Supplementary material

Raquel González-Armas[1], Jordi Vilà-Guerau de Arellano[1,2], Mary Rose Mangan[1], Oscar Hartogensis[1], and Hugo de Boer[3]

[1]Meteorology and Air Quality Section, Wageningen University Research, 6708 PB Wageningen, the Netherlands
[2]Atmospheric Chemistry Department, Max Planck Institute for Chemistry, 55128 Mainz, Germany
[3]Department of Environmental Sciences, Faculty of Geosciences, Utrecht University, 3508 TA Utrecht, the Netherlands

Correspondence: Raquel González-Armas (raquel.gonzalezarmas@wur.nl)

1 Tendencies of the leaf gas exchange

This document contains instructions to calculate the tendency equations for the A-g$_s$ model as implemented in CLASS model (details of A-g$_s$ in CLASS are in appendix E of Vilà-Guerau de Arellano et al. 2015). We do not write the equations of the A-g$_s$ model here but we used the same formulation than the reference excepting than vapor pressure deficit is referred as VPD instead of D_S. The code needed for calculating the budget tendency equation for CLASS model output is in a Github repository[1]. This repository also contains the code needed to reproduce all the figures and analysis of the manuscript.

1.1 General approaches to calculate tendencies

The tendency equations have been computed with respect to two different set of environmental drivers. The first set is the one used in the present manuscript and has been termed (1) process-based tendencies. Here the set of environmental variables are PAR, T, VPD, C$_a$ and soil water content at the rootzone (w_2). The second set of environmental variables is PAR, T, air water vapor pressure (e), C$_a$ and w_2. The tendency equations derived with respect to this set has been termed (2) model-based tendencies.

1.1.1 Process-based tendencies

With this approach, partial tendencies are computed with respect to environmental variables that are known to directly control the plant photosynthesis and the dynamic stomatal movements. However, the environmental variables are not completely independent from each other. Specifically, VPD is known to depend on T, through the following expression:

$$VPD = e_{sat}(T) - e \tag{1}$$

Here, we are assuming that water vapor is saturated inside the sub-stomatal cavities, and that the temperature inside those cavities is equal to the atmospheric temperature. A partial derivative with respect to a variable x_i (x_i = PAR, C$_a$, VPD, T or

[1]The repository was uploaded from Rglezarm github profile and it can be accessed through the URL https://github.com/Rglezarm/LIAISE_manuscript

w_2) is calculated by leaving all the other variables from the set constant. Because of the tight relation between T and VPD, eq. (1), we highlight this fact of partial derivative by explicitly indicating in the tendency with respect to T (VPD) that VPD (T) has been kept constant by adding it as a sub-index. To keep VPD constant when T changes, the atmospheric vapor pressure, e, must balance the temperature change. According to this approach and to our formulation, we write the process-based tendency equation for a general variable Y (e.g., g_s, A_n, or TR_{leaf}) with the following mathematical expression.

$$\frac{dY}{dt} = \frac{\partial Y}{\partial PAR}\frac{dPAR}{dt} + \left(\frac{\partial Y}{\partial T}\right)_{VPD}\frac{dT}{dt} + \left(\frac{\partial Y}{\partial VPD}\right)_{T}\frac{dVPD}{dt} + \frac{\partial Y}{\partial C_a}\frac{dC_a}{dt} + \frac{\partial Y}{\partial w_2}\frac{dw_2}{dt} \tag{2}$$

1.1.2 Model-based tendencies

In a similar fashion to the previous approach, the model-based tendency equation for a general variable Y can be mathematically written as:

$$\frac{dY}{dt} = \frac{\partial Y}{\partial PAR}\frac{dPAR}{dt} + \frac{\partial Y}{\partial T}\frac{dT}{dt} + \frac{\partial Y}{\partial e}\frac{de}{dt} + \frac{\partial Y}{\partial C_a}\frac{dC_a}{dt} + \frac{\partial Y}{\partial w_2}\frac{dw_2}{dt} \tag{3}$$

Although these two approaches view the tendencies through different lens, they are directly linked to each other.

1.1.3 Relation between process-based and model-based tendencies

Because we known that VPD is a function of T and e, a direct link between process-based and model-based budget tendency equations can be obtained. The following equations depict the relation between the partial tendency terms of the two approaches.

$$\frac{\partial Y}{\partial T} = \left(\frac{\partial Y}{\partial T}\right)_{VPD} + \left(\frac{\partial Y}{\partial VPD}\right)_{T}\frac{\partial VPD}{\partial T} \tag{4}$$

$$\frac{\partial Y}{\partial e} = \left(\frac{\partial Y}{\partial VPD}\right)_{T}\frac{\partial VPD}{\partial e} \tag{5}$$

Because the functional form of VPD is known (eq. (1)), its partial derivative with respect to T and e can be computed.

$$\frac{\partial VPD}{\partial T} = \frac{de_{sat}}{dT} \tag{6}$$

$$\frac{\partial VPD}{\partial e} = -1 \tag{7}$$

Considering all the concepts of this section we can construct the following final expression to calculate the model-based tendency equations from the process-based ones.

$$\frac{dY}{dt} = \frac{\partial Y}{\partial PAR}\frac{dPAR}{dt} + \left[\left(\frac{\partial Y}{\partial T}\right)_{VPD} + \left(\frac{\partial Y}{\partial VPD}\right)_{T}\frac{\partial e_{sat}}{\partial T}\right]\frac{dT}{dt} - \left(\frac{\partial Y}{\partial VPD}\right)_{T}\frac{de}{dt} + \frac{\partial Y}{\partial C_a}\frac{dC_a}{dt} + \frac{\partial Y}{\partial w_2}\frac{dw_2}{dt} \tag{8}$$

1.2 Strategy to calculate the budget tendency equations for A-g_s model

Now that we have described the connection between the process-based and model-based budget tendency equations, we will focus on deriving the process-based ones, eq. (2), for the A-g_s scheme. The tendency equations can be computed for any intermediate variable of the leaf gas exchange. Note that in the previous section we have denoted such generic variable as Y. This fact implies that we can quantify the effect that changes of the environmental variables have in any variable of the leaf gas exchange. Our final goal is to do that for the stomatal conductance to water vapor (g_s), the net assimilation rate (A_n) and the leaf transpiration (TR_{leaf}).

In leaf gas exchange models, these variables are generally linked to each other. Their dependency varies from one model (or even implementation of a model) to another. $A - g_s$ model structure can be summarized as follows. The first step of the model is to calculate the variables that depend solely on temperature. After that, C_i is computed through several equations that capture its dependency with T, VPD and C_a. These variables allow the calculation of CO_2 primary productivity (A_m). Subsequently, gross primary productivity is calculated for a soil at field capacity (A_g^*). This means that the plant is completely unstressed in terms of soil water content. At this step, the dependency on PAR is also included. The fourth step is to include the soil water content dependency of gross primary productivity. This is done by applying a soil water stress function ($f(w_2)$) that factorize the gross primary productivity at field capacity. At this point, both the stomatal conductance to water vapor, net assimilation rate of CO_2 and leaf transpiration can be computed. Table 1 defines A-g_s variable that may not have been introduced before. To see the A-g_s parameters, the reader is referred to Table 3 of the manuscript.

Taking advantage of this structure, we calculate the tendency equations as follows:

1. **Calculate the total temporal derivatives of the environmental variables.** $\frac{dPAR}{dt}$, $\frac{dT}{dt}$, $\frac{dVPD}{dt}$, $\frac{dC_a}{dt}$ and $\frac{dw_2}{dt}$ are calculated using a numerical technique called symmetric difference quotient applied to the output of the numerical experiments performed with CLASS.

2. **Calculate the tendency equation of the CO_2 primary productivity ($\mathrm{A_m}$).** Equations in Sect. 1.3.

3. **Calculate tendency equation of the gross primary productivity under unstressed water situations ($\mathrm{A_g}^*$).** Equations in Sect. 1.4.

4. **Calculate the tendency equation of the gross primary productivity at a particular soil water content in the root zone ($\mathrm{A_g}$).** Equations in Sect. 1.5.

5. **Calculate the tendency equation of the net leaf assimilation rate ($\mathrm{A_n}$).** Equations in Sect. 1.6.

6. **Calculate the tendency equation of the stomatal conductance to water vapor ($\mathrm{g_{sw}}$).** Equations in Sect. 1.7.

7. **Calculate the tendency equation of the leaf transpiration ($\mathrm{TR_{leaf}}$).** Equations in Sect. 1.8.

Table 1. List of variables used in the A-g_s model that may have not been introduced before.

Variables	
Symbol	Definition
α (mg J^{-1})	Light use efficiency
A_g (mg m_{leaf}^{-2} s^{-1})	CO_2 gross primary productivity at leaf level
A_g^* (mg m_{leaf}^{-2} s^{-1})	Unstressed CO_2 gross primary productivity at leaf level
A_m (mg m_{leaf}^{-2} s^{-1})	CO_2 primary productivity
$A_{m,max}$ (mg m_{leaf}^{-2} s^{-1})	CO_2 maximal primary productivity
A_n (mg m_{leaf}^{-2} s^{-1})	Net CO_2 assimilated rate
R_d (mg m_{leaf}^{-2} s^{-1})	Dark respiration
Γ (ppmv)	CO_2 compensation point
C_{frac} (-)	Fraction of the concentration (C_i-Γ)/(C_a-Γ)
D_0 (kPa)	Water vapor pressure deficit when stomata close
g_m (mm s^{-1})	Mesophyll conductance

1.3 The tendency equation of A_m

A_m depends on C_a, T and VPD. Its tendency equation can be described as follows:

$$\frac{dA_m}{dt} = \frac{\partial A_m}{\partial C_a}\frac{dC_a}{dt} + \left(\frac{\partial A_m}{\partial T}\right)_{VPD}\frac{dT}{dt} + \left(\frac{\partial A_m}{\partial VPD}\right)_{T}\frac{dVPD}{dt} \tag{9}$$

1.3.1 Dependency on C_a

$$\frac{\partial A_m}{\partial C_a} = g_m C_{frac}\left(1 - \frac{A_m}{A_{mmax}}\right) \tag{10}$$

1.3.2 Dependency on VPD at constant T

$$\left(\frac{\partial A_m}{\partial VPD}\right)_T = \frac{\partial A_m}{\partial C_i}\frac{\partial C_i}{\partial C_{frac}}\left(\frac{\partial C_{frac}}{\partial VPD}\right)_T \tag{11}$$

To calculate the above expression, some additional terms are needed:

$$\frac{\partial A_m}{\partial C_i} = g_m\left(1 - \frac{A_m}{A_{mmax}}\right) \tag{12}$$

$$\frac{\partial C_i}{\partial C_{frac}} = C_a - \Gamma \tag{13}$$

$$\left(\frac{\partial C_{frac}}{\partial VPD}\right)_T = -a_d \tag{14}$$

1.3.3 Dependency on T at constant VPD

$$\begin{aligned}\left(\frac{dA_m}{dT}\right)_{VPD} =& \frac{\partial A_m}{\partial A_{mmax}}\frac{dA_{mmax}}{dT} + \frac{\partial A_m}{\partial g_m}\frac{dg_m}{dT} + \frac{\partial A_m}{\partial \Gamma}\frac{d\Gamma}{dt} \\ &+ \frac{\partial A_m}{\partial C_i}\left[\frac{\partial C_i}{\partial \Gamma}\frac{d\Gamma}{dT} + \frac{\partial C_i}{\partial C_{frac}}\left(\frac{\partial C_{frac}}{f_{min}} + \frac{\partial C_{frac}}{\partial D_0}\frac{\partial D_0}{f_{min}}\right)\left(\frac{\partial f_{min}}{\partial f_{min0}}\frac{\partial f_{min0}}{\partial g_m} + \frac{\partial f_{min}}{\partial g_m}\right)\frac{dg_m}{dT}\right]\end{aligned} \tag{15}$$

To calculate the above expression, some temperature dependent functions are needed:

$$\frac{\partial \Gamma}{\partial T} = 0.1 \cdot \Gamma \cdot \log Q_{10\Gamma} \tag{16}$$

$$\frac{\partial A_{mmax}}{\partial T} = 0.1 \cdot A_{mmax}\left[\log Q_{10Am} + 3 \cdot \frac{e^{0.3(T_{1Am}-T)} - e^{0.3(T-T_{2Am})}}{(1+e^{0.3(T_{1Am}-T)})(1+e^{0.3(T-T_{2Am})})}\right] \tag{17}$$

$$\frac{\partial g_m}{\partial T} = 0.1 \cdot g_m\left[\log Q_{10gm} + 3 \cdot \frac{e^{0.3(T_{1gm}-T)} - e^{0.3(T-T_{2gm})}}{(1+e^{0.3(T_{1gm}-T)})(1+e^{0.3(T-T_{2gm})})}\right] \quad ; \tag{18}$$

together with other terms

$$\frac{\partial A_m}{\partial A_{mmax}} = \frac{A_m}{A_{mmax}} - \frac{g_m C_{frac}(C_a - \Gamma)}{A_{mmax}}\left(1 - \frac{A_m}{A_{mmax}}\right) \tag{19}$$

$$\frac{\partial A_m}{\partial g_m} = C_{frac}(C_a - \Gamma)\left(1 - \frac{A_m}{A_{mmax}}\right) \tag{20}$$

$$\frac{\partial A_m}{\partial \Gamma} = -g_m C_{frac}\left(1 - \frac{A_m}{A_{mmax}}\right) \tag{21}$$

$$\frac{dA_m}{dC_i} = g_m\left(1 - \frac{A_m}{A_{mmax}}\right) \tag{22}$$

$$\frac{dC_i}{d\Gamma} = 1 - C_{frac} \tag{23}$$

$$\frac{dC_i}{dC_{frac}} = C_a - \Gamma \tag{24}$$

$$\frac{\partial C_{frac}}{\partial f_{min}} = \frac{VPD}{D_0} \tag{25}$$

$$\frac{\partial C_{frac}}{\partial D_0} = (f_0 - f_{min})\frac{VPD}{D_0^2} \tag{26}$$

$$\frac{\partial D_0}{\partial f_{min}} = -\frac{1}{a_d} \tag{27}$$

$$\frac{\partial f_{min}}{\partial g_m} = \frac{g_{minw}}{1.6 \cdot g_m}\frac{1}{\sqrt{f_{min0}^2 + \frac{4 \cdot g_{minw}}{1.6}g_m}} - \frac{f_{min}}{g_m} \tag{28}$$

$$\frac{\partial f_{min}}{\partial f_{min0}} = -\frac{f_{min}}{2 \cdot g_m f_{min} + f_{min0}} \tag{29}$$

$$\frac{\partial f_{min0}}{\partial g_m} = -\frac{1}{9} \tag{30}$$

1.4 The tendency equation of A_g^*

$$\frac{dA_g^*}{dt} = \frac{\partial A_g^*}{\partial PAR}\frac{dPAR}{dt} + \frac{\partial A_g^*}{\partial C_a}\frac{dC_a}{dt} + \left(\frac{\partial A_g^*}{\partial T}\right)_{VPD}\frac{dT}{dt} + \left(\frac{\partial A_g^*}{\partial VPD}\right)_{T}\frac{dVPD}{dt} \quad ; \tag{31}$$

with

1.4.1 Dependency on PAR

$$\frac{\partial A_g^*}{\partial PAR} = \alpha\left(1 - \frac{A_g^*}{A_m + R_{dark}}\right) \tag{32}$$

1.4.2 Dependency on C_a

$$\frac{\partial A_g^*}{\partial C_a} = \left(\frac{\partial A_g^*}{\partial R_{dark}}\frac{\partial R_{dark}}{\partial A_m} + \frac{\partial A_g^*}{\partial A_m}\right)\frac{\partial A_m}{\partial C_a} + \frac{\partial A_g^*}{\partial \alpha}\frac{\partial \alpha}{\partial C_a} \tag{33}$$

To calculate the above expression some additional terms are needed:

$$\frac{\partial A_g^*}{\partial R_{dark}} = \frac{A_g^*}{A_m + R_{dark}} - \frac{\alpha PAR}{A_m + R_{dark}}\left(1 - \frac{A_g^*}{A_m + R_{dark}}\right) \tag{34}$$

$$\frac{\partial R_{dark}}{\partial A_m} = \frac{1}{9} \tag{35}$$

$$\frac{\partial A_g^*}{\partial A_m} = \frac{\partial A_g^*}{\partial R_{dark}} \tag{36}$$

$$\frac{\partial A_g^*}{\partial \alpha} = PAR\left(1 - \frac{A_g^*}{A_m + R_{dark}}\right) \tag{37}$$

$$\frac{\partial \alpha}{\partial C_a} = \frac{3 \cdot \alpha_0 \Gamma}{(C_a + 2\Gamma)^2} \tag{38}$$

1.4.3 Dependency on VPD at constant T

$$\left(\frac{\partial {A_g}^*}{\partial VPD}\right)_T = \left(\frac{\partial A_g^*}{\partial R_{dark}}\frac{\partial R_{dark}}{\partial A_m} + \frac{\partial A_g^*}{\partial A_m}\right)\left(\frac{\partial A_m}{\partial VPD}\right)_T \tag{39}$$

1.4.4 Dependency on T at constant VPD

$$\left(\frac{\partial A_g^*}{\partial T}\right)_{VPD} = \left(\frac{\partial A_g^*}{\partial R_{dark}}\frac{\partial R_{dark}}{\partial A_m} + \frac{\partial A_g^*}{\partial A_m}\right)\left(\frac{\partial A_m}{\partial T}\right)_{VPD} + \frac{\partial A_g^*}{\partial \alpha}\frac{\partial \alpha}{\partial \Gamma}\frac{d\Gamma}{dT} \tag{40}$$

$$\frac{\partial \alpha}{\partial \Gamma} = -\frac{3 \cdot \alpha_0 C_a}{(C_a + 2\Gamma)^2} \tag{41}$$

1.5 The tendency equation of $\mathrm{A_g}$

$$\frac{dA_g}{dt} = \frac{\partial A_g}{\partial PAR}\frac{dPAR}{dt} + \frac{\partial A_g}{\partial C_a}\frac{dC_a}{dt} + \left(\frac{\partial A_g}{\partial T}\right)_{VPD}\frac{dT}{dt} + \left(\frac{\partial A_g}{\partial VPD}\right)_T\frac{dVPD}{dt} + \frac{\partial A_g}{\partial w_2}\frac{dw_2}{dt} \tag{42}$$

As mentioned previously, the gross primary productivity (A_g) is calculated from that under unstressed water situations (A_g^*) and a soil water stress fucntion ($\beta(w_2)$), $A_g = A_g^* \cdot \beta(w_2)$. Similarly the tendency equation of $\mathrm{A_g}$ can be computed from that of A_g^* and an additional term:

$$\frac{dA_g}{dt} = \beta\frac{dA_g^*}{dt} + A_g^*\frac{d\beta(w_2)}{dw_2}\frac{dw_2}{dt} \tag{43}$$

1.5.1 Dependency on PAR

$$\frac{\partial A_g}{\partial PAR} = \frac{\partial A_g^*}{\partial PAR} \cdot \beta \tag{44}$$

1.5.2 Dependency on $\mathrm{C_a}$

$$\frac{\partial A_g}{\partial C_a} = \frac{\partial A_g^*}{\partial C_a} \cdot \beta \tag{45}$$

1.5.3 Dependency on VPD at constant T

$$\left(\frac{\partial A_g}{\partial VPD}\right)_T = \left(\frac{\partial A_g^*}{\partial VPD}\right)_T \cdot \beta \tag{46}$$

1.5.4 Dependency on T at cosntant VPD

$$\left(\frac{\partial A_g}{\partial T}\right)_{VPD} = \left(\frac{\partial A_g^*}{\partial T}\right)_{VPD} \cdot \beta \tag{47}$$

1.5.5 Dependency on $\mathrm{w_2}$

$$\frac{\partial A_g}{\partial w_2} = A_g^*\frac{d\beta(w_2)}{dw_2} \tag{48}$$

A_g^* is given by the model and as a consequence, the only term we analytically solve in this section is $\frac{d\beta(w_2)}{dw_2}$.

The functional form of the water-stress function β implemented in CLASS model is the one presented by Combe et al. (2016). The following equations govern the functional form and were proposed in the cited manuscript (see equations (13) and (14) of the manuscript).

$$SMI = \frac{w_2 - w_{wp}}{w_{fc} - w_{wp}} \tag{49}$$

$$\beta = \frac{1 - e^{-P(C_\beta)SMI}}{1 - e^{-P(C_\beta)}} \tag{50}$$

$$P(C_\beta) = \begin{cases} 6.4 \cdot C_\beta & \text{if } 0\ \% \leq C_\beta < 25\ \%, \\ 7.6 \cdot C_\beta - 0.3 & \text{if } 25\ \% \leq C_\beta < 50\ \%, \\ 2^{3.66 \cdot C_\beta + 0.34} - 1 & \text{if } 50\ \% \leq C_\beta \leq 100\ \%. \end{cases} \tag{51}$$

Taking into account that functional form, the analytical derivative of β with respect to w_2 is:

$$\frac{d\beta}{dw_2} = \frac{1}{w_{fc} - w_{wp}} \frac{P(C_\beta)e^{-P(C_\beta)SMI}}{1 - e^{-P(C_\beta)}} \tag{52}$$

1.6 The tendency equation of $\mathbf{A_n}$

A_n is the difference between the gross primary productivity and the dark respiration.

$$A_n = A_g - R_{dark} \tag{53}$$

The budget tendency equation of A_n is:

$$\frac{dA_n}{dt} = \frac{\partial A_n}{\partial PAR}\frac{dPAR}{dt} + \frac{\partial A_n}{\partial C_a}\frac{dC_a}{dt} + \left(\frac{\partial A_n}{\partial T}\right)_{VPD}\frac{dT}{dt} + \left(\frac{\partial A_n}{\partial VPD}\right)_T\frac{dVPD}{dt} + \frac{\partial A_n}{\partial w_2}\frac{dw_2}{dt} \tag{54}$$

which can be related to that of A_g

$$\frac{dA_n}{dt} = \frac{dA_g}{dt} - \frac{dR_{dark}}{dA_m}\frac{dA_m}{dt} \tag{55}$$

1.7 The budget tendency equation of $\mathbf{g_s}$ and $\mathbf{g_{sc}}$

The stomatal conductance to carbon dioxide g_{sc} is calculated through the following equation:

$$g_{sc} = g_{min,c} + \frac{a_1 A_g}{(C_a - \Gamma)\left(1 - \frac{VPD}{D_*}\right)} \tag{56}$$

The total temporal derivatives of g_s and g_{sc} are related, eq. (57). Therefore, we only need to calculate the budget tendency equation for one of the two.

$$\frac{dg_s}{dt} = \mu \cdot \frac{dg_{sc}}{dt} \tag{57}$$

where μ is the ratio of the molecular diffusivities between water vapor and carbon dioxide and is approximately 1.6.

The tendency equation for g_{sc} is:

$$\frac{dg_{sc}}{dt} = \frac{\partial g_{sc}}{\partial PAR}\frac{dPAR}{dt} + \frac{\partial g_{sc}}{\partial C_a}\frac{dC_a}{dt} + \left(\frac{\partial g_{sc}}{\partial T}\right)_{VPD}\frac{dT}{dt} + \left(\frac{\partial g_{sc}}{\partial VPD}\right)_{T}\frac{dVPD}{dt} + \frac{\partial g_{sc}}{\partial w_2}\frac{dw_2}{dt} \tag{58}$$

1.7.1 Dependency on PAR

$$\frac{\partial g_{sc}}{\partial PAR} = \frac{\partial g_{sc}}{\partial A_g}\frac{\partial A_g}{\partial PAR} \tag{59}$$

$$\frac{\partial g_{sc}}{\partial A_g} = \frac{a_1}{(C_a - \Gamma)\left(1 - \frac{VPD}{D_*}\right)} \tag{60}$$

1.7.2 Dependency on $\mathbf{C_a}$

$$\frac{\partial g_{sc}}{\partial C_a} = \left(\frac{\partial g_{sc}}{\partial C_a}\right)_{A_g} + \frac{\partial g_{sc}}{\partial A_g}\frac{\partial A_g}{\partial C_a} \tag{61}$$

$$\left(\frac{\partial g_{sc}}{\partial C_a}\right)_{A_g} = -\frac{g_{sc} - g_{minc}}{C_a - \Gamma} \tag{62}$$

$$\frac{\partial g_{sc}}{\partial A_g} = \frac{g_{sc} - g_{minc}}{A_g} \tag{63}$$

1.7.3 Dependency on VPD at constant T

$$\left(\frac{\partial g_{sc}}{\partial VPD}\right)_{T} = \left(\frac{\partial g_{sc}}{\partial VPD}\right)_{A_g,T} + \frac{\partial g_{sc}}{\partial A_g}\left(\frac{\partial A_g}{\partial VPD}\right)_{T} \tag{64}$$

$$\left(\frac{\partial g_{sc}}{\partial VPD}\right)_{A_g,T} = -\frac{g_{sc} - g_{minc}}{D_* + VPD} \tag{65}$$

1.7.4 Dependency on T at constant VPD

$$\left(\frac{\partial g_{sc}}{\partial T}\right)_{VPD} = \left(\frac{\partial g_{sc}}{\partial \Gamma}\right)_{A_g} \frac{d\Gamma}{dt} + \frac{\partial g_{sc}}{\partial A_g}\left(\frac{\partial A_g}{\partial T}\right)_{VPD} \tag{66}$$

$$\left(\frac{\partial g_{sc}}{\partial \Gamma}\right)_{A_g,T} = \frac{g_{sc} - g_{minc}}{C_a - \Gamma} \tag{67}$$

1.8 Tendency equation for $\mathbf{TR_{leaf}}$

In this research, we have estimated TR_{leaf} as:

$$TR_{leaf} = g_s \rho \frac{0.622}{P_s} VPD \tag{68}$$

where ρ is the air density and P_S the surface pressure taken as 101300 Pa. The tendency equation of TR_{leaf} has the following form

$$\frac{dTR_{leaf}}{dt} = \frac{\partial TR_{leaf}}{\partial PAR}\frac{dPAR}{dt} + \frac{\partial TR_{leaf}}{\partial C_a}\frac{dC_a}{dt} + \left(\frac{\partial TR_{leaf}}{\partial T}\right)_{VPD}\frac{dT}{dt} + \left(\frac{\partial TR_{leaf}}{\partial VPD}\right)_{T}\frac{dVPD}{dt} + \frac{\partial TR_{leaf}}{\partial w_2}\frac{dw_2}{dt} \tag{69}$$

1.8.1 Dependency on PAR

$$\frac{\partial TR_{leaf}}{\partial PAR} = \frac{dTR_{leaf}}{dg_s}\frac{dg_s}{dPAR} \tag{70}$$

$$\frac{dTR_{leaf}}{dg_s} = \rho \frac{0.622}{P_s} VPD \tag{71}$$

1.8.2 Dependency on C_a

$$\frac{\partial TR_{leaf}}{\partial C_a} = \frac{dTR_{leaf}}{dg_s}\frac{\partial g_s}{\partial C_a} \tag{72}$$

1.8.3 Dependency on VPD at constant T

$$\left(\frac{\partial TR_{leaf}}{\partial VPD}\right)_T = \frac{dTR_{leaf}}{dg_s}\left(\frac{\partial g_s}{\partial VPD}\right)_T + g_s \rho \frac{0.622}{P_s} \tag{73}$$

1.8.4 Dependency on T at constant VPD

$$\left(\frac{\partial TR_{leaf}}{\partial T}\right)_{VPD} = \frac{dTR_{leaf}}{dg_s}\left(\frac{\partial g_s}{\partial T}\right)_{VPD} \tag{74}$$

1.8.5 Dependency on $\mathbf{w_2}$

$$\frac{\partial TR_{leaf}}{\partial w_2} = \frac{dTR_{leaf}}{dg_s}\frac{\partial g_s}{\partial w_2} \tag{75}$$

References

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