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Influence of Stratification and Wind Forcing on the Dynamics of Lagrangian Residual Velocity in a Periodically Stratified Estuary

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Abstract

Wind and stratification play pivotal roles in shaping the structure of the Lagrangian residual velocity (LRV). However, the intricate dynamics by which wind and stratification modify the LRV remain poorly studied. This study derives numerical solutions of LRV components and eddy viscosity subcomponents to elucidate the dynamics within the periodically stratified Pearl River estuary. The vertical shear cross-estuary LRV (u_L) is principally governed by the interplay among the eddy viscosity component (u_{Ltu}), the barotropic component (u_{Lba}), and the baroclinic component (u_{Lgr}) under stratified conditions. During neap tides, southwesterly winds notably impact u_L by escalating u_{Ltu} by an order of magnitude within the upper layer. This transforms the eastward flow dominated by u_{Ltu} under wind influence into a westward flow dominated by u_{Lba} in upper shoal regions without wind forcing. The along-estuary LRV exhibits a gravitational circulation characterized by upper-layer outflow engendered by barotropic component (v_{Lba}) and lower-layer inflow predominantly driven by baroclinic component (v_{Lgr}). The presence of southwesterly winds suppresses along-estuary gravitational circulation by diminishing the magnitude of v_{Lba} and v_{Lgr}. The contributions of v_{Lba} and v_{Lgr} are approximately equal, while the ratio between u_{Lba} and u_{Lgr} (u_{Ltu}) fluctuates within the range of 1 to 2 in stratified waters. Under unstratified conditions, LRV exhibits a lateral shear structure due to differing dominant components compared to stratified conditions. In stratified scenarios, the eddy viscosity component of LRV is predominantly governed by the turbulent mean component, while it succumbs to the influence of the tidal straining component in unstratified waters.

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1. Introduction

Tidal currents are the principal movement in shallow seas and estuaries. However, tidal oscillations are not the predominant factor regarding the long-term transport of mass, such as pollutants, sediments, nutrients, and suspended materials. Instead, residual current, which remains after filtering out tidal movements, plays a crucial role in long-term mass transport. Therefore, unveiling the dynamic mechanisms governing the structure and magnitude of the residual current becomes particularly significant for a correct understanding of the circulation and long-term mass transport in shallow seas and estuaries.

Pritchard (1952) proposed a conceptual model of estuarine circulation characterized by a two-layer structure, drawing from extensive observations. A subsequent study by Pritchard (1956) emphasized the crucial role of the horizontal density gradient as the primary driving force for estuarine circulation. Subsequently, the theory of estuarine gravitational circulation was developed, assuming a constant eddy viscosity (Hansen and Rattray, 1965). Nevertheless, it is imperative to acknowledge that estuarine circulation is influenced not solely by density gradients but also by factors such as wind, tides, and other dynamic forces. These external factors possess the ability to modify or even reverse the structure of gravity circulation within estuaries.

Several studies have highlighted the significant impact of tidal straining on Eulerian residual velocity (ERV) (Becherer et al., 2011; Monismith et al., 1996). Jay and Musiak (1994) found the ERV induced by tidal straining is comparable to gravitational circulation. Additionally, tidal straining contributes twice as much to the ERV as gravitational circulation without consideration of river runoff (Burchard and Hetland, 2010). The flow induced by tidal straining varies in estuaries with different stratified conditions. When the horizontal density gradient is small, tidal straining dominates the structure of the ERV (Burchard et al., 2011). Cheng et al. (2011) showed that tidal straining induces a typical two-layer circulation in weakly

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stratified estuaries, while the circulation exhibits a vertical three-layer structure with inflow in the upper and lower layer and outflow in the middle layer in partially and strong stratified estuaries. As stratification intensifies, the ratio of flow induced by tidal straining to gravitational circulation decreases. In a weakly stratified short estuary, tidal straining plays a secondary role in ERV compared to gravitational circulation (Wei et al., 2021). Geyer and MacCready (2014) indicated that the Eulerian mean method tends to overestimate the contribution of tidal straining. Therefore, it is more reasonable to analyze dynamical mechanisms for residual current from the perspective of the Lagrangian tidally averaged theory.

In addition to tides and density gradients, wind also plays a significant role in influencing estuarine residual currents and stratification (Verspecht et al., 2009; Jongbloed et al., 2022). Burchard (2009) highlighted that upstream winds weaken stratification and reduce the magnitude of the ERV, whereas the downstream wind sheds the opposite effect. To quantify the destratification effect of upstream wind, Lange and Burchard (2019) introduced the Wedderburn number to analyze the relationship between upstream wind and density gradient. The wind is less inclined to affect the residual current with large Wedderburn numbers and may inhibit gravitational circulation, whereas the structure of ERV reverses with small Wedderburn numbers.

While the Eulerian mean method is commonly employed to study estuarine dynamics, there are certain terms within the momentum and mass transport equations that lack clear physical explanations (Ianniello, 1977; Feng et al., 1984). According to Lamb (1975), any flow field must adhere to the principle of mass conservation. In this regard, the Lagrangian residual velocity (LRV) is derived based on the fundamental nature of physical motion, ensuring material conservation and providing an accurate description of circulation in shallow seas (Feng, 1987; Jiang and Feng, 2014).

The influence of LRV in semi-closed estuaries and bays affected by tides has received attention from oceanographers (Deng et al., 2019; Jiang and Feng, 2011; Winant, 2008). Quan et al. (2014) employed a numerical model to investigate the impact of the ratio of tidal amplitude to water depth on LRV, and Jiang and Feng (2014) explored how the ratio of estuary length to wavelength affects LRV. Wang et al. (2010) examined the effects of wind, density gradient, and river runoff on LRV using a numerical model. However, this study aims to illustrate structural and magnitudinal variations of the total LRV under different factors, without delving into the underlying dynamic mechanisms. Liu et al. (2021) demonstrated that the influence of wind and density gradients on LRV is closely associated with the initial tidal phase based on the momentum equations, but the specific contribution of each dynamic component to LRV remains poorly studied.

Jiang and Feng (2014) explored the dynamical mechanisms for the LRV, which gives to the assumptions of a constant eddy viscosity and linear bottom friction in the entire estuarine. Subsequently, numerical models were utilized to study the contribution of tidal body force to LRV under a constant eddy viscosity, revealing that the Stokes' drift component plays a dominant role (Cui et al., 2019). Chen et al. (2020) analyzed the contribution of each dynamical term to the LRV and found the Stokes' drift component is the dominant component under the condition of the horizontal unvaried but depth-varying eddy viscosity. The above studies are all carried out under a temporally constant eddy viscosity. The impact of spatially varying eddy viscosity on LRV was examined in a narrow model, revealing that nonlinearity leads to a more complex LRV structure (Deng et al., 2017). However, these studies lack a quantitative analysis of the underlying dynamical mechanism. Sheng et al. (2022) demonstrated that the structure of LRV is primarily determined by the combined effects of the barotropic pressure gradient and tidal body force when only barotropic conditions are considered. Deng et al. (2022) further quantitatively analyzed the contributions of each driving force to LRV, considering both temporal and spatial variations in eddy viscosity under a constant density gradient. However,

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the roles of wind and stratification in LRV dynamics remain poorly studied.

The Pearl River, as the third largest river in China, encompasses a complex hydrodynamic environment. The Pearl River estuary (PRE) is a trumpet-like estuary characterized by two deep channels and shallow shoals. In recent years, researchers have increasingly focused on topics such as tidal currents, salinity intrusion, river plume dynamics, and residual current in the PRE (e.g., Gong et al., 2018; Pan et al., 2020; Wei et al., 2022). The estuary displays a typical two-layer circulation as observed in micro-tidal estuaries (Xue et al., 2001). Wang (2014) investigated the temporal and spatial variations of the ERV and analyzed its underlying dynamical mechanisms within the PRE. Lai et al. (2018) discussed the influence of tides and winds on the ERV and the associated dynamical processes using the Eulerian mean momentum equation. Additionally, the nonlinear advection term was identified as an important factor in the ERV within the PRE (Xu et al., 2021). While Chu et al. (2022) explored the hydrodynamic processes and connectivity of the circulation within the estuary from a Lagrangian tidally averaged perspective, a detailed dynamical analysis was not provided. Few studies have focused on the LRV within the PRE, especially regarding its underlying dynamical mechanisms.

Analytical solutions regarding the dynamics of LRV are constrained to a temporally constant eddy viscosity, while numerical solutions of LRV's dynamic components disregard the influence of stratification and wind. Consequently, the impact of wind and stratification on LRV dynamics remains enigmatic. Numerical solutions for LRV components are derived to grasp the modifications induced by wind and stratification within each LRV component, ultimately leading to changes in the overall LRV. Furthermore, wind and stratification influence turbulent mixing, subsequently affecting the LRV driven by the eddy viscosity term. Although scholars have extensively examined tidal straining effects on estuarine circulation via the Eulerian mean theory, the analysis of turbulent influences from the Lagrangian mean theory perspective yields distinctions from the Eulerian approach. To illuminate the mechanisms underlying the eddy viscosity component of LRV, we initiate by decomposing this component into four subcomponents. This study pursues two principal objectives: 1) to delve into the mechanisms by which wind and stratification modify LRV components, and 2) to investigate the roles of wind and stratification in the dominant contributor of the eddy viscosity component. This paper will provide valuable insights into the dynamic processes of longitudinal and lateral estuarine circulation based on Lagrangian mean theory under the influence of wind and stratification. These aspects have not been quantitatively assessed in previous studies. Additionally, the proposed decomposition theory of the eddy viscosity component offers a novel approach for analyzing the dominant mechanisms of turbulent components. This paper is structured as follows: Section 2 provides a delineation of model setup parameters, model validation, and LRV decomposition methods. Section 3 outlines the contribution of each component to the overall LRV and the contribution of each subcomponent to the total eddy viscosity component of LRV. The discussion and conclusions are presented in Section 4.

2. Theory and model description

2.1 The decomposition method

The LRV is decomposed into seven components, including the local acceleration component (u_{Lac} and v_{Lac}), horizontal nonlinear advection component (u_{Ladh} and v_{Ladh}), vertical nonlinear advection component (u_{Ladv} and v_{Ladv}), barotropic pressure gradient component (barotropic component; u_{Lba} and v_{Lba}), baroclinic pressure gradient component (baroclinic component; u_{Lgr} and v_{Lgr}), eddy viscosity component (u_{Ltu} and v_{Ltu}), and horizontal diffusion component (u_{Lho} and v_{Lho}). The detailed decomposition methods are shown in the appendix. Deng et al. (2022) considered a temporally constant density gradient but neglected the effects of periodic stratification and wind forcing. In this paper, one of the primary objectives is to quantify the effects of wind and stratification on the dynamics of the different components of

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LRV.

Wind and stratification play roles in turbulent mixing, which subsequently impacts the fluctuations of eddy viscosity over a tidal period. This influence extends to the eddy viscosity component of LRV. To clarify the mechanisms underlying this eddy viscosity component, we decompose it into four sub-components. We evaluate the distinct contributions of each sub-component to the total eddy viscosity component, aiming to delve into the dominant dynamic mechanisms, which is another objective of our paper. The study derives the following decomposition methods:

$$-\left\langle\frac{1}{D^2}\frac{\partial}{\partial\sigma}\left(v_h\frac{\partial u}{\partial\sigma}\right)\right\rangle/f=-\left\langle\frac{1}{D^2}\frac{\partial}{\partial\sigma}\left(v_{h0}\frac{\partial u_0}{\partial\sigma}\right)\right\rangle/f-\left\langle\frac{1}{D^2}\frac{\partial}{\partial\sigma}\left(v_{h0}\frac{\partial u_1}{\partial\sigma}\right)\right\rangle/f$$
$$-\left\langle\frac{1}{D^2}\frac{\partial}{\partial\sigma}\left(v_{h1}\frac{\partial u_0}{\partial\sigma}\right)\right\rangle/f-\left\langle\frac{1}{D^2}\frac{\partial}{\partial\sigma}\left(v_{h1}\frac{\partial u_1}{\partial\sigma}\right)\right\rangle/f, \tag{1}$$

$$\left\langle\frac{1}{D^2}\frac{\partial}{\partial\sigma}\left(v_h\frac{\partial v}{\partial\sigma}\right)\right\rangle/f=\left\langle\frac{1}{D^2}\frac{\partial}{\partial\sigma}\left(v_{h0}\frac{\partial v_0}{\partial\sigma}\right)\right\rangle/f+\left\langle\frac{1}{D^2}\frac{\partial}{\partial\sigma}\left(v_{h0}\frac{\partial v_1}{\partial\sigma}\right)\right\rangle/f+$$
$$\left\langle\frac{1}{D^2}\frac{\partial}{\partial\sigma}\left(v_{h1}\frac{\partial v_0}{\partial\sigma}\right)\right\rangle/f+\left\langle\frac{1}{D^2}\frac{\partial}{\partial\sigma}\left(v_{h1}\frac{\partial v_1}{\partial\sigma}\right)\right\rangle/f, \tag{2}$$

$$\text{and } u=u_0+u_1,\ v=v_0+v_1,\ v_h=v_{h0}+v_{h1}, \tag{3}$$

where <> represents the Lagrangian-averaged operator, u and v are horizontal tidal currents, v_h is the eddy viscosity, u_1 and v_1 are tidal average currents, u_0 and v_0 are tidal periodic oscillation tidal currents, v_{h0} is tidal average eddy viscosity, v_{h1} is tidal periodic oscillation eddy viscosity, D is time-varying depth, σ is sigma coordinate, and f is Coriolis parameter. The $-\langle\frac{1}{D^2}\frac{\partial}{\partial\sigma}\left(v_{h0}\frac{\partial u_0}{\partial\sigma}\right)\rangle/f$ and $\langle\frac{1}{D^2}\frac{\partial}{\partial\sigma}\left(v_{h0}\frac{\partial v_0}{\partial\sigma}\right)\rangle/f$ represent the coupled component of the tidal-average eddy viscosity and velocity gradient oscillation (v_{Lk0u0} and u_{Lk0u0}), the $-\langle\frac{1}{D^2}\frac{\partial}{\partial\sigma}\left(v_{h1}\frac{\partial u_0}{\partial\sigma}\right)\rangle/f$ and $\langle\frac{1}{D^2}\frac{\partial}{\partial\sigma}\left(v_{h1}\frac{\partial v_0}{\partial\sigma}\right)\rangle/f$ represent the tidal straining component (v_{Lk1u0} and u_{Lk1u0}), the $-\langle\frac{1}{D^2}\frac{\partial}{\partial\sigma}\left(v_{h0}\frac{\partial u_1}{\partial\sigma}\right)\rangle/f$ and $\langle\frac{1}{D^2}\frac{\partial}{\partial\sigma}\left(v_{h0}\frac{\partial v_1}{\partial\sigma}\right)\rangle/f$ represent the turbulent mean component (v_{Lk0u1} and u_{Lk0u1}), the $-\langle\frac{1}{D^2}\frac{\partial}{\partial\sigma}\left(v_{h1}\frac{\partial u_1}{\partial\sigma}\right)\rangle/f$ and $\langle\frac{1}{D^2}\frac{\partial}{\partial\sigma}\left(v_{h1}\frac{\partial v_1}{\partial\sigma}\right)\rangle/f$ represent the

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coupled component of eddy viscosity oscillation and the tidal-average velocity gradient (v_{Lk1u1} and u_{Lk1u1}).

2.2 Model configuration and experiments

This study employs the Finite Volume Coastal Ocean Model (FVCOM; Chen et al., 2006) to simulate the dynamic response of LRV to wind and stratification in the PRE. FVCOM is a three-dimensional primitive equation Community Ocean Model (Chen et al., 2003) that utilizes a finite-volume approach, accounting for a free-surface and employing prognostic techniques. The model consists of unstructured triangular cells and employs terrain-following vertical coordinates, allowing for a better fitness of the irregular coastline and complex topography present in the estuary.

The model domain, covering the PRE and adjacent coastal regions, is depicted in Fig. 1, spanning from 111.5°E to 116.5°E and 20°N to 23°N. The open boundary is situated in the northern South China Sea. Unidirectional grid nesting is implemented to enhance solution algorithms. The coarse grid consists of 8040 nodes and 15093 triangular elements. The spatial resolution of the horizontal grids varies across the entire region, ranging from 1 to 10 km. Specifically, a resolution of 1 km is employed within the PRE, 2.0−5.0 km off the Guangdong coast, and 10 km near the open boundary (Fig. 1a). On the other hand, the fine grid comprises 45368 nodes and 87179 triangular elements. The spatial resolution of the fine grids within the region also varies, ranging from 0.1 to 2.0 km. More specifically, a resolution of 0.1 km is utilized within the PRE, 0.1−1.0 km off the Guangdong coast, and 2.0 km close to the open boundary (Fig. 1b). In the vertical direction, the model employs fourteen uniformly assigned sigma levels.

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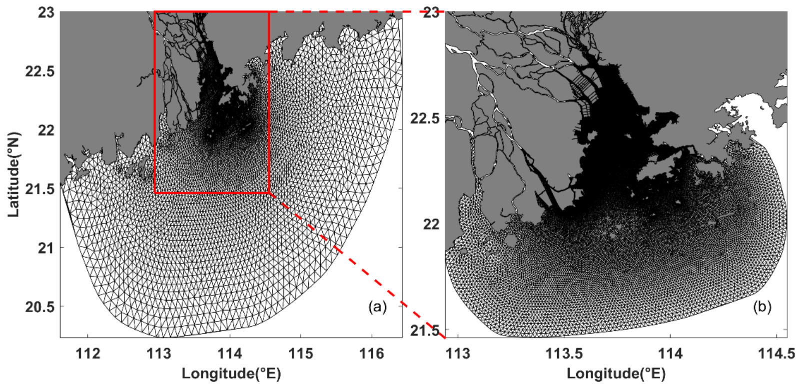

Figure 1. (a) Coarse mesh model, (b) fine mesh model.

The model incorporates eight major tidal constituents, namely M_2, N_2, S_2, K_2, K_1, O_1, P_1, and Q_1, as tidal driving forces at the open boundary. These constituents are obtained from the Oregon State University Tidal Prediction Software (OTPS). To initialize the model, salinity climatological data from the 1° World Ocean Atlas 2009 (WOA2009) dataset (https://accession.nodc.noaa.gov/0094866) is utilized. For wind forcing, monthly average wind data from the 0.25° CCMP dataset (http://www.remss.com/measurements/ccmp) is interpolated across the entire model domain. The lateral boundary incorporates monthly average river runoff data from eight river inlets, which are provided by the Water Conservancy Committee of the Pearl River under the Ministry of Water Resources. The topography data off the PRE is from the ETOPO2 dataset of NOAA, while the topography within the estuary is derived from electronic nautical chart data provided by the China Maritime Safety Administration.

The coarse grid model simulates a period from 1 January to 31 August 2017, and it reaches a quasi-steady state after one month. In this study, the outputs from the coarse grid model are utilized as the initial and boundary conditions for the fine grid model. The fine grid model, which begins in June, stabilizes after one month. The analysis focuses on the results from the fine grid model obtained on 24 July 2017 during spring tides and 2 August 2017 during neap tides. A split-mode time stepping method is employed with 2-second external and 10-second internal time steps for the coarse grid model, respectively. The fine grid model uses a 0.5-second external time step, which is half of the time step used in the coarse grid model. The bottom friction in the model is based on the quadratic bottom friction law, and the calculation of the eddy viscosity coefficient employs the Mellor-Yamada 2.5 order turbulent closure model.

To investigate the effects of wind and stratification on the dynamics of LRV, Case 1 (reference case) includes wind forcing and periodic stratification. Case 2 examines the influence of wind by removing wind forcing compared to Case 1. Case 3 explores the effects of stratification by imposing a uniformly constant salinity and temperature without considering river discharge compared to Case 2 (Table 1). The constant salinity and temperature, with values of 28 °C and 32 psu, respectively, are derived by averaging WOA2009 data for July and August across the whole domain.

Table 1. Numerical experiment scenarios

Experiments	Wind	Tide	Stratification
Case 1 (Reference case)	√	√	√
Case 2	×	√	√
Case 3	×	√	×

2.3 Model verification

The PRE is oriented in the north-south direction (Fig. 2). Accordingly, the positive *x*-axis, u, and u_L direct eastward; the positive *y*-axis, v, and v_L direct northward; and the positive *z*-axis, w, and w_L direct upward. In this context, u and v correspond to the cross-estuary and along-estuary velocities, respectively, with u_L and v_L denoting the corresponding LRV. The paper selects four sections, including three cross sections (Sections B–C) and one along-estuary section (Section A), which roughly cover the PRE (black lines in Fig. 2a). Section C is chosen to analyze the model results, and similar conclusions are drawn for the remaining three sections.

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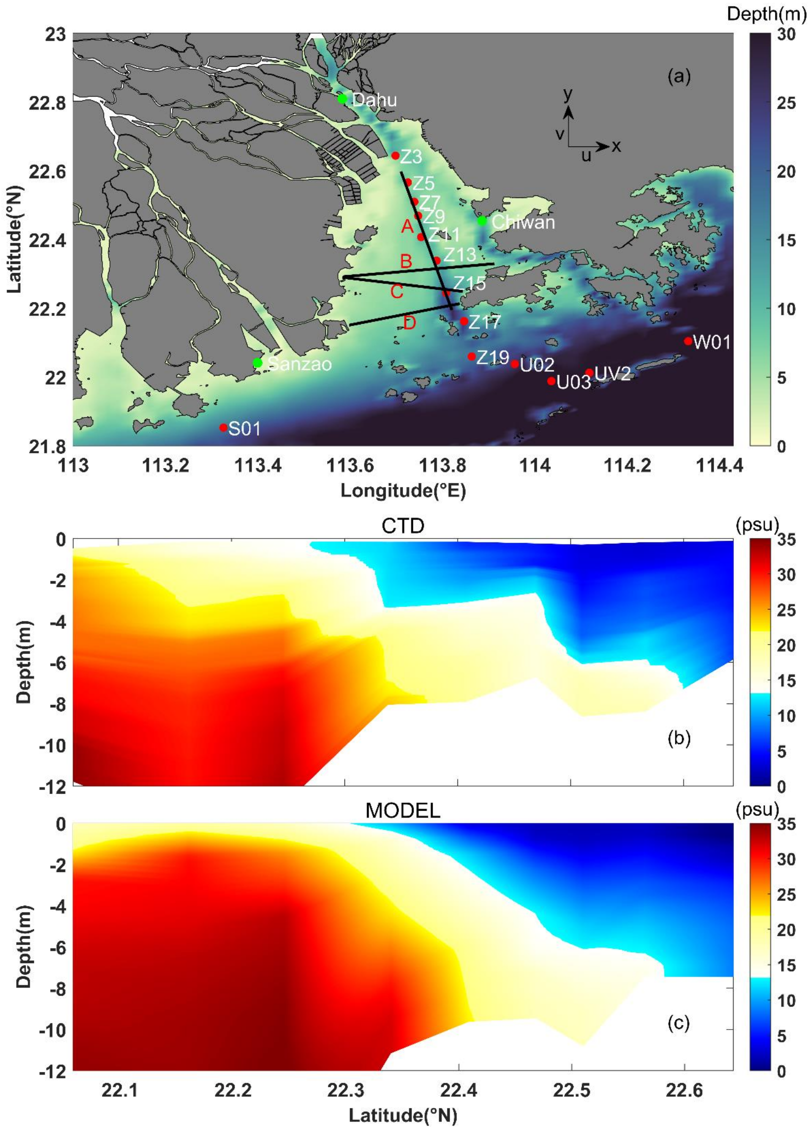

Figure 2. (a) Bathymetry of the model domain. Black lines mark sections for result analysis. Green dots indicate tide gauge stations for elevation validation, and red dots indicate CTD positions for salinity verification. (b) The along-estuary distributions of observed salinity interpolated from the CTD depth-profiled data in section C, and (c) the salinity obtained from the numerical model.

Model verification involves comparing the model-derived elevation and salinity with the corresponding observed values from the tide gauge and CTD stations, respectively (Fig. 3).

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The observed sea surface elevation data are collected between 2 and 4 August 2017, and the observed salinity data are acquired through CTD profiling from 4 to 6 August 2017. A good agreement between the model and observed values highlights the effectiveness of the model (Fig. 3). To further assess the model's performance, three statistical parameters are calculated: the correlation coefficient (CC), Willmott Skill score (Willmott, 1981), and Root Mean Square Error (RMSE). These parameters quantify the model's accuracy and skill:

$$CC = \frac{\sum_{i=1}^{N}(ob_i - \overline{ob})(mo_i - \overline{mo})}{\sqrt{\sum_{i=1}^{N}(ob_i - \overline{ob})^2 \sum_{i=1}^{N}(mo_i - \overline{mo})^2}}, \quad (4)$$

$$Skill = 1 - \frac{\sum_{i=1}^{N}(ob_i - mo_i)^2}{\sum_{i=1}^{N}(|mo_i - \overline{ob}| + |ob_i - \overline{ob}|)^2}, \quad (5)$$

$$\text{and } RMSE = \sqrt{\frac{1}{N}\sum_{i=1}^{N}(ob_i - mo_i)^2}, \quad (6)$$

where ob_i and mo_i are the observed data and model data, respectively, $\overline{ob}$ and $\overline{mo}$ are the average value of the observed data and the model data, and N represents the number of observations. The performance assessments of the modeled tidal elevation are presented in Figs. 3a–c. The model demonstrates a reasonable match with the observed tidal elevations, exhibiting good performance with a skill score greater than 0.98, a correlation coefficient exceeding 0.97, and a root mean square error less than 0.09 m. This indicates that the model performs well in simulating tidal elevations. The assessments of the model's performance in simulating salinity are depicted in Figs. 2b–c and Figs. 3d–l. The correlation coefficients for salinity are higher than 0.94, with the majority of skill scores exceeding 0.85 and root mean square errors less than 3 psu. The model exhibits well performance in simulating salinity.

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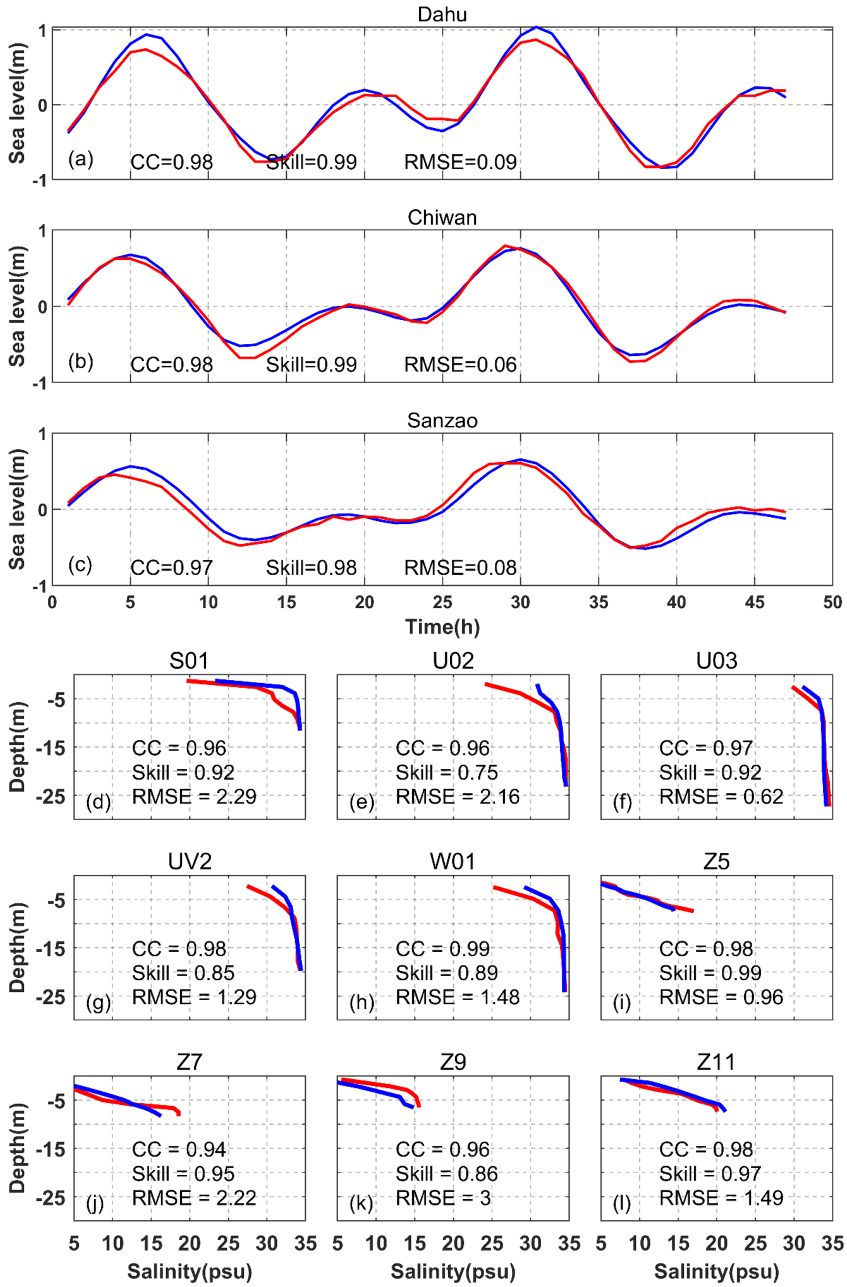

Figure 3. Comparisons between the observed (red line) and modeled (blue line) elevation and salinity. The three parameters including CC, Skill, and RMSE are calculated at each station.

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3. Results

3.1 Contributions of dominant components for LRV

To quantify the contribution of each dynamic component of the LRV, the absolute values of each component are averaged throughout Section C in this study, as follows:

$$M(\cdot) = \frac{1}{B}\int abs(\cdot)dB, \tag{7}$$

where *abs* are the absolute value function, the symbol · can be replaced by each dynamic component of the LRV, and *B* represents the area of the cross-section.

Figure 4 illustrates the decomposition of cross-estuary LRV into dominant contributions for the reference case. During neap tides, the eddy viscosity component (u_{Ltu}) exhibits a two-layer structure with eastward flow in the upper layer and westward flow in the lower layer (Fig. 4a). The barotropic pressure gradient component (u_{Lba}) generally flows westward in most areas of the shoal, while it displays an eastward flow in the upper layer and a westward flow in the lower layer of the deep channel (Fig. 4b). Conversely, the contribution from the baroclinic pressure gradient (u_{Lgr}) opposes u_{Lba} (Fig. 4c). During spring tides, the structure of the three components, namely u_{Ltu}, u_{Lba}, and u_{Lgr}, remains analogous to that during neap tides throughout the cross section (Figs. 4f−h). During both spring and neap tides, the three striking components (u_{Ltu}, u_{Lgr}, and u_{Lba}) are aggregated (Figs. 4e and j) and compared to the total LRV obtained directly from the model based on the Lagrangian particle tracking algorithms (Figs. 4d and i). It is observed that u_L primarily arises from an imbalance between u_{Ltu}, u_{Lgr}, and u_{Lba}. The eastward exchange circulation is predominantly attributed to u_{Ltu} in the upper layer of the shoal, while the westward flow in the lower layer of the shoal is primarily driven by u_{Ltu} and u_{Lba}. In the upper layer of the deep channel, the eastward flow is determined by the interplay of u_{Lba} and u_{Ltu}, which also induces the westward flow in the lower layer of the channel. Notably, u_{Lgr} predominantly counteracts u_{Lba}.

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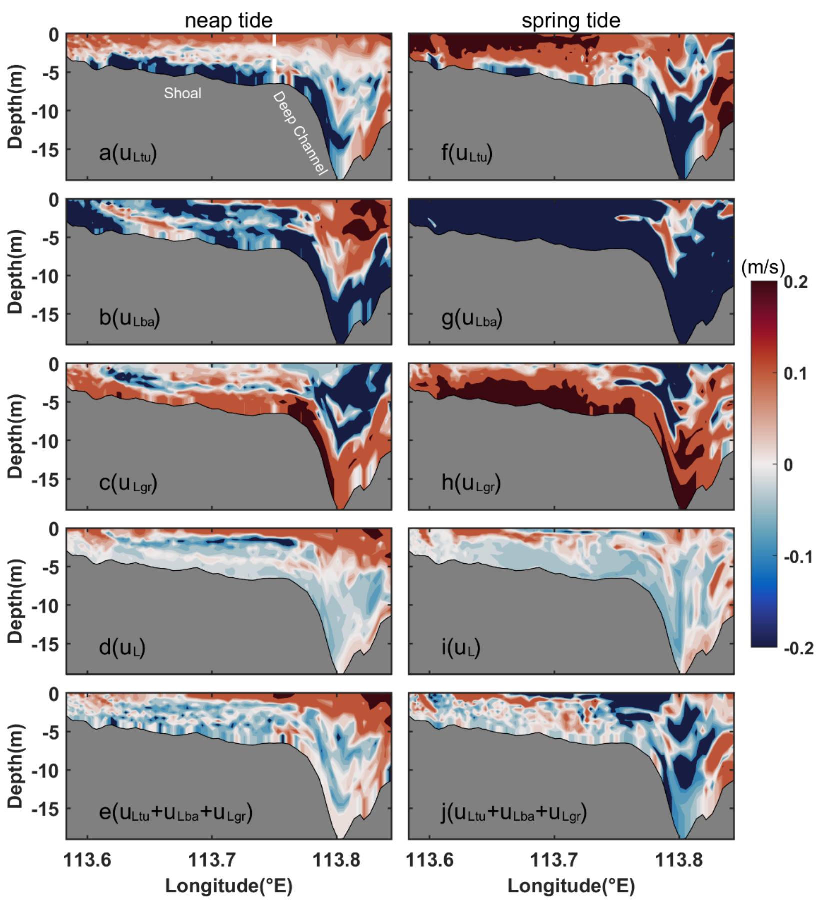

Figure 4. The structure of each dominant component of u_L in Section C for Case 1. (a) the eddy viscosity component, (b) the barotropic component, (c) the baroclinic component, (d) the total LRV directly obtained by the model, and (e) the sum of the eddy viscosity component, barotropic component, and baroclinic component during neap tides. The counterparts during spring tides are shown in the right column. Red shading represents eastward flow, and blue shading represents westward flow.

The intensities of the exchange flows are quantified in Table 2 for the reference case. During spring tides, the magnitude of u_{Ltu} is approximately 2 times higher than that during neap tides, the magnitude of u_{Lgr} nearly doubles compared to that during neap tides, and the magnitude of u_{Lba} is roughly 4 times as large as that during neap tides. Among the dominant components of u_L, u_{Lba} exhibits the most pronounced contributions, being 1−2 times as strong

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as u_{Ltu} and u_{Lgr}.

Table 2. The magnitude of each component of u_L *and* v_L

	Case 1 (neap)	Case 1 (spring)	Case 2 (neap)	Case 2 (spring)	Case 3 (neap)	Case 3 (spring)
$M(u_{Lba})$	0.12	0.43	0.15	0.42	0.04	0.17
$M(u_{Lgr})$	0.10	0.23	0.11	0.23	—	—
$M(u_{Ltu})$	0.09	0.23	0.07	0.20	0.03	0.16
$M(u_{Lac})$	0.09	0.13	0.09	0.14	0.02	0.09
$M(u_{Ladh})$	0.13	0.19	0.13	0.18	0.02	0.09
$M(u_{Ladv})$	0.08	0.11	0.09	0.11	0.0041	0.10
$M(u_{Lho})$	0.01	0.01	0.01	0.01	0.0007	0.0049
$M(v_{Lba})$	0.17	0.25	0.30	0.36	0.02	0.06
$M(v_{Lgr})$	0.15	0.22	0.25	0.28	—	—
$M(v_{Ltu})$	0.06	0.09	0.04	0.10	0.02	0.06
$M(v_{Lac})$	0.10	0.13	0.10	0.13	0.03	0.08
$M(v_{Ladh})$	0.12	0.14	0.12	0.14	0.03	0.08
$M(v_{Ladv})$	0.04	0.05	0.05	0.05	0.0006	0.0054
$M(v_{Lh0})$	0.01	0.01	0.01	0.01	0.0004	0.0023

The decomposition of along-estuary LRV into dominant contributions is depicted in Fig. 5 for the reference case. During neap tides, the barotropic pressure gradient component (v_{Lba}) contributes to an up-estuary flow in most areas of the shoal and a down-estuary flow in the deep channel (Fig. 5a); the baroclinic pressure gradient component (v_{Lgr}) exhibits a two-layer circulation with seaward flow in the upper layer and landward flow in the lower layer of the shoal along with inflow in most areas of the deep channel (Fig. 5b). It shows the opposite pattern to v_{Lba}. During spring tides, there is a down-estuary flow of v_{Lba} in the shoal, which is contrary to the flow pattern during neap tides (Fig. 5e). Additionally, the outflow area of v_{Lgr}

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in the upper layer of the shoal is smaller during spring tides than during neap tides (Fig. 5f). Both during spring and neap tides, the sum of v_{Lba} and v_{Lgr} (Figs. 5d and h) closely resembles the total along-estuary LRV (v_L) (Figs. 5c and g). Therefore, the dominant components of v_L are v_{Lba} and v_{Lgr}. Since these components must balance across the estuary, the outflow in the upper layer is mainly determined by v_{Lba}, while the inflow in the lower layer is induced by v_{Lgr}. During spring tides, the magnitudes of v_{Lba} and v_{Lgr} are 1.4 times as large as those during neap tides (Table 2). The contributions from gravitational circulation and barotropic pressure gradient component to total LRV are of the same magnitude.

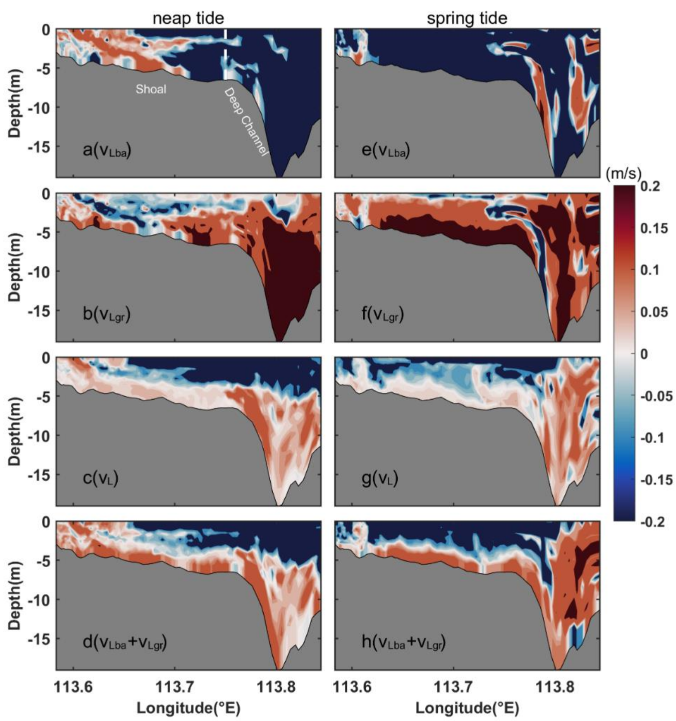

Figure 5. The structure of each dominant component of v_L in Section C for Case 1. (a) barotropic pressure gradient component, (b) baroclinic pressure gradient component, (c) the total LRV obtained directly by the model, and (d) the sum of barotropic and baroclinic pressure gradient components during neap tides. The counterparts during spring tides are shown in the right column. Red shading represents inflow to the estuary, and blue shading represents outflow to the sea.

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Neglecting the influence of wind, the cross-estuary dominant components are displayed in Fig. 6 for Case 2. The eddy viscosity component (u_{Ltu}) exhibits a similar pattern to the reference case both during neap and spring tides (Figs. 6a and f). However, during neap tides, the magnitude of the eastward flow of u_{Ltu} in the upper 2 m is approximately one order of magnitude smaller than that in Case 1 (Fig. 6a vs. Fig. 4a), although the absolute value of u_{Ltu} averaged in Section C for Case 2 is slightly different compared to that in Case 1 (Table 2). This suggests that wind primarily affects the upper exchange circulation by influencing the mixing of the upper water column. During spring tides, u_{Ltu} shows small differences in magnitude between Case 1 and Case 2 (Fig. 6f vs. Fig. 4f), indicating that wind sheds a slight influence on exchange flow during spring tides. During both spring and neap tides, the structures and magnitudes of the barotropic pressure gradient component (u_{Lba}) and the baroclinic pressure gradient component (u_{Lgr}) are similar to that in Case 1. When wind effects are not considered, the structure of the cross-estuary LRV (u_L) (Figs. 6d and i) is still determined by the combined contributions of u_{Lba}, u_{Lgr}, and u_{Ltu} (Figs. 6e and j). However, the eastward flow determined by u_{Ltu} in the upper layer of the shoal in Case 1 transforms into a westward flow primarily driven by u_{Lba} in Case 2.

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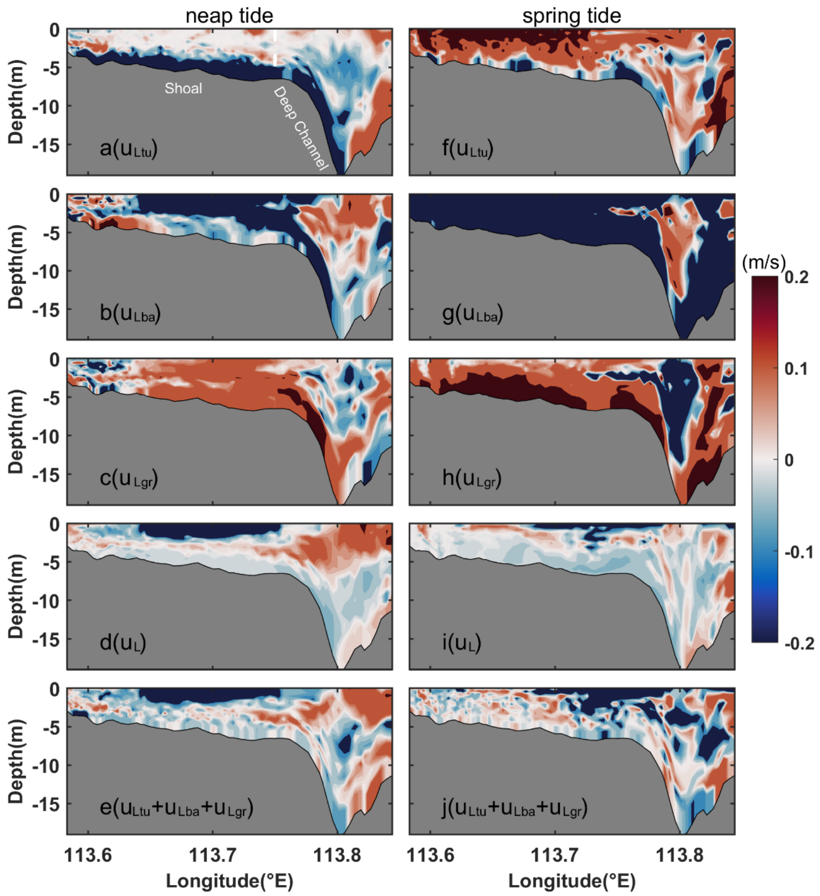

Figure 6. Same as Figure 4, but for Case 2 without wind forcing.

The along-estuary dominant components in Case 2 are shown in Fig. 7. The v_{Lba} changes from inflow in Case 1 to outflow in the shoal during neap tides (Fig. 7a). Similarly, v_{Lgr} shifts from outflow in Case 1 to inflow in the upper layer of the shoal during neap tides in Case 2 (Fig. 7b). This suggests that wind plays a crucial role in the components of LRV in the upper water column of the shoal. During spring tides, v_{Lba} and v_{Lgr} maintain the same structure as observed in Case 1 (Figs. 7e and f), indicating that wind is unimportant during spring tides. The structure of the along-estuary LRV (v_L) (Figs. 7c and g) is primarily determined by the combined contributions of v_{Lba} and v_{Lgr} (Figs. 7d and h), analogous to that in Case 1. But in the

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absence of wind, the magnitudes of v_{Lba} and v_{Lgr} are larger than those in Case 1, indicating that southwesterly wind suppresses gravitational circulation. The relative contributions of v_{Lba} and v_{Lgr} to v_L are approximately equal (Table 2).

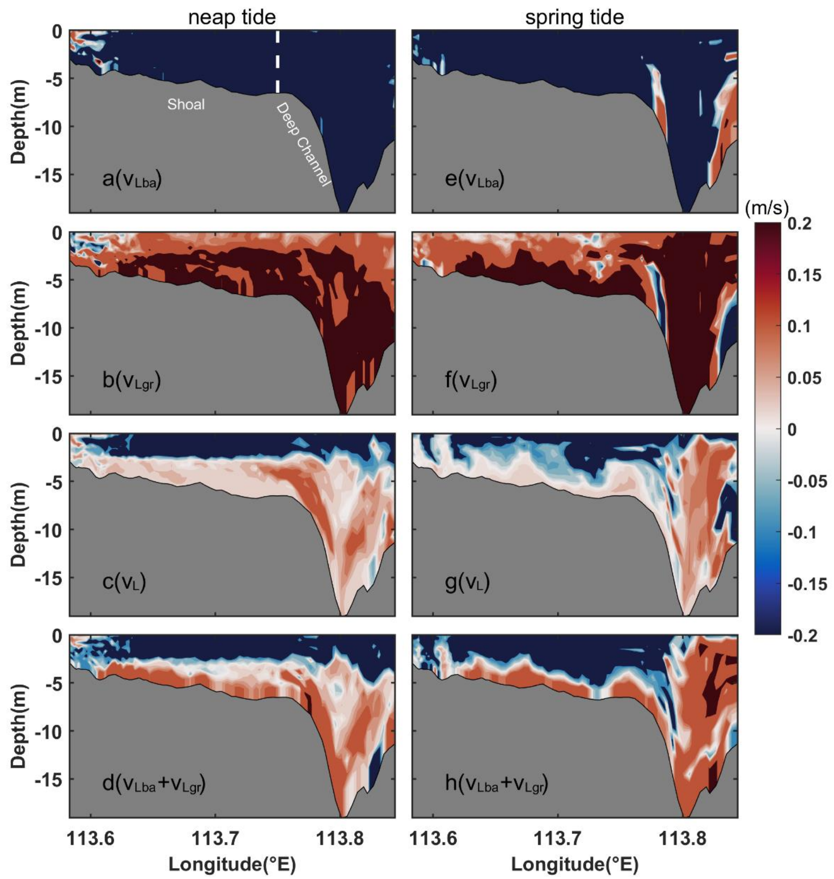

Figure 7. Same as Figure 5, but for Case 2 without wind forcing.

The stratification and wind forcing are ignored in Case 3. The dominant components of the cross-estuary LRV in Section C are shown in Fig. 8. During neap tides, the local acceleration component (u_{Lac}) predominantly exhibits eastward flow in most areas, with minor regions showing westward flow in the shoal and deep channel (Fig. 8a). Conversely, during spring tides, a prevailing westward flow characterizes the majority of the shoal regions, while

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an eastward flow prevails in the deep channel (Fig. 8g). These results highlight the significant impact of tides on the structure of u_{Lac} in a homogeneous water column. Comparing the results with those of Case 2, u_{Lac} undergoes a transition from vertically sheared flow in Case 2 to horizontally sheared flow in Case 3, indicating that stratification plays a notable role in shaping the structure of u_{Lac}. The horizontal nonlinear advective component (u_{Ladh}) exhibits a flow pattern that is the reverse of u_{Lac} (Figs. 8b and h). The barotropic pressure gradient component (u_{Lba}) primarily shows unidirectional westward flow throughout the cross section (Figs. 8c and i). The pattern of u_{Lba} in the shoal and most of the lower layer of the deep channel is consistent with that observed in Case 2. However, in the upper layer of the deep channel, u_{Lba} transforms eastward flow in Case 2 into westward flow in Case 3. The eddy viscosity component (u_{Ltu}) induces a flow opposite to that of u_{Lba} (Figs. 8d and j), which differs from the vertically sheared flow observed in Case 2.

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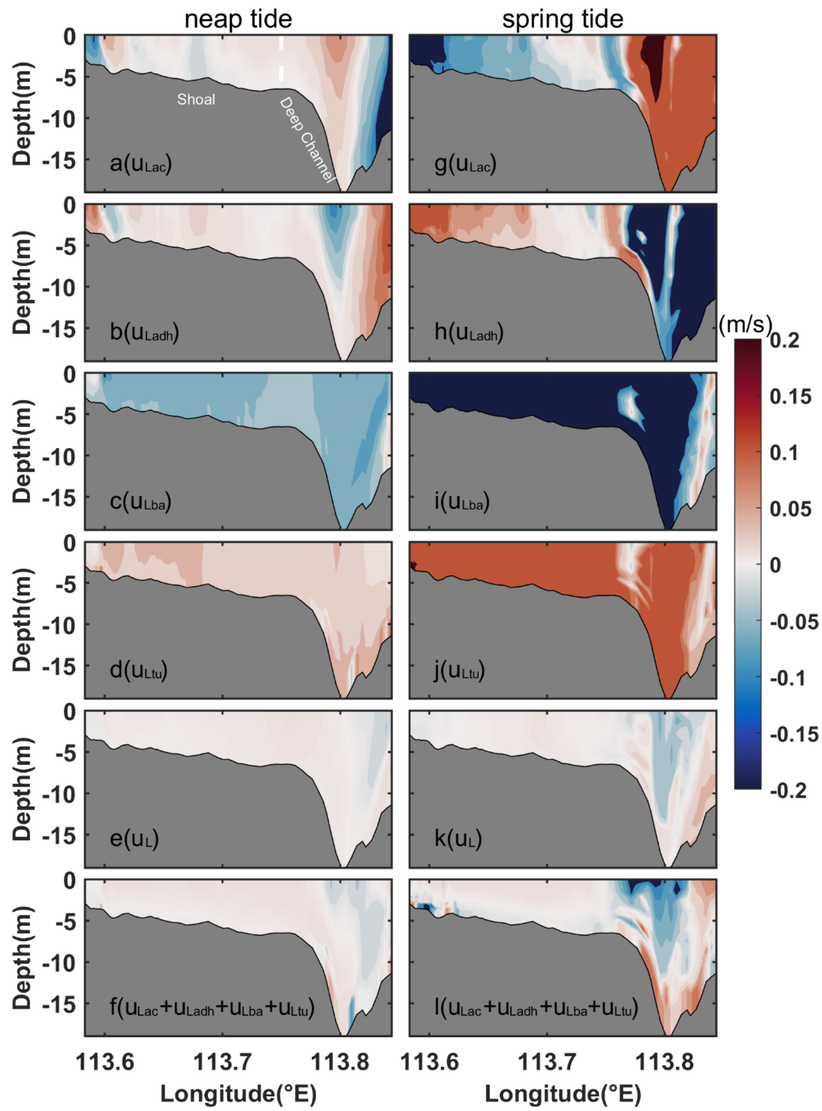

Figure 8. The structure of each dominant component of u_L in Section C for Case 3. (a) local acceleration component, (b) horizontal nonlinear advection component, (c) barotropic pressure gradient component, (d) eddy viscosity component, (c) the total LRV obtained directly by the model, and (f) sum of local acceleration component, horizontal nonlinear advection component, barotropic pressure gradient component, and eddy viscosity component during neap tides. The counterparts during spring tides are shown in the right column. Red shading represents eastward flow and blue shading represents westward flow.

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The structure of the cross-estuary LRV (u_L) (Figs. 8e and k) closely resembles the structure of the sum of the four components: u_{Lac}, u_{Ladh}, u_{Lba}, and u_{Ltu} in Case 3 (Figs. 8f and l). This indicates that the overall structure of u_L (Figs. 8e and k) is primarily determined by the combined effects of these four components. Among them, the eastward flow in the shoal and the lower layer of the deep channel is mainly determined by u_{Ltu} (Figs. 8d and j), with u_{Lac} playing a secondary role (Figs. 8a and g). On the other hand, the westward flow in the upper layer of the deep channel is primarily influenced by u_{Lba} (Figs. 8c and i), with u_{Ladh} contributing as a secondary component (Figs. 8b and h).

The magnitudes of u_{Lac}, u_{Ladh}, and u_{Lba} during spring tides are approximately four times as large as those during neap tides in Case 3 (Table 2). The magnitude of u_{Ltu} during spring tides is 4.8-fold compared to neap tides. The relative contributions of u_{Lba} and u_{Ltu} to u_L are roughly equal, and u_{Lac} and u_{Ladh} have similar contributions. Moreover, the contribution of u_{Lba} is approximately 1−2 times as large as that of u_{Lac}.

Both during spring and neap tides, the along-estuary barotropic pressure gradient component (v_{Lba}) exhibits outflow in most areas in Case 3 (Figs. 9a and 9e), which is similar to Case 2, indicating that stratification has minimal effects on the structure of v_{Lba}. The eddy viscosity component (v_{Ltu}) shows a nearly opposite pattern compared to v_{Lba} (Figs. 9b and f). Compared to Case 2, the pattern of v_{Ltu} exhibits significant changes at the bottom of the shoal and in the deep channel. The imbalance between the two components, v_{Lba} and v_{Ltu} (Figs. 9d and h), determines the along-estuary circulation (v_L) (Figs. 9c and g). The inflow in the shoal is primarily driven by v_{Ltu}, while the outflow in the deep channel is dominated by v_{Lba}. During spring tides, the magnitudes of v_{Lba} and v_{Ltu} are about 4-fold that during neap tides (Table 2). During neap and spring tides, the relative contributions of v_{Lba} and v_{Ltu} to v_L are equal.

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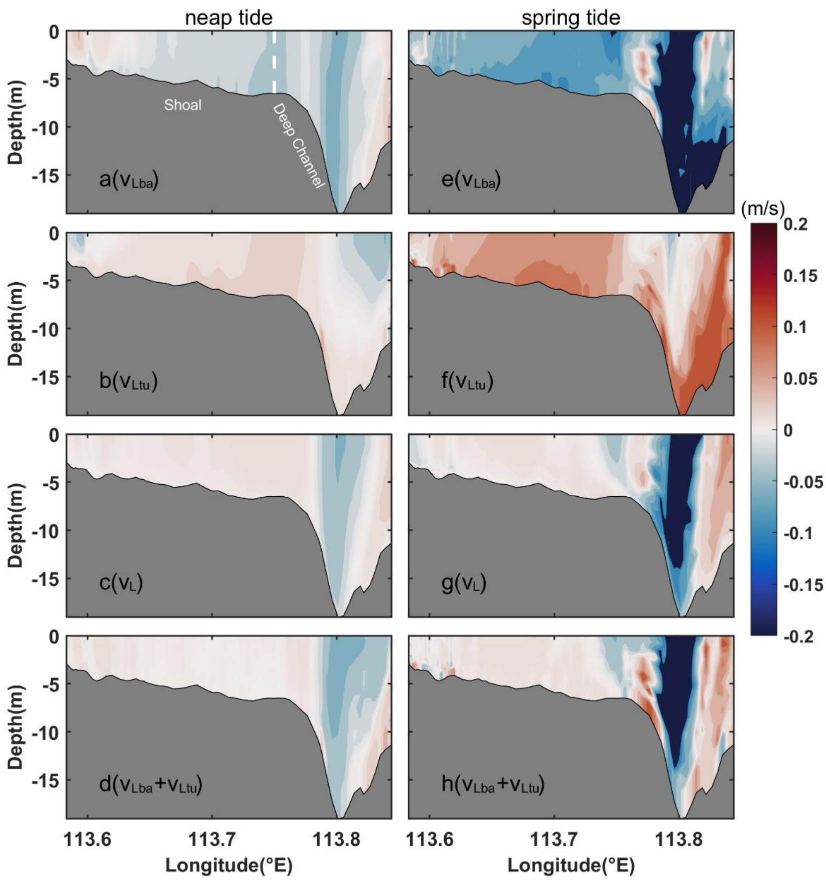

Figure 9. The structure of each dominant component of v_L in Section C for Case 3. (a) the barotropic pressure gradient component, (b) the eddy viscosity component, (c) the total LRV obtained directly by the model, and (d) the sum of barotropic pressure gradient component and eddy viscosity component. The counterparts during spring tides are shown in the right column. Red shading represents inflow to the estuary, and blue shading represents outflow to the sea.

3.2 Contributions of Non-dominant Components for LRV

The analysis of the contributions from non-dominant components to LRV for Case 1 is depicted in Fig. 10. During neap tides, the local acceleration (u_{Lac}) induces eastward flow in the majority of the upper layer and westward flow in the lower layer (Fig. 10a). Conversely,

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the horizontal nonlinear advection component (u_{Ladh}) exhibits an opposite pattern to u_{Lac} across most regions (Fig. 10b). Meanwhile, the vertical nonlinear advective component (u_{Ladv}) serves as a sandwiched structure, characterized by vertically staggered eastward and westward flow (Fig. 10c). The combined configuration of u_{Lac} and u_{Ladh} contrasts with that of u_{Ladv}, yielding a relatively small and negative contribution from the sum of these three components to u_L. Consequently, the three components are denoted as non-dominant components. The magnitudes of the non-dominant components of u_L during spring tides are slightly larger than those during neap tides. The general patterns of these three components during spring tides closely resemble those during neap tides (Figs. 10e−g). Moreover, both during spring and neap tides, the horizontal diffusion component (u_{Lho}) is smaller compared to the other components (Figs. 10d and h), and its contribution is negligible.

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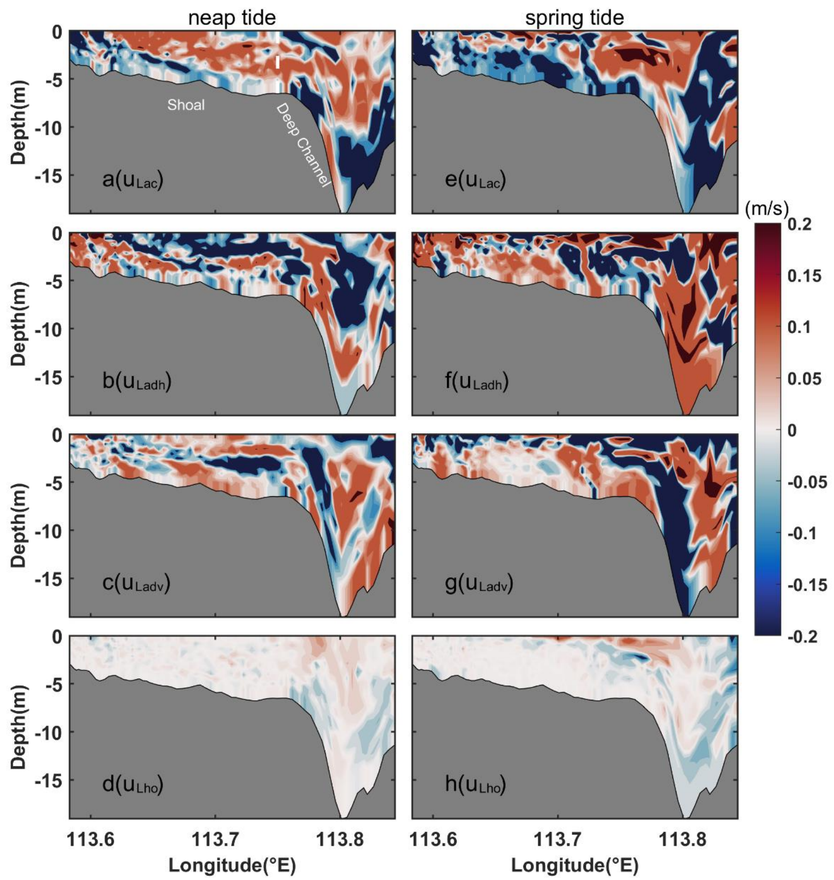

Figure 10. Vertical section of each non-dominant component of u_L in Section C for Case 1. (a) local acceleration component, (b) horizontal nonlinear advection component, (c) vertical nonlinear advection component, and (d) horizontal diffusion component during neap tides. The counterparts during spring tides are shown in the right column. Red shading represents eastward flow and blue shading represents westward flow.

During neap tides, the local acceleration component (v_{Lac}) exhibits a three-layer structure in the shoal, with inflow in the upper and lower layer and outflow in the middle layer. In the deep channel, unidirectional outflow prevails (Fig. 11a). The pattern of the horizontal nonlinear advective component (v_{Ladh}) is nearly the reverse of v_{Lac} (Fig. 11b). The vertical nonlinear term (v_{Ladv}) results in down-estuary flow in the upper and lower layer while up-estuary flow

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dominates in the middle layers (Fig. 11c). The combination of three components contributes to total LRV less and negatively. Additionally, the eddy viscosity-induced flow (v_{Ltu}) during neap tides exhibits a vertical shear structure, with outflow in the upper and lower layer and inflow in the middle layer (Fig. 11d). During spring tides, the overall structures for each non-dominant component resemble those during neap tides; however, the magnitudes during spring tides exceed those recorded during neap tides (Figs. 11g–j). For both spring and neap tides, the contributions of the horizontal diffusion components (v_{Lho}) are negligible (Figs. 11e and k; Table 2). Moreover, the contribution of v_{Ltu} is relatively smaller compared to their respective dominant components (Table 2). In the absence of wind effects, the structure and contribution of each non-dominant component of the cross-estuary LRV (u_L) in Case 2 closely resemble those observed in Case 1 during both spring and neap tides (not shown), with the exception of the noticeably reduced along-estuary eddy viscosity component (v_{Ltu}) in the upper layer in Case 2 during neap tides (Fig. 11f) and slightly intensified v_{Ltu} during spring tides (Fig. 11i). These indicate that wind has a weak influence on the non-dominant components of cross-estuary circulation. However, wind significantly affects the non-dominant component v_{Ltu} of the along-estuary circulation in the upper layer.

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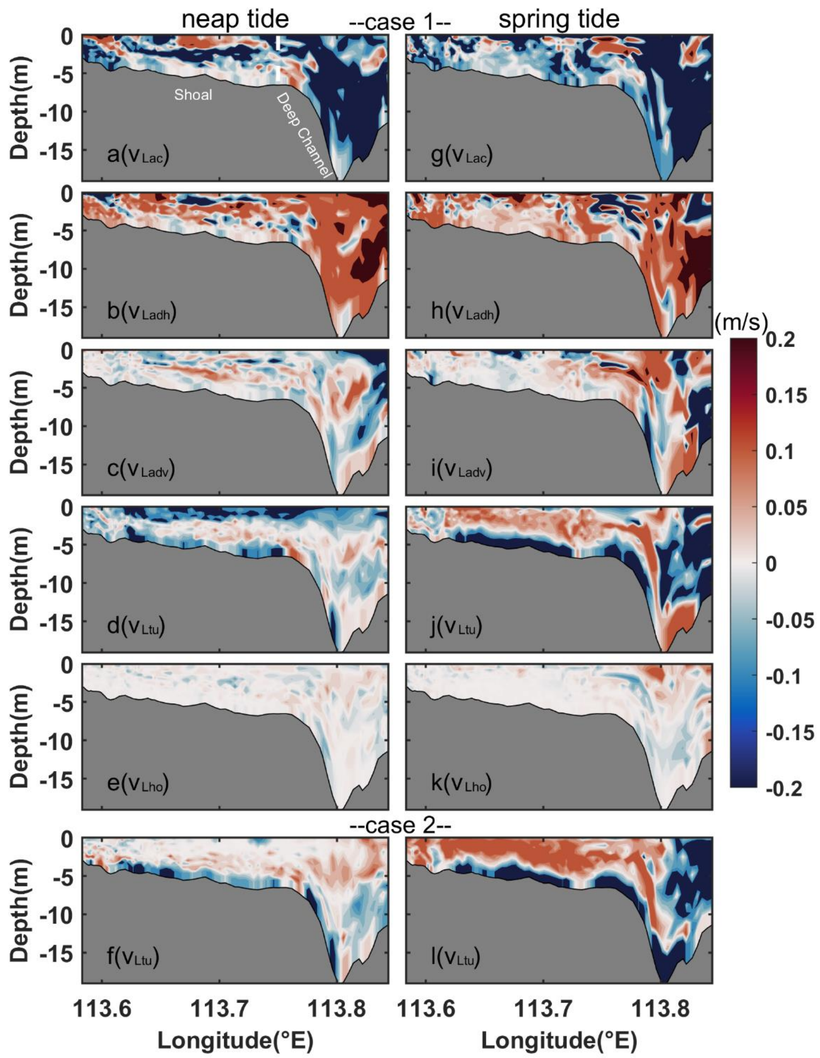

Figure 11. Vertical section of each non-dominant component of v_L in Section C for Case 1 (a–e; g–k) and Case 2 (f and l). (a) local acceleration component, (b) horizontal nonlinear advection component, (c) vertical nonlinear advection component, (d) eddy viscosity component, and (e) horizontal diffusion component during neap tides for Case 1. (f) eddy viscosity component during neap tides for Case 2. The counterparts during spring tides are shown in the right column. Red shading represents inflow, and blue shading represents outflow.

Neglecting wind forcing and stratification, the magnitudes of the vertical nonlinear

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advection component (u_{Ladv}) and horizontal diffusion component (u_{Lho}) are relatively low during both spring and neap tides. Compared to Case 2, the magnitude of u_{Lho} (Figs. 12b and h) in Case 3 is reduced by half during spring tides and by a factor of 14 during neap tides, while the magnitude of u_{Ladv} (Figs. 12a and g) in Case 3 experiences a tenfold reduction during spring tides and a twentyfold reduction during neap tides (Table 2). For both neap and spring tides, v_{Lac} shifts from inflow in Case 2 to outflow in Case 3 in some areas of the shoal (Figs. 12c and i). The horizontal nonlinear advection component (v_{Ladh}) in Case 3 exhibits a pattern opposite to that of v_{Lac} (Figs. 12d and j). Their combined contributions of these two components to total LRV can be disregarded. The contributions from the vertical nonlinear advection component (v_{Ladv}) and horizontal diffusion component (v_{Lho}) during spring and neap tides remain relatively low in Case 3 (Figs. 12e, k, f, and l). The magnitude of v_{Lho} in Case 3 is fivefold smaller during spring tides and 25 times smaller during neap tides than those in Case 2, while the magnitude of v_{Ladv} in Case 3 experiences an approximately tenfold reduction during spring tides and an eightyfold reduction during neap tides compared to Case 2 (Table 2).

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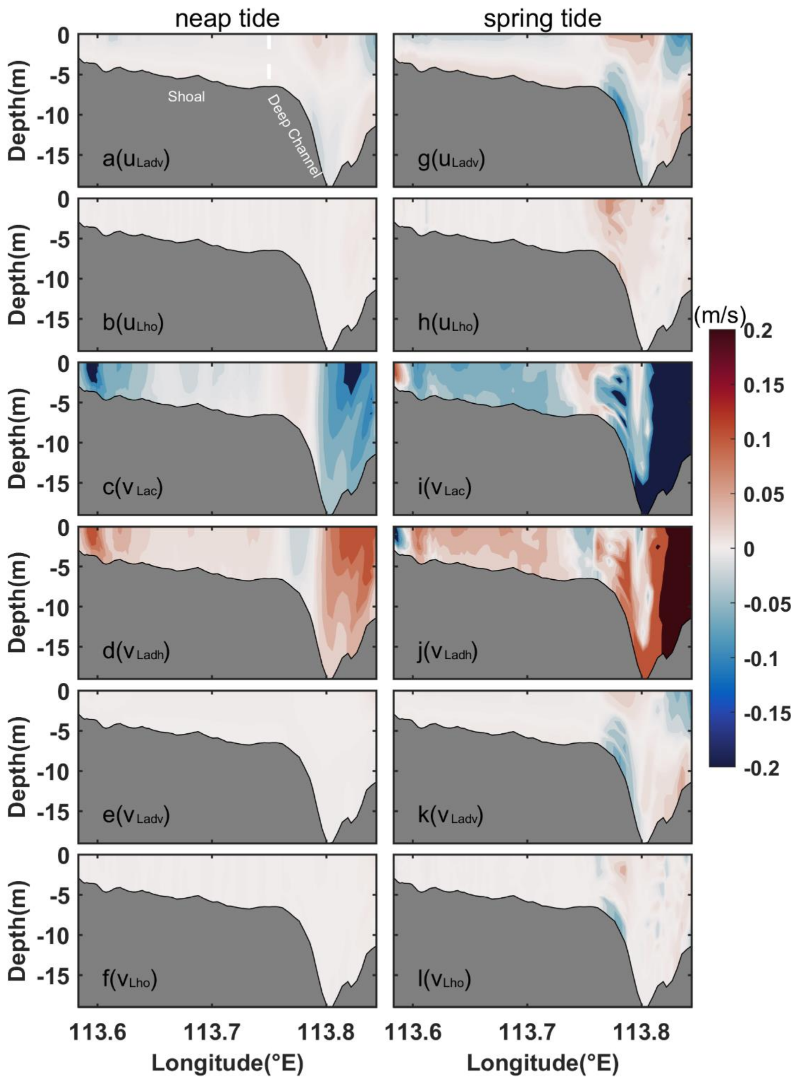

Figure 12. The vertical distribution of each non-dominant component of u_L and v_L in Section C for Case 3. (a) cross-estuary vertical nonlinear advection component, (b) cross-estuary horizontal diffusion component, (c) along-estuary local acceleration component, (d) along-estuary horizontal advection component, (e) along-estuary vertical advection component, and (f) along-estuary horizontal diffusion during neap tides. Red shading in (a) and (b) indicates eastward flow and blue shading indicates westward flow. Red shading area in (c)−(f) represents inflow, and the blue shading area represents outflow. The counterparts during spring tides are shown in the right column.

3.3 Contributions of dominant components for the eddy viscosity component

Through an analysis of dominant mechanisms influencing LRV under various dynamic factors, the results reveal that the cross-estuary eddy viscosity component significantly shapes the structure of cross-estuary LRV due to the prevailing southwesterly wind during the summer in the PRE. However, the along-estuary eddy viscosity component is not the predominant contributor to along-estuary LRV under stratified circumstances. In the case of destratification, both the along-estuary and cross-estuary eddy viscosity components play roles in shaping the total LRV. A comprehensive exploration of the dominant mechanisms of the eddy viscosity component entails further decompositions of both the along-estuary and cross-estuary eddy viscosity components into four subgroups. This analysis provides general conclusions and implications for future studies. These subgroups encompass the coupled component of tidal-averaged eddy viscosity and velocity gradient oscillation, the tidal straining component, the turbulent mean component, and the coupled component of tidal-averaged velocity gradient and eddy viscosity oscillation.

During neap tides, the cross-estuary turbulent mean component (u_{Lk0u1}) for Case 1 displays eastward flows in the upper layer and westward flows in the lower layer (Fig. 13g). During spring tides, u_{Lk0u1} closely resembles the pattern observed during neap tides (Fig. 13h). The structure of u_{Lk0u1} during neap and spring tides is identical to that of the eddy viscosity (u_{Ltu}) (Figs. 13a and b). Therefore, u_{Ltu} is predominantly influenced by u_{Lk0u1}. During neap tides, the along-estuary turbulent mean component (v_{Lk0u1}) for Case 1 exhibits a three-layer structure in the shoal, with outflow occurring in the surface and bottom layers, and inflow in the middle layer (Fig. 13i). In the deep channel, there is a two-layer flow pattern with outflow in the upper layer and inflow in the lower layer. This structure aligns with that of the eddy viscosity component (v_{Ltu}) (Fig. 13c). Hence, during neap tides, v_{Ltu} is primarily influenced by v_{Lk0u1}. During spring tides, the structure of v_{Ltu} for Case 1 (Fig. 13d) is contributed by the combined

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effect of the four components: v_{Lk0u0}, v_{Lk0u1}, v_{Lk1u0}, and v_{Lk1u1} (Fig. 13j), which differs from the structure observed during neap tides. The inflow occurring in the upper layer of the shoal is primarily determined by v_{Lk0u0} and v_{Lk1u0} (Figs. 13e and f), and the outflow in the lower layer of the shoal is mainly influenced by v_{Lk0u1} (Fig. 13k). The structure in the deep channel is primarily determined by v_{Lk0u1}.

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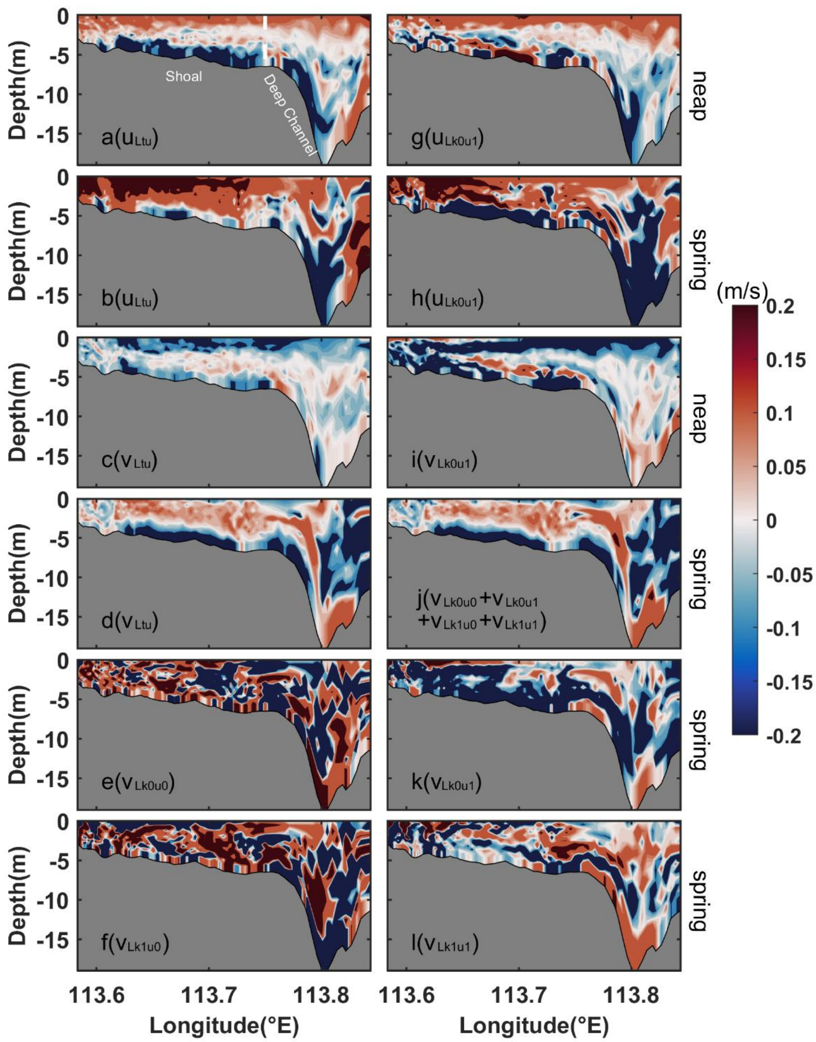

Figure 13. Vertical section of cross-estuary (u_{Ltu}) and along-estuary (v_{Ltu}) eddy viscosity and the corresponding dominant components in Section C for Case 1.The u_{Ltu} during (a) neap tides and (b) spring tides, and (g) and (h) the corresponding dominant components of turbulent mean component (u_{Lk0u1}). The v_{Ltu} during (c) neap tides and (d) during spring tides, (i) the corresponding dominant components of turbulent mean component (v_{Lk0u1}), and (j) the sum of four dominant components (e, f, k, and g). The red shading represents eastward flow, and the blue shading represents westward flow for the cross-estuary components. For the along-estuary components, the red shading indicates inflow and the blue shading indicates outflow.

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During neap tides, the cross-estuary turbulent mean component (u_{Lk0u1}) for Case 2 exhibits eastward flow in the upper layer and westward flow in the lower layer (Fig. 14b). This pattern aligns with Case 1. However, the magnitude of the eastward flow in the upper layer of u_{Lk0u1} during neap tides is one order of magnitude smaller than that observed in Case 1. During spring tides, the structure and magnitude of u_{Lk0u1} for Case 2 are similar to those of Case 1 (Fig. 14j), suggesting a weak influence of wind on u_{Lk0u1}. Similar to Case 1, both during neap and spring tides, the cross-estuary eddy viscosity component (u_{Ltu}) (Figs. 14a and i) is predominantly determined by u_{Lk0u1} (Figs. 14b and j). During neap tides, the along-estuary turbulent mean component (v_{Lk0u1}) for Case 2 exhibits inflow in the upper layer and outflow in the lower layer (Fig. 14d). The structure of v_{Lk0u1} in the lower layer is consistent with that in Case 1, while the structure in the upper layer is opposite to that of Case 1. Without the influence of wind, the structure of v_{Lk0u1} in the upper layer shifts from outflow in Case 1 to inflow. During spring tides, the area and magnitude of inflow in the upper layer of v_{Lk0u1} for Case 2 are larger than those during neap tides (Fig. 14l). Both during neap and spring tides, the along-estuary eddy viscosity component (v_{Ltu}) (Figs. 14c and k) exhibits the same structure as v_{Lk0u1} (Figs. 14d and l). Hence, v_{Ltu} is predominantly influenced by the turbulent mean component (v_{Lk0u1}).

Without consideration of stratification, the cross-estuary tidal straining component (u_{Lk1u0}) for Case 3 exhibits eastward flow (Fig. 14f) in the shoal during neap tides. The u_{Lk1u0} undergoes a transition from westward flow in Case 2 to eastward flow in the lower layer. During spring tides, the u_{Lk1u0} for Case 3 maintains the same pattern as observed during neap tides, and its magnitude is greater than that during neap tides (Fig. 14n). During neap tides, the along-estuary tidal straining component (v_{Lk1u0}) for Case 3 exhibits inflow in most areas of the shoal, and shows a two-layer structure in the deep channel with outflow in the upper layer, and inflow in the lower layer (Fig. 14h), which is analogous to the structure of v_{Lk1u0} in the shoal in Case 2. Stratification mainly affects the structure of v_{Lk1u0} in the lower layer of the deep channel. During

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spring tides, the inflow area of v_{Lk1u0} for Case 3 in the deep channel is larger than that during neap tides (Fig. 14p). During both neap and spring tides, the u_{Ltu} and v_{Ltu} (Figs. 14e, g, m, and o) align with u_{Lk1u0} and v_{Lk1u0} (Figs. 14f, h, n, and p), respectively. Hence, u_{Ltu} and v_{Ltu} are primarily influenced by u_{Lk1u0} and v_{Lk1u0}, differing from the dominant components in Case 2. Without consideration of stratification, the dominant components of u_{Ltu} and v_{Ltu} shift from the turbulent mean components (u_{Lk0u1} and v_{Lk0u1}) in Case 2 to the tidal straining components (u_{Lk1u0} and v_{Lk1u0}) in Case 3. During neap tides, the magnitude of u_{Lk1u0} is approximately 5 times smaller than that in Case 2, while the magnitude of v_{Lk1u0} is around 14 times smaller than that in Case 2 (Table 3). During spring tides, the magnitude of u_{Lk1u0} is roughly 4 times smaller than that in Case 2, and the magnitude of v_{Lk1u0} is approximately 6 times smaller than that in Case 2.

Table 3. The contribution of each component to the total eddy viscosity component in three scenarios.

	Case 1 (neap)	Case 1 (spring)	Case 2 (neap)	Case 2 (spring)	Case 3 (neap)	Case 3 (spring)
$M(u_{Lk0u0})$	0.16	0.42	0.14	0.42	0.001	0.068
$M(u_{Lk0u1})$	0.11	0.27	0.07	0.20	0.006	0.010
$M(u_{Lk1u0})$	0.16	0.46	0.14	0.43	0.031	0.103
$M(u_{Lk1u1})$	0.08	0.17	0.04	0.16	0.001	0.003
$M(v_{Lk0u0})$	0.15	0.30	0.11	0.28	0.005	0.023
$M(v_{Lk0u1})$	0.11	0.19	0.07	0.15	0.011	0.032
$M(v_{Lk1u0})$	0.16	0.37	0.11	0.28	0.008	0.044
$M(v_{Lk1u1})$	0.11	0.20	0.05	0.13	0.001	0.004

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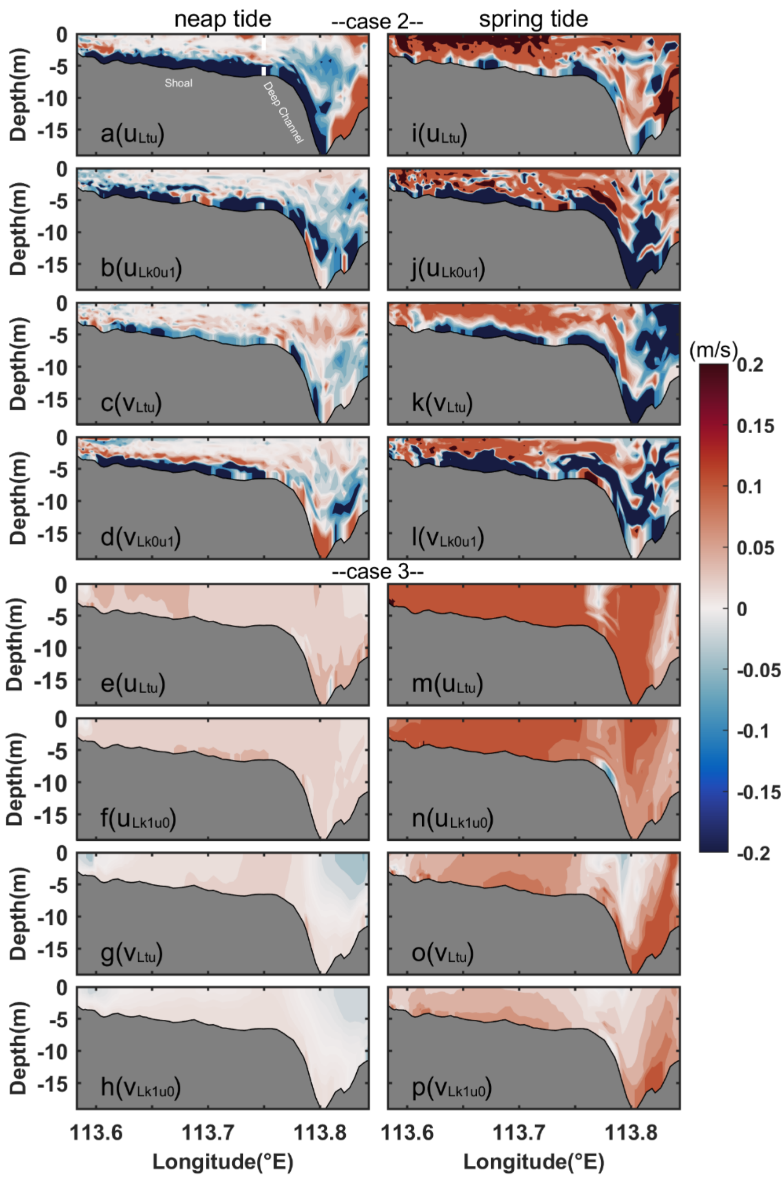

Figure 14. The structure of cross-estuary (u_{Ltu}) and along-estuary (v_{Ltu}) eddy viscosity components and the corresponding dominant components for Case 2 (a–d and i–l) and 3 (e–h, and m–p). Red shading represents eastward flow and blue shading represents westward flow for cross-estuary components. For along-estuary components, red shading represents inflow and blue shading represents outflow. The left column is for neap tides, and the right column is for spring tides.

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3.4 Contributions of non-dominant components for eddy viscosity component

During neap tides, the cross-estuary coupled component of the tidal-averaged eddy viscosity and velocity gradient oscillation (u_{Lk0u0}) for Case 1 demonstrates a vertically sheared structure in the shoal, with alternating westward and eastward flows (Fig. 15a). During spring tides, u_{Lk0u0} for Case 1 predominantly flows eastward in the shoal and displays a two-layer structure in the deep channel with eastward flow in the upper layer and westward flow in the lower layer (Fig. 15d). The cross-estuary tidal straining component (u_{Lk1u0}) during neap tides exhibits an opposing structure to that of u_{Lk0u0} in the lower layer (Fig. 15b). In the upper layer, it displays a similar pattern to u_{Lk0u0}. During spring tides, the extent and magnitude of the eastward flow of u_{Lk1u0} in the deep channel are larger than during neap tides (Fig. 15e). During neap tides, the cross-estuary coupled component of the eddy viscosity oscillation and the tidal-averaged velocity gradient (u_{Lk1u1}) exhibits a complex vertically sheared structure (Fig. 15c). During spring tides, u_{Lk1u1} displays a similar structure but with a greater magnitude than that during neap tides (Fig. 15f). The combined effect of the three components, namely u_{Lk0u0}, u_{Lk1u0}, and u_{Lk1u1}, contrasts with u_{Lk0u1}.

During neap tides, the along-estuary coupled component of the tidal-averaged eddy viscosity and velocity gradient oscillation (v_{Lk0u0}) exhibits a vertically sheared structure with alternating outflow and inflow in Case 1 (Fig. 15g). The structure of the along-estuary tidal straining component (v_{Lk1u0}) closely resembles that of v_{Lk0u0} in the upper layer of the shoal, while it is opposite in the lower layer of the shoal and deep channel (Fig. 15h). Additionally, the cross-estuary coupled component of the eddy viscosity oscillation and the tidal-average velocity gradient (v_{Lk1u1}) displays an opposite pattern to v_{Lk0u0} in the upper layer of the shoal (Fig. 15i). The combined effects of the three along-estuary non-dominant components are opposite to the dominant component (v_{Lk0u1}) and exert a negative contribution to the total eddy viscosity component.

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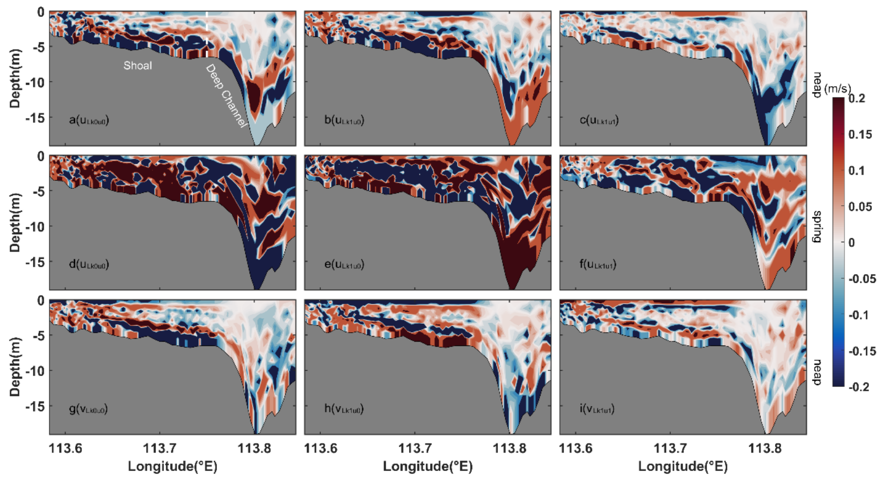

Figure 15. The structure of each non-dominant component of u_{Ltu} during neap tides (a−c) and spring tides (d−f) for Case 1. Red shading represents eastward flow and blue shading represents westward flow. The counterparts for v_{Ltu} during neap tides (g−i), in which red shading represents inflow and blue shading represents outflow.

Without the wind forcing, the structure (Fig. 16) and magnitude (Table 3) of the non-dominant components of the eddy viscosity component in Case 2 remain consistent with those in Case 1 throughout the entire cross section. However, during neap tides, their magnitudes in the upper layer are approximately one order of magnitude smaller compared to Case 1 (Figs. 16a−f), suggesting that wind has a significant effect on these subcomponents during relatively small tides. During spring tides, both the structure (Figs. 16g−l) and magnitude (Table 3) of each non-dominant component of the eddy viscosity component align with those in Case 1. This suggests a weak influence of wind on the non-dominant components during spring tides.

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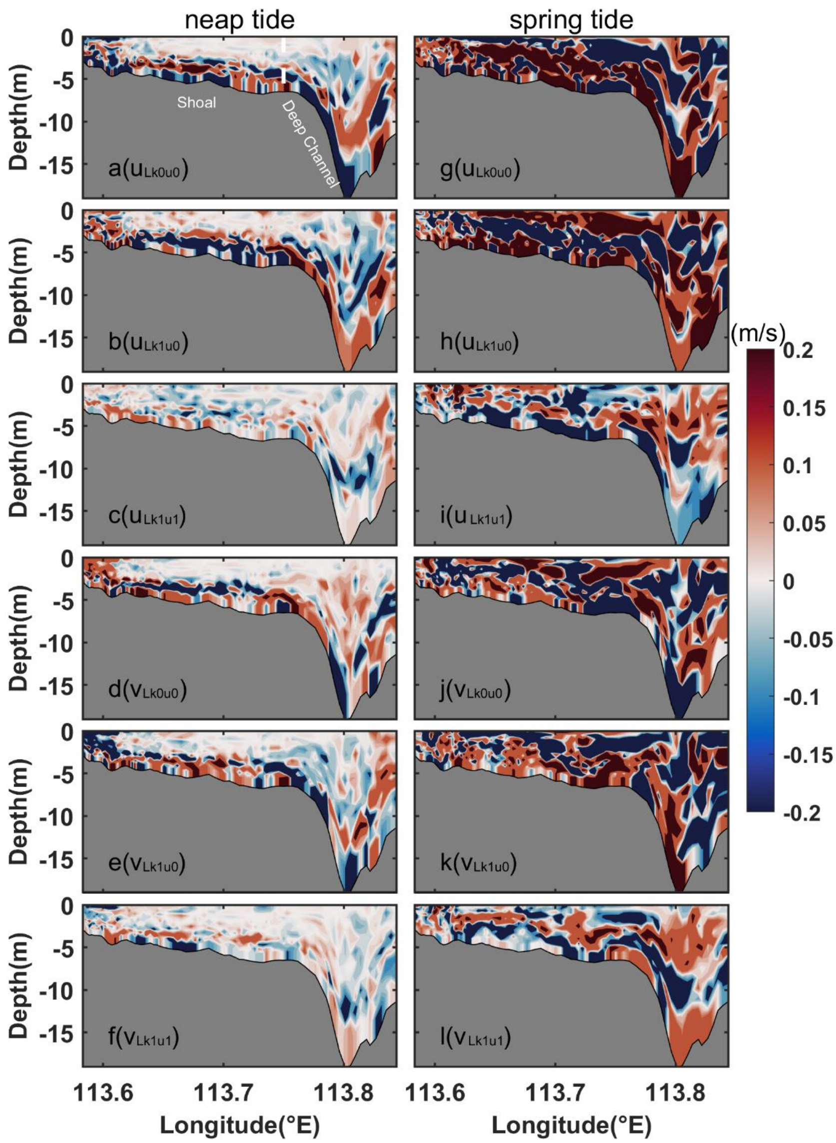

Figure 16. The structure of each non-dominant component of u_{Ltu} and v_{Ltu} during neap tides (a–f) and spring tides (g–l) for Case 2. Red shading represents eastward flow and blue shading represents westward flow for the cross-estuary component. For the along-estuary component, red shading represents inflow and blue shading represents outflow.

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When stratification is further ignored in Case 3, the cross-estuary coupled component of the tidal-averaged eddy viscosity and velocity gradient oscillation (u_{Lk0u0}) exhibits eastward flow in the shoal and the lower layer of the deep channel, while displaying westward flow in the upper layer of the deep channel during neap tides (Fig. 17a). This structure differs from that in Case 2, and the magnitude of u_{Lk0u0} is approximately 14 times smaller than that in Case 2 (Table 3). The cross-estuary turbulent mean component (u_{Lk0u1}) for Case 3 predominantly flows westward in most of the shoal, and eastward in most of the deep channel (Fig. 17b). The u_{Lk0u1} transitions from westward flow in Case 2 to eastward flow in Case 3 in the lower layer of the deep channel. Furthermore, the magnitude of u_{Lk0u1} in Case 3 is approximately 12 times smaller than that in Case 2. During spring tides, the area of eastward flow of u_{Lk0u0} in the shoal is larger than that observed during neap tides in Case 3 (Fig. 17g), and its magnitude is approximately 6 times smaller than that in Case 2. The structure of u_{Lk0u1} during spring tides aligns with that observed during neap tides (Fig. 17h), while its magnitude is roughly 20 times smaller than that in Case 2. The magnitude of the cross-estuary coupled component of eddy viscosity oscillation and tidal-average velocity gradient (u_{Lk1u1}) (Figs. 17c and i) in Case 3 is the smallest among the components (Table 3), ranging from 40 to 50 times smaller than that in Case 2.

The along-estuary non-dominant eddy viscosity subcomponents for Case 3 are depicted in Figs. 17d−f and j−l. During neap tides, both the along-estuary coupled component of the tidal-averaged eddy viscosity and velocity gradient oscillation (v_{Lk0u0}) and the along-estuary coupled component of eddy viscosity oscillation and tidal-average velocity gradient (v_{Lk1u1}) exhibit horizontally sheared structures (Figs. 17d and f) that differ from those in Case 2. The magnitudes of v_{Lk0u0} and v_{Lk1u1} are approximately 22−50 times smaller than those in Case 2 (Table 3). During spring tides, the structures of v_{Lk0u0} and v_{Lk1u1} (Figs. 17j and l) are relatively similar to those during neap tides, and their magnitudes are approximately 12−32 times smaller

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compared to Case 2. During neap tides, the along-estuary turbulent mean component (v_{Lk0u1}) for Case 3 displays inflow in the shoal and the lower layer of the deep channel, as well as outflow in the upper layer of the deep channel (Fig. 17e). This pattern is opposite to that in Case 2, and the magnitude of v_{Lk0u1} is approximately 14 times smaller than that in Case 2. During spring tides, the outflow area of v_{Lk0u1} for Case 3 in the deep channel is larger than that during neap tides (Fig. 17k), and the magnitude is approximately 5 times smaller than that in Case 2. The results demonstrate the significant impact of stratification on each non-dominant component of the eddy viscosity component.

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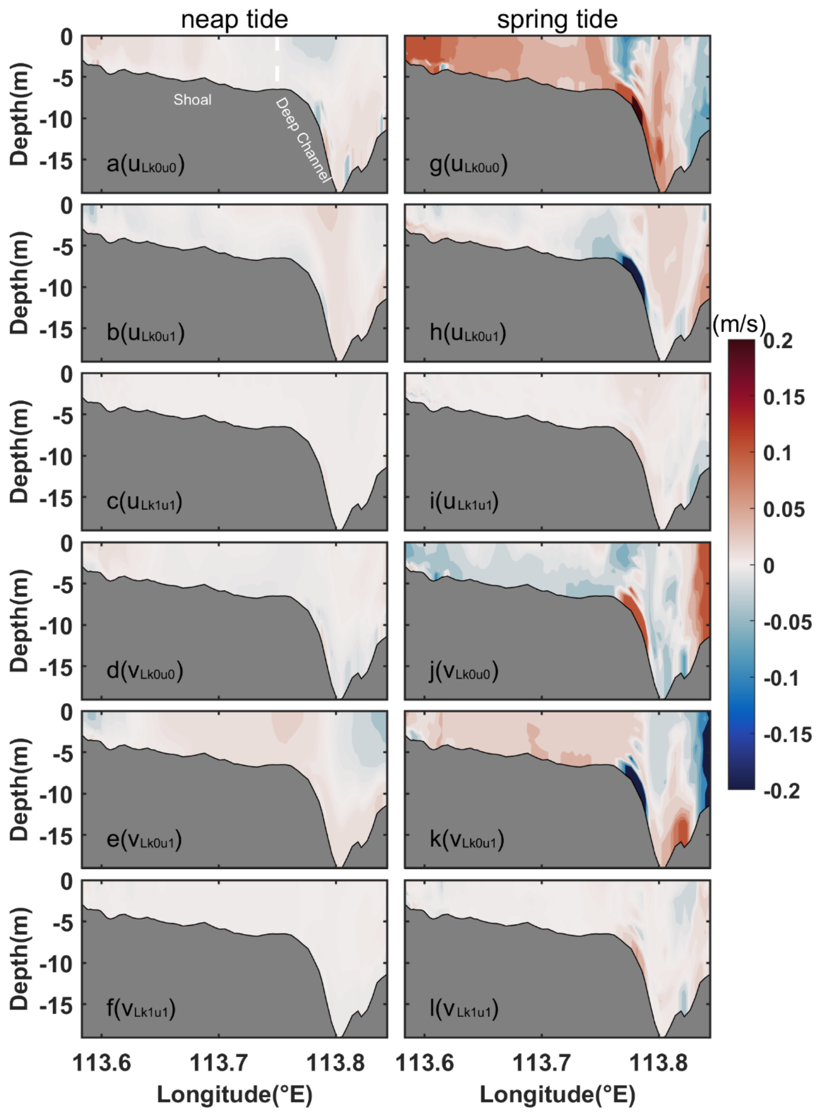

Figure 17. Vertical section of each non-dominant component of u_{Ltu} and v_{Ltu} during neap tides (a–f) and spring tides (g–l) for Case 3. Red shading represents eastward flow and blue shading represents westward flow for cross-estuary components. For the along-estuary component, red shading represents inflow, and blue shading represents outflow.

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4. Discussion

Several dimensionless parameters are examined to quantify the relative impact of the two distinct forcings, respectively. The $K=\zeta_c / h_c$ is a parameter utilized to measure the intensity of advection nonlinearity in the system (Jiang and Feng, 2014), where ζ_c and h_c are the characteristic values of the tidal amplitude and depth, respectively. In most regions of the PRE, the values of K are below 0.2, indicating relatively weak advection nonlinearity. Nonetheless, in proximity to the shorelines, K surpasses 0.4 and can even approach 1 due to the shallow topography, which suggests strong advection nonlinearity in nearshore regions of the PRE. The selected regions for the four cross sections in this paper pertain to the relatively weakly nonlinear zone, thus the LRV displays insensitivity to the initial release phase. The Pelect number (Pe), defined as $u_c L_c / \upsilon_{Dc}$, measures the relative contribution between the nonlinear advection and horizontal diffusion, where u_c, L_c, and υ_{Dc} are the scales of tidal current, the estuary length, and the horizontal diffusion coefficient. The Pe for the PRE domain is several orders of magnitude larger than 1 indicating horizontal diffusion is so small that it can be ignored. The results in the paper have suggested the contribution of the horizontal diffusion component is significantly lower than other components. Among all terms, the barotropic pressure gradient has the largest scale, making the barotropic pressure gradient component of LRV contribute the most compared to other components. The Wedderburn number (W) is calculated to measure the contribution ratio of wind forcing to the baroclinic pressure gradient, defined as $W = L_c T_w / (g \triangle\rho H_c^2)$ (Lange and Burchard, 2019). The value of W in the PRE is 0.0294 during neap tides and 0.0447, suggesting the baroclinic effects dominate in periodically stratified waters and small W inhibits along-estuary gravitational circulation, which is identical to that in Lange and Burchard (2019). The Simpson number (Si) is a parameter used to quantify the level of stratification in estuaries (Simpson et al., 1990). It is calculated using the following formula:

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$$Si = \frac{\partial_x b H^2}{u_{max}^2}, \tag{8}$$

where $\partial_x b$ represents the tidal mean horizontal density gradient, H represents the water depth, and u_{max} represents the absolute magnitude of the velocity amplitude. Based on the Simpson number values, different stratification conditions can be determined for the estuary. The estuary is categorized as well-mixed when $Si < 0.088$; In the case of $0.088 < Si < 0.84$, the estuary displays periodic stratification; For $Si > 0.84$, the estuary is strongly stratified, as indicated by Becherer et al. (2011). The Si for the PRE ranges from 0.1 to 0.45 in stratified conditions in Cases 1 and 2, indicating that the estuary is periodically stratified. Sections B–D are arranged in a north-to-south distribution, gradually approaching the open sea. The Si progressively increases towards the open sea, with values ranging from 0.1 to 0.4 during neap tides and 0.05 to 0.1 during spring tides. This indicates that the magnitude of tides has substantial influences on Si. With the increment in Si, the relative contributions of the tidal straining component and the baroclinic pressure gradient component diminish. These findings align with those of Cheng et al. (2011). Forced by wind, the relative contribution of the two components changes from 2 to 0.57 during neap tides and 2 to 1.4 during spring tides. However, in the absence of wind, the relative contribution varies from 0.67 to 0.26 during neap tides and 1.4 to 0.9 during spring tides, where the value of Si closely mirrors those with wind forcing. These results emphasize the significant influence of the southwesterly wind on the relative contribution of these components.

According to the Eulerian mean theory, the coupled component of tidal-averaged eddy viscosity and velocity gradient oscillation (u_{Ek0u0}), and the coupled component of tidal-averaged velocity gradient and eddy viscosity oscillation (u_{Ek1u1}) are zero (Burchard and Hetland, 2010), however, in the Lagrangian mean theory, those components are not zero and their magnitudes are comparable to other components under most conditions. Although the

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tidal straining component of ERV has been extensively discussed, the contribution of the turbulent mean term to the total ERV has not been analyzed in previous studies (Burchard and Hetland, 2010; Burchard et al., 2011). This paper further analyzes the contribution from the turbulent mean component of the LRV, in which the tidal mean component predominates the eddy viscosity component under stratified conditions, and the tidal straining component plays a significant role in the eddy viscosity component under homogeneous conditions.

The relevance of the Lagrangian residual circulation for mass transport in estuaries or bays is evident. In the Eulerian-averaged salinity balance equation, a tidal dispersion term emerges (Hansen and Rattray, 1965). This tidal dispersion term exhibits different dynamic mechanisms in various estuaries (Fischer, 1976), and even within different sections of the same estuary. However, when the isohaline averaging method is employed to quantitatively assess estuarine circulation, the tidal dispersion term vanishes (MacCready, 2011; MacCready et al., 2018; Wang et al., 2017). Nevertheless, the salinity coordinate method is only an approximate Lagrangian approach. Future studies focusing on the dynamic mechanisms of salinity transport from a Lagrangian averaging perspective will provide further insights into the subject.

5. Conclusions

This paper utilizes the FVCOM model to construct a hydrodynamic model in the PRE. The model simulation results are validated using observed data, and the numerical model is then employed to investigate the dynamic mechanism of the LRV in the estuary. By quantitatively analyzing the contribution of each dynamic component to the LRV, the primary mechanisms governing the LRV in the PRE under various dynamic conditions are elucidated. Furthermore, to explore the influence of the eddy viscosity component on the LRV, it is decomposed into four subcomponents and the contribution of each subcomponent is quantified. This analysis reveals the dominant mechanism controlling the structure of the eddy viscosity

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component under different dynamic conditions.

In the reference case, the cross-estuary LRV (u_L) exhibits a two-layer vertical structure with eastward flow in the upper layer and westward flow in the lower layer. The two-layer structure is primarily determined by the combined effects of the eddy viscosity component (u_{Ltu}), the barotropic pressure gradient component (u_{Lba}), and the baroclinic pressure gradient component (u_{Lgr}). The u_{Ltu} is the main contributor to the eastward flow in the upper layer of the shoal, and u_{Lba} determines the eastward flow in the upper layer of the deep channel. For the entire lower layer, the westward flow is dominated by u_{Ltu} and u_{Lba}, with u_{Lgr} playing a balancing role. The along-estuary LRV (v_L) exhibits a two-layer gravitational circulation pattern. The v_L is predominantly influenced by the imbalance of the barotropic pressure gradient component (v_{Lba}) and the baroclinic pressure gradient component (v_{Lgr}). The outflow is mainly dominated by v_{Lba} in the upper layer, while the inflow is primarily driven by v_{Lgr} in the lower layer. For non-dominant components, the combined effects of the local acceleration component, and the horizontal and vertical nonlinear component contributes less to total LRV. The contribution of the horizontal diffusion component is negligible.

Without wind forcing, the eastward flow dominated by the eddy viscosity component (u_{Ltu}) transforms into the westward flow dominated by the barotropic pressure gradient component (u_{Lba}) in the upper 2 m of the shoal. In other regions, the dominant components of the cross-estuary LRV (u_L) roughly remain the same as those in the reference case, indicating that wind mainly affects u_L in the upper layer by influencing u_{Ltu}. The structure and dominant components of the along-estuary LRV (v_L) are nearly consistent with those in the reference case except for some regions in the shoal, but the magnitude of the dominant components is larger than that in the reference case, indicating that the southwesterly wind inhibits the along-estuary gravitational circulation. The non-dominant components show no significant changes without wind forcing, except for the along-estuary eddy viscosity component, which exhibits a reverse

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structure in the upper layer compared to that with wind forcing.

Under unstratified conditions, the cross-estuary and along-estuary LRV (u_L, v_L) are transformed from the vertical shear structure in stratified waters to the lateral shear structure. The u_L is dominated by the sum of the local acceleration component (u_{Lac}), horizontal nonlinear component (u_{Ladh}), barotropic pressure gradient component (u_{Lba}), and eddy viscosity component (u_{Ltu}). The v_L is dominated by the sum of the barotropic pressure gradient component (v_{Lba}) and eddy viscosity component (v_{Ltu}), indicating that stratification significantly affects the structure and dominant components of the LRV.

This study highlights that the eddy viscosity component remains dominant regardless of the presence of stratification. Specifically, under stratified conditions, the turbulent mean component plays a dominant role in the total eddy viscosity component. Conversely, under unstratified conditions, the tidal straining component takes precedence over other factors in contribution to the total eddy viscosity component. The combined effects of non-dominant components have a negative contribution to the total eddy viscosity component.

Appendix

Numerical solutions of each component of the Lagrangian Residual Velocity (LRV)

Each term in the momentum equations is integrated along the particle trajectories over a tidal period and divided by the tidal period to obtain each dynamic component of Lagrangian residual velocity.

$$v_L = \underbrace{\langle\frac{\partial uD}{D\partial t}\rangle/f}_{1} + \underbrace{\langle\frac{\partial u^2 D}{D\partial x} + \frac{\partial uvD}{D\partial y}\rangle/f}_{2} + \underbrace{\langle\frac{\partial u\omega D}{D\partial \sigma}\rangle/f}_{3} + \underbrace{\langle g\frac{\partial \zeta}{\partial x}\rangle/f}_{4}$$

$$\underbrace{-\langle\frac{1}{D^2}\frac{\partial}{\partial \sigma}\left(v_h\frac{\partial u}{\partial \sigma}\right)\rangle/f}_{5} + \underbrace{\langle\frac{g}{\rho_0}\left(D\int_\sigma^0 \frac{\partial \rho}{\partial x}d\sigma_1 + \frac{\partial D}{\partial x}\int_\sigma^0 \sigma_1\frac{\partial \rho}{\partial \sigma_1}d\sigma_1\right)\rangle/f}_{6} \underbrace{-\langle F_x\rangle/f}_{7}, \quad \text{(A1)}$$

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$$u_L = -\underbrace{\langle \frac{\partial vD}{D\partial t}\rangle/f}_{1} - \underbrace{\langle(\frac{\partial uvD}{D\partial x}+\frac{\partial v^2D}{D\partial y})\rangle/f}_{2} - \underbrace{\langle\frac{\partial v\omega D}{D\partial\sigma}\rangle/f}_{3} - \underbrace{\langle g\frac{\partial\zeta}{\partial y}\rangle/f}_{4}$$

$$+\underbrace{\langle\frac{1}{D^2}\frac{\partial}{\partial\sigma}\left(v_h\frac{\partial v}{\partial\sigma}\right)\rangle/f}_{5} - \underbrace{\langle\frac{g}{\rho_0}\left(D\int_\sigma^0 \frac{\partial\rho}{\partial y}d\sigma_1 + \frac{\partial D}{\partial y}\int_\sigma^0\sigma_1\frac{\partial\rho}{\partial\sigma_1}d\sigma_1\right)\rangle/f}_{6} + \underbrace{\langle F_y\rangle/f}_{7}, \qquad \text{(A2)}$$

where *u* (*x*, *y*, *σ*, *t*), *v* (*x*, *y*, *σ*, *t*), and *ω* (*x*, *y*, *σ*, *t*) represent velocity components in the longitudinal (*x*), latitudinal (*y*), and vertical (*σ*) directions, respectively. The *ρ* (*x*, *y*, *σ*, *t*) is water density, ρ_0 is the reference density, *t* is the time, *f* is the Coriolis parameter, and v_h (*x*, *y*, *σ*, *t*) is eddy viscosity coefficient. The $D = H + \zeta$, where *H* (*x*, *y*) is the water mean depth, *ζ*(*x*, *y*, *t*) is the water surface elevation. The first term refers to local acceleration component, the second terms represent horizontal nonlinear advection components, the third term depicts the nonlinear vertical advection component, the fourth term corresponds to the barotropic pressure gradient component, the fifth term describes the eddy viscosity component, the sixth terms denote the baroclinic pressure gradient components, and the seventh term pertains to horizontal diffusion component. The < > denotes the Lagrangian mean operator.

Data availability

Hydrodynamic datasets used in this study are available online at https://doi.org/10.5281/zenodo.8323286 (Deng et al., 2023). The 1° World Ocean Atlas 2009 (WOA2009) datasets are accessible online from (https://accession.nodc.noaa.gov/0094866). The 0.25° CCMP datasets are available online (http://www.remss.com/measurements/ccmp). The monthly average river runoff data are provided by the Water Conservancy Committee of the Pearl River under the Ministry of Water Resources. The topography data off the PRE are from the ETOPO2 dataset of NOAA (https://www.ngdc.noaa.gov/mgg/global/relief/ETOPO2/ETOPO2v2-2006/), while those within the estuary are provided by the China Maritime Safety Administration.

Author contributions

All authors have contributed to the conceptualization and design of this study. The analytical methods were originally formulated by FD. Subsequently, FD and ZC meticulously processed and analyzed the data. The model was collaboratively developed and the manuscript was co-authored by FD, FJ, and ZC. The final manuscript underwent a thorough review and editing process, led by RS, SZ, QL, and XZ, ensuring its quality and accuracy.

Competing interests

The contact author has declared that none of the authors has any competing interests.

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