Transformation of internal solitary waves ~~under ridged ice cover~~ at the ice-open water boundary

Kateryna Terletska[1,2], Vladimir Maderich[2], and Elena Tobisch[1]

[1]Institut für Analysis, Johannes Kepler Universität Altenberger Straße 69, 4040 Linz, Austria
[2]Institute of Mathematical Machine and System Problems, Glushkov av., 42, Kyiv 03187, Ukraine

Correspondence: Vladimir Maderich (vladmad@gmail.com)

Abstract. Internal wave-driven mixing is an important factor in the balance of heat and salt fluxes in the polar regions of the ocean. Transformation of ~~the~~ internal waves at the edge of the ice cover can ~~essentially~~ enhance the mixing and melting of ice in the Arctic Ocean and Antarctica. In the Polar Oceans ~~the~~ internal solitary waves (ISWs) are generated by various sources, including tidal currents over ~~the~~ bottom topography, the interaction of ice keels with tides, ~~varying in time~~ time-varying winds,
5   vortices, and lee waves. In ~~the~~ this study, a numerical investigation of the transformation of ISW propagating from open water in the stratified sea under the edge of the ice cover is carried out to compare the depression ISW transformation and loss of energy on smooth ice surfaces, including those on the ice shelf and glacier outlets, with the processes beneath the ridged underside of the ice. They were carried out using a nonhydrostatic model, that is based on the Reynolds averaged Navier-Stokes equations in the Boussinesq approximation for a continuously stratified fluid. The Smagorinsky turbulence model extended for stratified
10 fluid was used to describe the small-scale turbulent mixing explicitly. Two series of numerical experiments were carried out in an idealized 2D setup. The first series aimed to study the processes of the ISW of depression transformation under an ice cover of constant submerged ice thickness. ~~A energy~~ Energy loss was estimated based on a budget of depth-integrated pseudoenergy before and after the wave transformation. The transformation of ISW of depression is controlled by the blocking parameter β which is the ratio of the ~~height of the~~ minimum thickness of the upper layer under the ice cover to the incident wave amplitude.
15 The energy loss was relatively small for large positive and large negative values of β. The maximal value of energy loss was about 38%, and it was reached at $\beta \approx 0$ for ISW. In the second series of experiments, a number of keels were located on the underside of the constant thickness ice layer. The ISW transformation under ridged ice also depends on the blocking parameter β. For large keels ($\beta < 0$), more than 40% of energy is lost on the first keel, while for relatively small keels ($\beta > 0.3$), the losses on the first keel are less than 6%. Energy losses due to all keels depend on the distance between them, which is characterized
20 by the parameter μ which is the ratio of keel depth to the distance between keels. ~~If the tidal flow around the large keels is the source of internal waves, then under conditions of strongly ridged ice the waves excited by the tidal flow are dispersed in the vicinity of their formation.~~ In turn, for a finite length of the ice layer the distance between keels depends on the keel quantity.

1 Introduction

Internal wave-driven mixing is an important factor in the balance of heat and salt fluxes in the polar regions of the ocean (Guthrie et al., 2013). In these areas, internal gravity waves are generated by various sources, including tidal currents over the bottom topography e.g. (Urbancic et al., 2022), time-varying winds (Rainville and Woodgate, 2009), vortices (Johannessen et al., 2019), and lee waves (Vlasenko et al., 2003). Another source of energy for internal waves in the near-surface pycnocline can be an interaction of ice keels with tides (Zhang et al., 2022a). These waves, in the form of internal solitary wave (ISW), often propagate along the pycnocline in a stratified ocean under ice cover. The interaction between internal waves and ice cover is complex and depends on both the characteristics of the ice and the characteristics of internal waves (Carr et al., 2019). The transformation of an ISW under an ice keel can cause the advection of water below the ice layer, due to wave motion, whereas ISW shear and convective instabilities result in turbulent mixing. The heat advection and turbulent flux both will contribute to the vertical heat flux and consequently the change in temperature under the sea ice and increase of melting (Zhang et al., 2022b). An increased level of dissipation of the energy of internal waves propagating from the open water should be expected at the edge of the ice cover, which can represent the edge of an ice shelf or pack ice. In turn, the relief of the underside of the ice and, in particular, the presence of ice keels can essentially affect ISW transformation, breaking, and energy dissipation. These aspects of the complicated problem of the interaction of internal waves and ice cover have not yet been investigated due to severe conditions for field observations in the polar regions of the ocean.

The problem of the transformation of a depression ISW under smooth ice cover is mathematically close to the problem of the transformation of an elevation IWS over a bottom step of constant height which has been considered analytically (Grimshaw et al., 2008) and numerically using a nonhydrostatic model (Maderich et al., 2009; Talipova et al., 2013). It was found that the transformation of an ISW over the step in a two-layer fluid depends on the ratio of the thickness of the lower layer over the step to the ISW amplitude. The transformation of the elevation ISW over a single obstacle (ridge) on the bottom has been studied in the laboratory (Wessels and Hutter, 1996; Chen, 2007; Du et al., 2021) and numerically (Vlasenko and Hutter, 2001; Xu et al., 2016). Wave breaking on the lee side of the ridge was accompanied by the generation of second mode ISWs. The propagation of an elevation ISW over a corrugated bed (Carr et al., 2010) was accompanied by shear instability in the form of billows. ISWs propagating from open water to ice were studied in the laboratory by Carr et al. (2019) for grease, level, and nilas ice. The experiments showed that the dissipation of turbulent kinetic energy under the ice is comparable to that of the ISW in the water column. The disintegration of an ISW of depression under a single ice keel was simulated by Zhang et al. (2022b). It was concluded that corresponding turbulent mixing can enhance the melting of ice keels.

In this study, a numerical investigation of the transformation of an ISW propagating from ice-free water in the stratified sea under the edge of the ice cover is carried out to compare the depression ISW transformation and loss of energy on smooth ice surfaces, including those on the ice shelf, with the processes beneath the ridged underside of the ice. The rest of the paper is organized as follows. The formulation of the problem, the model setup, and the relevant numerical tools are given in Section

2. Section 3.1 presents the simulation results for smooth ice cover, whereas the results of the simulation of ridged ice cover are considered in Section 3.2. The results of the simulations are summarized and discussed in Section 4.

2 Numerical experiment setup

The numerical simulations were carried out using a nonhydrostatic model (Maderich et al., 2012). The numerical model used here is based on the Reynolds averaged Navier–Stokes equations in the Boussinesq approximation for a continuously stratified fluid. The Smagorinsky turbulence model extended for stratified fluid (Siegel and Domaradzki, 1994) was used to explicitly describe the small-scale turbulent mixing in the ocean-scale ISWs. Two series of numerical experiments were carried out in an idealized 2D setup. The first series aimed to study processes of the ISW of depression transformation under ice cover of constant submerged ice thickness (draft) h_{ice} (Fig. 1a). The second series was carried out to simulate the effect of ridged ice on ISW of depression propagation in a similar two-layer stratification (Fig. 1b). A computational tank of constant depth $H = 200$ m and length $L = 10000$ m was used. It was assumed that the ice layer of length $L_{ice} = 5000$ m is rigid and does not interact with ~~ISWs. A~~ the ISWs. The coordinate x is directed along the computational domain, and z is directed vertically upward. Idealized stratification of the vertical distribution of potential density is considered in the form:

$$\sigma_\theta = \frac{(\sigma_{\theta 2} - \sigma_{\theta 1})}{2} \tanh\left(\frac{z - h_1}{\Delta h}\right) + \frac{(\sigma_{\theta 2} + \sigma_{\theta 1})}{2}, \tag{1}$$

here h_1 is the thickness of the upper layer of water in the absence of the ice cover, $h_2 = H - h_1$ is the thickness of the lower layer, whereas $h_{1+} = h_1 - h_{ice}$. As shown by Maderich et al. (2010); Talipova et al. (2013), the transformation of both elevation and depression ISWs is controlled by the blocking parameter β which is the ratio of the height of the minimum thickness of the upper layer under the ice cover h_{1+} to the incident wave amplitude a_i:

$$\beta = \frac{h_{1+}}{a_i}, \tag{2}$$

where β is positive in the case $h_{1+} > 0$, $(h_1 > h_{ice})$ and negative for $h_{1+} < 0$, $(h_1 < h_{ice})$. In the first series submerged ice thickness h_{ice} was constant along the computational tank varying in different numerical experiments from 0.5 m to 40 m (Table 1). In the second series of experiments, several keels were placed underside of the ice layer of constant thickness h_{ice} (Fig.1b). The ice keel shape was approximated by Versoria function (Skyllingstad et al., 2003) as

$$h_{keel}(\delta x) = \frac{h_k b_k^2}{b_k^2 + (\delta x)^2}, \tag{3}$$

where h_k is maximal keel penetration, b_k is a parameter governing to determine the keel width, $\delta x = x - x_k$ is the horizontal distance from the centre of the keel placed at x_k. The keel form was similar: i.e. ~~the product of $h_k b_k$ was~~ h_k/b_k is constant. Following Zhang et al. (2022b), we define keel width as the horizontal width of the consolidated ice zone at a depth of 4 m

below the bottom of the ice (Marchenko, 2008). Typical values of h_k are $3 - 28$ m (Strub–Klein and Sudom, 2012) reaching 45 m (Leppäranta, 2007), whereas typical keel width varies in the range of $3 - 200$ m (Strub–Klein and Sudom, 2012). In the

85 ocean, the ratio of the maximum height of the keel h_k to the distance between the keels L_k varies from $1/20$ for heavily ridged ice to $1/1000$ for moderately ridged ice (Lu et al., 2011).

For this idealized case study, the vertical distribution of potential density anomaly mimics the summer profile of potential density over the Yermak Plateau (Randelhoff et al., 2017) in the Arctic Ocean ~~as~~ (1), where $h_1 = 20$ m, $\triangle h = 10$ m, $\sigma_{\theta1} = 25.4$ kg m^{-3}, $\sigma_{\theta2} = 27.7$ kg m^{-3}. As seen in Fig. 2, the summer profile of density ~~has not~~ does not have a well-mixed surface layer

90 due to the stratification caused by ice melting.
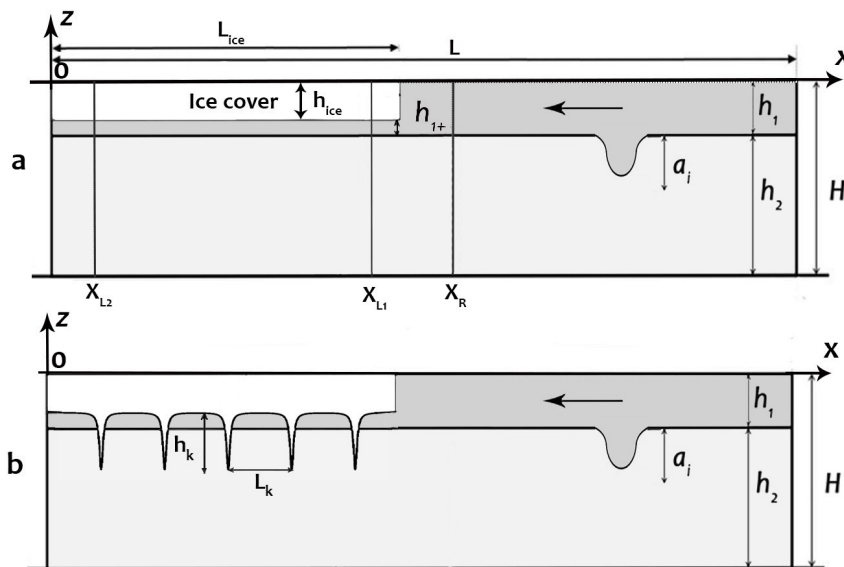
Figure 1. Sketch of the numerical configuration for simulation of ISWs transformation under the ice. (a) Smooth ice cover. (b) Ridged ice.

~~The free-slip~~ Free-slip boundary conditions were used at all boundaries except ~~the ice layer. The pressure zero gradient boundary condition was imposed on all~~ along the ice-water boundary. The Neumann-type boundary condition for the nonhydrostatic pressure component was used at the solid boundaries. At the free surface and open boundaries, this component was set zero (Maderich et al., 2012). At the corner of the underwater step, this condition is violated. However, numerical experiments for

95 different resolutions have shown that this problem does not occur at simulated fields of velocity and density. Ice-ocean tangential stress is parameterized using the quadratic bulk formula with a drag coefficient C_D. The value of C_D under ice varies in the range $10^{-3} - 10^{-2}$ (Lu et al., 2011). No-flux condition was also used at all boundaries. The model was initialized using the iterative solution of the Dubreil-Jacotin-Long (DJL) equation (Dubreil-Jacotin, 1932) with the initial guess obtained from a weakly nonlinear theory. The DJLES spectral solver from the MATLAB package https://github.com/ mdunphy/DJLES/ was

100 used to generate ISW of depression.
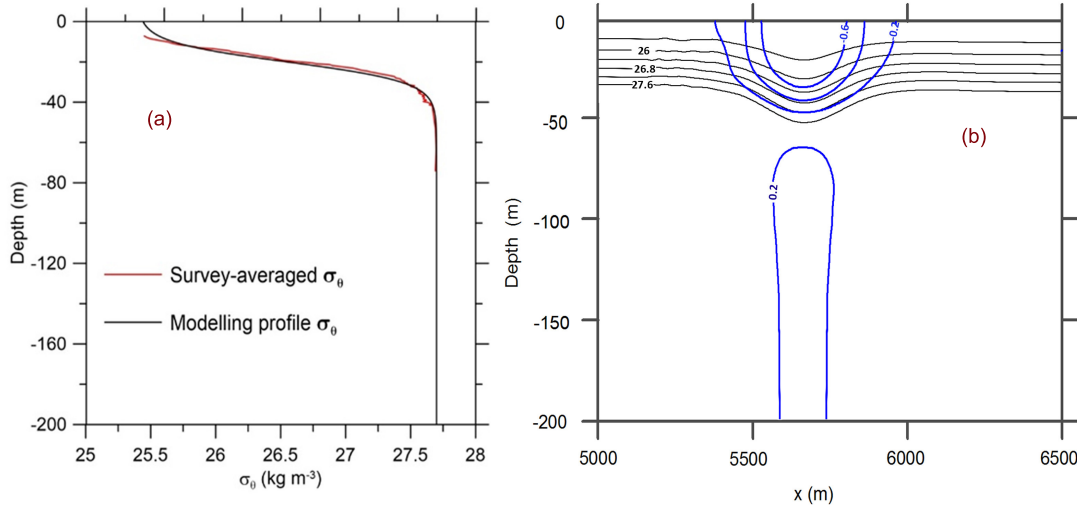
Figure 2. The comparison of the background stratification in the computational tank (1) with the survey averaged profile of anomaly of potential density σ_θ (Randelhoff et al., 2017) (a); The vertical cross-section of potential density and horizontal velocity fields in the incident ISW of amplitude 15 m (b).

To get around the difficulties associated with the numerical solution of the nonhydrostatic model equations in the presence of an ice layer, we considered the setting mirrored for the upper surface of the ocean, in which the ice layer was replaced by a step on the bottom. Then the vertical profile (1) was replaced by the distribution

$$\sigma_\theta = \frac{(\sigma_{\theta 1} - \sigma_{\theta 2})}{2} \tanh\left(\frac{z - (H - h_1)}{\Delta h}\right) + \frac{(\sigma_{\theta 2} + \sigma_{\theta 1})}{2}, \tag{4}$$

105 where $\sigma_{\theta 1} = 27.7 \, \text{kg m}^{-3}$, $\sigma_{\theta 2} = 25.4 \, \text{kg m}^{-3}$. The initial ISW of depression was changed, respectively, to a ISW of elevation. This approach is accurate when we consider the problem with rigid lid approximation at the free surface. However, the numerical model is a free-surface model, which leads to bottom fluctuations outside the step in the computational flume. Therefore, we conducted tests with ISWs of the same amplitude propagating as ~~a~~ an ISW of depression and as ~~a~~ an ISW of elevation in stratification (1) and (4). The tests aimed to estimate the effect of the free surface on the wave characteristics for free-slip

110 boundary conditions. These results demonstrate a weak effect of the free surface on ISW dynamics in the considered cases, which made it possible in this problem to replace the conditions on the free surface with conditions on the rigid lid. The results of the comparison for horizontal velocity taking into account the mirror reflection of the vertical coordinate in Fig. 3 showed that the difference in the velocity between the two configurations of the model does not exceed 1%. Note that in laboratory experiments (Carr et al., 2008; Luzzatto-Fegiz and Helfrich, 2014) the influence of a free surface on the stability of waves with

115 a trapped core was shown. This effect has been interpreted as the influence of surfactants essential in laboratory-scale pro-

cesses, however, these Marangoni effects have a negligible impact on the interior of full-scale oceanic waves (Luzzatto-Fegiz and Helfrich, 2014).
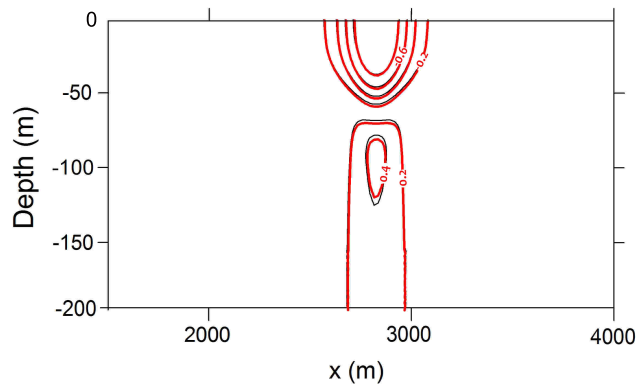
Figure 3. The comparison of the vertical cross-section of horizontal velocity fields in a wave of depression (black line) and a wave of elevation (red line) in stratification (1) and (4) respectively for ISW with an amplitude 33 m.

In the first series of experiments, 48 runs were performed using the generalized vertical system of coordinates (Maderich et al., 2012). The vertical and horizontal grid resolution was 400×3000. The quasi-z-level coordinate system (Maderich et al.,
120 2012) was used to describe this step-like ice layer. These runs cover a range of incident ~~ISW with moderate~~ISWs with moderate, $a_i = 8$ m, and large amplitudes, $a_i = 33$ m (Table 1). The incident ISW amplitude is defined as the maximum displacement of the undisturbed isopycnals. The wavelength $\lambda_{0.5}$ is estimated as the half-width ~~with which the~~ at the depth where the amplitude of the wave is reduced by half. ~~It was considered two~~Two cases with different drag coefficients ($C_D = 0.001$ and $C_D = 0.01$) were considered to investigate the influence of ice roughness on ISW transformation and energy loss. A wide range of ice cover
125 drafts h_{ice} from 0.5 m to 40 m ~~was considered~~ were used to investigate processes under ice cover from first-year ice to the ice shelf front.

In the second series of experiments (see Table 2), 12 runs (K1-K12) were performed using a sigma-system of coordinates, which allowed for accurately describing flow around the keel. The vertical and horizontal grid resolution was also 400 x 3000. The density stratification in this series was the same as in the first series. The ISW amplitude was $a_i = 15$m, wavelength $\lambda_{0.5} = $
130 320 m, and drag coefficient $C_D = 0.001$. The ice draft was 1 m which mimics one-year ice. The keel's maximal penetration h_k varied from 7 m to 21 m, and the width of the keel varied from 67 m to 200 m at a depth of 4 m.

To take into account the geometric characteristics of the keels and their frequency, we introduce the parameter μ which is the ratio of sum of submerged ice thickness and maximal keel penetration to the distance between keels

$$\mu = (h_{ice} + h_k)/L_k. \tag{5}$$

Table 1. The parameters of the first series of runs.

Run	a_i	h_{ice}	a_i/h_1	C_D	β
	m	m			
1-6	33	0.5, 5, 10, 20, 30, 40	1.65	0.001	$0.6, 0.45, 0.3, 0, -0.3, -0.6$
7-12	25	0.5, 5, 10, 20, 30, 40	1.25	0.001	$0.78, 0.6, 0.4, 0, -0.4, -0.8$
13-18	15	0.5, 5, 10, 20, 30, 40	0.75	0.001	$1.3, 1, 0.7, 0, -0.7, -1.33$
19-24	8	0.5, 5, 10, 20, 30, 40	0.4	0.001	$2.44, 1.88, 1.25, 0, -1.25, -2.5$
25-30	33	0.5, 5, 10, 20, 30, 40	1.65	0.01	$0.6, 0.45, 0.3, 0, -0.3, -0.6$
31-36	25	0.5, 5, 10, 20, 30, 40	1.25	0.01	$0.78, 0.6, 0.4, 0, -0.4, -0.8$
37-42	15	0.5, 5, 10, 20, 30, 40	0.75	0.01	$1.3, 1, 0.7, 0, -0.7, -1.33$
43-48	8	0.5, 5, 10, 20, 30, 40	0.4	0.001	$2.44, 1.88, 1.25, 0, -1.25, -2.5$

Table 2. The parameters of the second series of runs

Run	h_{ice}	h_k	b_k	L_k	β	μ	E_{loss}	E_{tot}
	m	m	m	m			%	%
$K1$	1	21	49.5	250	-0.13	0.088	-	82.4
$K2$	1	21	49.5	500	-0.13	0.044	-	76.3
$K3$	1	21	49.5	1000	-0.13	0.022	-	64.3
$K4$	1	21	49.5	> 5000	-0.13	—	41.2	47.4
$K5$	1	14	33	250	0.33	0.06	-	42.6
$K6$	1	14	33	500	0.33	0.03	-	40.2
$K7$	1	14	33	1000	0.33	0.015	-	29.8
$K8$	1	14	33	> 5000	0.33	—	6.3	13.2
$K9$	1	7	16.5	250	0.8	0.032	-	43.6
$K10$	1	7	16.5	500	0.8	0.016	-	37.3
$K11$	1	7	16.5	1000	0.8	0.008	-	28.6
$K12$	1	7	16.5	> 5000	0.8	—	3.5	10.2
$S1$	22	0	—	—	-0.13	—	36.2	75.2
$S2$	5	0	—	—	1	—	8.8	22

135   In ~~the~~ turn, for a finite length of the ice layer L_{ice} the distance between keels depends on keel number n as $L_k = L_{ice}/n$. In the second series μ varies in experiments $K1 - K3$ from 0.008 to 0.088 (Table 2). To directly compare with the step case, calculations were made for step (S1) with the same draft as the height of the keel in the ~~K1 experiment~~ K1-K4 experiments. In another experiment (S2), the step draft was chosen to be equal to the average draft in experiment ~~K1~~ K2.

3 Results

3.1 First series of experiments

The results of the first series of experiments for the transformation of a depression ISW for an incident wave at the ice were given for a wide range of ice drafts, incident wave amplitudes, and drag coefficients (Table 1). ~~As shown by (Maderich et al., 2010; Talipova), the transformation of both elevation and depression ISW is controlled by the blocking parameter β which is the ratio of the height of the minimum thickness of the upper layer under the ice cover h_{1+} to the incident wave amplitude a_i:~~

$$\beta = \frac{h_{1+}}{a_i}.$$

The snapshots of the density field for an incident ISW of amplitude $a_i = 15$ m passing under the ice cover are shown in Fig. 4 for different β. Transformation under ~~the~~ thin ice ($h_{ice} = 0.5$ m) with ~~the~~ $\beta = 1.3$ occurs without any instability and essential disturbances. For ~~increasing ice draft at~~ increased ice draft $\beta = 0.7$ ($h_{ice} = 10$ m), ~~it can be seen changes in the~~ the incident wave changes its form and amplitude ~~of the incident wave passing~~ as it passes under the ice. The amplitudes of reflected and transmitted waves were well predicted by the theoretical model (Grimshaw et al., 2008). For $\beta = 0$ ($h_{ice} = 20$ m) the transmitted wave has a smaller amplitude, and more energy is transferred to ~~reflected from~~ the reflected wave at the ice edge~~ISW~~. Waves under the ice transform into strongly nonlinear boluses, and more energy goes to the reflected waves when the draft of the ice is equal to the depth of the upper layer ($\beta = 0$). The bolus under the ice becomes smaller and reflected waves form as a result of the strong interaction with the ice front at $\beta = -0.7$ ($h_{ice} = 30$m).

An important characteristic of the ISW-ice interaction is the loss of kinetic and available potential energy during the ISW transformation. Energy transformation due to mixing leads to the ~~transition~~ transfer of energy to background potential energy and energy dissipation. An energy loss was estimated based on a budget of depth-integrated pseudoenergy before and after the wave transformation following (Lamb, 2007) and (Maderich et al., 2010). The characteristics of the incoming and reflected wave were recorded in the cross-sections X_R (Fig. 1a), which are located near the ice edge and in two cross-sections (X_{L1} placed at a distance of 500 m from the ice edge, and X_{L2} placed at a distance of 4500 m from the ice edge (Fig. 1a). The energy loss ΔE_{loss} in the cross-section x_{L1} characterizes energy transformations in the vicinity of ice edge, whereas energy losses ΔE_{visc} take into account the dissipation of energy due to the underside ice friction effects.

The total energy of the incident, reflected, and transmitted waves was calculated using the depth-integrated pseudoenergy flux $F(x,t)$ to find the balance of the total energy

$$F(x,t) = \int_{-H}^{0} (E_{PSE} + p)U\,dz, \tag{6}$$

where p is the pressure disturbance due to the passing wave, U is the horizontal velocity, and E_{PSE} is the pseudoenergy density, which is a sum of kinetic energy density E_k and available potential density E_a (part of the potential energy available
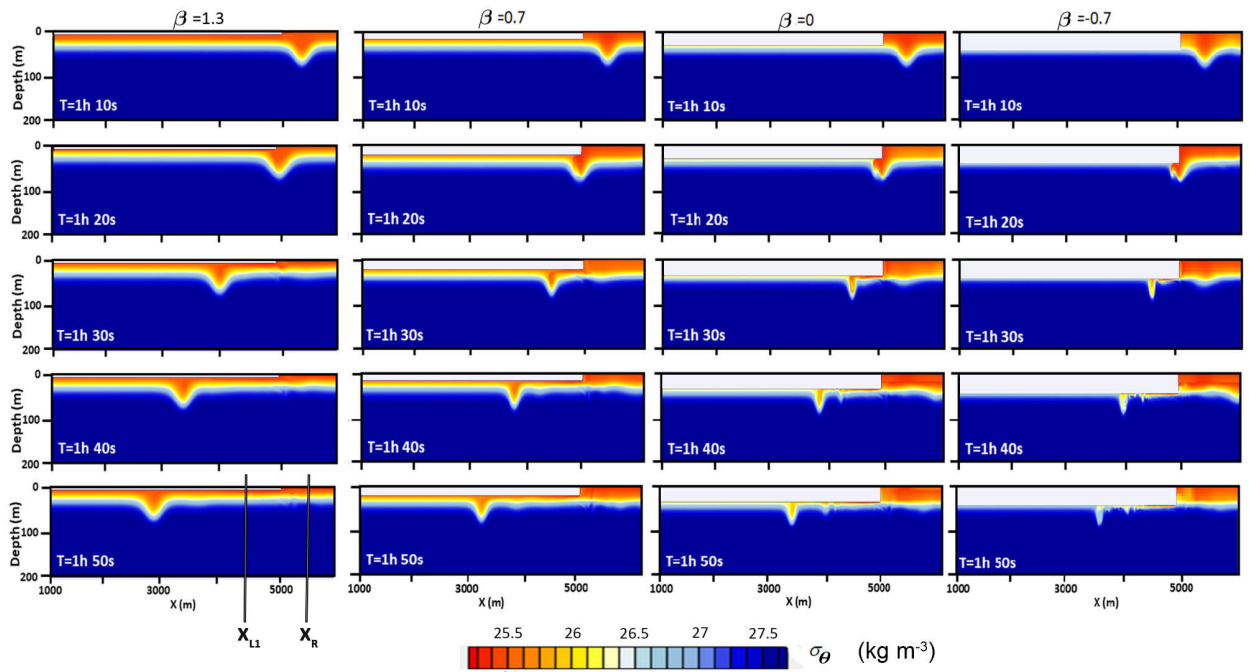
Figure 4. The snapshots of the density field for incident ISW with amplitude 15 m passing under the ice cover with a different draft. The integration region for the energetics calculations between X_{L1} and X_R is shown.
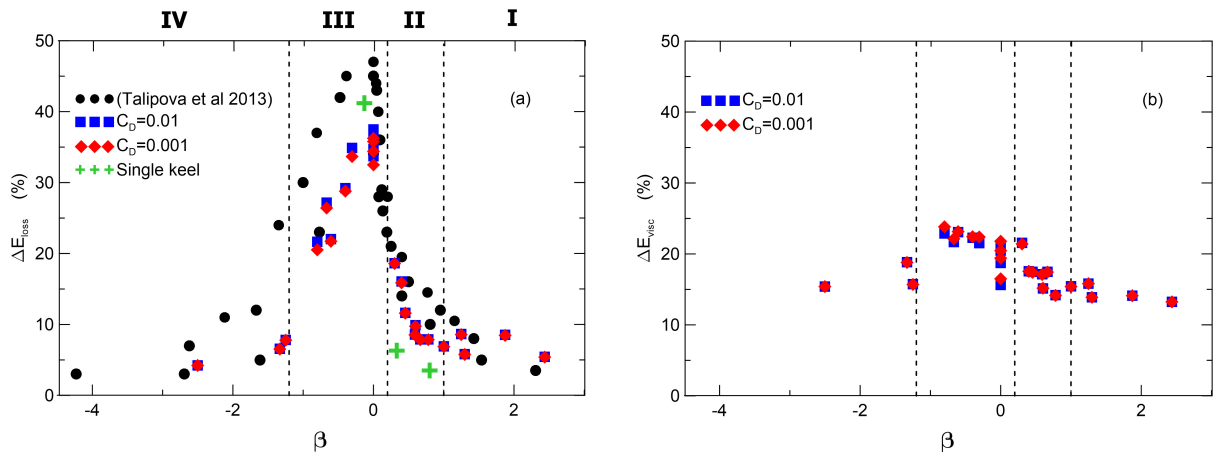
Figure 5. (a) The ISW energy loss ΔE_{loss} under the ice cover versus the blocking parameter β for various amplitudes of an incident wave (b) ΔE_{visc} that take into account the dissipation of energy due to the underside ice friction effects versus the blocking parameter β.

for conversion into kinetic energy). For the calculation of E_a, we used a reference density profile that was obtained by an adiabatic rearranging of the density field. The volume integration of these flows outside the mixing zone allows us to estimate

170 the energy of the incoming PSE_{in}, reflected PSE_{ref}, and transmitted under ice ~~ISW~~ ISWs in cross-sections ~~X_{L1}~~ X_{L1} and X_{L2} (~~from~~ see Fig. 1 a)PSE_{tr1} and PSE_{tr2} respectively:

$$
\begin{aligned}
PSE_{in} &= \int_{X_R}^{L} \int_{-H}^{0} E_{PSE} dz dx = -\int_{t_1}^{t_2} F(X_R, t) dt, \\
PSE_{tr1} &= \int_{0}^{X_{L1}} \int_{-H}^{0} E_{PSE} dz dx = -\int_{t_2}^{t_3} F(X_{L1}, t) dt, \\
PSE_{ref} &= \int_{X_R}^{L} \int_{-H}^{0} E_{PSE} dz dx = \int_{t_2}^{t_3} F(X_R, t) dt \\
PSE_{tr2} &= \int_{0}^{X_{L2}} \int_{-H}^{0} E_{PSE} dz dx = -\int_{t_4}^{t_5} F(X_{L2}, t) dt,
\end{aligned}
\tag{7}
$$

where ~~t_1, t_2, t_3, t_4, t_5 are time intervals when incoming, reflected, and transmitted waves pass the given~~ $t_2 - t_1$ is the interval of time when the incoming wave passes the cross-section ~~.~~ X_R, $t_3 - t_2$ is the interval of time when transmitted and reflected

175 wave pass the cross-sections X_{L1} and X_R respectively. Time interval $t_5 - t_4$ corresponds to the transmitted wave passes the cross-section X_{L2}.

The normalized energy loss ΔE_{loss}, ΔE_{visc} and ΔE_{tot} are given by

$$
\begin{aligned}
\Delta E_{loss} &= (PSE_{in} - PSE_{tr1} - PSE_{ref})/PSE_{in}, \\
\Delta E_{tot} &= (PSE_{in} - PSE_{tr2} - PSE_{ref})/PSE_{in}, \\
\Delta E_{visc} &= \Delta E_{tot} - \Delta E_{loss} = (PSE_{tr1} - PSE_{tr2})/PSE_{in}.
\end{aligned}
\tag{8}
$$

The energy loss as a result of ISW transformation under ice ΔE_{loss} at interval $X_R - X_{L1}$ versus the blocking parameter β is

180 shown in Fig. 5a. This loss was relatively small for large positive and large negative values of β. The maximal value of energy loss was about 38%, and it was reached at $\beta \approx 0$. The character of energy losses and the relationship between transmitted and reflected ISW energy ~~allow~~ allows us to distinguish different regimes for ISW interaction under ice cover: the weak interaction (I), moderate interaction (II), strong interaction (III), and reflection regime (IV). The weak interaction (I) is when the ISW transforms under ice cover without any instability; the energy losses are mainly due to viscous dissipation. It corresponds to

185 values $\beta > 0.5$. The energy losses at cross-sections X_R - X_{L1} are about 10%. The amplitudes and numbers of reflected and transmitted waves are well predicted by the theoretical model of (Grimshaw et al., 2008). Moderate interaction (II) occurs when the waves become unstable under ice cover, resulting in energy losses due to the turbulent mixing varying from 10% to 20%. The strong interaction (III) of the ISW with the ice is the regime when the flow under the ice is supercritical. This regime is identified by the condition that the maximal composite Froude number Fr_{max} at the step cross-section is greater than 1,

190 where Fr is defined as

$$
Fr^2 = \frac{(U_1)^2}{g' h_1(x)} + \frac{(U_2)^2}{g' h_2},
\tag{9}
$$

where U_1 and U_2 are the layer-averaged velocities in each layer, $g' = g \cdot \Delta\rho/\rho_0$, where g is the gravity acceleration, $\Delta\rho$ and ρ_0 are the density difference between upper and lower layers and undisturbed density of fluid, respectively.

Supercritical flow $Fr_{max} = 1$ resulted in bolus formation and intensive mixing, which reached about 40 %. The reflection regime (IV) is when the height of the ice floe is large enough to result in full reflection of the ISW. The energy losses are again small ($\triangle E_{loss}$ less than 10%–15%). In this regime, energy losses depend on the wave amplitude; small and moderate incident waves reflect without turbulent mixing. This dependence of ΔE_{loss} on β is comparable to values for a bottom step (Talipova et al., 2013) obtained using direct simulation by the Navier-Stokes equations (Fig.5a). The differences in values of the energy losses from (Talipova et al., 2013) and from the present investigation can be explained by the fact that the field scale problem was studied in this work using the Reynolds averaged equations, while in (Talipova et al., 2013) the propagation of ISWs in a laboratory-scale computational domain was studied by using the Navier-Stokes equations. The eddy viscosity and diffusivity calculated from the turbulence model (Siegel and Domaradzki, 1994) vary in space and time with characteristic values $10^{-4} - 10^{-3}$ m^{2}s^{-1}. The difference between the energy losses in the cross-sections X_{L2} and X_{L1} characterizes their losses due to friction effects. This difference $\Delta E_{visc} = \Delta E_{tot} - \Delta E_{loss}$ is shown in Fig.5b as the function of β. This shows that, the contribution of friction is $15 - 20$ % of the energy of the incident wave. The simulations showed a weak dependence of energy loss on the friction parameter C_D (Fig. 5b).

3.2 Second series of experiments

The results of the second series of experiments for the transformation of depression ISWs under ridged ice for different ice keel heights and distances between keels (Table 2) are discussed in this section. Similar to (2), we can introduce the blocking parameter for a single keel in the form

$$\beta = \frac{h_1 - h_{ice} - h_k}{a_i}. \tag{10}$$

The snapshots of the density field for an incident ISW passing under the layer of constant draft (Run S1 from Table 2) are compared in Fig. 6 with the results for a wave passing under ridged ice (Run K2). In Run S1 the ISW amplitude is comparable to the draft of ice and thickness of the upper layer h_1, therefore interaction was strong. Initially (time interval: $T = 1$ h 30 m - 1 h 35 m), the wave propagated under the ice as a bolus (Fig. 6 a). This process is accompanied by intensive mixing. The bolus gradually loses mass. Estimates of energy loss at a distance of 500 m from the ice front E_{loss} in (Run S1 in Table 2) showed that 36.2% of energy was lost to mixing and dissipation, whereas loss of energy at the full length of ice cover (5000 m) was twice as much (E_{tot}=75.2%). The processes of ISW disintegration and mixing for ridged ice differ essentially from the case of the ice layer of the constant draft. The snapshots of the density field for the ISW passing under the ridged ice (Run K2) are shown in Fig. 6 b. As seen in the figure, the flow accelerates at the rear side of the keel ($T = 1$ h30 m, Fr_{max} reaches the value 1) entraining denser water from the underlying layers. The resulting vortex is accompanied by intense mixing ($T = 1$ h 33 m - 1 h45 m). The process of transformation of this wave with a slightly smaller amplitude is repeated on subsequent keels. As a result of passing through the first keel, the wave loses about 41% of incident wave energy. Energy
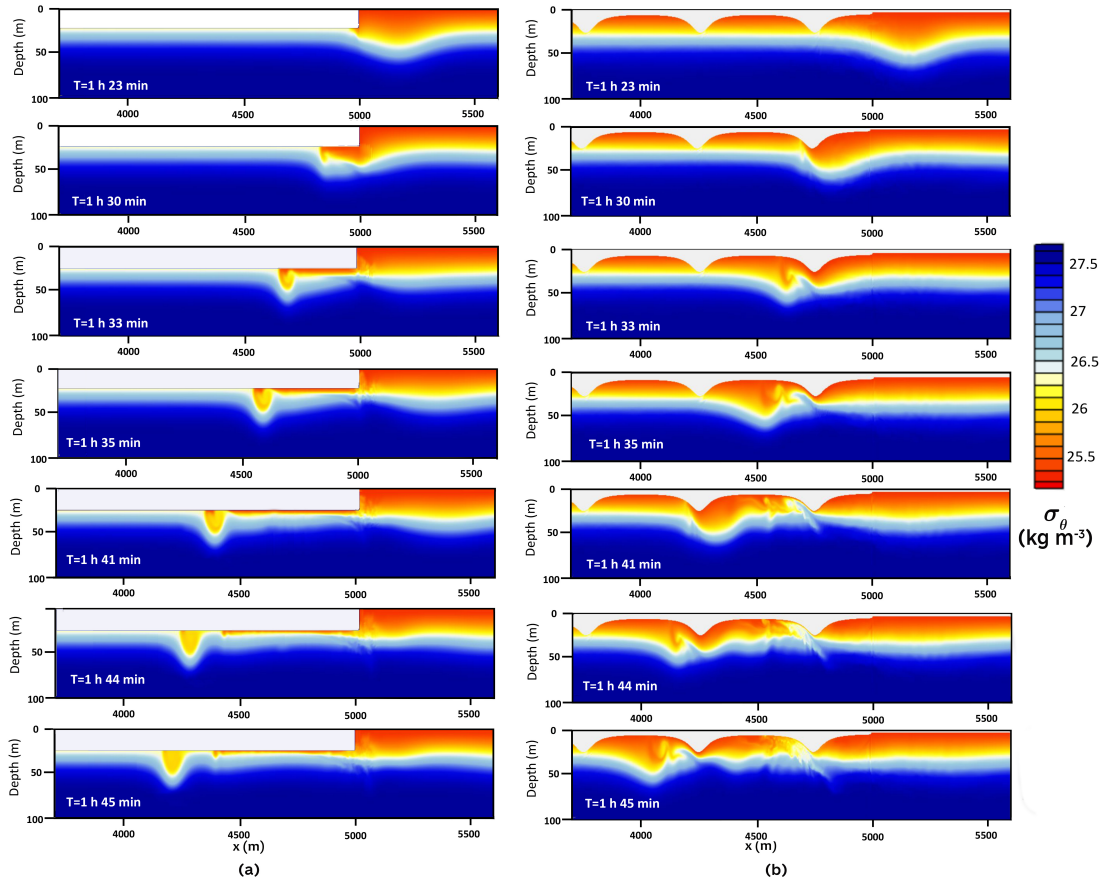
Figure 6. (a) The transformation of ISW of depression under a smooth ice layer (Run S1); (b) The transformation of ISW of depression under a ridged ice layer (Run K2).

losses due to all keels depend on the distance L_k between them, that in turn depend on keel quantity. When $\beta = -0.13$ E_{tot} changes from 47.4% for a single keel to 82.4 % for $L_k = 250$ m. This means that energy losses on the first keel account for about half of all losses. For $L_k = 1000$ m, the energy loss due to all keels was 64.3 %. As β increases to 0.8, the contribution of the first keel decreases to 3.5 %.

230   In the limiting case of the interaction of ISW with a single keel (Zhang et al., 2022b), the maximum energy dissipation was about 25% which is somewhat less than in our calculations, but we need to keep in mind the differences in the calculation parameters and turbulence ~~parametrization. Zhang et al. (2022b)~~ parameterization. Zhang et al. (2022b) used constant eddy coefficients whereas in our study the ~~model of turbulence was used where eddy coefficients vary~~ turbulence model was used with eddy coefficients varying in space and time. To characterize the dependence of ΔE_{tot} on keel height and
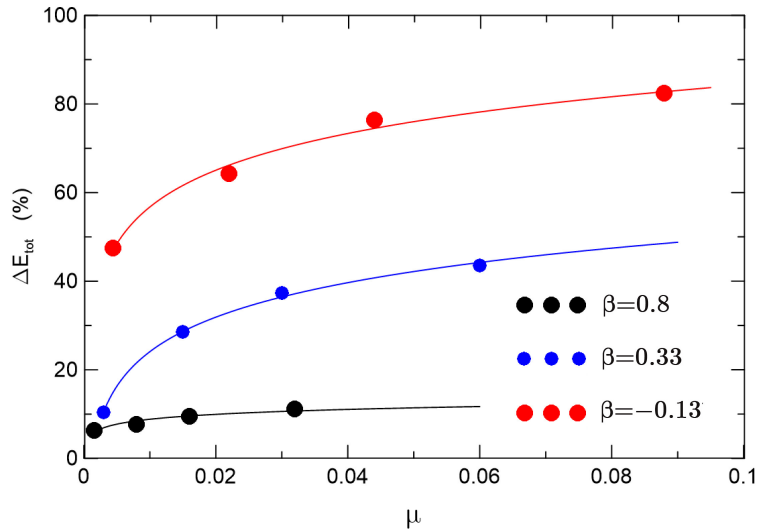
Figure 7. The ISW energy loss $\triangle E_{loss}$ under the ice cover versus parameter μ. The logarithmic curves approximate calculated dependencies.

distance between keels we introduced parameter μ (5). As seen in Fig. 7 this dependence can be approximated by logarithmic curves $\Delta E_{loss} = q \ln \mu + r$, where $\beta = (0.8, 0.33, -0.13)$, $q = (1.60, 11.24, 11.96)$, $r = (16.21, 75.84, 111.85)$. The energy loss ΔE_{tot} increases with the decrease of distance between keels or an increase of keel height. The level of ΔE_{tot} is highest for β values near zero. As seen in Fig. 5a, this range of β corresponds to the regime of strong interaction (III). Energy loss in this regime is maximal, both in the case of the ridged underside of the ice and in the case of smooth ice surfaces with the same parameter β. When β values increase, the dependence of energy loss on the μ and distance between the keels decreases. ~~For~~ $\beta = 0.8$ is on the boundary between ~~regime~~ regimes (II) ~~moderate~~ and (I) ~~weak interaction~~ (moderate ad weak) and the distance between the keels is no longer significant. ~~If we assume that the tidal flow around the keels is the source of internal waves (Zhang et al., 2022b), then we can conclude based on our simulations that under conditions of strongly ridged ice, the waves excited by the tidal flow disperse in the vicinity of their formation.~~

In another limiting case, an ISW of elevation propagates over a corrugated bottom when the bottom element length was much less than the ISW wavelength (Carr et al., 2010) a comparison with ISW propagated under an ensemble of ice keels of horizontal scales greater than ISW length was not straightforward. In addition, Reynolds equations with turbulent closure describe real-scale processes in the ocean, in contrast to laboratory scales in ~~(Carr et al., 2010). Unlike (Carr et al., 2010)~~ Carr et al. (2010). Unlike Carr et al. (2010) we cannot describe in detail the instant spatial-temporal dynamics of high shear ~~region~~ layer near the ice. However, ~~the~~ Fig. 6 b ~~showed~~ shows wave-induced currents over the keels, their interaction with the apex of the keels and a sequence of lee vortices formed as a result of such interaction (see Fig. 6 b $T = 1$ h 35 m, $T = 1$ h 41 m). Similarly to ~~(Carr et al., 2010)~~ Carr et al. (2010) the vortices developed after the main wave passed over the keel (see Fig.

6 b at $T = 1$ h 44 m, $T = 1$ h 45 m) resulting in deformation of the overlying pycnocline and, in some instances, significant vertical mixing.

4   Conclusions

In ~~the~~ this study, a numerical investigation of the transformation of ISW propagating from open water in ~~the stratified sea under the edge of the ice cover~~ a stratified sea into an ice covered region is carried out. We compared the ~~depression ISW transformation and loss of energy on~~ transformation and energy loss of depression ISW under smooth ice surfaces, ~~including those on the ice shelf and glacier outlets or fast ice,~~ with the processes beneath ~~the ridged underside of the~~ ridged ice. It was shown that the transformation of depression ~~ISW~~ ISWs under smooth ice cover is controlled by the blocking parameter β. Several regimes of ISW transformation ~~under ice cover~~ at the ice-open water boundary were identified: (I) the weak interaction when the ISW transforms under ice cover without any instability; the energy losses are caused mainly due to viscous dissipation. It corresponds to values $\beta > 0.5$; (II) moderate interaction, which occurs when the waves become unstable under ice cover resulting in energy losses due to the turbulent mixing varying from 10% to 20%; (III) strong interaction of ISW with the ice($\beta \simeq 0$) is the regime when the flow under the ice was supercritical and the values of energy loss were about 38% ; and reflection regime (IV), when the depth of the ice cover is large enough to result in full reflection of the ISW. The ice's roughness has relatively little effect on energy conversions under ice cover.

The ISW transformation under ridged ice also depends on the blocking parameter β. For large keels ($\beta < 0$), more than 40% of energy is lost on the first keel, while for relatively small keels ($\beta > 0.3$), the losses on the first keel are less than 6%. The energy losses in the flow around the ridges can be of the same order as for ice cover, in which the draft is commensurate with the amplitude of the keels. Energy losses due to all keels depend on the distance between them, which in turn depends on a keel quantity. These losses which is characterized by the parameter μ which is the ratio of keel depth to the distance between keels. ~~If the tidal flow around the large keels is the source of internal waves, then under conditions of strongly ridged ice the waves excited by the tidal flow are dispersed in the vicinity of their formation.~~

The energy loss processes of ISWs under ice deserve more ~~profound~~ in-depth studies to bridge with ISWs mixing and heat balance of polar oceans (Pinkel, 2005). The next step could be an explicit representation of heat and salt fluxes between the ice cover due to the ISW interaction with the ridged ice, e.g. following flux parametrization by (McPhee et al., 1987).

Code availability.   The output files for all numerical experiments reported in the paper are available from the corresponding author.

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Competing interests. The authors declare that they have no conflict of interest.

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