

1 Organic matters, but inorganic matters too: column examination
2 of elevated mercury sorption on low organic matter aquifer
3 material using concentrations and stable isotope ratios.

4 David S. McLagan^{1,2,3,*}, Carina Esser^{1,*}, Lorenz Schwab^{4,5}, Jan G. Wiederhold⁴, Jan-
5 Helge Richard⁶, Harald Biester¹.

6 1 - Institute of Geoecology, Technische Universität Braunschweig, Braunschweig, 38106, Germany.

7 2 - Department of Geological Sciences and Geological Engineering, Queen's University, Kingston, ON, K7L3N6, Canada.

8 3 - School of Environmental Studies, Queen's University, Kingston, ON, K7L3J6, Canada.

9 4 - Department for Environmental Geosciences, Centre for Microbiology and Environmental Systems Science, University
10 of Vienna, Vienna, 1090, Austria.

11 5 - Environmental Engineering Institute IIE-ENAC, Soil Biogeochemistry Laboratory, Ecole Polytechnique Fédérale de
12 Lausanne (EPFL), Sion, Switzerland.

13 6 - Institute for Hygiene and Environment Hamburg, 20539 Hamburg, Germany

14 * - These authors contributed equally to the manuscript.

15

16 Abstract

17 Sorption of mercury (Hg) in soils is suggested to be predominantly associated with organic matter
18 (OM). However, there is a growing collection of research that suggests clay minerals and Fe/Mn-
19 oxides are also important solid-phases for the sorption of soluble Hg in soil-groundwater systems.
20 We use a series of (60 mL syringe based) column experiments to examine sorption and subsequent
21 desorption of HgCl₂ solutions (Experiment 1 [EXP1]: 46.1 ± 1.1 mg L⁻¹; and Experiment 2 [EXP2]: 144
22 ± 6 mg L⁻¹) in low OM (0.16 ± 0.02 %) solid-phase aquifer materials. Analyses of total Hg
23 concentrations, Hg speciation (i.e., pyrolytic thermal desorption (PTD)), and Hg stable isotopes are
24 performed on both solid- and liquid-phase samples across sorption and desorption phases.

25 Sorption breakthrough curve best fitted a Freundlich model. Despite the very low OM content, the
26 Hg equilibrium sorptive capacity in these columns is very high: 1510 ± 100 and 2320 ± 60 mg kg⁻¹ for
27 the EXP1 and EXP2, respectively, and is similar to those determined for high OM soils. Data from the
28 experiments on mass dependent fractionation of Hg stable isotope fractionation data (described by
29 δ²⁰²Hg) support preferential sorption of lighter isotopes to the solid-phase materials with results
30 indicating isotopically heavier liquid-phase and isotopically lighter solid-phase. Desorption fits
31 exponential decay models and 46 ± 6% and 58 ± 10% of the sorbed Hg is removed from the solid-
32 phase materials at the termination of desorption in EXP1 and EXP2, respectively. The divergence of
33 δ²⁰²Hg values between liquid- and solid-phase also continues into desorption. This desorption
34 profile is linked to the initial release of easily exchangeable Hg(II) species physically sorbed to
35 Fe/Mn-oxides and clay mineral surfaces (liquid-phase enriched in heavy isotopes) and then slower
36 release of Hg(II) species that have undergone secondary reaction to more stable/less soluble Hg(II)
37 species and/or diffusion/transport into the mineral matrices (processing favouring lighter isotopes;
38 solid-phase enriched in lighter isotopes). ~~Hg-stable isotope support preferential sorption of lighter~~
39 ~~isotopes to the solid-phase materials with results indicating isotopically heavier liquid-phase and~~
40 ~~isotopically lighter solid-phase. The divergence of δ²⁰²Hg (describing mass dependent fractionation~~
41 ~~(MDF)) between liquid- and solid-phase continues into desorption and we attribute this to lighter~~
42 ~~isotopes being favoured in secondary processes occurring after initial sorption to the solid-phase~~
43 ~~materials (i.e., matrix diffusion, change in Hg(II) speciation, elemental Hg (Hg(0)) production) that~~
44 ~~lead to less exchangeable forms of Hg. Consequently, heavy isotopes are preferentially released~~
45 ~~during desorption. These observations agree with data from HgCl₂ contaminated sites.~~ The
46 secondary production of Hg(0) within the columns is confirmed by PTD analyses that indicate
47 distinct Hg(0) release peaks in solid-phase samples at <175 °C, which again agree with field
48 observations. Retardation (R_D) and distribution (K_D) coefficients are 77.9 ± 5.5 and 26.1 ± 3.0 mL g⁻¹
49 in EXP1, respectively, and 38.4 ± 2.7 and 12.4 ± 0.6 mL g⁻¹ in EXP2, respectively. These values are
50 similar to values derived from column experiments on high OM soil and provide the basis for future
51 Hg fate and transport modelling in soil-groundwater systems.

52 **Keywords:** Mercury stable isotopes, column experiments, sorption/desorption, groundwater,
53 polluted sites, distribution coefficient.

54 1 Introduction

55 Mercury (Hg), a transition metal of group 12 and period 6 of the periodic table, has a unique
56 electrochemical structure. The pair of electrons in the outermost (6s) shell have a relativistically
57 contracted radius, which greatly reduces the element's ability to form metal-metal bonds (Norrby,
58 1991). Hence, Hg is the only liquid-phase metal at standard temperature and pressure. Even with

59 this radial contraction, Hg is an atomically large element, and species in its divalent oxidation state
60 qualify as “soft-acids”, which under hard and soft Lewis acid and base theory results in Hg having
61 greater affinity for “soft-bases” (Ho, 1975). One particularly pertinent “soft-base” for Hg is sulphur.
62 Cinnabar (α -HgS) and meta-cinnabar (β -HgS) are the dominant forms of Hg in the lithosphere
63 (Gettens et al., 1972; Clarkson, 1997), but are relatively stable ores ~~that~~ have very low solubility,
64 and ~~low~~ bioavailability (Llanos et al., 2011; Lu et al., 2011). Mining of these cinnabar ores for
65 industrial use of Hg has heavily perturbed the natural biogeochemical cycle of Hg. Other primary
66 sources of Hg emissions/releases to the environment include geogenic (natural), fossil-fuel
67 combustion, industrial and medical uses of Hg, and legacy emissions from Hg polluted sites (Pirrone
68 et al., 2010; Kocman et al., 2013; Streets et al., 2019).

69 While redox conditions and organic matter (OM) availability and composition are key determinants
70 in the mobility of Hg in aquatic/saturated subsurface environments, pH (Andersson, 1979; Gu et al.,
71 2011; Manceau and Nagy, 2019), chloride concentration (Cl⁻; Schuster, 1991), and speciation of Hg
72 inputs (particularly for polluted systems; McLagan et al., 2022) also play important roles. Solubilities
73 of Hg species vary widely from practically insoluble cinnabar species ($\approx 2 \cdot 10^{-24}$ g L⁻¹) to low solubility
74 elemental Hg (Hg(0): $\approx 5 \cdot 10^{-5}$ g L⁻¹) to highly soluble Hg(II)-chloride (HgCl₂) (66 g L⁻¹) (Sanemasa,
75 1975; Schroeder and Munthe, 1998; Skyllberg et al., 2012). In systems that are OM limited, clay
76 minerals and oxides, hydroxides, and oxyhydroxides of Fe, Mn and Al become increasingly important
77 sorbents for Hg species (Lockwood and Chen, 1973; Schuster 1991; Kim et al., 2004). Additionally,
78 there is a strong tendency of Hg(II) to complex with hydroxides and halides under oxic conditions
79 (Schuster, 1991, Ullrich et al., 2001). Uptake of Hg to inorganic sorbents has been reported to occur
80 via rapid initial surface sorption followed by slower phase of Hg undergoing secondary
81 transformation to more stable/less soluble species or diffusing into the mineral matrices (Avotins,
82 1975; Miretzky et al., 2005; McLagan et al., 2022).

83 More recently, laboratory and field studies have expanded biogeochemical assays of Hg in
84 subsurface environments using stable isotopes (Jiskra et al., 2012; Zheng et al., 2018; McLagan et
85 al., 2022). Hg is an isotopic system that has seven stable isotopes and to which environmental
86 processes can impart mass-dependent (MDF) as well as both odd and even mass-independent (MIF)
87 fractionation (Bergquist and Blum, 2007; 2009; Wiederhold, 2015). In particular, this capacity for Hg
88 stable isotope analyses to elicit valuable information on tracing/identifying specific environmental
89 processes make them a vital tool in the examination of Hg biogeochemical cycling (Bergquist and
90 Blum, 2007; 2009; Wiederhold, 2015).

91 Traditionally, column and batch experiments have been utilised to assess the sorption (including
92 sorption or distribution coefficient: K_D and the related retardation coefficient: R_D) and mobility of
93 contaminants for solid-phase soil and aquifer materials. Both methods have strengths and
94 weaknesses. Batch experiments represent the simplest means to test analyte sorption, but these
95 experiments are static, and equilibrium oriented; questions about the applicability of the results to
96 natural systems with flowing water and potentially changing levels of saturation logically persist
97 (Schlüter et al., 1995 Schlüter, 1997; Van Glubt et al., 2022). Flow-through columns provide a much
98 more dynamic and manipulatable experimental environment that is also not exclusively limited to
99 equilibrium-based sorption simulations. Nonetheless, they are more laborious, difficult to replicate
100 from column to column, column boundaries (walls) can present preferential flow problems, and
101 despite the ability to manipulate the physicochemical properties of the columns this inevitably
102 underrepresents the inherent variability of actual soil/aquifer conditions (Sentenac et al., 2001;

103 USEPA, 2004). Soil contaminant transport modelling is a rapidly developing field of research and
104 provides an alternative/complementary method to these traditional experimental methods. While
105 Hg soil transport modelling is also advancing, progress is somewhat limited by the lack of
106 measurement data particularly relating to K_D values, Hg speciation and methods of assessing specific
107 processes for different soil/solid-phase materials (Leterme et al., 2014; Richard et al., 2016a).

108 Thus, it is important from both experimental and modelling standpoints that we determine effective
109 means of deriving information on sorption/mobility of Hg in soils. Lacking the capacity to measure
110 aquifer systems *in-situ*, we deem column experiments using solid-phase materials sourced from
111 sites of interest as the best available method to do so. Within this study, we aim to determine the
112 sorptive (and desorptive) capacity of low OM aquifer materials for Hg(II) using column experiments
113 and total Hg (THg) concentration, speciation, and stable isotope analyses of both solid and liquid-
114 phase materials. These experiments will be the first conducted on such low OM soil/aquifer material
115 and provide critical data into Hg transport and sorption within low OM soil and aquifer systems to
116 improve our geochemical understanding of subsurface Hg behaviour and for soil chemistry and
117 transport modelling. In addition, these column experiments on uncontaminated aquifer material
118 sourced from [an area](#) adjacent to a former industrial site at which HgCl₂ was applied as wood
119 preservative will simulate the contamination process. Data will aid our interpretation of the Hg
120 biogeochemistry in coupled soil-groundwater systems, as well as future Hg groundwater transport
121 modelling, and potentially provide guidance on contaminated site remediation.

122 2 Methods

123 2.1 Materials and experimental setup

124 The solid-phase material used in these experiments is highly permeable sand-gravel sediments
125 sourced from the saturated zone of an unconsolidated aquifer (approximate depth: 10 m) extracted
126 by a soil drill core in 2019. This site was impacted by losses of approximately 10-20 tonnes of Hg in
127 the form of high concentration HgCl₂ solution ($\approx 0.66\%$ HgCl₂) that was applied to timber as a
128 preservative (Schöndorf et al., 1999; Bollen et al., 2008; McLagan et al., 2022). The solid-phase
129 materials were extracted from outside of the plume of contaminated groundwater (Site B in
130 McLagan et al., 2022); and hence, the starting THg concentration within was very low (Table 1). [The
131 geology and structure of the soil/aquifer profile has been described in detail in previous works
132 \(Schöndorf et al., 1999; Bollen et al., 2008; McLagan et al., 2022\).](#) The material was stored in a dark
133 and cool place before drying at 30 °C for 48 hours. It was then sieved to a size of <2 mm using a
134 mesh soil sieve, which resulted in a distribution of $74.1 \pm 4.6\%$ coarse load (>2 mm; not used) and
135 $25.8 \pm 4.6\%$ fine load (<2 mm). A subsequent particle size analysis of the fine load was carried out
136 using sieving and sedimentation method (DIN ISO 11277, 2002), and results (see Table 1) categorise
137 the solid-phase aquifer materials as a sandy-loam on the soil texture triangle. A summary of the
138 properties of the investigated material is shown in Table 1.

139 *Table 1: Properties of the solid-phase aquifer material used.*

Parameter	Fe (g kg ⁻¹)	Mn (mg kg ⁻¹)	Hg (μ g kg ⁻¹)	TC (%)	TOC (%)	TIC (%)	Clay (%)	Silt (%)	Sand (%)
Value	19.2 \pm 1.5	690 \pm 160	20.4 \pm 1.0	0.50 \pm 0.03	0.16 \pm 0.02	0.34 \pm 0.03	13.5	23.2	63.3
Samples (n)	16	16	6	3	3	3	1	1	1

140

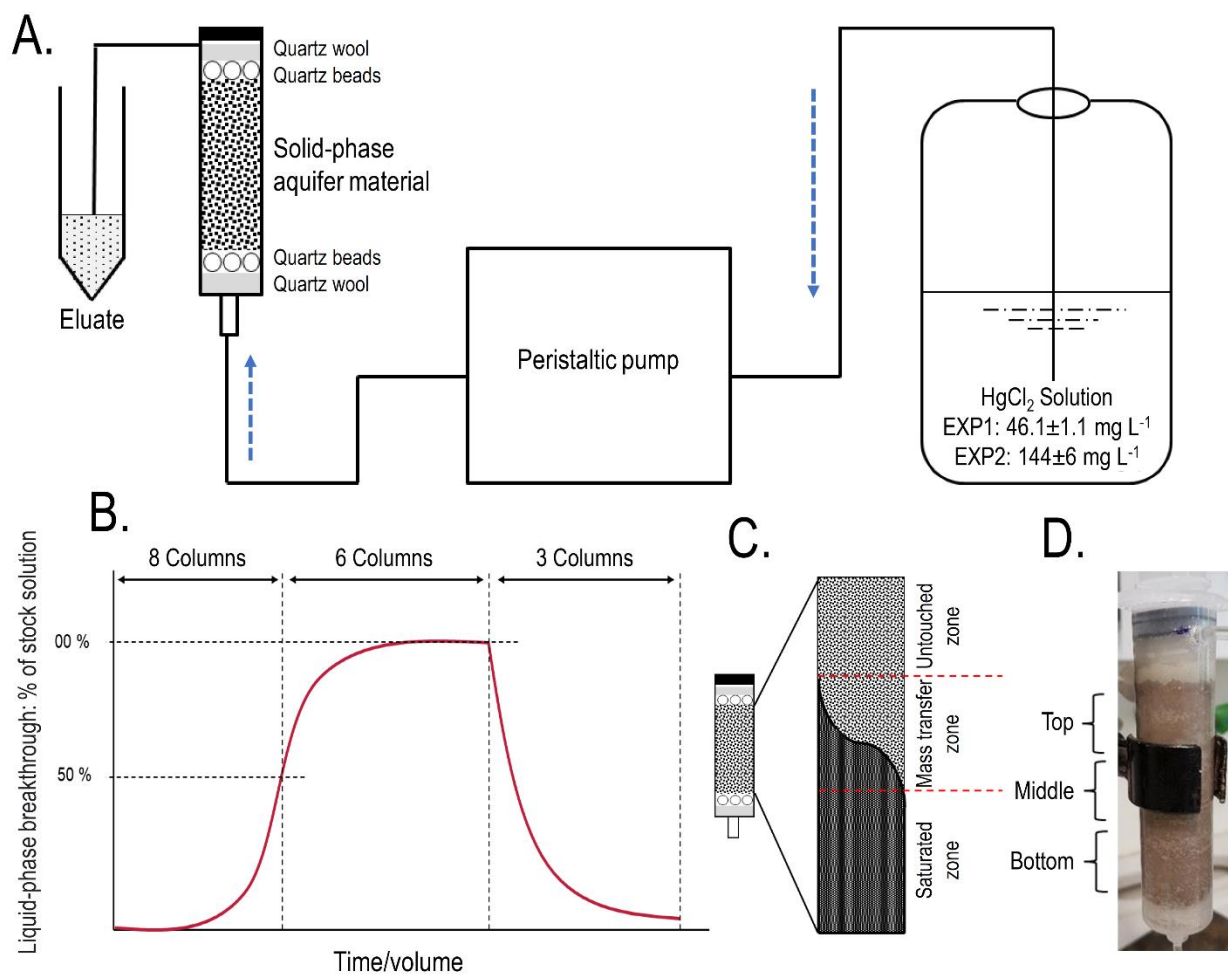
141 A set of preliminary experiments prior to experiment 1 (EXP1) and experiment 2 (EXP2) were run to
142 optimise packing methods, flow rates, stock solution concentration, and time the experiments
143 would take, and these are detailed in Section S1. Based on these preliminary data the experimental
144 setup was based on a modified version of DIN method 19528-01 (DIN 2009). 8 x 60 mL disposable
145 polypropylene syringes (height: 15.49 cm; inner diameter: 2.97 cm) were used as columns in each
146 experiment (Figure 1). The insides of the columns were roughened with sandpaper (and thoroughly
147 cleaned with surfactant and rinsed with deionised water to remove any debris) in order to
148 minimise preferential flow along the walls of the column. Each column was then filled with a layer
149 of quartz wool and a layer of quartz beads whose combined volume reached the 10 ml mark on the
150 syringe. The sieved and dried material was then transferred by ≈ 14 g aliquots into the syringes
151 (preliminary testing revealed dry packing achieved optimal column density and was best at
152 preventing separation). Each aliquot was compacted to the desired volume and the surface of each
153 aliquot was broken up before the addition of the subsequent aliquot to prevent layering between
154 each addition. The mean mass and bulk density (ρ_b) of the solid-phase aquifer materials added to
155 the columns was 70.09 ± 0.04 g and 1.42 ± 0.01 g cm⁻³, respectively, in EXP1, and 70.05 ± 0.03 g and
156 1.43 ± 0.01 g cm⁻³, respectively, in EXP2. This resulted in the height of the solid-phase materials
157 within the column being ≈ 11 cm. Additional layers of quartz beads then quartz wool (syringe volume
158 again ≈ 10 mL) were added on top of the solid-phase materials to reduce column separation and
159 particle transport. Individual columns are named C1.1 to C1.8 for EXP1 and column C2.1 to C2.8 in
160 EXP2. According to Lewis and Sjöstrom (2010), the average bulk densities range from 1.2 – 2.0 g cm³
161 for sands and 1.6 – 2.0 g cm³ for gravel. Thus, we deem the achieved bulk density of the columns to
162 be appropriate for these materials, particularly as densities of the removed coarse materials are
163 higher (solid densities are estimated at 2.65 g cm³; Lewis and Sjöstrom (2010)).

164 All column experiments were conducted under saturated conditions. Figure 1A shows the
165 configuration of the setup with the peristaltic pump upstream of the columns and flow through the
166 columns was bottom to top to minimise entrapment of air and preferential flow paths. The stock
167 solution, peristaltic pump, columns, and eluate sampling points were connected with 3.125 mm
168 (inner-diameter) polypropylene tubing (length: 105 ± 10 cm; $n = 16$). To simulate the aquifer (flow
169 velocity of $\approx 3 - 10$ m day; Schöndorf et al., 1999; Bollen et al., 2008) and prevent separation of the
170 solid-phase materials within the column, the lowest possible volume flow of 0.62 ± 0.02 ml min⁻¹ (n
171 = 16) was set across all columns (flow velocities measured before and after experiments; Section
172 S2). The stock solution was made using mixing HgCl₂ salt with tap water and stored in a 20 L
173 polyethylene container. Tap water was selected due to its inherent concentration of ions, low
174 potential for biological activity, and ease-of-use (challenges in extraction, storage, and transport of
175 large groundwater volumes from study site ≈ 600 km away). Critically, the tap water and eluate DOC
176 concentrations ($2.3 - 3.3$ mg L⁻¹) were of a similar range (even slightly less) than the values measured
177 by Richard et al (2016a) at the site these solid-phase materials were removed ($3.8 - 6.3$ mg L⁻¹). This
178 should eliminate the possibility that tap water would introduce a significant amount of artificial
179 sorption sites associated with DOC being added to the system.

180 Stock solutions were 46.1 ± 0.1 mg L⁻¹ in EXP1 ($n = 6$) and 144 ± 6 mg L⁻¹ in EXP2 ($n = 12$) and were
181 selected for (i) experimental constraints/time considerations (see Figure S1.6) and (ii) these values
182 remain between HgCl₂ concentration applied during industrial activities (6600 mg L⁻¹; spillages of
183 this solution to the top of the soil profile) and as estimates of the original concentrations of HgCl₂
184 contaminated solution entering the soil-groundwater system considering recently measured

185 groundwater concentrations up to $164 \pm 75.4 \mu\text{g L}^{-1}$ ~~are still~~ observed 55 years after ~~closure~~
 186 ~~cessation~~ of the industrial activities at the site ~~the solid-phase materials were extracted~~ (McLagan
 187 et al., 2022). The physicochemical properties of both the stock solutions and eluate were monitored
 188 across the experiments and data are listed in Section S2. Desorption was performed by replacing
 189 the stock solution with tap water flowing at the same velocity. In total (sorption, equilibrium, and
 190 desorption), EXP1 and EXP2 ran continuously for 14 days, 3 hours, and 9 minutes, and 10 days, 13
 191 hours and 4 minutes, respectively.

192 Columns were pre-conditioned with tap water for 1 week at the experimental flow velocity to allow
 193 equilibration between the solid-phase materials and the dissolved substances in the tap water, the
 194 major component of the stock solution used within the experiment. After 24 hours of pre-
 195 conditioning, NaCl salt solution tracer experiments were conducted to monitor the rate of water
 196 transfer through the columns (assuming NaCl is a conserved tracer that does not interact with the
 197 solid-phase materials). The NaCl solution was passed into the system for 10 minutes and then
 198 replaced with tap water. The change in conductivity was measured over time using a hand-held
 199 electronic conductivity meter to produce NaCl (tracer) breakthrough curves. Results show good
 200 column flow consistencies similar to the volumetric flow measurements and both data sets are
 201 described in detail in Sections S1 and S2. The system was rigorously tested and checked for leaks
 202 during both the pre-conditioning and testing phases.



203

204 *Figure 1: A. Schematic representation of the experimental setup. B. Theoretical model of the*
 205 *experiments indicating sorption and desorption phases and column termination points for solid*
 206 *phase analyses (2 columns terminated at 50% breakthrough, 3 columns terminated at ~equilibrium,*

207 and the final 3 columns terminated after desorption; end of experiment). C. Representation of the
208 zones of mass transfer of Hg during the sorption phase (“saturated zone” refers to solid-phase in
209 that zone reaching its equilibrium uptake capacity for Hg at the experimental solution
210 concentration). The dark area describes the rising front of mercury. D. Allocation of column sections
211 (≈15 mL in each section) for solid-phase analyses (“Bottom” is the solution entry point).

212 10 mL of eluate was allowed to flow off into a waste vessel before 5 mL of sample was collected
213 periods for analysis (this applied to all analyses). The liquid-phase was sampled for ~~total Hg~~ (THg)
214 concentrations consistently throughout the experiments: 38x in EXP1 (10x up to ≈50% breakthrough
215 – columns C1.1-C1.8; 11x between ≈50% breakthrough and ≈equilibrium – columns C1.1-C1.6; and
216 17x during desorption – columns C1.1-C1.3) and 35x in EXP2 (8x up to ≈50% breakthrough – columns
217 C2.1-C2.8; 16x between ≈50% and ≈100% breakthrough – columns C2.1-C2.3 and C2.6-C2.8; and 11x
218 during desorption – columns C2.1-C2.3). Liquid-phase speciation samples were collected 8x at ≈25%,
219 50%, 75% breakthrough, and ≈equilibrium, at the end of the equilibrium (immediately before stock
220 solution was changed to tap water), and ≈0% (immediately after stock solution was changed to tap
221 water), 50% and at the end of desorption for both experiments. Liquid-phase stable isotope samples
222 were collected only from columns C2.1-C2.3 in EXP2 9x in total. Collections were similar to liquid-
223 phase speciation sampling points with an additional collection during the sorption stage of the
224 experiment. After termination, solid-phase materials were analysed for THg concentrations, Hg
225 species, and Hg stable isotopes. In summary, C1.7 and C1.8 and C2.4 and C2.5 were sacrificed at
226 ≈50% breakthrough; C1.4-C1.6 and C2.6-C2.8 after equilibrium (≈100% breakthrough); while C1.1-
227 C1.3 and C2.1-C2.3 went through to the end of desorption.

228 2.2 Analyses

229 2.2.1 Liquid-phase THg and speciation analyses

230 Eluate samples for THg and Hg stable isotope analyses were immediately stabilized by adding 1% by
231 volume of 0.2 M bromine monochloride (BrCl) prepared according to Bloom et al. (2003). In order
232 to break up all of the organically bound mercury in the liquid, a reaction time of the BrCl of 24-hours
233 is recommended (US EPA method 1631, 2002). However, with little OM (Table 1), we assessed
234 sample THg analysis only 1-hour after BrCl addition and there was no impact on sample recovery
235 (Table S1.2). Immediately prior to analysis, hydroxylamine hydrochloride (NH₂OH·HCl) was added to
236 neutralize the BrCl followed by addition of tin(II) chloride (SnCl₂) solution as the Hg reducing agent.

237 Liquid-phase speciation analyses followed the same methods described elsewhere (Bollen et al,
238 2008; Richard et al., 2016b; McLagan et al., 2022). We describe this method is described as a
239 complementary, semi-quantitative-qualitative analytical tool and produces four distinct “fractions”
240 of the total pool of liquid-phase Hg: (i) elemental Hg (Hg(0)) (purged from untreated eluate sample),
241 (ii) dissolved inorganic Hg(II) termed Hg(II)A; (purged after reduction with SnCl₂ treatment; e.g.
242 HgCl₂); (iii) DOM-bound Hg(II) termed Hg(II)B (purged after BrCl and SnCl₂ treatment), and (iv)
243 particulate Hg termed Hg(II)P (difference between THg concentrations in filtered and total
244 unfiltered eluate samples). Both concentration and speciation results were measured using a cold-
245 vapor atomic absorbance spectrometer (CV-AAS) (Hg-254 NE, Seefelder Messtechnik GmbH,
246 Germany) according to DIN method 1483 (2007) and USEPA method 1631 (2002). Confidence in
247 liquid phase Hg(0) concentrations is higher than for other species, as these result from purging
248 untreated/unstabilised samples of Hg(0) with nitrogen gas directly into the CV-AAS; all Hg(0)
249 samples were analysed within 30 mins of sample collection.

250 2.2.2 Solid-phase THg and speciation analyses

251 After individual columns were sacrificed for solid-phase analyses, the ends of the columns were
252 sealed to prevent the columns from draining and stored in the same upright position as the
253 experimental setup (Figure 1) to prevent further disturbance. Columns were cut into sections (Figure
254 1D), homogenised and subset within 1 week of the end of the experiments and stored at 4 °C in
255 brown (opaque) falcon tubes until digestions or analyses. All analyses were performed on wet
256 samples to minimise any potential losses of Hg(0)~~All analyses were performed on wet samples to~~
257 ~~ensure there were no losses of Hg(0)~~. The moisture content of solid-phase samples was determined
258 on separate aliquots for each column by difference after drying at 35 °C and was $23 \pm 2\%$ ($n = 48$)
259 (Section S8).

260 THg and Hg stable isotope analyses were cold digested in modified aqua regia following the methods
261 described in McLagan et al. (2022) (8 mL HCl, 3 mL HNO₃, and 1 mL BrCl~~1 mL nitric acid replace with~~
262 ~~1 mL BrCl~~). Analyses of THg concentrations from the digestion extracts were determined using CV-
263 AAS following DIN method 1483 and USEPA method 1631. Results are reported on a dry weight basis
264 and moisture content was determined by difference after baking at 105 °C using aliquots of the
265 solid-phase sample (Section S8). Due to the low concentrations in the original solid-phase aquifer
266 materials, THg concentrations were measured with a DMA80 (Milestone SCI) via thermal
267 decomposition, amalgamation, and AAS (Table 1).

268 Speciation analyses were performed by pyrolytic thermal desorption (PTD), which continually
269 measures Hg at 254 nm within an AAS detector that is connected to a sample combustion furnace
270 that heats samples from room temperature to 650°C at 1°C per minute in a stream of N₂ gas. This
271 method is described in detail by Biester and Scholz (1996). The sample release curves were
272 compared to the release curves for a series of Hg reference materials (Hg(0), HgCl₂, Hg₂Cl₂ (calomel),
273 cinnabar: α-HgS, metacinnabar: β-HgS, and Hg²⁺-sulphate: HgSO₄) in silicon dioxide (SiO₂) matrix
274 (see Section S9 for reference material curves) to qualitatively assess the species or “fractions” of Hg
275 present in the samples.

276 2.2.3 Liquid- and solid-phase Hg stable isotope analyses

277 Samples for stable Hg isotope analyses included stabilized liquid-phase eluate samples and solid-
278 phase aqua-regia extracts diluted with deionised water (18.2 MΩ cm). Liquid-phase samples were
279 collected in 15 mL polypropylene tubes and stabilized with BrCl to reach 1% of the sampled volume.
280 Analyses were made using a Nu Plasma II (Nu Instruments) multicollector inductively coupled
281 plasma mass spectrometer (MC-ICP-MS) with a cold-vapor generator (HGX-200; Teledyne Cetac)
282 that allows direct addition of Hg(0) into MC-ICP-MS plasma by reducing all Hg in samples with SnCl₂.
283 The isotope ratios were determined relative to NIST-3133 (National Institute of Standards and
284 Technology; NIST) using the standard bracketing approach and corrected for mass-bias using
285 thallium (Tl) doping from NIST-997 (NIST) introduced using an Aridus-2 desolvating nebulizer
286 (Teledyne CETAC). MDF was assessed by variation in $\delta^{202}\text{Hg}$, while $\Delta^{199}\text{Hg}$, $\Delta^{200}\text{Hg}$, $\Delta^{201}\text{Hg}$, and
287 $\Delta^{204}\text{Hg}$ were used to assess MIF of odd and even isotopes) (see Grigg et al., 2018; McLagan et al.,
288 2022 for method details).

289 2.2.4 Complementary analyses

290 Metal cations in the solid- and liquid-phases were measured with inductively coupled plasma optical
291 emission spectrometry (ICP-OES; Varian 715-ES; Agilent Technologies Inc.). Solid-phase total carbon

292 (TC), total organic carbon (TOC), and total inorganic carbon (TIC; dissolved by hydrochloric acid)
293 were measured by infra-red detection of CO₂ released (DIMA 1000NT; Dimatec, Germany).
294 Dissolved organic carbon of stock solution and eluate was measured with a carbon/nitrogen
295 analyser (Multi N / C 2100; Analytic Jena) (see Section S2). Liquid-phase dissolved oxygen content,
296 redox potential, electrical conductivity, and pH were measured by handheld probes.

297 2.2.5 Retardation (R_D) and sorption/partitioning/distribution (K_D) coefficient calculations

298 The retardation coefficient (R_D) is essentially the ratio of the velocity of the water front (v_w) and
299 velocity of the Hg front delayed by sorption processes (v_{Hg}) moving through the columns (Equation
300 1). Since the path of the the soluble pollutant (Hg) and water are the same, transport time can be
301 determined based on the time it takes the fronts to pass through the columns (t_{Hg} and t_w ,
302 respectively). NaCl breakthrough curve was used as a proxy for water based on the assumption it is
303 a conservative tracer. t_{Hg} and t_w are given when the respective ratios of the NaCl and THg
304 concentrations in the eluate is equal to half the input concentration (stock solution; $C_{eluate} / C_{initial} =$
305 0.5) (Patterson et al., 1993; Reichert, 1991; Schnaar and Brusseau, 2013).

$$306 R_D = v_w / v_{Hg} = t_w / t_{Hg} \quad \text{Equation 1}$$

307 R_D is related to the sorption or partitioning or distribution coefficient (K_D ; mL g⁻¹) according to
308 Equation 2 and Equation 3 (USEPA, 2004):

$$309 R_D = 1 + (\rho_b / n_e) K_D \quad \text{Equation 2}$$

$$310 K_D = (R_D - 1) (n_e / \rho_b) \quad \text{Equation 3}$$

311 Where, n_e is the effective porosity (EXP1: 0.470 ± 0.008, $n = 3$; EXP2: 0.459 ± 0.004, $n = 3$; assumed
312 to be equal to total porosity), which is the ratio of the column pore volume (EXP1: 23.3 ± 0.5 mL, n
313 = 3; EXP1: 22.5 ± 0.1 mL, $n = 3$) to the total volume of the solid-phase materials of the columns (EXP1:
314 49.7 ± 0.3 mL, $n = 3$; EXP2: 49.0 ± 0.5 mL, $n = 3$). R_D could only be calculated for columns that went
315 to equilibrium and desorption (not 50% breakthrough), n_e was calculated for columns that went
316 through desorption (C1.1-C1.3 and C2.1-C2.3); and hence, K_D was only calculated for these columns.
317 Note, the pore volumes reported above are the data used when reporting the number of pore
318 volumes.

319 2.3 Quality Assurance and quality control (QAQC)

320 For liquid-phase analyses, a 140.8 ng L⁻¹ Hg(II) stock solution (Sigma Aldrich) was measured
321 throughout the analyses and recovery was 99 ± 5% ($n = 250$). For solid-phase analyses, Chinese Soil
322 (NCS DC73030; Chinese National Analysis Centre for Iron and Steel) was measured and recovery was
323 101 ± 6% ($n = 16$). The accuracy and precision of Hg stable isotope measurements was assessed
324 using the “in-house” *ETH Fluka* standard. Mean values across the measurement sessions were:
325 $\delta^{202}\text{Hg} = -1.42 \pm 0.08 \text{ ‰}$; $\Delta^{199}\text{Hg} = 0.08 \pm 0.02 \text{ ‰}$; $\Delta^{200}\text{Hg} = 0.02 \pm 0.02 \text{ ‰}$; $\Delta^{201}\text{Hg} = 0.03 \pm 0.03 \text{ ‰}$;
326 $\Delta^{204}\text{Hg} = -0.01 \pm 0.06 \text{ ‰}$ ($n = 26$; all uncertainty values are reported as 2SD). All uncertainties are
327 1SD, unless otherwise reported (i.e., 2SD used to report Hg stable isotope analysis uncertainty).
328 These values are within the range of other studies (i.e., Obrist et al., 2017; Goix et al., 2019; McLagan
329 et al., 2022). Theoretical solid-phase THg concentration (compared to measured THg
330 concentrations) are determined via mass balance of liquid-phase THg concentrations of stock

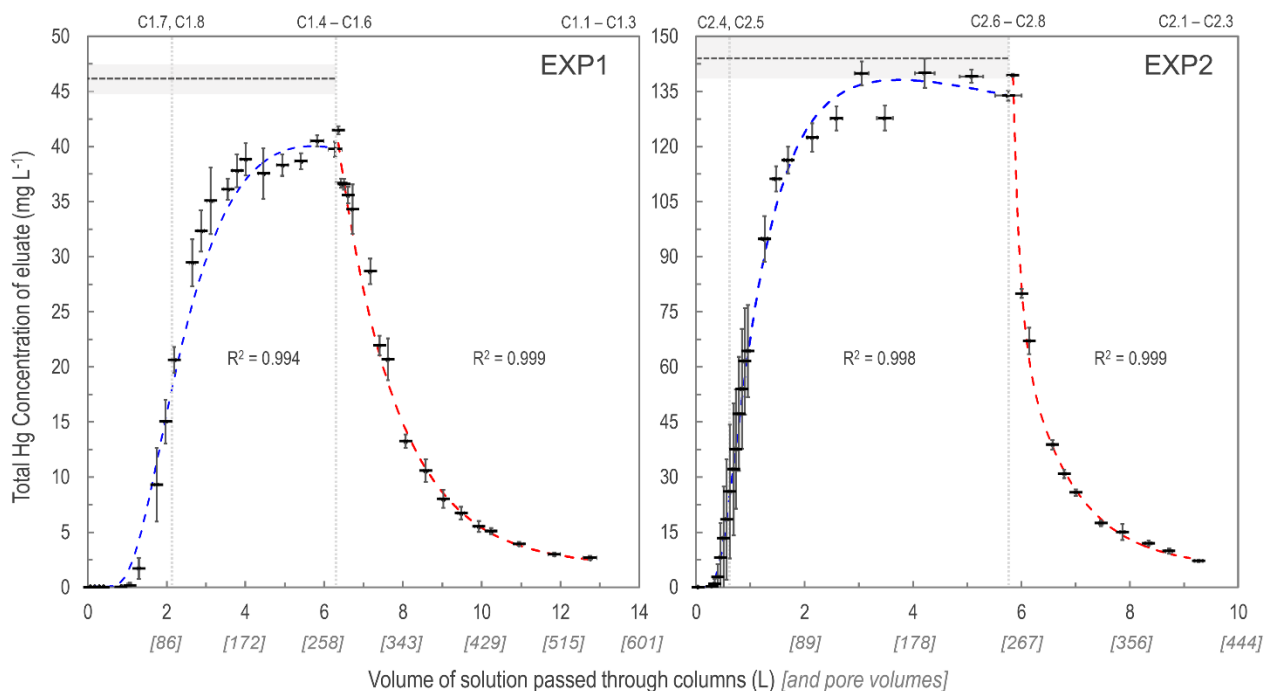
331 solution and eluate and the volume of stock solution applied to the columns. All statistical tests and
332 sorption fitting comparisons were performed in OriginPro 2018 (Origin Lab Corporation).

333 3 Results and discussion

334 3.1 Sorption and desorption behaviour of mercury in column experiments

335 3.1.1 Sorption

336 As expected, the uptake of the HgCl_2 solution to the solid phase aquifer materials followed an S-
337 shaped breakthrough curve best described by ~~the a~~ Freundlich ~~function model~~ (Figure 2; note these
338 are empirically fitted functions). Initially, >99.9% of the Hg in solution was sorbed to the solid phase
339 materials and 1.0-1.3 L (43 – 55 pore volumes) and 0.3-0.45 L (13 – 16 pore volumes), in EXP1 and
340 EXP2, respectively, was required to reach eluate THg concentrations equivalent to 1% of stock
341 solution (Section S5). This was followed by a phase of rapid increase in the eluate concentrations
342 (decreasing fraction of the Hg in solution sorbing to the solid-phase). Finally, the increase in eluate
343 THg concentration slowed as it approached the upper asymptotic bound of the original stock
344 solution concentration in each experiment and equilibrium of Hg fluxes between the solid- and
345 liquid-phases was approached/reached. EXP1 likely did not completely reach a stable equilibrium
346 point (eluate concentration was at $\approx 91\%$ of stock solution concentration when the stock solution
347 was changed to water), and more time/volume of solution was required. This would have required
348 creation of more stock solution; instead, green chemistry prevailed, and the choice was made to
349 move onto the desorption phase with consideration of the higher concentration (faster) follow-up
350 EXP2.



351

352 *Figure 2: Total Hg concentration eluate breakthrough curves for low (EXP1; left panel) and high*
353 *(EXP2; right panel) concentration stock solution experiments. Horizontal dashed lines (mean) and*
354 *shaded area (1SD) indicate the original stock solution concentrations in each experiment and vertical*
355 *dotted lines indicate column removal points (column IDs above panels indicate which columns were*
356 *removed). Uncertainty in the x-axis relates to the differing volumes passed through individual*
357 *columns at each sampling period. Sorption curves were fitted with Freundlich functions (blue dashed*
358 *lines), and desorption curves were fitted with exponential decay functions (red dashed lines). These*

359 *functions were empirically (not mechanistically) fitted to the data as these plots are not sorption*
360 *isotherms (see. These relationships presented the best fits compared to the fit of sorption functions*
361 *and full details of these functions are listed in Section S6 for details of fitting functions).*

362 This *S-shaped sorption* behaviour was similar to the one other detailed study on Hg sorption in
363 natural soils with sufficient liquid-phase sampling frequency to create column breakthrough curves
364 on OM-rich (9.4 – 24.7% OM) Amazonian soils and similar stock solution concentrations (60 – 120
365 mg L⁻¹; Miretzky et al., 2005). *Qualitative-Semi-quantitative* liquid-phase Hg speciation analyses
366 confirm that the majority of Hg was dissolved inorganic Hg(II) (EXP1: 83 ± 6%; EXP2: 77 ± 8%), a
367 fraction of which will be soluble HgCl₂ (species used to generate stock solution), but also fractions
368 of hydrolysed species (i.e., HgClOH, Hg(OH)₂, [HgCl₃]⁻) formed in solution at pH in the observed range
369 (7.7 – 8.1) of these experiments (Delnomdedieu et al., 1992; Gunneriusson and Sjöberg, 1992; Kim
370 et al., 2004; see also Section S10 for theoretical Hg speciation results using Visual MINTEQ v3.1).
371 These liquid-phase Hg speciation results are similar to those reported for groundwater samples
372 previously collected at the contaminated site where these materials were extracted from (Bollen et
373 al., 2008; Richard et al., 2016a; McLagan et al., 2022).

374 Despite the very low OM content (Table 1) within these solid-phase aquifer materials, the
375 equilibrium uptake capacity was very high in both experiments. These concentrations were
376 determined both (i) analytically by solid-phase THg analyses, and (ii) theoretically, based on the
377 inverse of the breakthrough curve integral: the area above the curve and below the stock solution
378 concentration. This has been referred to as “holdup” (*H*; mg of Hg), (Van Genuchten and Parker,
379 1984) and is described in Equation 4:

$$380 \quad H = [C_0 V_f - \int C_e dV] \quad \text{Equation 4}$$

381 Where, *C_e* is the eluate THg concentration (mg L⁻¹), *C₀* is the stock solution THg concentration (mg
382 L⁻¹), and *V_f* is the accumulated solution volume that has passed through the columns at the point
383 they were removed (L). Theoretical concentrations reached 1880 ± 20 mg kg⁻¹ in EXP₁ and 2810 ±
384 40 mg kg⁻¹ in EXP₂ (Table 2; Section S3). These data are directly comparable, and indeed within the
385 same range as the theoretical solid-phase concentrations calculated by Miretzky et al. (2005) for the
386 OM-rich Amazonian soils (THg concentrations: 950 – 3960 mg kg⁻¹). The elevated Hg sorption
387 observed by Miretzky et al. (2005) is to be expected due to the affinity of Hg for OM (e.g., Yin et al.,
388 1996; Jiskra et al., 2015; Manceau and Nagy, 2019). Nonetheless, Miretzky et al. (2005) found their
389 calculated solid-phase THg concentrations at equilibrium (sorptive capacity of the soils) were
390 greater when OM% + clay% was considered rather than OM% alone was considered (Miretzky et al.,
391 2005), which highlights the potential role clay (and oxide) minerals can play in Hg sorption to solid-
392 phase soil or aquifer materials.

393 Hg sorption to OM has been observed to increase at lower pH (Andersson, 1979; Yin et al., 1996).
394 However, the opposite has been reported for sorption of Hg to clay minerals: in neutral and slightly
395 basic soils, the sorption capacity is controlled by the mineral components (Andersson, 1979;
396 Schuster, 1991; Gabriel and Williamson, 2004). Indeed, the pH range of the eluate and stock solution
397 (pH range: 7.7 – 8.1) present ideal conditions for Hg sorption to clay minerals and Fe and Mn
398 (oxy)hydroxide minerals. Hg sorption to these inorganic minerals becomes more likely in our
399 experiments considering the very low OM content of the solid-phase materials (Table 1). Haitzer et
400 al. (2002) estimated that at ratios of THg-to-OM above 1 µg of Hg per mg of OM the strong thiol-
401 group bonding sites for Hg within OM are saturated. Based on the TOC data of these solid-phase

402 materials (assuming 0.16% TOC = 0.32 % OM), there would be 224 mg of OM within a column. To
 403 surpass the ratio of 1 µg of Hg per mg of OM, only 4.9 and 1.6 mL of stock solution or 0.21 and 0.07
 404 pore volumes in EXP1 and EXP2, respectively, would need to be added to the columns to saturate
 405 the strong thiol-group binding sites with Hg. Considering that Hg breakthrough occurred only after
 406 about 50 and 15 pore volumes in EXP1 and EXP2, respectively, it can be assumed that not only the
 407 strong Hg-binding thiol-groups but also the other less strong Hg-binding functional groups (e.g.,
 408 carboxyl groups) of the small OM pool in the columns were fully saturated early in the experiments.
 409 Hence, solid-phase sorption of Hg within these experiments was dominated by interactions with
 410 inorganic minerals. The role of such inorganic minerals was also highlighted in one of the few studies
 411 that exist examining Hg transport and fate in aquifers (Lamborg et al., 2013).

412 *Table 2: Theoretical (liquid-phase THg mass-balance) and measured solid-phase THg concentrations*
 413 *and recoverys of the measured-to-expected (theoretical) concentrations for each the columns in*
 414 *EXP1 and EXP2.*

Experiment 1 (EXP1; 46.1 ± 1.1 mg L ⁻¹)					Experiment 2 (EXP2; 144 ± 6 mg L ⁻¹)				
Column	Stage	Theoretical Hg conc. (mg kg ⁻¹)	Measured Hg conc. (mg kg ⁻¹)	Recovery	Column	Stage	Theoretical Hg conc. (mg kg ⁻¹)	Measured Hg conc. (mg kg ⁻¹)	Recovery
C1.1	Desorption	820	722 ± 91	88.0%	C2.1	Desorption	1360	1060 ± 230	78.3%
C1.2	Desorption	890	877 ± 206	98.6%	C2.2	Desorption	1300	786 ± 390	60.2%
C1.3	Desorption	847	835 ± 120	98.6%	C2.3	Desorption	1490	1050 ± 57	70.1%
C1.4	Equilibrium	1870	1470 ± 221	78.5%	C2.4	50% breakthrough	1030	785 ± 220	76.1%
C1.5	Equilibrium	1910	1630 ± 286	85.1%	C2.5	50% breakthrough	1140	702 ± 330	61.4%
C1.6	Equilibrium	1870	1440 ± 92	77.1%	C2.6	Equilibrium	2770	2380 ± 452	86.1%
C1.7	50% breakthrough	1320	1470 ± 384	111.3%	C2.7	Equilibrium	2850	2320 ± 388	81.2%
C1.8	50% breakthrough	1300	960 ± 524	73.6%	C2.8	Equilibrium	2820	2260 ± 272	79.8%

415

416 Measured THg concentrations were typically lower than the theoretical calculated values (Table 2)
 417 and contaminant masses can be difficult to balance in contaminant batch and column experiments
 418 (Van Genuchten and Parker, 1984; Hebig et al., 2014). This is of particular concern for a contaminant
 419 such as Hg whose stability and contamination issues have been widely studied due to the capacity
 420 of different Hg species to sorb to and diffuse through plastic polymers (at differing rates) (Hall et al.,
 421 2002; Parker and Bloom, 2005; Hammerschmidt et al., 2011). Loss of a fraction of the THg in solution
 422 to/through tubing and the walls of the column is likely contributing to the lower recovery in some
 423 of these samples. Other factors that could be contributing to the differences between the
 424 theoretical and measured concentrations are heterogeneity of the solid-phase and solid-phase
 425 sample extraction (particularly during movement of the Hg mass transfer front), loss of Hg from
 426 solid-phase before sample extraction and analyses (particularly for volatile Hg(0); Parker and Bloom,
 427 2005), and inherent analytical uncertainties. The heterogeneity of the materials is emphasized by
 428 the absence of trends in THg concentrations within the sections of the columns, even for the
 429 columns undergoing movement of the mass transfer zone (see Section S8). Unfortunately, Miretzky
 430 et al. (2005) did not provide total sampling volumes for their experiments and no assessment of
 431 measured THg recoveries was (or can be) made for direct comparison to our recovery data.

432 3.1.2 Desorption

433 The desorption phase of both EXP1 and EXP2 followed an exponential decay model; results confirm
 434 that sorption is (partially) reversible and initially rapid (Figure 2). After the stock solution was

435 switched to water for the desorption phase, the eluate solution reached <50% of the stock solution
436 THg concentration with additions of ≈ 1 L (≈ 43 pore volumes) and ≈ 0.5 L (≈ 22 pore volumes) of
437 solution in EXP1 and EXP2, respectively (Figure 2). At the termination of the experiments eluate THg
438 concentrations dropped to <10% of the original stock solution (Figure 2). While it is evident that
439 more Hg would have been released if desorption was permitted to proceed further (terminated due
440 to time and to prevent excess contaminated waste solution), measured data indicated that $46 \pm 6\%$
441 (Theoretical: $55 \pm 2\%$) in EXP1 and $58 \pm 10\%$ (Theoretical: $51 \pm 4\%$) in EXP2 of THg could be extracted
442 from the solid-phase materials before the experiments were terminated. Evidence from the
443 contaminated aquifer where these solid-phase materials were extracted suggest that the retention
444 of a fraction of this Hg within the solid-phase materials is long-term (Bollen et al., 2008; McLagan et
445 al., 2022). McLagan et al. (2022) report that elevated solid- (up to 562 mg kg^{-1}) and liquid-phase (up
446 to $164 \pm 75.4 \text{ } \mu\text{g L}^{-1}$) THg concentrations are still found at the site to the present day, more than 55
447 years since the industrial use of Hg (kyanisation) at the site ceased.

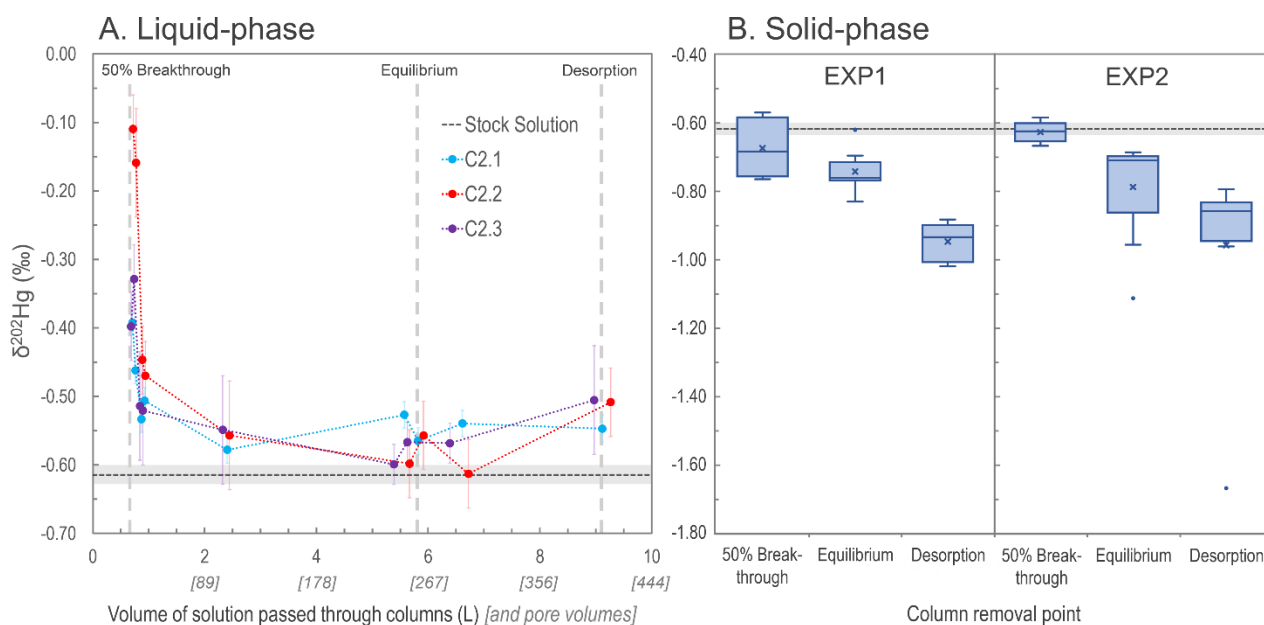
448 ~~The authors of that~~ McLagan et al. (2022) study associate this residual retention of Hg to the
449 diffusion of Hg into the mineral matrix or secondary transformation to a more stable (and less
450 soluble) Hg(II) species (McLagan et al., 2022). Previous work agrees that sorption and subsequent
451 release of Hg to/from solid-phase soils and solid-phase materials is likely controlled by multiple
452 processes (Yin et al., 1997; Bradl, 2004; Reis et al., 2016). The more easily extractable Hg is likely to
453 be associated with Fe and Mn (oxy)hydroxide, and clay minerals through outer-sphere complexes
454 that form through cation exchange and electrostatic intermolecular forces (Bradl, 2004; Reis et al.,
455 2016). Over time, some of the Hg associated through these weaker surface interactions will diffuse
456 into the matrix and/or form inner-sphere complexes, processes that both slow the release of the
457 sorbed Hg (Bradl, 2004; Reis et al., 2016). Similar results were observed by Miretzky et al. (2005) in
458 the OM rich Amazonian soil columns with 27 - 38% of Hg sorbed to the solid-phase materials being
459 rapidly redissolved in the initial desorption phase. However, the soils with higher OM content
460 showed stronger hysteresis and considerably less Hg was released during the second phase of
461 desorption (Miretzky et al., 2005) than in our low OM solid-phase materials suggesting stronger
462 interactions of inner-sphere complexed Hg with OM; results supported by work done in other
463 studies examining Hg sorption to solid-phase materials (Yin et al., 1996; Reis et al., 2016).

464 3.1.3 Insights from stable Hg isotopes

465 Variations in $\delta^{202}\text{Hg}$ values, describing MDF of Hg isotopes, were observed in both the liquid- and
466 solid-phase across the experiments (Figure 3; Section S7; Section S8). During the initial phase of the
467 experiments (before eluate breakthrough), transfer of Hg from the applied stock solution
468 ($\delta^{202}\text{Hg}$: $-0.61 \pm 0.01\%$ relative to NIST-3133, 1SD; $n = 3$) to the solid-phase materials is complete.
469 When there is complete transfer of a “pool” of Hg from reactants to products there is complete
470 transfer of stable isotopes; and hence no fractionation can be observed.

471 Once Hg begins to breakthrough the columns, the eluate is initially enriched in heavy isotopes
472 associated with the preferential transfer (sorption) of lighter isotopes to the solid-phase materials
473 (Jiskra et al., 2012; Wiederhold, 2015) with heavier isotopes retained in solution ~~and~~ (passed into
474 the eluate). In all three of the EXP2 columns examined for stable isotopes in the liquid-phase, the
475 first two liquid-phase stable isotope samples (sampled just after $\approx 50\%$ breakthrough column
476 removals) had more positive $\delta^{202}\text{Hg}$ values than the remaining liquid-phase samples (Figure 3).
477 However, it is also apparent that at $\approx 50\%$ breakthrough, there was little MDF imparted on the solid-
478 phase materials compared to the stock solution (Figure 3). This ostensibly contrasting finding

479 (observable positive MDF in the liquid-phase and little negative MDF in the solid-phase) can be
 480 explained by the proportion of Hg transferred to the solid-phase of the total mass added in solution.
 481 At the 50% breakthrough column removal, the proportion of Hg sorbed by the columns was 95.4
 482 and 90.4%, respectively for C1.7 and C1.8 (EXP1) and 83.8 and 88.5%, respectively for C2.4 and C2.5
 483 (EXP2; based on theoretical calculations). The majority of this sorption occurred during the complete
 484 (or near-complete) transfer of isotopes before (or just after) eluate breakthrough. Hence, the MDF
 485 that began to occur after breakthrough (observable in the early liquid-phase eluate samples) had
 486 little influence on the Hg stable isotope ratios of the solid-phase materials of columns removed at
 487 the $\approx 50\%$ breakthrough point.



488

489 *Figure 3: Development of liquid-phase $\delta^{202}\text{Hg}$ values for columns C2.1 – C2.3 measured at nine*
 490 *intervals during EXP2 (Panel A) and box plots of solid-phase $\delta^{202}\text{Hg}$ values measured in both EXP1*
 491 *and EXP2 (“x” denotes mean values, dots denote outliers) (Panel B). In both panels, the grey dash*
 492 *line represents the mean $\delta^{202}\text{Hg}$ value (light grey rectangle: 1SD) measured for the stock solution.*
 493 *Note, the vertical grey dashed lines indicating solid-phase column removal points in the left panel*
 494 *are only approximations as the liquid-phase stable isotope measurements were only made on*
 495 *columns C2.1-2.3 that proceeded until the end of desorption.*

496 This process-finding of limited MDF on solid phase materials at $\approx 50\%$ breakthrough is further
 497 supported when examining consistent with the $\delta^{202}\text{Hg}$ values observed within the column layers
 498 at $\approx 50\%$ breakthrough. The bottom layers of C1.7 ($\delta^{202}\text{Hg}$: $-0.76 \pm 0.07\text{‰}$) and C1.8 ($\delta^{202}\text{Hg}$: $-0.75 \pm$
 499 0.07‰) in EXP1 were more negative than the stock solution, while the top layers ($\delta^{202}\text{Hg}$: $-0.57 \pm$
 500 0.15‰ and $\delta^{202}\text{Hg}$: $-0.59 \pm 0.07\text{‰}$ for C1.7 and C1.8, respectively) were equivalent to the stock
 501 solution (Section S8). These data suggest observable MDF was beginning to occur in the part of the
 502 column exposed to the Hg front (bottom) for the longest. The same was not the case in EXP2 (no
 503 observable trend in $\delta^{202}\text{Hg}$ between layers; Section S8). We attribute this to the more elevated THg
 504 concentrations and faster movement of the Hg front moving through the columns (see Table 3
 505 below) in EXP2 overwhelming the layering MDF observed in EXP1.

506 As sorption progresses to equilibrium, we observe a negative shift in the eluate $\delta^{202}\text{Hg}$ value of all
 507 three columns falling in the range of ≈ -0.6 to -0.5‰ , which is slightly more positive than the stock
 508 solution ($\delta^{202}\text{Hg}$: $-0.61 \pm 0.01\text{‰}$ 1SD; $\pm 0.08\text{‰}$ analytical 2SD; Figure 3). During this transition in the

509 Hg uptake process the net effect is that most, and then essentially all, Hg input from the stock
510 solution is passing through the columns and into the eluate and any kinetic MDF occurring would
511 be limited. Nonetheless, equilibrium-based isotope exchange would also drive lighter isotopes into
512 the solid-phase materials (Wiederhold et al., 2010; Jiskra et al., 2012; Wiederhold, 2015), which is
513 the likely explanation for the liquid-phase $\delta^{202}\text{Hg}$ values remaining slightly more positive than the
514 stock solution. While the impact of this MDF on the continuously flowing eluate is small when the
515 system is at equilibrium, the effect of this equilibrium-based MDF on the solid-phase is more
516 manifest as its effect is cumulative. Over time, more and more lighter isotopes preferentially sorb
517 to the solid-phase; and hence, the mean $\delta^{202}\text{Hg}$ values of the solid-phase materials in EXP1
518 ($\delta^{202}\text{Hg}$: $-0.74 \pm 0.06\text{‰}$ 1SD) and EXP2 ($\delta^{202}\text{Hg}$: $-0.79 \pm 0.15\text{‰}$ 1SD) at the end of the sorption
519 experiments (at or near column equilibrium) are more negative than the stock solution (and solid-
520 phase materials at $\approx 50\%$ breakthrough). Thus, we suggest equilibrium-based MDF (with some
521 potential for kinetic MDF contributions) to be the primary driver of the more negative $\delta^{202}\text{Hg}$ values
522 observed in the solid-phase materials at the end of the equilibrium-phase of the experiments. These
523 observations agree with the observed results of McLagan et al. (2022) sampled within the
524 contaminated aquifer adjacent to which these uncontaminated materials were derived.

525 At the end of the desorption phase, the solid-phase materials have undergone further MDF to more
526 negative $\delta^{202}\text{Hg}$ values (EXP1 $\delta^{202}\text{Hg}$: $-0.95 \pm 0.05\text{‰}$; EXP2 $\delta^{202}\text{Hg}$: $-0.96 \pm 0.27\text{‰}$ 1SD). Two of the
527 three columns monitored for liquid-phase stable isotopes at the end of desorption also show a slight
528 positive MDF shift and values for all three columns are slightly more positive ($\delta^{202}\text{Hg}$: -0.55 to -0.51
529 ‰) than the stock solution (Figure 3). As discussed, desorption proceeds via a two-step mechanism:
530 a rapid initial desorption as easily exchangeable, outer-sphere complexed Hg is released, followed
531 by a slower phase of desorption as this easily exchangeable pool depletes. Brocza et al. (2019) and
532 McLagan et al. (2022) suggest that this easily exchangeable pool is enriched in heavier isotopes
533 compared to the fraction that diffuses into the mineral matrix or transforms to more stable, less
534 soluble Hg(II) species as these secondary processes favour lighter isotopes. Thus, removal of the
535 heavy isotope enriched, easily exchangeable pool of Hg is the likely driver of more negative $\delta^{202}\text{Hg}$
536 values in the solid-phase materials after desorption. While Demers et al. (2018) studied
537 predominantly surface water samples linked to Hg soil-groundwater contamination at a site in
538 Tennessee, USA (industrial use of Hg(0)), they did observe more positive $\delta^{202}\text{Hg}$ values with elevated
539 dissolved THg concentrations values in samples from the hyporheic zone associated with exfiltrating
540 groundwater from the contaminated areas. These data would agree with the more positive liquid-
541 phase $\delta^{202}\text{Hg}$ values observed in our study and by McLagan et al. (2022).

542 Variation in both odd- and even-isotope MIF was within the range of analytical uncertainties
543 (Section S7; Section S8). McLagan et al. (2022) did observe small variation in $\Delta^{199}\text{Hg}$ between solid-
544 and liquid-phases, which the authors suggest may be linked to MIF driven by dark abiotic reduction
545 of Hg(II) (Zheng and Hintelmann, 2010). However, it is unlikely that this process could manifest into
546 an observable change in $\Delta^{199}\text{Hg}$ considering the short duration of these experiments even if the
547 process could occur at all within these columns.

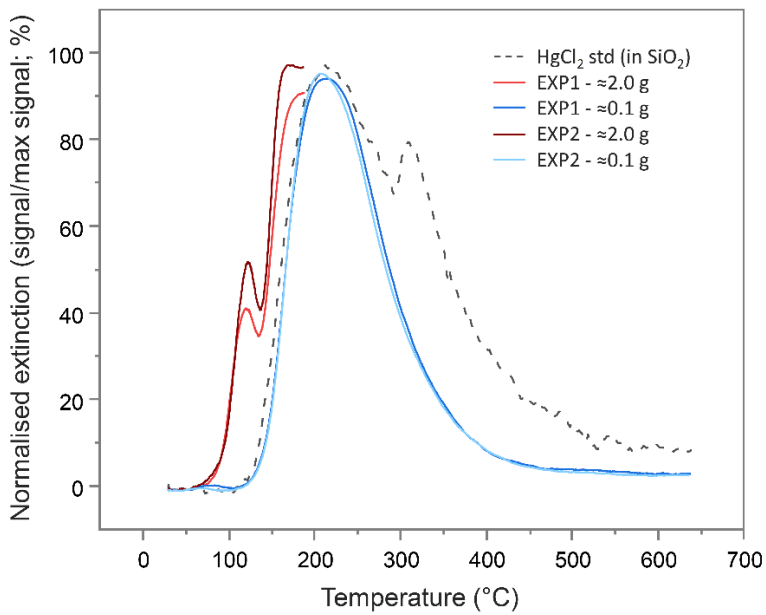
548 3.2 Is reduction of Hg(II) to Hg(0) occurring within the columns?

549 Reduction of Hg(II) to Hg(0) has been observed previously at this and other sites impacted by
550 kyanisation activities (Bollen et al., 2008; Richard et al., 2016a; 2016b; McLagan et al., 2022). In
551 these subsurface environments with low OM and very high THg concentrations, this secondary Hg(0)

552 production has been linked to abiotic, (hydr)oxide mineral surface catalysed reactions driven by
553 other redox active metals (Bollen et al., 2008; Richard et al., 2016a; 2016b; Schwab et al., 2023).
554 Since HgCl₂ solution was the only form of Hg applied in the column experiments, the presence of
555 Hg(0) in either the liquid- or solid-phases must be explained via reduction of Hg(II).

556 To examine the presence of Hg(0), PTD analyses were run on the (undried) solid-phase materials
557 from the columns after the sorption experiments. The PTD extinction curves showed little variation
558 across all sections of all columns from either experiment (see Section S9). All curves mimic the low
559 sample weight (≈ 0.1 g) mean extinction curves displayed in Figure 4 and are dominated by a single
560 peak with a maximum release of ≈ 225 °C, which aligns with the maximum extinction of the HgCl₂
561 standard in silicon dioxide (SiO₂). This supports the hypothesis of direct (outer-sphere) complexation
562 or electrostatic interaction of dissolved Hg(II) species to the mineral surfaces posited previously
563 (Bradl, 2004; Reis et al., 2016) and by McLagan et al. (2022). Nonetheless, these low sample weight
564 PTD curves were indicative of some qualitative evidence of very small peaks at < 175 °C (Section S9);
565 peaks in this range are associated with Hg(0) (Biester and Scholz, 1996; McLagan et al., 2022). The
566 initial sample masses used in the PTD analyses were low (≈ 0.1 g) so as to not overwhelm the AAS
567 detector, release large amounts of gas-phase Hg(0), and potentially cause memory effects in future
568 analyses. Nevertheless, this would not occur if sample masses were increased (≈ 2.0 g) and the
569 temperature ramp stopped at ≈ 175 °C. When the solid-phase materials were analysed in this
570 manner, Hg(0) peaks were detected across all sections of all columns in both experiments (see
571 Section S9; Figure 4).

572 Additionally, detectable concentrations of Hg(0) were observed across all of the ~~qualitative~~semi-
573 quantitative liquid-phase Hg speciation analyses and elevated above the Hg(0) concentrations
574 measured in the stock solution (Section S4). The observed liquid-phase fraction of Hg(0) was highest
575 at the $\approx 25\%$ breakthrough sample collection point in EXP1 (0.7%) and EXP2 (0.1%) with the fraction
576 being $\leq 0.1\%$ in all other samples (Section S4). While these data suggest that reduction of Hg(II) to
577 Hg(0) begins almost immediately after the introduction of the HgCl₂ solution, we link the declining
578 proportion of Hg(0) to the low solubility of Hg(0) (≈ 50 $\mu\text{g L}^{-1}$) (Skylberg, 2012; Brocza et al., 2019),
579 which was already reached at the $\approx 25\%$ breakthrough sample collection point in both experiments.



580

581 *Figure 4: Mean pyrolytic thermal desorption (PTD) extinction curves from solid-phase materials from*
 582 *EXP1 and EXP2 assessed with two different sample masses. Analyses of the larger sample mass (≈ 2.0*
 583 *g of material) were terminated when the temperature ramp reached ≈ 175 °C to prevent excessive*
 584 *gas-phase Hg release and potential memory effects on the instrument.*

585 These measured Hg(0) fractions in solid- and liquid-phase analyses provide further direct evidence
 586 of Hg(0) production under saturated, oxic conditions in low OM solid-phase materials. Hg(0)
 587 production in these contaminated aquifers has been linked to the slower than expected horizontal
 588 progress of the plume of Hg in the aquifer at the site where this contamination occurred (Bollen et
 589 al., 2008; Richard et al., 2016a; 2016b; McLagan et al., 2022). While these data indicate that the
 590 fraction of Hg(0) produced is relatively small, the volume of soil and aquifer materials in which this
 591 process can occur is large. The contamination plume of the aquifer at the site where the solid phase
 592 materials were removed from is ≈ 1000 m long and covers with an area of $\approx 6 \times 10^4$ m² (Bollen et al.,
 593 2008; McLagan et al., 2022). If we conservatively assume conservative values for a mean depth of
 594 contamination of 2 m (aquifer $\approx 3-4$ m depth; Bollen et al., 2008; McLagan et al., 2022), mean THg
 595 concentration of 2 mg kg⁻¹ (solid phase THg concentration of 2-162 mg kg⁻¹ along the contaminated
 596 aquifer; Bollen et al., 2008), the fraction of Hg(0) produced per day is 0.01 – 0.001% of the THg
 597 (based off 0.1% Hg(0) peak integration of total peak area of mean PTD curve from EXP2; see Section
 598 S9) (all conservative estimates) based off data from Bollen et al., 2008; McLagan et al., 2022, and
 599 the same bulk density and flow rates as in our experiments, we can produce a *back-of-the-envelope*
 600 estimate of the mass of Hg(0) produced and potentially lost from the aquifer to overlying soils. Based
 601 off these numbers, we estimate that 0.3 – 0.4 g of Hg(II) is transformed to Hg(0) each day within the
 602 aquifer of the contaminated site in southern Germany; over the course of one-year, this equates to
 603 the transformation $\approx 5 - 15$ kg of Hg(II) to Hg(0). Even a relatively conservative estimate of the
 604 conversion (and potential loss) of this mass of Hg(II) in contaminated aquifers such as this provides
 605 strong evidence that the process of Hg(II) reduction plays a key role in limiting the transport of the
 606 10-20 tonnes of Hg that was added to this soil-groundwater system in the ≈ 120 years since industrial
 607 operations commenced.

608 3.3 Retardation (R_D) and sorption coefficient (K_D) calculations

609 As expected, R_D values were substantially greater than 1, confirming substantial interaction
 610 between the applied $HgCl_2$ solution and the solid-phase aquifer materials (Table 3). The difference
 611 in R_D and K_D values between EXP1 and EXP2 (Table 3) indicate stock solution concentration is a factor
 612 in the transport of mercury within these columns. The elevated stock solution concentrations may
 613 be undermining the assumption of equal accessibility to sorption sites (USEPA, 2004). However, the
 614 purpose of these experiments was to simulate the original contamination by the industrial
 615 (mis)use/misuse of $HgCl_2$ solution, and while we can only estimate original concentration of solution
 616 being transported through the soil-groundwater system, we do expect they were very high due to
 617 the extent (both in terms of elevated concentrations and longitudinal and transverse dispersion
 618 three-dimensional spread of the contamination plume) of contamination that remains and the very
 619 high concentration of the solution used in rot-prevention treatment of timber (Bollen et al., 2008;
 620 Richard et al., 2016a; McLagan et al., 2022). Considering the high concentrations of Hg that have
 621 been observed within this and other Hg contaminated aquifers (Katsenovich et al., 2010; Lamborg
 622 et al., 2013; Demers et al., 2018), it is critical that we do not isolate our study of Hg transport
 623 dynamics to low concentration experiments that meet assumptions for theoretical sorption (batch
 624 and column) experiments.

625 *Table 3: Calculated retardation (R_D) and sorption (K_D) coefficients for EXP1 and EXP2 (definitions are*
 626 *given in Section 2.2.5).*

EXP1					EXP2				
Column	t_w (min)	t_{Hg} (min)	R_D	K_D (mL g ⁻¹)	Column	t_w (min)	t_{Hg} (min)	R_D	K_D (mL g ⁻¹)
C1.1	48.9	3628	74.7	23.8	C2.1	43.0	1615	37.6	11.8
C1.2	41.0	3629	88.5	29.5	C2.2	38.2	1567	41.2	12.9
C1.3	50.0	3779	75.6	25.1	C2.3	45.8	1837	39.9	12.6
C1.4	49.5	3678	74.3	-	C2.6	41.0	1438	35.1	-
C1.5	44.0	3488	79.3	-	C2.7	44.1	1623	36.9	-
C1.6	47.8	3599	75.3	-	C2.8	37.5	1317	35.1	-
		Mean	77.9	26.1			Mean	38.4	12.4
		SD	5.5	3.0			SD	2.7	0.6

627
 628 R_D values can be calculated from Miretzky et al. (2005) based on the inverse of their v/v_{water} value
 629 and the mean of these derived R_D values is 48 ± 13 for the high OM Amazonian soils. This again
 630 affirms the high sorptive capacity of our low OM solid-phase aquifer materials at these comparative
 631 concentration $HgCl_2$ applications. Lamborg et al. (2013) calculated K_D values for a Hg contaminated
 632 (from wastewater treatment) aquifer between 100 and 6300 mL g⁻¹ (log K_D : 2-3.8); yet calculations
 633 had to assume liquid-phase concentrations from other studies. Log K_D values calculated from soil
 634 and sediment batch experiments typically range from ≈ 2 in lower OM materials (Akçay et al., 1996)
 635 up to ≈ 6 in higher OM materials (Lyon et al., 1997). The logical next step is to utilise the measured
 636 R_D and K_D data from our study to perform soil-groundwater modelling to better understand Hg
 637 transport in this and other soil-groundwater systems as there are no previous estimates of R_D and
 638 K_D values based on measured data for low OM solid-phase aquifer materials. The range of coefficient
 639 values from ours and other studies described above relating to differing solid-phase properties,
 640 input solution speciation, and assumptions used highlights the caution that should be made applying
 641 these values to other systems as R_D and K_D values tend to be highly site specific (USEPA, 2004).

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654 Author contributions

655 D.S.M., C.E., and H.B. designed the study and experiments with some feedback from other co-
656 authors, particularly J.-H.R during preliminary experiments. C.E. led all concentration and speciation
657 analyses with assistance from D.S.M. Isotope analyses were led by L.S. with assistance from J.W.
658 (and A.C. see above). This work was the basis for C.E.'s master's thesis, which was written in German.
659 The manuscript first draft was written by D.S.M. and all other authors provided feedback in building
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