Analogue experiments on releasing and restraining bends and their application to the study of the Barents Shear Margin

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Abstract:
The Barents Shear Margin separates the Svalbard and Barents Sea from the North Atlantic. During the break-up of the North Atlantic the plate tectonic configuration was characterized by sequential dextral shear, extension, an eventually contraction and inversion. This generated a complex zone of deformation that contains several structural families of over-lapping and reactivated structures.
A series of crustal-scale analogue experiments, utilizing a scaled stratified sand-silicon polymer sequence were utilized in the study of the structural evolution of the shear margin.

The most significant observations of particular significance for interpreting the structural configuration of the Barents Shear Margin are:
1) Prominent early-stage positive structural elements (e.g. folds, push-ups) interacted with younger (e.g. inversion) structures and contributed to a hybrid final structural pattern.
2) Several structural features that were initiated during the early (dextral shear) stage became overprinted and obliterated in the subsequent stages.
3) All master faults, pull-part basins and extensional shear duplexes initiated during the shear stage quickly became linked in the extension stage, generating a connected basin system along the entire shear margin at the stage of maximum extension.
4) The fold pattern generated during the terminal stage (contraction/inversion became dominant in the basin areas and was characterized by fold axes striking parallel to the basin margins. These folds, however, strongly affected the shallow intra-basin layers.

The experiments reproduced the geometry and positions of the major basins and relations between structural elements (fault and fold systems) as observed along and adjacent to the Barents Shear Margin. This supports the present structural model for the shear margin.

Plain language summary:
The Barents Shear Margin defines the border between the relatively shallow Barents Sea that is situated on a continental plate, and the deep ocean. The margin is characterized by a complex structural pattern that has resulted from the opening and separation of the continent and the ocean, starting c. 65 million years ago. This history included on phase of right-lateral shear and one phase of spreading, the latter including a sub-phase of shortening, perhaps due to plate tectonic reorganizations. The area has been mapped by the study of reflection seismic lines for decades, but many details of its development is not yet fully constrained. We therefore ran a set of scaled experiments to investigate what kind of structures could be expected in this kind of tectonic environment, and to figure out what is a reasonable time relation between them. From these experiments we deducted several types of structures (faults, folds and sedimentary basins) that help us to improve the understanding of the history of the opening of the North Atlantic.

Key words: Analogue experiments, dextral strike-slip, releasing and restraining bends, multiple folding, Barents Shear Margin**,** basin inversion

Introduction

Physiography, width and structural style of the Norwegian continental margin vary considerably along its strike (e.g. Faleide et al., 2008, 2015). The margin includes a southern rifted segment between 60° and 70°N and a northern sheared-rifted segment between 70° and 82°N (**Figure 1A**). The latter coincides with the ocean-ward border of the western Barents Sea and Svalbard margins (e.g. Faleide et al., 2008) and is referred to here as "the Barents Shear Margin". This segment coincides with the continent-ocean transition (COT) of the northernmost part of the North Atlantic Ocean, and its configuration is typical for that of transform margins where the structural pattern became established in an early stage of shear, later to develop into an active continent-ocean passive margin (Mascle & Blarez, 1987; Lorenzo, 1997; Seiler et al., 2010; Basile, 2015; Nemcok et al., 2016). Late Cretaceous - Palaeocene shear, rifting, breakup and incipient spreading in the North Atlantic was associated with voluminous magmatic activity, resulting in the development of the North Atlantic Volcanic Province (Saunders et al., 1997; Ganerød et al., 2010; Horni, 2017). According to its tectonic development, the Barents Shear Margin (**Figure 1B**) incorporates, or is bordered by, several distinct structural elements, some of which are associated with volcanism and halokinesis.

The multistage development combined with a complex geometry caused interference between structures (and sediment systems) in different stages of the margin development. Such relations are not always obvious, but interpretation can be supported by the help of scale-models. We combine the interpretation of reflection seismic data and analogue modeling. Thus, we investigate structures generated in (initial) dextral shear. These were generated during initial dextral shear the development into seafloor spreading and subsequent contraction. The later stages (contraction) were likely influenced by plate reorganization (Talwani & Eldholm, 1977; Gaina et al., 2009; see also Vågnes et al., 1998; Pascal & Gabrielsen, 2001; Pascal et al., 2005; Gac et al., 2016) or other far-field stresses (Doré & Lundin, 1996; Lundin & Doré, 1997; Doré et al., 1999; 2016; Lundin et al., 2013). The present experiments were designed to illuminate the structural complexity affiliated with multistage sheared passive margins, so that the significance of structural elements like fault and fold systems observed along the Barents Shear Margin could be set into a dynamic context. The study area suffered

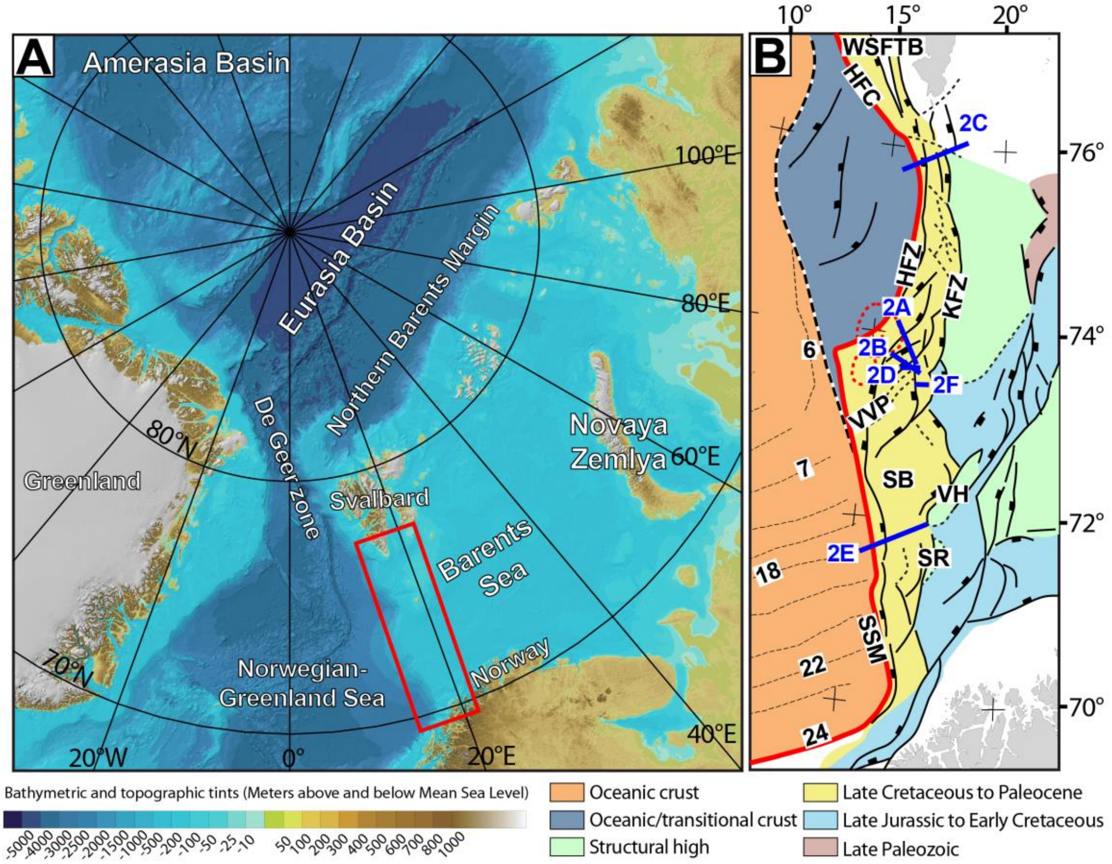


Figure 1: A) The Barents Sea is separated from the Norwegian-Greenland Sea by the de Geer transfer margin. Red box shows the present study area. **B)** Structural map Barents Sea shear margin. Note segmentation of the continent-ocean transition. Abbreviations (from north to south): WSFTB = West Spitsbergen Fold-and-Thrust Belt, HFZ = Hornsund Fault Complex, KFC = Knølegga Fault Zone, VVP = Vestbakken Volcanic Province, SB = Sørvestsnaget Basin, VH = Veslemøy High, SR = Senja Ridge, SSM = Senja Shear Margin. Blue lines indicate position of seismic profiles in Figure 2 and red line X-X′ shows western border of thinned crust (see also Figure 3). Chron numbers are indicated on oceanic crust area.

repeated and contrasting stages of deformation, including dextral shear, oblique extension, inversion and volcanic activity. This is a particular challenge in such tectonic settings that are characterized by repeated overprinting and cannibalization of younger structural elements. Results from the he experiments facilitate the identification and characterization of structural elements at the different stages of deformation and to identify the structural elements that were developed at stages of deformation preceding the present-day margin configuration.

Regional background

In the following sections we provide definitions and a short description of the main structural elements constituting the study area. The structural elements are presented in-sequence from north to south (**Figure 1B**).

The greater **Barents Shear Margin** is a part of the more extensive De Geer Zone mega shear system which linked the Norwegian Greenland Sea and the Arctic Eurasia system (Eldholm et al., 1987; 2002; Faleide et al., 1988; Breivik et al., 1998; 2003). Together with its conjugate Greenland counterpart it carries the evidence of post-Caledonian extension that culminated with Cenozoic break-up of the North Atlantic (e.g. Brekke, 2000; Gabrielsen et al., 1990; Faleide et al., 1993; Gudlaugsson et al., 1998). Two shear margin segments are separated by a central rift-dominated segment along the Barents Shear Margin (Myhre et al., 1982; Vågnes, 1997; Myhre & Eldholm, 1988; Ryseth et al., 2003; Faleide at al., 1988; 1993; 2008). Each segment maintained the structural and magmatic characteristics of the crust during its development. Of these the Senja Shear Margin is the southernmost segment, originally termed the Senja Fracture Zone by Eldholm et al. (1987). Here NNW-SSE-striking folds interfere with NE-SW-striking structures (Giannenas, 2018). Strain partitioning characterizes the shear zone system (e.g. West Spitsbergen; Leever et al., 2011a,b and the Sørvestsnaget Basin; Kristensen et al., 2017).

The Hornsund Fault Zone and West Spitsbergen Fold-and Thrust Belt form the northernmost segment of the Barents Shear Margin. It coincides with the southern continuation of the De Geer Zone and the Senja Shear Margin. The Hornsund Fault Zone belongs to this system and provides a type setting for transpression and strain partitioning together with the West Spitsbergen fold-and-thrust-belt (Harland, 1965; 1969; 1971; Lowell, 1972; Gabrielsen et al., 1992; Maher et al., 1997; Leever et al., 2011 a,b). Plate tectonic reconstructions suggest that the plate boundary accommodated c. 750 km along-strike dextral displacement and 20-40 km of shortening in the Eocene (Bergh et al., 1997; Gaina et al., 2009).

The Knølegga Fault Zone can be seen as a part of the Hornsund fault system extending from the southern tip of Spitsbergen (Gabrielsen et al., 1990). It trends NNE-SSW to N-S and defines the western margin of the Stappen High. The vertical displacement approaches 6 km. Although the main movements along the fault may be Tertiary of age, it is likely that it was initiated much earlier. The Tertiary displacement may have a lateral (dextral) component (Gabrielsen et al., 1990).

The Vestbakken Volcanic Province is the main topic of this contribution. It represents the central rifted segment of the Barents Shear Margin and links the sheared margin segments to the north and south occupying a right-double stepping (eastward) releasing-bend-setting. Prominent volcanoes and sill-intrusions suggest three distinct volcanic events in the Vestbakken Volcanic Province (Jebsen & Faleide, 1998; Faleide et al., 2008; Libak et al., 2012). It is constrained to its east by the eastern boundary fault (EBF in **Figure 1B**), that is a part of the Knølegga Fault Complex, separating the Vestbakken Volcanic Province from the marginal Stappen High to the east. To the south and southeast the Vestbakken Volcanic Province drops gradually towards the Sørvestsnaget Basin across the southern extension of the eastern boundary fault and its associated faults. To the west and north the area is delineated by the continent – ocean boundary/transition. The Vestbakken Volcanic Province includes both extensional and contractional structures (e.g. Jebsen & Faleide, 1998; Faleide et al., 2008; Blaich et al., 2017). Two main episodes of Cenozoic extensional faulting were identified in the Vestbakken Volcanic Province: (i) a late Paleocene-early Eocene event, which correlates in time with the continental break-up in the Norwegian-Greenland Sea, (ii) an early Oligocene event that is tentatively correlated to plate reorganization around 34 Ma activating NE-SW striking faults. Volcanic activity coincides with these events.

The Sørvestsnaget Basin occupies the area east the COT between 71 and 73^{o}N and is characterized by an exceptionally thick Cretaceous-Cenozoic sequence (Gabrielsen et al., 1990). To the west it is delineated by the Senja Shear Margin and to the northeast it is separated from the Bjørnøya Basin by the southern part of the Knølegga Fault Complex (Faleide et al., 1988). The position of the Senja

Ridge coincides with southeastern border of the Sørvestsnaget Basin (Figure 1B), whereas the Vestbakken Volcanic Province is situated to its north. An episode of Cretaceous rifting in the Sørvestsnaget Basin climaxed in the Cenomanian-middle Turonian (Breivik et al., 1998), succeeded by Late Cretaceous-Palaeocene fast sedimentation (Ryseth et al., 2003). Particularly the later stages of the basin formation were strongly influenced by the opening of the North Atlantic (Hanisch, 1984; Brekke & Riis, 1987). Salt diapirism also contributed to the development of this basin (Perez-Garcia et al., 2013).

The Senja Ridge (SR in **Figure 1B**) runs parallel to the continental margin and coincides with the western border of the Tromsø Basin. It is characterized by a N-S-trending gravity anomaly which are interpreted as buried mafic-ultramafic intrusions which are associated with the Seiland Igneous Province (Fichler & Pastore, 2022). The structural development of the Senja Ridge has been associated with shear affiliated with the development of the shear margin (Riis et al., 1986) and though it was a positive structural element from the mid Cretaceous to the Pliocene it may have been activated at an even earlier stage (Gabrielsen et al., 1990).

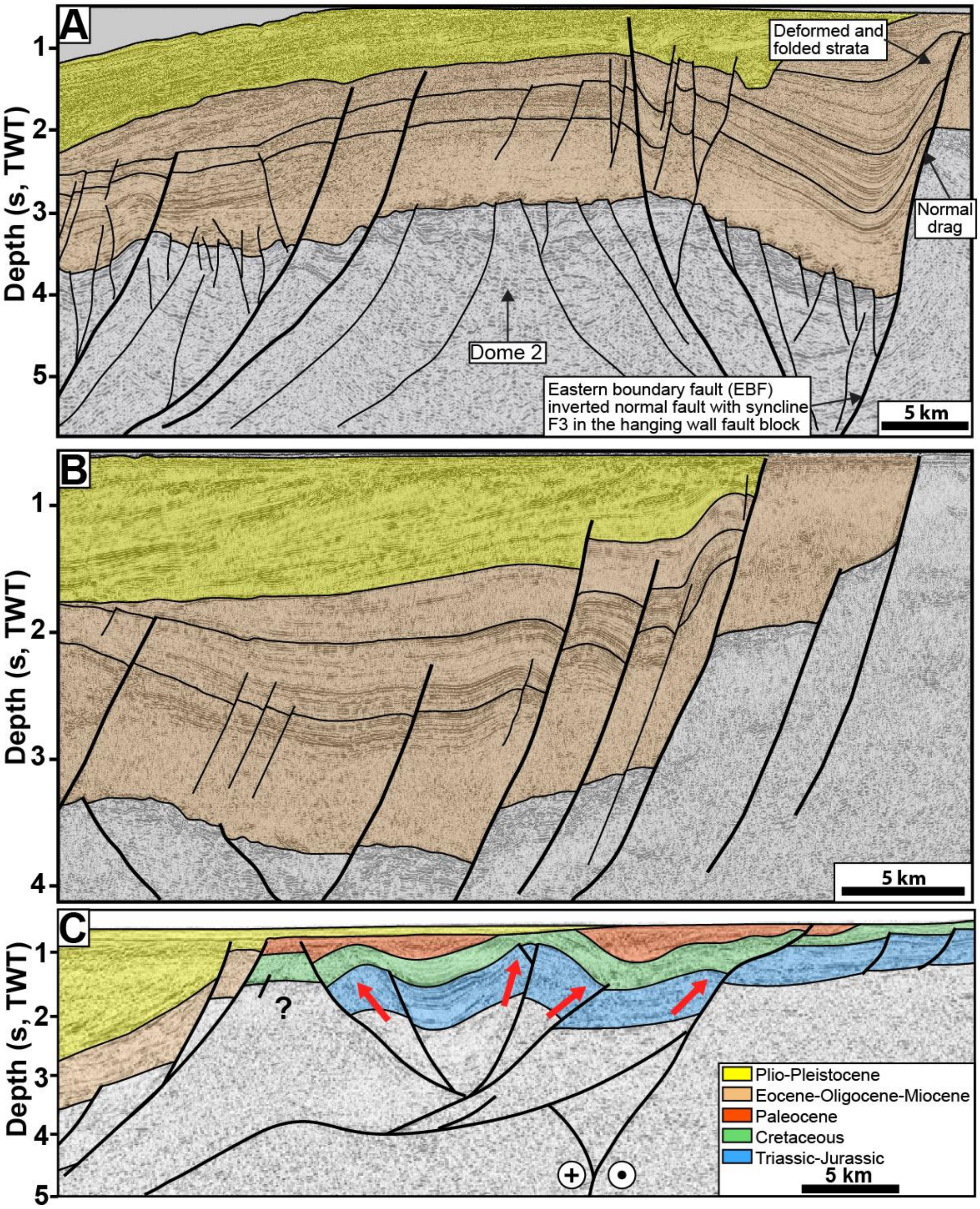
The Senja Shear Margin was active during the Eocene opening of the Norwegian-Greenland Sea dextral shear causing splitting out of slivers of continental crust. These slivers became embedded in the oceanic crust during continued seafloor spreading (Faleide et al., 2008). The Senja Shear Margin coincides with the western margin of a basin system superimposed on an area of significant crustal thinning. This part of the shear margin was characterized by a composite architecture even at the earliest stages of its development (Faleide et al., 2008). The basin system accumulated sedimentary sequences that reached thicknesses of up to 18-20 km. Subsequent shearing contributed to the development of releasing and restraining bends, associated pull-apart-basins, neutral strike-slip segments, flower-structures and fold-systems (*sensu* Crowell, 1974 a,b; Biddle & Christie-Blick, 1985a,b; Cunningham & Mann, 2007a,b). Particularly the hanging wall west of the Knølegga Fault Complex (see below) of the Barents Shear Margin was affected by wrench deformation as seen from several push-ups and fold systems (Grogan et al., 1999; Bergh & Grogan 2003). The structural development of the margin was complicated by active halokinesis (Knutsen & Larsen, 1997; Gudlaugsson et al., 1998; Ryseth et al., 2003).

Reflection seismic data and structural interpretation

The data set of this study includes 2D seismic reflection data from several surveys and well data in the Vestbakken Volcanic Province. Data coverage is less dense in northern part of the study area. Typical spacing of seismic lines is 4 km. Well 7316/5-1 was used to correlate the seismic data with formation tops in the study area whereas published paper based correlations provided calibration and age of each seismic horizon mapped (e.g. Eidvin et al., 1993; 1998 Ryseth et al., 2003). Three stratigraphic groups are encountered in the well, namely the Nordland Group (between 473 - 945 m); the Sotbakken Group (between 945-3752m) and Nygrunnen Group (between 3752-4014m) (Eidvin et al., 1993; 1998; www.npd.com). Several folds of regional significance and with axial traces that can be followed along strike for 2-3 km or more occur in the Vestbakken Volcanic Province. The folds commonly are situated in the hanging walls of extensional faults and the fold traces and the structural grain of the thick-skinned master faults are generally parallel. This shows that the position and orientation of the folds were determined by the preexisting basement structural fabric. The mapping of the folds is constrained by the spacing of refection seismic lines, so each fold trace may include undetected overlap-zones or axial off-sets. The folds were identified on the lower Eocene, Oligocene and lower Miocene levels. All the mapped folds are either positioned in the hanging walls of extensional (sometimes inverted) master faults or are dissected by younger faults with minor throws.

Strike-slip systems and analogue shear experiments

Shear margins and strike-slip systems are structurally complex and highly dynamic, so that the eventual architecture of such systems include structural elements that were not contemporaneous (e.g. Graymer et al., 2007; Crowell, 1962; 1974a,b; Woodcock & Fischer, 1986; Mousloupoulou et al., 2007; 2008). Analogue models offer the option to study the dynamics of such relations and therefore attracted the attention of early workers in this field (e.g. Cloos, 1928; Riedel, 1929) and have continued to do so until today. Early experimental works


A
Deformed and folded strata
Normal drag
Dome 2
Eastern boundary fault (EBF) inverted normal fault with syncline F3 in the hanging wall fault block
5 km
Depth (s, TWT)
1
2
3
4
5
B
5 km
Depth (s, TWT)
C
?
Plio-Pleistocene
Eocene-Oligocene-Miocene
Paleocene
Cretaceous
Triassic-Jurassic
5 km
Depth (s, TWT)

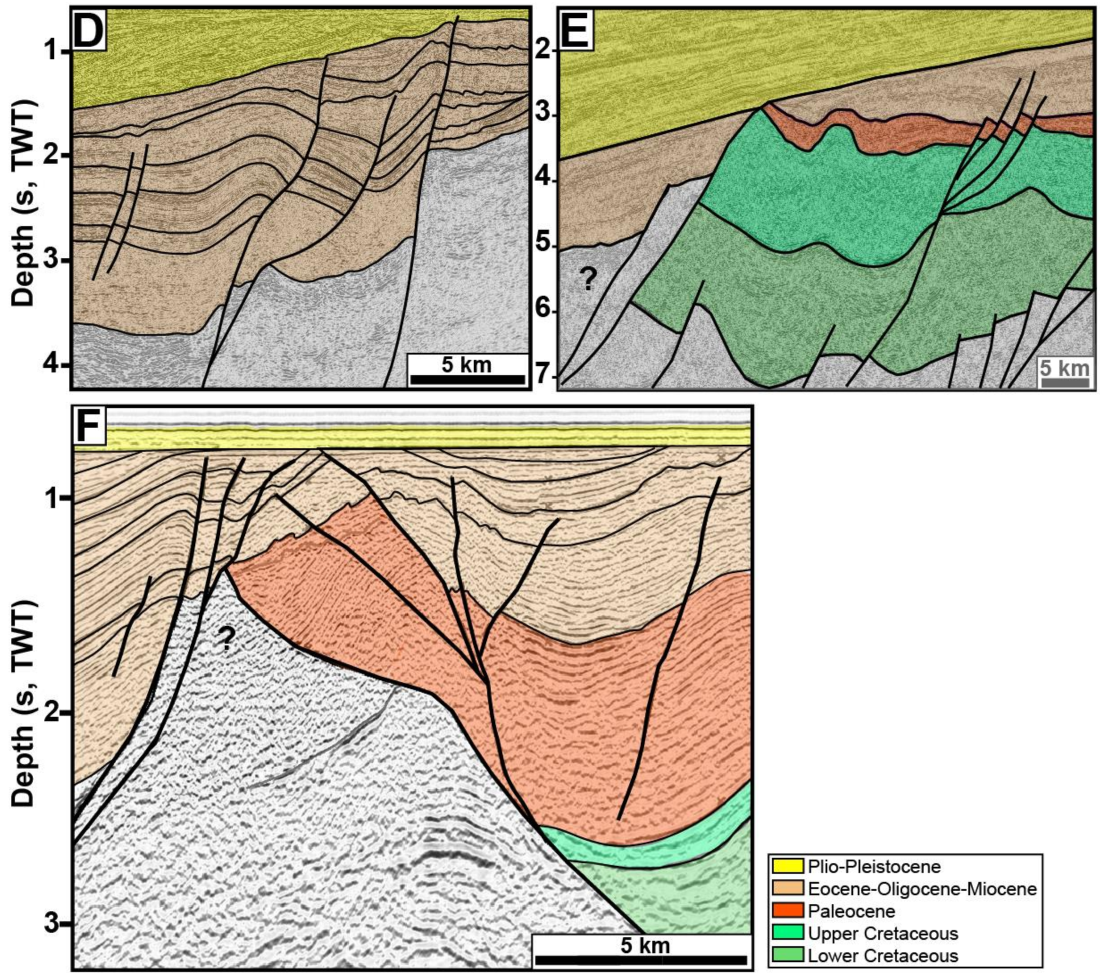


Figure 2: Seismic examples, Vestbakken Volcanic Province. **A)** Gentle, partly collapsed NE-SW-striking anticline/dome of uncertain origin in the eastern terrace domain of the southern Vestbakken Volcanic Province. **B,C**) Asymmetrical folds (fold family 2; Giannenas 2018) situated along the eastern margin of the Vestbakken Volcanic Province. These may represent primary SPE-4-structures focused in the hanging walls along margins of master fault blocks, representing reactivated SPE-2-structures. **D)** trains of symmetrical folds with upright fold axes (corresponding to PSE-5-structures) are preserved inside larger fault blocks. See text for explanation of SPE-structures. **E)** Section through push-up associated with restraining bend (PSE-4-structure). **F)** Flower (PSE-2)-structure in aera dominated by neutral shear.

mostly utilized one-layer ("Riedel-box") models (e.g. Emmons, 1969; Tchalenko, 1970; Wilcox et al., 1973), which were soon to be expanded by the study of multilayer systems (e.g. Faugère et al., 1986; Naylor et al., 1986; Richard et al., 1991; Richard & Cobbold, 1989, 1995; Schreurs, 1994, 2003; Manduit & Dauteuil, 1996; Dateuil & Mart, 1998; Schreurs & Colletta, 1998, 2003; Ueta et al., 2000; Dooley & Schreurs, 2012). The systematics and dynamics of strike-slip systems have been focused upon in a number of summaries like Sylvester (1985; 1988);

Biddle & Christie-Blick (1985 a,b); Cunningham & Mann (2007); Dooley & Schreurs (2012); Nemcok et al. (2016) and Peacock et al. (2016). Concepts and nomenclature established in these works are used in the following descriptions and analysis. Also, following Christie-Blick & Biddle (1985a,b) and Dooley & Schreurs (2012) we apply the term Principal Deformation Zone (PDZ) for the junction between the movable polythene plates underlying the experiment. The contact between the fixed and movable base defined a non-stationary velocity discontinuity ("VD"; Ballard et al., 1987; Allemand & Brun, 1991; Tron & Brun, 1991).

Several experimental works have particularly focused on the geometry and development of pull-apart-basins in releasing bend settings (Mann et al., 1983; Faugére et al., 1983; Richard et al., 1995; Dooley & McClay, 1997; Basile & Brun, 1999; Sims et al., 1999; Le Calvez & Vendeville, 2002; Mann, 2007; Mitra & Paul, 2011). The pull-apart basin was described by Burchfiel & Stewart (1966) and Crowell (1974a,b) as formed at a releasing bend or at a releasing fault step-over along a strike-slip zone (Biddle & Christe-Blick, 1985a,b). This basin type has also been termed "rhomb grabens" (Freund, 1971) and "strike-slip basins" (Mann et al., 1993) and is commonly considered to be synonymous with the extensional strike-slip duplex (Woodcock & Fischer, 1986; Dooley & Schreurs, 2012). In the descriptions of our experiments, we found it convenient to distinguish between extensional strike-slip duplexes in the context of Woodcock & Fischer (1986) and Twiss & Moores (2007, p. 140-141) and pull-apart basins (rhomb grabens: Crowell, 1974 a,b; Aydin & Nur, 1993) since they reflect slightly different stages in the development in our experiments (see discussion).

Experimental setup

To study the kinematics of complex shear margins, a series of analogue experiments were performed at the tectonic modelling laboratory (TecLab) of Utrecht University, The Netherlands. All experiments were built on two overlapping 1 mm thick plastic sheets (each 100 cm long and 50 cm wide) that were placed on a flat, horizontal table surface. The boundary between the underlying movable and overlying stationary plastic sheets had the shape of the mapped continent-ocean boundary (COB; **Figure 1B**). The moveable sheet was connected to an electronic engine, which pulled the sheet at constant velocity during all three deformation stages. Displacement rates were therefore not scaled. The modelling material was then placed on these sheets where the layers on the stationary sheet represent the continental crust including the continent-ocean transition (COT) whereas those on the mobile sheet represents the oceanic crust. The model layers were confined by aluminum bars along the long sides and sand along the short sides (**Figure 3A**). The continental crust tapers off towards the oceanic crust with a relatively constant gradient. A sand-wedge with a constant dip angle determined by the difference in thickness between the intact and the stretched crust, and that covered the width of the silicon putty layer, was made to simulate the ocean-continent transition (**Figure 3B**). The taper angle was kept constant for all models.

The pre-cut shape of the plate boundary includes major releasing bends positioned so that they correspond to the geometry of the COB and the three main structural segments of the Barents Shear Margin as follows. *Segment 1* of the BarMar-experiments (**Figure 4**) contained several sub-segments with releasing and restraining bends as well as segments of “neutral” (Wilcox et al., 1973; Mann et al. 1983; Biddle & Christie-Blick, 1985b) or “pure” (Richard et al., 1991) strike-slip. *Segment 2* had a basic crescent shape, thereby defining a releasing bend at its southern margin in the position similar to that of the Vestbakken Volcanic Province that merged into a neutral shear-segment along the strike of, whereas a restraining bend occupied the northern margin of the segment. *Segment 3* was a straight basement segment, defining a zone of neutral shear and corresponds to the strike-slip segment west of Svalbard (**Figure 1**).

The experiments included three stages of deformation with constant rates of movement of the mobile sheet at 10 cmhr^{-1} in all three stages. The relative angles of plate movements in the experiments were taken from post late Paleocene opening directions in the northeast Atlantic (Gaina et al., 2009). Dextral shear was applied in the *first phase* in all experiments by pulling the lower plastic sheet by 5 cm. In the *second phase* the left side of the experiment was extended by 3 cm orthogonally (BarMar6) or obliquely (315 degrees; BarMar 8 & 9) to the trend of the shear margin, whereas plate motion was reversed during the *third phase of deformation*, leading to inversion of earlier formed basins that had been

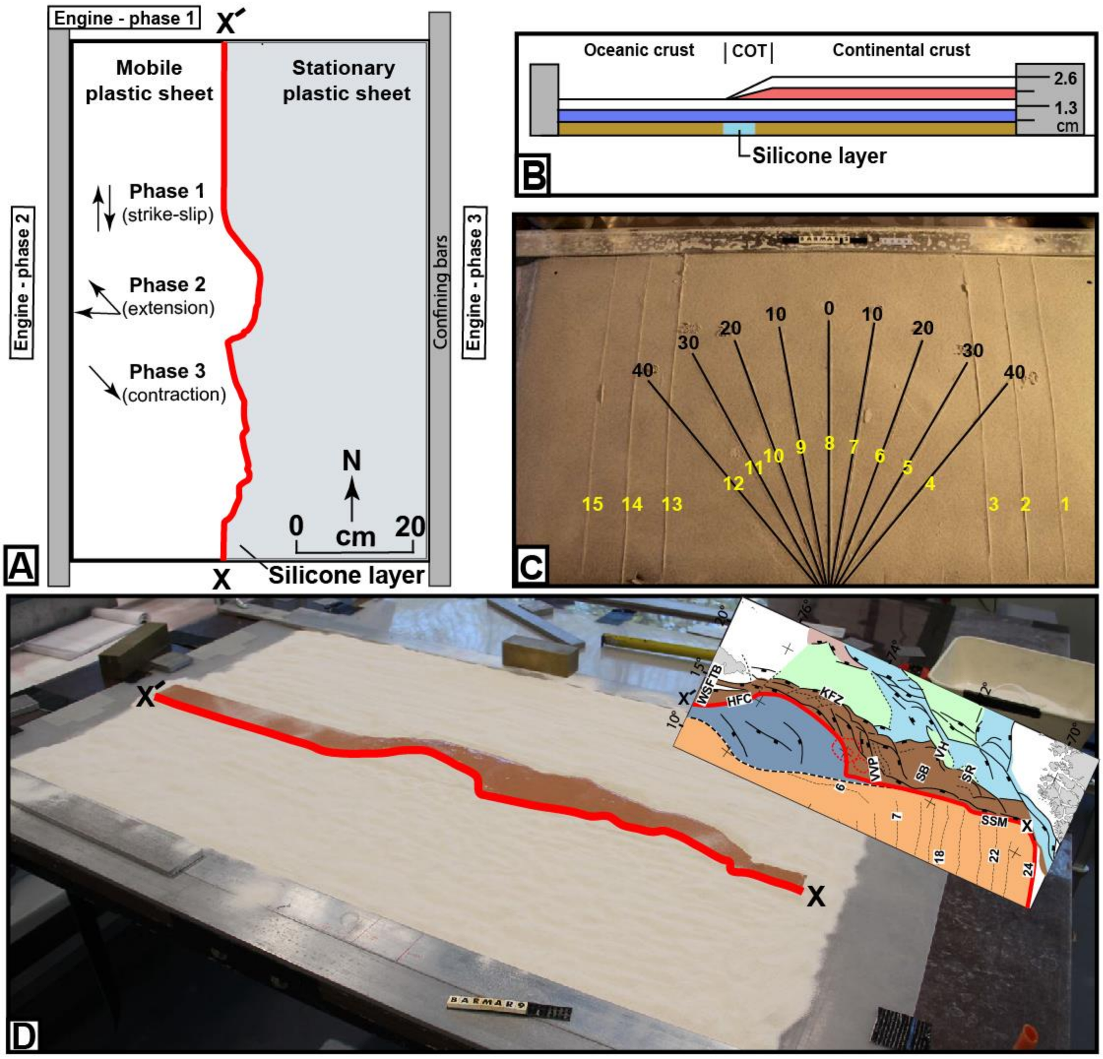


Figure 3: A) Schematical set-up of BarMar3-experiment as seen in map view. **B)** Section through same experiment before deformation, indicating stratification and thickness relations. **C)** Standard positions and orientation for sections cut in all experiments in the BarMar-series. Yellow numbers are section numbers. Black numbers indicate angle between the margins of the experiment (relative to N-S) for each profile. **D)** Outline of silicone putty layer as applied in all experiments. Inset shows original structural map of the Barents Margin used to define the width of the thinned crust. Red line (X-X') indicates the western limit of the thinned zone.

developed in the strike-slip and extensional phases. Sedimentary basins that develop due to strike-slip (phase 1) or extension (phase 2) have been filled with layers of colored feldspar sand by sieving, so that a smooth surface was obtained. These layers are primarily important for discriminating among deformation phases and thus act as marker horizons. Phase 3 was initiated by inverting the orthogonal (BarMar6) or oblique (BarMar 8 & 9) extension of Phase 2 to contraction as a proxy for ridge-push that likely was initiated when the mid-

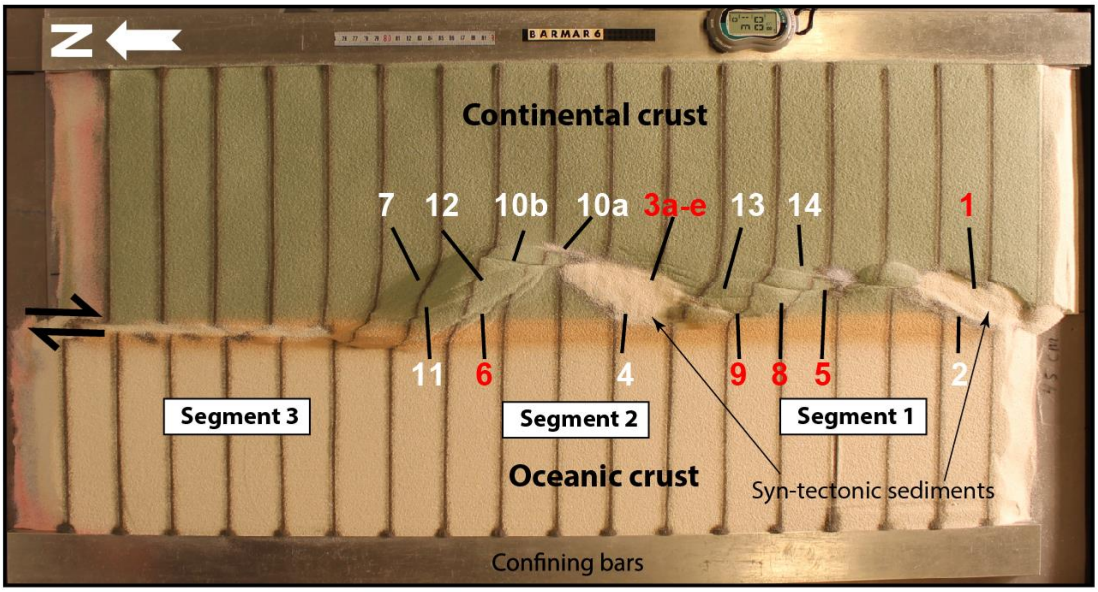


Figure 4: Position of segments and major structural elements as referred to in the text and subsequent figures (see particularly **Figures 5 and 6**). This example is taken from the reference experiment BarMar6. All experiments BarMar6-9 followed the same pattern, and the same nomenclature was used in the description of all experiments and provides the template for the definition of structural elements in **Figure 7**.

oceanic ridge was established in Miocene time in the North Atlantic (Moser et al., 2002; Gaina et al., 2009). Contraction generated by ridge-push has been inferred from the mid Norwegian continental shelf (Vågnes et al., 1998; Pascal & Gabrielsen, 2001; Faleide et al., 2008; Gac et al., 2016) and seems still to prevail in the northern areas of Scandinavia (Pascal et al., 2005), although far-field compression generated by other processes have been suggested (e.g. Doré & Lundin, 1996).

Coloured layers of dry feldspar sand represent the brittle oceanic and continental crust. This material has proven suitable for simulating brittle deformation conditions (Willingshofer et al., 2005; Luth et al., 2010; Auzemery et al., 2021). It is characterized by a grain size of 100-200 μm, a density of 1300 kgm^{-3}, a cohesion of ~16-45 Pa and a peak friction coefficient of 0.67 (Willingshofer et al., 2018). Additionally, a 8 mm thick and of variable width corresponding to the transition zone (as mapped in reflection seismic data) of 'Rhodorsil Gomme GSIR' (Sokoutis, 1987) silicone putty mixed with fillers was used as a proxy for the thinned and weakened continental crust at the ocean-continent transition (**Figure**

1B and 3A,B). This Newtonian material (n=1.09) has a density of 1330 $kgm^{-3}$and a viscosity of $1.42x10^4$ Pa.s.

The experiments were scaled following standard scaling procedures as described by Hubbert (1937), Ramberg (1967) or Weijermars and Schmeling (1986), assuming that inertia forces are negligible when modelling tectonic processes on geologic timescales (see Ramberg (1981) and Del Ventisette et al. (2007) for a discussion on this topic). The models were scaled so that 10 mm in the model approximates c. 10 km in nature yielding a length scale ratio of $1.00E^{-6}$. As such, the model oceanic and continental crusts scale to 18 and 26 km in nature, respectively, which, although slightly overestimating the oceanic crustal thickness (10-12 km) is in full agreement with the estimated thickness of the thinned oceanward segment of the continental crust (30-20 km Breivik et al., 1998).

The brittle crust, dry feldspar sand, deforms according to the Mohr-Coulomb fracture criterion (Horsfield, 1977; Mandl et al., 1977; McClay, 1990; Richard et al., 1991; Klinkmüller et al., 2016), whereas silicone putty promotes ductile deformation and folding. The geometry applied in the present experiments is accordingly well suited for the study of the COB in the Barents Shear Margin (Breivik et al., 1998).

When complete, the experiments were covered with a thin layer of sand further to stabilize the surface topography before the models were saturated with water and cross-sections that were oriented transverse to the velocity discontinuity were cut in a fan-shaped pattern (**Figure 3C**). All experiments have been monitored with a digital camera providing top-view images at regular time intervals of one minute.

All experiments performed were oriented in a N-S-coordinate framework to facilitate comparison with the western Barents Sea area and had a three-stage deformation sequence (dextral shear – extension – contraction). All descriptions and figures relate to this orientation. It was noted that all experiments reproduced comparable basic geometries and structural types, demonstrating robustness against variations in contrasting strength of the “ocean-continent”-transition zone, which included a zone of silicone putty with variable width below an eastward thickening sand-wedge (**Figure 3B**). The experiments were terminated before the full closure of the basin system, in accordance with the extension vector

> contraction vector as in the North Atlantic (see Vågnes et al. 1998; Pascal & Gabrielsen 2001; Gaina et al. 2009).

Modelling Results

A series of nine experiments (BarMar1-9) with the set-up described above was performed. Experiments BarMar1-5 were used to calibrate and optimize geometrical outline, deformation rate, and angles of relative plate movements and are not shown here. The optimized geometries and experimental conditions were utilized for experiments BarMar6-9, of which BarMar6 and 8 (and some examples from BarMar9) are illustrated here. They yielded similar results in that all crucial structural elements (faults and folds) were reproduced in all experiments as described in the text are shown in **Figure 4**. It is emphasized that the extensional basins affiliated with the extension phase (phase 2) were wider for the orthogonal (BarMar6) as compared to the oblique extension experiments (BarMar 8) (**Figures 5 and 6**). Furthermore, the fold systems generated in the experiments that utilized oblique contraction of $315/135^0$ (BarMar8-9) produced more extensive systems of non-cylindrical folds. These folds also had continuous, but more curved fold traces as compared to the experiments with orthogonal extension/contraction (BarMar6). The fold axes generally rotated to become parallel to the (extensional) master faults delineating the pull-apart basins generated in deformation stage 1 in experiments with an oblique opening/closing angle.

Examples of the sequential development is displayed in **Figures 5 and 6**, and summarized in **Figure 7**. Elongated positive structural elements with fold-like morphology as seen on the surface were detected during the various stages of the present experiments. The true nature of those were not easily determined until the experiments were terminated and transects could be examined. Such structures included buried push-ups (*sensu* Dooley & Schreurs, 2012), antiformal stacks, back-thrusts, positive flower structures, fold trains, and simple anticlines. For convenience, we use the non-genetic term “positive structural elements” termed *PSEm-n* for such structure types as seen in the experiments in the following description. In the following the deformation in each segment is characterized for the three deformation phases **(Table 1).**

Table 1

Characteristics of Positive Structural Element (PSE 1-6) as described in the text and shown in figures. Note that the PSE-1-structures that were developed in the earliest stages of the experiments became cannibalized during the continued deformation. No candidates of these structures were identified in the reflection seismic sections.

Struct. type	Structural configuration	Orientation	Expr. stage	Segment	Recognized in seismic	Figure Expr	Figure Seism
PSE-1	Open syn-anticline system	135 deg	Stage 1	1,3	?	5,6	1A?
PSE-2	Incipient flower or half-flower	Parallel master fault	Stage 1	1,2,3	Yes	5,6,8	1B
PSE-3	Forced folds above rotated fault blocks	Parallel master fault in releasing bend	Stage 2	1,2	Yes	9B	
PSE-4	Push-up	Paralllel master fault in restraing bend	Stage 1	2	Yes	9D	1C
PSE-5	Anticlines/snake-heads in hanging walls	Parallel master faults	Stage 3	1,2,3	Yes	9C,D	1D,E
PSE-6	Anticline-syncline trains	Parallel master faults	Stage 3	1,2,3	Yes	12	1F

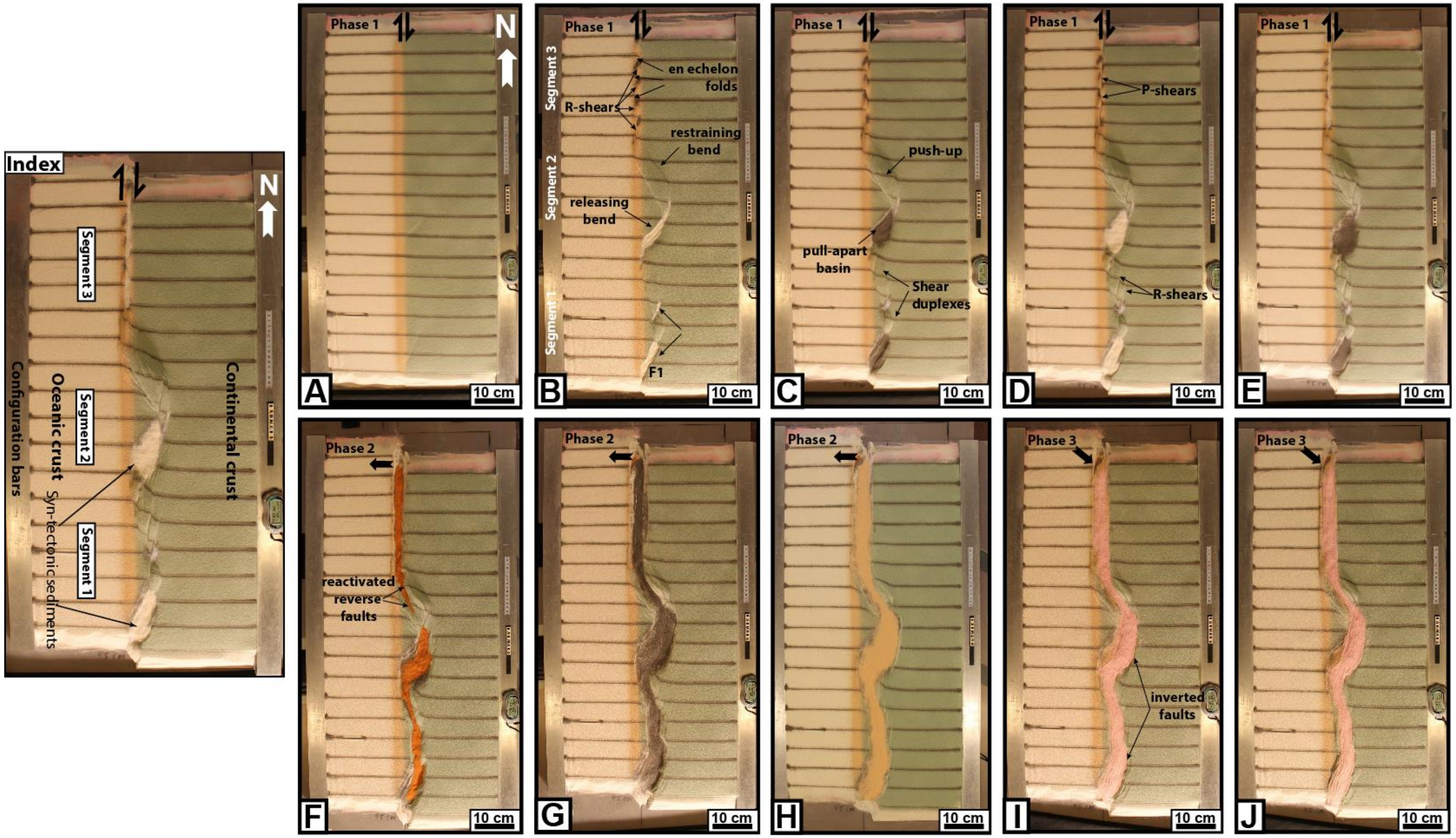


Figure 5: Sequential development of experiment BarMar6 by 0.5, 2.4, 3.5, 4.0 and 5.0 cm of dextral shear (Steps A-E), orthogonal extension (steps F-H) and oblique contraction (steps I-J). The master fault strands are numbered in **Figure 4**, and the sequential development for each structural family is shown in **Figure 7**. The reference panel to the upper left shows the positions of the segments.

Deformation phase 1: Dextral shear stage

Segment 1: Differences in the geometry of the pre-cut fault trace between segments 1, 2 and 3 became visible after the very initial deformation stage. Particularly in segments 1 and 3 an array of oblique *en échelon* folds in between Riedel shear structures (*PSE-1-structures*) oriented c. 135°(NW-SE) to the regional VD rotating towards NNW-SSE by continued shear (**Figure 8**; see also Wilcox et al., 1973; Ordonne & Vialon, 1983; Richard et al., 1991; Dooley & Schreurs, 2012). These were simple, harmonic folds with upright axial planes and fold axial traces extending a few cm beyond the surface shear-zone described above. They had amplitudes on the scale of a few millimeters and wavelengths on scale of 5 cm. The PSE-1-structures interfered with or were dismembered by younger structures (Y-shears and PSE-2-structures; see below) causing northerly rotation of individual intra-fault zone lamellae (remnant PSE-1-structures; **Figure 8**). Structures similar to PSE-1-fold arrays are known from almost all strike-slip experiments reported and described in the literature (e.g. Cloos, 1928; Riedel, 1929; See Dooley & Schreurs, 2012 for summary) and are therefore not given further attention here.

By 0.25 cm of horizontal displacement in segment 1, which included releasing and restraining bends separated by a central strand of neutral shear, a slightly curvilinear surface trace of a NE-SW-striking, top-NW normal fault in the southernmost part of segment 1 developed. This co-existed with the PSE-1-structures and became paralleled by a normal fault with opposite dip (fault 2, **Figure 4**) so that the two faults constrained a crescent- or spindle-shaped incipient extensional shear duplex (**Figures 5B and 6B**; see also Mann et al., 1983).

A system of separate *en échelon* N-S to NNE-SSE-striking normal and shear fault segments became visible in segment 1 after ca. 1 cm of shear (**Figure 5C,D**). These faults did not have the orientations as expected for R (Riedel) - and R' (anti-Riedel)- shears (that would be oriented with angles of approximately 15 and 75° from the master fault trace) but became progressively linked with along strike growth and the development of new faults and fault segments. They thereby acquired the characteristics of Y-shears (oriented sub-parallel to the master fault trace), dissecting the PSE-1-structures. By 2.4 cm of shear, segment 1 had become one unified fault array (**Figures 5D and 6D**), delineating a system of incipient

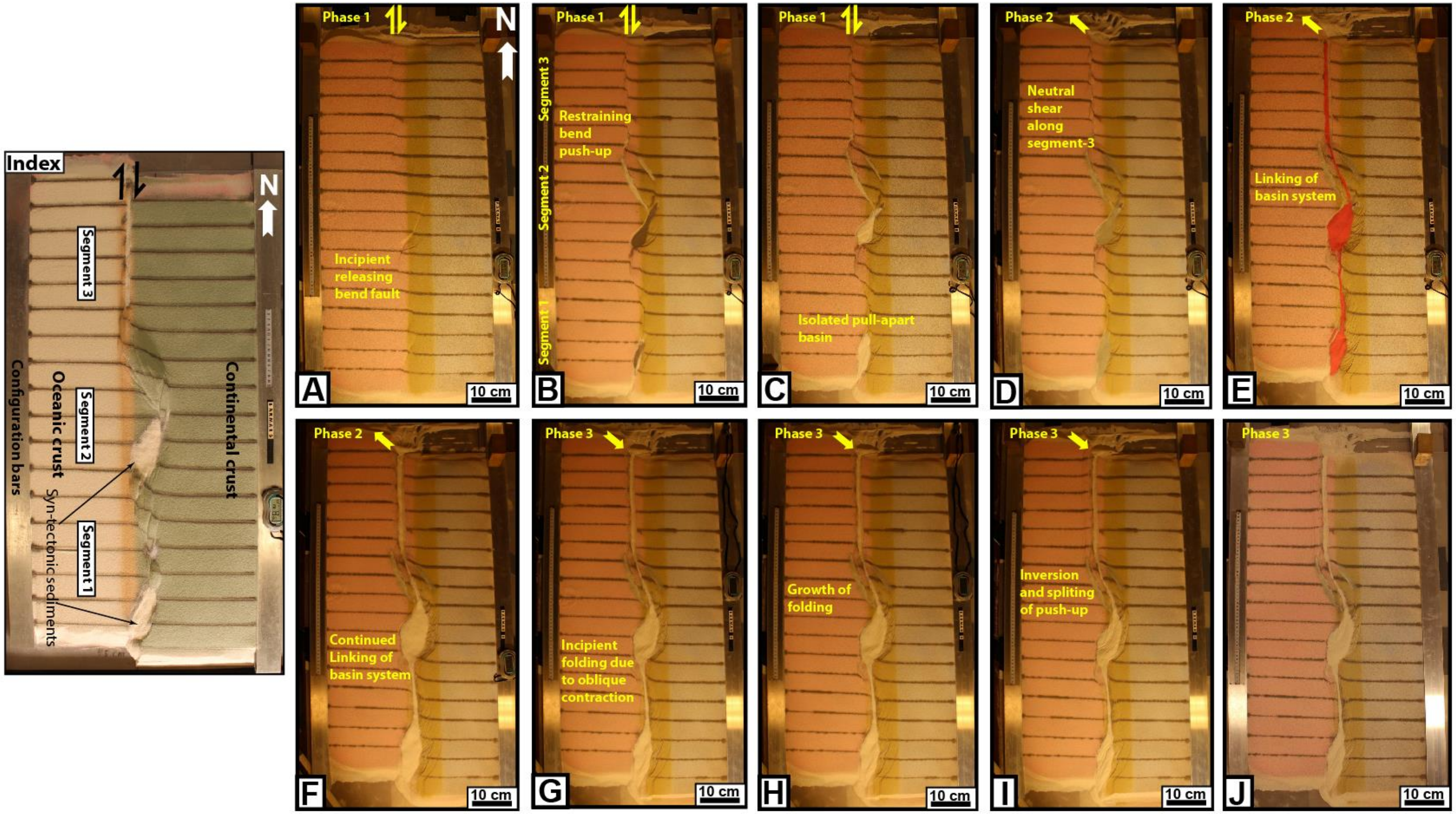


Figure 6: Sequential development of experiment BarMar8 by 0.5, 2.4, 3.5, 4.0 and 5.0 cm of dextral shear (Steps A-E), oblique extension (steps F-H) and oblique contraction (steps I-J). The master fault strands are numbered in **Figure 3**, and the sequential development for each structural family is shown in **Figure 7**. Phases 2 and 3 involved oblique (315^0) extension and contraction in this experiment. The reference panel to the upper left shows the positions of the segments.

push-ups or positive flower structures (*PSE-2-structures;* **Figures 8 and 10, sections B1 and B3**).

The PSE-2-structures had amplitudes of 1 - 2 cm and wavelengths of 3 - 5 cm as measured on the surface with fault surfaces that steepened down-section, the deepest parts of the structures having cores of sand-layers deformed by open to tight folds. The folds had upright or slightly inclined axial planes, dipping up to 55^{o}, mainly to the east. The structures also affected the shallowest layers down to 1-2 cm in the sequence, but the shallowest sequences were developed at a later stage of deformation and were characterized by simple gentle to open anticlines. These structures were constrained to a deformation zone directly above the trace of the basement fault, similar to that commonly seen along shear zones (e.g. Tchalenko, 1971; Crowell, 1974 a,b; Dooley & Schreurs, 2012). This zone was 3-4 cm wide and remained stable throughout deformation stage 1 and was restricted to the close vicinity of the basement shear fault itself. A horse-tail-like fault array developed by ca. 3 cm of shear at the transitions between segments 1 and 2 (**Figures 5B-D and 6B-D)**.

The structuring in *Segment 2* was ruled by the pre-cut crescent-shaped basement fault (velocity discontinuity) that caused the development of a releasing bend along its southern, and a restraining bend along its northern border (**Figure 11**). The first fault of fault array 3a-e in the southern part of Segment 2 (**Figure 4**) was activated after c. 0.15 cm of bulk horizontal displacement (**Figure 7**). It was situated directly above the southernmost precut releasing bend, defining the margin of crescent-shaped incipient extensional strike-slip duplexes (in the context of Woodcock & Fischer, 1986, Woodcock & Schubert, 1994 and Twiss & Moores, 2007, p. 140-141). The developing basin got a spindle-shaped structure and developed into a basin with a lazy-S-shape (Cunningham & Mann, 2007; Mann, 2007). The basin widened towards the east by stepwise footwall collapse, generating sequentially rotating crescent-shaped extensional fault blocks that became trapped as extensional horses in the footwall of the releasing bend (**Figure 11**). In the areas of the most pronounced extension the crestal part of the rotational fault blocks became elevated above the basin floor, generating ridges that influenced the basin floor topography and hence, the sedimentation. By continued rotation of the fault blocks and simultaneous sieving of sand the crests

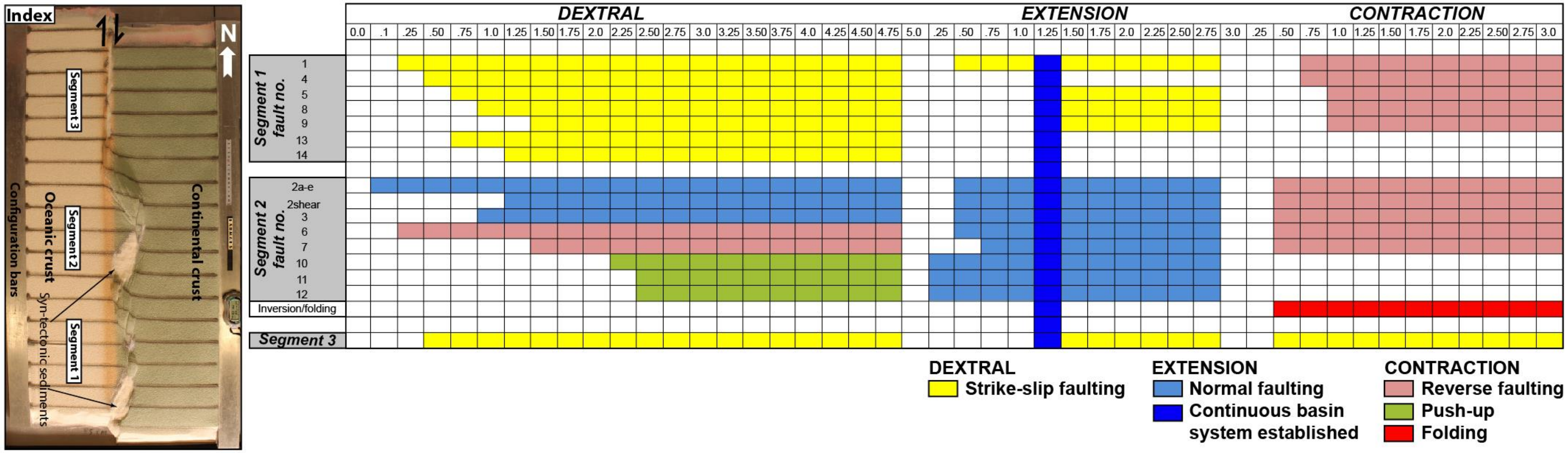


Figure 7: Summary of sequential activity in each master fault in Experiment BarMar6 (**Figure 5**) (for position of each fault, see **Figure 4**). Type and amount of displacement is shown in two upper horizontal rows. The vertical blue bar indicates the stage at which full along-strike communication became established between marginal basins. Color code (see in-set) indicates type of displacement at any stage. The reference panel to the left shows the positions of the segments.

of the blocks became sequentially uplifted, generating forced folds (Hamblin, 1965; Stearns, 1978; Groshong, 1989; Khalil & McClay, 2016) (**Figure 10A**). In the analysis we used the term *PSE-3-structures* for these features. Simultaneously, an expanding sand-sequence became trapped in the footwalls of the master faults, defining typical growth-fault geometries.

By a shear displacement of 0.55 cm additional curved splay faults were initiated from the northern tip of the master fault of fault 3f; **Figure 7**), delineating the northern margin of a rhombohedral pull-apart-basin (Mann et al., 1983; Mann, 2007; Christie-Blick & Biddle, 1985) and with a geometry that was indistinguishable from pull-apart basins or rhomb grabens affiliated with unbridged *en échelon* fault arrays (Crowell, 1974 a,b; Aydin & Nur, 1993). Although sand was filled into the subsiding basins to minimize the graben relief

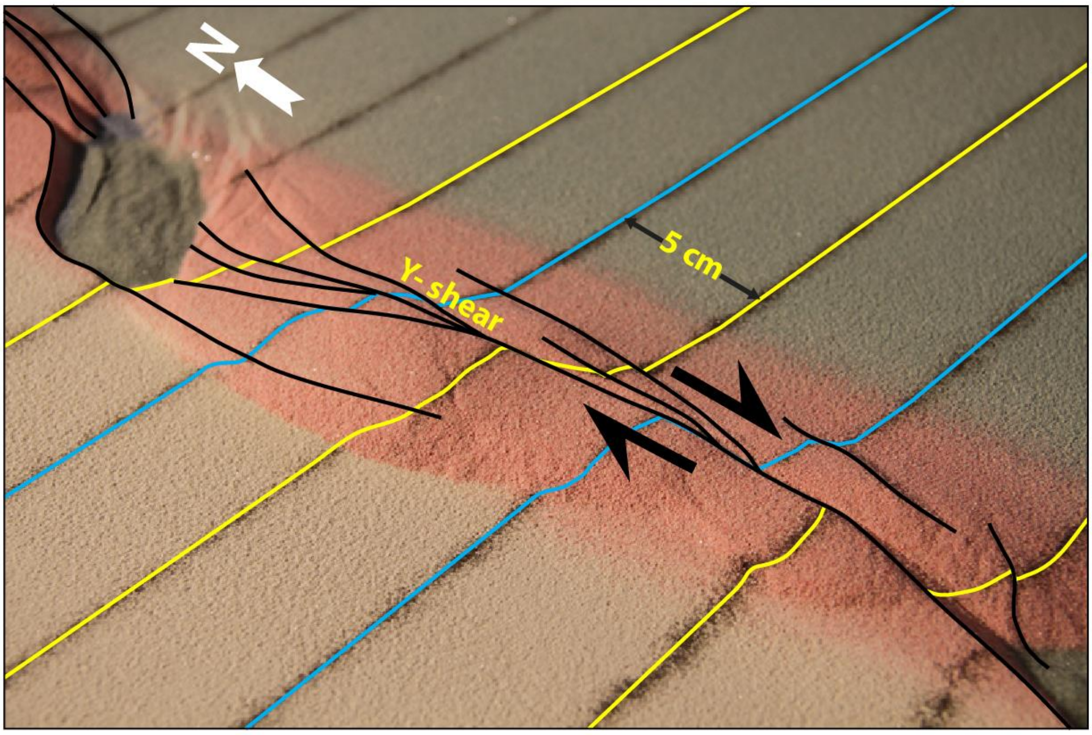


Figure 8: PSE-1 anticline-syncline pairs in segment 1 of experiment BarMar6 in an oblique view (see **Figure 4** for position of Segment 1). PSE-1 folds (indicated by relief defined by blue and yellow markers) were constrained to the central fault zone (defined by Y-shear and its splay faults) and extended only 3-4 cm beyond it. PSE-2 structures (incipient push-ups and positive flower structures) were delineated by shear faults (black lines) and completely cannibalized PSE-1 structures by continued shear. Yellow and blue reference lines illustrate the rotation of the fold axial trace caused by dextral shear. Already pre-shear distance between the markers (blue and yellow lines) was 5cm. Black arrow indicates shear direction.

and to prevent gravitational collapse, the sub-basins that were initiated in the shear-stage were affected by internal cross-faults, and the initial basin units remained the deepest so that the buried internal basin topography maintained a high relief with several apparent depo-centers separated by intra-basinal platforms. Systems of linked shear faults and PSE-structures became established in the central part with neutral shear that separate the releasing and restraining bends and development similarly to that seen for segment 3 (see below), but these structures were soon destroyed by the interaction between the northern and southern tips of the extensional and contractional shear duplexes (**Figure 10**).

The first structure to develop in the regime of the restraining bend (segment 2; was a top-to-the-southwest (antithetic) thrust fault at an angle of 145^0 with the regional trend of the basement border as defined by segments 1 and 3 (Fault 6). It became visible by 0.5 cm of displacement. The northern part of segment 2 became, however, dominated by a synthetic contractional top-to-the-northeast fault that was initiated by 0.85 cm of shear (Fault 7; **Figures 5 and 6**). Thus, faults 6 and 7 delineated a growing half-crescent-shaped 5-7-cm wide push-up structure (Aydin & Nur, 1982; Mann et al., 1983) south of the restraining bend (**Figure 9**; *PSE-4-structures*). By continued shear these structures got the character of an antiformal stack.

Segment 3 defined a straight strand of neutral shear. Its development in the BarMar-experiments followed strictly that known from numerous published experiments (e.g. Tchalenko, 1970; Wilcox et al., 1973; Harding, 1974; Harding & Lowell, 1979; Naylor et al., 1986; Sylvester, 1988; Richard et al., 1991; Woodcock & Schubert, 1994; Dauteuil & Mart, 1998; Mann, 2007; Casas et al., 2001; Dooley & Schreurs, 2012). A train of Riedel-shears, occupying the full length of the segment, appeared simultaneously on the surface after a shear displacement of 0.5 cm, occupying a restricted zone with a width of 2-3 cm. The Riedel-shears dominated the continued structural development of Segment 3. Riedel'-shears were absent throughout the experiments, as should be expected for a sand-dominated sequence (Dooley & Schreurs, 2012). P-shears developed by continued shear, creating linked rhombic structures delineated by the Riedel- and P-shears generating positive structural elements with NW-SE- and NNE-SSE-striking axes (see also Morgenstern & Tchalenko, 1967), soon coalescing to form Y-shears.

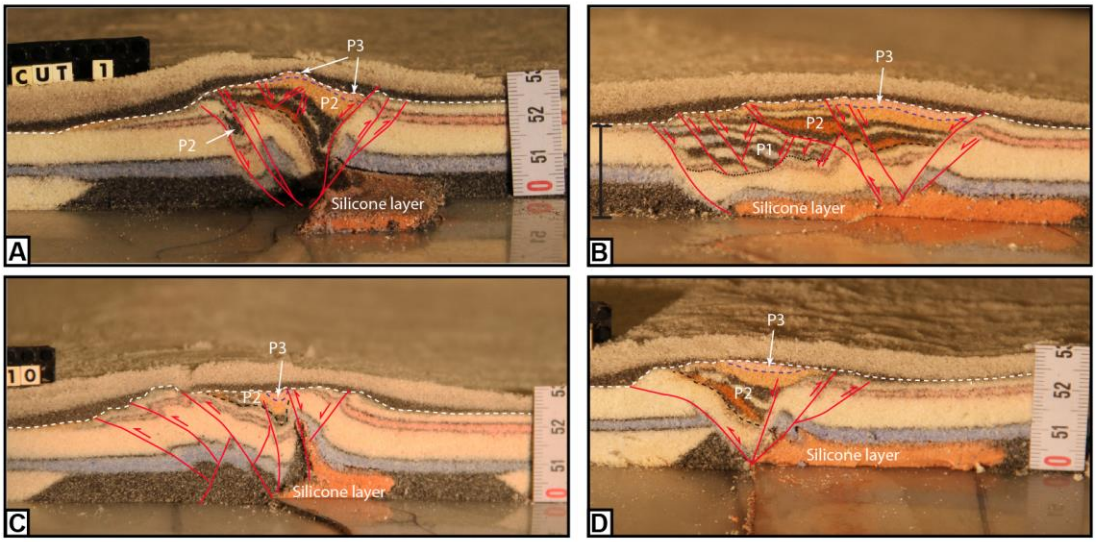


Figure 9: Cross-sections through PSE-2-related structures. PSE-structures are marked with P and PSE-number as described in text (see also Table 1). **A)** Folded core of incipient push-up/positive flower structure in segment 1, experiment BarMar6. The fold structure is completely enveloped of shear faults that have a twisted along-strike geometry. Note that the eastern margin of the structure developed into a negative structure at a late stage in the development (filled by black-pink sand sequence) and that the silicone putty sequence (basal pink sequence) was entirely isolated in the footwall. **B)** Similar structure type in experiment BarMar8. However, the basal silicone putty layer here bridged the basal high-strain zone so that folding occurred in the footwall as well as in the hanging. Folds propagated up-section into the sand layers (blue). The folds in upper (pink) layers are younger and were associated with the contractional stage (PSE-6-structures). **C)** Contraction associated with "crocodile structure" in the footwall of the main fault in segment 1, experiment BarMar8. Note disharmonic folding with contrasting fold geometries in hanging wall and footwall and at different stratigraphic levels in the footwall, indicating that shifting stress situation in time and space occurred in the experiment. **D)** Transitional fault strand between to more strongly sheared fault segments (experiment BarMar9).

Transverse sections document that these structures were cored by push-up anticlines, positive half-flower structures and full-fledged positive flower structures in the advanced stages of shear (*PSE-4-structures*) (**Figures 5 and 6; See also Figure 10**). These were accompanied by the development of *en échelon* folds and flower structures as commonly reported from strike-slip faults in nature and in experiments. The width of the zone above the basal fault remained almost constant throughout the experiments, but was somewhat wider in experiments with thicker basal silicone polymer layers, similar to that commonly described from comparable experiments (e.g. Richard et al., 1991).

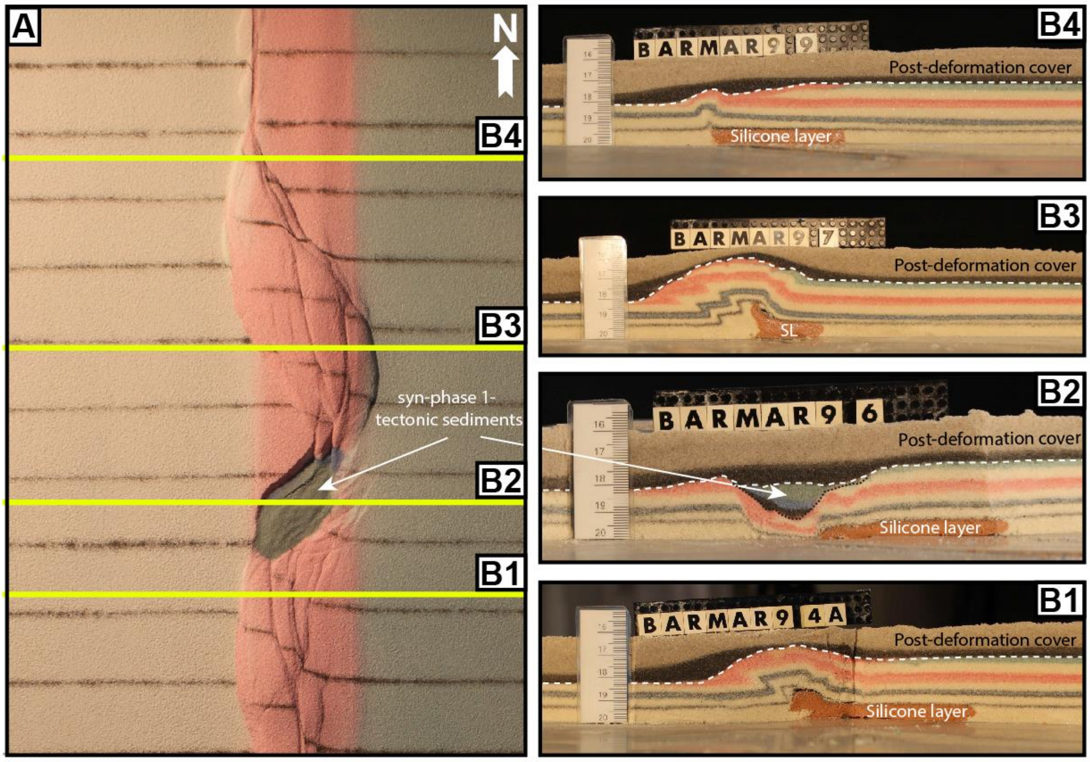


Figure 10: A) Contrasting structural styles along the master fault system in segment 2 in map view and **(B)** cross sections of experiment BarMar9. SL denotes silicone layer, the stippled line the boundary between pre-and syn-deformation layers and the white dashed line the boundary with the post-deformation layers.

Deformation Phase 2: Extension

The late Cretaceous-Palaeocene dextral shear was followed by pure extension that accompanied the opening along the Barents Shear Margin in the Oligocene. Our experiments focused on the effects of oblique extension, acknowledging that plate tectonic reconstructions of the North Atlantic suggest an extension angle of 315^{o} (Gaina et al., 2009).

All strike-slip basins widened in the extensional stage and as one would expect, the basins generated in orthogonal extension became wider than those generated in oblique extension. In both cases, however, extension promoted enhanced relief that had been generated in the shear-stage. In the earliest extensional stage, the strike-slip basin in segment 2 dominated the basin configuration. By continued extension the linear segments and the minor pull-apart basins in segments 1 and 2 started to open and became interlinked, subsequently generating a linked basin system that runs parallel to the entire shear margin (**Figures 5F-G, 6F-G**). The basins had become completely interlinked by an extension of 1.25 cm (marked by the vertical dark blue line in **Figure 7**). The orthogonal extension-phase also reactivated and linked several master faults that were established in deformation phase 1 (**Figures 5A and 6A**). This became evident by an extension of 0.25 – 0.50 cm and included the southern fault margin, the push-up and the splay faults defining the crestal collapse graben (Faults 6, 11 and 12; **Figure 4**). Among the faults that remained inactive throughout the extension phase were the antithetic contractional fault delineating the push-ups in segment 2 (Fault 6; **Figure 4**). The Y-shear in Segment 3 was reactivated as a straight, continuous extensional fault in phase 2. Total extension in stage 2 was 5 cm.

Deformation Phase 3: contraction

In our experiments the extension stage was followed by oblique contraction (parallel to the direction of extension as applied for each experiment). A part of the early-stage contraction was accommodated along new faults. It was more common, however, that faults that had been generated in the strike-slip and extensional stages became reactivated and rotated, and the development of isolated folds, which were commonly associated with inverted fault traces, generating snake-head or harpoon-structures structures (Cooper et al., 1989; Coward, 1994; Allmendinger, 1998; Yameda & McClay, 2004; Pace & Calamitra, 2014; *PSE-5-stuctures*). The dominant structures affiliated with the contractional stage was still new folds with traces oriented orthogonal to the shortening direction and sub-parallel to the preexisting master fault systems that defined the margin and basin margins (**Figure 12**). Also, some deep fold sets that had been generated during the strike-slip phase and seen as domal surface features became reactivated, causing renewed growth of surface structures (see **Figure 10** and explanation in figure caption). These folds were generally up-right cylindrical buckle folds in the initial contractional and with very large trace length: amplitude-ratio (*SPE-6-structures*). Some intra-basin folds, however, defined fold arrays that crossed the basins in a diagonal fashion. Particularly the folds situated along the basin margins developed into fault propagation-folds above low-angle thrust planes. Such faults aligning the western basin margins could have an antithetic attitude relative to the direction of contraction.

During the contractional phase the margin-parallel, linked basin system started immediately to narrow and several fault strands became inverted. The basin-closure was a continuous process until the end of the experiment by 3 cm of contraction. The contraction was initiated as a proxy for an ESE-directed ridge-push stage. The first effect of this deformation stage was heralded by uplift of the margin of the established shear zone that had developed into a rift during deformation stage 2. This was followed by the reactivation and inversion of some master faults (e.g. fault a2; **Figure 4**) and thereafter by the development of a new set of low-angle top-to-the-ESE contractional faults. These faults displayed a sequential development (fault family 1; **Figure 7**) and were associated with folding of the strata in the rift structure, probably reflecting foreland-directed in-sequence thrusting (SPE-5 and PSE-6 fold populations).

Discussion

The break-up and subsequent opening of the Norwegian-Greenland Sea was a multi-stage event (**Figure 13**) that imposed shifting stress configurations overprinting the already geometrically complex Barents Shear Margin. Therefore, scaled experiments were designed to illuminate its structural development. The experiments utilized three main segments that correspond to the Senja Fracture Zone (segment 1), the Vestbakken Volcanic Province (segment 2) and the Hornsund Fault Zone (segment 3) respectively and three deformation phases (dextral shear, oblique extension and contraction). Several structural families (PSE 1-6) generated in the experiments correspond to structural features observed in reflection seismic sections. In the following discussion we utilize these two data sets in explaining the sequential development of each segment of the shear margin.

Structures of phase 1 (dextral shear)

Segment 1 (corresponding to the Senja Fracture Zone) was dominated by neutral dextral shear, although jogs in the (pre-cut) fault provided minor sub-segments with subordinate releasing and restraining bends.

PSE-1-folds seen in the incipient shear phase were confined to the area just above the basal master fault (VD) and its immediate vicinity (see also experiments in

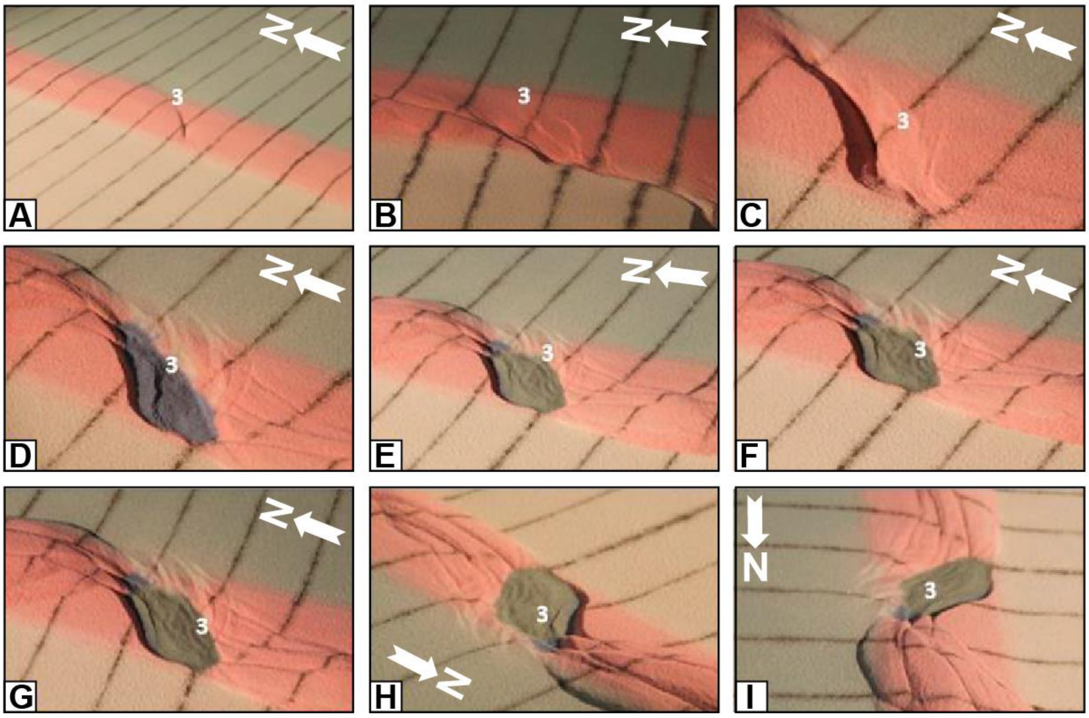


Figure 11: Nine stages in the development of the extensional shear duplex system above the releasing bend in experiment BarMar9. The master faults that developed at an incipient stage (e.g. Fault 3 that constrained the eastern margin of the extensional shear duplex, marked with"3" in the figure; see also **Figure 7**) remained stable and continued to be active throughout the experiment, but became overstepped by new faults in its footwall. These were reactivated as contraction faults at the later stages (stages H and I in this figure). The developing basement was stabilized by infilling of gray sand during this part of the experiment. Fault 3 remained broke through the basin infill also after the basin infill overstepped the original basin margin. The distance between the markers (dark lines) is 5cm. White arrow marks north-direction. Note that figures "H" and "I" (bottom right) is viewed from directions that differs from the other figures.

series "e" and "f" of Mitra & Paul, 2011). Counterparts to PSE-1 structural population were not identified in the seismic data, although some isolated, local anticlinal features could be dismembered remnants of such. Because of their constriction to the near vicinity of the master fault it is reasonable that structures generated at an early stage of shear are vulnerable to cannibalization by younger structures with axes striking parallel to the main shear fault (Y-shears; SPE-2-structures). We therefore conclude that this structure population was destroyed during the later stages of shear and during the subsequent stages of extension and contraction.

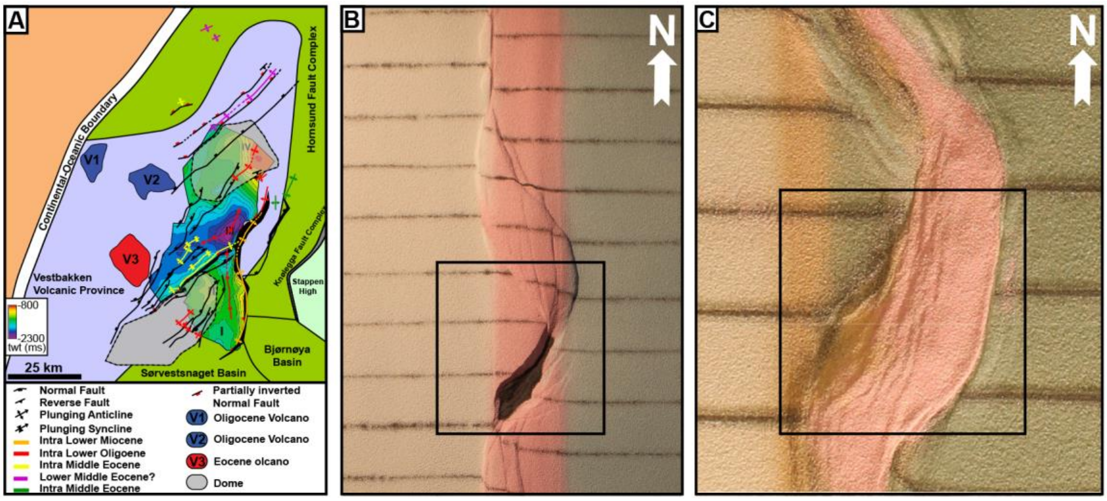


Figure 12: PSE-5-folds generated during phase 3-inversion, experiment BarMar8. Note that fold axes mainly parallel the basin rims, but that they deviate from that in the central parts of the basins in some cases. The folds are best developed in segment 2, which accumulated extension in the combined shear and extension stages.

PSE-1-folds that developed at an incipient stage were immediately pursued by the development of two sets of NNE-SSW-striking normal faults with opposite throws in the releasing bend areas (e.g. fault 2 **Figure 4**). The two faults defined crescent- or spindle-shaped incipient extensional shear duplexes. These structures were stable during the remainder of the experiments and their master faults became reactivated during the extensional and contractional phases (see below). The most prominent of these structures corresponds to the position of the Sørvestsnaget Basin (**Figure 1B**).

Segment 2, which was controlled by a pre-cut crescent-shaped discontinuity in the experiments corresponds to the Vestbakken Volcanic Province and the southern extension of the Knølegga Fault Complex of the Barents Shear Margin (**Figures 1B and 4**). The Vestbakken Volcanic Province is dominated by interfering NNW-SSE- and NE-SW striking fold- and fault systems in its central part, whereas N-S-structures are more common along its eastern margin (**Figure 12A**) (Jebsen & Faleide, 1998; Giannenas, 2018). Intra-basinal highs and other internal configurations seen in the BarMar-experiments mainly reflect step-wise collapse of the intrinsic basin that generated rotational fault blocks, the crests of which separated local sediment accumulations. Such structures are common in strike-slip basins (e.g. Dooley & McClay, 1997; Dooley & Schreurs, 2012) and are consistent with the intra-basin depo-centers seen within the Vestbakken Volcanic province and in the Sørvestsnaget Basin as well (Knutsen & Larsen, 1997; Jebsen & Faleide, 1998; **Figure 13**). The crests of the rotating fault blocks are termed PSE-3-structures above, and such eroded fault block crests are defining the footwalls of major faults in the Vestbakken Volcanic Province, providing space for sediment accumulation in the footwalls. The area that was affected by the basin formation in the extensional shear duplex stage seems to have remained the deepest part of the Vestbakken Volcanic Province, whereas the part formed in basin widening by sequential footwall collapse created a shallower sub-platform (*sensu* Gabrielsen, 1986) (**Figure 11**).

The Knølegga Fault Complex occupies a km-wide zone in segment 2. The master fault strand is paralleled by faults with significant normal throws on its hanging wall side and this belongs to the larger Knølegga Fault Complex (EBF; Eastern Boundary Fault; Giannenas, 2018; **Figure 12A**). The EBF zone is a top-west normal fault with maximum throw of nearly 2000 ms (3000 meters). It can be followed along its strike for more than 60 km and seems to die out by horse-tailing at its tip-points. The vicinity of the master faults of the Knølegga Fault Complex locally display isolated elongate positive structures constrained by steeply dipping faults. These structures sometimes display internal reflection patterns that seem exotic in comparison to the surrounding sequences. Some of these structures resemble positive flower structures or push-ups or define narrow anticlines. They are found in both the footwall and hanging wall of the border faults and strike parallel to those and the axes of these structures parallel the master faults. The traces of such structures can be followed over shorter distances than the master faults, and do not occur in the central parts of the Vestbakken Volcanic Province. We suggest that the composite geometry of the Knølegga Fault Complex is due to the development of PSE-2-structures within the realm of a pre-existing normal fault zone.

Due to the right-stepping geometry during dextral shear in segment 2, the southern and northern parts were in the releasing and restraining bend positions, respectively (e.g. Christie-Blick & Biddle, 1985). Hence, the southern part of segment 2 was subject to oblique extension, subsidence and basin formation while the northern part was subject to oblique contraction, shortening and uplift. The

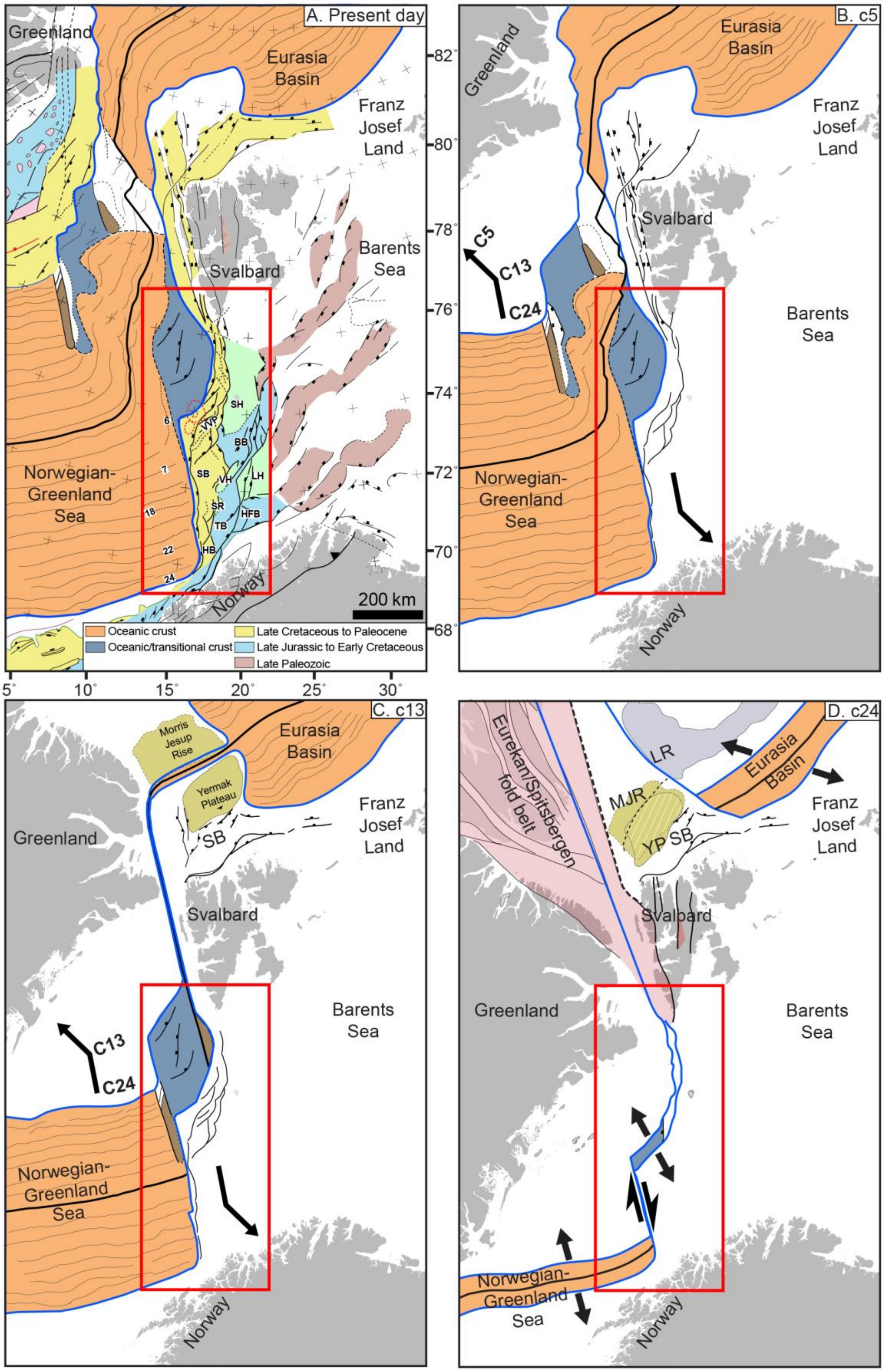


Figure 13; Main stages in opening of the North Atlantic. The figure builds on figure 5 in Faleide et al. (2008) and has been updated and redrawn.

southern segment expanded to the east and northeast by footwall collapse and activation of rotating fault blocks that contributed to a basin floor topography that affected the pattern of sediment accumulation (**Figure 9A,B**).

The positive structural elements that prevail in *segment 3* belong to the PSE-2-structure population. The structures affiliated with segment 3 in the BarMar-experiments are similar to those seen in the reflection seismic sections along parts of the Spitsbergen and the Senja shear margins (Myhre, et al. 1982) and elsewhere (Cloos, 1928; Riedel, 1929; Tchalenko, 1970; Wilcox et al., 1973). In the experiments *én echelon* folds (corresponding to PSE-1-structueres) first became visible, to be succeeded by the development of Riedel- and P-shears (R'-shears were subdued as expected for sand-dominated sequences (Dooley & Schreurs, 2012). Continued shear followed by collapse and interaction between Riedel and P-shears and the subsequent development of Y-shears initiated push-up- and flower-structure with N-S-axes (PSE-2) structures that were expressed as non-cylindrical (double-plunging) anticlines on the surface (e.g. Tchalenko, 1970; Naylor et al., 1986). Structures similar to the PSE-2-structures that were initiated in the present experiments are common in scaled experiments with mechanically stratified sequences where viscous basal strata are covered by sand (e.g. Richard et al., 1991; Dauteuil & Mart, 1998).

Structures of phase 2 (extension)

It is expected that (regional) basin and (local) fault block subsidence became accelerated during phase 2 (extension), and more so in the orthogonal extension experiments (BarMar 6) than in the experiments with oblique extension (BarMar 8). However, due to stabilization of basins by infilling of sand, this was not documented in the final photographs. The widening occurred mainly by fault-controlled collapse of the footwalls, and dominantly along the master faults that correspond to the Knølegga Fault Complex, but also new intra-basin cross-faults that were initiated in the shear stage (see above) became reactivated, contributing to the complexity of the basin topography. It is not likely that a stage was reached where all (pull-apart) basin units along the margin became fully linked, although sedimentary communication along the margin may have become established.

During the oblique extension stage segment 1 of experiments BarMar7-9 the basin subsidence was focused in the minor pull-apart basins, which soon became linked along the regional N-S-striking basin axis. Remains of several such basin centers, of which the Sørvestsnaget Basin (Knutsen & Larsen, 1997; Kristiansen et al., 2017) is the largest, are preserved and found in seismic data (**Figure 1B**). During the experiments a continuous basin system was developed in the hanging wall side of the master fault. It is, however, not likely that linking of shear basins occurred prior to the opening stage along the Barents Shear Margin.

Structures of phase 3 (contraction)

The contraction phase (phase 3) reactivated both normal and shear faults in the master fault zone also causing folding in the hanging wall. Simultaneously rotation of (intra-basinal) fault blocks and steepening of pre-existing faults occurred. New fold populations (PSE-5-folds) with axial traces parallel to the basin axis and the master faults characterized the inversion stage. Remnants of such folds are locally preserved in the thickest sedimentary sequences affiliated with the Senja Shear Margin.

Fold systems with fold axes paralleling the basin margins as seen in the experiments are also common in the Vestbakken Volcanic Province. Although shortening occurred inside individual reactivated fault blocks by large wavelength bulging of the entire sedimentary sequence also trains of folds with larger amplitude and shorter wavelength were developed at this stage (**Figure 12B,C**). Thus, the tectonic inversion was focused along the N-S-striking basin margins but also occurred along some pre-existing NE-SW-striking faults and in the central parts of the basin.

During phase 3 the restraining bend configuration in the northern part of segment 2 was characterized by increasing contraction across strike-slip fault strands that splayed out to the northwest from the central part of segment 2 in an early stage of dextral shear. This deformation was terminated by the end of phase 1 by stacking of oblique contraction faults (PSE-5 and PSE-6-structures), defining an antiformal stack-like structure. This type of deformation falls outside the mapped area, but to the north this type of oblique shortening during the Eocene (phase 1) was accommodated by regional-scale strain partitioning (Leever et al., 2011a,b).

Also, the Vestbakken Volcanic Province is characterized by extensive regional shortening. Onset of this event of inversion/contraction is dated to early Miocene (Jebsen & Faleide, 1998, Giannenas, 2018) and this deformation included two main structural fold styles. The first includes upright to steeply inclined closed to open anticlines that are typically present in the hanging wall of master faults. These folds typically have wavelengths in the order of 2.5 to 4.5 kilometers, and amplitudes of several hundred meters. Most commonly they appear with head-on snakehead-structures and are interpreted as buckle folds, albeit a component of shear may occur in the areas of the most intense deformation. The second style includes gentle to open anticline-syncline pairs with upright or steep to inclined axial planes with wavelengths in the order of 5 to 7 kilometers and amplitudes of several tens of meters to several hundred meters. We associate those with the PSE-4-type structures as defined in the BarMar-experiments. These folds are situated in positions where sedimentary sequences have been pushed against buttresses provided by master faults along the basin margins. The PSE-6 folds developed as fold trains in the interior basins, where buttressing against larger fault walls was uncommon. Also, this pattern fits well with the development and geometry seen in the BarMar-experiments, where folding started in the central parts of the closing basins before folding of the marginal parts of the basin. In the closing stage the folding and inversion of master faults remained focused along the basin margins.

The experiments clearly demonstrated that contraction by buckle folding was the main shortening mechanism of the margin-parallel basin system generated in phase 2 (orthogonal or oblique extension) in all segments. In the Vestbakken Volcanic Province segments of the Knølegga Fault Complex, the EBF and the major intra-basinal faults contain clear evidence for tectonic inversion, whereas this is less pronounced in others. The hanging wall of the EBF is partly affected by fish-hook-type inversion anticlines (Ramsey & Huber, 1987; Griera et al., 2018) (**Figure 2D,E**), or isolated hanging wall anticlines or pairs or trains of synclines and anticlines (e.g.; Roberts, 1989; Coward et al., 1991; Cartwright, 1989; Mitra, 1993; Uliana et al., 1995; Beauchamp et al. 1996; Gabrielsen et al. 1997; Henk & Nemcok 2008), the fold style and associated faults probably being influenced by the orientation and steepness of the pre-inversion fault (Williams et al., 1989; Cooper et al., 1989; Cooper & Warren, 2010). Some structures of this type can still be followed for many kilometers having consistent geometry and attitude. These structures have not been much modified by reactivation and are invariably found in the proximal parts footwalls of master faults, suggesting that these are inversion structures. They correlate to PSE-type 5-structures in the experiments that developed in areas of focused contraction along pre-existing fault scarps during Oligocene inversion.

Trains of folds with smaller amplitudes and higher frequency are sometimes found in fault blocks in the central part of the Vestbakken Volcanic Province (**Figure 12A**). Although these structures are not dateable by seismic stratigraphical methods (on-lap configurations etc.) we regard these fold strains to be correlatable with the tight folds generated in the inversion stage in the experiments (PSE-6-structures) and that they are contemporaneous with the PSE-5-structures.

Segment 1 in the experiments, that corresponds to the Senja Shear Margin , displays a structural pattern that is a hybrid between segments 1 and 2: It contains incipient structural elements that were developed in full in segments 2 and 3, segment 2 being dominated by releasing and restraining bend configurations and segment 3 dominated by neutral shear. Due to internal configurations, the three segments were affected to secondary (oblique) opening and contraction in various fashions. Understanding these differences was much promoted by the comparison of seismic and model data.

Some considerations about multiphase deformation in shear margins

The Barents Shear Margin is a challenging target for structural analysis both because it represents a geometrically complex structural system with a multistage history, but also because high-quality (3D) reflection seismic data are limited and many structures and sedimentary systems generated in the earlier tectono-thermal stages have been overprinted and obliterated by younger events. This makes analogue experiments very useful in the analysis, since they offer a template for what kind of structural elements can be expected. By constraining the experimental model according to the outline of the margin geometry and imposing a dynamic stress model in harmony according to the state-of-the-art knowledge about the regional tectono-sedimentological development, we were able to interpret the observations done in reflection seismic data in a new light.

Continental margins are commonly segmented containing primary or secondary transform elements, and pure strike-slip transforms are relatively rare (e.g. Nemcok et al. 2016). Such margins, however, invariably become affected by extension following break-up and sometimes contraction due to ridge-push or far-field stress perhaps related to plate reorganization. The complexity of shear margins has ignited several conceptual discussions. One such discussion concerns the presence of zones of weakness prior to break-up (e.g. Sibuet & Mascle 1978; Taylor et al, 2009; Gibson et al. 2013; Basile 2015). In the case of the Barents Shear Margin the de Geer zone provides such a pre-existing zone of weakness, and this premise was acknowledged when the scaled model was established. The relevance of our model is therefore constrained to cases where a crustal-scale zone of weakness existed before break-up. Furthermore, in cases with pre-existing zones of weakness, our model demonstrates that the incipient architecture of the margin is important indeed and the detailed geometry and width of the pre-existing week zone must be mapped and included in the model.

Summary and conclusions

Our observations confirmed that the main segments of the Barents Shear Margin, albeit undergoing the same regional stress regime, display contrasting structural configurations. The deformation in segment 2 in the BarMar-experiments, was determined by releasing and restraining bends in the southern and northern parts, respectively. Thus, the southern part, corresponding to the Vestbakken Volcanic Province, was dominated by the development of a regional-scale extensional shear duplex as defined by Woodcock & Fischer (1983) and Twiss & Moores (2007). By continued shear the basin developed into a full-fledged pull-apart basin or rhomb graben (Crowell, 1974; Aydin & Nur, 1982) in which rotating fault blocks were trapped. The pull-apart-basin became the nucleus for greater basin systems to develop in the following phase of extension also providing the space for folds to develop in the contractional phase.

We conclude that fault- and fold systems found in the realm of the Vestbakken Volcanic Province are in accordance with a three-stage development that includes dextral shear followed by oblique extension and contraction (315/135^0) along a shear margin with composite geometry. Folds with NE-SW-trending fold axes are dominant in wider area of the Vestbakken Volcanic Province and are dominated by folds in the hanging walls of (older) normal faults, sometimes characterized by narrow, snake-head- or harpoon-type structures that are typical for tectonic inversion (Cooper et al., 1989; Coward, 1994; Allmendinger, 1998; Yameda & McClay, 2004; Pace & Calamitra, 2014).

Comparing seismic mapping and analogue experiments it is evident that a main challenge in analyzing the structural pattern in shear margins of complex geometry and multiple reactivation is the low potential for preservation of structures that were generated in the earliest stages of the development.

Author contribution

R.H.Gabrielsen: Contributions to outline, design and performance of experiments. First writing and revisions of manuscript. First drafts of figures.

P.A.Giannenas: Seismic interpretation in the Vestbakken Volcanic Province. Identification and description of fold families.

Suggestion:

D.Sokoutis: Main responsibility for set-up, performance and handling of experiments. Revisions of manuscript.

E.Willigshofer: Performance and handling of experiments. Revisions of manuscript. Design and revisions of figure material.

M. Hassaan: Background seismic interpretation. Discussions and revisions of manuscript. Design and revisions of figure material.

J.I.Faleide: Regional interpretations and design of experiments. Participation in performance and interpretations of experiments. Revisions of manuscript, design and revisions of figure material.

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