Scaling between volume and runout of rock avalanches explained by a modified Voellmy rheology

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Abstract. Rock avalanches reach considerably greater runout lengths than predicted by Coulomb friction. While it has been known for a long time that runout length increases with volume, explaining the increase qualitatively is still a challenge. In this study, the widely used Voellmy rheology is reinterpreted and modified. Instead of adding a Coulomb friction term and a velocity-dependent term, the modified rheology assigns the two terms to different regimes of velocity. While assuming a
5   transition between Coulomb friction and flow at a given velocity is the simplest approach, a reinterpretation of an existing model for the kinetic energy of random particle motion predicts a dependence of the crossover velocity on the thickness of the rock avalanche. Analytical solutions for a lumped mass on a simple 1-D topography reveal the existence of a slope-dominated and a height-dominated regime within the regime of flow. In the slope-dominated regime, the kinetic energy at the foot of the slope depends mainly on the slope angle, while the absolute height relative to the valley floor has little effect, and vice
10   versa. Both regimes can be distinguished by the ratio of a length scale derived from the rheology and the length scale of the topography. Long runout occurs in the height-dominated regime. In combination with empirical relations between volume, thickness, and height, the approach based on the random kinetic energy model reproduces the scaling of runout length with volume observed in nature very well.

1 Introduction

15   The long runout of rock avalanches has puzzled scientists for decades. Rapid mass movements with volumes $V \gtrapprox 10^6$ m³ achieve a considerably greater runout length than a solid block under Coulomb friction. Theoretically, a lumped mass slowly sliding downward along a topographic profile comes to rest when the ratio of total height drop H and traveled horizontal distance L equals the coefficient of friction μ (e.g., de Blasio, 2011). This ratio is often referred to as Heim's ratio. Huge rock avalanches with volumes of some km³ even reach ratios $\frac{H}{L} < 0.1$, while typical values of μ for Coulomb friction are between
20   0.5 and 1. The biggest landslides of Olympus Mons on Mars even reach $\frac{H}{L} \approx 0.02$ (Crosta et al., 2018), which would even correspond to the friction of steel on ice.

     Although the lumped-mass model is oversimplified, the occurrence of ratios $\frac{H}{L}$ much lower than μ suggests a transition from Coulomb friction to a more fluid-like behavior with a lower effective friction. Since L refers to a straight line, movement along a curved track even increases $\frac{H}{L}$. The same holds for the effect of centrifugal forces due to profile curvature. Practically,

25 longitudinal spreading is the only process that may reduce $\frac{H}{L}$ considerably. While the definition of $\frac{H}{L}$ refers to the highest point of the detachment area and the most distant point of the deposits, lumped-mass models rather describe the center of mass. Davies (1982) proposed a relation between runout length and volume based on longitudinal spreading. However, this relation becomes geometrically inconsistent if the runout length exceeds twice the respective length for the center of mass and thus cannot predict a strong decrease in $\frac{H}{L}$ compared to the lumped-mass model. Furthermore, data collected by Legros

30 (2002) reveal that the center-to-center $\frac{H}{L}$ ratio may also be considerably smaller than typical values of μ. So long runout and longitudinal spreading of rock avalanches are probably facets of a fluid-like behavior, but longitudinal spreading cannot be considered the primary reason for the long runout.

In turn, there is no consensus about the mechanism behind the fluid-like behavior of rock avalanches. It is even unclear whether it can be attributed to a unique mechanism. Water is present in many rock avalanches and may play a part as well as

35 air. Frictional heating may also have a strong effect on the mechanical properties. Alternatively, the increase in runout length with volume may be an inherent property of granular flow without any specific process beyond the interaction of particles.

Numerical simulations of discrete particles are able to reproduce the observed decrease in effective friction with volume (Campbell et al., 1995; Johnson et al., 2016) at least qualitatively. However, discrete models involving a large number of particles are numerically costly, in particular in 3D (e.g., Mead and Cleary, 2015). Therefore, depth-averaged continuum

40 models are still preferred for large-scale simulations and for hazard assessment. Such models are typically based on the theory of granular flow proposed by Savage and Hutter (1989). As a major advantage over lumped-mass models, continuum models are able to predict the morphology of the deposits, which allows for a better constraining of the parameter values. Similarly to lumped-mass models, depth-averaged continuum models require only a model for the shear stress at the bed and no further parameters. This parsimony is an advantage over 3D simulations beyond the lower numerical complexity and also over depth-

45 averaged multi-phase flow models (e.g., Pudasaini and Mergili, 2019).

The most widely used relation for the basal shear stress in depth-averaged models of granular flow dates back to work on snow avalanches of Voellmy (1955) and assumes a shear stress of

$$\tau = \mu\sigma + \frac{\rho g}{\xi} v^2. \tag{1}$$

The first term describes Coulomb friction with a coefficient μ where σ is the normal stress. The second term was introduced

50 as an effective friction term for turbulent flow of snow, where ρ, g, and v are density, gravity, and vertically averaged velocity, respectively. The parameter ξ refers to the roughness of the bed.

As a central property of Voellmy's rheology, the velocity-dependent contribution to friction does not increase with normal stress. In the simplest case, the normal stress is $\sigma = \rho g h \cos\beta$, where h is the thickness of the layer and β the slope angle. Then the effective coefficient of friction

55 $$\mu_{\text{eff}} = \frac{\tau}{\sigma} = \mu + \frac{v^2}{\xi h \cos\beta} \tag{2}$$

decreases with increasing thickness and thus also with volume. So Voellmy's approach predicts increase in runout length with volume.
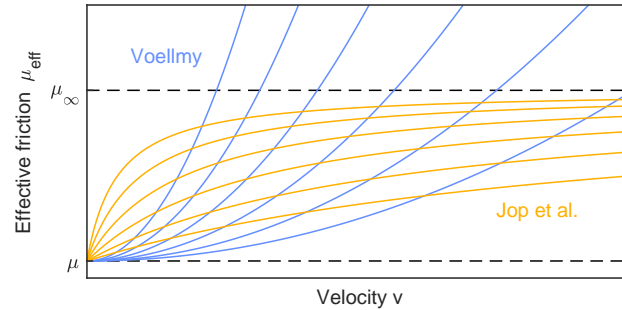
Figure 1. Velocity-dependence of the effective coefficient of friction for Voellmy's rheology and the rheology proposed by Jop et al. (2005). Lower curves correspond to greater thickness.

While Voellmy's approach started from observations of snow avalanches in combination with the analogy to turbulent flow, an alternative concept based on theoretical scaling arguments and laboratory experiments also received great interest (Jop et al., 2005, 2006). This approach does not predict the shear stress at a rough bed, but for each point of a granular medium. The respective effective coefficient of friction

$$\mu_{\text{eff}} = \mu + \frac{\mu_\infty - \mu}{1 + \frac{I_0}{I}} \tag{3}$$

depends on the so-called inertial number I, which is proportional to the shear rate and decreases with increasing normal stress. Equation (3) predicts an increase of μ_{eff} from the Coulomb friction coefficient μ towards a higher coefficient μ_∞, which is approached in the limit $I \to \infty$. The parameter I_0 defines the value of I at which μ_{eff} is the middle between μ and μ_∞.

Both approaches are qualitatively similar in the sense that the effective friction increases with velocity and decreases with thickness. As illustrated in Fig. 1, however, they differ fundamentally concerning the dependence on v. Voellmy's rheology predicts a rather weak increase at small velocities, but a strong increase in friction at high velocities. In turn, the rheology proposed by Jop et al. (2005) predicts a rapid increase in friction at small velocities in combination with an upper limit (μ_∞) at high velocities.

Although the rheology proposed by Jop et al. (2005) was also applied to rock avalanches (Lucas et al., 2014), Voellmy's rheology is more widely used in the field of large-scale modeling and hazard assessment, e.g., in the model RAMMS (Christen et al., 2010). For this reason, focus of this study is on Voellmy's rheology.

Voellmy (1955) explicitly referred to turbulent flow of snow and adopted the respective relations for turbulent flow of water in rough channels. In particular when transferred to rock avalanches, however, the idea of turbulent flow is questionable. Turbulent flow causes a strong mixing of the particles and is thus incompatible with the preservation of the stratigraphy often found in the deposits (Dufresne et al., 2016).

However, this apparent issue was already clarified by Salm (1993). The lowermost particles are deflected by collisions with the rough bed. Assuming that the bed-parallel component of the velocity is reduced by a given factor f in each collision results in a loss in kinetic energy of $\delta E = \frac{1}{2}m(1 - f^2)v^2$. If we further assume that collisions take place after traveling a given distance

δx, the effective friction force is

$$F = \frac{\delta E}{\delta x} = \frac{(1 - f^2)m}{2\delta x}v^2 \tag{4}$$

per particle of the lowermost layer. This simple argument explains the v^2-dependence in Eq. (1). A part of the energy taken from the bed-parallel velocity is transformed into vertical motion of particles in the body of the avalanche. Up to this point,

85 the mechanism is even the same as for turbulent flow of water, which explains the identical relation for the basal shear stress. The difference arises from the way the energy transferred from the bed into the body is dissipated. Owing to its low viscosity, water can only dissipate this energy by turbulent flow. In contrast, collisions between rock fragments are strongly inelastic and consume kinetic energy easily without the need for a turbulent flow pattern. So the mechanism of energy conversion at the bed and thus also the basal shear stress follows basically the same relation as for turbulent flow of water, but the way the energy

90 is finally dissipated in the body is different. In this sense, the occurrence of the same relation for the basal shear stress as for turbulent flow is not coincidence, but does not imply that the flow must be turbulent.

Another issue of Voellmy's rheology is, however, not resolved so easily. Since $\mu_{\text{eff}} \geq \mu$ for any values of v and h, a long runout can only be achieved by assuming values of μ much lower than typical coefficients for Coulomb friction. As an example, the best-fit values of all events analyzed by Aaron et al. (2022) are lower than 0.25 with some even lower than 0.1. Furthermore,

95 the individual values of μ and ξ are often not constrained well since different combinations yield similar results, in particular with regard to the runout length. The rheology proposed by Jop et al. (2005) (Eq. 3) also predicts $\mu_{\text{eff}} > \mu$ and thus also suffers from the problem that μ is not the same as for Coulomb friction.

The random kinetic energy (RKE) model (Buser and Bartelt, 2009; Bartelt and Buser, 2010) seems to be the only approach to overcome this limitation that raised attention. This approach takes into account that the energy converted at the rough bed

100 causes a random movement of the particles in the body of the avalanche. It is assumed that the respective kinetic energy R is transported with the depth-averaged velocity v and dissipated by particle collisions. Finally, the entire friction (both terms in Eq. 1) are multiplied by a factor $e^{-\frac{R}{R_0}}$, where R_0 is considered an activation energy.

The RKE model is available as an option in the model RAMMS (Christen et al., 2010). While the RKE model was developed for snow avalanches, it was also applied to rock avalanches (Preuth et al., 2010). In turn, Issler et al. (2018) pointed out

105 several shortcomings of the RKE model. Owing to the exponential factor, the RKE model even predicts a decrease in friction with velocity at high velocities, so that the velocity increases more and more on a straight slope once a threshold velocity is exceeded. Furthermore, the velocity-dependent reduction of the friction term is not consistent with Salm's explanation of Voellmy's rheology in its spirit. Given that the v^2-term describes the conversion of kinetic energy at the rough bed into RKE, which is then dissipated in the avalanche body, there is no reason why the conversion should become weaker at high velocities.

110 Developing some kind of minimum Voellmy-type rheology that is able to explain the long runout at large volumes without these inconsistencies is the subject of this paper.
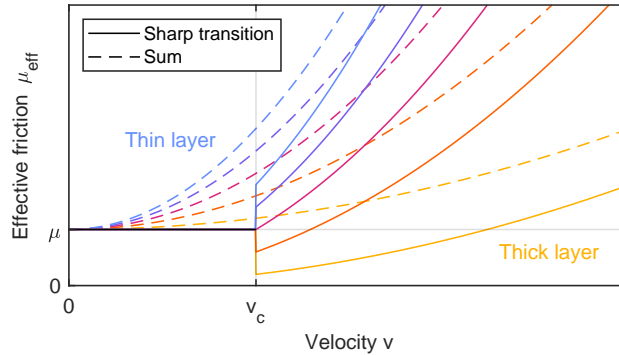
Figure 2. Comparison of a sharp transition (Eq. 5) to the sum typically used for Voellmy's rheology (Eq. 1). Lower curves correspond to greater thickness h.

2 A modified Voellmy rheology

The ideas of Voellmy (1955) and Salm (1993) focus to the v^2-term in Eq. (1), which dominates the rheology at high velocities. In turn, the Coulomb friction term describes the well-constrained behavior at low velocities. The v^2-term alone would predict avalanches that move and spread forever and would come to rest only in topographic depressions.

Adding the two terms in Eq. (1) is elegant since the correct term automatically becomes dominant in the respective regime of velocities. However, this approach is not unique and does not necessarily describe the behavior at intermediate velocities well. Given that the behavior at small and at large velocities is captured well, the inability to reproduce the long runout of rock avalanches without reducing the coefficient μ artificially must even arise from a wrong behavior at intermediate velocities.

In this paper, a complementary approach is proposed by assuming a sharp transition between two distinct regimes of movement in the form

$$\tau = \begin{cases} \mu\sigma & \text{for} & v < v_{\text{c}} \\ \frac{\rho g}{\xi} v^2 & & v \geq v_{\text{c}} \end{cases}. \tag{5}$$

For the moment, it is assumed that the transition takes place at a given crossover velocity v_{c}.

Figure 2 illustrates the difference of the sharp transition (Eq. 5) towards the sum (Eq. 1) in terms of $\mu_{\text{eff}} = \frac{\tau}{\sigma}$. A fundamental difference occurs if the moving layer is so thick that $\frac{\rho g}{\xi} v_{\text{c}}^2 < \mu\sigma$. Then μ_{eff} decreases instantaneously if v exceeds v_{c}. If the decrease is sufficiently strong, Heim's ratio may decrease below the coefficient of friction μ, so that a long runout can occur without decreasing μ artificially.

In the following, the framework is reduced to the minimum that is necessary for investigating the new approach in the context of velocity and runout. The movement of a point-like mass on a given topographic profile is considered, and it is assumed that the thickness h is constant. Since the normal stress only affects the shear stress at low velocities ($v < v_{\text{c}}$), dynamic effects (centrifugal forces) on the normal stress can be neglected. Then $\sigma = \rho g \cos\beta$ can be assumed, and the total acceleration parallel

to the topography is

$$a = g\sin\beta - \begin{cases} \mu g\cos\beta & v < v_{\mathrm{c}} \\ \frac{g}{\xi h}v^2 & v \geq v_{\mathrm{c}} \end{cases} \quad \text{for} \quad . \tag{6}$$

As already pointed out by Perla et al. (1980), considering the velocity v as a function of the position s (arc length along the profile) is simpler than considering s and v as functions of time. The governing equation becomes particularly simple if the kinetic energy per unit mass, $E = \frac{1}{2}v^2$, is considered, since

$$\frac{\mathrm{d}E}{\mathrm{d}s} = v\frac{\mathrm{d}v}{\mathrm{d}s} = \frac{\mathrm{d}s}{\mathrm{d}t}\frac{\mathrm{d}v}{\mathrm{d}s} = \frac{\mathrm{d}v}{\mathrm{d}t} = a, \tag{7}$$

Inserting Eq. (6) yields

$$\frac{\mathrm{d}E}{\mathrm{d}s} = g\sin\beta - \begin{cases} \mu g\cos\beta & v < v_{\mathrm{c}} \\ \frac{E}{\lambda} & v \geq v_{\mathrm{c}} \end{cases} \quad \text{for} \tag{8}$$

with

$$\lambda = \frac{\xi h}{2g}. \tag{9}$$

The differential equation is linear in both regimes. It is easily recognized that the solution for a straight slope (constant β) is

$$E(s) = (E(0) - E_{\mathrm{e}})\,e^{-\frac{s}{\lambda}} + E_{\mathrm{e}}, \tag{10}$$

for $v \geq v_{\mathrm{c}}$, where

$$E_{\mathrm{e}} = \lambda g\sin\beta. \tag{11}$$

is the kinetic energy in equilibrium ($\frac{\mathrm{d}E}{\mathrm{d}s} = 0$). The kinetic energy approaches E_{e} downslope, and λ is the respective e-folding distance.

So λ has two different meanings beyond its definition in terms of the parameters ξ and h (Eq. 9). First, it controls the equilibrium velocity via the respective kinetic energy (Eq. 11). More important, however, it defines the length scale of adjustment of the velocity to the slope. The combination of this length scale with the length scale of the topography will be the basis of the scaling properties investigated in Sect. 4.

Voellmy (1955) estimated $\xi \approx 500\ \mathrm{ms}^{-2}$ for snow avalanches on a rough bed. Typical best-fit values for rock avalanches are slightly lower ($\xi \approx 300\ \mathrm{ms}^{-2}$, e.g., Aaron et al., 2022; Argentin et al., 2022), leading to an estimate $\lambda \approx 15h$.

In the following, a straight slope is combined with a horizontal plane, although other geometries such as the cycloidal or parabolic profiles considered by Gauer (2018) may be more realistic. As a major advantage beyond the simple analytical solution, the slope length l defines a unique length scale here, and the ratio of the length scales λ (rheology) and l (topography) will turn out to be the main control on the behavior.
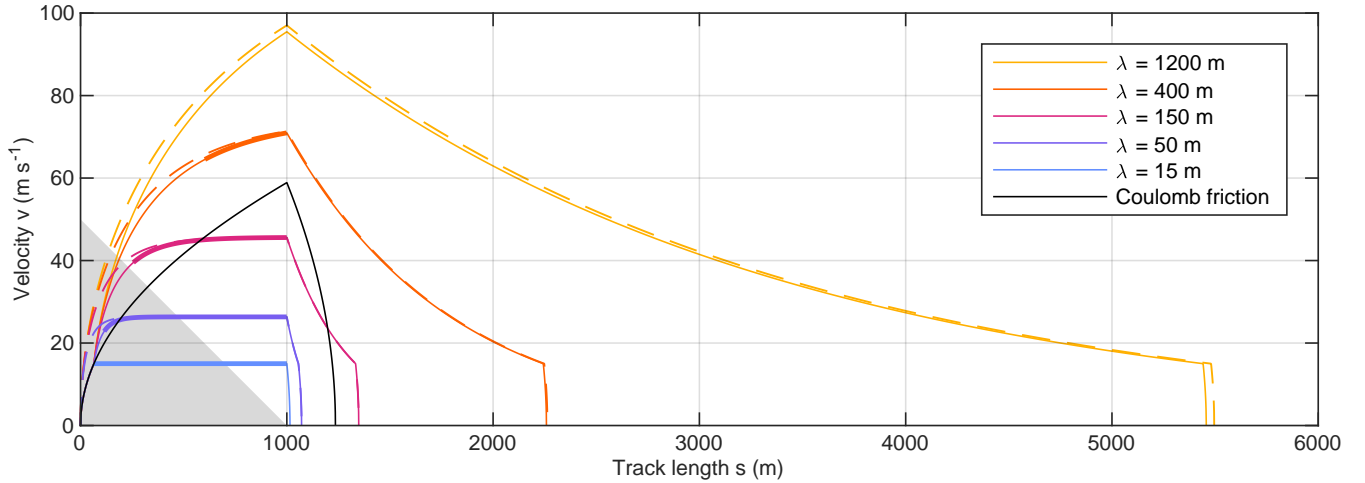
Figure 3. Phase space trajectories for $\beta = 45°$, $l = 1000$ m, $\mu = 0.75$, and $v_c = 15$ m s^{-1}. Solid lines start with Coulomb friction as long as $v < v_c$. Dashed lines correspond to a simplified scenario which immediately starts with flow instead of Coulomb friction. Thick line segments describe the range where flow is less efficient than Coulomb friction.

The velocity at each point is easily composed from Eq. (10) for each of the two segments and the respective solution for Coulomb friction. The latter is even independent of the specific topography and is readily obtained in terms of the horizontal coordinate x instead of the arc length s,

$$\frac{\mathrm{d}E}{\mathrm{d}x} = \frac{\mathrm{d}E}{\mathrm{d}s}\frac{\mathrm{d}s}{\mathrm{d}x} = g\tan\beta - \mu g = -g\frac{\mathrm{d}z}{\mathrm{d}x} - \mu g, \tag{12}$$

where $z(x)$ is the topography and the relations $\frac{\mathrm{d}x}{\mathrm{d}s} = \cos\beta$ and $\tan\beta = -\frac{\mathrm{d}z}{\mathrm{d}x}$ were used. Then,

$$E(x) = E(0) + g\left(z(0) - z(x)\right) - \mu g x, \tag{13}$$

which recovers the widely used energy-line approach.

Figure 3 shows phase space trajectories (v vs. s) for $\beta = 45°$, $l = 1000$ m, $\mu = 0.75$, and $v_c = 15$ m s^{-1}. The total height is $H = l\sin\beta = 707$ m. Pure Coulomb friction ($v_c \to \infty$) is used as a reference scenario (black line).

For all considered scenarios except for $\lambda = 15$ m, the transition to flow at $v = v_c$ reduces friction. However, this condition does not guarantee an increase in runout length compared to Coulomb friction. Since the advantage is lost at high velocities (See Fig. 2), flow is less efficient than Coulomb friction for a part of the track, except for the highest value $\lambda = 1200$ m.

So the value of λ at which the runout length exceeds that of Coulomb friction is considerably higher than that where flow is more efficient than Coulomb friction at $v = v_c$. This value of λ is, however, less important than the occurrence of two different regimes. For small values of λ (here $\lambda \leq 150$ m), v approaches the equilibrium velocity $2\sqrt{E_e}$ (Eq. 11) along the slope, and the runout length is finally not much larger than for Coulomb friction. In turn, the mass is still accelerated considerably at the foot of the slope for large values of λ (here $\lambda \geq 400$ m). The runout length increases rapidly with λ in this regime, resulting in low values of Heim's ratio. The runout reaches almost 5.5 km for $\lambda = 1200$ m in terms of arc length, corresponding to almost

$L = 5.2$ km horizontal distance and to $\frac{H}{L} = 0.14$. This value of Heim's ratio is more than five times smaller than the coefficient of friction $\mu = 0.75$ assumed here. The two different regimes will be investigated in detail in Sect. 4.

The dashed lines in Fig. 3 describe a simplified scenario which neglects the initial Coulomb friction phase. Here it is assumed that the movement already starts with the flow rheology, although $v < v_c$ in the beginning. As a consequence, friction is low
180 during the initial phase, which results in higher velocities. For low values of λ, however, v approaches the equilibrium velocity rapidly. Then the additional kinetic energy is consumed before the mass reaches the foot of the slope, so that its effect on the runout length is negligible.

In turn, a part of the additional kinetic energy is preserved for large values of λ, which leads to a longer runout. However, the effect is in an order of magnitude of only 1 % for $\lambda = 1200$ m and thus still negligible. The same holds for the phase of
185 deceleration after falling back to Coulomb friction. The respective length is $\frac{v_c^2}{2\mu g} = 16$ m here, which is also negligible. So the transition to Coulomb friction if the velocity drops below v_c is important, but the coefficient of friction μ is irrelevant compared to the parameters λ and v_c.

3   The relation to the RKE model

The transition between Coulomb friction and flow at a given velocity v_c was an ad-hoc assumption in Sect. 2. Let us now find
190 out whether this assumption can be substantiated by the RKE model. For simplicity, the lumped-mass model is considered here.

The energy per area and time dissipated at the bed is τv. Following the idea of the RKE model, a fraction ϕ of this energy is converted into RKE and then dissipated according to a linear decay model with a decay constant k. Accordingly, the average RKE per unit mass R follows the differential equation

195
$$\rho h \frac{\mathrm{d}R}{\mathrm{d}t} = \phi \tau v - k\rho h R \tag{14}$$

and thus

$$\frac{\mathrm{d}R}{\mathrm{d}t} = \frac{\phi g}{\xi h}v^3 - kR = \frac{\phi}{2\lambda}v^3 - kR \tag{15}$$

for $v \geq v_c$ with τ from Eq. (5) and λ from Eq. (9). At constant velocity, R approaches an equilibrium value

$$R = \frac{\phi}{2\lambda k}v^3. \tag{16}$$

200 Assuming that this adjustment is much faster than changes in velocity as already proposed by Issler et al. (2018), it can be assumed that R always follows Eq. (16).

The above considerations are just a simplification of the original RKE model. Introducing a dependence of friction on R would be the next step. This step is, however, questionable as discussed in Sect. 1. Instead, assuming that R controls the transition between the two regimes of friction is almost straightforward. This means that a given minimum amount of RKE per
205 mass R_c is required for maintaining flow and a fallback to Coulomb friction occurs as soon as $R < R_c$. In combination with
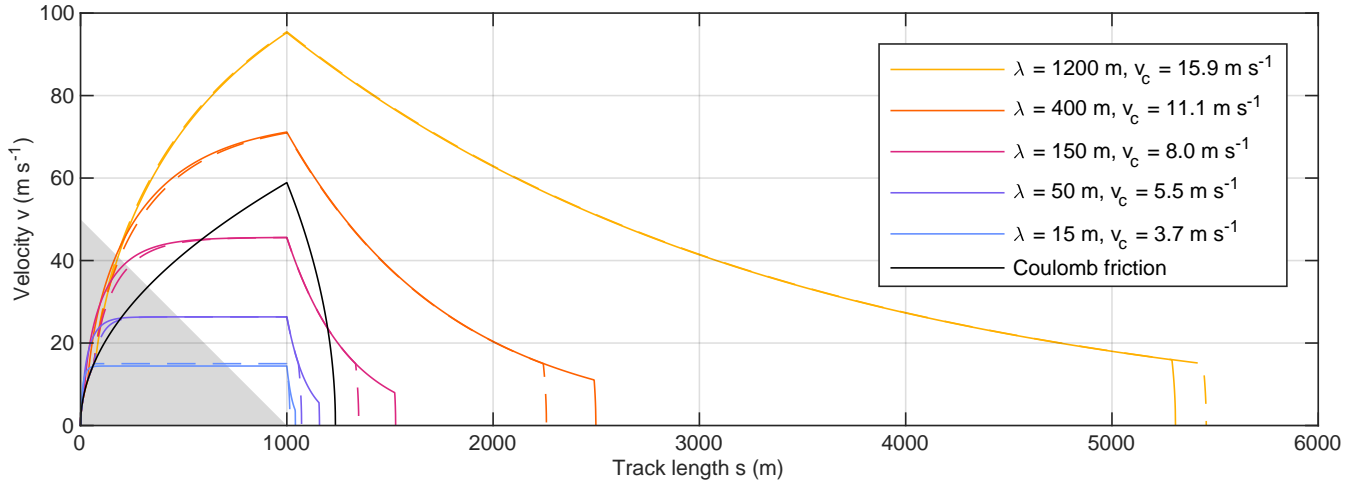
Figure 4. Phase space trajectories for $\beta = 45°$, $l = 1000$ m, $\mu = 0.75$. Solid lines correspond to a given minimum RKE per mass (Eq. 17), while dashed lines describe the respective trajectories for $v_\mathrm{c} = 15$ m s^{-1} already shown in Fig. 3.

Eq. (16), this concept predicts a crossover velocity of

$$v_\mathrm{c} = \left(\frac{2kR_\mathrm{c}}{\phi} \lambda \right)^{\frac{1}{3}}.$$
(17)

Similarly to the friction term itself, v_c does not depend on h and ξ individually, but only on their product via the length scale λ. For the lumped-mass model, this implies that the entire solution only depends on the product ξh and not on the individual

210 values, which will simplify the analysis of the scaling properties in Sect. 4.

Figure 4 compares the phase space trajectories from Fig. 3 to those obtained with a given minimum RKE per mass. The respective relation $v_\mathrm{c} \propto \sqrt[3]{\lambda}$ (Eq. 17) was implemented in the form $v_\mathrm{c} = \sqrt[3]{\frac{\lambda}{l}}\ 15$ m s^{-1}. As discussed in Sect. 2, the initial phase has no big effect, so that the trajectories mainly differ at the end when the flowing medium falls back to Coulomb friction. The crossover velocity v_c is greater than in Fig. 3 for $\lambda > l$ and vice versa. Accordingly, the runout length is reduced

215 for $\lambda > l$ and vice versa. The increase in runout length with increasing λ persists, but becomes weaker. This effect will be investigated further in the following.

4 Scaling regimes

The findings from Sect. 2 suggest to consider a simplified model neglecting the two phases of Coulomb friction. So let us assume that the movement immediately starts with flow and stops suddenly when the velocity drops below v_c. Then the kinetic

220 energy at the foot of the slope is obtained from Eqs. (10) and (11):

$$
\begin{aligned}
E(l) &= E_\mathrm{e} \left(1 - e^{-\frac{l}{\lambda}} \right) = \lambda g \sin \beta \left(1 - e^{-\frac{l}{\lambda}} \right) \\
&= gH \frac{\lambda}{l} \left(1 - e^{-\frac{l}{\lambda}} \right)
\end{aligned}
$$
(18)
(19)

with the total height $H = l \sin \beta$. For any position $s > l$, the kinetic energy is

$$E(s) = E(l) e^{-\frac{s-l}{\lambda}} = gH \frac{\lambda}{l} \left(e^{\frac{l}{\lambda}} - 1 \right) e^{-\frac{s}{\lambda}}. \tag{20}$$

225 The runout (arc) length S is then defined by the condition

$$E(S) = \frac{1}{2} v_{\mathrm{c}}^2, \tag{21}$$

which yields

$$S = \lambda \ln \left(\epsilon \frac{\lambda}{l} \left(e^{\frac{l}{\lambda}} - 1 \right) \right) \tag{22}$$

with the energy ratio

230 $$\epsilon = \frac{gH}{\frac{1}{2} v_{\mathrm{c}}^2}. \tag{23}$$

The energy ratio is the ratio of the total available potential energy and the minimum kinetic energy required to maintain flow.

If we consider scenarios with different values of λ on the same topography (as in Figs. 3 and 4), it makes sense to divide Eq. (22) by l. Then the runout length S relative to the slope length l is a function of the ratio $\frac{\lambda}{l}$ and ϵ. For the simplest model with a constant threshold velocity v_{c}, the energy ratio ϵ is even constant ($\epsilon \approx 60$ for the scenario from Fig. 3). In turn, the RKE

235 concept introduces a dependence of ϵ on λ. Using the same scaling as in Sect. 2, this dependence can be written in the form

$$\epsilon(\lambda, l) = \epsilon(l, l) \left(\frac{\lambda}{l} \right)^{-\frac{2}{3}}. \tag{24}$$

Figure 5(a) shows the dependence of $\frac{S}{l}$ on $\frac{\lambda}{l}$. Since both S and l refer to arc length, these properties were converted to the height $H = l \sin \beta$ and the horizontal distance $L = S - l + l \cos \beta$ in Fig. 5(b). This plot is not as universal as the original plot since it depends on the slope angle ($\beta = 45°$ here). However, the plot of the inverse of Heim's ratio, $\frac{L}{H}$, is in principle similar

240 to that of $\frac{S}{l}$.

The existence of two different scaling regimes is immediately recognized. If $\frac{\lambda}{l}$ is small, the runout length increases only weakly with λ, while the increase apparently approaches a power law for greater ratios $\frac{\lambda}{l}$. The fundamental difference between the two regimes is already recognized in the kinetic energy at the foot of the slope. For $\lambda \ll l$, Eq. (18) yields

$$E(l) \approx E_{\mathrm{e}} = \lambda g \sin \beta, \tag{25}$$

245 which depends only on λ and on the slope angle β, but not on the absolute slope length l and height H individually. In turn, Eq. (18) yields

$$E(l) \approx gH \tag{26}$$

for $\lambda \gg l$, which means that the initial potential energy is converted almost completely into kinetic energy. Then the kinetic energy at the foot of the slope depends on the height, but not on the slope angle β.
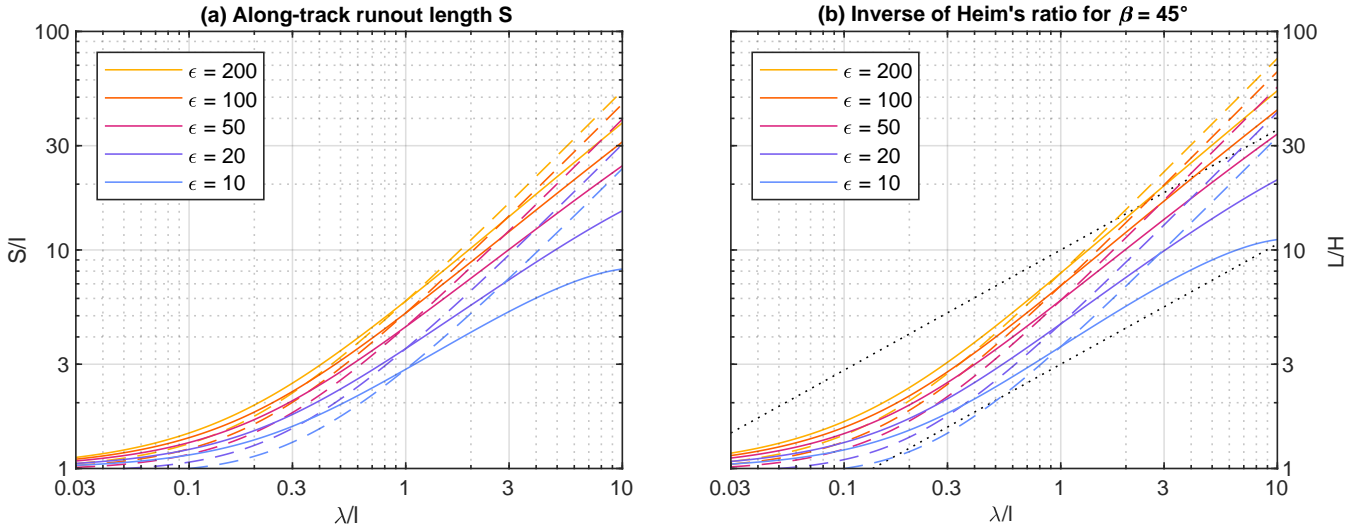
Figure 5. Runout length as a function of λ on the same topography (constant l and β for each curve). Dashed lines refer to the model with constant v_c (constant ϵ along each curve). Solid lines refer to the RKE model, where ϵ is the energy ratio for $\lambda = l$ ($\epsilon(l,l)$ in Eq. 24). The dotted lines reflect the power law with an exponent $\gamma = 0.55$ expected from real rock avalanches.

250   These results suggest a subdivision of the parameter space into a slope-dominated regime ($E(l)$ depends mainly on β) and height-dominated regime ($E(l)$ depends mainly on H). In the form $\lambda \gg l$, however, the height-dominated regime is just a mathematical limit. Using the estimate $\lambda \approx 15h$, $\frac{\lambda}{l} = 15$ would already require $h = l$, which is geometrically unrealistic. This is also the reason why Fig. 3 is limited to $\frac{\lambda}{l} \leq 15$.

The two regimes can be defined beyond the mathematical limits by comparing the dependence of $E(l)$ on l at constant β

255   (making the slope longer) and at constant H (making the slope less steep). Equation (18) yields

$$\left.\frac{\mathrm{d}E(l)}{\mathrm{d}l}\right|_{\beta=\text{const.}} = g\sin\beta\, e^{-\frac{l}{\lambda}} \tag{27}$$

$$\left.\frac{\mathrm{d}E(l)}{\mathrm{d}l}\right|_{H=\text{const.}} = g\sin\beta\left(e^{-\frac{l}{\lambda}} - \frac{\lambda}{l}\left(1 - e^{-\frac{l}{\lambda}}\right)\right) \tag{28}$$

It is found easily graphically or numerically that $\frac{\mathrm{d}E(l)}{\mathrm{d}l}|_{\beta=\text{const.}} > -\frac{\mathrm{d}E(l)}{\mathrm{d}l}|_{H=\text{const.}}$ for $\frac{\lambda}{l} > 0.8$. In this sense, the regime with $\frac{\lambda}{l} > 0.8$ is height-dominated and the regime with $\frac{\lambda}{l} < 0.8$ slope-dominated.

260   Approximating the term $e^{\frac{l}{\lambda}}$ by $1 + \frac{l}{\lambda}$ for $\lambda \gg l$ in Eq. (22) yields

$$S \approx \lambda \ln \epsilon. \tag{29}$$

The dashed lines in Fig. 5 show that this linear increase in runout length holds reasonably well for the model with constant v_c over the height-limited range. After transforming the arc length S to the horizontal distance L, the curves follow the linear increase even slightly better.

265   For the model based on RKE (solid lines in Fig. 5), however, the decrease in ϵ with λ causes a weaker increase in runout length. Theoretically, the runout length would even decrease for $\lambda \gg l$ since $\epsilon(\lambda, l) \to 0$ then (Eq. 24). While this effect is visible for the lowest energy ratio $\epsilon = 10$, the other curves can be described reasonably well by a power law with an exponent lower than 1 in the height-limited regime.

The exponent γ of the power-law relation

$$\frac{L}{H} \propto \left(\frac{\lambda}{l}\right)^{\gamma} \tag{30}$$

is the most important criterion for testing the approach against real-world data. Fifty years ago, Scheidegger (1973) found a power-law relation in terms of volume,

$$\frac{L}{H} \propto V^{0.16}, \tag{31}$$

although referring to the original definition of H and L and not to the center of mass. This relation was confirmed later
275   by Legros (2002). Larsen et al. (2010) found the relation $V \propto A^{1.40}$ between volume and area for the deposits of bedrock landslides. This leads to the relation

$$h = \frac{V}{A} \propto V^{1-\frac{1}{1.4}} = V^{0.29}, \tag{32}$$

so that the exponent in Eq. (30) should be

$$\gamma = \frac{0.16}{0.29} = 0.55. \tag{33}$$

280   The dotted lines in Fig. 5(b) illustrate the expected power-law relation. In particular, the linear increase ($\gamma = 1$) of $\frac{L}{H}$ found for constant v_{c} is way too strong. The results based on RKE are closer to the expected power law, in particular for small energy ratios. For larger values of ϵ, however, the increase is still too strong, e.g., $\gamma \approx 0.75$ for $\epsilon = 50$. These findings lead to the conclusion that considering different volumes on the same topography overestimate the increase in runout length with volume.

Figure 6 shows the complementary scenario of the same volume on different topographies. Here λ defines the characteristic
285   length scale. Assuming a constant slope angle, the energy ratio depends on l according to the relation

$$\epsilon(\lambda, l) = \epsilon(\lambda, \lambda) \frac{l}{\lambda} \tag{34}$$

for both models of v_{c} then. As expected, the runout length increases with increasing slope length (Fig. 6a). However, the increase is weaker than linear except for small values of $\frac{l}{\lambda}$ in combination with small energy ratios. As a consequence, the ratio $\frac{L}{H}$ mostly decreases with $\frac{l}{\lambda}$ (Fig. 6b). So the ratio $\frac{L}{H}$ decreases with increasing slope length if the volume is constant.

290   These findings suggest that the power-law increase of $\frac{L}{H}$ with volume observed in nature may arise from a combination of the rheology and a positive correlation of volume and slope length (or height). Legros (2002) found a power-law relation $H \propto V^{0.09}$ for the maximum height. Assuming that this relation also holds for the center of mass, combining it with the above scaling relation between volume and thickness yields

$$l \propto H \propto \lambda^{\chi} \tag{35}$$
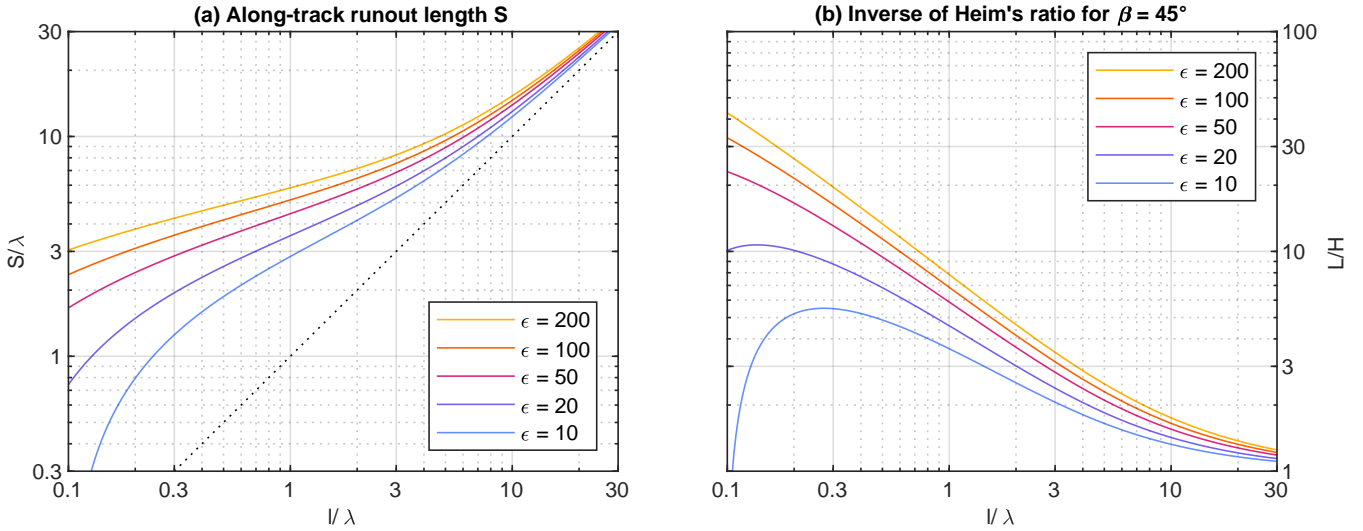
Figure 6. Runout length as a function of the slope length l for the same volume (constant λ) and the same slope angle β. Since λ is constant here, there is no difference between the version based on RKE and the version with constant v_c. The parameter ϵ is the energy ratio for $l = \lambda$ ($\epsilon(\lambda, \lambda)$ in Eq. 34). The dotted line illustrates runout to the foot of the slope ($S = l$).

295   with $\chi = \frac{0.09}{0.29} = 0.31$ for constant slope angle.

Since λ and l are no longer independent here, we cannot use either of them as a characteristic length scale. Instead, it is convenient to define the slope length l_0 at which $\lambda = l$ as a characteristic length scale, so

$$\frac{l}{l_0} = \left(\frac{\lambda}{l_0}\right)^{\chi}. \tag{36}$$

Then the energy ratio (Eq. 23) scales like

300    $$\epsilon(\lambda, l) = \epsilon(l_0, l_0)\left(\frac{\lambda}{l_0}\right)^{\chi - \frac{2}{3}}, \tag{37}$$

where the term $-\frac{2}{3}$ in the exponent occurs only in the version based on RKE. The runout length is then obtained by inserting ϵ into Eq. (22), which leads to

$$\frac{S}{l_0} = \frac{\lambda}{l_0} \ln\left(\epsilon(l_0, l_0)\left(\frac{\lambda}{l_0}\right)^{1 - \frac{2}{3}} \left(e^{\left(\left(\frac{\lambda}{l_0}\right)^{(\chi - 1)}\right)} - 1\right)\right). \tag{38}$$

Figure 7 reveals that the increase in runout length is still way too strong for the version with constant v_c. For the version based

305   on RKE, however, the increase reproduces that of natural rock avalanches strikingly well for $50 \leq \epsilon(l_0, l_0) \leq 200$.

These findings strongly support the idea of two distinct regimes of friction with a transition controlled by the amount of RKE per mass. Furthermore, it becomes clear that the relation $\frac{L}{H} \propto V^{0.16}$ is considerably affected by the correlation. Given that the results including this correlation (Fig. 7) fit the real-world relation well for $\epsilon(l_0, l_0) \geq 50$, the respective exponent in the scenario without this correlation (Fig. 5) is not lower than 0.75. Calculated back to the volume, the exponent in the power

310   law would be 0.22 or even larger instead of 0.16.
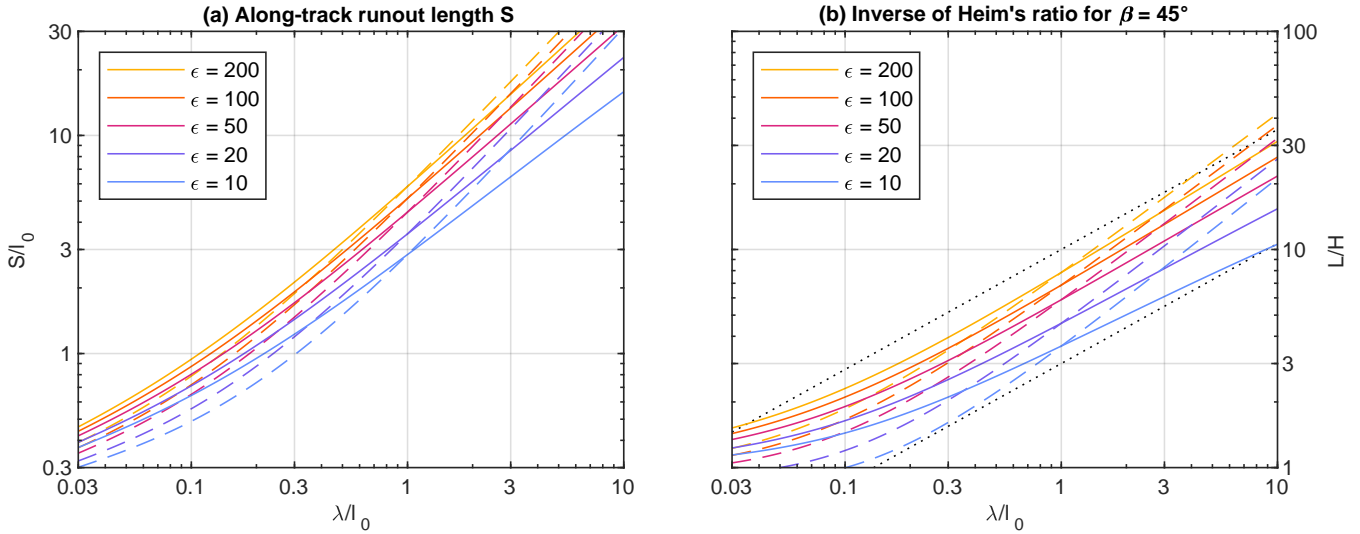
Figure 7. Runout length as a function of λ for slope length and height increasing with volume (Eq. 36 with $\chi = 0.31$). Dashed lines refer to the model with constant v_c and solid lines to the RKE model. The energy ratio in the legend refers to $\lambda = l = l_0$ ($\epsilon(l_0, l_0)$ in Eq. 37). The dotted lines reflect the power law with an exponent $\gamma = 0.55$ expected from real rock avalanches.

5 Conclusions and outlook

In this study, the widely used Voellmy rheology was reinterpreted and modified. Instead of adding a Coulomb friction term to the v^2-term that describes the processes at a rough bed, both terms were assigned to different regimes. It was assumed that the Coulomb friction applies to low flow velocities and the v^2-term to high velocities. The effective friction at high velocities

315 can be parameterized by a single length scale λ, which is proportional to the thickness and to the the parameter ξ of Voellmy's rheology.

Two different model versions were tested. The simplest form assumes a transition at a given threshold velocity v_c. The alternative approach adopts some ideas from the RKE model. While the original RKE model assumes that the kinetic energy of random particle motion reduces the effective friction, it is assumed here that it controls the transition from Coulomb friction

320 to flow (so v_c) without affecting friction itself. In a simplified form, the RKE model predicts an increase in v_c with the cube root of the length scale λ.

Using a lumped-mass model on a straight slope combined with a horizontal plane, two different scaling regimes were found. The transition is controlled by the ratio of λ and the slope length l. For $\frac{\lambda}{l} < 0.8$, the slope angle is more important than the height since the mass approaches a constant velocity along the slope. In turn, Heim's ratios much lower than typical Coulomb

325 friction coefficients occur in the height-dominated regime, where the mass is still accelerated at the foot of the slope.

The decrease of Heim's ratio of height and runout length with volume observed in nature was used for testing the two versions of the model. While the simple version with a constant threshold velocity v_c overestimates this decrease under all conditions, the version based on RKE turned out to be much better. However, the predicted decrease in Heim's ratio is still stronger than

observed in nature if different volumes are considered on the same topography. If we take into account the correlation that large
330 volumes are typically released from larger slopes than small volumes, the observed dependence of Heim's ratio on volume is
reproduced strikingly well.

These findings strongly support the modified version of Voellmy's rheology in combination with a threshold velocity v_c
derived from the concept of RKE. Furthermore, the results suggest the observed decrease in Heim's ratio with volume arises
from a combination of rheology and the positive correlation between height and volume.

335 As a limitation, the lumped-mass considerations neither take into account the increase in runout length by longitudinal
spreading nor the respective reduction in thickness and its effect on friction. It has to be tested with continuum model whether
the relations found here hold. Larsen et al. (2010) found that the scaling relations between thickness and volume are the same
for the detached volume and for the deposits. This would mean that longitudinal spreading reduces Heim's ratio systematically,
but would not affect its dependence on volume fundamentally. Following this argument, it can be expected that the lumped-
340 mass approach already captures the fundamental behavior quite well.

The new approach should be able to improve numerical continuum simulations. As a technical aspect, the strong correlation
between the parameters of the original Voellmy rheology may be reduced. This may allow for a better constraining of the
parameters and make estimates more consistent across different simulations. Scientifically, the sudden fallback from flow to
Coulomb friction may improve our understanding of the occurrence of hummocky deposit morphologies.

345 *Code availability.* All figures and further results were obtained by evaluating the respective formulas without using any numerical methods.

Competing interests. The authors declare that there is no conflict of interest.

References

Aaron, J., McDougall, S., Kowalski, J., Mitchell, A., and Nolde, N.: Probabilistic prediction of rock avalanche runout using a numerical model, Landslides, 19, 2853–2869, https://doi.org/10.1007/s10346-022-01939-y, 2022.

350 Argentin, A.-L., Hauthaler, T., Liebl, M., Robl, J., Hergarten, S., Prasicek, G., Salcher, B., Hölbling, D., Pfalzner-Gibbon, C., Mandl, L., Maroschek, M., Abad, L., and Dabiri, Z.: Influence of rheology on landslide-dammed lake impoundment and sediment trapping: Back-analysis of the Hintersee landslide dam, Geomorphology, 414, 108 363, https://doi.org/10.1016/j.geomorph.2022.108363, 2022.

Bartelt, P. and Buser, O.: Frictional relaxation in avalanches, Ann. Glaciol., 51, 98–104, https://doi.org/10.3189/172756410791386607, 2010.

Buser, O. and Bartelt, P.: Production and decay of random kinetic energy in granular snow avalanches, J. Glaciol., 55, 3–12,
355 https://doi.org/10.3189/002214309788608859, 2009.

Campbell, C. S., Cleary, P. W., and Hopkins, M.: Large-scale landslide simulations: Global deformation, velocities and basal friction, J. Geophys. Res. Solid Earth, 100, 8267–8283, https://doi.org/10.1029/94JB00937, 1995.

Christen, M., Kowalski, J., and Bartelt, P.: RAMMS: Numerical simulation of dense snow avalanches in three-dimensional terrain, Cold Reg. Sci. Technol., 63, 1–14, https://doi.org/10.1016/j.coldregions.2010.04.005, 2010.

360 Crosta, G. B., Frattini, P., Valbuzzi, E., and de Blasio, F. V.: Introducing a new inventory of large Martian landslides, Earth Space Sci., 5, 89–119, https://doi.org/10.1002/2017EA000324, 2018.

Davies, T. R. H.: Spreading of rock avalanche debris by mechanical fluidization, Rock Mech., 15, 9–24, https://doi.org/10.1007/BF01239474, 1982.

de Blasio, F. V.: Introduction to the Physics of Landslides, Springer, Dordrecht, Heidelberg, London, New York, https://doi.org/10.1007/978-
365 94-007-1122-8, 2011.

Dufresne, A., Bösmeier, A., and Prager, C.: Sedimentology of rock avalanche deposits – Case study and review, Earth Sci. Rev., 163, 234–259, https://doi.org/10.1016/j.earscirev.2016.10.002, 2016.

Gauer, P.: Considerations on scaling behavior in avalanche flow along cycloidal and parabolic tracks, Cold Reg. Sci. Technol., 151, 34–46, https://doi.org/10.1016/j.coldregions.2018.02.012, 2018.

370 Hergarten, S.: OpenLEM, http://hergarten.at/openlem, last access: 04.07.2022, 2022a.

Hergarten, S.: Self-organization of channels and hillslopes, https://doi.org/10.5281/zenodo.6794117, 2022b.

Issler, D., Jenkins, J. T., and McElwaine, J. N.: Comments on avalanche flow models based on the concept of random kinetic energy, J. Glaciol., 64, 148–164, https://doi.org/10.1017/jog.2017.62, 2018.

Johnson, B. C., Campbell, C. S., and Melosh, H. J.: The reduction of friction in long runout landslides as an emergent phenomenon, J.
375 Geophys. Res. Earth Surf., 121, 881–889, https://doi.org/10.1002/2015JF003751, 2016.

Jop, P., Forterre, Y., and Pouliquen, O.: Crucial role of sidewalls in granular surface flows: consequences for the rheology, J. Fluid Mech., 541, 167–192, https://doi.org/10.1017/S0022112005005987, 2005.

Jop, P., Forterre, Y., and Pouliquen, O.: A constitutive law for dense granular flows, Nature, 441, 727–730, https://doi.org/10.1038/nature04801, 2006.

380 Larsen, I. J., Montgomery, D. R., and Korup, O.: Landslide erosion controlled by hillslope material, Nature Geosci., 3, 247–251, https://doi.org/10.1038/ngeo776, 2010.

Legros, F.: The mobility of long-runout landslides, Engin. Geol., 63, 301–331, https://doi.org/10.1016/S0013-7952(01)00090-4, 2002.

Lucas, A., Mangeney, A., and Ampuero, J. P.: Frictional velocity-weakening in landslides on Earth and on other planetary bodies, Nat. Commun., 5, 3417, https://doi.org/10.1038/ncomms4417, 2014.

385   Mead, S. R. and Cleary, P. W.: Validation of DEM prediction for granular avalanches on irregular terrain, J. Geophys. Res. Earth Surf., 120, 1724–1741, https://doi.org/10.1002/2014JF003331, 2015.

Perla, R., Cheng, T. T., and McClung, D.: A two-parameter model of snow-avalanche motion, J. Glaciol., 26, 197–207, https://doi.org/10.3189/S002214300001073X, 1980.

Preuth, T., Bartelt, P., Korup, O., and McArdell, B. W.: A random kinetic energy model for rock avalanches: Eight case studies, J. Geophys.
390   Res. Earth Surf., 115, F03 036, https://doi.org/10.1029/2009JF001640, 2010.

Pudasaini, S. P. and Mergili, M.: A multi-phase mass flow model, J. Geophys. Res. Earth Surf., 124, 2920–2942, https://doi.org/10.1029/2019JF005204, 2019.

Salm, B.: Flow, flow transition and runout distances of flowing avalanches, Ann. Glaciol., 18, 221–226, https://doi.org/10.3189/S0260305500011551, 1993.

395   Savage, S. B. and Hutter, K.: The motion of a finite mass of granular material down a rough incline, J. Fluid Mech., 199, 177–215, https://doi.org/10.1017/S0022112089000340, 1989.

Scheidegger, A. E.: On the prediction of the reach and velocity of catastrophic landslides, Rock Mech., 5, 231–236, https://doi.org/10.1007/BF01301796, 1973.

Voellmy, A.: Über die Zerstörungskraft von Lawinen, Schweiz. Bauzeitung, 73, 212–217, https://doi.org/10.5169/seals-61891, 1955.