



THE IMPACT OF RISING ATMOSPHERIC CO2 LEVELS AND RESULTING OCEAN ACIDIFICATION

TO THE PHYSICAL (SOLUBILITY) OCEAN PUMP OF CO2.

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7	Abstract
8	An alternative measure of the ocean's carbonate buffer system efficiency to absorb CO_2
9	from the atmosphere is proposed. Instead of the Revelle factor R = ($\Delta CO2/CO2$)/($\Delta DIC/DIC$) =
10	(DIC/CO2)/ (Δ DIC/ Δ CO2) the sensitivity S = (Δ DIC/ Δ CO2) is preferable because it gives
11	directly the change ΔDIC of the concentration of DIC in the seawater caused by the change
12	Δ CO2 of carbon dioxide in the atmosphere. To this end the DIC concentration of seawater at
13	temperature T in equilibrium with a defined CO_2 level in the surrounding atmosphere is
14	calculated by use of the geochemical program PHREEQC. From the function DIC(CO2,T) one
15	obtains by differentiation the sensitivity S = dDIC/dCO2 = Δ DIC/ Δ CO2 and also the Revelle
16	factor R. Using S as the change of the ocean's buffer capacity reveals a better insight of its
17	future evolution than using the Revelle factor R.
18	One finds that the buffer capacity S has declined by about 30% from 1945 to present and
19	that its future decline from 400 to 600 ppm will be a further 30%. By calculating the uptake
20	of CO $_2$ of his equilibrium pump an upper value of 1.3 Gigatons/year is obtained, small in
21	comparison to the 10 Gigatons/year absorbed by the ocean at present. The Revelle factor R
22	at present is calculated R = 13 and rises to 18 at a CO ₂ level of 800 ppm. This increase of R





23	has been interpreted as indication of the collapse of the solubility pump. S and R, however,
24	are defined from equilibrium chemistry and are a measure of the $\ensuremath{CO_2}$ absorbed by the
25	ocean's upper mixed layer by increase of the \mbox{CO}_2 level in the atmosphere without regarding
26	its sinking into the deep-ocean by the thermohaline circulation. The difference ΔDIC
27	between the actual value and the value at 280 ppm is transported into the deep-ocean by
28	the global meridional conveyor belt. ΔDIC increases with increasing CO ₂ level. At 280 ppm
29	the system ocean-atmosphere is in equilibrium and the sink is zero. At 400 ppm a value of
30	about 1.9 Gtons/year is estimated that increases to 3.9 Gtons/year at 600 ppm and to 5
31	Gtons/year at 800 ppm. At present CO ₂ level increase of 2ppm/year 10 Gtons/year are
32	absorbed by the ocean. The solubility pump contributes 3.2 Gtons/year: 1.3 Gtons/year by
33	equilibrium absorption into the mixed layer and 1.9 Gtons/yeat by thermohaline circulation.
34	At 600 ppm the total sink is 4.6 Gtons/year and at 800 ppm 5.5 Gtons/year. To conclude, the
35	solubility pump is not endangered by ocean acidification. In contrast, it increases with
36	increasing CO_2 level of the atmosphere to yield significant contribution.
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38 1. Introduction

39 Only one half of anthropogenic CO₂ emitted remains in the atmosphere. About one quarter 40 is absorbed by the land sink via vegetation. The remaining quarter sinks into the ocean by 41 the biological pump and the physical (solubility pump) (Friedlingstein et al., 2022). The ocean 42 CO₂ sink has increased steadily with rising CO₂ level since the beginning of industrialisation. 43 As an example, CO₂ level of 317 ppm in 1960 raised to 420 ppm in 2021 and accordingly the ocean sink from 1.1 ± 0.4 GtC/yr in 1960 to 2.8 ± 0.4 GtC/ y during 2021 (Friedlingstein et al., 44 2022). Thus, the ocean sink has increased proportional to the rise in atmospheric CO₂. To 45 46 predict the future evolution of the CO2-concentation (ppm) in the atmosphere by models





- 47 one has to know whether this increase will be permanent. One part of the oceanic sink is the
- 48 solubility pump that transports dissolved inorganic carbon (DIC) in equilibrium with the
- 49 partial pressure p_{co2} in the atmosphere (0.0001 atm \triangleq 100 ppm) into the deep ocean. The
- 50 future effectivity of this physical pump has been questioned because with increasing
- 51 acidification of the ocean its buffering capacity decreases. This is commonly expressed by
- 52 the Revelle factor R (Zeebe and Wolf-Gladrow, 2001, Eglestone et al., 2010).
- 53 R = $(\Delta DIC/DIC)/(\Delta CO2/CO2) = (\Delta DIC/\Delta CO2)/(DIC/CO2)$.
- 54 Δ DIC is the change in concentration DIC caused by a small increase Δ CO2 of the

55 concentration CO₂ in the atmosphere. CO₂ and DIC are the corresponding concentrations.

- 56 However, the Revelle factor is used mostly only qualitatively stating that increasing values
- 57 of R indicate weakening of the buffer capacity (e.g., Climate Change 2007: The Physical
- 58 Science Basis. AR4 IPPC, Bates and Johnson, 2020). A more appropriate measure, the
- 59 sensitivity

$S = \Delta DIC/\Delta CO2$ has not been used in the scientific community. Middelburg et al., 2020
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- 61 "there are few studies where buffer and/or sensitivity factors are being used, except for the
- 62 well-known Revelle factor." To judge quantitively the decrease of buffer capacity that gives
- 63 the amount of DIC increase by reaction of CO_2 to HCO_3^- and CO_3^- the evolution of sensitivity S
- 64 in dependence on the CO₂ level in the atmosphere is a better alternative. To this end I
- 65 calculate using the geochemical program PHREEQC (Parkhurst and Appelo, 2013) the
- 66 chemical composition of sea water in chemical equilibrium with CO₂ of defined partial
- 67 pressure p_{CO2} (ppm) in the surrounding atmosphere at defined temperature T. This way
- 68 DIC(pCO2,T) as a function of p_{CO2} and T is obtained. By differentiation one gets dDIC/dpCO2
- $69 = \Delta DIC/\Delta CO2 = S$ at defined temperature. From this I discuss the decrease of buffer capacity
- 70 with increasing p_{CO2}. I report the Revelle factor R as a function of S to enable quantitative





- 71 arguments using the Revelle factor R. This equilibrium pump does not consider the
- 72 overturning circulation of the ocean that transports the water of the mixed zone into deep-
- 73 ocean. This transport pump increases steadily with increasing p_{CO2}. The physical pump is the
- sum of the sink by the equilibrium pump and the overturning transport pump. It increases
- 75 steadily to yield significant contributions.
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77 Methods
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78 The input file of the program PHREEQC is shown in Table 1. The first block SOLUTION 1

79 defines the composition of sea water including major elements and boron. The second block

- 80 EQUILIBRIUM_PHASES equilibrates this solution with gaseous CO₂ of the surrounding
- 81 atmosphere. Input parameters are temperature "temp" in °C and CO2(g) as log(p_{CO2}) where
- 82 p_{CO2} is in atm.
- 83 From the output file one can read pH and extract the concentrations of DIC (C(4)) and its

SOLUTION	1 Seawater
units ppr	n
pH 8.22	
pe 8.451	
density i	1.023
temp 5	
Ca 412.3	
Mg 1291.8	3
Na 10768	
K 399.1	• •
	0
	.0
	141 600
	-
S(6) 2712	2.0
	IUM_PHASES
CO2 (ag)	-2.921
END	
as 1 S(6) 2712 EQUILIBR CO2(ag)	ty 141.682 HCO3 2.0 IUM_PHASES

pH = 7	7.715
DIC C(4)	2.425e-03
HCO3- MgHCO3+ NaHCO3 CO2 CaHCO3+	1.753e-03 3.129e-04 2.253e-04 6.588e-05 3.420e-05
8.017e-06 NaCO3 MgCO3 1.542e-05 CO3-2 - 5.031e-06 CaCO3	4.984e-06

84

85 Table 1: Input file of PHREEQC

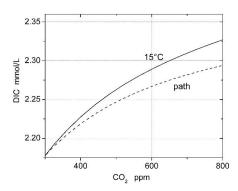
Table 2: Output results

86 species in mol/kg. The program includes ion pairs with Ca and Mg. MgHCO₃⁺ and NaHCO₃





- 87 occur in considerable concentrations. In programs that do not include ion pairs these are
- 88 included as HCO3⁻. I have calculated DIC and pH from CO2 levels of 300 ppm in steps of
- 89 33ppm up to 800 ppm. The data points were transferred to the program Origin. Then they
- 90 were fitted to a 5th order polynomial (R-square = 0.99995; SD = $3,3 \cdot 10^{-4}$; p< 10^{-4}) to smooth the
- data for differentiation performed by the program. The figures were created by the graphics 91
- 92 of Origin.
- 93
- 94 3. Results
- 95 Fig.1 represents the results for DIC at fixed temperature T = 15°C (solid line). The dashed line
- 96 depicts the path where according to the increasing CO_2 level the temperature increases



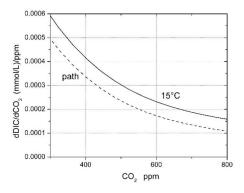


Fig. 1: DIC at fixed temperature of T = 15°C temperature changes with increasing CO₂

Fig. 2: Sensitivity S = dDIC/dCO2 for fixed (solid line). The dashed line depicts DIC when temperature (solid line) and the path (dashed line) taking into account temperature increase with increasing CO₂ level. See text.

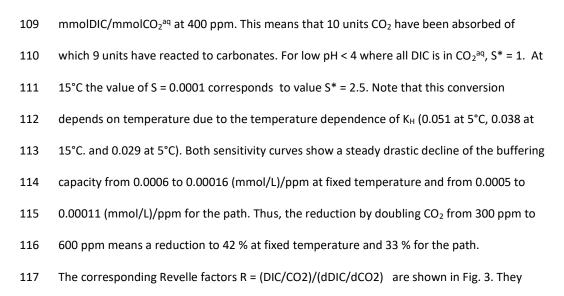
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      linearly by 0.01 °C per 1ppm increase of CO<sub>2</sub> level corresponding to their linear correlation
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- 98 obtained from NASA data of temperature and CO_2 level. The curve starts at T = 15°C, 300
- 99 ppm with steps of 33 ppm and 0.34°C and ends at 800 ppm and T = 19.1 C. Due to the rising
- 100 temperature DIC is reduced slightly in comparison to fixed temperature a1 15 °C. Fig 2
- 101 depicts the sensitivity S = dDIC/dCO2 obtained from differentiation of the curves in Fig. 1.





- 102 dDIC is the change in the concentration of DIC in mmol/L that is caused by an increase of CO₂
- 103 by dCO₂ in ppm. This change can be converted as change of the aqueous CO₂ concentration
- 104 c_{aq} in the liquid by Henry's law $c_{aq} = K_{H} \cdot p_{CO2}$. At 15°C for sea water, $K_{H=} = 0.04$ mol/atm
- 105 (Zeebe and Wolf-Gladrow, 2001). For 1ppm the change $dc_{aq} = 4 \cdot 10^{-5} \text{ mmol CO}_2^{aq}$. The
- 106 corresponding change dDIC = S·1ppm = 0.0004 mmol DIC. Defining S*in units of
 - 8.3 25 - pH 15 - pH path path 8.2 Revelle Factor 20 8.1 Hd 15°C path 8.0 15°C 15 7.9 7.8 400 600 800 400 600 800 CO, ppm CO, ppm Fig. 4: pH for fixed temperature Fig. 3: Revelle factor for fixed temperature (solid line) and path (dashed line). (solid line) and path (dashed line).
- 107 mmolDIC/mmolCO_{2^{aq}} this way S*= 0.0004/0.00004 mmolDIC/mmol CO_{2^{aq}} = 10





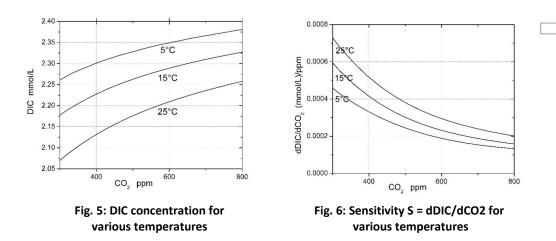


118	illustrate why the Revelle factor cannot be used easily as quantitative measure because the
119	reduction of buffer capacity is by its change and not by its absolute value. Therefore, one has
120	to know the end values. In contrast, sensitivity S gives the reduction from the known initial
121	value. In other words, the large background of R at 300 ppm prevents a reasonable
122	interpretation. Finally, in Fig. 4 acidification of ocean, the reason for declining buffer capacity
123	is shown as pH versus CO_2 level. pH drops almost linearly with CO_2 level from pH = 8.3 at 300
124	ppm to 7.9 at 800 ppm. There is little difference between constant temperature at 15° C and
125	the path regarding global warming. The change in pH is close to the projection of Jiang et al.,
126	2019 using the RCP 6.0 scenario of IPCC. This holds also for the change of the Revelle factor
127	R in Fig. 3.
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129 4. Discussion

To obtain some overview on the variability of sensitivity S and Revelle factors R in Fig. 5 one
finds DIC for 5, 15, and 25°C respectively. The corresponding sensitivities S are shown in Fig.
6 and the Revelle factors are depicted in Fig. 7. For completion pH is illustrated in Fig. 8.



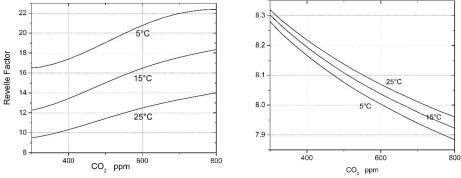


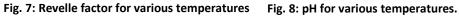


- 134 At fixed CO₂ the DIC concentration (Fig. 5) decreases with temperature whereas the
- 135 sensitivity S increases as can be seen from the slopes increasing with rising temperature.
- 136 These slopes are shown as S = dDIC/dCO2 in Fig. 6. S increases with rising temperature. As
- 137 one can read from Fig. 6 an increase of temperature by 5°C causes a reduction of the initial
- 138 value at 15°C by about 10% for all CO₂ levels. The impact of changing CO₂ level by far exceeds
- 139 that of increasing temperature.
- 140 S decreases with increasing CO_2 level. It is important to note that one finds a reduction by 36
- 141 % at the beginning from 300 to 420 ppm, corresponding to the time from 1945 to 2021.

142 Further reduction from 400 to 500 ppm is 16 % and continues to decrease further on for all

- 143 temperatures. This is in contrast to the opposite behaviour of the Revelle factor in Fig. 7.
- 144 One finds a small increase at the beginning up to 400 ppm followed by rise about twice of
- the initial one for CO₂ between 400 to 600 ppm, valid for all temperatures. Thus, using S as
- 146 measure for impact to the oceans buffer capacity leads to conflictive conclusion about future



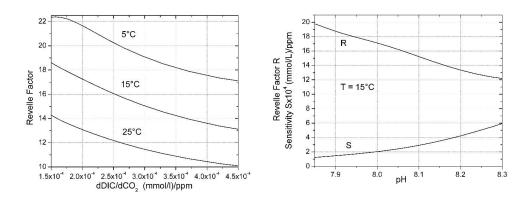


evolution with consequences in defining pathways for CO₂ emissions in climate change
policy. At present public policy seems to be convinced that at least the physical ocean pump
will fail in the near future. Although the mixed layers capacity has been reduced by about
30% of its initial value for all temperatures during 1945 (300ppm) to 2015 (400ppm). The



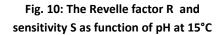


- 151 ocean sink (Friedlingstein et al., 2022), however has continuously increased during this time
- 152 span. This leads to the conjecture that the physical sink into the mixed layer may not
- 153 contribute as significantly to the total ocean sink as thought by using the concept of
- 154 equilibrium chemistry (Revelle factor).



155 Finally, to relate sensitivity S to Revelle factor R, Fig. 9 illustrates R as a function of S.

Fig. 9: The Revelle factors R in relation to the sensitivity S for various temperatures



156	It is obvious why using S should be preferred. If S changes from 1.5 $\cdot 10^{-4}$ to 4.5 $\cdot 10^{-4}$ by 200 %
157	the corresponding chage in R is only about 40 % for 25°C and 20% for 5°C. Therefore, S gives
158	a more realistic view. Fig. 10 shows R and S as function of pH at 15°C. R changes from 12 to
159	20 with pH dcreasing from 8.3 to 7.85. But, in contrast to the sensitivity from its value no
160	direct meaning can be derived. From its defition a simple relation is: $R = 2.27/(CO2 \cdot S)$
161	because DIC \approx 2.27 mmol/L remains constant within a few percent (see Fig. 1 and Fig. 5).
162	From this one may understand why R is used only qualititavely to judge ocean's physical
163	pump buffer capacity.
164	Using the DIC data one can estimate the upper limit of the present CO_2 flux from the
165	atmosphere to the ocean's mixed layer. I calculate the volume V_1 of the upper 1 meter of the

166 mixed layer V₁ = $0.71 \cdot 4\pi R^2 \cdot 1 \text{ m}^3$ = $3.6 \cdot 10^{17}$ L. R is Earth radius and 0.71 ocean coverage. The





- amount M₁ of DIC that can be absorbed with a sensitivity $S_1 = 10^{-7} (mol/L)/ppm$ is $M_1 = V_1 \cdot S_1$
- 168 mol/ppm. Consequently, the amount Mt absorbed by a mixed layer with depth t(m) and a
- 169 change of n ppm CO₂ is $M_t = M_1 \cdot t \cdot s \cdot n \mod CO_2$ when sensitivity $S = s \cdot S_1$. Converting to g CO₂
- 170 one has to multiply by the molecular weight 44 g/mol of CO₂ to obtain
- 171 $M_t = M_1 \cdot t \cdot s \cdot n \mod 44g/mol = M_1 \cdot t \cdot s \cdot n \cdot 44$ (g).
- 172 A reasonable estimation of the mixed layer depth t is 100 m (de Boyer et al., 2004, Boyer et
- 173 al., 2022, Birol Kara et al., 2000, Doney et al., 2004). At present the increase of CO₂ is
- 174 2 ppm/year (n = 2) and (s = 4). Using these numbers, one finds $M_t = 1.3$ Gigatons/year. The
- 175 value of s = 4 corresponds to a temperature of 15°C at 420 ppm (see Fig. 6). This assumption
- 176 is reasonable because oceans temperature is distributed between 25° at the equator to 5°C
- in the polar oceans.
- 178 Another argument must also be considered. Carbon is absorbed by the ocean where water
- 179 sinks to the deep ocean. At regions of upwelling water rich in CO₂, however, CO₂ is released
- 180 into the atmosphere (Landschützer et al., 2014, Crisp et al., 2022). This water outgasses CO₂
- 181 into an atmosphere with higher partial pressure. This causes a reduced flux of outgassing
- 182 and the difference of outgassing between higher and lower partial pressure at the intake
- acts as effective influx in upwelling regions and justifies the assumption.

184 It must be stressed that the flux calculated so far by equilibrium chemistry represents the 185 capacity to absorb CO_2 from the atmosphere by a stagnant isolated mixed layer that does 186 not sink into depth. Therefore, this sink is caused by equilibrium chemistry and could be

- 187 termed as equilibrium sink (pump). This pump declines with increasing acidification of the
- 188 ocean. At pH < 4 the only existing carbonate species are aqueous CO₂ and H₂CO₃. Therefore,
- 189 the absorption of CO_2 is governed by Henry's law. Therefore, dDIC/dCO2 = K_H and stays
- 190 constant with further decreasing pH. At 15°C dDIC/dCO2 = 4·10⁻⁵ mmol/ppm. This



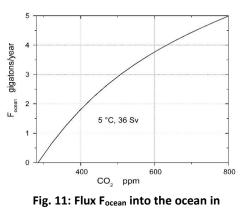


- 191 corresponds to a flux of 0.13 Gt/year, an almost total breakdown of the mixed layer's
- 192 capacity to absorb CO₂.
- 193 This, however, does not mean that the physical pump breaks down as has been concluded
- 194 from the increase of the Revelle factor. In IPCC AR4 one finds: "The ocean's capacity to
- 195 buffer increasing atmospheric CO₂ will decline in the future as ocean surface pCO₂ increases
- 196 (Figure 7.11a). This anticipated change is certain, with potentially severe consequences."
- 197 (Denman et al., 2007).
- 198 The total CO₂ sink consists of two parts: the equilibrium sink as already stated and the
- 199 transport sink. This is governed by the global meridional overturning circulation where
- 200 surface waters of the mixed layer flow from the equator to the polar regions and sink there
- 201 into the deep ocean by thermohaline circulation. In the North Atlantic deep water formation
- is 15 ± 2 Sv (1 Sv = 10^6 m³/s) and 21 ± 6 Sv in the southern ocean (Ganachaud and Wunsch,
- 203 2000, <u>Rahmstorf, 2002</u>). These waters have cooled to low temperatures (about 5°C) when
- 204 they sink. They transfer the CO₂ in the mixed layer that contains also the anthropogenic
- 205 carbon into deep-ocean. These waters are replaced by upwelling waters back to the surface
- without anthropogenic carbon (Terhaar et al., 2022) that readily absorb CO_2 from the
- 207 atmosphere until equilibrium is established.
- 208 Dividing the volume V_{mix} of the mixed layer by the global formation of deep water of 36 ± 6 Sv
- 209 one obtains, τ_{drain} , the time needed to drain that layer into the ocean as 57 years. The time
- for chemical equilibration to a change of atmospheric CO_2 is on the order of 1 year (Jones et
- 211 al., 2014). Therefore, DIC in the mixed layer is in equilibrium with the CO₂ in the atmosphere
- as given in Fig.5. At a CO_2 level of 280 ppm the flux of CO_2 into the ocean is zero and the
- 213 system is in equilibrium (Friedlingstein et al., 2022). With increasing CO₂ level, the deviation
- of DIC equilibrium concentration is given by $(DIC_{ppm} DIC_{280}) = \Delta DIC_{ocean}$. ΔDIC_{ocean} represents





- the amount of anthropogenic carbon absorbed into the mixed layer since the onset of
- 216 industrialisation. The flux F_{ocean} into the ocean is given by $\Delta DIC \cdot V_{mix} / \tau_{drain} = F_{ocean}$ in
- 217 Gtons/year. At 400 ppm one finds a value of F_{ocean} = 1.9 Gtons/year
- 218 Fig. 9 depicts F_{ocean} in dependence on the CO₂ level. F_{ocean} does not increase linearly with CO₂



dependence on CO₂ level

level but increases with declining slope to 0.0087 Gtons/(year ppm) that stays constant for p_{CO2} > 1 atm as calculated by PHREEQC. This way for an increase of 1 ppm/year of CO₂ level, F_{ocean} increases by 0.0087 Gtons/year.

At present the total Ocean sink is 10 Gt/year. If at 400 ppm a total sink of 3.2 Gt/year is correct the contribution of the physical pump is relatively small. It is possible that the biological pump (Hauck and Völker, 2015, Riebesell et. al., 2007) compensates for this. In view of the fact that this estimation might be critiqued it should motivate further research and discussion in ongoing projects.

- 232
- 233 5. Conclusion

234 An alternative measure of the ocean's carbonate buffer to absorb CO₂ from the atmosphere

- is proposed. Instead of the Revelle factor R = $(\Delta CO2/CO2) / (\Delta DIC/DIC) = (DIC/CO2) / (\Delta DIC) = (DIC/CO2) / (DIC) = (DIC/$
- 236 ($\Delta DIC/\Delta CO2$) the sensitivity S = ($\Delta DIC/\Delta CO2$) is preferable because it gives directly the
- 237 change Δ DIC of the concentration of DIC in the seawater caused by the change Δ CO2 of
- 238 carbon dioxide level in the atmosphere. To this end the DIC concentration of seawater in





- 239 equilibrium with a defined CO₂ level in the surrounding atmosphere is calculated by use of
- 240 the geochemical program PHREEQC. From the function DIC(CO2) by derivation one obtains
- 241 the sensitivity S = dDIC/dCO2 = Δ DIC/ Δ CO2 and also the Revelle factor R.
- 242 Using S, the change of the ocean's buffer capacity better insight of its future evolution is
- 243 obtained than by use of the Revelle factor R.
- 244 S declines heavily since 1945 until it breaks down at CO₂ levels of 800ppm. One has to
- 245 consider, however, that R and S are calculated by equilibrium chemistry that does not
- 246 contain the sink caused by the thermohaline overturning circulation that transports the
- 247 water of the mixed zone into deep-ocean. S therefore, gives the amount of carbon as ΔDIC
- 248 that is stored in the mixed layer when the CO_2 level increases by $\Delta CO2$.
- 249 The total solubility sink consists of two mechanisms: The equilibrium pump as described and
- the transport pump that is caused by the global meridional overturning circulation of 36 Sv.
- 251 This transfers into deep-ocean the difference (DIC_{ppm} DIC_{280}) = ΔDIC_{ocean} that has been
- accumulated in the mixed layer from onset of industrialisation to the actual CO₂ level.
- 253 This sink increases continuously replacing the failure of the equilibrium pump. At 400 ppm
- the total sink is 1.9, at 600 ppm it is 3.8 and at 800 ppm it amounts to 5 Gtons/year
- depending solely on the CO_2 level in the atmosphere for ppm > 600.
- 256 To conclude, the total solubility pump is not endangered by ocean acidification. In contrast,
- 257 it increases with increasing CO₂ level of the atmosphere to yield significant contribution to
- 258 remove anthropogenic CO₂ from the atmosphere into deep-ocean.

- 260 I declare that I do not have any competing interests.
- 261
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