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Time-varying drainage basin development and erosion on volcanic edifices

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Abstract. The erosional state of a landscape is often assessed through a series of metrics that quantify the morphology of drainage basins and divides. Such metrics have been well-explored in tectonically-active environments to evaluate the role of different processes in sculpting topography, yet relatively few works have applied these analyses to radial landforms such as volcanoes. We quantify drainage basin geometries on volcanic edifices of varying ages using common metrics (e.g., Hack's Law, drainage density, number of basins that reach the edifice summit, as well as basin hypsometry integral, length, width, relief, and average topographic slope). Relating these measurements to the log-mean age of activity for each edifice, we find that drainage density, basin hypsometry, basin length, and basin width quantify the degree of erosional maturity for these landforms. We also explore edifice drainage basin growth and competition by conducting a divide mobility analysis on the volcanoes, finding that young volcanoes are characterized by nearly-uniform basin geometries in unstable configurations that are prone to divide migration. Finally, we analyze basin spatial geometries and outlet spacing on edifices, discovering an evolution in radial basin configurations that differ from typical linear mountain ranges. From these, we present a novel conceptual model for edifice degradation that allows new interpretations of composite volcano histories and provides predictive quantities for edifice morphologic evolution.

1.0 Introduction

Understanding how drainage basins on eroding landforms develop and evolve is a fundamental principle of Geomorphology. Over regional scales, basin geometry, structure, and spacing evolve in response to both external (e.g., climate, tectonics; Castelltort et al., 2012; Duvall and Tucker, 2015; Han et al., 2015; Yang et al., 2015) and internal (e.g., channel piracy; Bishop, 1995; Whipple et al., 2016) forcing as topographic slopes adjust to develop and maintain an equilibrium between erosion and uplift (e.g., Willett et al., 2001; Castelltort et al., 2009). As these landscapes adjust, transient signals within basins propagate upstream to surrounding channel heads, where opposing signals between adjacent basins drive divide migration that modify available area for overland flow (e.g., Willett et al., 2014; O'Hara et al., 2019).

Work in the 20th century established foundational relationships between basin drainage areas, lengths, and slopes (e.g., Horton, 1945; Strahler, 1952; Hack, 1957; Flint, 1974), providing the basis for analyzing landscape disequilibrium and evolution in both tectonically-active (e.g., Kirby and Whipple, 2012; Fox et al., 2014) and passive regions (Prince and Spotila, 2013; Willett et al., 2014; Braun, 2018). These relationships are built on the assumption of a dominantly-dendritic fluvial network existing on a near-linear primary landform (e.g., a mountain range; Castelltort and Simpson, 2006). Furthermore, basin competition is often considered in the simplified

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configuration of a binary drainage system, where a divide supports only two opposing basins that compete across it (e.g., Gilbert, 1909; Mudd and Furbish, 2007).

Although dendritic channel networks are most prevalent on Earth, they are not the only type of configuration. Trellis, rectangular, parallel, and radial drainages also occur (Howard, 1967). The formation of these other drainages often relate to the region's tectonic, volcanic, or glacial history, subsurface structure, or geometry of the primary landform that they erode (Zernitz, 1932). However, compared to dendritic basins, studies that explore the geometries and evolution of other drainage settings are scarce (e.g., Mejía and Niemann, 2008; Becerril et al., 2021; Hamawi et al., 2022).

Volcanic edifices are characterized by radial drainages. In these settings, quantifying drainage evolution can be challenging as these landforms experience interspersed, short-term eruptive episodes superimposed onto the long-term degradation record (e.g., Thouret et al., 2014). Additionally, drainage formation can lag behind surfacing by volcanic deposits over 1 – 100 kyr timescales due to transmission losses associated with permeable volcanic material (e.g., lava flows, pyroclasts; Lohse and Dietrich, 2005; Jefferson et al., 2010; Sweeney and Roering, 2017). Finally, the binary drainage divide typical of linear mountain ranges breaks down on volcanic edifices due to their radial nature, with multiple catchments constrained to the conical structure of the volcano and converging towards a single main summit. Despite these challenges, volcanic edifices represent ideal primary landforms to investigate drainage evolution due to their well-defined conical initial conditions, datable surfaces, and scarce inheritance from regional tectonics. Furthermore, quantifying the relationships between edifice construction and drainage basin morphology provides new insight for investigating edifices remotely, and can thus expand our understanding of basin dynamics while also complimenting field-based surveys to resolve volcano edifice histories.

Here, we explore the development of drainage basins and topography on stratovolcanoes from Indonesia, Papua New Guinea, and New Zealand (Fig. 1). Using common hydrographic metrics and broad volcanic histories, we determine stages of maturation during basin evolution and derive a new generalized model for volcanic edifice degradation that builds off of previous studies (Ollier, 1988). We then quantify divide mobility on radial structures within the context of our conceptual model and discuss the applicability of our analyses to characterize an edifice's history.

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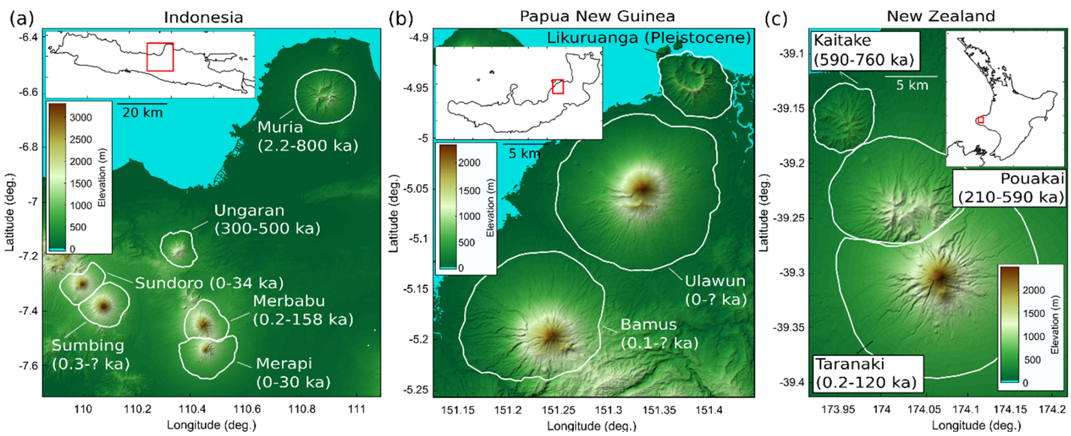

Figure 1 – Regional maps of 12 analyzed edifices from (a) Indonesia, (b) Papua New Guinea, and (c) New Zealand. White lines represent edifice boundaries. Text describes volcano names and known ages of activity (Table T2).

2.0 Methods

We focus on closely-spaced sets of volcanic edifices (Fig. 1). Within each respective region, volcano sets are fed by similar magma sources and likely experienced similar climate conditions, but the volcanoes were active over different time intervals and show spatially-varying degrees of degradation. We exclude complex massifs from the analysis and consider only relatively simple edifices.

2.1 Edifice Delineation

We follow the method of van Wees et al. (2021) to delineate edifice boundaries from surrounding topography. Although automated algorithms exist to generate boundaries (e.g., Bohnenstiehl et al., 2012; Euillades et al., 2013), these often create conservative limits around the edifice that ignore lower flanks and volcano-sedimentary aprons (e.g., O'Hara et al., 2020). Using 30-m Shuttle Radar Topography Mission (SRTM) Digital Elevation Models (DEMs) (Farr et al., 2007), we first generate hillshade, aspect, and slope angle rasters of the raw topography. Lower edifice flanks are generally characterized by slope angles greater than some threshold value (Karátson et al., 2012); we therefore filter topography using a 300 m wavelength and reclassify the slope map using a 3° slope threshold (van Wees et al., 2021). Using these maps as visual aids, we then hand-draw boundaries that separate the edifice from surrounding terrain. Afterwards, the DEMs are clipped using these boundaries to isolate the edifices for morphometric analysis. None of the chosen volcanoes have closed summit craters, recognizable collapse scars, or any other irregular surface that required special preprocessing; we thus use the entire edifice topography for our analysis.

2.2 Edifice Basin Morphology

We analyze edifice basin morphologies with DrainageVolc, a series of scripts modified from TopoToolbox (Schwanghart and Scherler, 2014), which is designed to investigate volcanic topography through a set of topography-, drainage-, and channel-based analyses. The metrics considered here are commonly used within tectonic settings but have not previously been applied to radial drainages. Figure 2 displays an example of our methods using the Ungaran volcano in Indonesia.

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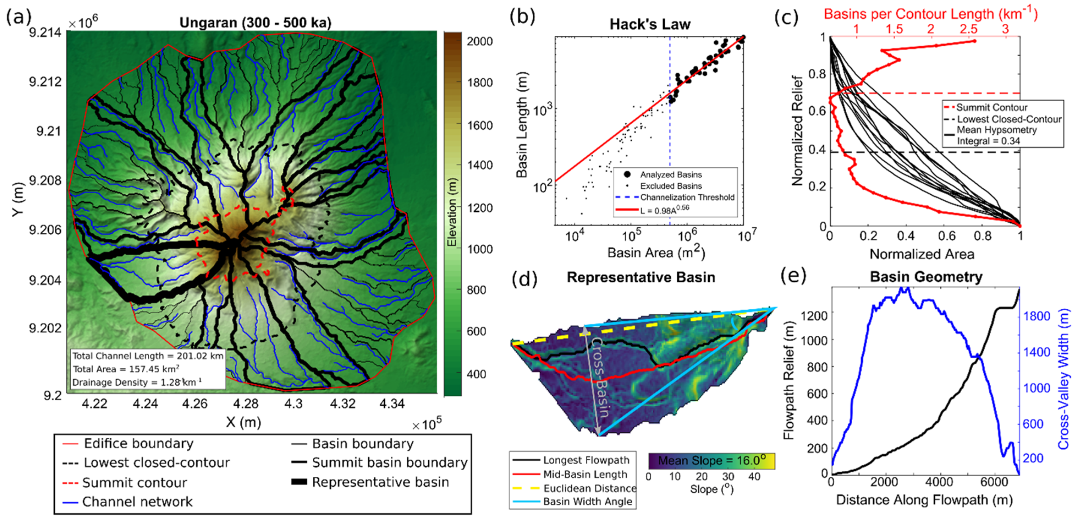

Figure 2 – Analyzed basin metrics. a: Map of Ungaran volcano (Indonesia), colored lines defined in legend. b: Hack's Law relationship between basin areas and lengths. Black circles are basins used in power-law analysis, black dots are excluded basins; blue-dashed line is drainage area threshold (A_T; 0.5 km^2) for channelization. c: Scaled edifice metrics. Red line shows normalized number of basins along elevation contours. Black lines are summit basin hypsometry curves. d: Local slope and geometry values of representative basin (thick black line in 2a). Gray line represents cross-basin direction perpendicular to the Euclidean basin length. e: Cross-basin values along basin shown in 2d. Black line is relief along flowpath, blue line is cross-valley width.

We first fill sinks in the DEM through TopoToolbox's preprocessing algorithm (Schwanghart and Scherler, 2014) to ensure continuous flow to the edifice boundary and extract drainage basins from topography using steepest-descent flow routing (Fig. 2a). We then perform a series of analyzes related to basin geometry. The lengths (L) of all basins draining to the edifice boundaries are calculated by determining mid-point paths between basin divides perpendicular to the Euclidean distance between the highest and lowest reaches of the basin, irrespective of whether there is an actual flow channel in this path (Fig. 2d). Assuming basins with drainage areas (A) greater than some threshold (A_T) support overland flow, we then explore the correlation between the lengths and drainage areas of these basins through a power-law regression to derive the Hack's Law relationship (Fig. 2b) for the edifice as (Hack, 1957)

$$L = k_a A^H, \quad (1)$$

where k_a and H are Hack's coefficient and exponent, respectively. H values are compared across edifices as this exponent describes general basin geometry, with values of ~0.47 – 0.6 typically attributed to dendritic systems (Hack, 1957; Mueller, 1972). Our Hack's Law derivation uses mid-point basin lengths as opposed to typical flow path lengths to remove the effects of channel sinuosity and focus explicitly on basin geometry; however, within the context of our edifice basins, this derivation does not significantly alter our results, and values are thus comparable to those of previous studies (Fig. S1). We also analyze the density of the edifice's channel network by extracting

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flow paths with drainage areas greater than A_T from the landform, and calculate the edifice-scale drainage density as (Horton, 1945)

$$DD = \frac{\sum L_c}{A_E}, \tag{2}$$

where $\sum L_c$ is the cumulative sum of all channel lengths and A_E is the planform area of the edifice's boundary (Fig. 2a). Using an automated slope-area analysis of basins to determine the drainage area threshold that best corresponds with the power-law decrease in slope (Montgomery and Dietrich, 1994) for each edifice, we find A_T ranges between 0.32 – 1.42 km^2, with a mean threshold of 0.78 km^2 (Supplemental text). For consistency across all edifices, we assume a constant drainage area threshold of 0.5 km^2 to delineate networks. Sensitivity analysis (Fig. S3) demonstrates that although the selection of A_T does not significantly impact the general behavior of drainage density results, the Hack's Law exponent is more sensitive to this choice.

Afterwards, we calculate mean values of basin geometries on each edifice. Rather than analyze the geometry of all basins that exist on a volcano, we limit our analysis to larger basins that best characterize the edifice's drainage, and thus its dismantling. These large characteristic basins may be determined using a variety of methods, such as through an arbitrary number or percentage of basin sizes, using the basins that are within some radial distance of the edifice's peak, or determining basins that extend to some portion of the edifice's height. Determining characteristic basins by an arbitrary number or percentage of basin sizes may introduce bias as the population of basins drastically vary between edifices (Fig. 8a), whereas determining characteristic basins by radial distance from the edifice's peak introduces geometric constraints as edifice shapes often deviate from the textbook symmetric, single-peaked edifice, instead developing large, irregular summit regions that are defined by high topography and multiple peaks (e.g., Karátson et al., 1999; Grosse et al., 2012). As slope (and thus elevation) is an essential component of erosion and basin development (Hack, 1957; Flint, 1974), we define characteristic basins as those that reach the edifice's summit region. However, we note that defining characteristic basins based on radial distance can produce different trends (Fig. S4), and may be more appropriate for some of our analyzed metrics (Section 5.3).

Generating a series of elevation contours along the edifice at intervals of 2.5% of the edifice's relief, we calculate the number of basins that intersect each contour, normalized by the contour's length (Fig. 2c, red line). For all edifices, we define the edifice's summit as the upper 30% of the edifice's relief, and thus consider the basins that reach this summit region (referred here as *summit basins*) as those that best characterize the edifice's drainage development. We then determine summit basin numbers, mean basin slopes (Fig. 2d), basin lengths (L_B; Fig. 2d, red line), basin reliefs (Fig. 2e, black line), and maximum cross-basin widths (W_B; Fig. 2e, blue line). To compare values across edifices of varying sizes, summit basin numbers are normalized by the length of the summit contour (Fig. 2c) and basin reliefs are normalized by the relief of the entire edifice. We also utilize the radial nature of edifices to generate normalized values of basin length (L_B') and width (W_B') as

$$L_B' = \frac{L_B}{L_E}, \tag{3}$$

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and

$$W_B' = 2\tan^{-1}\left(\frac{W_B/2}{L_{W_B}}\right), \quad (4)$$

respectively, where L_E is the edifice's effective radius, defined as the radius of the circle with the same planform area (A_E) as the edifice's boundary ($L_E = \sqrt{A_E / \pi}$), and L_{W_B} is the distance from the highest point within a basin to where the basin is widest. W_B' thus converts basin widths into an angle relative to the summit (Fig. 2d, light blue lines). Mean values of these quantities are then calculated for each edifice.

We also calculate mean summit basin hypsometry integrals for each edifice (Strahler, 1952; Fig. 2c, black lines). Individual basin hypsometry curves (H_C) are derived by counting the number of basin pixels N_{P_B} at or above normalized elevation values ($\dot{Z}$, ranging from 0 to 1); afterwards, these values are normalized by the total number of basin pixels ($N_{P_{Tot}}$) as

$$H_C(\dot{Z}_I) = \frac{N_{P_B}(\dot{Z} \geq \dot{Z}_I)}{N_{P_{Tot}}}, \quad (5)$$

where I is a counter over normalized elevation values from 0 to 1. Hypsometry integrals of each basin are calculated as the positive integration over the curves from eq. (5). These are also averaged for each edifice.

2.3 Edifice Landform Morphology

As well as studying the temporal evolution of drainages on edifices, we also consider the broad geometry of the volcanoes. Grosse et al. (2009, 2012) developed the initial MorVolc algorithm in IDL, which quantifies edifice morphologies through a series of size, shape, slope, orientation, peak, and summit parameters. Using the same framework as DrainageVolc, we redeveloped the IDL code in Matlab, also utilizing the TopoToolbox DEM analysis package (Schwanghart and Scherler, 2014). Both DrainageVolc and the updated MorVolc scripts are available for use on GitHub (https://github.com/danjohara/Volc_Packages).

We analyze simple edifice geometry measurements with this updated version of MorVolc, including effective radius, height, height-radius ratio, and mean slope of the main flank (edifice region between the lowest closed-contour that encompasses the edifice and the edifice's summit contour). We also quantify the mean contour ellipticity and irregularity indices of the main flank from the previously-computed contours. The ellipticity index (EI) describes the elliptical nature of the edifice elevation contours, and is defined as

$$EI = \frac{\pi (L_M/2)^2}{A_C}, \quad (6)$$

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where L_M is the length of the major axis of a best-fitting ellipse through the contour and A_C is the area enclosed by the contour (Grosse et al., 2012). The irregularity index (II) describes divergence of the contour from a smooth ellipse as

$$II = di_{contour}\left(di_{ellipse} - 1\right), \tag{7}$$

where di is the dissection index, defined as

$$di = \frac{P_C}{2A_C}\sqrt{A_C/\pi}, \tag{8}$$

with P_C and A_C being the perimeter and area of the contour, respectively (Grosse et al., 2012). Finally, we also incorporate new measurements within MorVolc, including the slope variance of the entire edifice (standard deviation of all slope values divided by the mean slope, similar to roughness), as well as a minimum eroded volume estimate. Eroded volume is estimated from a convex-hull reconstruction of the edifice, using the methodology described in O'Hara and Karlstrom (2023). Afterwards, eroded volume is normalized as a percent relative to the total reconstructed volume.

2.4 Edifice Ages

To explore morphological evolution through time, we correlate edifice landform and drainage basin metrics to volcano ages of activity. We thus compile known eruption records of each volcano, with ages ranging from present to early Pleistocene (Table T2). Volcanoes often have complex surface evolutions, with lifespans of activity that range 100-1000 kyrs and characterized by stochastic episodes of growth interspersed with periods of erosion during quiescence (e.g., Karátson et al., 1999; Lahitte et al., 2012). Furthermore, episodes of activity are often constrained to localized regions of the edifice and thus do not fully resurface the entire landform (e.g., Civico et al., 2022). Similarly, erosion across the edifice is typically non-uniform as local conditions are dependent on the age and type of activity within the vicinity (e.g., Ferrier et al., 2013; Pierson and Major, 2014; Thouret et al., 2014; Ricci et al., 2015).

Despite the spatial and temporal heterogeneities of activity and erosion, we argue that a generalized morphologic age of an edifice may be derived that quantifies the erosional state of the landform and relates to the edifice's lithologic age. To account for the time differences between short-term events and the cumulative long-term history on morphology, we define an edifice's age as a single value using the log-mean between the most recent eruption and oldest date of activity. This definition thus accounts for the span of temporal magnitudes; however, we note that using linear-mean ages produce similar results (Fig. S5). Afterwards, we analyze the temporal evolution of edifice morphologies by fitting logarithmic relationships between edifice age and morphometric parameters. Some volcanoes (Sumbing, Bamus, and Ulawun) have poorly-documented histories (only the most recent eruption has been dated) and are therefore excluded from the regression. Conversely, Likuruanga is only known to have erupted during the Pleistocene and is incorporated in the analysis.

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3.0 Results

We find trends between volcano age and our morphometric metrics through time (Figs. 3-4; Supplemental Table T3). Considering all metrics, we find that edifice height, effective edifice radius, mean irregularity index (with the exception of an outlier; Fig. 4e), mean ellipticity index, edifice slope variance, normalized eroded volume, drainage density, mean summit basin hypsometry integral, normalized basin length, and normalized basin width have R^2 values ranging 0.38 – 0.75 and correlation p-values < 0.1, suggesting these metrics provide quantitative measures to characterize the overall maturity of the edifice. Other metrics have weaker correlation values (0.21 – 0.32) and are statistically insignificant (with p-values of 0.11 – 0.21), and thus may be more sensitive to the initial edifice geometry or other processes that alter edifice morphology, or that age is not a significant factor for these metrics. The noted outlier in irregularity index is Muria (Indonesia) and originates from two broad fluvial networks on opposite flanks that are deeply incised into the landform and may be associated with breached craters (Fig. 1a).

Of the statistically-significant metrics related to edifice drainage morphology, mean summit basin hypsometry integral and normalized width increase through time, whereas drainage density and mean summit basin normalized length decrease (Fig. 3). Similarly, considering statistically-significant metrics related to the edifice as a primary landform, mean irregularity index, mean ellipticity index, and convex-hull based eroded volumes increase with age, while edifice height, effective radius, and slope variance decrease with age (Fig. 4).

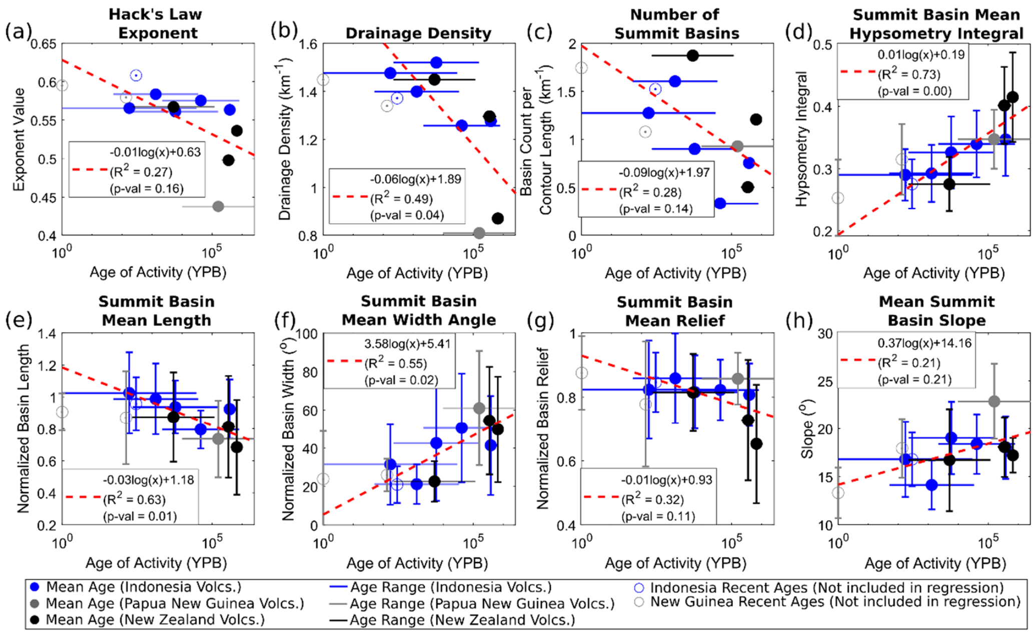

Figure 3 – Temporal relationships of drainage basin morphology metrics. Colors correspond to volcanic region. Horizontal lines are edifice age ranges of activity, with filled circles representing log-mean age. Vertical lines represent one standard deviations of values (where appropriate). Red-dashed lines and equations characterize logarithmic regressions; open circles are excluded in the regression due to age limitations.

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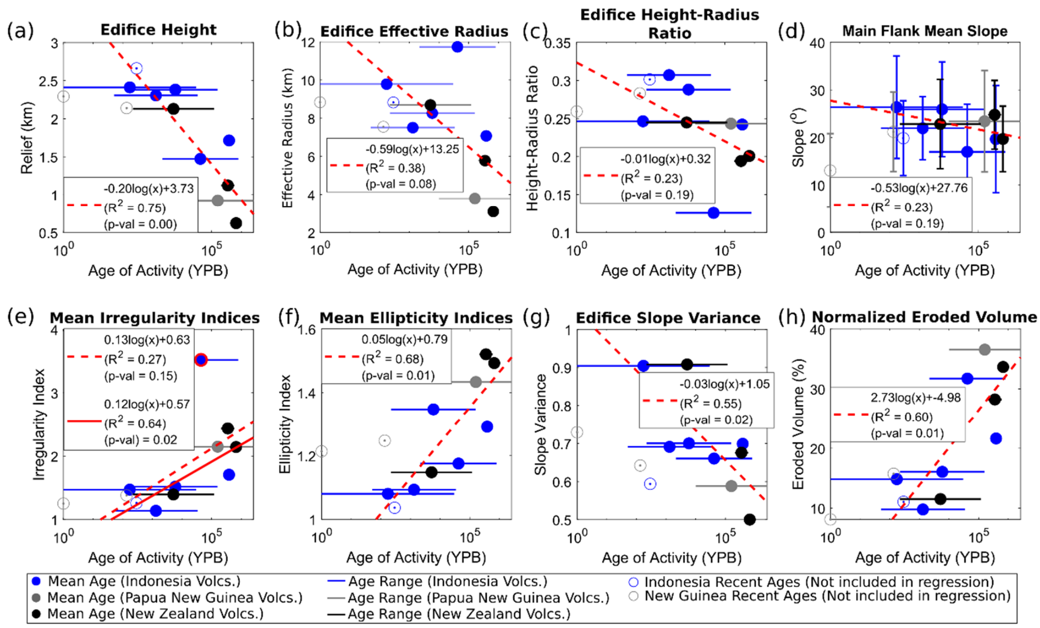

Figure 4 – Temporal relationships of landform morphology metrics. Colors and symbols are same as those described in Fig. 3. Solid red line in e is secondary regression with Muria (red circle) excluded.

4.0 Discussion

4.1 Generalized model for edifice degradation

The evolution of volcanic edifices as primary landforms and the drainage basins that erode them are inextricably linked. Our results thus establish a new framework for evaluating volcanic edifices by considering both the landform and its drainage systems. This evolutionary model expands on stages previously defined qualitatively (Ollier, 1988) and follows similar evolution to drainages observed in badlands (Schumm, 1956).

Erosion of a volcanic edifice can be described within the context of our metrics by considering a simplified, conical edifice (Fig. 5). In the initial stages of erosion (~10% of eroded volume; Fig. 5a), narrow (~ 20° normalized width angle) and uniform (normalized mean length near 1) drainages form that extend from the summit region to the lower flanks (i.e., 'parasol ribbing'; Ollier, 1988), giving a high drainage density (~1.5 km^{-1}).

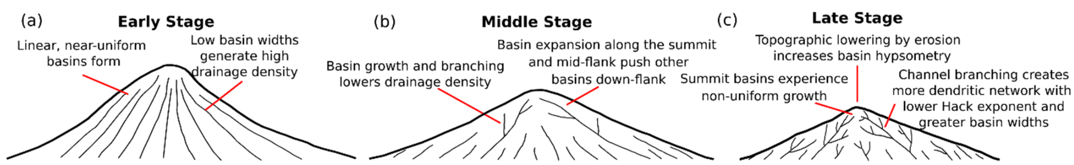

Figure 5 – Conceptual model of edifice dissection based on analysis results. Thin black lines represent drainage systems.

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As the edifice degrades to 30-40% eroded volume on 10-100 kyr timescales (Fig. 5b-c), both its height and area decrease; however, height decreases faster, leading to a decrease in height-radius ratios. The erosion of the edifice is accompanied by drainage basin growth, with summit basins expanding azimuthally along the edifice to normalized basin widths of 40-60°, pushing the headwaters of other basins down the edifice flanks. Furthermore, as summit basins expand, they incise into the edifice flanks and develop a more dendritic structure associated with lower drainage density (~1 km^{-1}). This is accompanied by non-uniform summit basin lengthening; combined with possible volcanic activity that can influence landform asymmetry (i.e., causing a higher ellipticity index), non-uniform basin growth causes normalized basin lengths to decrease below 1.

As the edifice erodes, processes occur over varying scales to alter general edifice morphology: 1) over the entire edifice, erosion-driven topographic lowering occurs faster than horizontal areal loss of the edifice, creating a flatter landform; and 2) at the scale of a basin, incision carves into the initially-planar flanks of the edifice, steepening surrounding valley walls and increasing contour irregularity. The relationship between basin-scale incision and edifice-scale flattening is recorded through summit basin hypsometry integrals and the slope variance of the entire edifice. The decrease in edifice slope variance suggests mean edifice slopes increase relative to the standard deviation of slope, thus suggesting overall steepening of topography. However, increasing values of summit basin hypsometry integrals suggest that edifice-scale flattening is the dominate process. This leads to a scale-dependent behavior in edifice morphology – although the edifice as a landform is becoming flatter, incision causes local relief within the bounds of the landform to become steeper.

This conceptual model represents a generalized view of edifice degradation, as a variety of processes (both volcanic and erosional) can impact an edifice's morphology throughout its lifespan. Furthermore, other climate conditions not considered here (e.g., glaciers, arid environments) are expected to alter the patterns and rates of basin evolution. Nonetheless, we propose that, barring major events that significantly alter topography, composite volcano degradation generally follows the model presented here.

4.2 How do basins compete on radial structures?

Our results suggest that drainages on radial structures are highly dynamic. From initially-uniform basin geometries, preferential erosion causes basins near the summit to become more dominant and expand, forcing other basins down-flank and generating a 'topographic hierarchy', with higher-order basins spanning the entire flank of the edifice and lower-order basins occurring on lower sections, analogous to inferred basin evolution on linear fault blocks (Talling et al., 1997). This hierarchy of basin ordering is a direct product of non-uniform basin development over the edifice that contributes to the preservation of less-eroded portions of the lower flanks (i.e., planèzes; Ollier, 1988).

Non-uniform basin development and transience is a natural component of landscape evolution (e.g., Hasbargen and Paola, 2000); however, various factors (both volcanic and non-volcanic) can influence erosional patterns and accentuate basin growth across volcanic edifices. These may include 1) local slope changes associated with magmatic intrusions (e.g., Wicks et al., 2002; Biggs et al., 2010; Castro et al., 2016) or mass-wasting (e.g., Ui and Glicken, 1986; Shea and van Wyk de Vries, 2008); 2) variable volcanic eruption activity that increase sediment

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loads (Hayes et al., 2002; Pierson and Major, 2014), alter infiltration and rock erodibility (e.g., Wells et al., 1985; Sklar and Dietrich, 2001; Jefferson et al., 2010), or remove bedrock through scouring by pyroclasts (Gase et al., 2017) or melting by lava flows (i.e., thermal erosion; Kerr, 2001) during deposition; 3) non-uniform changes in overland flow and stream power associated with breached craters (e.g,. Karátson et al., 1999) or edifice-scale precipitation gradients (e.g., Ferrier et al., 2013); and 4) downstream alterations to drainage channels that migrate upstream as a propagating incision wave (i.e., knickpoints; Kirby et al., 2003; Cook et al., 2013; Perron and Royden, 2013). The long-term compilation of such processes helps drive non-uniform erosion across the edifice, which in turn encourages divide migrations and changes in basin size and geometry. More specifically, basins that exhibit higher erosion rates would tend to expand at the expense of their neighboring basins and potentially become the dominant basins, while lower erosion rates will cause other basins to shrink and their boundaries to migrate further down the edifice's flank.

The morphology of drainage divides is sensitive to differences in erosion between neighboring basins and can thus be used to characterize basin competition. We quantify basin geometry unsteadiness through an exploration of divide stability using the *divide asymmetry index* (DAI; Forte and Whipple, 2018; Scherler and Schwanghart, 2020), calculated as the positive difference in hillslope relief (vertical distance between the ridge and nearest channel) across a divide and normalized by the sum of hillslope reliefs, ranging between 0 (symmetric) and 1 (asymmetric). We limit our analysis to only consider divides that have a Strahler order greater than 1 (Scherler and Schwanghart, 2020).

The divide mobility is expressed using probability density functions (PDFs) of DAI for all volcanoes (Fig. 6a). A clear temporal trend emerges – older volcanoes have distributions clustered around lower (< 0.4) DAI that rapidly decrease with increasing DAI; while younger volcanoes show monotonically-decreasing distributions, with fewer normalized populations of low-DAI and greater normalized populations of high-DAI values compared to older volcanoes. Integrating these PDFs into single values (referred to here as Γ; Fig. 6b) shows a moderate ($R^2 = 0.41$) correlation with age.

Combined with basin morphology trends (Fig. 3), this suggests younger volcanoes have basins with more uniform planform geometries and less-stable basin configurations. As the edifice erodes, basin planform geometries become less uniform, but develop more stable configurations as evidenced by the greater symmetry of hillslope relief across divides. The relationship between basin non-uniformity and stability can be observed spatially by comparing DAI values between Merapi (youngest) and Kaitake (oldest) volcanoes (Fig. 6c-d). Highest DAI values on both volcanoes generally occur at the mid- and lower-flanks of the volcano, suggesting basin expansion occurs mainly azimuthally along edifice flanks, rather than across the edifice summit. This spatial analysis highlights the process that generates topographic hierarchy – by expanding azimuthally, basin growth drives less-dominant basins down-flank through a zippering process, creating drainages with tapered geometries along the lower flanks.

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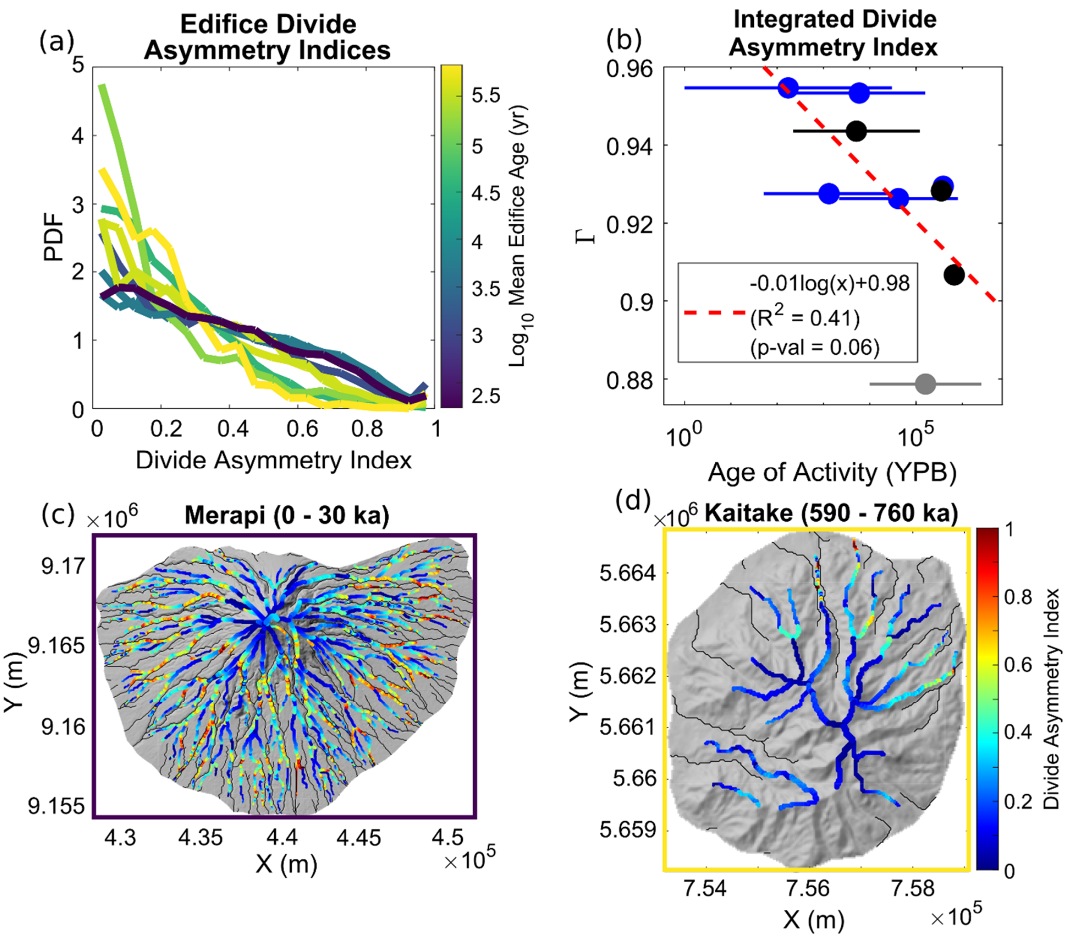

Figure 6 – a: Probability density functions (PDFs) of volcano divide asymmetry indices (*DAI*); colors correspond to log-mean edifice ages. b: Integral of PDFs (*Γ*) compared to edifice age. Colors and symbols are the same as Fig. 3. c-d: *DAI* values for (c) Merapi and (d) Kaitake at the divides, black lines are edifice channel network. Border colors correspond to ages in a.

4.3 Edifice basin widths and spacing

Our results show that edifices experience the same morphologic trends when considering the number of basins along edifice relief (Fig. 7a): lower flanks are characterized by normalized basin numbers between 2–6 km^{-1}, main flanks are characterized by relatively consistent normalized basin numbers < 2 km^{-1}, while the normalized basin numbers increase near the summit (upper 30% of the edifice). This trend appears to occur largely independent of age, even within the upper flank (as demonstrated by a low R^2 value of 0.28 at the summit contour, Fig. 3c), suggesting that this morphologic trend is a direct consequence of the conical nature of volcanoes. Furthermore, non-normalized summit basin numbers also demonstrate a weak temporal trend, both at the upper 30% height designation (Fig. 7b) as well as other percentages (Fig. S6). This suggests that basins that initially form on the summit region may retain their topographic position as the edifice erodes. However, Fig. 3f demonstrates that these basins still widen through

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time, to a width angle of ~60° (though further analysis on older volcanoes is needed to explore whether this persists on the Myr-timescale).

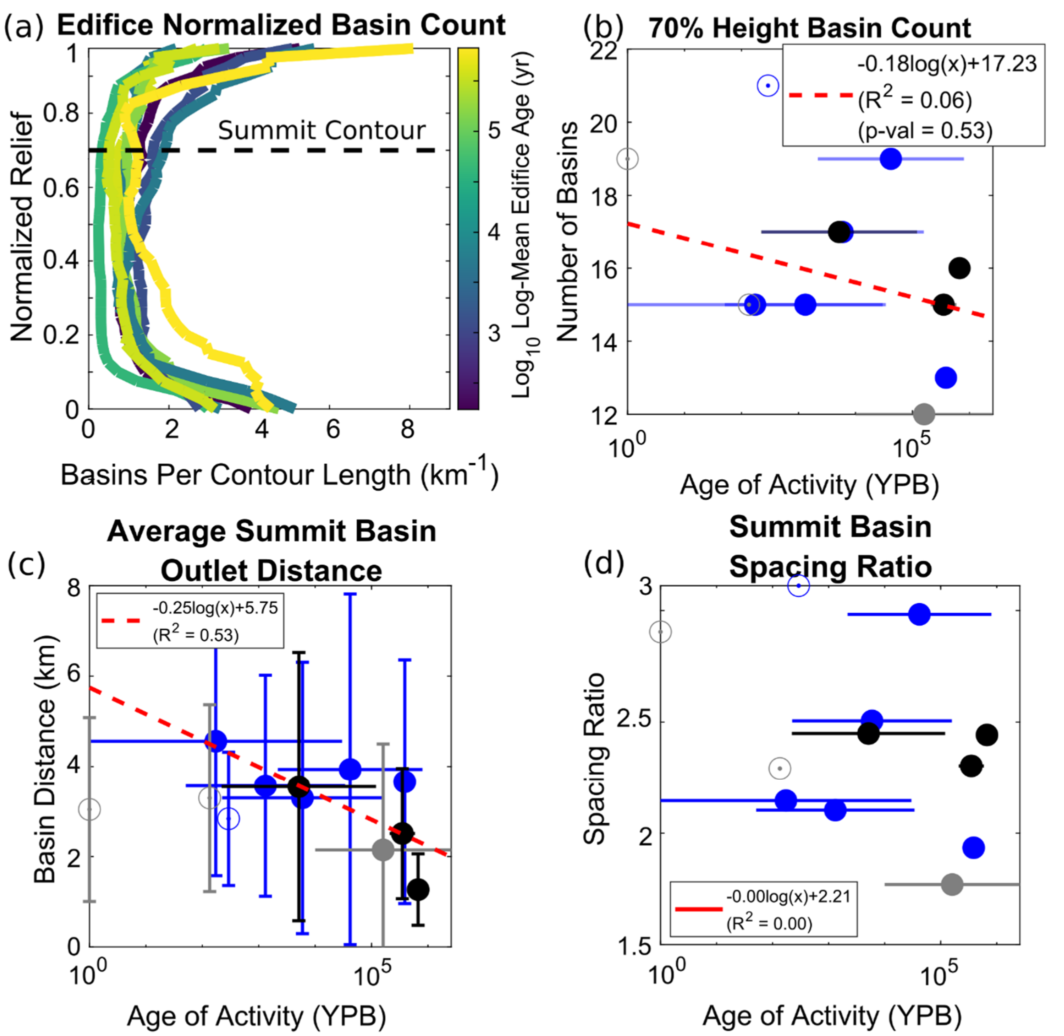

Figure 7 – a: Normalized number of basins along normalized relief for each volcano; colors are log-mean edifice age. b: Non-normalized number of summit basins (defined by the upper 30% of the edifice's height; black-dashed line of a) compared to log-mean edifice age. c: Average along-perimeter summit basin distance compared to edifice age. d: Summit basin spacing ratio (data from Fig. 4b divided by data from c) compared to edifice age. Colors and symbols in b-d are the same as Fig. 3.

An apparent contradiction occurs when comparing mean summit basin width angles to the number of summit basins. If all summit basins reached a width angle of ~60°, it would be expected that only ~6 basins would exist at the summit; however, Fig. 7b shows that the number of basins that reach the summit on all edifices is greater than 10. This difference is a consequence of how basin widths are calculated – by normalizing basin widths as an angle

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relative to the distance from the summit to the widest part of the basin, basins become normalized by different lengths corresponding to their widest regions. Indeed, as discussed in Section 5.2, divide asymmetry is most frequent in the mid- and lower-flanks of the edifice (Fig. 6), thus accommodating largest basin widths at different sections of the flank.

If the number of basins that reach the summit is time invariant, how does this translate to the circumferential spacing of their outlets at the base of the edifice? Hovius (1996) compiled the ratio between mountain belt half-widths (distance between the major divide and mountain front, W_M) and distances between major drainage basin outlets (those that reach the major divide; s) in 11 mountain ranges globally, and determined a globally-averaged spacing ratio (W_M / s) of ~ 2-3. We perform a similar analysis by dividing edifice effective radii by the average along-perimeter spacing between summit basin outlets. Figs 4b and 7c shows that while edifice effective radii decrease through time, so does the average perimeter distance between summit basin outlets. These behaviors thus combine to produce a relatively constant summit basin spacing ratio ~1.8 – 3.1 (Fig. 7d), consistent with Hovius (1996) as well as modeling studies of drainage patterns (Habousha et al., 2023). This suggests that while summit basins azimuthally expand their widths, the edifice is also decreasing in area as the landform erodes, thus decreasing the distances between summit basin outlets.

However, a different behavior emerges when considering basins by their radial distance relative to the edifice's peak (Fig. 8), which is more sensitive to the areal expansion of basins along the edifice's flank. Plotting the non-normalized number of basins as a function of radial distance (normalized by maximum radius for each edifice) and time shows a clear temporal trend (Fig. 8a), with younger edifices having more basins along all sections of the volcano (as schematized in Fig. 5). This trend becomes more apparent through the logarithmic regression between log-mean edifice age and the number of basins that exist at 30% radial distance from the peak (Fig. 8b), and at other normalized distances (Fig. S7). Conducting a similar outlet perimeter-distance analysis on these basins shows that the average distance between basin outlets is relatively constant at ~2 km (Fig. 8c), giving a strong (R^2 = 0.82) temporal decrease in basin spacing ratios (Fig. 8d). This behavior is similar to that described for the evolution of basin spacing on linear fault blocks (Talling et al., 1997) and is associated with the decreasing number of basins through time (driven by basin widening), highlighting the evolution and dynamics of radial drainage basins on volcanic edifices.

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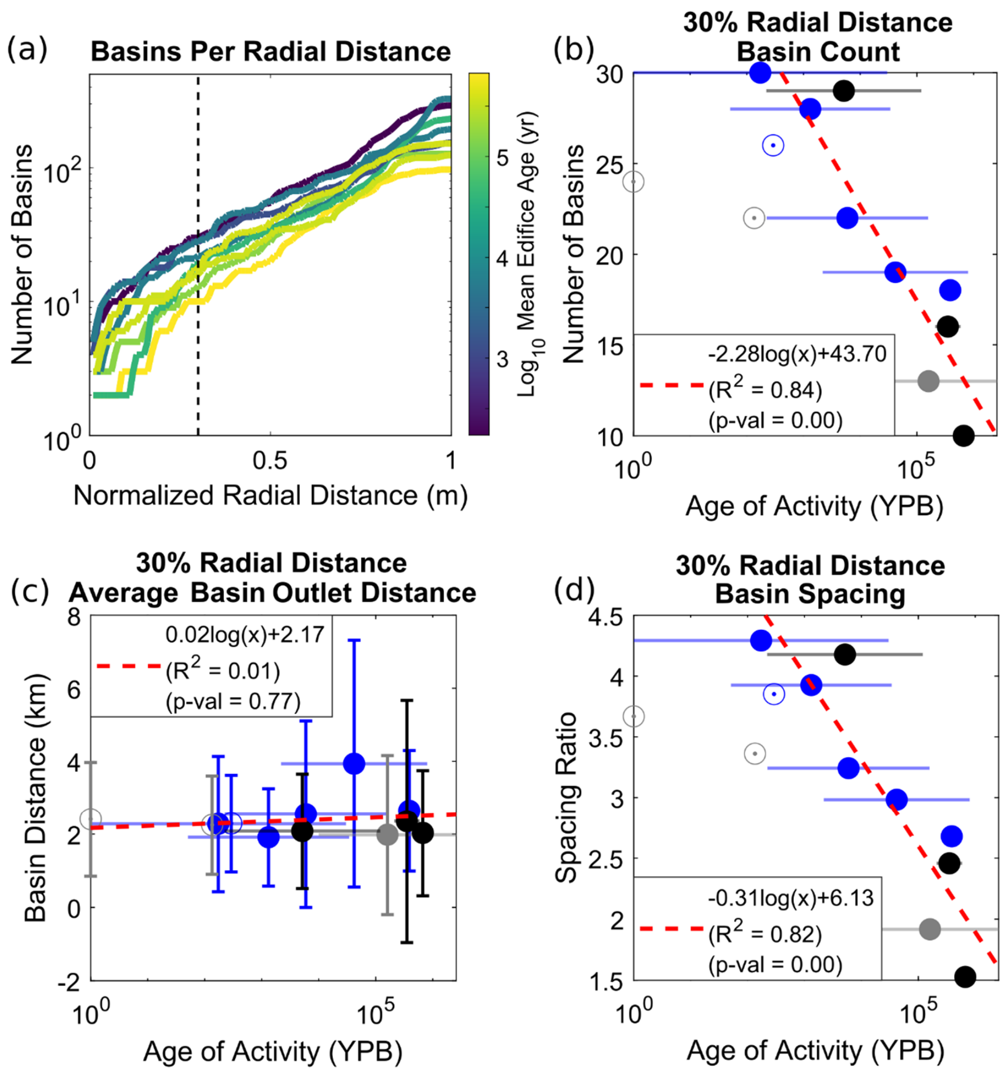

Figure 8 – a: Non-normalized number of basins as a function of normalized distance from the edifice's peak; colors are log-mean edifice age, black-dashed line represents 30% normalized distance from the edifice's peak. b: Non-normalized number of basins within 30% of the edifice's peak (black-dashed line of a) compared to log-mean edifice age. c: Average along-perimeter basin distance compared to edifice age. d: Basin spacing ratio (data from Fig. 4b divided by data from c) compared to edifice age. Colors and symbols in b-d are the same as Fig. 3.

4.4 Radial drainage basin area-length relationship

As a final observation for volcanic edifice drainage basins, we consider basin geometries in reference to Hack's power-law relationships between basin areas and lengths (Hack, 1957). Our analysis indicates that basins with drainage areas greater than 10^5 m^2 are well-fit by a power-law regression (Figs. 2b, 9a, c), whereas basins smaller than 10^5 m^2 have steeper trends between basin area and length, and are likely non-fluvial within the bounds of the edifice.

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Analyzing Hack's Law regressions for Merapi and Kaitake (Fig. 9), the relationships between spatial location and basin geometries become apparent. Basins that are less than 10^5 m^2 are constrained to the lowest regions of the edifice's flank, likely corresponding to non-channeled surfaces. Of those considered for the Hack's Law regression, the $\log_{10}$ basin length deviation (D_L) from the power-law is calculated as

$$D_L = \log_{10}(L_H(A)) - \log_{10}(L), \quad (9)$$

where L_H is the basin length of the Hack's Law regression from a given basin's area (A), and L is the basin's length. As expected from the geometric relationship, basins that fall below the power-law regression ($D_L < 0$) are wider, and those that are above the power-law regression ($D_L > 0$) are narrower.

Calculating D_L for basins with areas greater than our imposed channelization threshold (0.5 km^2), we do not observe any specific spatial pattern related to basins that deviate above or below the Hack's Law regression. However, one clear observation is the presence of highly-elongated basins on Merapi that exist on the mid- to upper-flanks and have D_L values > 0.2 (Fig. 9b). These basins appear wedged or pinched between larger basins and would be expected to not have as much growth potential compared to their wider neighbors. Elongated basins also exist on Kaitake; however, they do not have as high of a deviation (maximum $D_L \approx 0.1$; Fig. 9d). This may be a product of the lower number of basins that exist on Kaitake, or the overall lower amount of drainage area that Kaitake basins occupy, decreasing the amount of variability from the power law relationship. On both Merapi and Kaitake, these elongated basins may further highlight the dynamics of basin competition on radial structures – through drainage divide migration and areal loss (likely influenced by edifice-scale sector collapses or regrowth events; Gertisser et al., 2023), less-erosive and lower-order drainages become passive players to more dominant basins and adopt non-standard geometries, becoming narrow, chute-like basins on the mid- and upper-flanks. The generation of these narrow, 'nested' basins has also been observed to occur in response to differential tectonic uplift within analog and numerical experiments (Habousha et al., 2023).

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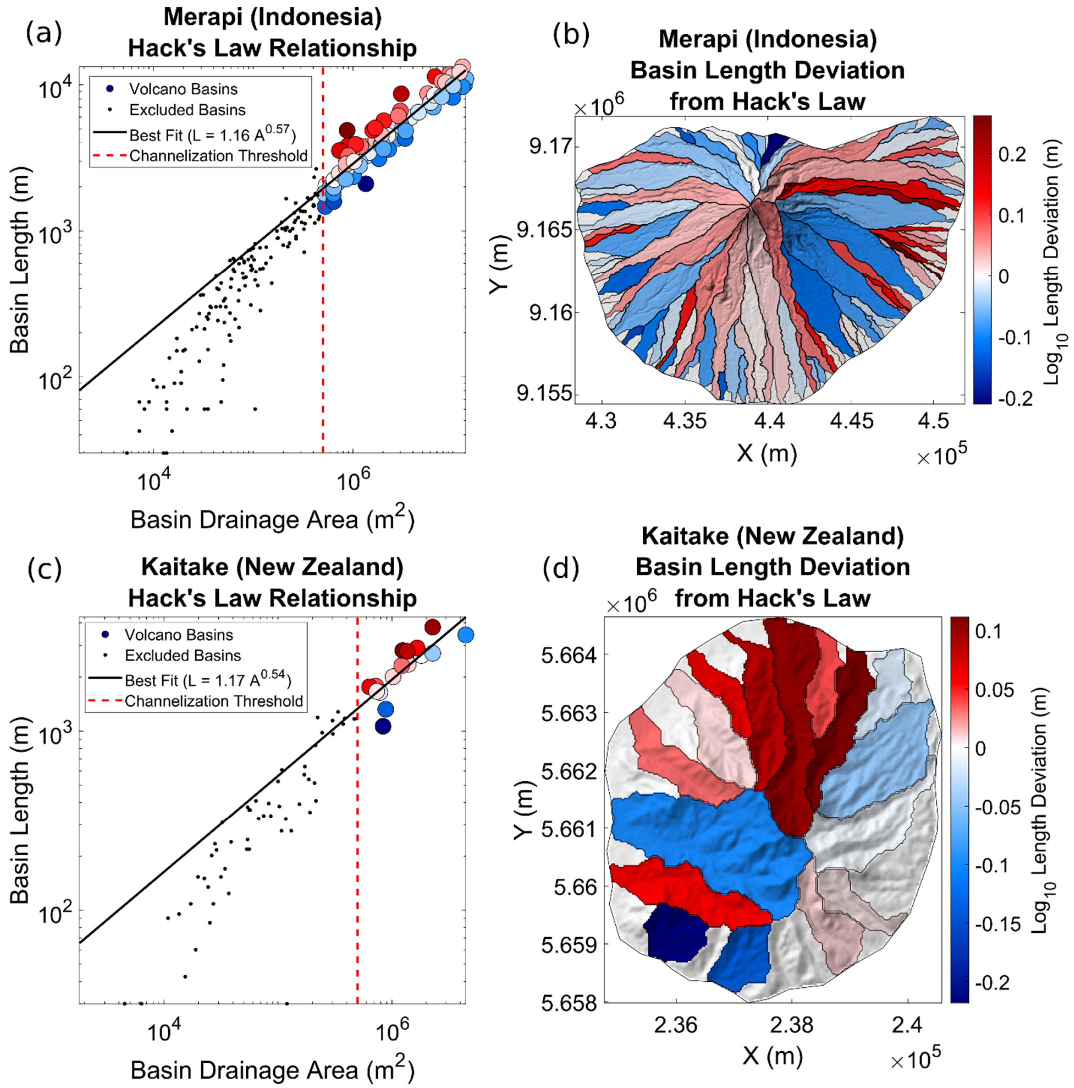

Figure 9 – Hack's Law analysis of (a-b) Merapi and (c-d) Kaitake. a, c: Basin drainage area – length relationships. Black lines represent Hack's Law regressions. Colored circles correspond to the deviation from the regression trend (eq. 9), associated with the color bars in b and d. Red-dashed line is imposed 0.5 km^2 channelization threshold, black dots are basins less than the threshold and excluded from the regression. b, d: Maps showing the deviation of each basin from the best-fit power-law regression.

4.5 How do radial drainages compare to other settings?

Thus far, our discussion has focused on deriving a foundational understanding of how radial drainages on volcanic edifices evolve and compete. However, we note similarities between our interpretation and those from previous studies in other drainage settings. This leads to a simple question – is there a significant difference between radial and dendritic drainage development and evolution?

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Our results show that basin formation on edifices follows the development of rills and gullies within badlands (Schumm, 1956). As radial drainages evolve and certain basins expand to become dominant features on the edifice, less-dominant basins become passive and are pushed down-flank as nested basins, often adhering to non-standard geometries as imposed by their more-dominant neighbors (Habousha et al., 2023; Beeson and McCoy, 2022). The dynamics of this basin competition and formation of nested basins is demonstrated by edifice basin spacing ratios. Summit basins on edifices have spacing ratios that appear time-independent and fit within the range of values observed in linear mountain ranges globally (Hovius, 1996) (Fig. 7), suggesting the spacing of these basins is set during the initial stages of basin formation – an attribute of basin evolution that has been shown to occur on linear fault blocks (Talling et al., 1997; Habousha et al., 2023); however, basins that are within a radial distance from the summit that is 30% of the edifice's maximum radius do experience a temporally-decreasing spacing ratio and constant distance between outlets (Fig. 8), capturing the development of a basin topographic hierarchy along the edifice – a behavior not previously observed. Finally, our drainage divide analysis on volcanic edifices suggest that radial drainage basins evolve towards a stable basin configuration as topography matures towards a dynamic equilibrium, similar to regional landscape evolution globally (e.g., Perron and Royden, 2013; Willett et al., 2014).

This comparison suggests that drainage development and evolution on radial structures are largely similar to those occurring within linear mountain settings. However, some differences still occur, particularly in relation to basin geometries imposed by the larger-scale, radial primary landform. Dendritic drainages in linear mountain belts and fault blocks are characterized by their leaf-like geometries (e.g., Zernitz, 1932; Strahler, 1952; Talling et al., 1997), having a broad headwater region that decreases towards the outlet to a tapered point. Although radial drainages also have tapered outlets and basin widths increase upstream, these widths are hindered by the conical geometry of the primary landform and convergence of multiple basins towards the summit, leading to a tapered headwater as well as a tapered outlet. This geometric constraint is well-demonstrated by the drainages on Merapi (Fig. 9b), where summit basins are generally widest on the lower- or mid-flanks; however, this trend is not as obvious on Kaitake (Fig. 9d), where erosion has dissected the landform and weakened the conical influence of the edifice on basin geometries. Furthermore, as edifice drainages are limited to an isolated, conical landform, their evolution and configuration are constrained by a cumulative areal limit. As opposed to linear mountain ranges (where a morphologic change in one basin impacts its neighbors, which then impacts their neighbors as a cascading chain across the landscape), on volcanic edifices, a morphologic change in one basin (particularly a dominant basin) may directly impact the erosional state and morphology of most other basins on the landform due to the high number of basins that may share a divide with this basin. This areal effect on radial basin evolution may be further augmented by the higher diversity of underlying host rocks between edifice basins associated with magmatic and volcanic products (e.g., tephra deposits, lava flows, intrusions) that is not as prevalent within linear mountain ranges.

Despite the differences in basin geometries and interactions discussed above, edifice-averaged morphometric values (e.g., Hack's Law exponent, drainage density, mean basin hypsometry, mean basin slopes) are similar to those of other settings (Hack, 1957; Strahler, 1952; Horton, 1945). This suggests that although radial drainages experience phenomena that differ from those typically experienced in dendritic settings, drainage development, geometries, and

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competition largely follow those of dendritic patterns. As volcanic surfaces are easily datable and their ages can often vary by orders magnitude on a single edifice, volcanoes represent ideal locations for studying terrain evolution over varying temporal scales within a general framework.

4.6 Basin morphology capturing volcanic processes

In this study, we considered edifice morphologies using mean values over the entire edifice. However, our metrics also allow for the comparison of basin morphologies on a single edifice. Variations associated with these metrics would likely relate to spatially-localized attributes of aggradation, degradation, and climate, and would thus provide a quantitative method to disentangle these signals using topography. For example, edifice flanks that have been resurfaced by large volcanic deposits or destroyed by sector collapses should exhibit younger drainage networks according to the metrics explored here that differ from other parts of the volcano. Furthermore, alterations to the erosional efficiency of a basin by tephra accumulation or lava flow emplacement should create spatial variability that can be quantified by similar analyses. These concepts should be tested over well-constrained cases and would be beneficial for both preliminary fieldwork and to approximate relative volcanic chronologies remotely. Our model for edifice degradation, radial drainage evolution, and divide stability thus provides a first step to deconvolving the various signals that relate to edifice morphology. This presents new avenues of exploration for the volcanology community to interrogate volcanic histories from topography, and for the geomorphic community to investigate surface evolution on landforms that often fall outside standard tectonic studies.

5.0 Conclusion

Volcanic edifices represent a class of primary landforms whose erosion remains relatively unexplored. We analyzed the degradational histories of volcanic edifices using a set of metrics that have not previously been considered for radial drainage networks. We show that these metrics relate to the overall age of a volcano and propose a new general model for the temporal evolution of edifice drainage morphology. Divide stability analysis underscores the dynamic nature of basin evolution, and suggests radial drainage networks initiate with nearly-uniform geometries and unstable configurations that evolve towards non-uniform basin geometries and more stable configurations to generate a basin topographic hierarchy on volcanoes. Finally, comparing basin geometries, configurations, and outlet spacing between basins that exist on volcanic edifices to those that exist on linear mountain ranges highlights similarities and differences between radial and dendritic drainage basins.

6.0 Code availability

DrainageVolc and MorVolc codes are available at https://github.com/danjohara/Volc_Packages.

7.0 Data availability

Collected edifice data is included in the supplement as both an Excel file and shapefile.

8.0 Author contribution

All authors provided editorial advice on the manuscript. DO'H wrote the DrainageVolc and updated MorVolc codes, conducted the morphology analyses, and wrote the manuscript. RMJvW assisted in data collection, determined edifice boundaries from topography, and tested DrainageVolc/MorVolc. LG and BC gave advice on drainage basin morphology and evolution, while PG, PL, and GK provided insight on volcanic edifice morphology, evolution, and general volcano ages. MK secured funds and coordinated the project, giving advice on the research direction, analyses, and interpretation.

9.0 Competing interests

The authors declare that they have no conflict of interest.

10.0 Acknowledgement

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