

# Microphysical modelling of aerosol scavenging by different types of clouds.

## Description and validation of the approach

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### **Short abstract**

A new in-cloud scavenging scheme is proposed. It is based on a microphysical model of cloud formation and may be applied to long-distance atmospheric transport models (>100 km) and climatic models. This model is applied to for the two most extreme precipitating cloud types, in terms of both relative humidity and vertical extension: cumulonimbus and stratus.

### **Abstract**

With dry deposition and below-cloud scavenging, in-cloud scavenging is one of the three components of aerosol transfer from the atmosphere to the ground. There is no experimental validation of in-cloud particle scavenging models for all cloud types that is not impacted by uncertainties concerning below-cloud scavenging. In this article, the choice was made to start with a recognised and validated microphysical cloud formation model (DESCAM) to extract a scheme of aerosol scavenging by clouds, valid for different cloud types. The resulting model works for the two most extreme precipitation clouds: from cumulonimbus to stratus. It is based on data accessible a priori from Numerical Weather Prediction (NWP) outputs, i.e., the intensity of the rain and the relative humidity in the cloud. The diagnostic of the altitude of the cloud base proves to be a key parameter, and accuracy in this regard is vital. This new in-cloud scavenging scheme is intended for use in long-distance (> 100 km) Atmospheric Transport Models (ATMs) or Global Climate Models (GCMs).

### **Introduction**

Clouds are an essential component of the troposphere. They play a central role in meteorological forecasting and in the water cycle on the planet (Zhang *et al.*, 2020). Similarly, by interacting with solar radiation, they make a significant contribution to the terrestrial radiation balance (Twomey, 1974; Wang and Su, 2013). Moreover, they are often cited as one of the main sources of uncertainty in climate prediction models (Bony and Dufresne, 2005; Palmer, 2014). They can seriously disrupt air traffic, and even produce aircraft crashes (e. g. Air France flight 447 Rio-Paris air disaster).

By scavenging aerosols, they contribute to improve air quality (Leaith *et al.*, 1987; Sievering *et al.*, 1984), but also to impact soil pollution, through the deposition of atmospheric pollutants via precipitation (Clark and Smith, 1988; Flossmann, 1998). In case of severe nuclear accidents, radioactive aerosol particles might be released into the troposphere (De Cort, 1998 ; Baklanov and Sørensen, 2001 ; Adachi *et al.*, 2013). When radionuclides are emitted into the environment, it is essential, in order to protect populations, to jointly assess the concentrations of radioactive aerosols in the atmospheric boundary layer, as well as their transfer to the ground. Thus, while an accident is occurring, it is necessary to accurately assess the exposures of populations, both by inhalation and by ingestion (Mathieu *et al.*, 2004; Quélo *et al.*, 2007; Quérel *et al.*, 2012).

In nature, deposition of aerosols (and therefore a fortiori of particulate radionuclides) on the ground consists of the contribution of dry deposition and of wet deposition (Slinn 1977). Dry deposition is approximately 1000 times less effective than wet deposition but is the only mechanism operating when there is no precipitation. To date, there are still many uncertainties about the modelling of these two deposition pathways (Petroff *et al.*, 2008, Croft *et al.*, 2010 and Ervens, 2015).

44 Flossmann (1998) used the DESCAM model (Flossmann *et al.*, 1985, 1987, 1988) to assess that, for a droplet from a convective cloud, about 70% of the mass  
 45 of particles the droplet contains when deposited on the ground was incorporated into the droplet in the cloud. This result is consistent with the  
 46 measurements in the environment of Laguionie *et al.*, (2014), which estimate the cloud to be 60% responsible for the total downwash of particles.

47 Our objective in this article is to establish theoretically a scavenging coefficient applicable to clouds. Scavenging by clouds is more challenging to model than  
 48 scavenging by rain, under the cloud, as it is much more sensitive to certain input parameters. Rain scavenging is only controlled by a single microphysical  
 49 mechanism: collection by raindrops (Kerker and Hampl, 1974; Beard, 1974; Grover *et al.*, 1977; Wang and Pruppacher, 1977; Lai *et al.*, 1978; Pranesha and  
 50 Kamra, 1996; Vohl *et al.*, 1999; Quérel *et al.*, 2014; Lemaitre *et al.*, 2017), whereas cloud scavenging encompasses a set of mechanisms which will firstly  
 51 make it possible to incorporate aerosols into the cloud droplets (activation, collection, ice nucleation, collection by crystals) then, secondly, to convert a  
 52 fraction of the cloud hydrometeors into raindrops (condensation, coalescence, Bergeron effects). Only after raindrops have been deposited on the ground  
 53 is the atmosphere washed out and, by the same process, the soil contaminated. Furthermore, most atmospheric transport models use significantly different  
 54 schemes to model scavenging by cloud and by rain. Quérel *et al.*, 2021 summarised a few of them in Table 3 of their article.

55 Therefore, in theoretically assessing cloud scavenging, the use of a cloud formation model such as DESCAM (DEtailed SCAvenging Model), forms a good  
 56 foundation. This model, developed by Andrea Flossmann and her group since the mid-80s (Flossmann *et al.*, 1985; Flossmann, 1998; Monier *et al.*, 2006;  
 57 Leroy *et al.*, 2007; Planche *et al.*, 2007; Flossmann and Wobrock, 2010; Hiron and Flossmann, 2015; Dépée, 2019), makes it possible, through a detailed  
 58 microphysical description, to model clouds from their formation through to precipitation, and to monitor the aerosols and what becomes of them once  
 59 incorporated into the droplets.

60 In this article, we will show how, using a model like DESCAM, it is possible to theoretically calculate a scavenging coefficient in the cloud, on the scale of the  
 61 cloud system. We will apply this approach to two extreme types of cloud: a cumulonimbus (CCOPE, Dye *et al.*, 1986) and a stratus (Zhang *et al.*, 2004). This  
 62 approach will then be compared to the models derived from the deposits observed following the Fukushima nuclear accident (Leadbetter *et al.*, 2015; Quérel  
 63 *et al.*, 2021). Finally, in the last part we will present, a theoretical scheme of the scavenging coefficient, applicable to any type of cloud, will be proposed.  
 64 We begin by considering some key elements of the theoretical context and some definitions.

## 65 **1. Definitions and theoretical context**

### 66 **1.1. Definition of cloud scavenging**

67 In large range transport models, the description of scavenging shall remain simple, the operational scientific community models it through a parametrisation  
 68 involving the cloud scavenging coefficient ( $\Lambda_{cloud}$ ). It is defined as the fraction of pollutants that is transferred from the atmosphere to precipitation (then  
 69 to the ground) per unit of time. In this article, we will focus on pollutants carried by aerosols (and not gaseous pollutants). The scavenging coefficient is  
 70 therefore defined spectrally thus:

$$71 \quad \left. \frac{d\mathcal{N}(d_{ap})}{\mathcal{N}(d_{ap})} \right|_{cloud} = \left. \frac{d\mathcal{M}(d_{ap})}{\mathcal{M}(d_{ap})} \right|_{cloud} = -\Lambda_{cloud}(d_{ap}) \cdot dt \quad \text{Equation 1}$$

72 In this equation  $\mathcal{N}(d_{ap})$  and  $\mathcal{M}(d_{ap})$  are respectively the concentrations in number and in mass of aerosols of diameter  $d_{ap}$  per unit of air volume;  
 73 likewise,  $d\mathcal{N}(d_{ap})$  and  $d\mathcal{M}(d_{ap})$  are respectively the variations in concentration in number and in mass of aerosols of diameter  $d_{ap}$ , in relation to their  
 74 transfer into precipitation, per unit of time. The two definitions are considered equal when expressed spectrally, assuming a uniform density of all aerosol  
 75 particles. In this study, we specifically considered aerosol particles composed of ammonium sulphate, thus confirming this equality. However, in real  
 76 atmospheric conditions, aerosol particle density is typically not uniform. In such cases, it becomes crucial to specify whether we are referring to a mass  
 77 scavenging coefficient or a **number one**. To prevent any confusion, **in the rest of the article**, the exponent  $m$  is introduced to the scavenging coefficient  
 78  $\Lambda_{cloud}^m$ .

79 The approach we use is to apply this definition to an elementary volume of cloud (volume outlined in red in Figure 1). This volume is bounded at its base by  
 80 an arbitrary section ( $dS$ ) aligned with the base of the cloud, with this volume extending vertically to the cloud summit.

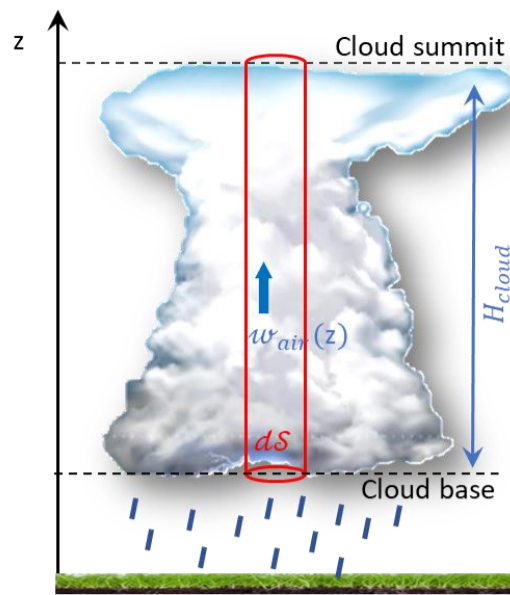


Figure 1. Definition of the scavenging coefficient at the scale of a cloud

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84 In this elementary cloud volume, it is elementary to calculate the variation in the average mass concentration of aerosols of diameter  $d_{ap}$ , in relation to  
85 their transfer into precipitation:

86

$$87 \quad d\mathcal{M}(d_{ap}) = - \frac{\phi_{ap,precip}(d_{ap}) \cdot dS \cdot dt}{dV_{cloud}} \quad \text{Equation 2}$$

88

89 In this equation,  $\phi_{ap,precip}(d_{ap})$  is the mass flow of dry particles of diameter ( $d_{ap}$ ) leaving the cloud via precipitation (solids and liquids), and  $dV_{cloud}$  is the  
90 elementary volume of cloud considered ( $dV_{cloud} = H_{cloud} \cdot dS$ ).

$$\Delta_{cloud}^m(d_{ap}) = - \frac{1}{dt} \frac{d\mathcal{M}(d_{ap})}{\langle \mathcal{M}(d_{ap}) \rangle_{cloud}} \Big|_{cloud} = \frac{\phi_{ap,precip}(d_{ap})|_{dS}}{\langle \mathcal{M}(d_{ap}) \rangle_{cloud} \cdot H_{cloud}} \quad \text{Equation 3}$$

91 In this equation,  $\langle \mathcal{M}(d_{ap}) \rangle$  is the average mass concentration (over the thickness of the cloud) of dry particles of diameter  $d_{ap}$ . It is noteworthy that  
92  $\langle \mathcal{M}(d_{ap}) \rangle$  is not the average concentration of interstitial aerosols in the cloud but the average concentration of particles, which includes, in addition to the  
93 interstitial aerosols, all the particles included in the droplets and potentially in the ice phase. Thus, if we jointly determine  $\langle \mathcal{M}(d_{ap}) \rangle$ ,  $\phi_{ap,precip}$  as well  
94 as the thickness of the cloud  $H_{cloud}$ , it is possible to deduce a scavenging coefficient.

95 The average particle concentration is calculated, using Equation 4, by spatially averaging, over the entire thickness of the cloud, the concentrations of  
96 interstitial aerosols (of diameters  $d_{ap}$ )  $\mathcal{M}_{int}(z, d_{ap})$ , the concentrations of particles in the drops ( $\mathbb{M}(z, d_{ap})$ ), and the concentrations in the ice phase  
97 ( $\mathfrak{M}(z, d_{ap})$ ).

$$\langle \mathcal{M}(d_{ap}) \rangle = \frac{1}{H_{cloud}} \int_{cloud\ base}^{cloud\ summit} (\mathcal{M}_{int}(z, d_{ap}) + \mathbb{M}(z, d_{ap}) + \mathfrak{M}(z, d_{ap})) dz \quad \text{Equation 4}$$

98

99 Finally, in order to evaluate the mass flow of particles exiting the cloud at its base ( $\phi_{ap,precip}(d_{ap})$ ), it is necessary to evaluate the cloud volume  
100 ( $\mathcal{V}(\mathcal{D}_{drop})$ ) which contains all the droplets whose drop velocity  $w_{\infty}(\mathcal{D}_{drop})$  is sufficient for them to pass through the section  $dS$ , during the time  $dt$ . Using  
101 the velocity composition law, we can deduce Equation 5.

$$\mathcal{V}(\mathcal{D}_{drop}) = \max(0, w_{\infty}(\mathcal{D}_{drop}) - w_{air}(Z_{cloud\ base})) \cdot dS \quad \text{Equation 5}$$

102

103 In this equation,  $w_{air}(Z_{cloud\ base})$  is the velocity of the air parcel at the base of the cloud. By convention,  $w_{air}$  is positive for an updraft and negative for  
104 a downdraft.

105 It is then immediately possible to deduce the flow of particles passing  $dS$  through liquid precipitation:

$$\phi_{ap,rain}(d_{ap}) = \int_{d_{droplet}=0}^{\infty} \max(0, w_{\infty}(\mathcal{D}_{drop}) - w_{air}(Z_{cloud\ base})) \cdot \mathbb{M}(z, d_{ap}, \mathcal{D}_{drop}) \cdot d\mathcal{D}_{drop} \quad \text{Equation 6}$$

106 In this equation,  $\mathbb{M}(z, d_{ap}, \mathcal{D}_{drop})$  is the concentration of particles contained in the droplets and of dry diameter  $d_{ap}$ .

107 The same applies to solid precipitation  $\phi_{ap, ice}(d_{ap})$  :

$$\phi_{ap, ice}(d_{ap}) = \int_{d_{ice}=0}^{\infty} \max(0, w_{\infty}(d_{ice}) - w_{air}(Z_{cloud\ base})) \cdot \mathfrak{M}(z, d_{ap}, d_{ice}) \cdot d_{ice} \quad \text{Equation 7}$$

108 By adding these two flows together, it is possible to deduce the total flow of particles (of diameter  $d_{ap}$ ) exiting the cloud through all precipitation:

$$\phi_{ap, precip}(d_{ap}) = \phi_{ap, rain}(d_{ap}) + \phi_{ap, ice}(d_{ap}) \quad \text{Equation 8}$$

110

111 Thus, to theoretically evaluate the cloud scavenging coefficient, it is first and foremost essential to be able to evaluate its contours, but also to be able to  
112 determine the mass concentrations of particles in the droplets  $\mathbb{M}(z, d_{ap}, \mathcal{D}_{drop})$ , in the ice phase  $\mathfrak{M}(z, d_{ice}, d_{ap})$ , and in the interstitial aerosol  $\mathcal{M}_{int}(z, d_{ap})$ .

113 To evaluate the contours of the cloud, it seems necessary in the first instance to consider once again its definition.

## 114 **1.2. What is a cloud? (how to define its boundaries?)**

115 The World Meteorological Organization defines clouds as: “an aggregation of minute particles of liquid water or ice, or of both, suspended in the atmosphere  
116 and usually not touching the ground” (WMO, 2014). This definition would appear to be very inadequate for enabling the contours of a cloud to be  
117 determined. Clouds, although very commonly talked about in everyday life and subject to numerous scientific studies, have contours that remain very  
118 blurred. It is therefore always difficult to define them rigorously, and above all non-recursively. Spankuch *et al.*, (2022) further emphasised that, depending  
119 on the scope of the authors’ expertise (meteorology, climate, satellite observations, airborne, from ground radars, or using microphysical models), these  
120 authors use significantly differing definitions and thresholds.

121 For example, Wood and Field, 2011 proposed criteria with respect to liquid water content (LWC), ice water content (IWC), or total concentrations in numbers  
122 of hydrometeors (droplets and crystals).

123 Hiron (2018) proposed separating cloud water and precipitation water based on the criterion of the size of hydrometeors (hydrometeors with a diameter of  
124 less than 64  $\mu\text{m}$  are considered part of the cloud; larger than that are considered part of the rain); then, if the total cloud water content is greater than 0.1  
125  $\text{g}/\text{cm}^3$ , the air parcel is considered part of the cloud.

126 Other authors proposed contours based on relative humidity (Del Genio *et al.*, 1996) or total water content (TWC), whereas meteorologists and  
127 climatologists tend to prefer optical thickness (Sassen and Cho, 1992), each with arbitrarily established thresholds.

128 Although these definitions can be linked mathematically to each other, these relationships are most often highly non-linear. Therefore, in this article, a  
129 variety of cloud definitions will be considered, and we will examine the criteria that are most relevant for studying in-cloud scavenging and distinguishing it  
130 from below-cloud scavenging. This relevance of the definition what constitutes a cloud will be analysed from two perspectives. Firstly, we consider a purely  
131 physical perspective and, secondly, a more pragmatic perspective linked rather to applicability in an atmospheric dispersion model dedicated to crisis  
132 management.

## 133 **1.3. The DESCAM model**

134 To simulate clouds of different types and theoretically evaluate their scavenging coefficient, it is necessary to have a model that makes it possible to simulate  
135 all the water phase changes, considering the catalyst role of aerosols in most of these state changes (activation, ice nucleation, etc.). It is also necessary to  
136 calculate the sink terms of interstitial aerosols (related to droplet collection or activation) and associate them with the source terms of particles in droplets  
137 and ice, in order to calculate the mass of particles in droplets ( $\mathbb{M}(d_{drop})$ ) and in ice ( $\mathfrak{M}(d_{ice})$ ) throughout the simulation (Equation 6, Equation 7).

138 The DESCAM model meets these specifications. This detailed microphysical model classifies droplets ( $\mathcal{D}_{drop} \in [1 \mu\text{m}, 6.5 \text{mm}]$ ), ice ( $d_{ice} \in$   
139  $[1 \mu\text{m}, 6.5 \text{mm}]$ ), and aerosols ( $d_{ap} \in [2 \text{nm}, 12.7 \mu\text{m}]$ ), each into 39 logarithmically distributed size classes. This makes it possible to explicitly monitor  
140 their respective particle size distributions  $\mathbb{N}(\mathcal{D}_{drop})$ ,  $\mathfrak{N}(d_{ice})$  and  $\mathcal{N}(d_{ap})$ , spatially and temporally. This model can be coupled with various dynamic models  
141 that allow consideration of atmospheric flows. In this article, we will only consider a dynamic called 1D1/2 (Asai and Kasahara, 1967), implemented in the  
142 DESCAM model by Monier, 2003. More realistic 3D dynamics (Clark and Hall, 1991) are implemented in DESCAM (Leroy 2007) but will not be considered in  
143 this article.

## 144 **Description of the microphysical models modelled in DESCAM**

145 All the microphysical processes considered in the DESCAM model are presented in Figure 2.

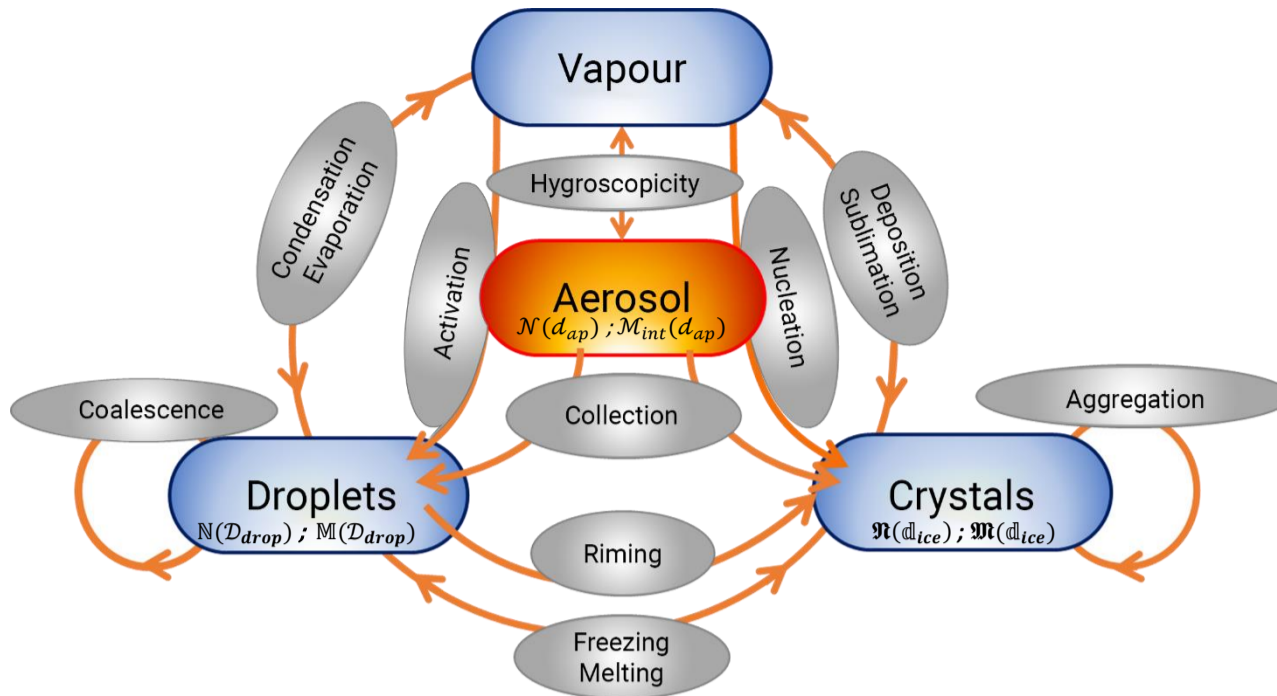


Figure 2. Modelling of microphysical processes in the DESCAM model.

In this figure, we can see the central role of aerosols in most water phase changes. The explicit resolution of all these microprocesses enables calculation of the particle size distributions of aerosols in each grid cell and at each time step (in number:  $\mathcal{N}(d_{ap})$  (Equation 9) and in mass:  $\mathcal{M}(d_{ap})$ ), as well as the particle size distributions of the droplets (in number  $\mathcal{N}(\mathcal{D}_{drop})$ , Equation 10) and of the ice (in number  $\mathcal{N}(\mathcal{d}_{ice})$ , Equation 11). In addition, in order to preserve the total mass of particles, the model also calculates two other quantities that are used to determine the masses of particles in droplets of diameter  $d_{drop}$  ( $\mathcal{M}(\mathcal{D}_{drop})$ ), and in ice crystals of diameter  $d_{ice}$  ( $\mathcal{M}(\mathcal{d}_{ice})$ ).

$$\frac{d\mathcal{N}(d_{ap})}{dt} = \left. \frac{d\mathcal{N}(d_{ap})}{dt} \right|_{dyn} + \left. \frac{d\mathcal{N}(d_{ap})}{dt} \right|_{coll} + \left. \frac{d\mathcal{N}(d_{ap})}{dt} \right|_{hygro} + \left. \frac{d\mathcal{N}(d_{ap})}{dt} \right|_{act, deact} \quad \text{Equation 9}$$

$$\begin{aligned} \frac{d\mathcal{N}(\mathcal{D}_{drop})}{dt} = & \left. \frac{d\mathcal{N}(\mathcal{D}_{drop})}{dt} \right|_{dyn} + \left. \frac{d\mathcal{N}(\mathcal{D}_{drop})}{dt} \right|_{act, deact} + \left. \frac{d\mathcal{N}(\mathcal{D}_{drop})}{dt} \right|_{coal} \\ & + \left. \frac{d\mathcal{N}(\mathcal{D}_{drop})}{dt} \right|_{cond, vap} + \left. \frac{d\mathcal{N}(\mathcal{D}_{drop})}{dt} \right|_{riming} + \left. \frac{d\mathcal{N}(\mathcal{D}_{drop})}{dt} \right|_{frz, melt} \end{aligned} \quad \text{Equation 10}$$

$$\begin{aligned} \frac{d\mathcal{N}(\mathcal{d}_{ice})}{dt} = & \left. \frac{d\mathcal{N}(\mathcal{d}_{ice})}{dt} \right|_{dyn} + \left. \frac{d\mathcal{N}(\mathcal{d}_{ice})}{dt} \right|_{nucleation} + \left. \frac{d\mathcal{N}(\mathcal{d}_{ice})}{dt} \right|_{frz, sub} + \left. \frac{d\mathcal{N}(\mathcal{d}_{ice})}{dt} \right|_{agg} \\ & + \left. \frac{d\mathcal{N}(\mathcal{d}_{ice})}{dt} \right|_{riming} + \left. \frac{d\mathcal{N}(\mathcal{d}_{ice})}{dt} \right|_{frz, melt} \end{aligned} \quad \text{Equation 11}$$

$$\begin{aligned} \frac{d\mathcal{M}(\mathcal{D}_{drop})}{dt} = & \left. \frac{d\mathcal{M}(\mathcal{D}_{drop})}{dt} \right|_{dyn} + \left. \frac{d\mathcal{M}(\mathcal{D}_{drop})}{dt} \right|_{act, deact} + \left. \frac{d\mathcal{M}(\mathcal{D}_{drop})}{dt} \right|_{coal} \\ & + \left. \frac{d\mathcal{M}(\mathcal{D}_{drop})}{dt} \right|_{cond, vap} + \left. \frac{d\mathcal{M}(\mathcal{D}_{drop})}{dt} \right|_{riming} + \left. \frac{d\mathcal{M}(\mathcal{D}_{drop})}{dt} \right|_{frz, melt} \end{aligned} \quad \text{Equation 12}$$

$$\begin{aligned} \frac{d\mathcal{M}(\mathcal{d}_{ice})}{dt} = & \left. \frac{d\mathcal{M}(\mathcal{d}_{ice})}{dt} \right|_{dyn} + \left. \frac{d\mathcal{M}(\mathcal{d}_{ice})}{dt} \right|_{nucleation} + \left. \frac{d\mathcal{M}(\mathcal{d}_{ice})}{dt} \right|_{frz, sub} + \left. \frac{d\mathcal{M}(\mathcal{d}_{ice})}{dt} \right|_{agg} \\ & + \left. \frac{d\mathcal{M}(\mathcal{d}_{ice})}{dt} \right|_{riming} + \left. \frac{d\mathcal{M}(\mathcal{d}_{ice})}{dt} \right|_{frz, melt} \end{aligned} \quad \text{Equation 13}$$

In these equations, except for the index ( $|_{dyn}$ ) denoting variations due to atmospheric transport, each term corresponds to one of the microphysical processes outlined in Figure 2. For instance, ( $|_{act, deact}$ ) denotes to activation and deactivation processes. The subscripts  $coll$ ,  $hygro$ ,  $frz$ ,  $sub$ ,  $coal$ ,  $cond$ ,  $vap$  and  $agg$  respectively refers to the processes of aerosol collection by droplets, hygroscopicity of aerosol particles, freezing, sublimation,

163 coalescence, condensation, vaporization, and aggregation. The hygroscopic growth of aerosol particles is calculated assuming they are in thermodynamic  
164 equilibrium with the air supersaturation  $S$  (Equation 14). This equilibrium is modelled after the  $\kappa$ -Köhler theory.

$$\left. \frac{d\mathcal{N}(d_{ap})}{dt} \right|_{hygro} = \left. \frac{\partial \mathcal{N}(d_{ap})}{\partial S} \right|_{\kappa\text{-Köhler}} \left. \frac{\partial S}{\partial t} \right|_{dyn} \quad \text{Equation 14}$$

165

166 Concerning the cold microphysics (Figure 2), this simulation integrates homogeneous freezing mechanisms (i.e., which do not require aerosol contribution)  
167 and heterogeneous freezing mechanisms (for which aerosols act as a catalyst for phase change). For homogeneous freezing, we consider the parametrisation  
168 of Koop *et al.*, (2000) adapted to DESCAM by Monier *et al.*, (2006). To model heterogeneous ice nucleation, we consider all the mechanisms described by  
169 Vali *et al.*, (2015). The Biggs formula (1953) is used to describe immersion freezing and the model of Meyers *et al.*, (1992) for condensation and contact  
170 freezing, as well as deposition nucleation. All these mechanisms have recently been incorporated into the DESCAM model by Hiron and Flossmann, (2015).

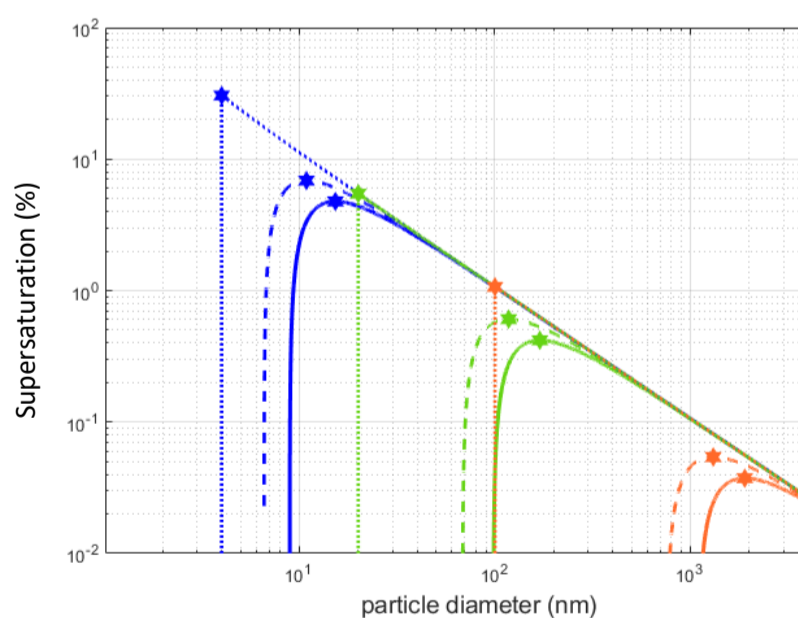
171 The main mechanism responsible for the flow of particles exiting the cloud via precipitation ( $\phi_{ap, precip}(d_{ap})$ , Equation 3) is activation. The collection of  
172 aerosols by droplets is only second order (Flossmann and Wobrock, 2010; Dépée, 2019). In the DESCAM model, activation is modelled by the  $\kappa$ -Köhler theory  
173 (Petters and Kreidenweis, 2007). This model makes it possible to determine equilibrium vapour pressure in the vicinity of a droplet of diameter  $\mathcal{D}_{drop}$ , as a  
174 function of the mass and type of solute (modelled by the  $\kappa$  value) it contains, and therefore the supersaturation for this droplet. For a given mass and  
175 chemical nature of the pristine dry particle, one can compute the corresponding supersaturations for given size of solution droplets. This curve has a unique  
176 maximum, called critical supersaturation (Figure 3). The diameter associated with this critical supersaturation is called the activation diameter. Aerosols  
177 with a diameter smaller than the activation diameter are brought into thermodynamic equilibrium with their environment by hygroscopicity, with aerosols  
178 of a diameter greater than the activation diameter being converted into droplets and growing by means of vapour diffusion (by condensation).

179 In the DESCAM code, the microphysical process of collection (i.e. the process by which, during falling, droplets encounter impact and capture interstitial  
180 aerosol particles), is modelled in Equation 12 by the term  $\left. \frac{d\mathbb{M}(\mathcal{D}_{drop})}{dt} \right|_{coll}$  which is calculated by solving Equation 15. In this equation, the central term is the  
181 collection efficiencies ( $E(d_{ap}, \mathcal{D}_{drop}, \mathcal{RH})$ ). This is calculated by the model developed and validated by Dépée (Dépée *et al.*, 2019; Dépée *et al.*, 2021, Part I;  
182 Dépée *et al.*, 2020, Part II).

$$\left. \frac{d\mathbb{M}(\mathcal{D}_{drop})}{dt} \right|_{coll} = \int_{d_{ap}=0}^{\infty} \mathcal{N}(d_{ap}) \frac{\pi \mathcal{D}_{drop}^2}{4} \mathcal{U}_{\infty, droplet}(\mathcal{D}_{drop}) E(d_{ap}, \mathcal{D}_{drop}, \mathcal{RH}) \frac{\pi d_{ap}^3}{6} \rho_{ap} dd_{ap} \quad \text{Equation 15}$$

183 In this equation  $\mathcal{U}_{\infty, droplet}(\mathcal{D}_{drop})$  corresponds to the terminal velocity of a droplet of diameter  $\mathcal{D}_{drop}$  (calculated after the Beard (1973) model),  $\rho_{ap}$  is  
184 the density of the aerosol particle, and  $\mathcal{RH}$  refers to the relative humidity of air in the parcel.

185



186

187 Figure 3. Thermodynamic equilibrium of an aerosol calculated as a function of particle diameter and nature of the initial dry particle. This  
188 calculation is made using the  $\kappa$ -Köhler theory (for a temperature of 293 K and a surface tension between solution and air of  $72 \times 10^{-3} \text{ N.m}^{-1}$ ).

189 (—) initial dry radius of the particles set at 4 nm; (—) initial dry radius set at 20 nm; (—) initial dry radius set at 100 nm;  
190 (···)  $\kappa = 0$ , insoluble aerosol; (--)  $\kappa = 0.61$ , moderately hygroscopic, as  $(\text{NH}_4)_2\text{SO}_4$ ; (—)  $\kappa = 1.28$ , highly hygroscopic, as NaCl;  
191 ★ critical supersaturations needed to activate the aerosol and convert it into a cloud droplet.

192

193 Note that Equation 6 and Equation 7 are not directly calculable by the DESCAM model. This is because the model makes an inventory of the mass of particles  
194 in the droplets and crystals according to the size of the hydrometeors ( $M(\mathcal{D}_{drop})$ , Equation 12 and  $\mathfrak{M}(\mathbb{d}_{ice})$ , Equation 13), but without memorising the size  
195 of the aerosols before their incorporation. The scavenging coefficients calculated in this article are therefore averaged, in mass, over the particle size  
196 distribution of the aerosols. In this article we focus on validating the approach described by applying it to different types of cloud. Current work and future  
197 publications will focus on demonstrating that the scavenging coefficient may be simply spectrally calculated, without modifying the model.

198

### 199 **Modelling of atmospheric dynamics**

200 As stated previously, in this article we have limited our study to the 1.5D Dynamic framework developed by Asai and Kasahara, (1967). This has been regularly  
201 used (Monier *et al.*, 2005; Leroy *et al.*, 2006; Quérel *et al.*, 2014; Hiron & Flossmann, 2015) to study the microphysical processes involved in the life cycle of  
202 cumulus clouds. This model considers two concentric cylinders. The inner cylinder has a radius 10 times smaller than the outer cylinder. In the inner cylinder,  
203 the vertical velocity of the flows is determined by solving a simplified form of the Navier-Stokes equations, coupled with the energy conservation equation.  
204 The outer cylinder serves primarily for guaranteeing the condition of zero velocity divergence (continuity equation for incompressible flow). To this end, a  
205 radial velocity component is introduced at the interface between these two cylinders (hence the expression of a 1.5D model), calculated from the  
206 convergence or divergence layers and allowing entrainment from the environment. In this environment the only variable updated in this outer cylinder is  
207 the vertical velocity to evaluate the radial gradient in vertical velocity and the subsequent turbulent flux; all the other variables are assumed to be unaffected  
208 by the cloud processes within the inner cylinder and kept constant throughout the simulation.

209 All the microphysical processes detailed in the previous section and summarised in Figure 2 are calculated only in the central cylinder. Thus, this is also in  
210 the inner cylinder, for each grid layer, that phase changes in the water will be computed with the subsequent absorption or release of latent heat that will  
211 alter the buoyancy of the air and which ultimately generate the updraft and downdraft motions.

## 212 **2. Application to example cloud types**

213 To establish a theoretical scavenging coefficient scheme, the methodology described above is applied to two very different idealised case studies  
214 representative of two different types of clouds. First, we will model a vigorous cumulonimbus, then a shallow stratus. These two cloud types were selected  
215 as they present, respectively, the higher and lower values, in terms of vertical extension, relative humidity, and rainfall intensity. Furthermore, while the  
216 stratus that we simulate is shallow enough to be a warm cloud, cold microphysical processes are essential to capture the development of the cumulonimbus  
217 situation.

218

### 219 **2.1. Application to a cumulonimbus**

#### 220 **Description of the cumulonimbus considered**

221 The cloud selected to model the cumulonimbus is the episode of 19 July 1981 of the CCOPE campaign (Cooperative Convective Precipitation Experiment;  
222 Knight 1982 and Dye *et al.*, 1986), which took place near Miles City in Montana (USA). This episode was selected because it is very finely documented and  
223 this episode is a test case for many codes simulating the formation of convective clouds, and in particular the DESCAM model (Flossmann & Wobrock, 2010).  
224 A radio sounding taken at Miles City at 16h00 local time (just before the storm) is used to initialise the thermodynamic conditions of the atmospheric column:  
225 temperature and humidity. For the vertical pressure profiles, standard conditions are assumed. In addition, we used the observations of both two Doppler  
226 radars measured high-resolution reflectivity as well as the movements of the cloud and five aircrafts that were able to make numerous passes through the  
227 cloud throughout its maturation and through to the precipitation episodes. The spatial-temporal evolution of the thermodynamic conditions, associated  
228 with the microphysical properties of the cloud system, and the atmospheric flows are therefore recorded in fine detail for the entire life of this cumulonimbus  
229 and can be used to evaluate the model performance to capture the clouds physics. For this article, we therefore used the same modelling hypotheses as  
230 those detailed by Leroy *et al.*, (2006). Convection was triggered by +2.3°C heating of the ground during the first 10 minutes of the simulation. During this  
231 campaign, no physicochemical measurements were made of the aerosols, hence we consider that they consisted of ammonium sulfate ( $\kappa = 0.61$  and  $\rho_{dry} =$   
232  $1.77 \cdot 10^3 \text{ kg} \cdot \text{m}^{-3}$  Petters and Kreidenweis, 2007) with an initial particle size distribution of the Jaenicke continental type (1988). We considered a homogeneous  
233 distribution in the atmospheric boundary layer (i.e., over the first 3 kilometres), then above the concentration is assumed to decrease exponentially with a  
234 scale height of 3000 m (Figure 4).

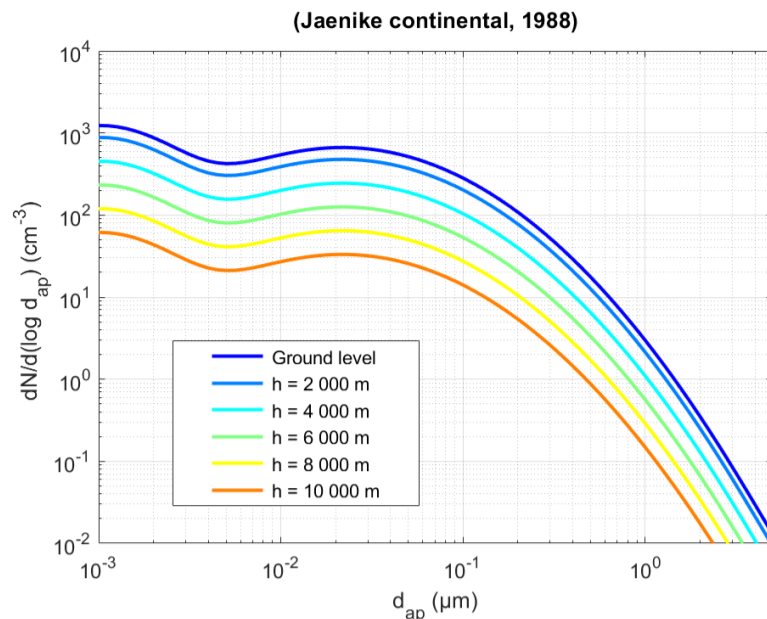
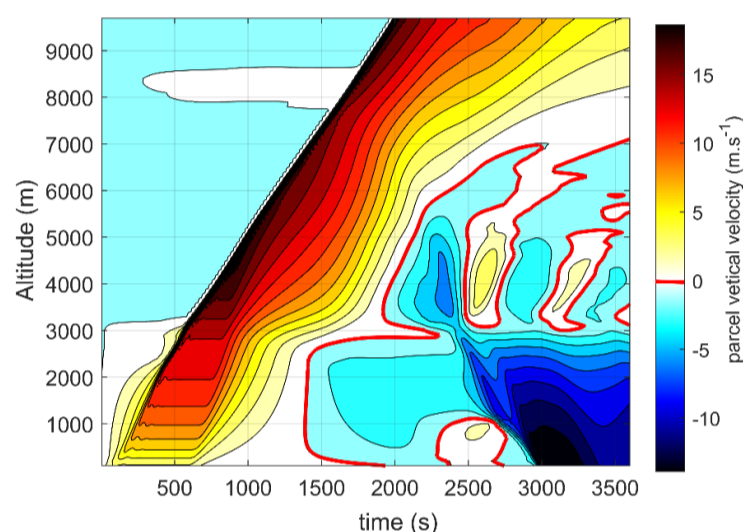


Figure 4. Initial particle size distribution of aerosols considered for this simulation.

235  
236

237 The simulation lasted 3600 s, on a 10 km high column. The spatial and temporal resolutions were set to 100 m and three seconds respectively.

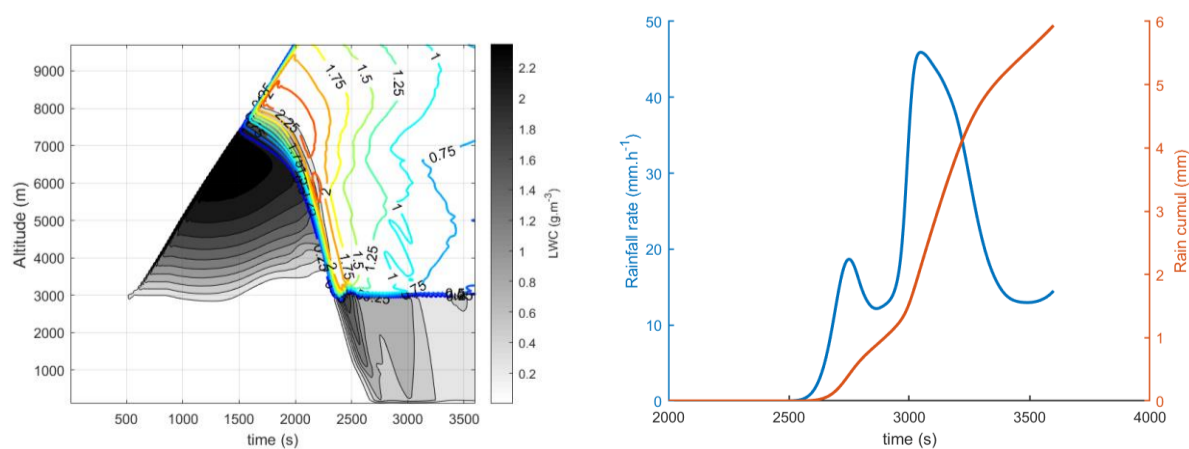
238 Figure 5 and Figure 6 show respectively the spatial-temporal evolutions of the vertical flows in the central cylinder and the liquid water and ice content.



239

240 Figure 5. Spatial-temporal distribution of the vertical components of atmospheric flows. The thick line in red separates the updraft ( $w_{air} > 0$ ) flows from  
241 the downdraft flows ( $w_{air} < 0$ ).

242 In these figures, we can see that the initial superheating of the air layer at ground level induces an updraft flow due to buoyancy forces. Approximately 500 s  
243 after the start of the simulation, the air reaches critical supersaturation at an altitude of 3000 m and the aerosols are gradually converted into droplets. The  
244 spatial-temporal distribution shown on the left of Figure 6 highlights the appearance of a cloud at the spatial-temporal coordinate (500 s, 3000 m). Vapour  
245 condensation induces a latent heat release, which in turn increases buoyancy of the air parcel, accelerating the updraft flows (approx.  $15 \text{ m.s}^{-1}$  at 4000 m).  
246 This flow transports the vapour at altitude and by cooling this induces the progressive activation of the aerosols, and a vertical extension of the cloud. Near  
247 7000 m, the first ice crystals are formed. The coexistence of ice crystals and supercooled droplets will allow rapid crystal growth with a corresponding  
248 reduction of liquid water content (best known as the WBF process for: Wegener, 1911; Bergeron, 1928; Findeisen, 1938). Then, the crystals begin to  
249 precipitate at around 1700 s since they reach sizes large enough for their gravitational settling velocity to supersede updraft speed. In precipitating, the  
250 larger crystals collect the suspended droplets. Hence, under the coupled influence of the WBF process and, above all, the collection of droplets by the ice  
251 particles, after 2200 seconds of simulation the cloud only contains ice. Finally, below an altitude of 3000 m, the solid hydrometeors melt and liquid  
252 precipitation forms. Figure 6 shows on the right the rainfall intensities, as well as the cumulative precipitation calculated by the model at ground level. This  
253 timeline presents two local maxima: the first at 2750 s after the start of the simulation, corresponding to an intensity of  $18 \text{ mm.h}^{-1}$  and the second 300 s  
254 later, with an intensity of about  $46 \text{ mm.h}^{-1}$ .



255

256 Figure 6. On the left: Spatial-temporal distributions of liquid water content (LWC, greyscale) and ice content (IWC, iso-contours).  
257 On the right: Temporal evolution of rainfall intensity and cumulative precipitation at ground level

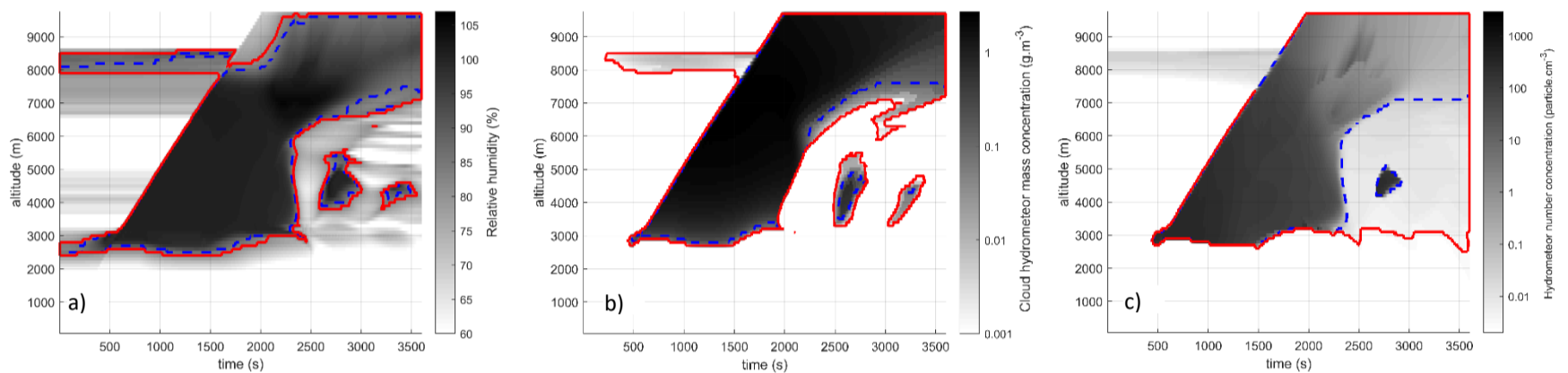


258 **Calculation of the scavenging coefficient**

259 Based on this modelling results, we applied all the methodology described in section 1.1. The first step consisted in establishing the contours of the cloud,  
 260 in order then, using Equation 3 integrated over the entire aerosol distribution, to be able to calculate the equivalent cloud scavenging coefficient.

$$A_{cloud}^m = - \left. \frac{1}{dt} \frac{d\mathcal{M}}{\langle \mathcal{M} \rangle} \right|_{cloud} = \frac{\Phi_{ap, precip}}{\langle \mathcal{M} \rangle \cdot H_{cloud}} \quad \text{Equation 16}$$

261 As already indicated in section 1.2, there is no strict definition of the boundaries of the cloud, particularly at the interface with the precipitation, and it can  
 262 also be observed in Figure 6 that the total water content does not show any demarcation between the cloud and the precipitation. Moreover, as Spänkuch  
 263 *et al.*, (2022) point out, the physical phenomenon studied will determine which contours are the most relevant. Therefore, for this study, we examined three  
 264 of the physical parameters to establish this contour. These three criteria are the relative humidity of the air parcel (calculated in relation to liquid water),  
 265 the mass concentration of hydrometeors with a diameter of less than 64  $\mu\text{m}$  and, lastly, the concentration of hydrometeors. The contours of this  
 266 cumulonimbus are presented in Figure 7 for each of these criteria, each with two thresholds considered. **The thresholds levels were chosen arbitrarily, mainly to**  
 267 **observe their influence on scavenging when they vary over wide ranges of values.**



268

269 Figure 7. Test of different criteria to establish the contours of the simulated cumulonimbus.

270 a) threshold based on relative humidity: (---)  $RH > 85\%$ ; (—)  $RH > 80\%$ .

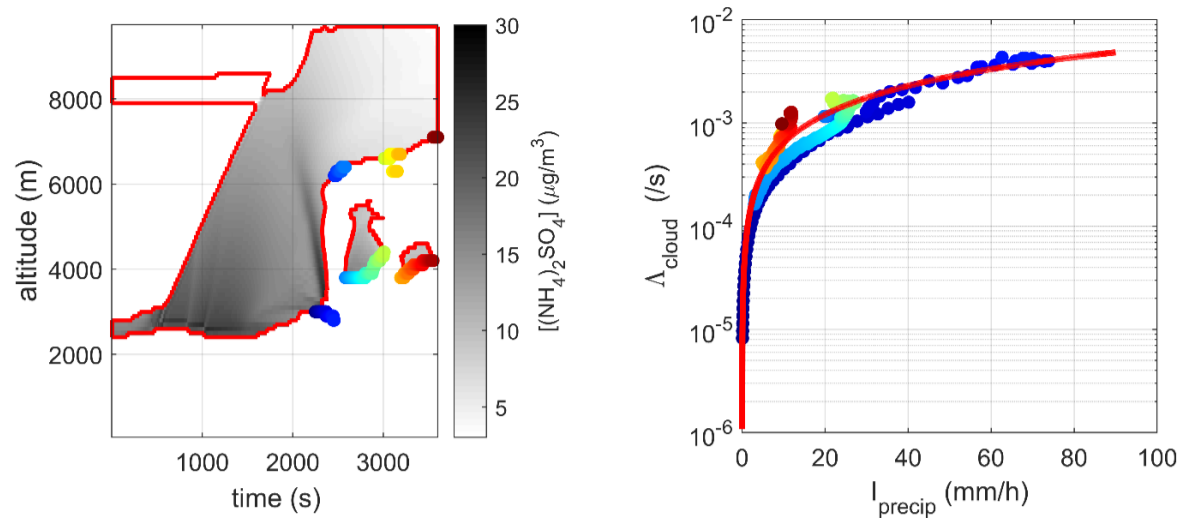
271 b) threshold based on the total water content of hydrometeors with a diameter less than 64  $\mu\text{m}$ : (---) mass concentration of cloud  
 272 hydrometeors  $> 0.1 \text{ g.m}^{-3}$ ; (—) mass concentration of cloud hydrometeors  $> 0.001 \text{ g.m}^{-3}$ .

273 c) threshold based on number concentration of total hydrometeors: (---)  $\int dN + dN > 0.03 \text{ cm}^{-3}$   
 274 (—)  $\int dN + dN > 0.003 \text{ cm}^{-3}$

275 We can see in this figure that, apart from the criterion based on the concentration of hydrometeors (Equation 9), with a threshold of 0.003 hydrometeors  
 276 per cubic centimetre, all the other criteria yield very similar contours. Thus, the cloud forms close to an altitude of 3000 m and its base remains constant for  
 277 up to 2500 s of simulation. During these 2500 s, the cloud thickens vertically until it reaches the tropopause (considered to be at 10,000 m in this calculation).  
 278 As shown in Figure 6 (on the right), 2500 s corresponds to the start of precipitation. This moment corresponds to an elevation of the base of the cloud up to  
 279 about 7000 m, except for the last criterion ( $N_{hydrometeor} > 0.003 \text{ cm}^{-3}$ ), for which the height of the base of the cloud remains constant close to the  
 280 altitude of 3000 m, even during rain.

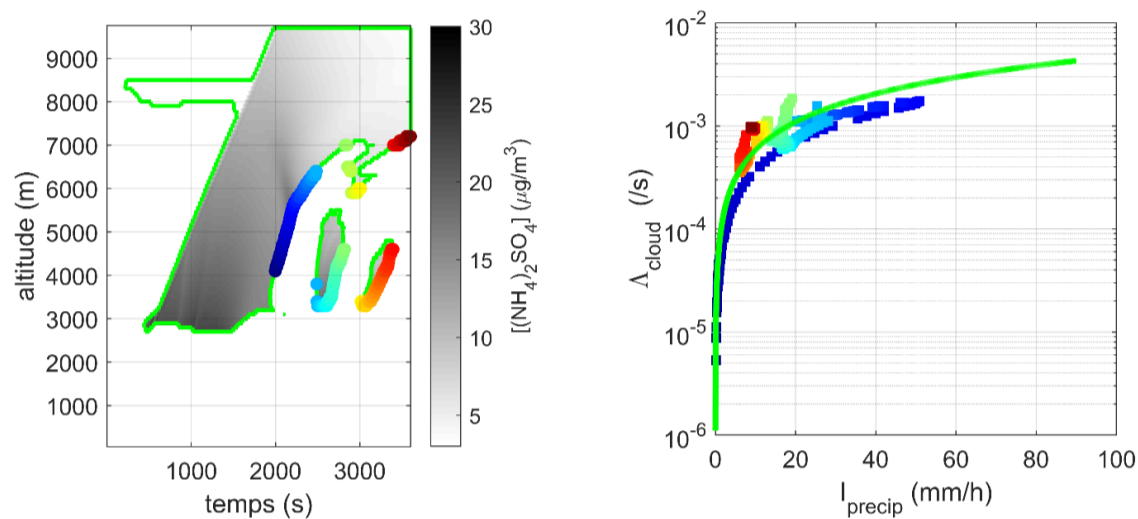
281 Initially, our objective was to find a bijective relationship between a set of meteorological parameters available in DESCAM and the scavenging coefficient  
 282 calculated by this methodology. **The reason for a bijective relationship is twofold, first it ensures a better robustness of the model, second it allow to perform inverse**  
 283 **calculation to estimate the discharge in case of ground contamination.**

284 Most often in the literature, cloud scavenging is described as a power function of precipitation intensity (Hertel *et al.*, 1995; MRI, 2015; Leadbetter *et al.*,  
 285 2015; Groell *et al.*, 2014; Quérel *et al.*, 2021). Figure 8, Figure 9 and Figure 10 respectively present the contours of the cloud established on the basis of the  
 286 three criteria previously introduced (Figure 7). Within these contours, we calculated the total mass concentration of ammonium sulfate ( $\mathcal{M}(z)$ ), adding  
 287 together the respective concentrations of the aerosol phases ( $\mathcal{M}_{int}(z)$ ), in the droplets ( $\mathcal{M}(z)$ ) and in the crystals ( $\mathcal{M}(z)$ ). Knowing the flux of ammonium  
 288 sulfate that is within the precipitative hydrometeors through the base of the cloud (Equation 6, Equation 7 and Equation 8), we could deduce the scavenging  
 289 coefficient, which we plotted according to the precipitation intensity calculated at the base of the cloud. Like Costa *et al.*, (2010), Stephan *et al.*, (2008) and  
 290 Quérel *et al.* (2021), a threshold of 0.1  $\text{mm.h}^{-1}$  was considered to limit noise. In Figure 8, 9, 10, the correspondence of the dots can be deduced with the  
 291 colour codes of the points. On the left-hand side, the identification of the spatial-temporal coordinates where precipitation and scavenging coefficient are  
 292 calculated is plotted. On the right-hand side, the corresponding relationship between scavenging coefficient and precipitation intensity can be read. These  
 293 results are of great importance because they show that the relationship between the scavenging coefficient and the rainfall intensity is the same at the  
 294 beginning and the end of the rainfall episode. In addition, an adjustment by a power law is determined for each contour. The coefficients for these  
 295 adjustments are shown in Table 1.



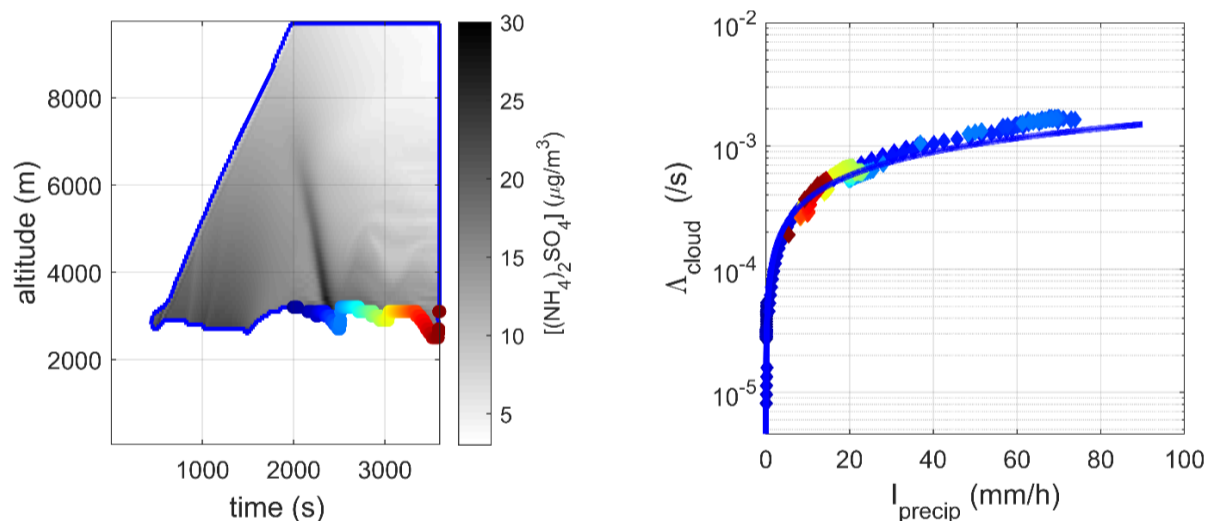
296

297 Figure 8. On the left: spatial-temporal distribution of the ammonium sulfate concentration in the cloud contour (— cloud contour for a  
 298 relative humidity greater than 80%). On the right: correlation between the scavenging coefficient and the precipitation intensity determined  
 299 at the base of the cloud, (—) adjusted by a power law.



300

301 Figure 9. On the left: spatial-temporal distribution of the ammonium sulfate concentration in the cloud contour (— cloud contour for a mass  
 302 concentration of cloud hydrometeors greater than 0.001 g.m<sup>-3</sup>). On the right: correlation between the scavenging coefficient and the  
 303 precipitation intensity determined at the base of the cloud, (—) adjusted by a power law.



304

305 Figure 10. On the left: spatial-temporal distribution of the ammonium sulfate concentration in the cloud contour (— cloud contour for a  
 306 concentration in number of hydrometeors greater than 0.003 particles.cm<sup>-3</sup>). On the right: correlation between the scavenging coefficient  
 307 and the precipitation intensity determined at the base of the cloud, (—) adjusted by a power law.

308

309 In these three figures, we observe that the relationship linking the intensity of precipitation to the scavenging coefficient by the cloud is fairly insensitive to  
 310 the definition selected to describe its contour. Moreover, the power law adjustments plotted in Figure 8, Figure 9 and Figure 10 are very similar (Table 1).  
 311 Nevertheless, only the last contour, based on the hydrometeor concentration (and with a threshold of 0.003 cm<sup>-3</sup>), gives a perfectly bijective relationship  
 312 between the precipitation intensity at the base of the defined contour and the scavenging coefficient. This result is surprising because, as previously  
 313 mentioned in section 1.3, the driving mechanism for in-cloud scavenging is dominated by the activation (which is driven by the supersaturation level and  
 314 physical-chemical properties of the aerosols, Flossmann and Wobrock, 2010). It would therefore seem logical that a criterion based on the relative humidity  
 315 in the grid cell would be the most relevant. However, it is the criterion based on the concentration of hydrometeors that is the more reliable. This is because  
 316 there are zones in the cloud where the humidity is too low to activate the aerosols (e.g., at 4000 m at 2500 s where RH < 85%, or indeed Figure 7a), but  
 317 where there is a significant number of droplets and crystals (> 0.03 cm<sup>-3</sup>). These droplets and crystals have been activated elsewhere and previously, but  
 318 they nevertheless continue to collect aerosols around them – for example by Brownian capture, contributing to scavenging. It therefore justifiable to define  
 319 a cloud contour based on a diagnostic of the numeric concentration of hydrometeors.

320

321

Table 1: Power law adjustment associated with each of the cloud contours studied.

Contour type	Power law adjustments
Based on relative humidity (Figure 8)	$\Lambda_{cloud}^m = 7.6 \times 10^{-5} I^{0.92}$
Based on mass concentration of cloud hydrometeors (Figure 9)	$\Lambda_{cloud}^m = 7.2 \times 10^{-5} I^{0.9}$
Based on numeric concentration of hydrometeors (Figure 10)	$\Lambda_{cloud}^m = 8.6 \times 10^{-5} I^{0.6}$

322

323 However, this numeric concentration criterion, although more precise for theoretically assessing the scavenging coefficient, is not easily accessible in a crisis  
324 code. Nevertheless, detailed analysis of the results of these simulations seems to show that it would be wise to define the cloud base as being constant and  
325 equal to the altitude at which critical supersaturation was first reached, i.e., the altitude at which the cloud began its formation.

326

327

## 2.2.Application to a stratus

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### Description of the stratus considered

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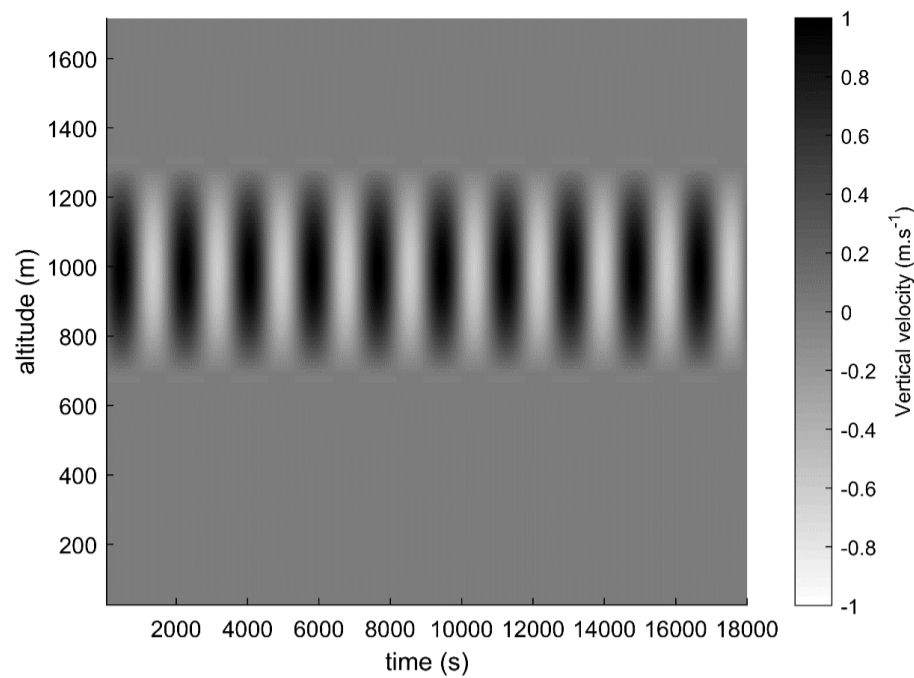
341

342

The same approach as above was considered for modelling scavenging by a shallow stratus cloud. The main differences with the previous modelling (i.e., of the cumulonimbus) beyond the initialisation of thermodynamical profile is the treatment of the vertical advection within the cloud. Whereas, for the previous modelling, differences in air buoyancy (related to the initial thermal gradients and latent heat released by water phase changes) were the cause of vertical velocities and could be described and captured by the dynamics of the model. When it comes to modelling stratus clouds, the dynamics are governed by large scales features that are not included in the 1.5D model. Therefore, the idea is to completely prescribe the time evolving profile for vertical velocity to model this forcing. Since convection is forced rather than triggered by buoyancy, it's reasonable to prescribe it and not calculate the microphysical feedback on dynamics. For the scenario, we considered the vertical advection model proposed by Zhang *et al.*, (2004) and recapitulated in Equation 17. We therefore imposed a sinusoidal profile vertical velocity, the maximum oscillating from positive to negative values with a period of 1800 s. The maximum of the velocities was located at the altitude ( $z_c$ ) of 1000 m and vertical motions allowed between 700 and 1300 m ( $h_c = 600$  m, Figure 11). Like Zhang *et al.*, (2014), in the advection model, we imposed an average updraft velocity ( $w_0$ ) of  $0.2 \text{ m.s}^{-1}$  and an oscillation amplitude ( $w_1$ ) of  $0.8 \text{ m.s}^{-1}$  at an altitude of 1000 m. Figure 5 shows the spatial-temporal distribution of vertical flows prescribed in the central cylinder. The temperature profile follows a dry adiabatic lapse rate with a temperature of  $15^\circ\text{C}$  on the ground so that there are no negative temperatures in the cloud. Above 1300 m, like Zhang *et al.* (2014), we imposed an inversion of the thermal profile. At altitudes between 700 and 1300 m, the relative humidity was initialised at 98.5%, and 95% outside of this range. For the aerosols, the initial conditions were identical to those for cumulonimbus (Equation 5).

$$\left\{ \begin{array}{l} w(z, t) = \cos\left(\pi \frac{z - z_c}{h_c}\right) \left[ w_0 + w_1 \sin\left(\frac{2\pi t}{t_c}\right) \right] \quad \text{if } |z - z_c| \leq \frac{h_c}{2} \\ w(z, t) = 0 \quad \text{if } |z - z_c| > \frac{h_c}{2} \end{array} \right. \quad \text{Equation 17}$$

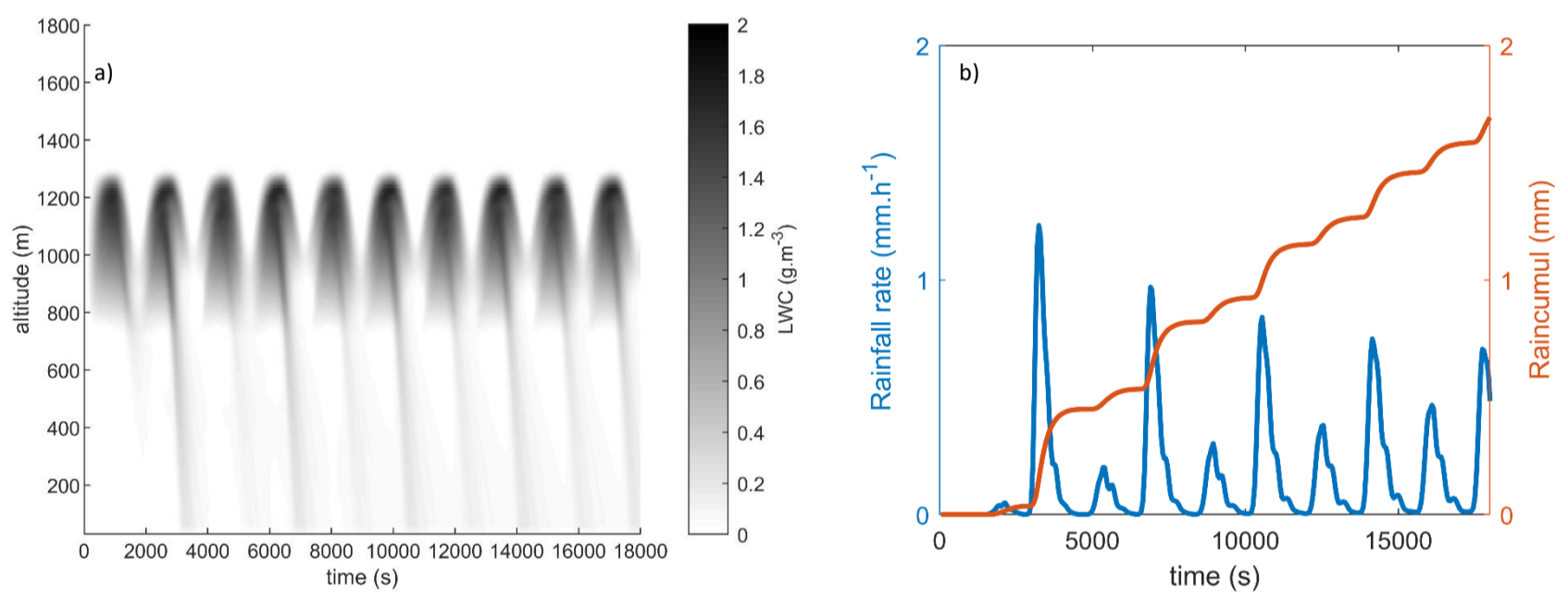
$z_c = 1000 \text{ m}; h_c = 600 \text{ m}; t_c = 1800 \text{ s}; w_0 = 0.2 \text{ m.s}^{-1}; w_1 = 0.8 \text{ m.s}^{-1}$



343

344 Figure 11. Spatial-temporal distribution of the vertical components of atmospheric flows (Zhang *et al.*, 2004)

345 Figure 12 shows on the left the spatial-temporal distribution of the water content calculated by DESCAM. The critical supersaturation was reached close to  
 346 the altitude of 700 m from the first updraft phase (0–1000 s). The LWC then increased with altitude throughout the phase where the atmospheric flows  
 347 were ascending. At the cloud summit, the liquid water content reached approximately  $1.6 \text{ g.m}^{-3}$ . Conversely, during the downdraft phases, the supply of dry  
 348 air to lower altitudes induced, due to the temperature profile considered, a drop in the relative humidity occurs, which in turn induced evaporation of the  
 349 droplets, resulting in a significant reduction in the LWC. These downdraft phases also had the effect of advecting droplets below the cloud band. During the  
 350 period of velocity oscillations ( $t < t_c$ ), precipitation completely evaporated before reaching the ground. However, from the second period onwards, rain  
 351 was diagnosed at ground level (Figure 6. b).



352

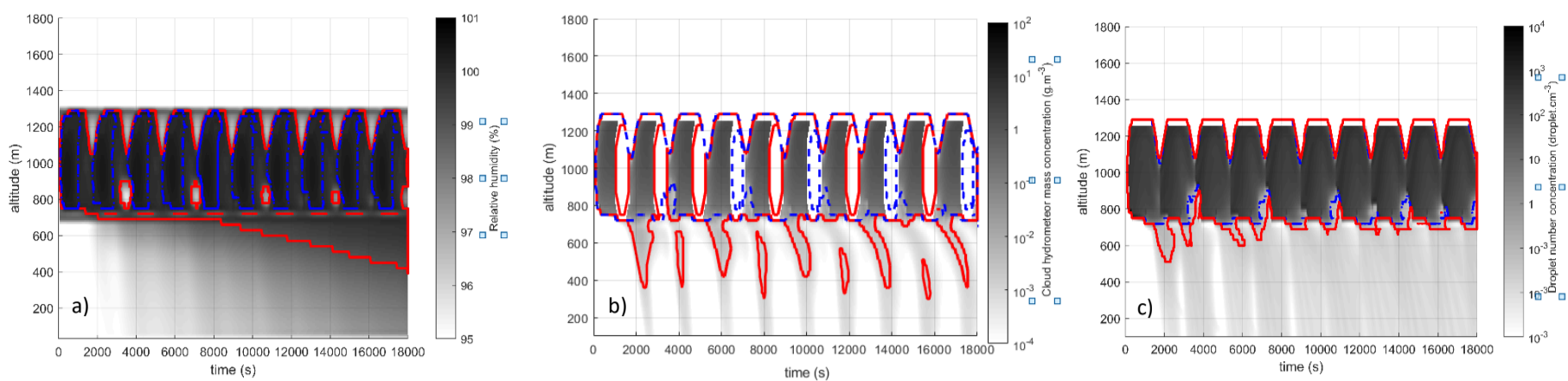
353 Figure 12. On the left: Spatial-temporal distribution of the liquid water content calculated by DESCAM (LWC, in greyscale).  
 354 On the right: Temporal evolution of rainfall intensity and cumulative precipitation diagnosed by DESCAM at ground level.

355 The DESCAM model predicts intermittent precipitation at ground level with flurries of precipitation in the order of a millimetre per hour. Over a precipitation  
 356 period of approximately four hours, the cumulative precipitation was only approximately 3 mm.

357

### 358 Calculation of the stratus scavenging coefficient

359 As before in the case of cumulonimbus, it is necessary to define the contours of the cloud. We therefore used the three criteria previously introduced and  
 360 look for the one with the clearest demarcation line between the cloud zone and the precipitation zone, to apply a dedicated scavenging coefficient (Figure  
 361 13). As before, we observe from Figure 12.a that water content is not a good indicator to outline the cloud boundaries. Indeed, no discontinuity is observed  
 362 for this parameter enabling demarcation between the cloud and the precipitation.



363

364

Figure 13. Test of different criteria to establish the contours of the simulated stratus.

365

a) threshold based on relative humidity: (---)  $RH > 99\%$ ; (—)  $RH > 100\%$ .

366

b) threshold based on the mass concentration of hydrometeors with a diameter less than  $64 \mu\text{m}$ : (---) mass concentration of cloud hydrometeors  $> 0.01 \text{ g} \cdot \text{m}^{-3}$ ; (—) mass concentration of cloud hydrometeors  $> 0.001 \text{ g} \cdot \text{m}^{-3}$ ;

367

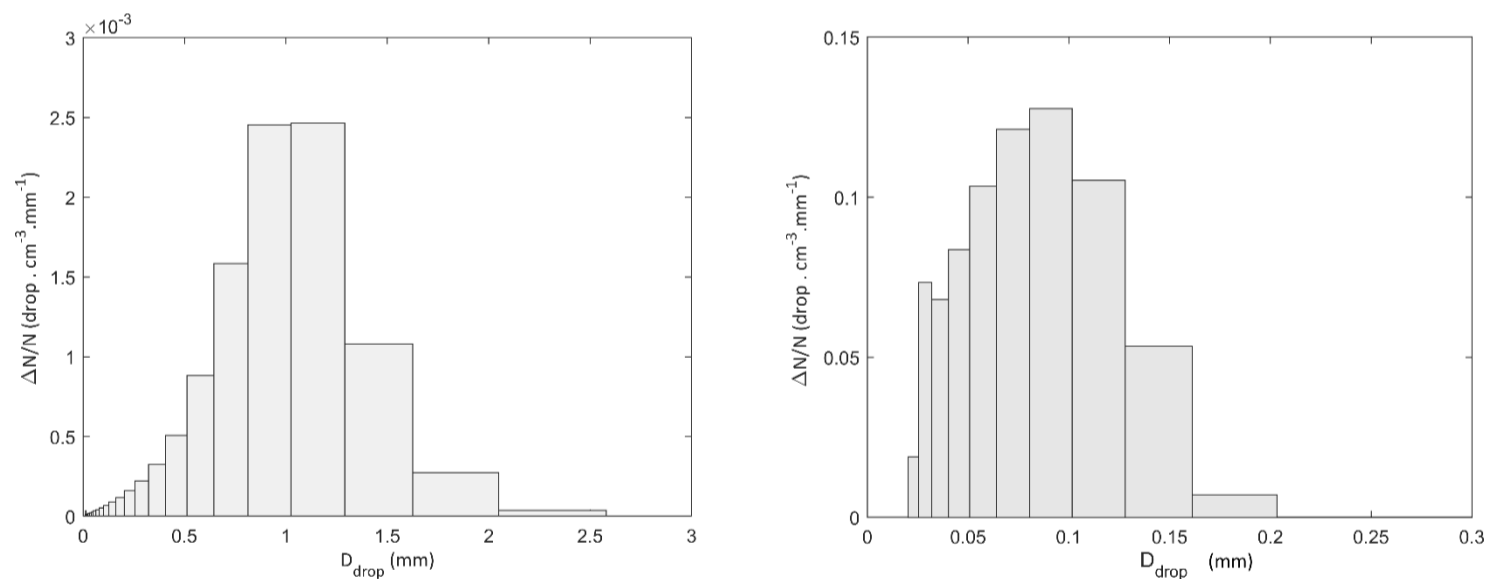
c) threshold based on the concentration of hydrometeors: (---);  $\int dN > 0.1 \text{ cm}^{-3}$ ; (—)  $\int dN + dN > 0.03 \text{ cm}^{-3}$ .

368

369

370 Based on these results, it is more difficult to delineate the contours of this stratus than for the cumulonimbus. This is because, for these three criteria, only  
 371 the droplets concentration shows a clear demarcation between precipitation and cloud zone. Moreover, only this criterion gives stable cloud contours,  
 372 regardless of the threshold value selected. This difference with respect to the cumulonimbus is mainly due to the size of the precipitating hydrometeors,  
 373 which are much larger in the case of cumulonimbus. Figure 14 shows that the particle size distribution mode in number of raindrops, for the cumulonimbus,  
 374 is close to a diameter of 1 mm, whereas it is  $100 \mu\text{m}$  for the stratus. It is therefore easier with a cumulonimbus than with a stratus to define a size threshold  
 375 distinguishing droplet (belonging to the cloud) from raindrops (belonging to precipitation). The criterion based on the mass concentration of hydrometeors  
 376 exceeding  $64 \mu\text{m}$  is therefore less effective under a stratus than under a cumulonimbus. To explain the poor performance of the criterion based on relative  
 377 humidity, again it is the particle size that counts. As the droplets under the stratus are smaller than under the cumulonimbus, their velocities are lower, and  
 378 they reside longer in the atmosphere – about 10 times longer. This longer residence time promotes the increase in relative humidity under the cloud, and  
 379 humidity saturation under the cloud. This makes it difficult to use this criterion to determine the boundary between rain and cloud for a stratus.

380



381

Figure 14. Particle size distributions of raindrops determined by the DESCAM model at ground level

382

Left: For cumulonimbus at time  $t=3000 \text{ s}$

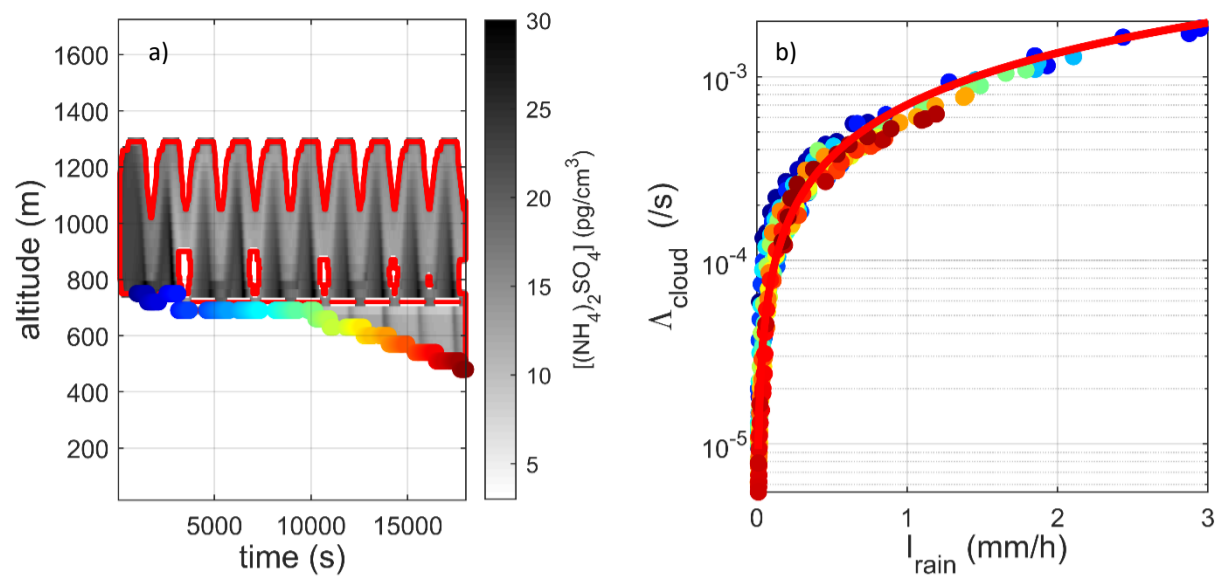
383

Right: For cumulonimbus at time  $t=8200 \text{ s}$

384

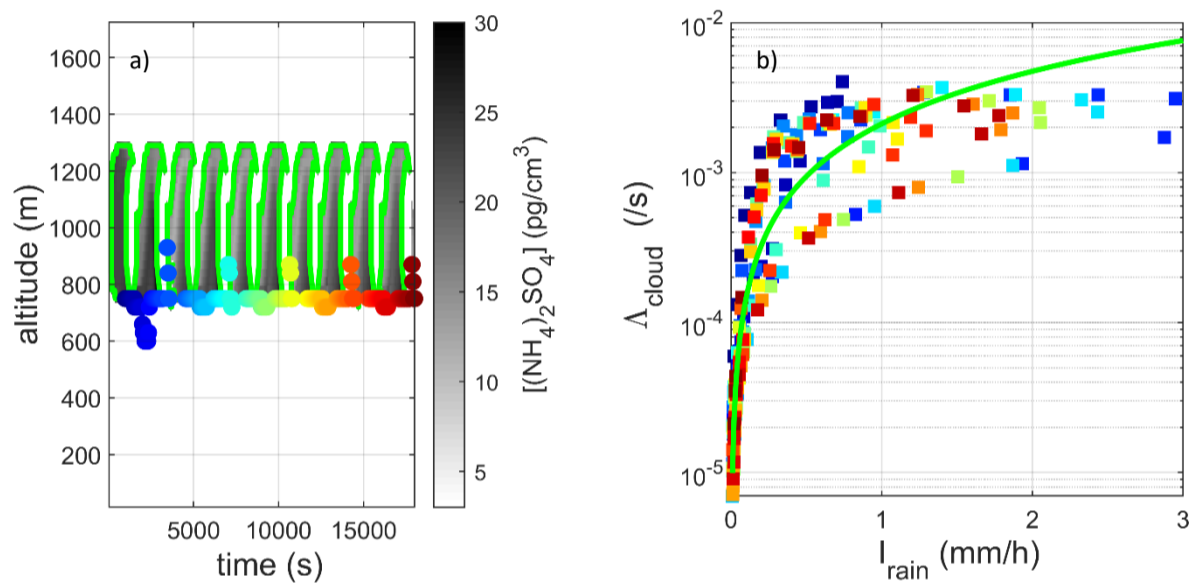
385

386 As previously, for the cumulonimbus, we search for a criterion to delimit cloud from rain. The same parameters as in section 2.1 are investigated and  
 387 presented in Figure 15, 16 and 17.



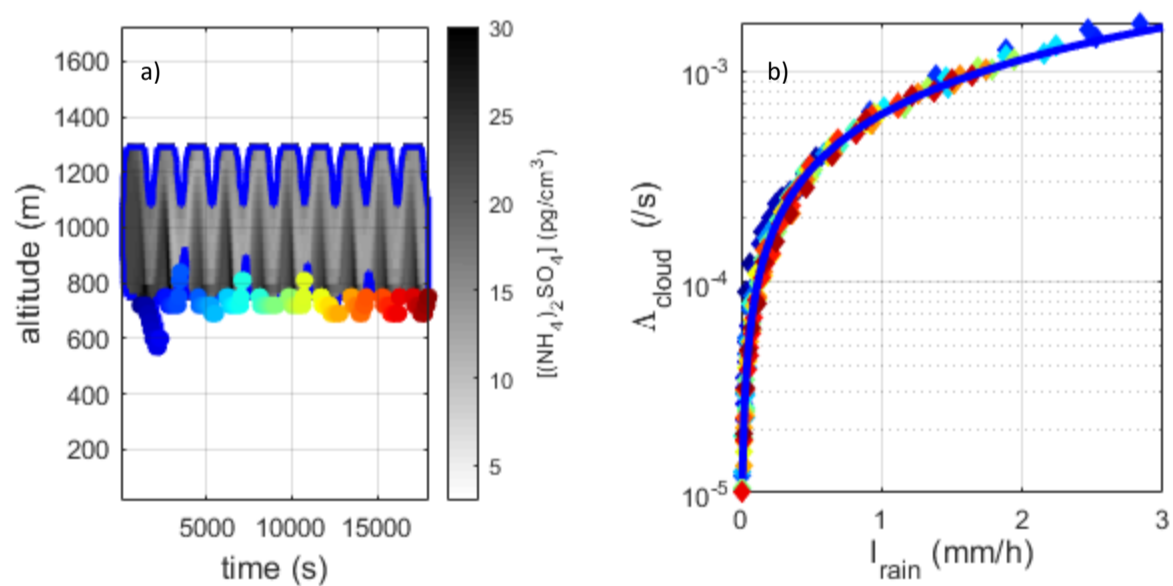
388

389 Figure 15. On the left: spatial-temporal distribution of the ammonium sulfate concentration in the cloud contour (— cloud contour for a  
 390 relative humidity above 99%). On the right: correlation between the scavenging coefficient and the precipitation intensity determined at the  
 391 base of the cloud, (—) adjusted by a power law.



392

393 Figure 16. On the left: spatial-temporal distribution of the ammonium sulfate concentration in the cloud contour (—) criterion based on the  
 394 mass concentration of hydrometeors with a diameter greater than 64 μm with a threshold set at 0.01 g.m<sup>-3</sup>). On the right: correlation  
 395 between the scavenging coefficient and the precipitation intensity determined at the base of the cloud, (—) adjusted by a power law.



396

397 Figure 17. On the left: spatial-temporal distribution of the ammonium sulfate concentration in the contour of the cloud (criterion based on  
 398 the concentration of hydrometeors with a threshold set at 0.01 particle.cm<sup>3</sup>). On the right: correlation between the scavenging coefficient  
 399 and the precipitation intensity determined at the base of the cloud, (—) adjusted by a power law.

400

401 In these three figures, we observe that the contour introduced by Hiron (2017) for cumulonimbus (based on a separation between cloud water and  
 402 precipitation water, on the basis of a criterion on the size of hydrometeors, cf. section 1.2) is no longer applicable for the stratus, and gives highly dispersed  
 403 scavenging coefficient results, particularly for low rain intensity ( $I < 2 \text{ mm} \cdot \text{h}^{-1}$ ). This is because, for this stratus, it is difficult to establish a strict boundary

404 between a raindrop and a cloud droplet, based on their size. However, the other two criteria yield bijective and similar relationships, both in terms of the  
 405 cloud contours (Figure 15.a and Figure 17.a) and the adjusted power laws (Table 2). Unlike cumulonimbus, stratus contours appear to be reliable using a  
 406 criterion based on relative humidity. This difference is related to the intensities of vertical flows in the cumulonimbus. Indeed, we observe in Figure 5 that,  
 407 in the simulated cumulonimbus, the downdraft flows can be very intense (up to  $5 \text{ m.s}^{-1}$ ), transporting to the base of the cloud air masses with a lower mixing  
 408 ratio and hence lower relative humidity.

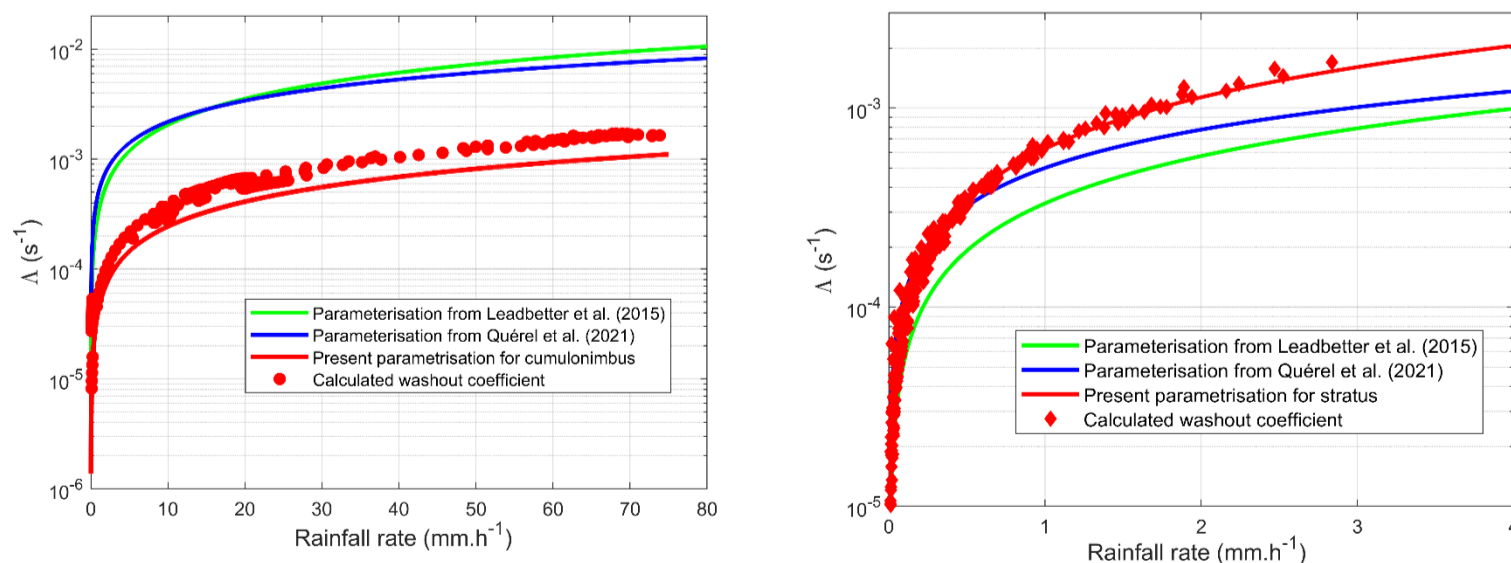
409 Table 2. Adjustment of scavenging coefficients by power laws for the three types of contours studied.

Contour type	Power law adjustments
Based on relative humidity (Figure 15)	$\Lambda_{cloud}^m = 7.03 \times 10^{-4} I^{0.94}$
Based on mass concentration of cloud hydrometeors (Figure 16)	$\Lambda_{cloud}^m = 2.10 \times 10^{-3} I^{1.16}$
Based on hydrometeor concentration (Figure 17)	$\Lambda_{cloud}^m = 6.24 \times 10^{-4} I^{0.86}$

410  
 411 These calculations show that, regardless of the type of simulated cloud, cumulonimbus or stratus, the criterion based on the hydrometeor concentration  
 412 makes it possible to yield cloud contours that are both stable (with little variation when the threshold value is varied), and for which the relationship between  
 413 the scavenging coefficient and the rainfall intensity is the most biunivocal (Figure 8, Figure 9 and Figure 10 for cumulonimbus and Figure 15, Figure 16 and  
 414 Figure 17 for stratus). This criterion is not directly accessible in meteorological models; however, examination of Figure 10 and Figure 17 suggests that the  
 415 cloud base remains stable over time. It would therefore be possible to assess the altitude at which critical supersaturation is reached, and to consider this  
 416 altitude constant over a period that depends on the ratio between the size of the grid cell and the velocity of the horizontal flows.

417  
 418 **2.3. Comparison with the literature and unification of the scavenging coefficient scheme for a cumulonimbus**  
 419 **and a stratus**

420 There is insufficient data to compare our theoretical findings with field study data. Few experimental data have established *in situ* scavenging coefficients  
 421 for different types of clouds. Based on caesium-137 deposition measured following the Fukushima Daiichi accident, Leadbetter *et al.*, (2015) used the Met  
 422 Office dispersion model: NAME (Numerical Atmospheric-dispersion Modelling Environment) for the dispersion of the radioactive plume emitted during the  
 423 accident, considering the meteorological data from the ECMWF model. The authors managed to determine the cloud scavenging coefficient which best suits  
 424 the ground measurements of deposition (Kinoshita *et al.*, 2011). In the same general approach, but using the IRSN LdX dispersion model (Quérel *et al.*, 2007  
 425 and Groëll *et al.*, 2014) and meteorological data from MRI (Sekiyama *et al.*, 2017), Quérel *et al.* (2021) established a very similar scavenging coefficient.  
 426 These two schemes are compared in Figure 18. The comparison is made using the  $\kappa$  value of ammonium sulfate. This decision is based on the findings of the  
 427 Kaneyasu *et al.* (2012) study, which demonstrated the long-distance transport of cesium-137 by these particles - a distance particularly relevant for in-cloud  
 428 scavenging.



429  
 430 Figure 18. Comparison of the parameterisations established respectively for a cumulonimbus (left) and a stratus (right) with the  
 431 parameterisations established by Leadbetter *et al.*, 2015 and Quérel *et al.*, 2021 following the Fukushima accident.  
 432

433 In this figure, we observe that the application of our scheme to a stratus (Figure 18, on the right), concurs excellently with the parametrisation of scavenging  
 434 by clouds established following the Fukushima accident; in particular the parametrisation of Qu  rel *et al.*, (2021). However, the application of our approach  
 435 to cumulonimbus presents much greater differences. Indeed, over the entire rainfall intensity range, our results are on average six times lower than the  
 436 correlations of Leadbetter *et al.*, (2015) and Qu  rel *et al.*, (2021). Two questions therefore arise:

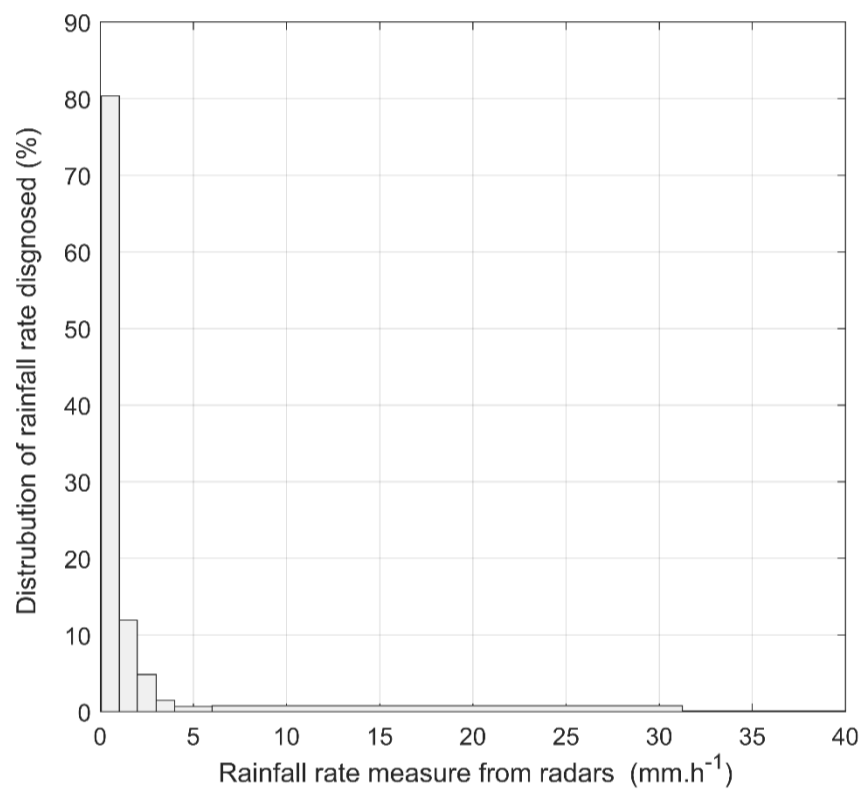
437 First, was there scavenging by cumulonimbus during the Fukushima accident? This would explain why it is difficult to compare our parametrisation of  
 438 scavenging by cumulonimbus with those deduced during the Fukushima accident.

439 Next, why, for the same rainfall intensity, do our calculations show that cumulonimbus scavenges less than stratus?

440 We will therefore address these two questions.

441 **Was there scavenging by cumulonimbus during the Fukushima accident?**

442 To answer this question, let us consider the distribution of rainfall intensities diagnosed from radar measurements by Saito *et al.*, (2015) during March 2011  
 443 in the Fukushima region (Figure 19). These results show that 80% of rain episodes diagnosed corresponded to rainfall intensities of less than 1.5 mm.h<sup>-1</sup>,  
 444 and 97% to intensities of less than 3.5 mm.h<sup>-1</sup> (range of rainfall intensity produced at the base of the simulated stratus, Figure 15) and less than 0.01% had  
 445 intensities of more than 10 mm.h<sup>-1</sup>. In view of these results, it is not possible to completely exclude the presence of rain issuing from cumulonimbus over  
 446 the period of the accident; however, if there was any, its contribution to the construction of the parameterisation of Leadbetter *et al.* (2015) and Qu  rel *et*  
 447 *al.* (2021) is negligible.



448

449 Figure 19. Distribution of rainfall intensity measured in the Fukushima region during March 2011 (Sekiyama *et al.*, 2017).

450

451 **How to unify the scavenging coefficient scheme for a cumulonimbus and a stratus?**

452 Our calculations show that cumulonimbus scavenges less than stratus under the same rainfall intensity. How can we understand this and unify the two  
 453 equations? This phenomenon can be attributed to the significantly higher level of supersaturation observed in cumulonimbus clouds (Figure 7.a) compared  
 454 to that in stratus cloud (Figure 13.a). Hence, if the supersaturation is higher, as is the case for cumulonimbus, for the same activated aerosol mass, these  
 455 particles are diluted in a larger mass of water, as the condensation is also much greater (in reality, the activated aerosol mass increases significantly since,  
 456 as we have indicated previously, the activation diameter of the aerosols decreases as supersaturation increases). Let us therefore examine the impact of  
 457 this effect of vapour condensation on the deduced parameterisation. In the DESCAM model, condensation is modelled by Equation 18. This equation is taken  
 458 from Pruppacher *et al.* (1998, chapter 13, section 2). It results from the vapour diffusion equation on a droplet of diameter  $\mathcal{D}_{drop}$  in the air with  
 459 supersaturation  $\mathcal{S}$  and temperature  $T_\infty$ , considering the thermodynamic equilibrium of the suspended drop within air using the  $\kappa$ -K  hler theory.

$$\left\{ \begin{array}{l} \frac{d\mathcal{D}_{drop}}{dt} = \frac{4}{\mathcal{D}_{drop}} \frac{\rho_w \mathcal{R} T_\infty}{p_{sat,w} \mathcal{D}_v M_w} \frac{\mathcal{S} - y}{1 + \frac{\mathcal{O} n \rho_w}{k T_\infty} (\frac{\mathcal{O} n \rho_w}{\mathcal{R} T_\infty} - 1)} \\ y = \frac{4 \sigma_w \mathcal{D}_{drop} M_w}{\rho_w \mathcal{R} T_\infty \mathcal{D}_{drop}} - \kappa \frac{a_{ap}^{dry^3}}{\mathcal{D}_{drop}^3} \end{array} \right. \quad \text{Equation 18}$$

460



461 In this equation  $\mathcal{R}$  is the ideal gas constant,  $p_{sat,w}$  the saturating vapour pressure,  $d_{ap}^{dry}$  the dry diameter of the aerosol,  $\mathcal{O}n$  the latent heat of vaporisation  
 462 of the water,  $\sigma_{w,D_{drop}}$  the surface tension,  $k$  the thermal conductivity of the air,  $M_w$  and  $\rho_w$  the molar mass and density of the water vapour, and finally  $\mathcal{D}_v$   
 463 **the diffusion coefficient of the water vapour in air**. As the Kelvin effect (linked to the curvature of the interface) and the solute effect become very quickly  
 464 negligible after activation of the aerosol, this equation can be greatly simplified and reduced to:  $\mathcal{D}_{drop} d\mathcal{D}_{drop} = \mathbb{C} \cdot \mathcal{S} dt$ , where  $\mathbb{C}$  is a constant, enabling it to  
 465 be integrated analytically, to give:  $\mathcal{D}_{drop}(t) = \sqrt{\mathcal{D}_{drop,t_0}^2 + 2\mathbb{C} \cdot \mathcal{S} \cdot t}$ . Thus, to assess the effect of dilution of the aerosol in the droplet due to condensation,  
 466 we can write:

$$\frac{\mathcal{D}_{drop}(t)_{stratus}^2}{\mathcal{D}_{drop}(t)_{cumulonimbus}^2} = \frac{\mathcal{D}_{drop,t_0}^2 + 2\mathbb{C} \cdot \langle \mathcal{S} \rangle_{stratus} \cdot t_{stratus}}{\mathcal{D}_{drop,t_0}^2 + 2\mathbb{C} \cdot \langle \mathcal{S} \rangle_{cumulonimbus} \cdot t_{cumulonimbus}} \quad \text{Equation 19}$$

467

468 Attention: In this equation,  $\mathcal{D}_{drop}(t)_{stratus}$  and  $\mathcal{D}_{drop}(t)_{cumulonimbus}$  are not the diameters of the droplets in the stratus and in the cumulonimbus, but  
 469 the diameters they would have had, if only the condensation mechanism had caused them to grow. We are in fact seeking to assess how large will be the  
 470 dilution of aerosol material in the droplets related to vapour condensation. There are other mechanisms modelled in DECAM (such as coalescence or riming,  
 471 **Figure 2**) that lead to the growth of hydrometeors, without necessarily diluting the aerosols in the droplets. If there had only been the condensation  
 472 mechanism, we could have used Figure 14 directly to assess this dilution.

473 For long periods of time, further simplification can still be made because  $\mathcal{D}_{drop,t_0}^2 \ll \mathcal{D}_{drop}(t)_{stratus}^2 < \mathcal{D}_{drop}(t)_{cumulonimbus}^2$ . Finally, we can write:

$$\frac{\mathcal{D}_{drop}(t)_{stratus}^2}{\mathcal{D}_{drop}(t)_{cumulonimbus}^2} = \frac{\langle \mathcal{S} \rangle_{stratus} \cdot t_{stratus}}{\langle \mathcal{S} \rangle_{cumulonimbus} \cdot t_{cumulonimbus}} \quad \text{Equation 20}$$

474 In this equation, the times  $t_{stratus}$  and  $t_{cumulonimbus}$  are therefore the times necessary for the formation of precipitation under the cloud. For each of the  
 475 types of cloud, we observe in Figure 6.a and Figure 12.a that these times are very similar ( $\approx 2200$  s), which allows us to write:

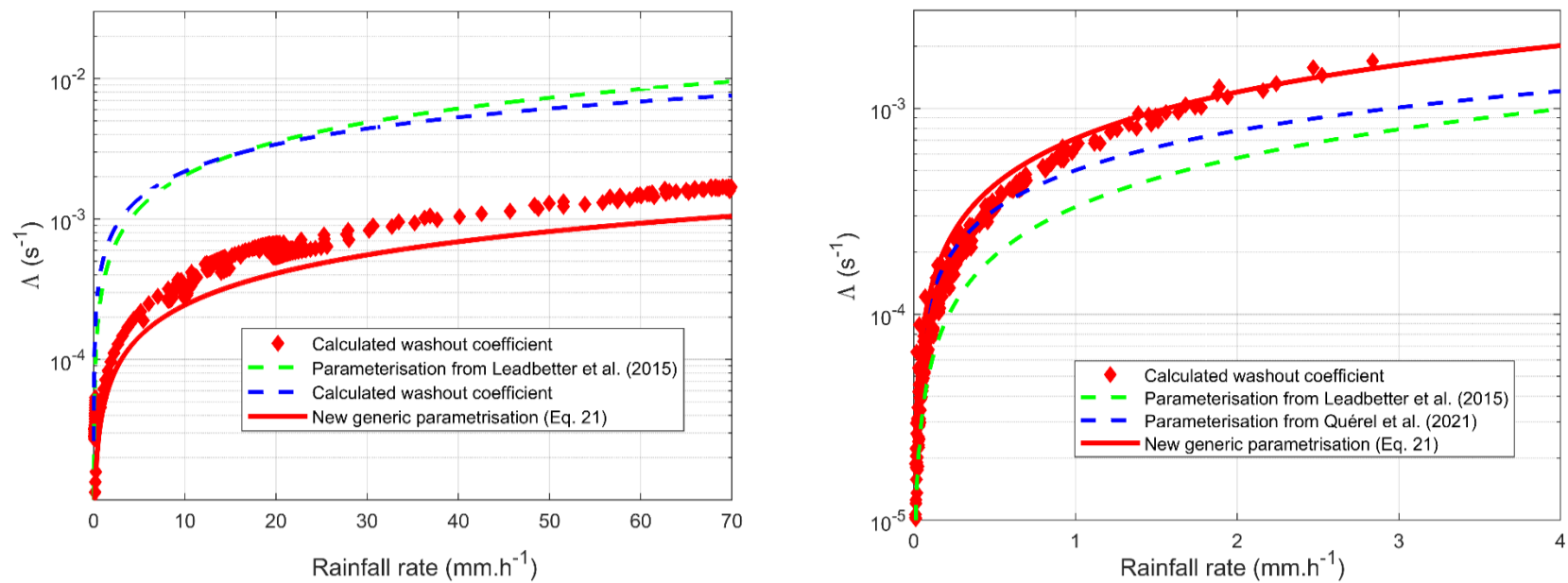
$$\frac{\mathcal{D}_{drop}(t)_{stratus}}{\mathcal{D}_{drop}(t)_{cumulonimbus}} = \sqrt{\frac{\langle \mathcal{S} \rangle_{stratus}}{\langle \mathcal{S} \rangle_{cumulonimbus}}} \quad \text{Equation 21}$$

476 The numerical application of this equation highlights a condensation growth ratio of a factor 2.3 between cumulonimbus and stratus. In mass, this coefficient  
 477 corresponds to a dilution factor of 12. However, Figure 18 shows that, with this new approach, we can calculate that cumulonimbus scavenges 6 times less  
 478 than stratus. This explanation is therefore satisfactory in view of all the hypotheses that have been made, especially since we have considered that the  
 479 activated aerosol mass remained constant when supersaturation increased. We therefore propose a new generic parametrisation to any type of cloud,  
 480 which this time considers this condensation-related dilution effect, Equation 22. This scavenging scheme is therefore corrected by a coefficient  $1/\langle \mathcal{S} \rangle_{cloud}^{3/2}$   
 481 which characterises the dilution related to the growth of droplets by condensation:

$$\Lambda_{cloud}^m = \frac{5 \times 10^{-8} \cdot 0.75}{\langle \mathcal{S} \rangle_{cloud}^{3/2}} I \quad \text{Equation 22}$$

482

483 The application of this new correlation, presented in Figure 20 shows an excellent match both for the cumulonimbus and for the simulated stratus. It  
 484 remains to be considered whether supersaturation is accessible in the NWP's and, if so, if the horizontal resolutions of 1 to 10 km of such models are  
 485 sufficiently representative of a real cloud.



486

487 Figure 20. Comparison of the newly developed correlation Equation 22 with the scavenging modelled by DESCAM for a cumulonimbus and a  
488 stratus.

489

490

### 491 **3. Conclusions**

492

493 The in-cloud scavenging scheme established in this article shows a dependence on rain intensity and average supersaturation in the cloud. Supersaturation  
494 allows the scheme to be applicable to both cumulonimbus and stratus clouds. If supersaturation in the cloud is not accessible, it is still possible to apply a  
495 different scheme for convective clouds and stratiform clouds. But, since this boundary between the two types of cloud may be ambiguous, it will be  
496 preferable to apply the scheme with supersaturation if available.

497 This scavenging scheme is based on the DESCAM microphysical cloud model. This model allows fine-scale description of the life cycle of a cloud up to  
498 precipitation development. It tracks particles, crystals, and droplets particle size distributions and models all the water phase changes and, above all, how  
499 aerosol particles impact them. The in-cloud scavenging scheme is established by calculating the mass fluxes of particle material exiting the cloud being  
500 included in precipitation hydrometeors (both liquid and solid) and based on the mass of particles initially present in the cloud volume.

501 This calculation of cloud volume has proved to be a complex issue, in particular for establishing the altitude of the cloud base, especially when rain occurs.  
502 The most relevant method to identify cloud base in this study has been proven to be the one using the number of hydrometeors, rather than the relative  
503 humidity or the mass of the hydrometeors. The problem with this method is that this information on the number is not available for most of the NWP. The  
504 use of the in-cloud scavenging scheme must be based on a diagnostic independent of the altitude of the base – and the summit – of the cloud.

505 In the case of stratus cloud, the parametrisation obtained with DESCAM is close to those currently used in the NAME and LdX atmospheric dispersion models,  
506 which were established on the basis of the Fukushima accident. As the precipitation that caused deposition of radioactive particles following the accident  
507 was largely generated by stratiform clouds, this study confirms *a posteriori* the choice of the in-cloud deposition scheme used to study radioactive deposition  
508 following the Fukushima accident and can be extended to all types of cloud.

509 In future works, this deposition scheme will be used with confidence to study deposition. As an example, it can be used for the deposition of radon progeny  
510 (Quérel *et al.*, 2022), in order to statistically measure the impact of this scheme in relation to the existing corpus.

511 Beyond the applications and validations of the scheme described in this article, the scheme itself is currently being refined. First of all, we are working on  
512 establishing an in-cloud scavenging rate that will depend on particle size. This important issue was discussed in section 1.3, and requires some modifications  
513 to the model to establish a model spectrally. This will make it possible to apply a finer-scale scheme to the atmospheric models with a spectral representation  
514 of the particles.

515 The influence of the coefficient  $\kappa$  of the  $\kappa$ -Köhler theory can be also examined. This will make it possible to measure the importance of the physical-chemical  
516 properties of the particles: what error is made by applying the same scavenging rate for a hygroscopic aerosol (salt or sulfate) and a non-hygroscopic aerosol  
517 (soot, desert dust).

518 The initial particle size distribution of aerosols could also have a significant influence on the final scavenging rate. A distribution centred on 100 nm will not  
519 create the same cloud as the same total mass centred around 5  $\mu\text{m}$  particles. This aspect must be assessed.

520 The question of evaporation of droplets between the cloud base and the ground has not yet been addressed. The scheme developed is based on the  
521 precipitation intensity at the cloud base, but in the models the precipitation intensity is diagnosed on the ground. This is important for the applicability of  
522 the scheme and this difference can lead to errors, especially in the event of high droplet evaporation.

523 Finally, it is not yet established that this scheme is as effective when applied to a model whose spatial resolution is lower than that of DESCAM, as is the  
524 case for all Climate (GCM) and Transport (ATM) models.

525 The work still to be carried out will make it possible to best define the scope of validity of this new scheme for in-cloud aerosol scavenging, as well as the  
526 uncertainties associated with this model. This will enable the scheme to be used in full knowledge of the facts and according to the highest scientific  
527 standards.

528

529

### 530 **Competing interests**

531 The contact author has declared that none of the authors has any competing interests.

532

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