

Coevolving edge rounding and shape of glacial erratics; the case of Shap granite, UK

Paul A. Carling¹

¹School of Geography and Environmental Science, University of Southampton, Southampton, SO17
1BJ, UK

Correspondence to: Paul A. Carling (p.a.carling@soton.ac.uk)

Abstract

The size distributions and the shapes of detrital rock clasts can shed light on the environmental history of the clast assemblages and the processes responsible for clast comminution. For example, mechanical fracture due to the stresses imposed on a basal rock surface by a body of flowing glacial ice releases initial 'parent' shapes of large blocks of rock from outcrop, which then are modified by the mechanics of abrasion and fracture during subglacial transport. The latter processes produce subsequent generations of shapes, possibly distinct in form from the parent blocks. Lacking is a complete understanding of both the processes responsible for block shape changes and the trends in shape adjustment with time and distance away from the source outcrop. Field data on edge rounding and shape changes of Shap granite blocks (dispersed by Devensian ice eastwards from outcrop) are used herein to explore the systematic changes in block form with distance from the outcrop.

The degree of edge rounding for individual blocks increases in a punctuated fashion with the distance from the outcrop as blocks fracture repeatedly to introduce new fresh unrounded edges. In contrast, block shape is conservative, with parent blocks fracturing to produce self-similar 'child' shapes with distance. Measured block shapes evolve in accord with two well-known models for block fracture mechanics — 1) stochastic and 2) silver ratio models — towards one or other of these two attractor states. Progressive reduction in block size, in accord with fracture mechanics, reflects the fact that most blocks were transported at the sole of the ice mass and were subject to the compressive and tensile forces of the ice acting on the stoss surfaces of blocks lying against a bedrock or till surface. The interpretations might apply to a range of homogeneous hard rock lithologies.

Short Summary

Edge rounding in Shap granite glacial transported boulders is an irregular function of distance from the source outcrop in northern England, UK. Block shape is conservative, evolving according to block fracture mechanics — stochastic and silver ratio models — towards either of two attractor states. Progressive reduction in size occurs to blocks transported at the sole of the ice mass where the blocks are subject to the compressive and tensile forces of the ice acting against a bedrock or till surface.

Key words

Glacial erratics, erratic rounding, erratic shape, fracture, subglacial

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1 Introduction

The concentration, size, shape, and the degree of rounding of glacial ice-transported blocks of rock may change with distance from the source outcrop. Spatial trends in concentration have been used frequently to indicate preferred ice flow directions (Kujansuu and Saarnisto, 1990; Evans, 2007, Benn and Evans, 2011, p. 675). Concentrated bands of ice-freighted erratics are referred to as ‘indicator plumes’, ‘indicator trains’ or ‘indicator fans’, with concentrations dropping off rapidly outside of the plumes due to ice-flow induced dispersion (Larson and Mooers, 2004). None-the-less, concentration is also sustained by comminution, whereby blocks fracture, or abrade to form smaller blocks and fragments through time and distance from the source outcrop. In contrast to dispersion, there has been less focus on changes in size, shape, and edge-rounding with distance from source (Benn and Evans, 2011). The changes in the shape of blocks are functions of the mechanical properties of the blocks, primarily rock strength and structure, as well as the physical processes promoting comminution. A change in block shape also represents a change in block size. To explore the controls on edge rounding and the shape of erratics, dispersal from a well-known exposure of the Shap granite (Sg) in the UK was examined in the present study. Improved understanding of process controls related to edge rounding and fracture should shed light on the associated basal ice dynamics related to block form changes generally. The two key issues are: 1) the relative importance of fracture mechanics in reducing block size in contrast to edge-rounding and 2) whether edge-rounding and shape coevolve with distance from the source outcrop.

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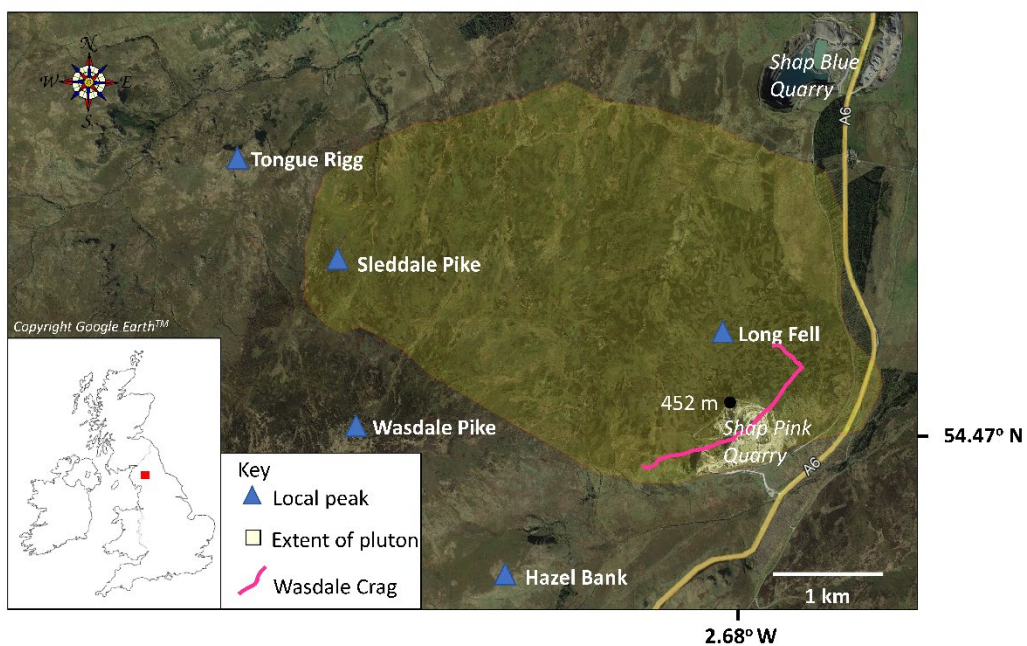
1.1 The Study Area and Context of the Study

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The exposure of the Sg pluton occupies a small area (c., 7 km²) in the eastern English Lake District (Fig. 1) defining a distinct, small, source area for granite blocks. The variation in the concentrations of Sg blocks with distance from the pluton has been used as a key indicator of the directions of ice

74 movement across northern England (reviewed by Carling *et al.*, 2013) during the Dimlington Stadial
 75 (c., 29 ka BP to 14.7 ka BP) within the Last Glacial Period (c., 115 ka BP to 11.7 ka BP; Rose, 1985;
 76 Scourse *et al.*, 2009; Chiverrell and Thomas, 2010; Davies *et al.*, 2019; Clark *et al.*, 2022). Around the
 77 Last Glacial Maximum (LGM: 26.5 ka BP to 19 ka BP, Clark *et al.*, 2009), the region was covered by ice,
 78 several hundred metres thick (Evans *et al.*, 2009), and Sg blocks were entrained from the subglacial
 79 bedrock (Ugelgiv *et al.*, 2016). Long Fell, on the eastern margin of the exposed pluton, is a kilometre-
 80 scale *r*oches moutonnées, severely ice-plucked in the east and south-east at Wasdale Crag (Fig. 1), with
 81 smooth, ice-planed surfaces occurring to the north, west and on the summit (point 452 m above sea
 82 level), indicating the erosional effects of moving ice and debris (Hallet, 1981). The west to east change
 83 in the style of erosion, from smoothing to plucking, is consistent with ice in the vicinity of the pluton
 84 moving predominately to the east in an early phase (c., 29-25 ka BP; Livingstone *et al.*, 2012; Merritt
 85 *et al.*, 2019) of the Dimlington Stadial, and generally northwards across the pluton subsequent to 22
 86 ka BP, *i.e.* towards the end of the LGM (Livingstone *et al.*, 2012; Merritt *et al.*, 2019); the latter
 87 supposition consistent with the W.S.W. to E.N.E. orientation of glacial striations on the pluton
 88 (Nicholson, 1868).

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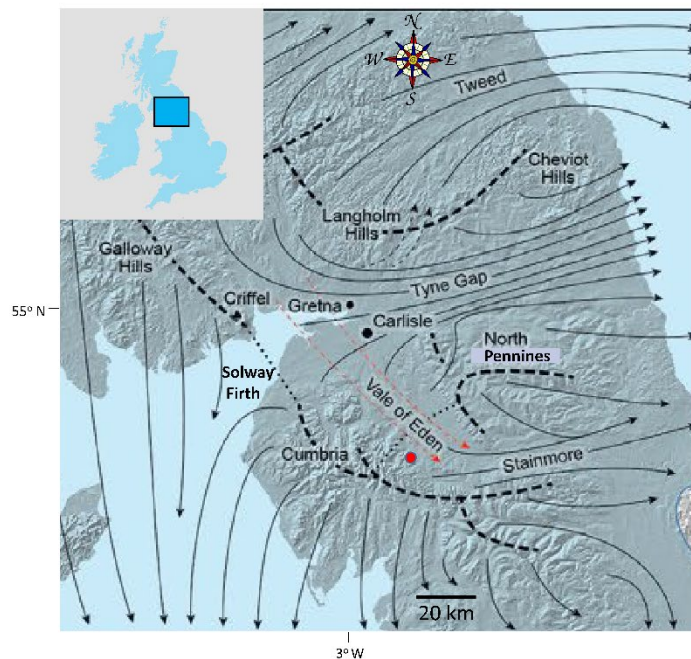
91 *Figure 1: Location of the Shap granite pluton relative to the A6 highway. The central portion of the*
92 *ice-plucked outcrop (Wasdale Crag) crag has been destroyed by quarrying. Spot height elevation is*
93 *metres above sea level. Base map is from Google Earth™. Approximate extent of the Shap Granite*
94 *pluton outcrop from the British Geological Survey ([https://www.bgs.ac.uk/map-viewers/geoindex-](https://www.bgs.ac.uk/map-viewers/geoindex-onshore/)*
95 *onshore/).*
96

97 In terms of concentration, the dominant dispersal of Sg erratics, during the early phase of the
98 Dimlington Stadial (Stage I; c., 29-25 ka BP; Merritt *et al.*, 2019) was eastward (Carling *et al.*, 2013)
99 within sustained ice flow through the topographically controlled corridor of the Stainmore gap across
100 the North Pennines hills (Fig. 2A). The plume extended as far as the east coast of England; a distance
101 more than 100 km (Fig. 3). Block size tends to diminish with distance, although examples of far-
102 travelled large blocks occur sparingly (Carling *et al.*, 2023). Due to shifting ice divides and competing
103 ice dispersal centres (Evans *et al.*, 2009; Merritt *et al.*, 2019), subsequently two Sg plumes dispersed
104 in southerly directions until, in the late stadial, erratics briefly were dispersed northwards from the
105 vicinity of the pluton (Carling *et al.*, 2013) in accord with the ice movements reported by Livingstone
106 *et al.* (2012). These latter dispersal directions are not considered further herein. The focus solely is
107 on those erratics the final transport vectors (direction and distance) which are roughly due east,
108 defining a simple linear direction over which changes in the nature of the erratic populations might be
109 measured.

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111 Less well understood than directions of travel and changes in concentration, is the process of edge-
112 rounding and shape changes of Sg blocks that accompany size reduction. The granite is an ideal choice
113 for study as the composition and texture is uniform (Grantham, 1928), mostly giving a massive,
114 unlayered, structure to individual blocks. Layering, such as found within sedimentary rocks, would
115 add complexity to the study of shape evolution, which is avoided in this study. Hopkins (1849) had
116 commented briefly on the rounding of Sg blocks (density ~ 2.61 tonnes m^{-3}) as size reduces towards
117 the east coast, yet such rapid changes in form are seemingly at odds with the high strength of the rock.
118 The strength of Sg in compression exceeds 207 MPa (Holland, 1959;

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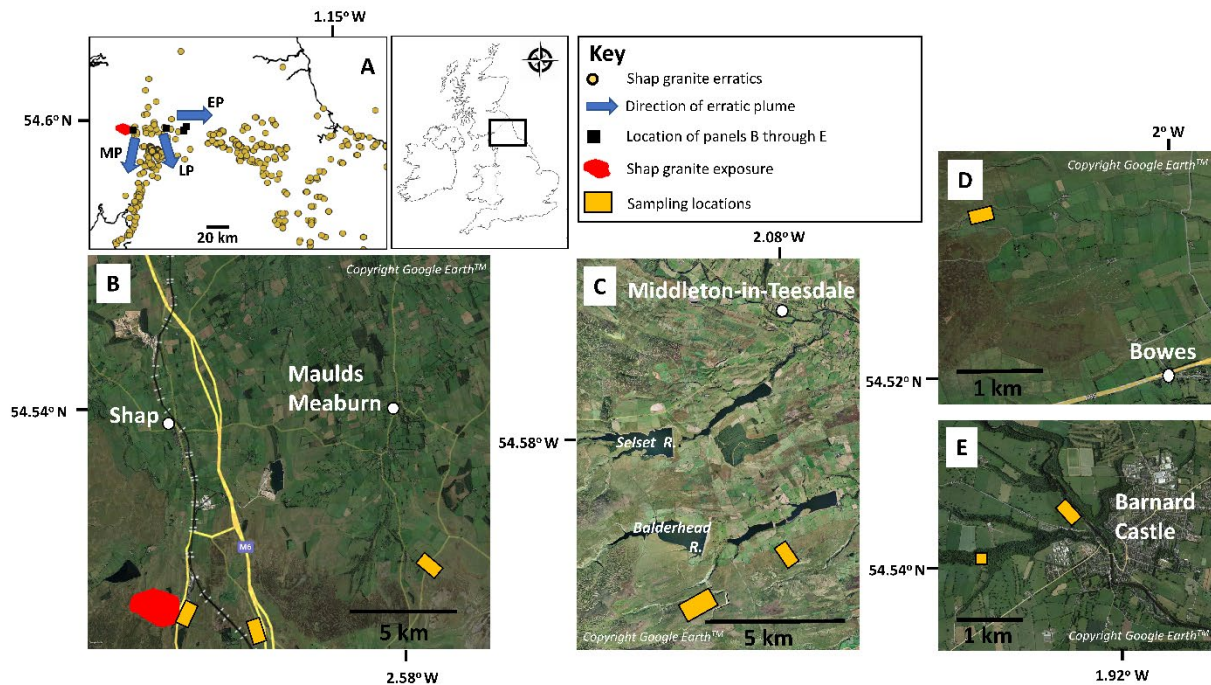
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123 *Figure 2: Ice flow directions for Stage I (29-25 ka BP) of the last British-Irish Ice Sheet around the Solway*
 124 *Firth (from Merritt et al., 2019. Reproduced with permission) in northern England (inset panel).*
 125 *Eastward ice flow through prominent topographic corridors occurs across the North Pennines. Broken*
 126 *and dotted black lines refer to ice divides. Black arrows indicate ice-flow vectors (dotted red arrows*
 127 *indicate alternative ice-flow scenarios). Topography from NEXTMap digital elevation data. Shap*
 128 *granite erratic plume dispersed to the east from the pluton (red dot) chiefly over Stainmore (see Fig 3).*
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130 Day and Goudie, 1977; Goudie, 2006) such that the rock is considered ‘very strong’ (British Standards,
 131 1981). Despite the rock strength, Hodgson (1870) had remarked on how seemingly rapid rounding of
 132 granite might be aided by rock friability due to a high mica content associated primarily with biotite
 133 (Firman, 1953). Biotite is soft compared with the large phenocrysts of feldspars and quartz (Firman,
 134 1953) that dominate the granite composition. Nevertheless, there has been no investigation of the
 135 changes in shape and rounding of Sg blocks with distance from the source; with very few granite blocks
 136 visually maintaining significant mass over tens of km. A study of blocks exposed on the modern land
 137 surface, away from major watercourses, should reveal rock-wear processes associated with glacial
 138 transport as there has been negligible losses to Sg surfaces due to post-glacial subaerial weathering
 139 (Wager, 1944; Parsons and Lee, 2005). The few weathered examples of blocks exhibit phenocrysts
 140 standing proud (3-5 mm) of the matrix, as the mica is readily subject to chemical weathering if *buried*

141 but the feldspars are not much altered (Wager, 1944). Consequently, an hypothesis was proposed:
 142 ‘Sg ice-transported blocks would display systematic changes in edge-rounding and shape’; with an aim
 143 ‘to demonstrate if edge rounding and shape coevolve with distance to the east from the pluton’.



144
 145 *Figure 3: A) Spatial distribution of examples of Shap granite erratics within the study area,*
 146 *northern England (inset), showing the early easterly-directed plume (EP) and the later southerly*
 147 *Mint and Lune plumes (MP and LP) relative to the source outcrop of Shap granite. Locations*
 148 *shown within panel A are indicative of the general sampling areas of: B) Wasdale Bridge,*
 149 *Haybanks, Blasterfield; C) upper Teesdale; D) Levy Pool; E) Barnard Castle. See main text for*
 150 *details. Base maps copyright Google Earth™.*

151 Shape (and size) changes in a Shap granite block occur due to three predominant processes which
 152 scale from affecting small areas of a block to larger areas:

- 153
- 154 1) abrasion, whereby grain-size fragments (*e.g.*, phenocrysts) are ground-off the block surface
 155 (Haldorsen, 1981; Benn and Evans, 2011) primarily by shear stresses associated with blocks
 156 moving across a bedrock or till surface in the direction of basal ice motion, or by ice and till
 157 moving over stationary blocks lodged against the substratum - this process can result in
 158 distinct rounded surfaces on a block (Boulton, 1978; Hallet, 1979);

159

160 2) spallation, whereby flakes of rock are freed from the surface of the block (Olsen, 1983) due
161 to externally-derived and internally-derived tensile deviatoric stresses in the rock, both
162 imposed by the motion of the ice overburden, with the shear stresses acting on planes at less
163 than the block scale (Li *et al.*, 2018) – this process reduces block mass but results in localized
164 scarred surfaces;

165

166 3) fracture (Buscarnera and Einav, 2021) whereby the ‘parent’ block splits into substantial
167 parts (often two; here referred to as ‘child’ products). The propagating fissure ultimately may
168 be due to compression loading but, at the block surface, it is the result of a tensile stress
169 (acting on a plane at block scale) flexing the stoss surface of a brittle block lying on a hard
170 basal surface, leading to fissure development often transverse to the direction of basal ice
171 motion (Morland and Boulton, 1975; Hallet, 1996; Benn and Evans, 2011, p. 264). The tensile
172 strength of a rock is typically an order of magnitude less than the compressive strength (Li *et*
173 *al.*, 2018). This tripartite classification informed the Method.

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175 To address the hypothesis, the focus of the study is abrasion and fracture, but observations on
176 spallation were obtained for completeness, with the latter results reported within Supplementary
177 Information section 2.1. There is justification from studies of bedrock outcrop erosion by basal ice
178 that both the degree of abrasion of bedrock surfaces and the number of fracture events are related
179 to time in transport (Cohen *et al.*, 2006) and thus the distance erratics are moved.

180

181 **2 Method**

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183 Shap granite blocks were sampled along a west to east transect, starting from below Wasdale Crag. It
184 was assumed that all the sampled blocks were from the same population subject to basal traction
185 transport (*vis.* Boulton, 1978) for much of the transport histories; the population being a coarser

186 component of a subglacial traction till (*sensu* Evans *et al.*, 2006) deposited during the waning of the
187 easterly phase of ice motion (Fig. 3A) (Hallet, 1979). Blocks ($L > c.$, 1.0 m) were located by field walking.
188 Locations sampled include Wasdale Old Bridge, Haybanks, Blasterfield, sites near Barnard Castle in
189 Teesdale and Levy Pool near Brough (Table S1), respectively 0.8 km, 3.5 km, 8.4 km, *c.*, 36 km and *c.*,
190 41 km from the Wasdale Crag outcrop (Fig. 3). From preliminary site survey, the sites selected were
191 known to have sufficient erratics within defined areas for sampling. However, to obtain similar sample
192 sizes, the areas searched for the final two locations necessarily increased as the surface density of
193 blocks decreased eastwards. Examples of erratics were selected that were sitting on exposed bedrock
194 or till surfaces, so as not to be partially buried. Distance from the source outcrop is assumed to relate
195 to time in transport.

196 At each location, edge, and shape measurements and scar enumeration were made on thirty blocks
197 as briefly described below; the full procedure developed within Supplementary Information. The
198 sample size was found to be sufficient (Daniel, 1999; Conroy, 2018) for the aims of the project and,
199 moreover, interpretation of data trends became possible once the sample size, n , reached 30 at each
200 location. These data were supplemented by a regional shape data compendium (Carling *et al.*, 2013).
201 Changes in block size with distance from the pluton are not considered herein using field data, as a
202 statistically significant sample size at each location would have to be prohibitively large to reflect the
203 complete size range of blocks. Rather block size changes are considered within a theoretical
204 framework related to shape changes. Blocks are considered as cuboids consisting of *faces* and *edges*.

205
206 In accord with 1) abrasion: edge rounding was measured after Wentworth (1923; Kirkbride, 1985). In
207 brief, each of the three most tightly rounded edges on the visible portion of each block was defined
208 by a chord (l), delimiting a segment of the block beneath each rounded edge, to give between 80 and
209 90 values for each location. Consideration of the height (h) of the segment in relation to the chord
210 length constrains the radius (r_c) of an inscribed circle beneath the rounded edge (see Fig. S2 in
211 Supplementary Information section 1.4), which radius is a measure of the degree of rounding:

212

213

$$r_c = \frac{l^2}{8h} + \frac{h}{2} \quad (1)$$

214

215 The radius of curvature reduces as the chord length reduces towards zero and often a right-angle
216 corner occurs when r_c approaches 0. More rounded blocks have larger radii of curvature than less
217 rounded blocks as the sizes of the inscribed circles increase as edges become less sharp. In similar
218 fashion, the edge rounding was measured for joints bounding *in situ* Shap granite blocks constituting
219 the outcrop of Wasdale Crag. These latter data provide a base line of the degree of edge rounding of
220 blocks which have been subject to ice abrasion in place, but without subsequent transport.

221

222 To consider 3) shape changes by fracture: from initial field reconnaissance, blocks close to the source
223 often appear cubic, but polyhedrons occur sparingly - ranging from wedges to prismaticoids. Further
224 from the source more ellipsoidal forms are evident. Consequently, to obtain an indication of the shape
225 of a cuboid or an ellipsoid block (Fig. S1), the lengths of the three orthogonal axes: long axis (L);
226 medium axis (M) and the short axis (S) were recorded in the field – polyhedrons were not sampled –
227 to give *c.*, 30 values for each location. Consideration of the mechanics of shape changes also sheds
228 light on the size reduction process with distance. Fracture within individual blocks is sometimes
229 associated with joints and other block-scale planes of weakness. Yet, ice compressive force is the
230 predominant mechanism for significant progressive change in shape for homogeneous granite blocks,
231 inducing tensile fracture and block size reduction. Shape and size changes were examined either via
232 a stochastic fracture model, applicable to fracture at right-angles to either of the L , M or S axes
233 (Domokos *et al.*, 2015) of ellipsoidal blocks or, in accord with the silver ratio model applicable to
234 cuboid blocks fracturing across the M -axis alone (Buscarnera and Einav, 2021), as is explained in the
235 Results. Shape indices are reported in the main text using the Zingg (1935) projection, whilst an
236 example of a simple ternary diagram (Fig. S3, after Hofmann, 1994) is provided in Supplementary
237 Information section 1.5.

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239 3 Results

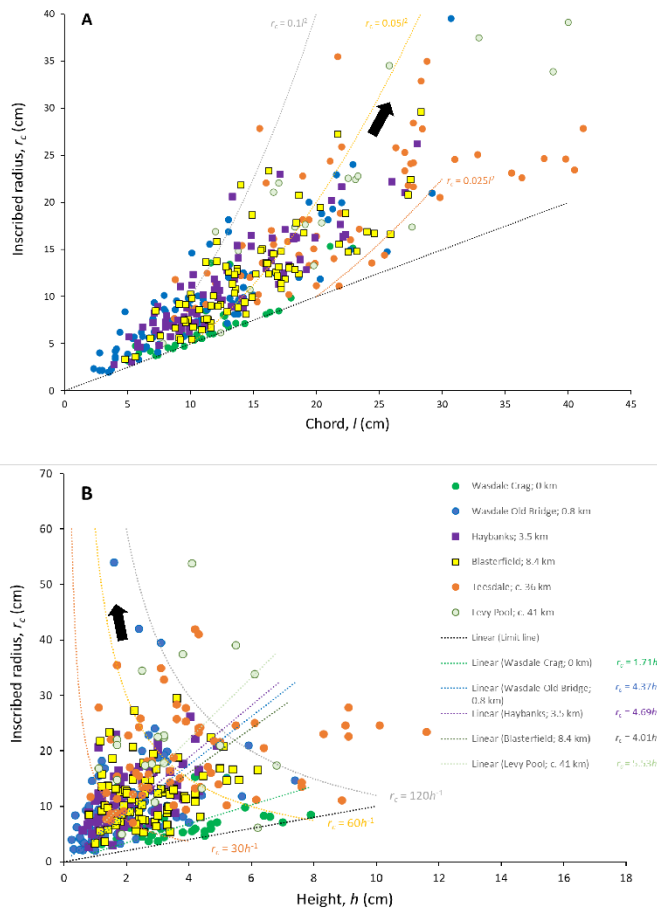
240 3.1 Edge rounding

241 As is evident from the form of equation 1, rounding is a positive function of the square of the length
242 of the chord of the segment, l , and an inverse function of the segment height, h (Fig. 4). As the
243 inscribed radius values are obtained from both the values of l and h (Equation 1), there is an element
244 of co-variance between the two axes in both panels A and B of Fig. 4. However, plotting the data in
245 this manner allows ready visualization of the trends of the radius data (r_c) relative to the variation in
246 the controlling parameters (l, h). Lower limits to data plotting positions occur in both panels equal to:
247 $r_c = l/2$ and $r_c = h$ respectively.

248 The joint rounding on the pluton is less developed in comparison with the rounding of edges of blocks
249 only 0.8 km away at Wasdale Old Bridge (Fig. 4). Although the range in heights of the segments are
250 similar for both locations, the range in chord lengths for the pluton includes smaller values giving
251 overall 'sharper' edge profiles for the pluton joints in contrast to the Wasdale Old Bridge blocks. It is
252 evident that any 'parent' blocks newly entrained from the outcrop will exhibit both lightly rounded
253 joint edges (glacially abraded when *in situ*) as well as sharp, fresh edges, the latter due to fracture
254 upon release from the outcrop. However, although the initial lightly rounded edges can be further
255 rounded with distance, fracture of entrained blocks introduces new 'sharp' edges as detailed next.

256 Although as distance increases larger radii are more frequent, small radii also occur at distance (Fig.
257 4). It is unlikely that small radii can survive abrasive transport over several tens of km from the pluton,
258 rather repeated fracture introduces new sharp edges and thus new small radii to different generations
259 of blocks. These new sharp edges begin to round far from the pluton. Although the plots of Fig. 4 are
260 developed considering singular data points from many blocks, if the trends are considered to
261 represent the rounding evolution that would occur for individual blocks, then the black arrows indicate
262 the general direction of edge rounding evolution (*i.e.*, Fig. 4 panel A: if h is constant and l is variable;

263 panel B: if l is constant and h is variable). The linear functions in Fig. 4B allow ready comparison
 264 between locations such that, for any value of h , the degree of edge rounding is more pronounced with
 265 distance from the pluton; specifically, the linear curves (green, blue, purple, and red) have increasing
 266 values of the constant (*i.e.*, 1.71, 4.37, 4.69; 5.53 respectively). Similar linear functions for values of l
 267 can be applied to Fig. 4A but, for the sake of clarity, these curves are not plotted. The detail of edge



268

269 *Figure 4: Trends in the values of the inscribed radius as a function of: A) chord length, and B) segment*
 270 *height. Black arrows indicate the direction of travel of the hypothetical function for an individual block*
 271 *(see main text). Examples of hypothetical curves (brown, yellow and grey) for the trends in individual*
 272 *clast evolution are given for both $r_c \propto l^2$ and $r_c \propto h^{-1}$. Key to symbols in panel B also applies to*
 273 *panel A.*

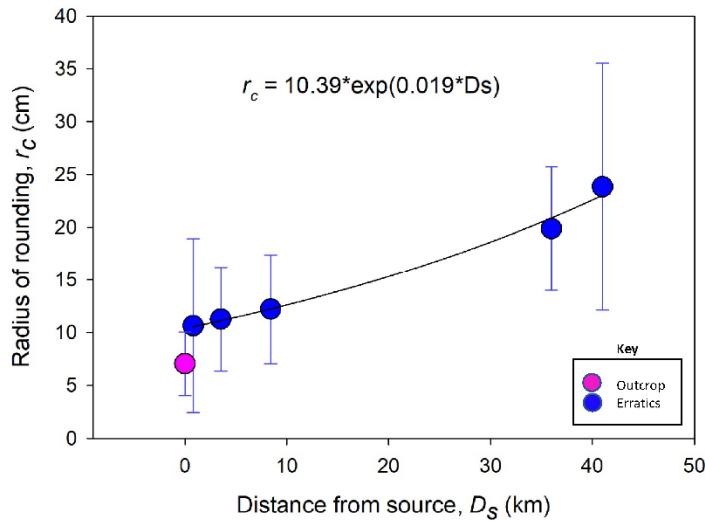
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275 rounding is considered within the Discussion, as edge-rounding of individual blocks is not a smooth

276 function of distance from the source as might be inferred from the black arrows in Fig. 4 and from

277 mean radius of edge rounding with distance from the outcrop (Fig. 5). The latter figure depicts an
 278 exponential increase in the mean radius of curvature with distance (D_s) from the source outcrop:

279
$$r_c = 10.3881e^{(0.0194D_s)} \quad (2)$$



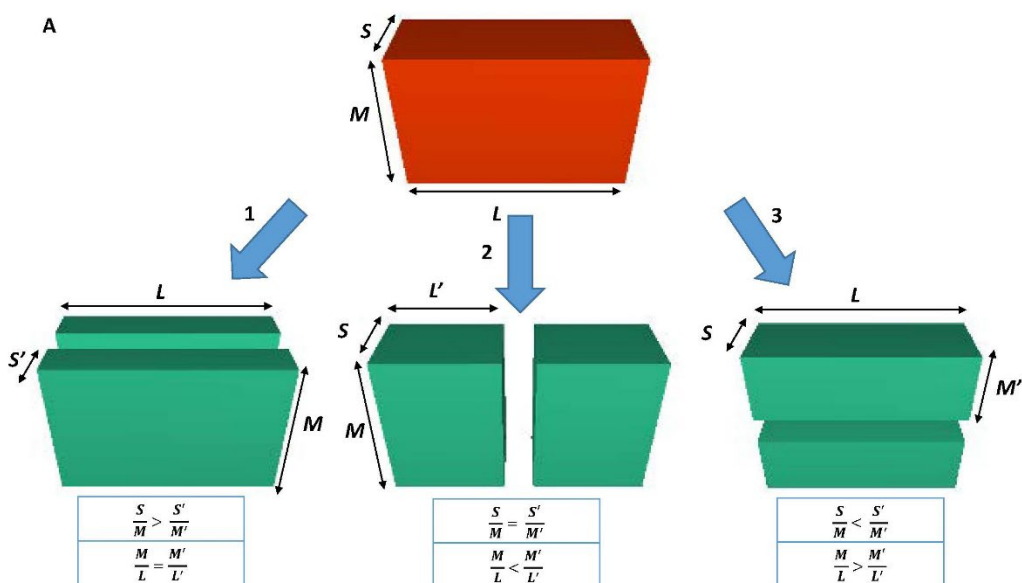
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281 *Figure 5: Mean values and s.d. of edge rounding as a function of distance from outcrop.*

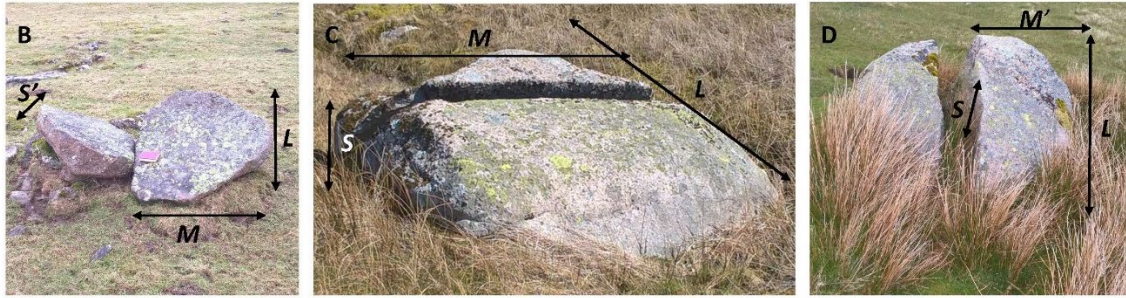
282 **3.2 Shape evolution**

283 In the context of natural hexahedrons, the *stochastic model* of progressive fracture due to the stress
 284 of compression (Domokos *et al.*, 2015), describes the generation of ellipsoids with the orthogonal axes
 285 length proportions: 2.32; 1.52: 1 (Fig. 6A), whereas the *silver ratio* progressive fracture model
 286 (Buscarnera and Einav, 2021) describes the generation of cuboids with the edge length proportions:
 287 $\sqrt[3]{2^2}$; $\sqrt[3]{2}$; 1, *i.e.*; 1.59: 1.26: 1 (Fig. 7A). In the former model, a fracture plane is orthogonal to any of
 288 the three sides of a cuboid (enclosing the ellipsoid) and separates two pieces of equal mass. In the
 289 silver ratio model, a fracture plane occurs orthogonal to the current longest axis, separating two pieces
 290 of equal mass. In nature, deviation from these two models can occur such that shape self-similarity,
 291 in terms of axial ratios, is not maintained necessarily upon successive fracture events if the subsequent
 292 fracture is across an axis that differs from the previous fracture event. Fracture across the plane of

293 the short axis was observed in nature (Fig. 6B). However, systematic fracture across the plane of the
 294 long axis (Fig. 6C) and across the medium axis (Figs. 6D, 7B) appeared predominant (*vis* Benn, 1992)
 295 for the blocks observed in the field, in accord with both the stochastic and silver models. Given that
 296 most blocks rest with the short axis vertical, fracture across the L or M axes is consistent with known
 297 fracture mechanics, whereby the centre of an object is the location, under loading, of the maximum
 298 in the tensile stress and the consequent nucleation point for fracture (Hiramatsu and Oka, 1966;
 299 Shipway and Hutchings, 1993). From this point, a fracture line develops to the block edges (Man *et al.*
 300 *al.*, 2018) transverse to the direction of tensile loading. For low values of static or dynamic loading,
 301 the rock eventually ruptures into two parts (Man *et al.*, 2018). Thus, although a block on occasion
 302 might fracture across an axis at variance with the two models above, there is a tendency for blocks to
 303 evolve towards one or the other model. The system state attractors for these two models are shown
 304 in Fig. 8, wherein natural block shapes are considered. Importantly, compression and tensile fracture
 305 leads in both models initially to uniquely defined anisotropic forms, although isotropic forms ($L = M =$
 306 S) can occur in principle with progressive fracture if the fracture rule in each model is relaxed and
 307 varied.

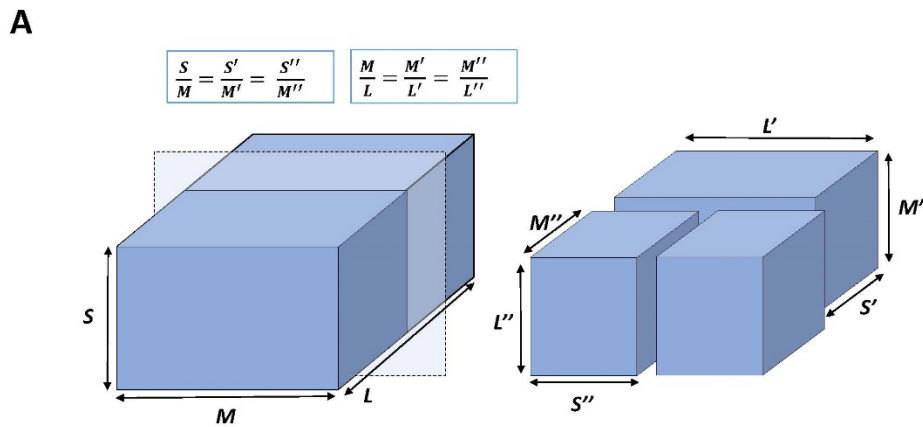


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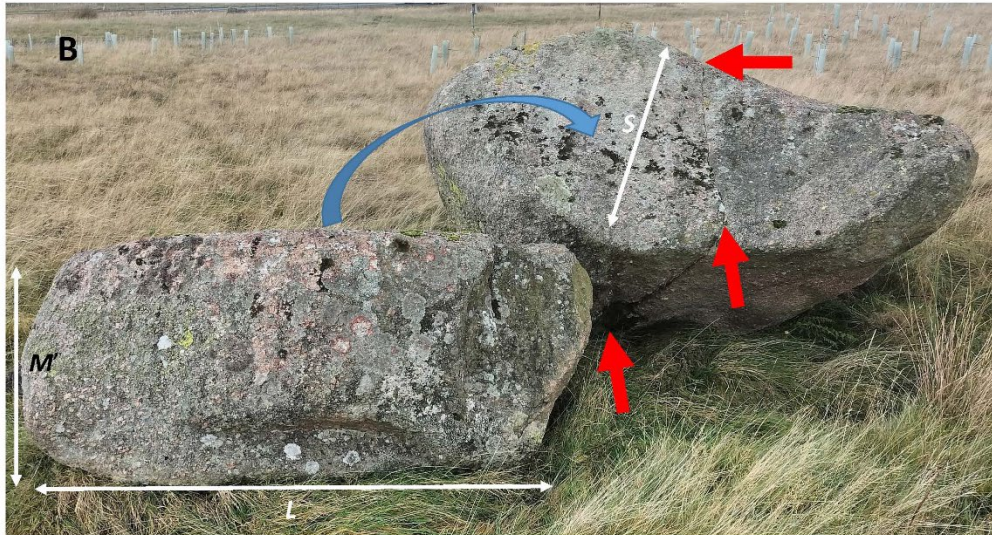


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310 *Figure 6: A) Schematic representation of the concept of the stochastic fracture model applied to a*
 311 *three-dimensional cuboid (enclosing an ellipsoid – see Fig. S1) subject to successive fracture given an*
 312 *assumed identical stress loading to the granite block at each fracture event. Fracture planes are*
 313 *orthogonal to a side and separate two pieces of equal mass. Shape self-similarity is not maintained*
 314 *upon successive fracture events. Three different fracture styles are possible within the model, as*
 315 *labelled 1, 2 and 3; B) Example of a well-rounded block split along a fracture plane consistent with*
 316 *model 1; C) Example of a well-rounded block split along a fracture plane consistent with model 2; D)*
 317 *Example of a well-rounded block split along a fracture plane consistent with model 3. The long axes*
 318 *are foreshortened in panels B, C and D.*

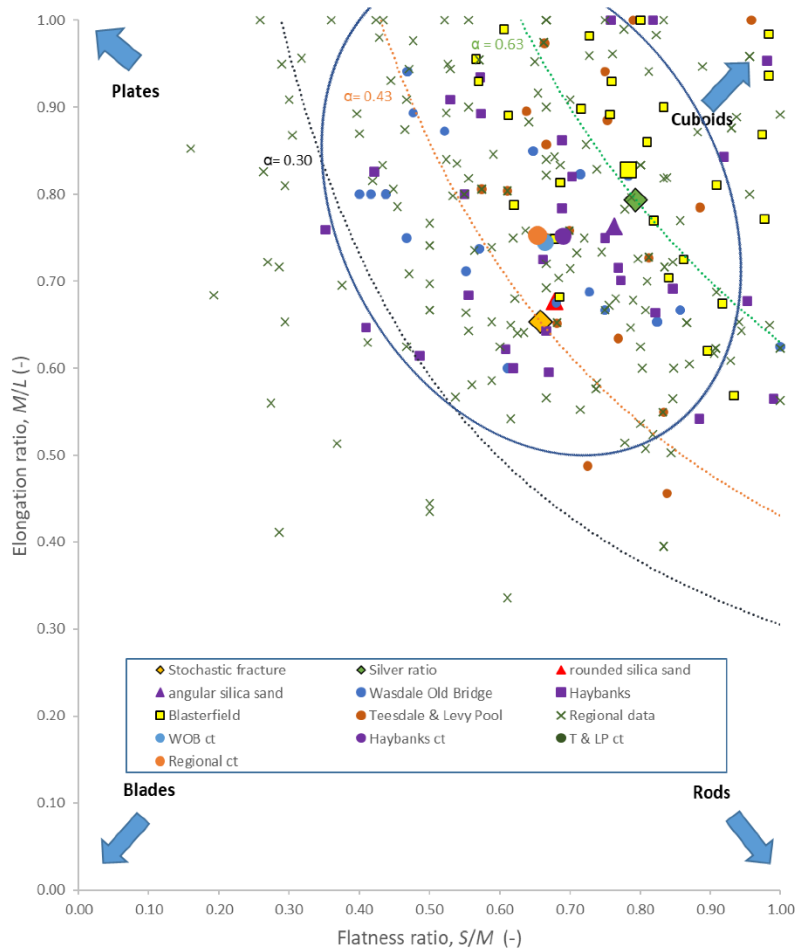


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321 *Figure 7: A) Schematic representation of the concept of the silver ratio model applied to a three-*
 322 *dimensional cuboid (– see Fig. S1) subject to successive fracture given an assumed identical direction*
 323 *of stress loading to the granite block at each fracture event. Fracture planes are orthogonal to the*
 324 *current long axis. Shape self-similarity is more closely maintained (in contrast to Fig. 6) upon successive*
 325 *fracture events; B) Example of silver ratio block. Block to left is approximately the same size as the*
 326 *block to the right and the lower surface (not seen) was originally on the top surface of the right-hand*
 327 *block with the exposed failure plane bisecting the M-axis alignment of the original parent block. The*
 328 *red arrows delineate a fracture plane, aligned with the M-axis of the right-hand block, which divides*
 329 *the right-hand block into two near-equal halves.*
 330



331

332 *Figure 8: The shape relationship for blocks in terms of the Zingg (1935) ratios. The system state*
 333 *attractors for stochastic fracture (gold diamond) and silver ratio (green diamond) are shown as*
 334 *larger symbols, as are the central tendency shapes for mechanically crushed silica sand grains that*
 335 *were initial sub-rounded or angular (Seo et al., 2021). The central tendency (ct) for each sampled*
 336 *location, defined by the mean values, are shown as larger symbols. Curves represent the trend in*
 337 *values of M/L and S/M for constant values of S/L . ct symbols represent the central tendency of each*
 338 *population. Oval is the 95% contour after Oakey et al. (2005).*

339

340 Within Fig. 8, the Zingg ratios (S/M and M/L) for the sampled locations are plotted together with a
 341 data set for the broader region (Regional data). Within Fig. 8, completely equant (isotropic) forms
 342 are absent and plate-like forms survive more readily than rods. Nonetheless, the central tendency of
 343 block shape within the regional data is $S/M = 0.65$ and $M/L = 0.75$; *i.e.*, roughly midway between the
 344 system state attractor for stochastic fracture and the silver ratio attractor. Lines of constant equal
 345 aspect ratios (S/L) are shown for the silver ratio model ($\alpha = 0.63$) and for the stochastic fracture model
 346 ($\alpha = 0.43$). Seo et al. (2021) showed that for homogeneous silica grains, fracture depended on initial

347 particle form (Fig. 8) with angular grains tending towards the silver ratio whilst rounded grains tended
348 towards stochastic fracture. If the fracture process is scale-invariant, then the size differences
349 between silica grains and the Shap blocks can be ignored, and one would expect the Shap granite (a
350 largely homogeneous lithology) to migrate across the diagram from silver to stochastic fracture as
351 cubic blocks become progressively more rounded and ellipsoidal. Blocks deviating from either model
352 (either too long or flat, *e.g.*, approaching $\alpha = 0.30$), will tend to fracture and migrate back towards $\alpha =$
353 0.43, as is especially evident in Fig. S6B within Supplementary Information section 2.2. The central
354 tendencies of the regional data and each of the sampled locations are closely grouped between the
355 central tendencies of the silver and stochastic fracture. The exception is the Blasterfield location
356 which lies closer to the silver ratio, but with increased distance of transport, Teesdale and Levy Pool
357 blocks are in accord with stochastic fracture. Thus, it is evident that block fracture fluctuates between
358 each model, with a trend for constant equal aspect ratios close to $\alpha = 0.50$ (not plotted in Fig. 8).

359 Although Fig. 8 provides an impression of the spread of block shapes around a central tendency there
360 is no clear impression of the actual shape evolution as possible representative shapes can only be
361 selected arbitrarily from the data clouds. Further, only the cube (or sphere) limit point (*e.g.*, 1, 1 in
362 Fig. 8) is real. Limit points for rods and plates exist only through mathematical definition, because as
363 the rod and plate limit points are approached, rods become infinitely long and plates infinitely thin.
364 Thus, representative shapes need to be selected objectively. To solve this problem the procedure of
365 Oakey *et al.* (2005) was utilized to define representative shapes that define the 95% contour around
366 the central tendency of the regional data, represented by the blue oval in Fig. 8. With reference to the
367 position of the 95% contour in the blade quadrant, curve $\alpha = 0.30$ is selected to demarcate a lower
368 bound for common block ratios; with a few plate-like or rod-like blocks occurring in the lower portion
369 of the diagram.

370

371 **3.3 Size evolution**

372 The size distribution of the Shap granite blocks with distance from the pluton source has not received
373 detailed attention, although Carling *et al.* (2013) provide some general observations suggesting there
374 is size reduction with distance. In this study, the sample sizes were insufficient to demonstrate the
375 reduction in block size expected with distance from the source outcrop. However, controls on size
376 reduction are evident. Specifically, blocks greater than $L = 4$ m are rare (Carling *et al.*, 2013), the size
377 being controlled by the close joint spacing of the granite at source (Firman, 1953). With few
378 exceptions, large blocks ($L > 3.0$ m) do not occur beyond 7 km from the pluton, at which point medium
379 blocks ($2.5 > L > 1.5$ m) become scarce, with small blocks ($1.5 > L > 0.5$ m) and cobble-sized material
380 dominating with further dispersal (Carling *et al.*, 2013). These observations indicate that there was a
381 control on the upper size of blocks entrained from the pluton and fracture rapidly reduced block size
382 inducing a crude size-reduction down plume within just a few kilometres. This process was
383 accompanied by local deposition of abrasion and spallation debris as components of a subglacial
384 traction till. Nevertheless, the fracture mechanics that control block shape inevitably control size
385 evolution (Figs. 6 and 7). For example, fracturing a parent cube with 4m long edges and its progeny
386 across the L -axis, only six sequent fracture divisions are required to produce a 1 m cube, as will be
387 demonstrated in the Discussion.

388

389 **4 Discussion: The context of size and shape constraints**

390

391 The initial hypothesis proposed that Sg ice-transported blocks would display changes in edge-rounding
392 and shape with distance to the east from the pluton. As shown in the Results, and elaborated below,
393 edge-rounding does change with distance but block shape is conservative.

394

395 Space-time substitution is an underlying tenant of this study, in that the size and shape characteristics
396 of multiple individual blocks (an erratic plume), dispersing across the landscape, can reflect the

397 evolution of a single erratic block through time along the same general spatial trajectory. An adequate
398 number of sampled blocks are required for this analogy to hold because perturbations to the
399 population of erratics can occur during dispersal. For example, blocks can have been introduced to
400 the W-E trajectory of the study plume by N-S ice movements reworking blocks previously deposited
401 outside of the eastern-directed plume during periods of time after the main W-E ice flow. Also, for
402 the purposes of determining transport distance, a zero x-axis origin has been assumed to be the most
403 easterly outcrop of the pluton at Wasdale Crag. However, some blocks might have been sourced up
404 to a few kilometres to the west of Wasdale Crag. Despite these potential perturbations, which include
405 a small degree of subaerial weathering, the small sample sizes are sufficient to clearly demonstrate
406 systematic change in edge rounding due to ice transport as well as block shape evolution. Finally,
407 edge-rounding and shape are re-set to a degree for the children each time a parent block fractures,
408 so the process of rounding and shape adjustment is not a smooth function of distance from the
409 outcrop, as is explained below.

410

411 **4.1 A conceptual model of block edge rounding controls**

412

413 It should be acknowledged that this study has not considered abrasion of the faces of blocks but has
414 focussed on the edges which tend to abrade and round more rapidly than the associated faces
415 (Boulton, 1974). The edges of blocks still within the outcrop are sharp, albeit some are subject to a
416 slight degree of rounding in place (Fig. 4) from glacial wear, as well as a little post-glacial subaerial
417 weathering. Detached blocks close to the outcrop also tend to exhibit slightly ice-rounded edges, with
418 sharply angled joint planes characterising the other faces due to fracture release of the block from
419 outcrop. The increase in edge rounding with distance confirms the initial hypothesis.

420

421 Block edge rounding initially is constrained by the hardness of the Shap granite and the way it fractures
422 when first entrained at outcrop. The absence of significant edge rounding at the outcrop indicates

423 that blocks were entrained continually until the imposed stresses fell below that required to quarry
424 further blocks. Otherwise, edge rounding of entrained blocks is associated with basal traction
425 transport (Boulton, 1978; Hallet, 1979). Although the compressive strength of granite is high, the
426 tensile strength is an order of magnitude lower; possible as low as 4% of the compressive strength,
427 *i.e.*, 8 MPa (Anikoh *et al.*, 2015; Demirdag *et al.*, 2018; Engineering ToolBox, 2008; Yu *et al.*, 2018).
428 Thus, where compression is translated into flexure, the propensity of the block to elongate across the
429 axis of flexure leads readily to fracture of the brittle granite. This condition means that many blocks
430 close to source initially exhibited near right-angle edges (Fig. 4). Given this geometric constraint, radii
431 of edge curvature inevitable are small initially, approaching the limit: $r_c = l/2$ and $r_c = h$, and
432 increase with distance from the outcrop due to abrasion. However, fracture away from the outcrop
433 introduces new sharp edges (Figs. 4 and 8), such that larger radii characterizing an individual edge-
434 rounded block just before fracture are augmented by smaller radii. This change is reflected in the
435 scatter of radii values found with increased distance from the outcrop (Fig. 4). However, as block size
436 reduces, a condition is approached whereby the population of blocks are increasingly those which
437 resist fracturing (see section 'Block size controls') which should allow edge rounding to become more
438 persistent and thus more pronounced with distance. This condition may be approached in the case
439 of the examples from Teesdale (Fig. 4A) where it is evident that short chords become fewer with
440 distance as larger values of r_c begin to dominate the population. As blocks in transport can reorientate
441 within the ice flow, edge rounding has no effect on block shape, given the shape definition herein.
442 However, if blocks are not free to reorientate, a case not considered herein, the form of blocks can be
443 significantly affected by abrasion in place (Boulton 1974; Hallet, 1979).

444

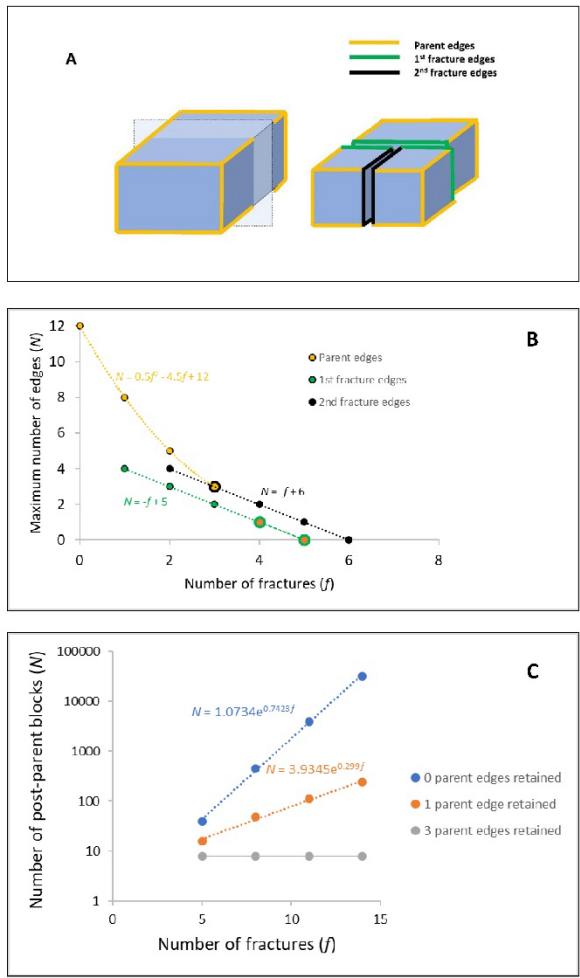
445 Although a positive exponential function (Equation 2) describes the increase in the mean radius of
446 edge rounding with distance from the source outcrop (Fig. 5), the function must eventually transition
447 to a negative function as abraded smaller blocks inevitably are characterized by smaller radii of
448 curvature. This latter condition was not recorded within the current study and sampling at greater

449 distances from the source would be required to determine if this transition occurs. A block (*e.g.*, 1 m
450 cube) subject to edge rounding equally on all 12 edges, as per Equation 2, would have lost about 4%
451 of its mass after 10 km and 9% after 40 km so, in contrast, fracture into two self-similar parts whereby
452 50% of mass is lost, is more significant than edge-rounding in terms of mass loss per block. The greater
453 significance of fracture is consistent with studies of ice erosion by quarrying and ripping versus
454 abrasion of basal bedrock surfaces (see references in Cohen *et al.*, 2006; Hall *et al.*, 2021).

455

456 Rounding of individual blocks is not a steady process, as is evident from the data scatter in Fig. 4 and
457 is further illustrated in the following section. The process whereby the percentage of edges of
458 different generations are rounding with distance, or time, is shown schematically in Fig 9A, wherein
459 there are initially no more than 12 slightly rounded edges to a cube block newly released from outcrop
460 (see Supplementary Information section 1.6 and Fig. S4 for detail of the model). The model is simple
461 but demonstrates the complexity in edge rounding that must accompany successive fracturing of
462 blocks. Fracturing the block successively across the *L*-axis introduces new generations of fracture
463 edges (sequent fractures – Fig. 9B) at the same time as reducing the number of edges on each new
464 block related to earlier fracture events (see Supplementary Information section 1.6 for further detail).
465 As the number of progeny blocks increases exponentially for each fracture event (Fig. 9C), and each
466 sibling can be further dissected along a choice of one, two or three *M*-axes depending on block shape,
467 a diagram including all fracture progeny introduces unreasonable complexity, obscuring the key
468 details. In Fig. 9A and B, for clarity, only one block is followed through one to six sequent fractures,
469 which reduces the number of data points for plotting to a manageable number. The key point to
470 illustrate is that the initial ‘parent’ block must be fractured five times for one of the ensuing progenies
471 to have lost all the initial 12 edges of the ‘parent’. The total number of initial parent edges is relatively
472 persistent because there are 12 edges to begin with (Fig. 9). Contrarily, only four new edges (Fig. 9A)
473 per block are produced on each fracture event. Thus, in contrast to the curve for the initial parent
474 edges, the 1st fracture edges can be lost in as little as four fracture events depending on which sibling

475 block is considered. The 2nd fracture edges are lost by a total of five fracture events and so on, as more
 476 fractures occur adding new fracture edges. Relaxing the model to allow fracture across either the *M*
 477 or *S* axis (see Supplementary Information section 1.6) only adds one or two fracture events to the
 478 process of edge extinctions. Thus, by introducing new edges at each fracture event, rounding of the
 479 block with distance or time is not a steady progression, with well-rounded edges being lost as blocks
 480 are split at the same time as new immature edges are added to a population of sub-mature edges.
 481 The model may not apply beyond some undetermined number of fracture events if there is a critical
 482 minimum block size that is less susceptible to fracture (as was noted above) and rounding then can
 483 become pronounced. Nonetheless, this model explains the presence of a ‘continuum’ from well-
 484 rounded edges to less-well-rounded edges on many individual blocks. The issue as to whether there
 485 is a minimum block size is considered in the next section.



486

487 *Figure 9: A) A regular block released from outcrop has 12 initial edges (Parent edges) all equally*
488 *rounded. Fracturing the block at right angles introduces four new edges (1st fracture edges) to each*
489 *of two sibling blocks, which edges are younger than the initial edges. A further fracture across the L-*
490 *axis is indicated by 2nd fracture edges; B) The maximum number of edges of each generation on a*
491 *block as a function of the number of fracture events, with only the parent edges and those edges*
492 *related to the first two fracture events plotted; C) The total number of blocks created at each fracture*
493 *event which retain 0, 1 or 3 of the original parent edges.*

494

495 The significant increase in the mean radius of edge rounding, with distance from outcrop (Fig. 5),
496 indicates that the blocks were transported within a mobile concentration of basal debris, in frequent
497 block-to-block contact and in contact with the bedrock, leading to abrasion before being deposited
498 within a subglacial traction till (Hallet, 1979). If the distance travelled towards the east is not the
499 controlling factor, then the high degree of edge-rounding may be due to prolonged temporal transport,
500 with some material moving east, south, and then north again, extending the transport distances.
501 However, compatible with studies showing block modification after distances of only 0.4 km (Humlum,
502 1985; Lliboutry 1994; MacGregor *et al.* 2009), an alternative main explanation is preferred for the
503 easterly edge-rounding trend. Although Sg is mechanically strong in compression (Goudie, 2006) it is
504 susceptible to abrasion and tensile fracture for the following reason. The blocks contain large pink
505 phenocrysts set within a matrix of smaller mineral crystals. The large pink crystals are orthoclase
506 feldspar (Moh hardness 6 – 6.5). The other common minerals are glassy quartz (Moh hardness 7),
507 white plagioclase feldspar (Moh hardness 6) and black biotite mica (Moh hardness 2.5 – 3) (Caunt,
508 1986). Thus, the granular composition of the granite with harder crystals adjacent to a soft mineral
509 may aid rapid rounding by abrasion and facilitate tensile fracture during glacial transport.

510 **4.2 Block shape controls**

511

512 Block shape is dependent on the initial controls exhibited at: 1) the outcrop of origin; and 2) the
513 subsequent transport history.

514

515 1) The primary control is the intersection of sub-vertical joints (Firman, 1953) in the granite with
516 horizontal expansion joint planes caused by unloading (Jahns, 1943). Horizontal joints largely are due
517 to glacio-isostatic rebound and surface erosion (Westaway, 2009), leading to the release of the
518 residual stresses accumulated at depth (Berger and Pitcher, 1970). The resultant blocks initially tend
519 to be cubic. Where blocks lie within a few metres from the parent outcrop, the block faces tend to be
520 planar, although curved fractured surfaces occur occasionally, as do conchoidal fracture hollows on
521 otherwise planar surfaces. Curved fracture surfaces tend to occur in homogeneous granite due to
522 pressure unloading (Wang *et al.*, 2022), which will have occurred as ice erosion reduced the
523 overburden. Such joint-defined blocks within an outcrop are readily entrained by moving ice (Matthes,
524 1930; Morland and Boulton, 1975).

525

526 2) Although inhomogeneous blocks in traction may be envisaged as breaking down into multiple
527 fragments at each compressive event (Boulton, 1978), the largely homogeneous nature of the Sg
528 lithology leads to simple tensile fracturing, at each breakage event, whereby subsequent generations
529 of blocks exhibit shapes largely similar to the parent forms. Thus, there is a tendency for equant blocks
530 to persist, through time and distance, due to the tensile stresses associated with flexure across the
531 stoss surfaces reducing block mass in accord with either the silver model or the stochastic model. This
532 trend is indicated by the fact that stronger plate-like blocks occur less frequently away from the pluton
533 in contrast to the general absence at distance of the weaker rod-like blocks. Thus, cuboids progress
534 to form both cubes and cuboids such that the initial hypothesis is rejected.

535

536 **4.3 Block size controls**

537

538 Block size is dependent on the initial controls exhibited at: 1) the outcrop of origin; and 2) the
539 subsequent transport history.

540

541 1) The primary control is the presence of the frequent, well-developed joint planes within the pluton
542 (Firman, 1953; Caunt, 1986) which tend to define and delimit the range of the initial block sizes from
543 c., 0.5 m to 4 m. Fault planes are of sufficient rarity to be ignored. Joints are largely orthogonal: *i.e.*,
544 sub-vertical and near horizontal but oblique joints also occur.

545

546 2) Once in ice-transport, other controls on block disintegration may pertain. In the present case,
547 larger blocks close to the outcrop (< 0.8 km) often exhibit one (or more) intact or partially opened
548 failure plane(s) inherited from the outcrop structure. More commonly, with distance from the outcrop
549 (> 0.8 km), the planes of failure within individual blocks represent the directions of compressive and
550 tensile forces exerted by the ice on the blocks (and thus bear no relationship to block structure or
551 composition), as appears to be the case where failure planes are aligned with the *L* or *M* axes. Fracture
552 occurred when the effective tensile stress exceeded the yield strength of the blocks. Glacial unloading,
553 and subsequent stress release, also may introduce planes of weakness within transported blocks.
554 Adopting the stochastic fracture mode or the silver ratio model for block shape changes indicates that
555 block volume effectively halves at each fracture event with consequent reduction in block size. This
556 conclusion has implications for the fractal evolution of erratic size distributions which, for brevity,
557 cannot be addressed within this paper.

558

559 Other small-scale planes of weakness can be attributed to spatial variations in the primary mineral
560 composition (Grantham, 1928; Parsons and Lee, 2005) leading to textural and grain-size variations
561 which can be visible rarely as parallel lineaments, and later hydrothermal alteration also induced
562 compositional and hence structural variations (Caunt, 1986). These weaknesses lead to loss of small
563 blocks and flakes from the larger parent blocks (see Fig. S5 in Supplementary Information section 2.1)
564 through spallation rather than fracture. Spallation may be related to the state of stress within a
565 deforming till layer (LeBone Hooke and Iverson, 1995) rather than the tensile stress on the stoss side
566 of a block which accounts for block fracture.

567

568 **4.4 General considerations**

569

570 A significant question is whether flowing ice can generate significant stress to fracture the granite
571 blocks. If the thickness of the deforming ice/till layer at the basal boundary is small relative to the size
572 of the boulder, then the compressive force is likely to dominate. However, if the converse applies
573 then the tensile force likely will dominate. Herein, given that there is no information as to the
574 thickness of the deforming layer, the distinction is not considered because, in most cases, blocks will
575 fracture at a lower stress due to tension in contrast to compression. In a consideration of similar
576 situations, emphasis was placed on the compressive strengths of blocks (Boulton, 1978) relative to the
577 normal stresses due to a static ice load above a block. In the present examples, the tensile strength
578 of the stoss side of a block resisting flexure is more relevant for brittle fracture and for granite can be
579 as low as 8 MPa, which is a tensile stress readily applied by a modest (c., 100m thick) yet dynamic ice
580 cover (Hallet, 1996). The distribution of compressive and tensile forces over the stoss side of a block
581 adjacent to the bedrock at the base of an ice mass will be complex and variable through space and
582 time (Hallet, 1979; Morland and Boulton, 1975; Ficker *et al.*, 1980; Cohen *et al.*, 2005). Yet, a simple
583 example below outlines the principles within the context of Shap granite erratics. Although a more
584 complex and complete appreciation of the stress environment of a boulder would be preferred, a
585 simple force balance is utilized instead. Simplicity is dictated by the absence of data to inform a more
586 complex model.

587

588 Setting the tensile stress at failure to 8 MPa and treating the rectangular block as subject to a critical
589 average driving force (τ_c) (Benn and Evans, 2011, p.114) due to ice flow, transverse and longitudinal
590 shear stresses arise of equal magnitude. Setting the fracture focus at half the block width in the
591 direction of loading, neglecting any water pressure variations (Cohen *et al.*, 2006) and deformation
592 within a basal till (Hooke and Iverson, 1995), and imposing the driving stress transverse to the fracture

593 plane, as little as 180 m thickness (H) of flowing glacial ice with an ice surface slope (β) of 1.5° would
594 be sufficient to induce fracture in the block:

595

$$596 \quad \tau_c = \rho_i g H \tan \beta, \quad (3)$$

597

598 where ρ_i is the density of glacial ice and g is the acceleration due to gravity. The value of $H = 180$ m
599 pertains for a rectangular block with a surface area (A) defined by $L = 2$ m and $M = 2$ m (see
600 Supplementary Information section 1.7). The effective instantaneous stress might be greater than as
601 given by Equation 3 (Hooke and Iverson, 1995) but for a block with $L = 3$ m, $M = 1$ m with the long axis
602 transverse to the ice flow the shear force maximum might be achieved with only 130 m of ice cover
603 (see Supplementary Information section 1.7). To the east of the pluton the Last British Ice Sheet was
604 several hundred metres thick *c.*, 25-22 ka BP (Evans *et al.*, 2009), such that blocks would readily
605 fracture during full-glacial warm-based conditions where ice is flowing, as well as after the Last Glacial
606 Maximum when ice was thinning.

607

608 The smallest block sizes ($L < c.$, 1.0 m) present in the field were not considered, which means that the
609 sampled population was truncated at the finer end. Nevertheless, although in some rock-types, a
610 lower limit to block strength may be related to a minimum structural block size (Dreimanis and
611 Vagners, 1971; Lim *et al.*, 2004; Domokos *et al.*, 2015) this is unlikely to pertain to granite which
612 breaks-down to grus at the scale of the phenocrysts. Nonetheless, fracture and surface wear, to an
613 initial block population, tend to result in the observed block population consisting of those blocks
614 which are strongly resistant to further comminution (Moss, 1972; Tavares and King, 1998; Larson and
615 Mooers, 2004; Pfeiffer *et al.*, 2022) which, in principle, enables some blocks to survive transport
616 adjacent to the sole of the ice for great distances before being deposited during the waning phase of
617 the easterly directed ice stream (Hallet, 1979). Thus, although there may be no lower effective block
618 size, a statistical increase in resistance to fracture of the block population with distance likely is evident

619 as witnessed by the increased rounding seen in the Teesdale population. The occasional far-travelled
620 large block, as noted in the Introduction, might be explained as being a statistically stronger example,
621 in contrast to the remainder of the population. Alternatively, large blocks can be cushioned within
622 the till body by smaller particles (Einav, 2007) thus avoiding fracture, or they can be transported
623 englacially, rather than basally, and consequently not subject to protracted abrasion and significant
624 compression whilst in traction. However, englacial blocks are more likely to be angular (Shilts, 1976;
625 Boulton, 1978) and might retain rugose faces.

626

627 Thus, although the reduction in plume parameters values, such as block size and concentration, are
628 commonly viewed as exponential functions of distance from the source (Shilts, 1976), such models
629 (*e.g.*, Fig. 5) consider the sampled population as a whole and the inferences derived may not apply to
630 the transport history of individual blocks. Certainly, the reduction in edge rounding for individual
631 blocks is irregular with distance.

632

633 **5 Conclusions**

634

635 The hypothesis that granite blocks would display an increase in edge rounding with distance from the
636 source outcrop is confirmed, whilst the hypothesis that shape would evolve with distance is refuted.
637 Although the increase in the mean radius of edge rounding for the whole block population increases
638 exponentially with distance, edge rounding on individual blocks is an irregular function mediated by
639 block fracture mechanics, as block size reduces (with shapes fluctuating between cuboids, slabs and
640 rods) with distance and new sharp edges are provided to partially edge-rounded blocks. Thus, edge
641 rounding, and shape coevolve as block size is reduced. Fracture transverse to block orientation is in
642 accord with the application of tensile stress which controls the process by which block form is
643 conserved as block size is reduced. Consideration of the orientation of the tensile fractures on blocks
644 in the field might be used to approximate the direction of ice flow at the time of fracture.

645

646 Overall, the results indicate that edge rounding is unlikely to be advanced if blocks continue to fracture.
647 Well-rounded blocks must represent blocks that have resisted splitting. In the case of exceptionally
648 large, rounded blocks, the rock mass likely is unusually homogeneous, lacking potential fracture lines.
649 However, smaller blocks are less likely to contain potential fracture lines and so fracture should
650 become less prevalent as blocks reduce in size, which then promotes edge rounding.

651

652 Future work should consider developing mathematical models that represent the function of edge
653 rounding as predicated by a model (*e.g.*, silver ratio) describing block size reduction. Similar studies
654 considering other lithologies (*e.g.*, stratified sedimentary rocks) likely would find different shape
655 evolution patterns in contrast to the cuboid central tendency displayed by the homogeneous granite,
656 with concomitant implications for edge rounding trends with time and distance.

657

658 **Author contribution**

659

660 PAC designed the study and conducted the field work, analysis, interpretation and drafting.

661

662 **Competing interests**

663

664 The author declares that he has no conflict of interest.

665

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667

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673 **Data Availability**

674 Basic data are available upon reasonable request from the author.

675

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