamber. f_{FS} is the Fuchs-Sutugin factor which is calculated as shown in **Eq. (S6)**,
109 where knn is the Knudsen Number calculated as shown in **Eq. (S7)**. \bar{s} represents the mean free path of the molecule and p_{dia}
110 the particle diameter. For p_{dia} we used the median diameter of the particle surface distribution measured (McFiggans et al.,
111 2019).

$$k_{cond} = \alpha * f_{FS} * \frac{\bar{v}}{4} * S_{Ptot} \quad (\text{S5})$$

$$f_{FS} = \frac{1 + knn}{1 + (0.75 * \frac{\alpha}{knn}) + knn + (0.283 * \alpha)} \quad (\text{S6})$$

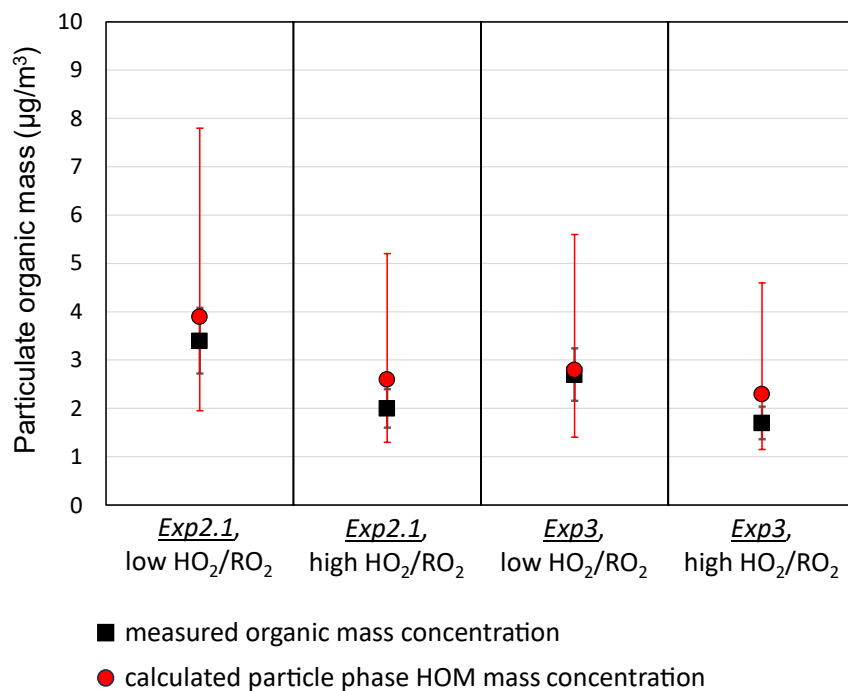
$$knn = \frac{2 * \bar{s}}{p_{dia}} \quad (\text{S7})$$

112 S7 Error estimation via error propagation

113 Error propagation was utilized to estimate the error of derived parameters. For a parameter q , the error is defined by the
114 errors of the variables x, \dots, z necessary to calculate q . The general equation to calculate the absolute uncertainty δq can be
115 found in **Eq. (S8)**. This equation is only valid if the uncertainties in x, \dots, z are independent and random. (Taylor, 1997)

$$\delta q = \sqrt{\left(\frac{\partial q}{\partial x} \delta x\right)^2 + \dots + \left(\frac{\partial q}{\partial z} \delta z\right)^2} \quad (\text{S8})$$

116 For all measured parameters the measured standard deviation in steady state was used as the absolute uncertainty. For
117 parameters that cannot be measured directly their uncertainties were calculated with error propagation as shown in **Eq. (S8)**.
118 For the diffusion coefficient and the OH concentration we used uncertainties reported in the literature: Tang et al. (2015)
119 reviewed diffusion coefficient calculation and came to the result that the difference between measurement and estimation via
120 the method of Fuller et al. (1966) are mostly below 10 %. Therefore, we assumed a 10 % uncertainty for the diffusion
121 coefficient of each formula composition. We assumed an uncertainty of 20 % for the OH concentration calculation as
122 published by Wildt et al. (2014).



124

125 Figure S3: Comparison of particulate, organic mass concentration (measured by AMS) and approximation from NO₃-
 126 MION-CIMS measurements. Error of AMS measurement is estimated as 20 %. For calculated particle phase HOM mass
 127 concentration we assumed an uncertainty of factor 2 in the calibration factor (He et al., 2023).

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