

1        **The higher relative concentration of K<sup>+</sup> to Na<sup>+</sup> in saline**  
2        **water improves soil hydraulic conductivity, salt leaching**  
3        **efficiency and structural stability**

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18 **Abstract**

19 Soil salinity and sodicity caused by saline water irrigation are widely observed  
20 globally. Clay dispersion and swelling are influenced by sodium ( $\text{Na}^+$ ) concentration  
21 and electrical conductivity (EC) of soil solution. Specifically, soil potassium ( $\text{K}^+$ ) also  
22 significantly affects soil structural stability, but which concern was rarely addressed in  
23 previous studies or irrigation practices. A soil column experiment was carried out to  
24 examine the effects of saline water with different relative concentrations of  $\text{K}^+$  to  $\text{Na}^+$   
25 ( $\text{K}^+/\text{Na}^+$ ), including  $\text{K}^+/\text{Na}^+$  of 0:1 (K0Na1), 1:1 (K1Na1), 1:0 (K1Na0) at a constant  
26 EC ( $4 \text{ dS m}^{-1}$ ), and deionized water as the control (CK), on soil physicochemical  
27 properties. The results indicated that at the constant EC of  $4 \text{ dS m}^{-1}$ , the infiltration rate  
28 and water content were significantly ( $P < 0.05$ ) affected by  $\text{K}^+/\text{Na}^+$  values, K0Na1,  
29 K1Na1 and K1Na0 significantly ( $P < 0.05$ ) reduced saturated hydraulic conductivity by  
30 43.62%, 29.04% and 18.06% respectively compared with CK. The volumetric water  
31 content was significantly ( $P < 0.05$ ) higher in K0Na1 than CK at both 15 and 30 cm soil  
32 depths. K1Na1 and K1Na0 significantly ( $P < 0.05$ ) reduced the desalination time and  
33 required leaching volume. K0Na1 and K1Na1 reached the desalination standard after  
34 the fifth and second infiltration, respectively, as K1Na0 did not exceed the bulk  
35 electrical conductivity required for desalination prerequisite throughout the whole  
36 infiltration cycle at 15 cm soil layer. Furthermore, due to the transformation of  
37 macropores into micropores spurred by clay dispersion, soil total porosity in K0Na1  
38 dramatically decreased compared with CK, and K1Na0 even increased the proportion

39 of soil macropores. The higher relative concentration of  $K^+$  to  $Na^+$  in saline water was  
40 more conducive to soil aggregates stability, alleviating the risk of macropores reduction  
41 caused by sodicity.

42 **Keywords:** Saline water; Cation composition; Hydraulic properties; Desalination; Pore  
43 structure.

## 44 **1 Introduction**

45 Freshwater shortage resulted from elevated demand for water resources as well as  
46 the irrational exploitation and use after economic and population growth (Zhang and  
47 Xie 2019; Prajapati et al. 2021), constrains the sustainability of agricultural production  
48 (Aparicio et al., 2019). Alternative water resources with variable water quality (such as  
49 saline water) are being considered for agricultural irrigation in several desert and saline  
50 areas (Singh et al. 2021; Liu et al. 2022a). Utilizing saline water could partly alleviate  
51 the undersupply of freshwater for agricultural production (Yang et al., 2020). However,  
52 the other side of the coin is that saline water irrigation could result in soil salinization  
53 and/or sodicity. Once the soil is salinized and/or alkalized, soil hydraulic properties,  
54 like infiltration rate, saturated hydraulic conductivity and permeability, will change  
55 inevitably (Scudiero et al., 2017). And cations in the soil solution change the soil  
56 structural characteristics through the soil clay particle dispersion and flocculation  
57 (Bouksila et al. 2013; Hack-ten Broeke et al. 2016; Zhang et al. 2018). Therefore, in  
58 order to optimize saline water utilization, the effects of saline water quality on the soil

59 hydraulic properties and pore structure characteristics should be paid more attention.

60 Saline water irrigation can increase the monovalent ions concentration in soil  
61 solution and affect soil structure (Qadir et al. 2007; Qadir et al. 2021). Excess sodium  
62 ( $\text{Na}^+$ ) from saline irrigation water is adsorbed onto the clay surface in salt-affected soils  
63 where sodium compounds predominate contributing to the disintegration of soil  
64 structure (Marchuk and Rengasamy 2011; Belkheiri and Mulas 2013; Awedat et al.  
65 2021). As percolation progresses, the thickness of the diffusion double electron layers  
66 increases due to the relatively larger hydrated radius of  $\text{Na}^+$ , and the repulsive force  
67 between adjacent diffusion double electron layers appears to increase, resulting in the  
68 dispersion and swelling of soil particles (Alva et al. 1991; Reading et al. 2015).

69 Soil calcium ( $\text{Ca}^{2+}$ ) and magnesium ( $\text{Mg}^{2+}$ ) can alleviate soil dispersibility by  
70 replacing  $\text{Na}^+$  in soil colloids, the outer layers of the  $\text{Ca}^{2+}$  and  $\text{Mg}^{2+}$  containing colloidal  
71 particles do not adsorb water molecules, turning  $\text{Na}^+$  qualitative hydrophilic colloid into  
72  $\text{Ca}^{2+}$  and  $\text{Mg}^{2+}$  hydrophobic colloids (Marchuk and Rengasamy 2011; Tsai et al. 2012).  
73 Colloidal particles move closer to each other, promoting soil particles forming water  
74 stable aggregates, thus improving soil structural stability (Gharaibeh et al. 2009;  
75 McKenna et al. 2019). Therefore, the concentration of  $\text{Na}^+$  in relation to  $\text{Mg}^{2+}$  and  $\text{Ca}^{2+}$   
76 (sodium adsorption ratio, SAR) (U.S. Salinity Laboratory Staff 1954) is a crucial  
77 criterion for soil structural stability and hydraulic conductivity (Rengasamy and  
78 Marchuk 2011). Although SAR can be used to predict soil clay dispersion effect caused  
79 by cations, the controlling mechanism of dispersion in SAR is presumed to be

80 exchangeable  $\text{Na}^+$ . However,  $\text{Na}^+$  does not alone cause soil dispersion since the  
81 chemical component of clay structure integrity is mainly a function of ionic valence  
82 and hydration radius (Marchuk et al., 2014). Potassium ( $\text{K}^+$ ) has been overlooked  
83 because salt-affected soils typically contain low amounts of  $\text{K}^+$ . However, Li et al.  
84 (2022) reported that under the continuous recycling use of underground saline water,  
85 water-soluble and exchangeable  $\text{K}^+$  is higher than  $\text{Ca}^{2+}$  and  $\text{Mg}^{2+}$  in the Hetao irrigation  
86 district—one of the large irrigation districts in China. It is anticipated that the long-term  
87 use of irrigation water with high  $\text{K}^+$  concentrations may therefore create substantial  
88 challenges in preserving good soil structure and adequate infiltration rates (Sposito et  
89 al., 2016).  $\text{K}^+$  is not as effective as  $\text{Na}^+$  in generating soil particle dispersion and  
90 swelling problems, yet Marchuk and Marchuk (2018) pointed out that  $\text{K}^+$  could  
91 substitute  $\text{Na}^+$  on exchange sites to encourage  $\text{Na}^+$  leaching and increase water  
92 conductivity to some extent. A lower concentration of  $\text{K}^+$  may have positive effects on  
93 soil permeability due to the substitution of exchangeable  $\text{Na}^+$  by  $\text{K}^+$  with lower  
94 dispersive potential, increasing aggregates stability and soil pore connectivity (Buelow  
95 et al., 2015). Traditional SAR ignored the role of  $\text{K}^+$ , a newly proposed equation, cation  
96 ratio of soil structural stability (CROSS) could integrate the effects of  $\text{Na}^+$  and  $\text{K}^+$  in  
97 soil, which is an important indicator for assessing the quality of saline water  
98 (Rengasamy and Marchuk 2011).

99 Thus, we hypothesized that the amount of  $\text{K}^+$  relative to  $\text{Na}^+$  would certainly have  
100 an effect on soil structural stability, which could be evaluated in a column experiment

101 under controlled conditions. The specific objectives of this study were to (1) ascertain  
102 the effect of irrigation saline water with different relative concentrations of  $K^+$  to  $Na^+$   
103 ( $K^+/Na^+$ ) on transport and distribution of water and salt; (2) determine the effect on soil  
104 pore structural characteristics; (3) predict these effects using a newly proposed index  
105 (CROSS) rather than SAR.

## 106 **2 Materials and methods**

### 107 **2.1 Soil sampling location and properties**

108 The study soil was collected from a layer of 0–40 cm field in Yangling (108°04'E,  
109 34°20'N), Shaanxi Province, China. After air-dried, the soil was grounded to pass  
110 through a 2-mm sieve. Soil's physical and chemical properties are listed in Table 1. Soil  
111 particle size distribution was measured by the Laser Mastersizer 2000 (Malvern  
112 Instruments, Malvern, UK), and according to the international classification system,  
113 soil texture was classified as silty clay. Soil bulk density was calculated using the soil  
114 core method.  $EC_e$  and pH were measured using conductivity meter (DDS-307, China)  
115 and pH meter (PHS-3C, China), respectively. Total soluble salts refer to the total  
116 amount of soluble salts in soil-saturated paste extract. Flame photometry (6400A, China)  
117 was used to measure soluble  $Na^+$  and  $K^+$ , concentrations of  $CO_3^{2-}$  and  $HCO_3^-$  were  
118 tested using the neutral titration method,  $Cl^-$  was analyzed using the silver nitrate  
119 titration method, and  $SO_4^{2-}$  was determined using barium sulfate turbidimetric method,  
120  $Mg^{2+}$  and  $Ca^{2+}$  were specified using ethylene diamine tetraacetic acid (EDTA)

121 titrimetric method (Bao 2005).

122 Table 1 The physicochemical properties of study soil.

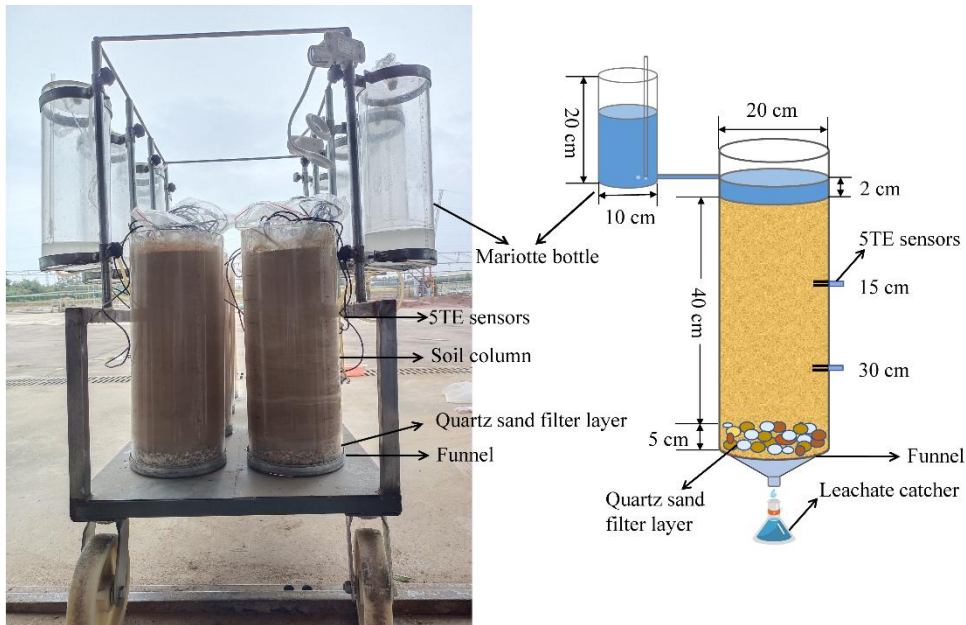
Property	Value
Particle size distribution (%)	
Sand (> 0.05 mm)	8.10
Silt (0.05–0.002 mm)	60.62
Clay (< 0.002 mm)	31.28
Texture	Silty clay
EC <sub>e</sub> (dS m <sup>-1</sup> )	0.72
pH	7.66
Total soluble salts (g Kg <sup>-1</sup> )	0.14
Ion concentration (mmol L <sup>-1</sup> )	
CO <sub>3</sub> <sup>2-</sup> +HCO <sub>3</sub> <sup>-</sup>	0.60
Cl <sup>-</sup>	0.23
SO <sub>4</sub> <sup>2-</sup>	2.18
Mg <sup>2+</sup>	0.32
Ca <sup>2+</sup>	0.54
Na <sup>+</sup>	0.10
K <sup>+</sup>	< 0.01

123 Note: EC<sub>e</sub> is electrical conductivity of soil-saturated extract.

## 124 2.2 Experimental design

125 Soil columns were prepared using transparent polyvinyl chloride cylinders, with  
126 an internal diameter of 20 cm and a height of 50 cm (Fig. 1). Round and small holes (6  
127 mm diameter) were arranged equally at the bottom of each cylinder for drainage. A 5  
128 cm depth quartz sand was laid at the bottom of the soil column as a filter layer before  
129 packing to prevent small soil particles from being washed away. After that, air-dried  
130 soil was packed at 40 cm height with a bulk density of 1.35 g cm<sup>-3</sup> (referring to the  
131 original level of the soil). The sieved dry soil was poured into each soil column in the

132 5-cm sections for uniform compaction, and the layer's surface was roughened to ensure  
 133 a tight connection to the next layer. The soil column was then allowed to stand in the  
 134 laboratory for 24 hours before starting the experiments described herein. The constant  
 135 water head (2 cm, using a Mariotte bottle) infiltration experiment was conducted with  
 136 3 replications for each treatment.



137  
 138 Fig. 1. Illustration of the experiment apparatus (a) and schematic diagram (b).

139 Three infiltration solutions were prepared with different ratios of  $K^+/Na^+$  [(0:1  
 140 (K0Na1), 1:1 (K1Na1), 1:0 (K1Na0)] at constant EC of  $4 \text{ dS m}^{-1}$ , with deionized water  
 141 was used as the control (CK) (Table 2). The cation ratio of soil structural stability  
 142 (CROSS) (Rengasamy and Marchuk 2011) is an indicator of soil structural behavior as  
 143 influenced by both  $Na^+$  and  $K^+$ , and it was calculated as follows (Smith et al., 2015):

144

$$CROSS = \frac{Na^+ + 0.335K^+}{\left[ \left( Ca^{2+} + 0.0758Mg^{2+} \right) / 2 \right]^{0.5}} \quad (1)$$

145 where the chemical element symbols denote charge concentrations ( $\text{mmol}_c \text{ L}^{-1}$ ).



146 Table 2 Saline water settings with different  $K^+/Na^+$  at a constant EC.

Treatment	Added salt/ (mmol L <sup>-1</sup> )			$K^+/Na^+$	Setting	Measured	CROSS (mmol <sub>c</sub> L <sup>-1</sup> ) <sup>0.5</sup>
	KCl	NaCl	CaCl <sub>2</sub>		EC (dS m <sup>-1</sup> )	EC (dS m <sup>-1</sup> )	
K0Na1	0	34	3	0:1	4.00	4.25	27.76
K1Na1	17	17	3	1:1	4.00	4.33	17.49
K1Na0	34	0	3	1:0	4.00	4.40	7.22
CK	Deionized water			/	0.00	0.02	/

147 Note: K0Na1, K1Na1 and K1Na0 indicate the saline water at EC of 4 dS m<sup>-1</sup> with  
 148  $K^+/Na^+$  of 0:1, 1:1 and 1:0, respectively; CK, deionized water; CROSS represents cation  
 149 ratio of soil structural stability.

150 The experiment implemented alternate leaching, as the prolonged leaching process  
 151 of soil substrates is more helpful in illuminating the function of electrolyte effect and  
 152 cation exchange (Shaygan et al., 2017). The next infiltration was performed two days  
 153 after the drainage of the previous infiltration was completed. Soil layers were regarded  
 154 as reaching desalination prerequisite when the soil salt content came to less than 0.3%,  
 155 which meant that bulk electrical conductivity was less than 1.5 dS m<sup>-1</sup> (transformation  
 156 from salt content to bulk electrical conductivity) (Yin et al., 2022). Water application  
 157 was stopped when the bulk electrical conductivity of all treatments at 15 cm depth  
 158 reached the prerequisite for desalination. This experiment was planned to fill all the  
 159 pores in the soil column throughout the infiltration cycle, therefore the water applied at  
 160 the first infiltration was described by the pore volume equation (Xu and Huang 2010):

161 
$$V_p = V_s \cdot TP \quad (2)$$

162 
$$TP = \frac{ds - BD}{ds} \quad (3)$$

163 where  $V_p$  is the pore volume (cm<sup>3</sup>),  $V_s$  is the volume of filled soil (cm<sup>3</sup>),  $TP$  is the soil

164 total porosity (%),  $d_s$  is the soil particle density ( $2.65 \text{ g cm}^{-3}$ ) (Xu and Huang 2010),  
165  $BD$  is the bulk density ( $\text{g cm}^{-3}$ ). According to Eq. (2) and Eq. (3), around 6 L of water  
166 was required in the first infiltration. Required water volume for each subsequent  
167 leaching was determined by the volume of leachate at the first infiltration, 0.5 L each  
168 time.

### 169 2.3 Soil properties measurements

170 During the whole experimental period, soil volumetric water content and bulk  
171 electrical conductivity were real-time monitored at 15 and 30 cm soil depths from the  
172 soil surface by capacitance sensors (ECH2O 5TE, METER Group, USA) (Fig. 1).  
173 Leachate was collected in the leachate catcher below the soil column. Cumulative  
174 leachate volume was monitored over time to determine the saturated hydraulic  
175 conductivity ( $K_{\text{sat}}$ ,  $\text{cm min}^{-1}$ ) of each treatment by using a derivation of Darcy's  
176 approach (Sahin et al., 2011):

$$177 \quad K_{\text{sat}} = \frac{V_1 \cdot H}{A \cdot t \cdot (H + h)} \quad (4)$$

178 where  $V_1$  is the leachate volume ( $\text{cm}^3$ ),  $H$  is the length of filled soil (cm),  $A$  is the surface  
179 area of soil column ( $\text{cm}^2$ ),  $t$  is the leaching time of measurement (min),  $h$  is the height  
180 of constant water head (cm).

181 To determine the amount of salt released, we measured the volume and EC of the  
182 leachate. The leachate was collected at 3 h intervals when the leachate started to drain,  
183 and leachate was stored in 100 ml wide-mouth polypropylene reagent bottles. The salt

184 accumulated in the soil column was determined by subtracting the salt in the leachate  
185 from the applied water, the salination rate ( $Rs$ , %) indicated the ratio of salt accumulated  
186 in the soil column at every time of infiltration to the salt content at the first applied  
187 water. Leaching efficiency ( $Le$ ,  $\text{g L}^{-1}$ ) refers to the amount of desalination per unit of  
188 water volume in the desalination process.  $Rs$  and  $Le$  were calculated as follows:

$$189 \quad Rs = m_s / m_w \quad (5)$$

$$190 \quad Le = (m_s - m_1) / w \quad (6)$$

191 Where  $m_s$  is the salt content accumulated in soil column at each infiltration (g),  $m_w$  is  
192 the salt content in the total water used for the first infiltration (g),  $m_1$  is the mass of salts  
193 after the first infiltration (g),  $w$  is the total water volume used for leaching (L).

194 Soil samples were collected from each soil column at 5-cm intervals with the 0–  
195 40 cm soil layer three days after the final infiltration. Soil  $BD$  was calculated using the  
196 soil core method, and  $TP$  was calculated by Eq. (3) based on  $BD$ . Soil water  
197 characteristics curve was measured with the high velocity centrifugal method (CR21  
198 Hitachi, Japan), and calibrated by RETC software (PC Progress Inc., Prague, Czech  
199 Republic). Currently, several defining sizes of macropores are proposed, rather than a  
200 precise definition and pore size range (Cameira et al. 2003; Kim et al. 2010; Hu et al.  
201 2018; Budhathoki et al. 2022; Aldaz-Lusarreta et al. 2022). In this study, macropores  
202 were defined as the pores with diameters larger than 1 mm, whereas micropores were  
203 defined as smaller than 1 mm (Luxmoore 1981; Wilson and Luxmoore 1988). Based on  
204 the capillary pressure data, the relationship between pore diameter ( $d$ , mm) and water

205 suction ( $S$ , Pa) was described according to the capillary bundle model (Jury et al., 1991):

206 
$$d = \frac{300}{S} \quad (7)$$

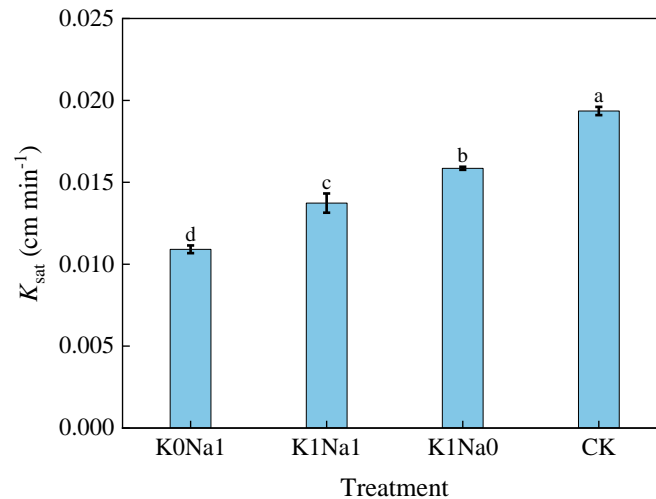
## 207 **2.4 Statistical analysis**

208 Statistical analysis among all treatments with different  $K^+/Na^+$  was performed in  
209 SPSS 22.0 software, using one-way analysis of variance (ANOVA) based on the least  
210 significant difference (LSD) test at 95% significance level ( $P < 0.05$ ). All figures were  
211 created through Origin 2022b.

## 212 **3 Results**

### 213 **3.1 Soil saturated hydraulic conductivity ( $K_{sat}$ )**

214 The K0Na1, K1Na1 and K1Na0 significantly ( $P < 0.05$ ) reduced  $K_{sat}$  by 43.62%,  
215 29.04% and 18.06% compared with CK, respectively (Fig. 2). Additionally,  $K_{sat}$  was  
216 negatively correlated with CROSS of saline water, increasing the CROSS of the applied  
217 saline water generally reduced  $K_{sat}$ .



218

219 Fig. 2. Saturated hydraulic conductivity ( $K_{sat}$ ) under different treatments. K0Na1,

220 K1Na1 and K1Na0 indicate the saline water at EC of 4 dS m<sup>-1</sup> with K<sup>+</sup>/Na<sup>+</sup> of 0:1, 1:1

221 and 1:0, respectively; CK, deionized water; Different letters after means of  $K_{sat}$  indicate

222 statistical differences ( $P < 0.05$ ) among treatments based on LSD. Bars indicate

223 standard deviations of means.

### 224 3.2 Soil water content

225 Water content increased immediately after each infiltration in all treatments, then

226 gradually decreases and the degree of variation tends to stabilize (Fig. 3). And water

227 content at deeper soil depths was greater than at shallow soil depths at the same time

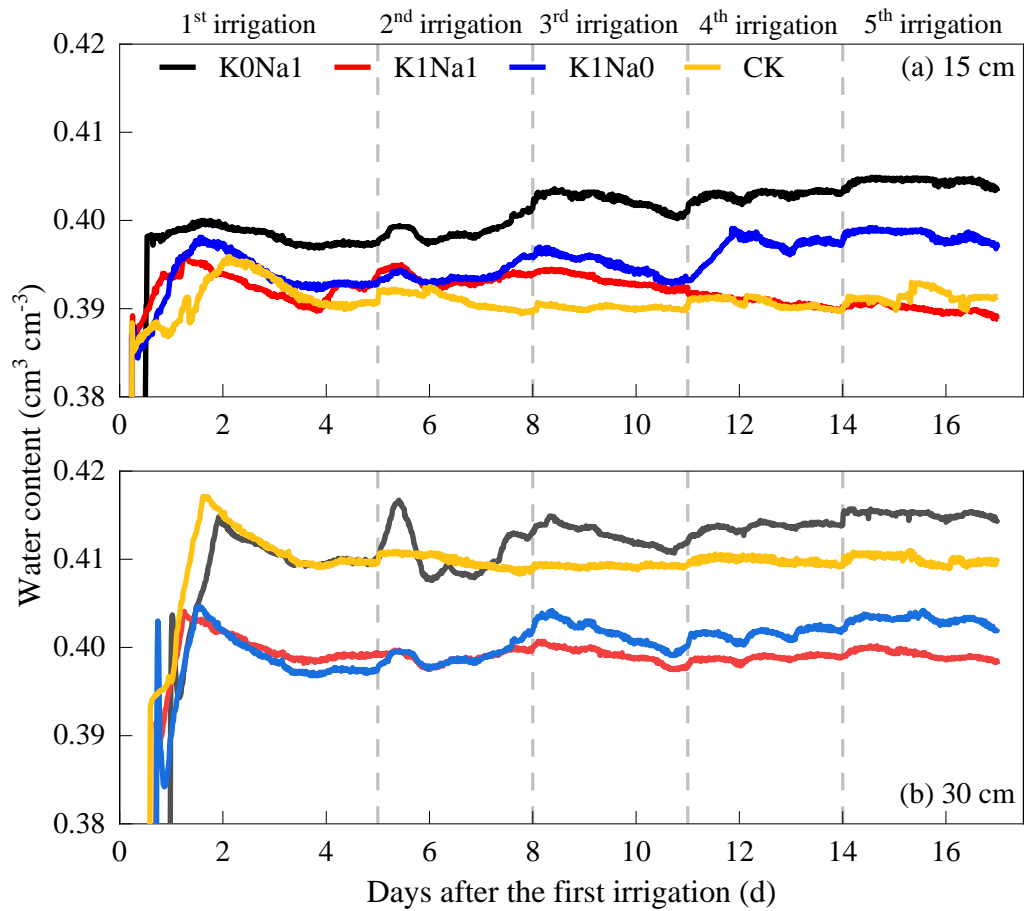
228 during the whole infiltration period. The water content ranged from 0.39–0.41 and

229 0.40–0.42 cm<sup>3</sup> cm<sup>-3</sup> at 15 and 30 cm soil depths, respectively. K0Na1 had the highest

230 water content at both 15 and 30 cm soil depths. K1Na1 and K1Na0 were greater than

231 CK at 15 cm soil depth and lower than CK at 30 cm soil depth, and the water content

232 of K1Na1 was higher than K1Na0 at both 15 and 30 cm soil layers.



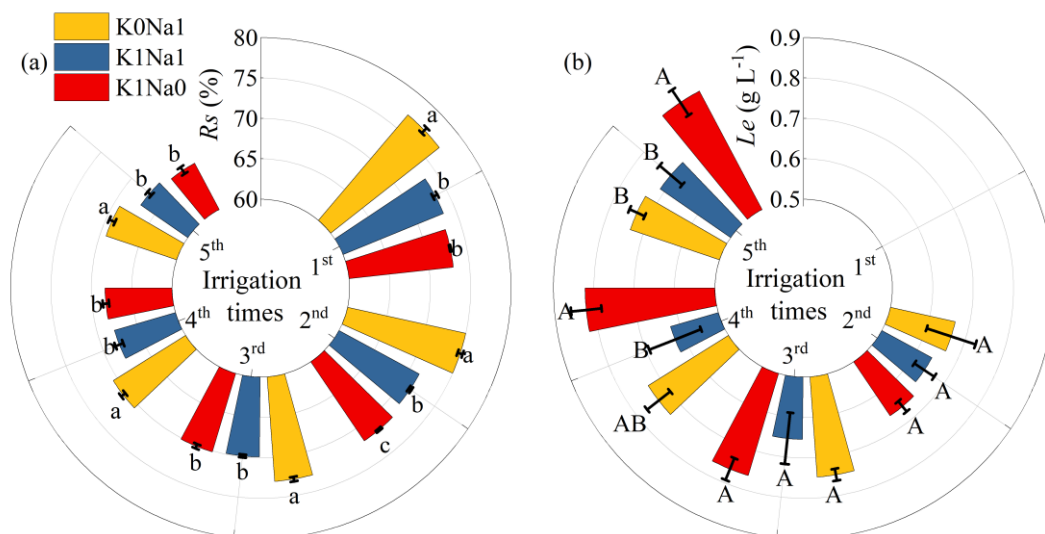
233

234 Fig. 3. Variation of water content over time under different treatments at 15 (a) and 30  
 235 cm (b) soil depths during the five times of infiltration.

### 236 3.3 Soil salination rate ( $R_s$ ) and leaching efficiency ( $Le$ )

237 The  $R_s$  and  $Le$  under CK were not shown in Fig. 4, because deionized water was  
 238 used as the control and there was almost no salt contained in the study soil, CK was  
 239 considered negligible for salt accumulation and leaching.  $R_s$  peaked at the first  
 240 infiltration, and approximately 70%–80% of the salt in the saline water was retained in  
 241 the soil column, after which the subsequent leaching had lower  $R_s$  values (Fig. 4). The  
 242 lower the relative concentration of  $K^+$  to  $Na^+$ , the larger soil  $R_s$ . Among the three saline

243 water treatments, K1Na0 had the lowest  $R_s$  and highest  $Le$  at five infiltrations.



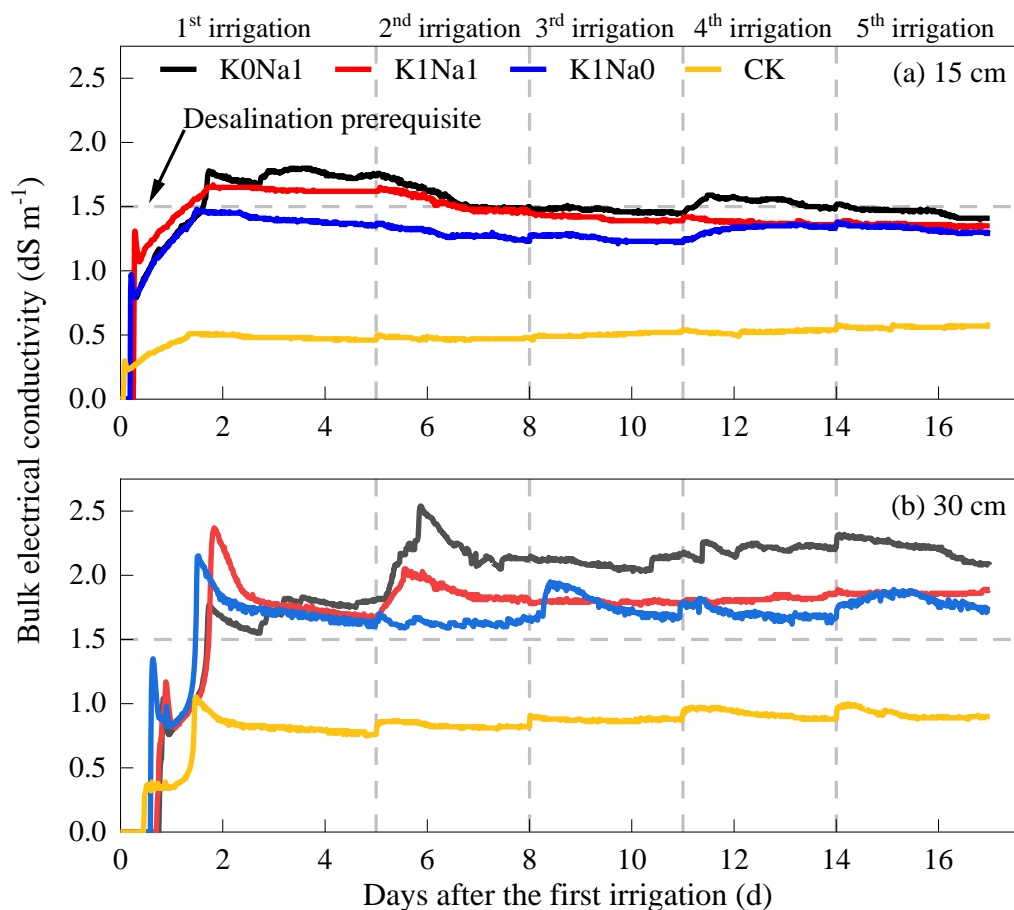
244

245 Fig. 4. Salination rate ( $R_s$ ) (a) and leaching efficiency ( $Le$ ) (b) at five infiltrations under  
 246 all saline water treatments. K0Na1, K1Na1 and K1Na0 indicate the saline water at EC  
 247 of  $4 \text{ dS m}^{-1}$  with  $K^+/Na^+$  of 0:1, 1:1 and 1:0, respectively; Different lowercase letters  
 248 followed means of  $R_s$  indicate statistical differences ( $P < 0.05$ ) among treatments based  
 249 on LSD, and different uppercase letters followed means of  $Le$  indicate statistical  
 250 differences ( $P < 0.05$ ) among treatments based on LSD. Bars indicate standard  
 251 deviations of means.

### 252 3.4 Soil bulk electrical conductivity

253 Bulk electrical conductivity of K0Na1, K1Na1 and K1Na0 ranged from 1.0–2.0  
 254  $\text{dS m}^{-1}$  at 15 cm, 1.5–2.5  $\text{dS m}^{-1}$  at 30 cm soil depth (Fig. 5). After the first infiltration,  
 255 bulk electrical conductivity in 15 cm soil depth peaked, and then exhibited a general  
 256 downward trend in the following infiltrations. However, more salts were leached to

257 deeper layers, where salt began to accumulate instead of desalination, and bulk  
 258 electrical conductivity at 30 cm soil depth gradually increased following the infiltration  
 259 events. Overall, K0Na1 had the highest bulk electrical conductivity among all  
 260 treatments at both 15 and 30 cm, and K1Na1 was quite higher than K1Na0.



261  
 262 Fig. 5. Variation of bulk electrical conductivity over time under treatments with  
 263 different  $K^+/Na^+$  at constant EC at 15 (a) and 30 cm (b) soil depths in the period of five  
 264 times of infiltration. K0Na1, K1Na1 and K1Na0 indicate the saline water at EC of 4 dS  
 265  $m^{-1}$  with  $K^+/Na^+$  of 0:1, 1:1 and 1:0, respectively; CK, deionized water.

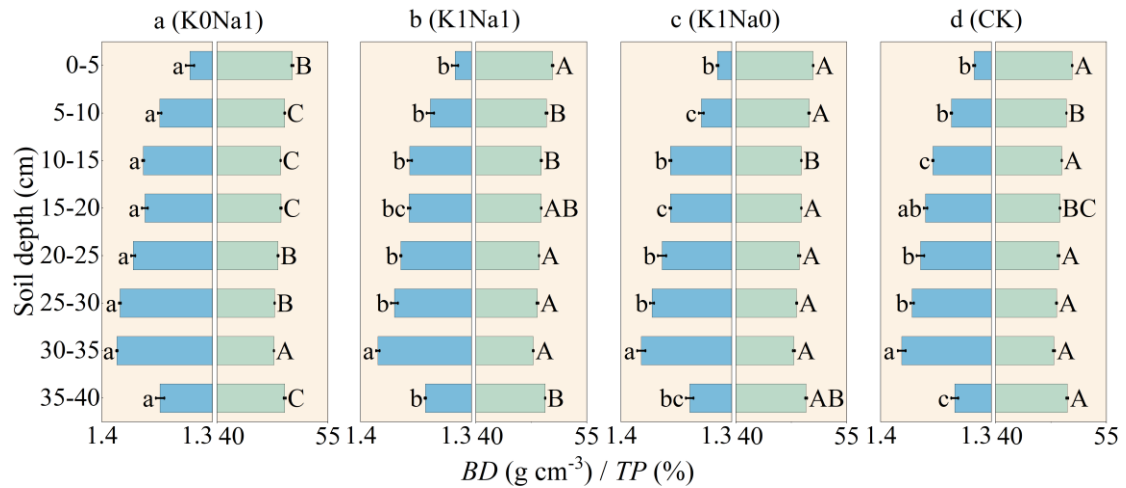
266 At 15 cm soil depth, K0Na1 reached the soil desalination prerequisite after the  
 267 fifth infiltration, while K1Na1 reached the desalination prerequisite after the second  
 268 infiltration, and K1Na0 did not exceed desalination prerequisite during the whole



269 infiltration period. Among all saline water treatments, K1Na0 reduced the desalination  
270 time and required leaching volume to reach the standard of desalination. K0Na1,  
271 K1Na1 and K1Na0 did not meet the desalination prerequisite at 30 cm soil depth, and  
272 the increased volume of infiltration water also increased the bulk electrical conductivity.

### 273 **3.5 Soil bulk density (*BD*) and total porosity (*TP*)**

274 Soil *BD* varied from 1.30–1.40 g cm<sup>-3</sup> across all treatments, and *BD* was below  
275 1.35 g cm<sup>-3</sup> at 0–10 and 35–40 cm soil layers, however, over 1.35 g cm<sup>-3</sup> at 10–35 cm  
276 soil depth (Fig. 6). K0Na1 significantly ( $P < 0.05$ ) enhanced soil *BD* throughout the soil  
277 column profile compared with CK. *TP* first diminished with soil depth to reach a  
278 minimum at about 30–35 cm, and then slightly increased at 35–40 cm. The *TP* of  
279 K1Na1 and K1Na0 slightly improved after five times of infiltration, and only K0Na1  
280 showed a decline compared with CK. Overall, over the whole infiltration period,  
281 K1Na0 was most conducive to the formation of soil pore structure and increasing the  
282 total pore volume. The saline water with lower CROSS was beneficial for reducing soil  
283 *BD* and increasing *TP*.



284

285 Fig. 6. Soil bulk density (*BD*) and total porosity (*TP*) throughout the soil column profile

286 under different treatments. K0Na1, K1Na1 and K1Na0 indicate the saline water at EC

287 of 4 dS m<sup>-1</sup> with K<sup>+</sup>/Na<sup>+</sup> of 0:1, 1:1 and 1:0, respectively; CK, deionized water; The

288 blue horizon columns represent *BD*, while the green horizon columns represent *TP*;

289 Different lowercase letters followed means of *BD* indicate statistical differences ( $P <$

290 0.05) among treatments based on LSD, and different uppercase letters followed means

291 of *TP* indicate statistical differences ( $P < 0.05$ ) among treatments based on LSD. Bars

292 indicate standard deviations of means.

### 293 3.6 Proportion of micropores and proportion of macropores

294 Micropores were the dominant pores for all treatments, the proportion of

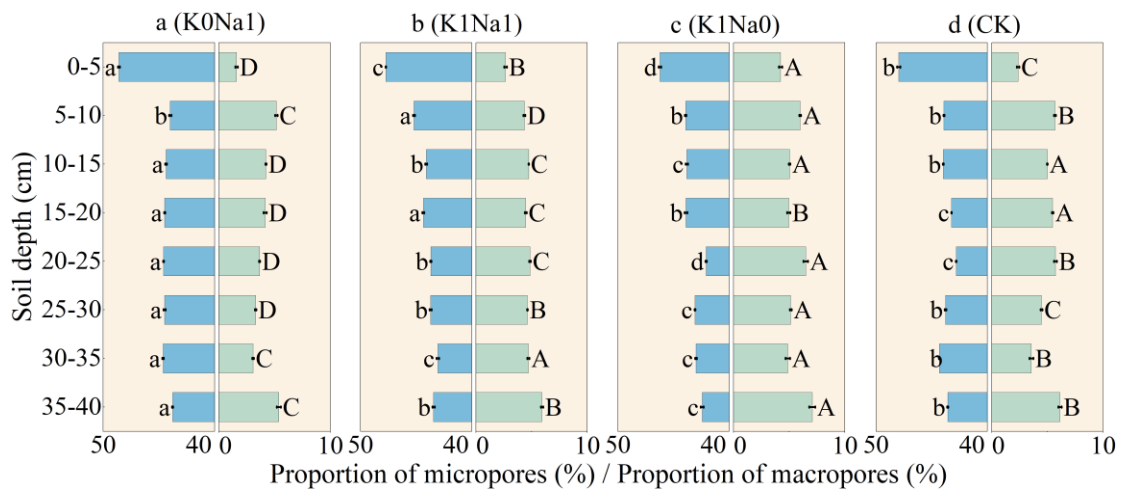
295 micropores accounting for more than 40% of the total soil volume, however, the

296 proportion of macropores did not exceed 8% (Fig. 7). The 0–5 cm soil layer had the

297 lowest proportion of macropores and retained the largest proportion of micropores

298 compared with other depths. K0Na1 had the highest proportion of micropores and the

299 lowest proportion of macropores. K1Na0 had a greater proportion of macropores in the  
 300 soil column than CK.



301  
 302 Fig. 7. Proportion of micropores and proportion of macropores in total soil volume  
 303 throughout the soil column profile under different treatments. K0Na1, K1Na1 and  
 304 K1Na0 indicate the saline water at EC of 4 dS m<sup>-1</sup> with K<sup>+</sup>/Na<sup>+</sup> of 0:1, 1:1 and 1:0,  
 305 respectively; CK, deionized water; The blue horizon columns represent proportion of  
 306 micropores, while the green horizon columns represent proportion of macropores;  
 307 Different lowercase letters followed means of proportion of micropores indicate  
 308 statistical differences (P < 0.05) among treatments based on LSD, and different  
 309 uppercase letters followed means of proportion of macropores indicate statistical  
 310 differences (P < 0.05) among treatments based on LSD. Bars indicate standard  
 311 deviations of means.

## 312 **4 Discussion**

### 313 **4.1 Effects of saline water on soil water movement and redistribution**

314 As a crucial soil hydraulic characteristic,  $K_{\text{sat}}$  reflects the transportation ability of  
315 water and solutes (Braud et al. 2001; Maillard et al. 2011; Albalasmeh et al. 2022). The  
316 cation composition and EC of soil solution affect  $K_{\text{sat}}$  by controlling electrostatic  
317 repulsive pressure through surface potential and midpoint potential between adjacent  
318 particles, and consequently influence water movement (Fares et al. 2000; Liu et al.,  
319 2022b). Specifically, the relative concentration of  $\text{K}^+$  to  $\text{Na}^+$  in saline water was related  
320 to the swelling and dispersion of soil particles (Yu et al. 2016; Zhu et al. 2019).  
321 Dispersed clay particles clogged soil macropores to subsequently restrict water  
322 transport (Awedat et al., 2021). The  $\text{Na}^+$  has a relatively higher ionicity index than  $\text{K}^+$ ,  
323 as a result, the low relative concentration of  $\text{K}^+$  to  $\text{Na}^+$  decreased the degree of  
324 covalency in clay-cation bonds, which was detrimental to clay particles aggregation  
325 (Marchuk and Rengasamy 2011). Therefore, in our study, the high relative  
326 concentration of  $\text{K}^+$  to  $\text{Na}^+$  promoted the flocculation and stabilization of soil clay  
327 particles, resulting in an increased water hydraulic conductivity (Fig. 2).

328 After a certain period of irrigation, soil moisture redistributed at different depths  
329 of soil column (Fig. 3). Soil water moved further down during the phase of water  
330 redistribution soon after each irrigation, reducing the water content in the upper soil  
331 layers. As the upper soil layers drained, the lower soil layers still had water inflow

332 (Kargas et al., 2021), increasing the water content in the lower soil layers. The results  
333 also implicated that the retention of soil water by  $\text{Na}^+$  was stronger than that by  $\text{K}^+$ , the  
334 cause may be that  $\text{Na}^+$  can increase the thickness of the diffuse-double layers around  
335 soil colloids theoretically due to its larger hydrated radius and lower charge than  $\text{K}^+$ ,  
336 and the adjacent double layers overlapped to provide more space between layers (He et  
337 al., 2015), where, subsequently, more water can be retained (Fig. 3).

338 Additionally, our study showed that K1Na1 was even more beneficial than  
339 deionized water for water downward transport (Fig. 3), which was due to that deionized  
340 water (CK) (below  $0.2 \text{ dS m}^{-1}$ ) tended to leach soluble minerals and salts, especially  
341  $\text{Ca}^{2+}$ , from the surface soil layers. This would lead to the reduction of its original solid  
342 soil structural stability. In the absence of salt and  $\text{Ca}^{2+}$ , the dispersed tiny particles filled  
343 the smaller pore spaces in soil, reducing even more channels for water flow and  
344 exacerbating water retention in deeper soil layers (Ayers and Westcot 1985). However,  
345 a lower concentration of soluble salts could increase colloid flocculation, and thereby,  
346 improving soil aeration and water conductivity (Tang and She 2016).

#### 347 **4.2 Effects of saline water on soil salination and desalination process**

348 Numerous factors influence soil salt leaching efficiency; for example, increasing  
349 EC and reducing SAR definitely improve clay flocculation, which can enhance salt  
350 leaching (Ebrahim Yahya et al., 2022).  $\text{Na}^+$  is more likely to trigger soil clay dispersion  
351 and swelling than  $\text{K}^+$ , thus  $\text{Na}^+$  generally inhibits water infiltration, which is detrimental

352 to salt leaching (Smiles and Smith 2004). Adding  $K^+$  could promote displacement of  
353 the adsorbed  $Na^+$ , and then decrease  $Na^+$  concentration and salt accumulation in soil  
354 solute through leaching.

355 A greater reduction in  $Na^+$  concentration was associated with a higher rate of  
356 cation exchange rate, and the slow rate of solute leaching from aggregates reduced the  
357 total leaching efficiency (Shaygan et al., 2017). During the leaching process, water flow  
358 preferentially passed through the macropores rather than aggregates. The slow water  
359 transportation through aggregates induced the slow removal of solutes from the  
360 aggregates, leading to a reduced leaching efficiency. In our study, the alternate leaching  
361 was implemented to improve solute leaching (Figs. 4 and 5). The soil solutes diffused  
362 into the aggregates surface during the rest period, improving salt leaching due to the  
363 water flow in macropores (Al-Sibai et al., 1997). Saline water with more  $K^+$  could  
364 increase the magnitude of cation exchange due to the substitution of  $Na^+$  on exchange  
365 sites by  $K^+$  with lower dispersive potential (Shaygan et al., 2017), the intensive release  
366 of cations from the soil further improved salt's leaching efficiency. In addition, the  
367 integrity of soil aggregates created by combining clay particles and the other soil  
368 components enhanced by  $K^+$  can benefit solute transportation (Marchuk and  
369 Rengasamy 2011).

#### 370 **4.3 Effects of saline water on soil pore structure characteristics**

371 The upper soil was longer exposed to water due to the long-term continuous

372 irrigation, causing the particles to swell and the surface layer to loosen (Vaezi et al.  
373 2017; Håkansson and Lipiec 2000), and also the decreased *BD* in the surface layer of  
374 soil column (Fig. 6). The subsoil *BD* increased with depth under the impact of water  
375 pressure and self-weight due to the declining pore diameter and pore branching closure  
376 (Schjønning et al., 2013). And for soil at the bottom, the loss of soil particles from small  
377 holes was responsible for the abrupt reduction in *BD* (Fig. 6). The value of *CROSS* in  
378 saline water could reflect changes in soil *BD* and *TP*, in agreement with the result of  
379 Marchuk and Marchuk (2018). The high *CROSS* implied an increase in the proportion  
380 of monovalent exchangeable cations, thickening the double layer at the interface  
381 between the clay surface and soil solution. Hence, soil swelling occurred at the expense  
382 of water-conducting pores. Additionally, aggregates slaking and subsequent clay  
383 dispersion and deposition of clay particles within the pore space contributed to the  
384 reduction in *TP* (Marchuk and Marchuk 2018).

385       Soil macropores play a crucial role in water and solute transport, accounting for  
386 85% of the total infiltration volume (Wilson and Luxmoore 1988; Weiler and Naef 2003;  
387 Kotlar et al. 2020). For saline water with the same EC, a decrease in  $K^+$  concentration  
388 may enhance soil clay dispersion, resulting in the loosening of clay particles from the  
389 aggregates. This, in turn, dispersed clay particles moved with water caused the  
390 macropores to become blocked, converting them into micropores (Cameira et al., 2003),  
391 thus leading to a decrease in the volume of soil macropores (Fig. 7).

## 392 **5 Conclusion**

393 We explored the effects of the relative ratio of  $K^+$  to  $Na^+$  in saline water on soil  
394 hydraulic characteristics and structural stability via a soil column experiment. Irrigation  
395 with saline water of  $K^+/Na^+$  of 1:0 caused fewer pore blockages due to soil clay particle  
396 dispersion than 0:1, which increased soil saturated hydraulic conductivity. The presence  
397 of  $K^+$  accelerated the sustained  $Na^+$  replacement and leaching, alleviating salt  
398 accumulation and enhancing leaching efficiency.  $K^+$  positively affected the  
399 establishment of soil structure due to the transformation of micropores into macropores,  
400 and the ever-increasing unobstructed water-conducting channels sped up water and  
401 solute transport. The rational use of saline water with adequate  $K^+$  could help mitigate  
402 the structural deterioration caused by  $Na^+$ . Appropriate adjustment of the relative  
403 concentration of  $K^+$  to  $Na^+$  in saline water during infiltration could ameliorate soil  
404 structural properties. In addition to  $Ca^{2+}$  and  $Mg^{2+}$  (primary concerns in earlier studies),  
405 the relative concentration of  $K^+$  to  $Na^+$  is an essential indicator for assessing the  
406 suitability of saline water quality for irrigation and should be considered when using  
407 saline water.

## 408 **Author contributions**

409 Sihui Yan and Tibin Zhang conceived and designed the experiments. Sihui Yan,  
410 Binbin Zhang and Tonggang Zhang led the data processing and statistical analysis,  
411 Sihui Yan, Yu Cheng, Chun Wang and Min Luo performed the experiments. Sihui Yan



412 wrote the initial draft. Hao Feng and Kadambot H.M. Siddique contributed to review  
413 and editing of the paper.

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