



- The higher relative concentration of K<sup>+</sup> to Na<sup>+</sup> in saline
- 2 water improves soil hydraulic conductivity, salt leaching
- **efficiency and structural stability**
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#### Abstract

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19 Soil salinity and sodicity caused by saline water irrigation are widely observed 20 globally. Clay dispersion and swelling are influenced by sodium (Na<sup>+</sup>) concentration 21 and electrical conductivity (EC) of soil solution. Specifically, soil potassium (K<sup>+</sup>) also 22 significantly affects soil structural stability, but which concern was rarely addressed in 23 previous studies or irrigation practices. A soil column experiment was carried out to 24 examine the effects of saline water with different relative concentrations of K<sup>+</sup> to Na<sup>+</sup>, 25 including K<sup>+</sup>/Na<sup>+</sup> of 0:1 (K0Na1), 1:1 (K1Na1), 1:0 (K1Na0) at a constant EC (4 dS m<sup>-</sup> 26 1), and deionized water as the control (CK), on soil physicochemical properties. The 27 results indicated that at the constant EC of 4 dS m<sup>-1</sup>, the infiltration rate and water 28 content were significantly (P < 0.05) affected by K<sup>+</sup>/Na<sup>+</sup> values, K0Na1, K1Na1 and 29 K1Na0 significantly (P < 0.05) reduced saturated hydraulic conductivity by 43.62%, 30 29.04% and 18.06% respectively compared with CK. The volumetric water content was 31 significantly (P < 0.05) higher in K0Na1 than CK at both 15 and 30 cm soil depths. 32 K1Na1 and K1Na0 significantly (P < 0.05) reduced the desalination time and required 33 leaching volume. K0Na1 and K1Na1 reached the desalination standard after the fifth 34 and second infiltration, respectively, as K1Na0 did not exceed the bulk electrical 35 conductivity required for desalination prerequisite throughout the whole infiltration 36 cycle at 15 cm soil layer. Furthermore, due to the transformation of macropores into 37 micropores spurred by clay dispersion, soil total porosity in K0Na1 dramatically decreased compared with CK, and K1Na0 even increased the proportion of soil 38





- 39 macropores. The higher relative concentration of K<sup>+</sup> to Na<sup>+</sup> in applied water was more
- 40 conducive to soil aggregates stability, alleviating the risk of macropores reduction
- 41 caused by sodicity.
- 42 **Keywords:** Saline water; Cation composition; Hydraulic properties; Desalination; Pore
- 43 structure.

#### 1 Introduction

Freshwater shortage resulted from elevated demand for water resources as well as 45 46 the irrational exploitation and use after economic and population growth (Zhang and 47 Xie 2019; Prajapati et al. 2021), constrains the sustainability of agricultural production 48 (Aparicio et al., 2019). Alternative water resources with variable water quality (such as 49 saline water) are being considered for agricultural irrigation in several desert and saline 50 areas (Singh et al. 2021; Liu et al. 2022a). Utilizing saline water could partly alleviate 51 the undersupply of freshwater for agricultural production (Yang et al., 2020). However, 52 the other side of the coin is that saline water irrigation could result in soil salinization 53 and/or sodicity. This disaster is related directly to soil pore size distribution, and in turn 54 to the dispersion and swelling of the clay fraction (Bouksila et al. 2013; Hack-ten 55 Broeke et al. 2016; Zhang et al. 2018). Therefore, in order to optimize saline water 56 utilization, the effects of saline water quality on the soil hydraulic properties and pore 57 structure characteristics should be paid more attention (Scudiero et al., 2017). 58 Saline water irrigation can increase the monovalent ions concentration in soil





59 solution and affect soil structure (Qadir et al. 2007; Qadir et al. 2021). Excess sodium 60 (Na<sup>+</sup>) from irrigation saline water is adsorbed onto the clay exchange surface in saltaffected soils where sodium compounds predominate contributing to the disintegration 61 62 of soil structure (Marchuk and Rengasamy 2011; Belkheiri and Mulas 2013; Awedat et 63 al. 2021). As percolation progresses, the thickness of the diffusion double electron layers raises due to the relatively larger hydrated radius of Na<sup>+</sup>, and the repulsive force 64 between adjacent diffusion double electron layers appears to increase, resulting in the 65 66 dispersion and swelling of soil particles (Alva et al. 1991; Reading et al. 2015). Soil calcium (Ca<sup>2+</sup>) and magnesium (Mg<sup>2+</sup>) can alleviate soil dispersibility by 67 replacing Na<sup>+</sup> in soil colloids, the outer layer of the Ca<sup>2+</sup> and Mg<sup>2+</sup> containing colloidal 68 69 particles do not adsorb water molecules, turning Na<sup>+</sup> qualitative hydrophilic colloid into Ca<sup>2+</sup> and Mg<sup>2+</sup> hydrophobic colloid (Marchuk and Rengasamy 2011; Tsai et al. 2012). 70 71 Colloidal particles get close to each other, promoting soil particles forming water stable 72 aggregates, thus improving soil structural stability (Gharaibeh et al. 2009; McKenna et al. 2019). Therefore, the concentration of Na<sup>+</sup> in relation to Mg<sup>2+</sup> and Ca<sup>2+</sup> (Sodium 73 74 adsorption ratio, SAR) (U.S. Salinity Laboratory Staff 1954) is considered a crucial 75 criterion in soil structural stability and hydraulic conductivity (Rengasamy and Marchuk 2011). Although SAR can be used to predict soil clay dispersion effect caused 76 77 by cations, the controlling mechanism of dispersion in SAR is presumed to be 78 exchangeable Na<sup>+</sup>. However, Na<sup>+</sup> does not alone cause soil dispersion since the 79 chemical component of clay structure integrity is mainly a function of ionic valence





80 and hydration radius (Marchuk et al., 2014). Potassium (K+) has been overlooked 81 because salt-affected soils typically contain low amounts of K<sup>+</sup>. However, Li et al. 82 (2022) reported that under the continuous recycling use of underground saline water, water-soluble and exchangeable K<sup>+</sup> is higher than Ca<sup>2+</sup> and Mg<sup>2+</sup> in the Hetao irrigation 83 84 district—one of the large irrigation districts in China. It is anticipated that the long-term 85 use of irrigation water with high K<sup>+</sup> concentrations may therefore create substantial challenges in preserving good soil structure and adequate infiltration rates (Sposito et 86 al., 2016). K<sup>+</sup> is not as effective as Na<sup>+</sup> in generating soil particle dispersion and 87 88 swelling problems, yet Marchuk and Marchuk (2018) pointed out that K<sup>+</sup> could 89 substitute Na<sup>+</sup> on exchange sites to encourage Na<sup>+</sup> leaching and increase water 90 conductivity to some extent. A lower concentration of K<sup>+</sup> may have positive effects on 91 soil permeability due to the substitution of exchangeable Na+ by K+ with lower 92 dispersive potential, increasing aggregates stability and soil pore connectivity (Buelow 93 et al., 2015). 94 Thus, we hypothesized that the amount of K<sup>+</sup> relative to Na<sup>+</sup> would certainly have 95 an effect on soil structural stability, and these relationships could be well evaluated by 96 a column experiment under controlled conditions. The specific objectives of this study 97 were to (1) ascertain the effect of irrigation saline water with different relative concentrations of K<sup>+</sup> to Na<sup>+</sup> (K<sup>+</sup>/Na<sup>+</sup>) on transport and distribution of water and salt; (2) 98 99 determine the effect on soil pore structural characteristics; (3) predict these effects using 100 a newly proposed index (CROSS) rather than SAR.





## 2 Materials and methods

## 2.1 Soil sampling location and properties

The study soil was collected from a layer of 0-40 cm field in Yangling (108°04′E, 34°20′N), Shaanxi Province, China. After air-dried, the soil was grounded to pass through a 2-mm seize. Soil physical and chemical properties are listed in Table 1. Soil particle size distribution was measured by the Laser Mastersizer 2000 (Malvern Instruments, Malvern, UK), and according to the USDA classification system, soil texture is classified as silty clay loam. Soil bulk density calculated by soil core method was 1.35 g cm<sup>-3</sup>. The soil had a low salt concentration with EC<sub>e</sub> (electrical conductivity of saturated extract) of 0.72 dS m<sup>-1</sup> and pH of 7.66, respectively. EC<sub>e</sub> and pH were measured by conductivity meter (DDS-307, China) and pH meter (PHS-3C, China), respectively. Flame photometry (6400A, China) was used to measure soluble Na<sup>+</sup> and K<sup>+</sup>, CO<sub>3</sub><sup>2-</sup> and HCO<sub>3</sub><sup>-</sup> concentrations were tested by the neutral titration method, Cl<sup>-</sup> was analyzed by the silver nitrate titration method, and SO<sub>4</sub><sup>2-</sup> was determined by barium sulfate turbidimetric method, Mg<sup>2+</sup> and Ca<sup>2+</sup> were specified using ethylene diamine tetraacetic acid (EDTA) titrimetric method (Bao 2005).





## 121 Table 1 The physicochemical properties of study soil.

| Property  | Value           |
|---|-----------------|
| Particle size distribution (%)                    |                 |
| Sand (> 0.05 mm)                                  | 8.10            |
| Silt (0.05-0.002 mm)                              | 60.62           |
| Clay (<0.002 mm)                                  | 31.28           |
| Texture   | Silty clay loam |
| $EC_e (dS m^{-1})$                                | 0.72            |
| pН  | 7.66            |
| Ion concentration (mmol L <sup>-1</sup> )         |                 |
| CO <sub>3</sub> <sup>2</sup> -+HCO <sub>3</sub> - | 0.60            |
| Cl <sup>-</sup>                                   | 0.23            |
| $SO_4^{2-}$                                       | 2.18            |
| $\mathrm{Mg}^{2+}$                                | 0.32            |
| $Ca^{2+}$   | 0.54            |
| $Na^+$  | 0.10            |
| K <sup>+</sup>                                    | < 0.01          |

Note: EC<sub>e</sub> represents electrical conductivity of soil saturated extract.

#### **2.2** Experiment design

Soil columns were prepared using transparent polyvinyl chloride cylinders, with an internal diameter of 20 cm and a height of 50 cm (Fig. 1). Round and small holes (6 mm diameter) were equally arranged at the bottom for drainage. A 5 cm depth quartz sand was laid at the bottom of the soil column as a filter layer before packing to prevent small soil particles from being washed away. After that, air-dried soil was packed at 40 cm height with a bulk density of 1.35 g cm<sup>-3</sup> (referring to the original level of the soil). The sieved dry soil was poured into each soil column in the 5-cm sections for uniform compaction, and the layer's surface was roughened to ensure a tight connection to the next layer. The soil column was then allowed to stand in the laboratory for 24 hours





before the initiation of the experiments described herein. The constant water head (2 cm, using a Mariotte bottle) infiltration experiment was conducted with three replications for each treatment.

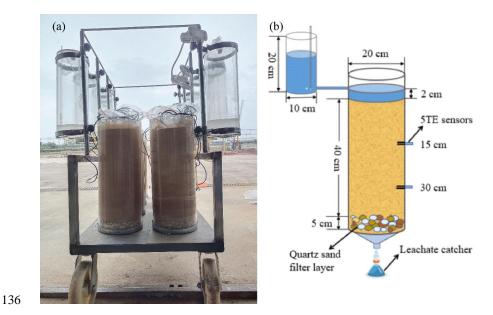


Fig. 1. Illustration of the experiment apparatus (a) and schematic diagram (b).

Three infiltration solutions were prepared with different ratios of  $K^+/Na^+$  (0:1 (K0Na1), 1:1 (K1Na1), 1:0 (K1Na0) at constant EC of 4 dS m<sup>-1</sup> and deionized water as the control (CK) (Table 2). The cation ratio of soil structural stability (CROSS) (Rengasamy and Marchuk 2011) was an indicator of soil structural behavior as influenced by both  $Na^+$  and  $K^+$ , and it was calculated accordingly (Smith et al., 2015):

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$$CROSS = \frac{Na^{+} + 0.335K^{+}}{\left[\left(Ca^{2^{+}} + 0.0758Mg^{2^{+}}\right)/2\right]^{0.5}}$$
 (1)

where different chemical element symbols denote charge concentrations (mmol<sub>c</sub> L<sup>-1</sup>).

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Table 2 Saline water settings with different K<sup>+</sup>/Na<sup>+</sup> at a constant EC.

| Treatment | Adding salt/<br>(mmol L <sup>-1</sup> ) |          |                   | K+/Na+ | Setting<br>EC | Measured<br>EC | CROSS  |
|-----------|---|----------|-------------------|--------|---------------|----------------|--|
|           | KCl                                     | NaCl     | CaCl <sub>2</sub> | -      | $(dS m^{-1})$ | $(dS m^{-1})$  | $(\text{mmol}_{\text{c}} \text{ L}^{\text{-1}})^{0.5}$ |
| K0Na1     | 0                                       | 34       | 3                 | 0:1    | 4.00          | 4.25           | 27.76  |
| K1Na1     | 17                                      | 17       | 3                 | 1:1    | 4.00          | 4.33           | 17.49  |
| K1Na0     | 34                                      | 0        | 3                 | 1:0    | 4.00          | 4.40           | 7.22   |
| CK        |   | Deionize | d water           | /      | 0.00          | 0.02           | /  |

Note: K0Na1, K1Na1 and K1Na0 indicate the saline water at EC of 4 dS m<sup>-1</sup> with

K<sup>+</sup>/Na<sup>+</sup> of 0:1, 1:1 and 1:0, respectively; CK, deionized water; CROSS represents cation

ratio of soil structural stability.

The experiment was implemented in the form of alternate leaching, the prolonged leaching process of soil substrates proved more useful for illuminating the function of electrolyte effect and cation exchange (Shaygan et al., 2017). The next infiltration was performed two days after the drainage of the previous infiltration was completed. Soil layers were regarded as reaching desalination prerequisite when the soil salt content came to less than 0.3%, which meant that bulk electrical conductivity was less than 1.5 dS m<sup>-1</sup> (transformation from salt content to bulk electrical conductivity) (Yin et al., 2022). Water application was stopped when the bulk electrical conductivity of all treatments at 15 cm depth reached the prerequisite for desalination. This experiment was planned to fill all the pores in the soil column throughout the infiltration cycle, therefore the water applied at the first infiltration was described by the pore volume equation (Xu and Huang 2010):

$$V_{p} = V_{s} \cdot TP \tag{2}$$





$$TP = \frac{ds - BD}{ds} \tag{3}$$

where  $V_p$  is the pore volume (cm<sup>3</sup>),  $V_s$  is the volume of filled soil (cm<sup>3</sup>), TP is the soil total porosity (%), ds is the soil particle density (2.65 g cm<sup>-3</sup>) (Xu and Huang 2010), BD is the bulk density (g cm<sup>-3</sup>). According to Eq. (2) and Eq. (3), around 6 L of water was required in the first infiltration. Required water volume for each subsequent leaching was determined by the volume of leachate at the first infiltration, 0.5 L each

#### 2.3 Measurements

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time.

During the whole experiment period, soil volumetric water content and bulk electrical conductivity were real-time monitored at 15 and 30 cm soil depths from the soil surface by capacitance sensors (ECH2O 5TE, METER Group, USA) (Fig. 1). The leachate was collected in the leachate catcher below the soil column. Cumulative leachate volume was monitored over time to determine the saturated hydraulic conductivity ( $K_{\text{sat}}$ , cm min<sup>-1</sup>) of each treatment by using a derivation of Darcy's approach (Sahin et al., 2011):

$$K_{sat} = \frac{V_l \cdot H}{A \cdot t \cdot (H + h)} \tag{4}$$

where  $V_1$  is the leachate volume (cm<sup>3</sup>), H is the length of filled soil (cm), A is the surface area of soil column (cm<sup>2</sup>), t is the leaching time of measurement (min), h is the height of constant water head (cm).

The salt accumulated in the soil column was determined by subtracting the salt in





the leachate from the applied water, the salination rate (Rs, %) indicated the ratio of salt accumulated in the soil column at every time of infiltration to the salt content at the first applied water. Leaching efficiency (Le, g L<sup>-1</sup>) referred to the amount of desalination per unit of water volume in the desalination process. Rs and Le were calculated as follows:  $Rs = m_s / m_w \tag{5}$ 

 $Le = (m_s - m_1) / w \tag{6}$ 

Where  $m_s$  is the salt content accumulated in soil column at every time of infiltration (g),  $m_w$  is the salt content in the total water used for the first infiltration (g),  $m_1$  is the mass of salts after the first infiltration (g), w is the total water volume used for leaching (L). Soil samples were collected from each soil column at 5-cm intervals with the 0-40 cm soil layer three days after the final infiltration. Soil BD was calculated using the soil core method, and TP was calculated by Eq. (3) based on BD. Soil water characteristics curve was measured with the high velocity centrifugal method (CR21 Hitachi, Japan), and calibrated by RETC software (PC Progress Inc., Prague, Czech Republic). Currently, several defining sizes of macropores are proposed, rather than a precise definition and pore size range (Cameira et al. 2003; Kim et al. 2010; Hu et al. 2018; Budhathoki et al. 2022; Aldaz-Lusarreta et al. 2022). In this study, macropores were defined as the pores with diameters larger than 1 mm, whereas micropores were defined as smaller than 1 mm (Luxmoore 1981; Wilson and Luxmoore 1988). Based on the capillary pressure data, the relationship between pore diameter (d, mm) and water suction (S, Pa) was described according to the capillary bundle model (Jury et al., 1991):





204 (7) 205 2.4 Statistical analysis Statistical analysis among all treatments with different K<sup>+</sup>/Na<sup>+</sup> was performed in 206 207 SPSS 22.0 software, using one-way analysis of variance (ANOVA) based on the least significant difference (LSD) test at 95% significance level (P < 0.05). All figures were 208 created through Origin 2022b. 209 210 3 Results 211 3.1 Soil saturated hydraulic conductivity (Ksat) 212 The K0Na1, K1Na1 and K1Na0 significantly (P < 0.05) reduced  $K_{\text{sat}}$  by 43.62%, 213 29.04% and 18.06% compared with CK, respectively (Fig. 2). Additionally,  $K_{\text{sat}}$  was 214 negatively correlated with CROSS of saline water, increasing the CROSS of the applied 215 saline water generally reduced  $K_{\text{sat}}$ . 216 217



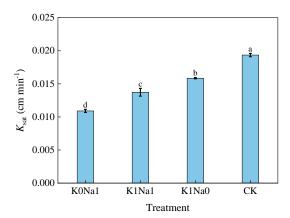


Fig. 2. Saturated hydraulic conductivity ( $K_{sat}$ ) under different treatments. K0Na1, K1Na1 and K1Na0 indicate the saline water at EC of 4 dS m<sup>-1</sup> with K<sup>+</sup>/Na<sup>+</sup> of 0:1, 1:1 and 1:0, respectively; CK, deionized water; Different letters after means of  $K_{sat}$  indicate statistical differences (P < 0.05) among treatments based on LSD. Bars indicate standard deviations of means.

## 3.2 Soil water content

Water content increased immediately after each infiltration for all treatments, and then gradually declined to a constant level (Fig. 3). And water content at deeper soil depths was greater than at shallow soil depths at the same time during the whole infiltration period. The water content ranged from 0.39-0.41 and 0.40-0.42 cm<sup>3</sup> cm<sup>-3</sup> at 15 and 30 cm soil depths, respectively. K0Na1 gained the highest water content at both 15 and 30 cm soil depths. K1Na1 and K1Na0 were greater than CK at 15 cm soil depth and lower than CK at 30 cm soil depth, and the water content of K1Na1 was higher than K1Na0 at both 15 and 30 cm soil layers.





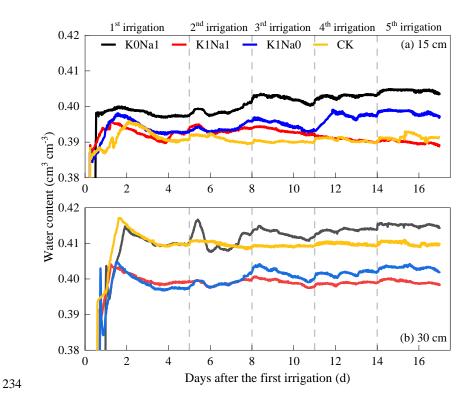


Fig. 3. Variation of water content over time under different treatments at 15 (a) and 30 cm (b) soil depths during the five times of infiltration.

# 3.3 Soil salination rate (Rs) and leaching efficiency (Le)

The *Rs* and *Le* under CK were not shown in Fig. 4, because deionized water was used as the control and there was almost no salt contained in the study soil, CK was considered negligible for salt accumulation and leaching. *Rs* peaked at the first infiltration, and approximately 70%-80% of the salt in the saline water was retained in the soil column, after which the subsequent leaching had lower *Rs* values (Fig. 4). The lower the ratio of K<sup>+</sup>/Na<sup>+</sup>, the larger soil *Rs*. Among the three saline water treatments,



## 244 K1Na0 had the lowest Rs and highest Le at five infiltrations.

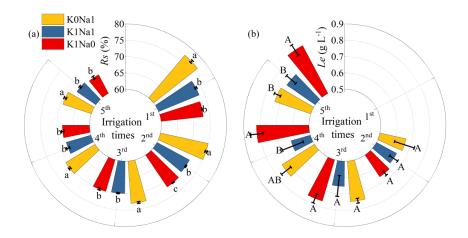


Fig. 4. Salination rate (Rs) (a) and leaching efficiency (Le) (b) at five infiltrations under all saline water treatments. K0Na1, K1Na1 and K1Na0 indicate the saline water at EC of 4 dS m<sup>-1</sup> with K<sup>+</sup>/Na<sup>+</sup> of 0:1, 1:1 and 1:0, respectively; Different lowercase letters followed means of Rs indicate statistical differences (P < 0.05) among treatments based on LSD, and different capital letters followed means of Le indicate statistical differences (P < 0.05) among treatments based on LSD. Bars indicate standard deviations of means.

## 3.4 Soil bulk electrical conductivity

Bulk electrical conductivity of K0Na1, K1Na1 and K1Na0 ranged from 1.0 to 2.0 dS m<sup>-1</sup> at 15 cm, 1.5 to 2.5 dS m<sup>-1</sup> at 30 cm soil depth (Fig. 5). After the first infiltration, bulk electrical conductivity in 15 cm soil layer reached its apes, and then exhibited a general downward trend in the following infiltrations. However, more salts were





leached to deeper layers, where salt began to accumulate instead of desalination, and bulk electrical conductivity at 30 cm soil depth gradually increased following the infiltration events. At both 15 and 30 cm soil layers, the bulk electrical conductivity of K0Na1 was considerably greater than K1Na1, and K1Na1 was quite higher than K1Na0.

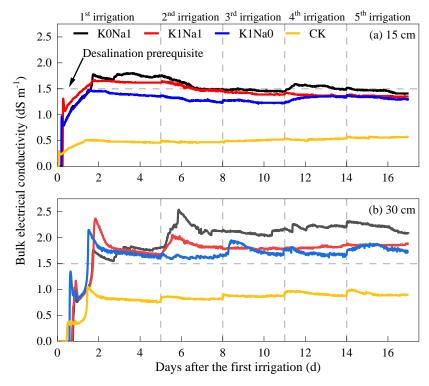


Fig. 5. Variation of bulk electrical conductivity over time under treatments with different  $K^+/Na^+$  at constant EC at 15 (a) and 30 cm (b) soil depths in the period of five times of infiltration. K0Na1, K1Na1 and K1Na0 indicate the saline water at EC of 4 dS  $m^{-1}$  with  $K^+/Na^+$  of 0:1, 1:1 and 1:0, respectively; CK, deionized water.

At 15 cm soil depth, K0Na1 reached the soil desalination prerequisite after the fifth infiltration, while K1Na1 reached the desalination prerequisite after the second infiltration, and K1Na0 did not exceed desalination prerequisite during the whole





271 time and required leaching volume to reach the standard of desalination. K0Na1, 272 K1Na1 and K1Na0 did not meet the desalination prerequisite at 30 cm soil depth, and 273 the increased volume of infiltration water also increased the bulk electrical conductivity. 274 3.5 Soil bulk density (BD) and total porosity (TP) Soil BD varied between 1.30 and 1.40 g cm<sup>-3</sup> for all treatments, and BD was below 275 1.35 g cm<sup>-3</sup> at 0-10 and 35-40 cm soil layers, however, over 1.35 g cm<sup>-3</sup> at 10-35 cm 276 277 soil depth (Fig. 6). K0Na1 significantly (P < 0.05) enhanced soil BD throughout the soil 278 column profile compared with CK. TP first diminished with soil depth to reach a 279 minimum at about 30-35 cm, and then slightly increased at 35-40 cm. The TP of K1Na1 280 and K1Na0 slightly improved after five times of infiltration, and only K0Na1 showed 281 a decline compared with CK. Overall, over the whole infiltration period, K1Na0 was 282 most conducive to the formation of soil pore structure and increasing the total pore

infiltration period. Among all saline water treatments, K1Na0 saved the desalination

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increasing TP.

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volume. The saline water with lower CROSS was beneficial for reducing soil BD and





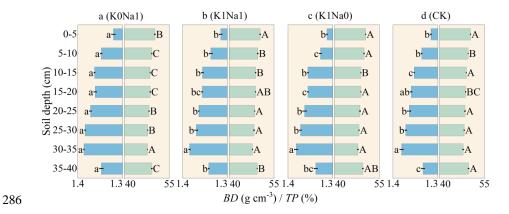


Fig. 6. Soil bulk density (BD) and total porosity (TP) throughout the soil column profile under different treatments. K0Na1, K1Na1 and K1Na0 indicate the saline water at EC of 4 dS m<sup>-1</sup> with K<sup>+</sup>/Na<sup>+</sup> of 0:1, 1:1 and 1:0, respectively; CK, deionized water; The blue horizon columns represent BD, while the green horizon columns represent TP; Different lowercase letters followed means of BD indicate statistical differences (P < 0.05) among treatments based on LSD, and different capital letters followed means of TP indicate statistical differences (P < 0.05) among treatments based on LSD. Bars indicate standard deviations of means.

## 3.6 Proportion of micropores and proportion of macropores

Micropores were the dominant pores for all treatments, the proportion of micropores accounting for more than 40% of the total soil volume, however, the proportion of macropores made up no more than 8% (Fig. 7). 0-5 cm soil layer had the lowest proportion of macropores and retained the largest proportion of micropores compared with other depths. K0Na1 had the highest proportion of micropores and the





lowest proportion of macropores. K1Na0 had a greater proportion of macropores in the soil column compared with CK.

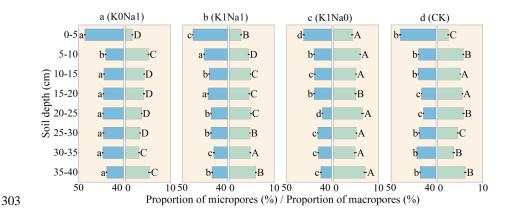


Fig. 7. Proportion of micropores and proportion of macropores in total soil volume throughout the soil column profile under different treatments. K0Na1, K1Na1 and K1Na0 indicate the saline water at EC of 4 dS  $\rm m^{-1}$  with  $\rm K^{+}/Na^{+}$  of 0:1, 1:1 and 1:0, respectively; CK, deionized water; The blue horizon columns represent proportion of micropores, while the green horizon columns represent proportion of macropores; Different lowercase letters followed means of proportion of micropores indicate statistical differences (P < 0.05) among treatments based on LSD, and differences (P < 0.05) among treatments based on LSD. Bars indicate standard deviations of means.

# 4 Discussion

#### 4.1 Effects of saline water on soil water movement and redistribution

As a crucial soil hydraulic characteristic,  $K_{\text{sat}}$  represents the transportation ability





316 of water and solutes (Braud et al. 2001; Maillard et al. 2011; Albalasmeh et al. 2022). 317 The cation composition and EC of soil solution affect  $K_{\text{sat}}$  by controlling electrostatic 318 repulsive pressure through surface potential and midpoint potential between adjacent 319 particles, and consequently influence water movement (Fares et al. 2000; Liu et al., 320 2022b). Specifically, the K<sup>+</sup>/Na<sup>+</sup> ratio in saline water was related to the swelling and 321 dispersion of soil particles (Yu et al. 2016; Zhu et al. 2019). Dispersed clay particles 322 clogged soil macropores to subsequently restrict water transport (Awedat et al., 2021). 323 The Na<sup>+</sup> has a relatively higher ionicity index than K<sup>+</sup>, as a result, the low K<sup>+</sup>/Na<sup>+</sup> ratio 324 decreased the degree of covalency in clay-cation bonds, which was detrimental to clay 325 particles aggregation (Marchuk and Rengasamy 2011). Therefore, in our study, the high 326 K<sup>+</sup>/Na<sup>+</sup> ratio promoted the flocculation and stabilization of soil clay particles, resulting 327 in an increased infiltration rate. 328 After a certain period of water supply, soil moisture redistributed at different 329 depths of soil column. Soil water moved further down during the phase of water 330 redistribution soon after each irrigation, reducing the water content in the upper soil 331 layers. As the upper soil layers drained, the lower soil layers still had water inflow 332 (Kargas et al., 2021), increasing the water content in the lower soil layers. The results 333 also implicated that the retention of soil water by Na<sup>+</sup> was stronger than that by K<sup>+</sup>, the 334 cause may be that Na+ can increase the thickness of the diffuse-double layers around 335 soil colloids theoretically due to its larger hydrated radius and lower charge than K<sup>+</sup>, 336 and the adjacent double layers overlapped to provide more space between layers, where,





subsequently, more water can be retained (He et al., 2015). Additionally, our study showed that an appropriate concentration of K<sup>+</sup>/Na<sup>+</sup> was even more beneficial than deionized water for water downward transport, which could be because the deionized water (CK) (below 0.2 dS m<sup>-1</sup>) tended to leach soluble minerals and salts, especially Ca<sup>2+</sup>, from the surface soil layers. This would lead to the reduction of its original solid soil structural stability. In the absence of salt and Ca<sup>2+</sup>, the dispersed tiny particles filled the smaller pore spaces in soil, reducing even more channels for water flow and exacerbating water retention in deeper soil layers (Ayers and Westcot 1985). However, a lower concentration of soluble salts could increase colloid flocculation, and thereby, improve soil aeration and water conductivity (Tang and She 2016).

#### 4.2 Effects of saline water on soil salination and desalination process

Numerous factors influence the leaching efficiency of soil salts; for example, increasing EC and reducing SAR definitely improve clay flocculation, which can enhance salt leaching (Ebrahim Yahya et al., 2022). Na<sup>+</sup> is more likely to trigger soil clay dispersion and swelling than K<sup>+</sup>, thus Na<sup>+</sup> generally inhibits water infiltration, which is detrimental to salt leaching (Smiles and Smith 2004). Adding K<sup>+</sup> could promote displacement of the adsorbed Na<sup>+</sup>, and then decrease Na<sup>+</sup> concentration and salt accumulation in soil solute through leaching.

A greater reduction in Na<sup>+</sup> concentration was associated with a higher rate of cation exchange rate, and the slow rate of solute leaching from aggregates reduced the





total leaching efficiency (Shaygan et al., 2017). During the leaching process, water flow preferentially passed through the macropores rather than aggregates. The slow water transportation through aggregates induced the slow removal of solutes from the aggregates, leading to a reduced leaching efficiency. In our study, the alternate leaching was implemented to improve solute leaching. The soil solutes diffused into the aggregates surface during the rest period, improving salt leaching due to the water flow in macropores (Al-Sibai et al., 1997). Increasing K<sup>+</sup>/Na<sup>+</sup> ratio could increase the magnitude of cation exchange due to the substitution of Na<sup>+</sup> on exchange sites by K<sup>+</sup> with lower dispersive potential (Shaygan et al., 2017), the intensive release of cations from the soil further improved salt's leaching efficiency. In addition, the integrity of soil aggregates created by combining clay particles and the other soil components enhanced by K<sup>+</sup> can benefit solute transportation (Marchuk and Rengasamy 2011).

## 4.3 Effects of saline water on soil pore structure characteristics

The upper soil was longer exposed to water due to the long-term continuous irrigation, causing the particles to swell and the surface layer to loosen (Vaezi et al. 2017; Håkansson and Lipiec 2000), and also the decreased BD in the surface layer of soil column. The subsoil BD increased with depth under the impact of water pressure and self-weight due to the declining pore diameter and pore branching closure (Schjønning et al., 2013). And for soil at the bottom, the loss of soil particles from small holes was responsible for the abrupt reduction in BD. The value of CROSS in saline





water could reflect changes in soil *BD* and *TP*, in agreement with the result of Marchuk and Marchuk (2018). The high CROSS implied an increase in the proportion of monovalent exchangeable cations, thickening the double layer at the interface between the clay surface and soil solution. Hence, soil swelling occurred at the expense of water-conducting pores. Additionally, aggregates slaking and subsequent clay dispersion and deposition of clay particles within the pore space contributed to the reduction in *TP* (Marchuk and Marchuk 2018).

Fewer soil macropores plays a crucial role in water and solute transport, accounting for 85% of the total infiltration volume (Wilson and Luxmoore 1988; Weiler and Naef 2003; Kotlar et al. 2020). The lower the K+/Na+ ratio, the more it enhanced soil clay dispersion, resulting in the loosening of clay particles from the aggregates. This, in turn, dispersed clay particles moved with water caused the macropores to become blocked, converting them into micropores (Cameira et al., 2003), thus leading to a decrease in the volume of soil macropores.

## **5 Conclusion**

We explored the effect of K<sup>+</sup>/Na<sup>+</sup> in saline water on soil hydraulic characteristics and structural stability via a soil column experiment. The higher K<sup>+</sup>/Na<sup>+</sup> ratio caused fewer pore blockages due to soil clay particle dispersion than lower K<sup>+</sup>/Na<sup>+</sup>, which increased soil saturated hydraulic conductivity. The presence of K<sup>+</sup> accelerated the sustained Na<sup>+</sup> replacement and leaching, alleviating salt accumulation and enhancing





leaching efficiency. Increasing K<sup>+</sup>/Na<sup>+</sup> positively affected the establishment of soil structure due to the transformation of micropores into macropores, and the everincreasing unobstructed water-conducting channels sped up water and solute transport. The rational use of saline water with adequate K<sup>+</sup> could help mitigate the structural deterioration caused by Na<sup>+</sup>. Appropriate adjustment of saline water K<sup>+</sup>/Na<sup>+</sup> during infiltration could ameliorate soil structural properties. In addition to Ca<sup>2+</sup> and Mg<sup>2+</sup> (primary concerns in earlier studies), the relative concentration of K<sup>+</sup> to Na<sup>+</sup> is an essential indicator for assessing the suitability of saline water quality for irrigation and should be considered when using saline water.

## **Author contributions**

Sihui Yan and Tibin Zhang conceived and designed the experiments. Sihui Yan, Binbin Zhang and Tonggang Zhang led the data processing and statistical analysis, Sihui Yan, Yu Cheng, Chun Wang and Min Luo performed the experiments. Sihui Yan wrote the initial draft. Hao Feng and Kadambot H.M. Siddique contributed to review and editing of the paper.

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