



## Going down the rabbit hole: An exploration of the soil erosion feedback system

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**Abstract.** Soil erosion rates on arable land frequently exceed the pace at which new soil is formed. This imbalance leads to soil thinning (i.e., truncation), whereby subsoil horizons and their underlying parent material become progressively closer to the land surface. As subsurface horizons often have contrasting properties to the original topsoil, truncation-induced changes to soil properties might affect erosion rates and runoff formation through a soil erosion feedback system. However, the potential interactions between soil erosion and soil truncation are poorly understood due to a lack of empirical data and the neglect of long-term erodibility dynamics in erosion simulation models. Here we present a novel model-based exploration of the soil erosion feedback system over a 500-year period, using measured soil properties from a diversified database of 265 soil profiles in the United Kingdom. We found that modelled erosion rates in 39 % of the soil profiles were sensitive to truncation-induced changes in soil properties and that most of these truncation-sensitive profiles (75 %) displayed a deaccelerating erosion trend over the simulation period. This was largely explained by decreasing silt contents in the soil surface due to selective removal of this more erodible particle size fraction and the presence of clayey or sandy substrata. Moreover, the profiles with deaccelerating erosion trends had an increased residual stone cover, which armoured the land surface and reduced soil detachment. Contrastingly, the soils with siltier subsurface horizons continuously replenished the plough layer with readily erodible material, which accelerated the soil losses over time. Ultimately, our results demonstrate how soil losses can be sensitive to erosion-induced changes in soil properties, which in turn may accelerate or slow down soil thinning. These findings are likely to affect how we calculate soil lifespans and make long-term projections of land degradation.



## 1 Introduction

Rates of soil erosion on agricultural land often exceed the rates at which new soil is formed (Evans et al., 2019; Montgomery, 2007). This imbalance is one which, left unchecked, can pose a critical threat to the sustainability of global soil resources and their ability to deliver vital ecosystem services across environments and society (Bot et al., 2000; Quinton et al., 2010). Moreover, as soils become thinner (i.e., truncated), the subsoil horizons and their underlying parent material become progressively closer to the land surface. This process might affect physical, chemical and biological topsoil properties (Bouchoms et al., 2019; Papiernik et al., 2009; Vanacker et al., 2019), as well as soil water availability to plants and ultimately crop growth (Herbrich et al., 2018; Öttl et al., 2021; Schneider et al., 2021).

Erosion-induced changes to soil depth and soil properties can therefore influence soil losses and runoff formation through a soil erosion feedback system (Morgan et al., 1984; Vanwalleghem et al., 2017). Understanding how such system might develop over time and under assorted conditions might be an important step to proactively design and implement effective soil conservation strategies, as different soils are likely to be impacted by erosion in varied ways (Hoag, 1998). However, the empirical data over decadal to centennial timescales required to explore the feedbacks between soil erosion and soil thinning are currently non-existent. It follows that process-oriented soil erosion models are arguably the only available tool to simulate how erosion processes interact with truncation-induced changes in the soil system.

To date most soil erosion models and model users assume that the inherent erodibility (i.e., the susceptibility of soil to erosion) of different soil horizons down a soil profile is constant over the period of a model simulation. As upper soil horizons are removed by erosion, exposing the subsurface material, the implicit assumption in soil erosion modelling is that this erodibility is not variable, such that any changes to projected erosion rates are solely a factor of climate, land cover, and topography (e.g., Ciampalini et al., 2020; Eekhout et al., 2021; Panagos et al., 2021). However, since erodibility is a reflection of soil physical, chemical, and biological properties, and given that subsoils typically (although not exclusively) exhibit contrasting soil properties to those observed in upper horizons, it follows that erodibility is not necessarily a constant as a soil profile thins. Furthermore, soil erodibility might change over longer timescales due to the coarsening and armouring of surface soils (Sharmeen and Willgoose, 2007; Willgoose and Sharmeen, 2006) and the depletion of erodible material as a result of extreme soil truncation (Anselmetti et al., 2007).

Although the soil erosion feedback system has been recognised as a key challenge for modelling past and future erosion rates (Vanwalleghem et al., 2017), long-term dynamics of soil erodibility are an underexplored topic in erosion research. Exceptions come from landscape evolution models, which



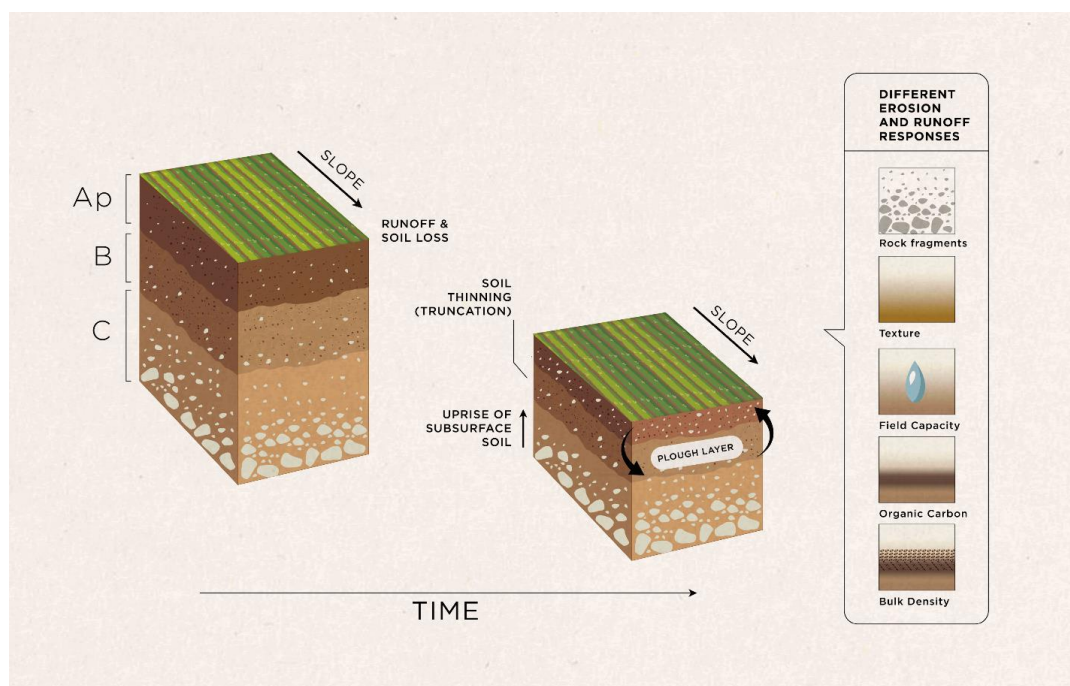
55 simulate the influence of erosion and deposition on soil development over millennia (Marijn Van Der Meij  
et al., 2020; Sommer et al., 2008). However, in areas under severe erosion rates, subsoil horizons can be  
exposed within a matter of decades (Evans et al., 2020), which might trigger unexpected responses  
regarding runoff formation and soil losses. Moreover, soil truncation can introduce substantial spatial  
variability to soil properties, often not accounted for in static soil maps used for a variety of purposes  
(Świtoniak et al., 2016).

60 Here, we present a novel exploration of the soil erosion feedback system by simulating 500 years of soil  
losses and surface runoff on 265 agricultural soil profiles in the United Kingdom. We investigate how soil  
erosion rates respond to truncation-induced changes in soil properties and unravel the processes potentially  
driving such responses in different soil types. To the best of our knowledge, this is the first time soil erosion  
models have been used to understand the interactions between soil erosion, soil thinning, and soil  
65 erodibility, and how these interactions are established in varying soil types. An enhanced understanding of  
such dynamic soil erosion feedback system will be crucial for improving the calculation of soil lifespans,  
providing future soil loss projections, and designing long-term soil conservation strategies.

## 2 Materials and methods

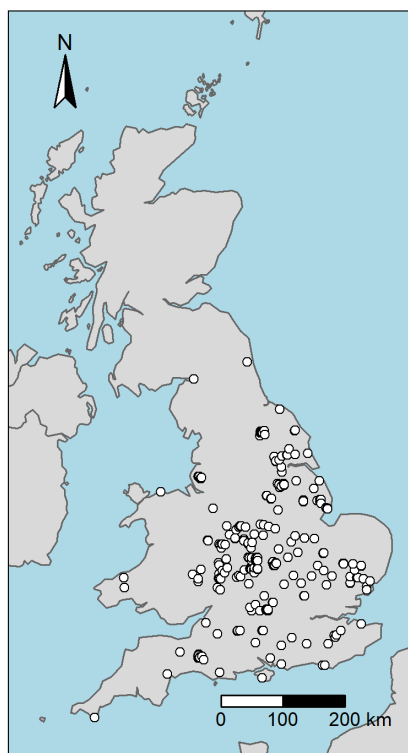
### 2.1 Concept

70 Our modelling concept is essentially a numerical thought experiment, in which land cover, agricultural  
management, climate, and topography parameters are held within a constant range, so that any changes in  
simulated soil losses and surface runoff over a 500-year period are solely a result of changes in soil  
properties due to erosion processes (Fig. 1). To perform this experiment, we parametrised a soil erosion  
model using data from 265 agricultural soil profiles spread across the United Kingdom (Fig. 2). The abstract  
75 spatial scale of the simulations can be perceived as a pedon located on conventionally tilled hillslope with  
winter cereals. For simplicity, we assume this spatial unit does not receive runoff and sediment input from  
upslope. As the original topsoil of each profile/pedon is successively removed by erosion, our model  
gradually mixes the subsurface horizons into a 20 cm plough layer, continuously updating soil properties  
through mass-balance models and pedotransfer functions (Fig. 1).



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Figure 1. Modelling concept: selective soil erosion processes alter topsoil properties, which are then mixed with the underlying substrata as the soil profile thins. Updated soil properties for the plough layer are used as model inputs for the following timestep.



85 Figure 2. Location of the 265 soil profiles used in this study. Data source: Land Information System (LandIS) (LandIS, 2022).

In order to implement our modelling concept, we adapted the Modified Morgan-Morgan-Finey model (MMMFM) (Morgan and Duzant, 2008). The model was chosen due to its ability to simulate multiple erosion subprocesses (e.g., runoff formation, detachment by raindrop impact and runoff, particle size selectivity) with a parsimonious parameter set. Importantly, the MMMFM has provided acceptable predictions of annual soil losses for different testing sites in England (Morgan and Duzant, 2008). In the following we provide a  
90 brief description of the basic MMMFM equations (Section 2.2). We subsequently characterise the soil profile database used for the modelling (Section 2.3) and describe the model implementation, including the mixing of surface and subsurface horizons (Section 2.4).

## 95 2.2 MMMFM operating equations

The MMMFM is a process-oriented conceptual model running on an annual timestep, in which soil erosion processes are separated into a water phase and a sediment phase (Morgan et al., 1984; Morgan and Duzant,



2008). In the water phase, effective annual rainfall ( $P_{EF}$ ; mm) is calculated considering the effect of interception by the vegetation cover:

$$P_{EF} = P \cdot (1 - PI) \quad (1)$$

100 Where  $P$  is the mean annual rainfall (mm) and  $PI$  is the average rainfall interception (proportion 0-1) afforded by the vegetation cover. For annual crops,  $PI$  and all other land cover parameters are taken as an approximate average over the growing season.

Annual leaf drainage ( $LD$ ; mm) and direct throughfall ( $DT$ ; mm) are separated as a function of the average canopy cover of the vegetation ( $CC$ ; proportion 0-1):

$$LD = P_{EF} \cdot CC \quad (2)$$

$$DT = P_{EF} - LD \quad (3)$$

105 The kinetic energy of direct throughfall  $KE_{DT}$  is calculated with the typical value of erosive rainfall intensity for a given location ( $I$ ; mm hr<sup>-1</sup>) and the amount of annual direct throughfall, whereas the kinetic energy of leaf drainage  $KE_{LD}$  is a function of the average plant height for the growing season ( $PH$ ; m). Total kinetic energy of the effective annual rainfall ( $KE$ ; J m<sup>-2</sup>) is then calculated as the sum of the throughfall and leaf drainage components.

$$KE_{DT} = DT \cdot (8.95 + 8.44 \cdot \log_{10} I) \quad (4)$$

$$\text{if } PH < 0.15; KE_{LD} = 0 \quad (5)$$

$$\text{if } PH \geq 0.15; KE_{LD} = 15.8 \cdot PH^{0.5} - 5.87 \quad (6)$$

$$KE = KE_{DT} + KE_{LD} \quad (7)$$

110 Saturation excess overland flow typically occurs in climates with low intensity precipitation and without a pronounced seasonal rainfall regime (Morgan and Duzant, 2008), specifically in areas with shallow soils



and impermeable bedrocks (Beven, 2012). In the MMMF model, saturation excess runoff generation is assumed to occur when the mean daily rainfall exceeds the mean daily storage capacity of the soil ( $SC$ ; mm):

$$SC = 1000 \cdot MS \cdot BD \cdot HD \cdot \left( \frac{ET_a}{ET_p} \right)^{0.5} \quad (8)$$

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Where  $MS$  is soil moisture at field capacity (% w w<sup>-1</sup>),  $BD$  is bulk density (Mg m<sup>-3</sup>),  $HD$  is effective hydrological depth (m) (i.e., the land cover dependent soil depth in which storage capacity controls the generation of runoff), and  $ET_a/ET_p$  is the ratio of actual to potential evapotranspiration. These parameters represent an approximate average for the cropping season.

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The annual runoff generation ( $Q$ ; mm) is then estimated as a function of annual effective rainfall, the ratio between storage capacity and mean daily rainfall ( $P_M$ , mm), and the slope length of the spatial modelling element ( $L$ ; m):

$$Q = P_{EF} \cdot e^{\left( -\frac{SC}{P_M} \right)} \cdot \left( \frac{L}{10} \right)^{0.1} \quad (9)$$

In the sediment phase, the annual detachment of soil particles by raindrop impact ( $E_R$  kg m<sup>-2</sup>) and by surface runoff ( $E_Q$ ; kg m<sup>-2</sup>) are calculated separately for the clay, silt, and sand texture classes, which are

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subsequently summed:

$$E_R = \sum_{n=1}^i \left[ K_{Ri} \cdot \frac{T_i}{100} \cdot (1 - ST) \cdot KE \cdot 10^{-3} \right] \quad (10)$$

$$E_Q = \sum_{n=1}^i \left\{ K_{Qi} \cdot \frac{T_i}{100} \cdot Q^{1.5} \cdot [1 - (GC + ST)] \cdot \sin^{0.3} \cdot S \cdot 10^{-3} \right\} \quad (11)$$

Where  $K_R$  is the detachability of the soil by raindrop impact (J m<sup>-2</sup>),  $T$  is the percentage of texture class  $i$ ,  $ST$  is stone cover (proportion 0-1),  $K_Q$  is the detachability of the soil by runoff (J m<sup>-2</sup>),  $GC$  is the average proportion of the soil covered by vegetation during the growing season (0-1), and  $S$  is slope angle (degrees). Soil detachability values for each texture class  $i$  (clay, silt, and sand) are taken from Quansah (1982).



- 130 The immediate deposition of detached sediments ( $D_i$ ; %) (i.e., the percentage of sediments not delivered to the runoff for transport) is estimated as a function of the average annual flow velocity, in our case for vegetated conditions ( $v_v$ ;  $\text{m s}^{-1}$ ), and the particle fall number ( $FN$ ):

$$v_v = \left( \frac{2 \cdot g}{\phi \cdot NV} \right)^{0.5} \cdot S^{0.5} \quad (12)$$

$$FN_i = \frac{L \cdot v_{s_i}}{v_v \cdot d} \quad (13)$$

$$D_i = 44.1 \cdot (FN_i)^{0.29} \quad (14)$$

- Where  $g$  is the gravitational acceleration ( $9.81 \text{ m s}^{-2}$ ),  $\phi$  is the diameter of plant stems (m),  $NV$  is the number of stems per unit area (number  $\text{m}^{-2}$ ),  $v_s$  is the fall velocity for texture class  $i$  ( $0.00002 \text{ m s}^{-1}$ ,  $0.002 \text{ m s}^{-1}$ , and  $0.02 \text{ m s}^{-1}$  for clay, silt, and sand, respectively), and  $d$  is the hydraulic radius of the flow ( $0.005 \text{ m}$  for unchanneled flow,  $0.01 \text{ m}$  for shallow rills, and  $0.25 \text{ m}$  for deeper rills). Again, in this case, land cover parameter values describe an average over the cropping season.
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The total detached material delivered annually to transport ( $G$ ;  $\text{kg m}^{-2}$ ) is modelled separately for each soil texture class  $i$ :

$$G = \sum_{n=1}^i \left[ (E_{R_i} + E_{Q_i}) \cdot \left( 1 - \frac{D_i}{100} \right) \right] \quad (15)$$

- 140 The annual transport capacity of the surface runoff ( $TC$ ;  $\text{kg m}^{-2}$ ) is calculated as a function of annual runoff volume ( $Q$ ; mm), slope, and the effect of plant cover/tillage on flow velocities, for each particle size class  $i$ :

$$TC = \sum_{n=1}^i \left[ \left( \frac{v_a \cdot v_v \cdot v_t}{v_b} \right) \cdot \left( \frac{T_i}{100} \right) \cdot Q^2 \cdot \sin S \cdot 10^{-3} \right] \quad (16)$$





The average flow velocities for the actual soil conditions ( $v_a$ ;  $\text{m s}^{-1}$ ), for the effect of tillage ( $v_t$ ;  $\text{m s}^{-1}$ ), and for the standard bare soil condition ( $v_b$ ;  $\text{m s}^{-1}$ ) are calculated using the Manning equation:

$$v_a = \frac{1}{n} \cdot d^{0.67} \cdot S^{0.5} \cdot e^{-0.0185T} \quad (17)$$

$$v_b; v_t = \frac{1}{n} \cdot d^{0.67} \cdot S^{0.5} \quad (18)$$

145 Where  $n$  is Manning's roughness coefficient. For the tilled conditions, Manning's  $n$  is estimated as a function of an implement-dependent surface roughness parameter (RFR) taken from Morgan (2005):

$$n = e^{(-2.11+0.03RFR)} \quad (19)$$

The annual soil loss ( $SL$ ;  $\text{kg m}^{-2}$ ) is calculated by comparing the annual transport capacity ( $TC$ ;  $\text{kg m}^{-2}$ ) and the annual sediment delivered to the runoff ( $G$ ;  $\text{kg m}^{-2}$ ), for each texture class  $i$ :

$$\text{If } TC_i \geq G_i; SL = G_i \quad (20)$$

150 If the amount of sediment delivered to the runoff is greater than the transport capacity, the excess sediment will be deposited until  $G = TC$ . Such deposition is modelled using the settling velocities and fall numbers described in equation 14. The sediment balance becomes:

$$\text{If } TC_i < G_i \text{ calculate } G1_i = G_i \left[ 1 - \left( \frac{D_i}{100} \right) \right] \quad (21)$$

$$\text{If } TC_i \geq G1_i; SL_i = TC_i; \text{ if } TC_i < G1_i; SL_i = G1_i;$$

Finally, the soil losses for the clay, silt, and sand texture classes are summed to produce total estimates of annual soil losses ( $SL$ ;  $\text{kg m}^{-2}$ ):



$$SL = \sum_{n=1}^i SL_i \tag{22}$$

### 2.3 Soil database

155 The soil profile data used in the model were retrieved from the UK SOILPITS dataset, which is one of  
 many datasets held within the Land Information System (LandIS) operated by the Soil and Agrifood  
 Institute at Cranfield University, UK (LandIS, 2022). The UK SOILPITS dataset represents a compilation  
 of a series of soil profile surveys conducted across the UK since 1984. We selected only the profiles under  
 agricultural land cover, and which had complete information on the key soil properties used for modelling  
 160 for all described horizons.

Table 1 presents a descriptive summary of the data representing each whole soil profile; that is, data for  
 each horizon from each profile has been bulked together. The profiles range in thickness from 0.22 m to  
 1.96 m (median depth is 0.60 m) and are typically composed by four characteristic horizons: an A, E, B,  
 and C horizon. More information about how each horizon was surveyed and differentiated in the field can  
 165 be found in Hodgson (1997).

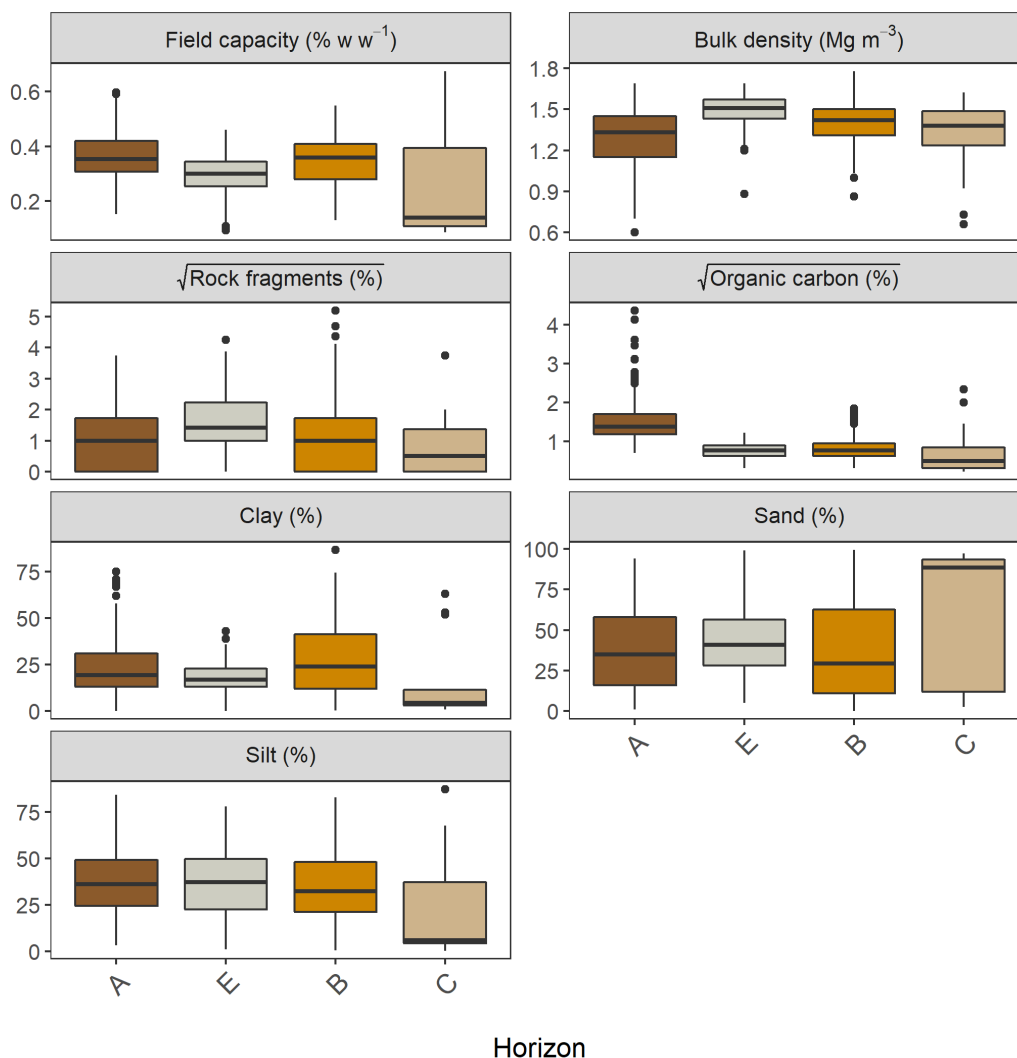
Table 1. Descriptive statistics of the soil properties from the 265 agricultural soil profiles (depths between  
 0.22 and 1.96 m) from the LandIS database used in the simulations.

Variable	Unit	Mean	Median	Quantiles			
				5th	25th	75th	95th
Soil moisture at field capacity	% w w <sup>-1</sup>	0.3	0.3	0.2	0.3	0.4	0.5
Bulk density	Mg m <sup>-3</sup>	1.4	1.4	1.0	1.3	1.5	1.6
Rock fragments	%	2.5	1.0	0.0	0.0	3.5	9.0
Clay	%	24.5	20.0	4.3	12.7	33.0	57.7
Sand	%	39.4	35.0	4.0	15.1	60.4	87.0
Silt	%	36.1	35.0	6.0	22.0	49.0	71.0
Organic carbon	%	4.6	4.7	3.2	4.1	5.3	6.1

170 Figure 3 demonstrates the variability of key soil properties within the four characteristic soil horizons,  
 compiling all soil profiles used in the dataset (by ‘key’, we mean those properties which are employed  
 directly or indirectly as input variables in our model). There is considerable overlap between each horizon,  
 largely due to the heterogeneity of soil types represented in the dataset. However, some distinctive patterns  
 can be discerned. For example, between the A and B horizon, bulk density tends to increase, while organic  
 175 carbon tends to decrease. Some 79 profiles were also observed to have an E horizon directly below the A



horizon. This was distinguished by the presence of a mineral layer with less organic carbon and clay content than the underlying B horizon indicating downward and/or lateral translocation into the subsoil. Another notable boundary lies between the B and C horizon, where the median volumetric water content at field capacity reduces by more than 2.5 times. This may be reflective of some distinctive textural changes  
180 between these two horizons: the median sand content increases thrice, while both clay and silt decrease by more than five times.



185 Figure 3. Boxplots of the key soil properties for each horizon of the soil profiles used in this study. Horizons which were not classified, or which occurred less than five times in the dataset are not show in the figure. Organic carbon and rock fragment values undergone a square root transformation to improve the visualisation of the data.



## 2.4 Model implementation

190 Our modelling framework consists of an application of the MMMF model for each of the 265 soil profiles over a 500-year period. Whilst the variability of the soil properties across profiles and horizons was incorporated into the model, all modelling units were parametrised the same for their climatic, land cover, and topographic variables. This was performed to test the sensitivity of modelled soil losses to erosion-induced changes to soil properties in different soil types.

195 We selected rainfall-associated parameter values based on UK average climatic variables for the 1991-2020 period (Kendon et al., 2021). For the land cover parameters, we took the guide values recommended by Morgan and Duzant (2008) for conventionally tilled winter cereals. These values represent an approximate average for the crop growing season. In addition, we assumed a 10 m slope length and 6° slope gradient for the spatial element of the simulation unit. For the soil parameters, we used the measured properties from  
 200 the soil profile database (Table 1). In addition, texture-dependent parameters values were taken for the model guide, considering the soils' particle size distribution. A Monte Carlo simulation with 100 iterations per year was included to provide a forward error assessment of the model outputs (Beven, 2009). Model parameters were sampled from a normal distribution with a 10 % standard deviation to partially account for measurement errors and the uncertainty in parameter estimation. The constant parameter distributions  
 205 used in all simulations are displayed in Table 2.

Table 2. Parameter values which were applied to all soil profiles and were sampled in the Monte Carlo simulation.

Parameter	Unit	Symbol	Mean	SD
Annual rainfall	mm	$P$	1200	120
Number of rainy days per year	-	-	160	16
Average intensity of erosive rainfall	mm h <sup>-1</sup>	$I$	10	1
Effective hydrological depth	m	$HD$	0.12	0.012
Permanent interception	-	$PI$	0.4	0.04
Ratio of actual to potential evapotranspiration	-	$ET_a/ET_p$	0.6	0.06
Canopy cover	-	$CC$	0.8	0.08
Ground cover	-	$CG$	0.3	0.03
Plant height	m	$PH$	1.5	0.15
Number of plants per unit area	number m <sup>-2</sup>	$NV$	250	25
Average diameter of plant elements at ground surface	m	$\phi$	0.05	0.005
Roughness of the soil surface	cm m <sup>-1</sup>	$RFR$	10	1
Slope*	degrees	$S$	6	-
Slope length*	m	$L$	10	-



Clay detachability by raindrop impact	$\text{J m}^{-2}$	$K_{Rclay}$	0.1	0.01
Silt detachability by raindrop impact	$\text{J m}^{-2}$	$K_{Rsilt}$	0.5	0.05
Sand detachability by raindrop impact	$\text{J m}^{-2}$	$K_{Rsand}$	0.3	0.03
Clay detachability by runoff	$\text{g mm}^{-1}$	$K_{Qclay}$	0.1	0.01
Silt detachability by runoff	$\text{g mm}^{-1}$	$K_{Qsilt}$	0.16	0.016
Sand detachability by runoff	$\text{g mm}^{-1}$	$K_{Qsand}$	0.15	0.015

\*The parameter value was held constant during the Monte Carlo simulation.

As the MMMF model is applied with an annual resolution, we used the soil bulk density to convert the modelled soil losses from their native units to  $\text{m yr}^{-1}$ , after each timestep. Next, the model reduced the depth of the upmost soil horizon considering the amount of eroded soil in the previous year. Since the model calculates soil losses separately for each particle size fraction, the soil texture of the 20 cm plough layer was updated after each timestep. Rock fragments were assumed not to be removed from the soil matrix, and therefore the stone cover (if present) undergoes a residual increment, considering the soil losses from the previous timestep. Of note, the selective removal of soil organic carbon associated to finer soil fractions was not simulated. If the upper horizon depth was greater than the 20 cm plough depth, we assumed that no mixing would occur with the underlying horizons. However, if the upper horizon was thinner than 20 cm for any given timestep, we used a mass balance model to recalculate soil texture, soil organic carbon, and the percentage of rock fragments (used as a proxy for the stone cover model parameter) for the plough layer, considering the proportion of the lower horizon in the mixture.

For every timestep, soil bulk density and soil moisture at field capacity were estimated using pedotransfer functions (PTFs). We established the PTFs by fitting a linear regression of bulk density and soil moisture at field capacity as a function of sand (%) and organic carbon content (%) for the A horizons in our soil profile dataset (Fig. A1, A2). This was performed because i) we assumed that bulk density and soil moisture at field capacity would be affected by the changes in soil texture due to selective particle size removal; and ii) we presupposed that, as the subsoil horizons get incorporated into the plough layer and become closer to the surface, their bulk density and soil moisture at field capacity would become more characteristic of an A horizon, due to tillage and organic matter input from plant biomass. Similarly, we established a pragmatic lower limit for soil organic carbon content for different soil texture classes, based on the lowest values observed in the A horizons from our dataset. That is, we assumed the organic carbon would not decrease indefinitely with soil truncation due to the continuous input from plant material and potentially other farming practices. This assumption is based on observations that even heavily eroded arable soils typically contain some type of Ap horizon (Świtoniak, 2014). The successive soil thinning and mixing processes continued for 500 years or until the plough layer reached the end of the lowermost soil horizon (i.e., 20 cm above the bedrock). We assumed that soil losses would outpace soil formation within the simulated system



(see Evans et al., 2019), and since we did not focus on calculating soil lifespans, it was not necessary to integrate soil formation rates into the model calculations.

240 The sensitivity of the simulated erosion rates to soil thinning was assessed with the correlation (Pearson's  $r$ ) between soil truncation (i.e., the cumulative annual reduction in soil depth) and annual soil losses (here taken as the median of the Monte Carlo simulations per year). Soil profiles exhibiting a positive correlation ( $r > 0$ ,  $p < 0.00001$ ) were assumed to display an accelerating erosion feedback trend for the simulation period, whereas the ones with a negative correlation ( $r < 0$ ,  $p < 0.00001$ ) were assumed to display a deaccelerating feedback trend. The remaining profiles were not considered sensitive to truncation and were assumed to present a stable erosion progression. Of note, we imposed a more restrictive significance level in order to  
245 screen out the profiles with very slight responses to soil truncation, considering this is a fully controlled modelling experiment.

In order to understand the processes driving the soil erosion feedback system, we used a random forest analysis to rank the importance of model parameters for predicting the above-mentioned erosion trends (i.e., deaccelerating, stable, accelerating). In this case, the differences between soil parameter values for the  
250 initial and final timesteps were used to predict the trends for each of soil the profiles. All model simulations and statistical analyses were performed in R (R Core Team, 2022), and the code is available as supplementary material (Batista et al., 2022).

Importantly, we did not consider all potential changes to the modelled systems. That is, we did not consider any feedbacks between soil thinning and crop development, nor the effects of climate change on rainfall,  
255 temperature, and farming practices. Although we are aware such factors would likely have an impact on the model simulations, our aim here is to analyse the sensitivity of modelled soil losses to erosion-induced changes to soil properties. This involves making fixed assumptions about other system components. In addition, we would like to highlight that our model simulations should not be mistaken as projections of future erosion rates in Britain, due to all the above-mentioned reasons.

### 260 **3 Results**

From the 265 soil profiles in the UK SOILPITS database, 103 (39 %) displayed a significant correlation ( $p < 0.00001$ ) between soil truncation and annual soil losses. Within these truncation-sensitive profiles, 75 % displayed a deaccelerating feedback trend (Pearson's  $r < 0$ ) in erosion rates over the simulation period, whereas 25 % showed an accelerating one (Pearson's  $r > 0$ ). Figure 4 illustrates the typical behaviour of  
265 these trends using data from two representative profiles with similar topsoil but different subsoil properties at the beginning of the simulation.

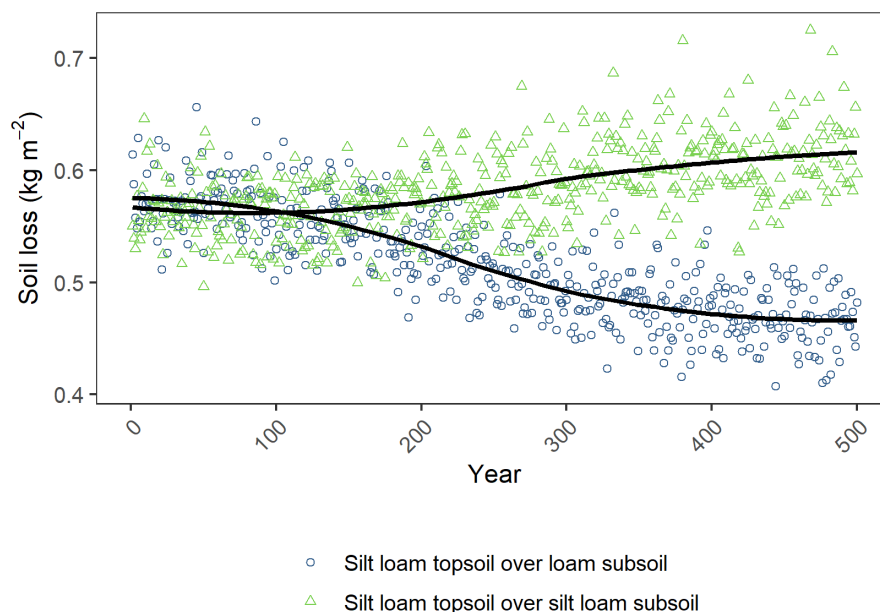


Figure 4. Soil erosion trends over 500 years of model simulations for two representative profiles from the UK SOILPITS dataset. Coloured symbols are the median of the simulations per year and the solid lines are local regression functions adjusted from the data.

The changes in erosion rates were mostly explained by alterations in soil texture. This is demonstrated in Fig. 5, which displays a random forest importance ranking for predicting the feedback trends in model outputs (i.e., deaccelerating, stable, accelerating). The random forest analysis described how soil erosion responses were highly influenced by variations in silt content and stone cover. Changes in soil moisture at field capacity had a lower impact on the modelled soil losses, whereas the simulated variations in bulk density had an almost null effect on model outputs (Fig. 5).



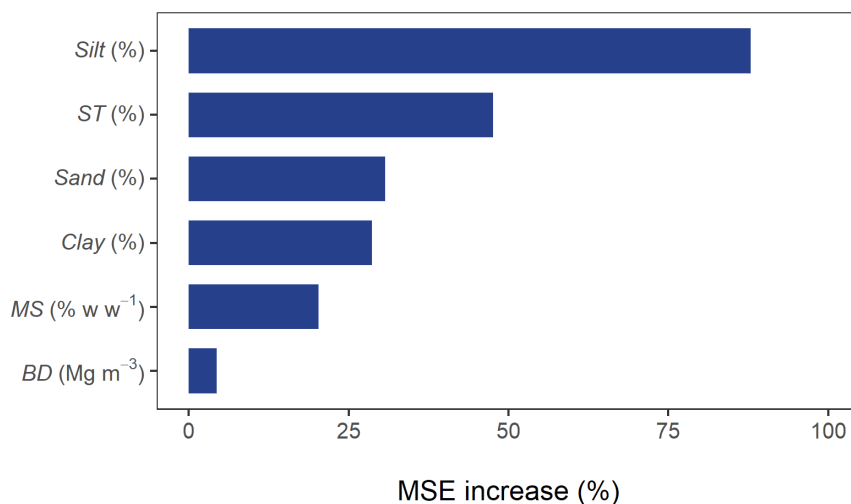


Figure 5. Random forest importance ranking for predicting the erosion trends for each soil profile (i.e., deaccelerating, stable, accelerating). Feature importance is represented by the relative increase of the mean squared error (MSE) of the random forest (i.e., how much removing the feature increased the prediction error).  
280

The soil erosion feedback system can be visualised comparing the difference in model parameter values with the variation in soil losses over 10-year rolling means (Fig. 6). Positive and negative changes in single parameter values did not yield consistent responses regarding the simulated soil losses (e.g., a 1 % decrease in sand content can lead to both accelerating and deaccelerating erosion rates over the rolling means).  
285 However, the direction of the changes in model parameters explains the feedback trends for the individual soil profiles (Fig. 6). For instance, the profiles with an accelerating erosion trend are characterised almost exclusively by increases in silt content within the 10-year rolling means. Contrarily, for the profiles in which soil losses show a deaccelerating trend over the whole simulation period have decreasing contents of silt and increasing stone cover within the rolling means. Less important parameters, such as bulk density and soil moisture at field capacity, display a scattered pattern, regardless of the erosion trends (Fig. 6).  
290

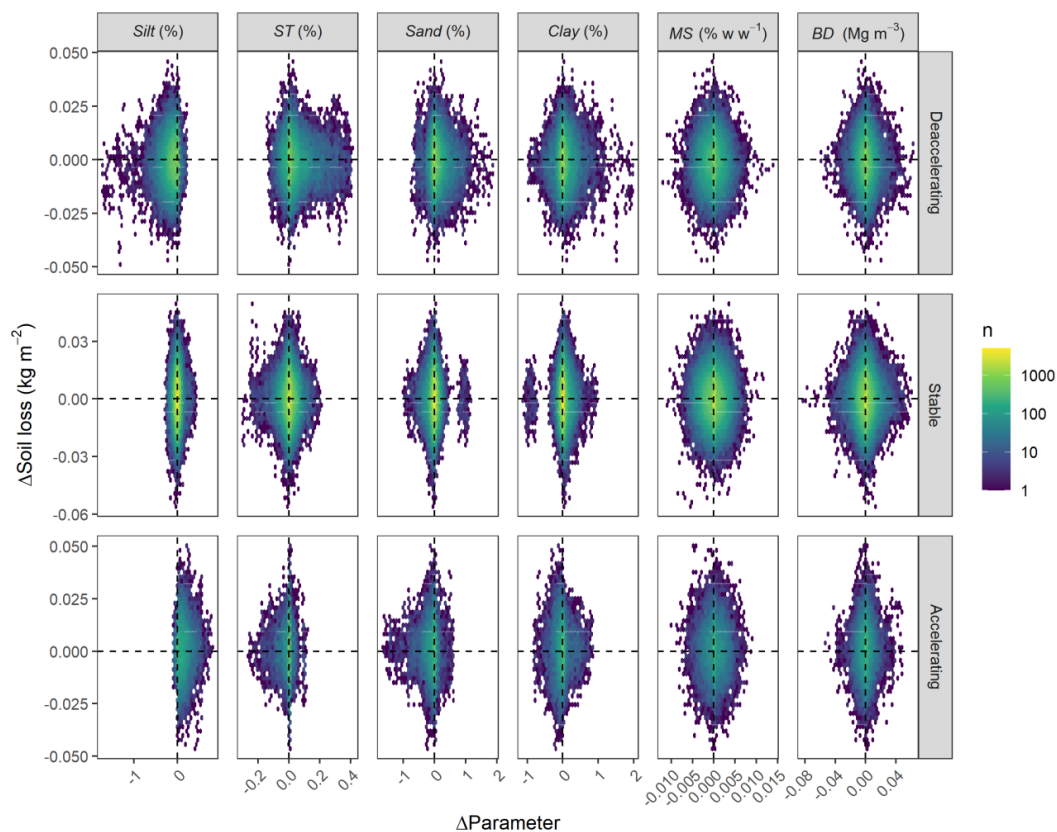


Figure 6. Hexagonal heatmaps relating the changes in model parameters to soil loss responses over 10-year rolling means for the soil profiles. Colours represent the number (n) of cases in each hexagon. Rows separate the profiles according to the erosion trend over the simulated period.



300

The main processes driving the soil erosion feedback system were particle detachment by raindrop impact and silt sediment supply ( $R^2 = 0.90$  and  $0.84$ , respectively; Fig. 7), while changes in runoff amounts, detachment by runoff, and runoff transport capacity had a narrow effect on the simulated soil losses ( $R^2 = 0.01$ ; Fig. 7). That is, only acute changes in discharge seem to have produced a sufficient response in detachment by runoff and in transport capacity to influence the net erosion rates (Fig. 7).

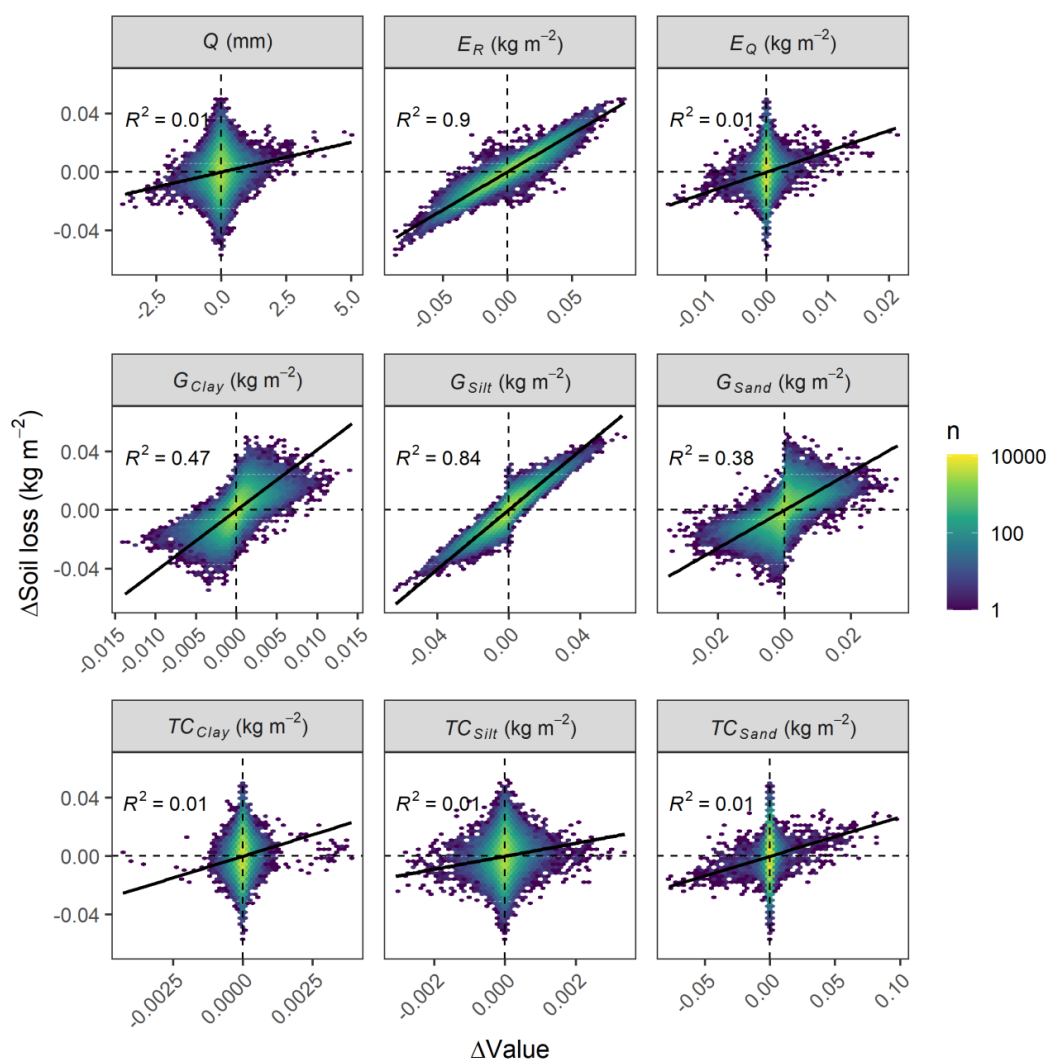
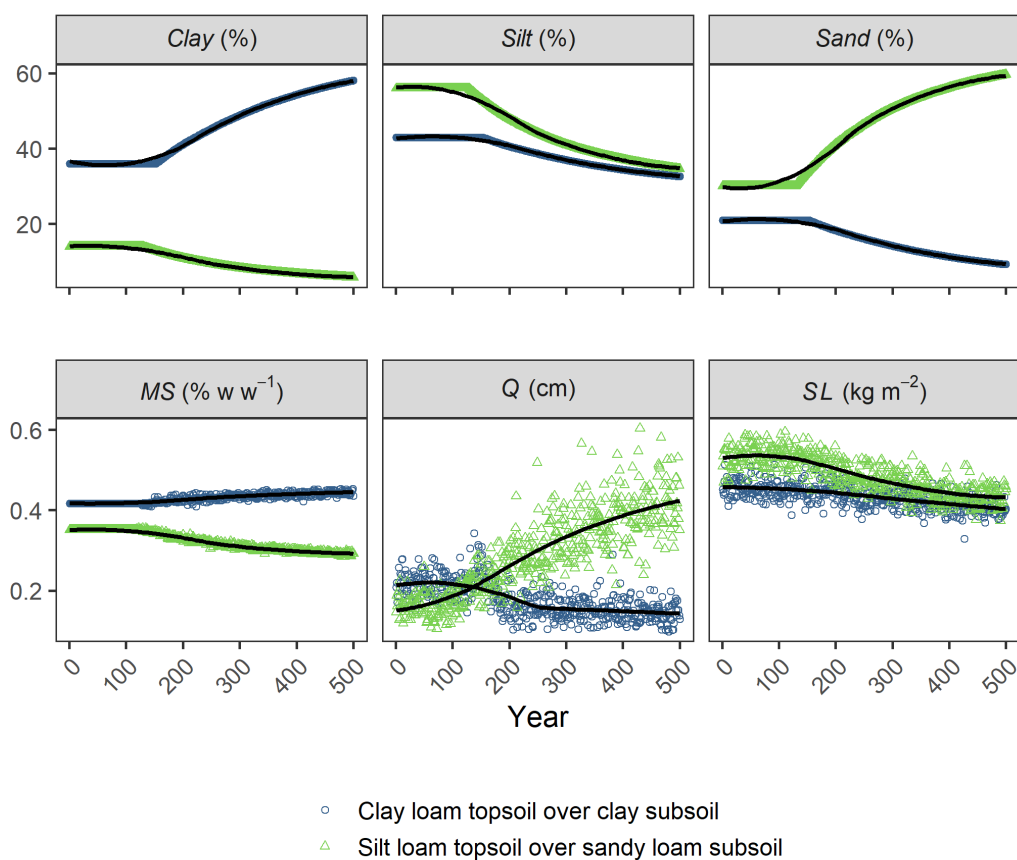


Figure 7. Hexagonal heatmaps and linear regression lines ( $p < 0.00001$ ) of the changes in soil loss over 10-year rolling means for the soil profiles. Fill colours represent the number (n) of cases in each hexagon.



305 Importantly, annual runoff depths and soil losses were correlated in only 31 (12 %) of the 265 soil profiles  
 (p < 0.00001). The positive correlations occurred for instance when the uprise of clayey subsurface horizons  
 led to a reduction in both runoff amounts (due to an increase in soil moisture storage capacity) and soil  
 detachment (Fig. 8). The negative correlations typically occurred in profiles with silty/loamy topsoils and  
 sandy substrata. As the silty material was removed, enriching the topsoil with sand, the erosion rates  
 declined, whereas runoff amounts increased due to a reduction in soil moisture at field capacity. However,  
 310 this increase in runoff was not sufficient to accelerate soil losses (Fig. 8).



315 Figure 8. Evolution of model parameters and simulated runoff and soil losses over 500 years for two soil profiles from the UK SOILPITS database. Annual runoff depth was converted to cm to improve the visualisation of the data. Coloured symbols are the median of the simulations per year and the solid lines are local regression functions adjusted from the data.



#### 4 Discussion

Our model simulations underline the strong interaction between current soil erosion dynamics and the erosion history of soil profiles. That is, the simulations demonstrate how different soils are likely to have contrasting responses to soil thinning, depending on the properties of the surface material, as well as those of the underlying soil horizons. In our database, most of the truncation-sensitive soil profiles presented deaccelerating feedback trends, which reflects both the characteristics of these soils and, importantly, our basic modelling assumptions.

For instance, as silt detachability in the MMMF model is assumed to be much higher than for other particle size fractions, silt was preferentially removed from the soil matrix. In addition, as silt contents typically remain stable or decrease in the subsurface horizons of the soil profiles in our database (Fig. 2), silt was often not replenished by the underlying substrata being mixed into the plough layer. Such behaviour is overall consistent with empirical observations of selective particle size removal by interrill erosion processes (Koiter et al., 2017) and the progressive coarsening of eroding surface soils (Parsons et al., 1991). However, it is worth highlighting that the soil detachability values used in MMMF have a limited empirical basis (Quansah, 1982), and the erodibility of the clay particles might be poorly described due to the neglect of other variables, such as aggregate stability (Morgan and Duzant, 2008).

The residual accumulation of rock fragments further contributed to the reduction in erosion rates for the profiles with a deaccelerating trend, as stone cover is assumed to armour the land surface and to reduce soil detachment. Specifically, even a small number of rock fragments in the soil matrix can disperse the overland flow and dissipate its energy, reducing rill incision and soil losses (Rieke-Zapp et al., 2007). Moreover, decreases in water erosion rates due to a residual increment of stone cover have previously been simulated by Govers et al. (2006), who warned, however, that the accumulation of rock fragments in arable soils depends on tillage practices. Notwithstanding, increases in rock fragment contents might also affect soil hydraulic conductivity and water holding capacity (Cousin et al., 2003), and therefore influence runoff formation. None of these potential interactions were represented in our model simulations, and might therefore warrant further scrutiny.

The soil profiles displaying an accelerating erosion trend were characterised by the presence of sandy or loamy surface horizons over a siltier substratum, which successively supplied the plough layer with readily erodible material as the original topsoil was removed by erosion. Moreover, these profiles were defined by the absence of a surface stone cover and by subsoil horizons with very limited amounts of rock fragments. Although accelerating erosion trends were relatively infrequent in our dataset, such behaviour might be



expected in soils with incrementing silt contents in their C horizons, which are common, for instance, where loess is the parent material (Finke, 2012; Świtoniak et al., 2016).

Moreover, potential accelerating erosion trends might have been under-detected by the model simulations, as we did not consider how truncation can decrease the soil moisture storage capacity due to a reduction in soil depth, and how this might affect runoff generation (Dunne and Black, 1970; Morgan et al., 1984). That is, as soils become shallower, excess saturation overland flow might increase, depending on the permeability of the bedrock or the presence of an impeding horizon (Beven, 2012; Moraes et al., 2010). We did not consider these processes in our simulation due to the absence of an explicit soil thickness parameter in the MMMF equations and the lack of data regarding the permeability of the soil profiles parent materials.

Furthermore, very different runoff responses to soil truncation can be expected in areas where infiltration excess is the dominant overland flow mechanism. While saturation excess is common under British edaphoclimatic conditions, most subhumid and semiarid zones are prone to infiltration excess runoff formation, which is a process primarily controlled at the soil surface (Smith and Goodrich, 2005). Under such circumstances, erosion-induced changes to topsoil properties might have an even greater interaction with runoff generation. In particular, soil crusting slows down infiltrability and rapidly increases the overland flow, leading to greater soil losses (Le Bissonnais, 2016; Fiener et al., 2008; Veihe et al., 2001). As the development of soil crusts is influenced by soil texture and organic carbon content (Fiener et al., 2011), the truncation-induced changes we have simulated would likely alter the susceptibility of surface soils to crusting and, consequently, to infiltration excess runoff formation. Another caveat in the model structure worth highlighting is that, differently to what is exhibited in Fig. 8, an uprise of subsurface clayey material might in fact increase infiltration excess overland flow, due to the lower infiltrability and saturated hydraulic conductivity of heavy-textured soils (Hao et al., 2020), which are also more susceptible to compaction, depending on their mineralogy (Bonetti et al., 2017; Hamza and Anderson, 2005).

In addition, accelerating erosion responses to soil truncation might have been more frequent if we assumed an increase in topsoil erodibility due to the lower aggregate stability and looser structure of the carbon depleted subsurface material being incorporated into the plough layer (Le Bissonnais, 2016; Doetterl et al., 2016; Tanner et al., 2018). That is, as the soil detachability coefficients from MMMF do not take soil organic carbon into account, the sensitivity of topsoil erodibility to soil truncation was likely downplayed. Our model simulations may have particularly underestimated erosion responses to soil thinning for the profiles which displayed an accumulation of sand and a depletion in clay and silt contents. This progressive coarsening should lead to lower soil water availability, and therefore, lower soil cover, lower crop biomass production, and less organic carbon input from plants. As sandier soils already have less carbon stabilisation



mechanisms (Doetterl et al., 2016), this would lead to even greater truncation-induced depletions in soil  
380 organic carbon and therefore to increases in erodibility (Auerswald et al., 2014; Fernández and Vega, 2018).  
In general, as organic carbon was only an indirect model input via the PTFs for estimating bulk density and  
soil moisture at field capacity, the interplays between soil thinning, soil organic matter, and soil erodibility  
were likely underrepresented here.

Although not all the complex interactions between soil erosion and soil thinning could be described in our  
385 simulations, we can identify where more empirical evidence would help constrain our modelling  
assumptions. For instance, investigating how truncation affects the aggregate stability of surface soils (due  
to changes in soil texture, mineralogy, and organic carbon dynamics) might be an important step in order  
to further understand the feedbacks between erosion and soil thinning. Interactions between soil truncation,  
water availability to plants, and crop growth – and how these could in turn reduce soil cover and organic  
390 carbon input – might also warrant further investigations. Similarly, the responses of different runoff  
generation mechanisms to soil thinning and erosion-induced changes to soil properties should be beneficial  
to increase our understanding of the erosion feedback system.

## 5 Conclusions

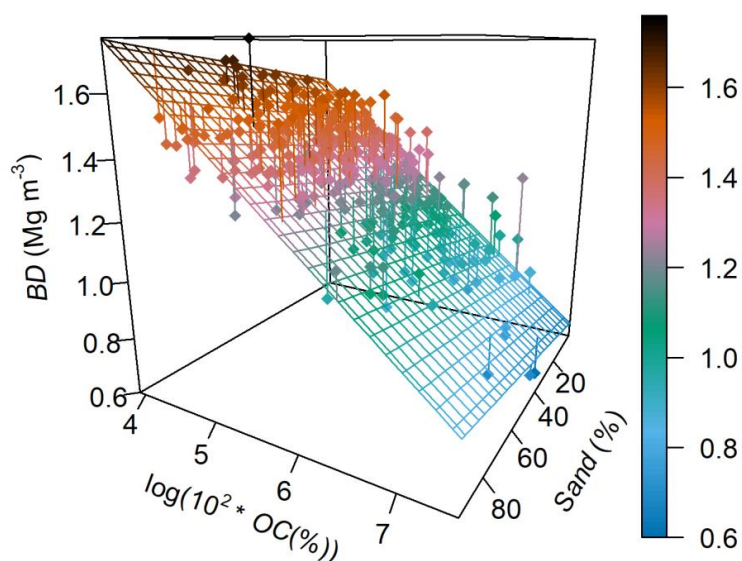
Here we explored the soil erosion feedback system in 265 agricultural soil profiles in the United Kingdom.  
395 In particular, we simulated how selective erosion processes and the incorporation of different subsoil  
horizons into the plough layer affected the erodibility of surface soils. We further analysed how these  
processes could change erosion rates during a 500-year period. We found that i) soil erosion rates in 39 %  
of the soil profiles were sensitive to soil truncation, ii) that most of these truncation-sensitive profiles (75  
) displayed a deaccelerating trend, and iii) that changes in soil texture and stone cover were the main  
400 drivers of the modelled soil erosion feedbacks loops. Importantly, we found that different soils had  
drastically different simulated responses to soil truncation, depending on the properties of the surface  
material as well as those of the underlying soil horizons.

Ultimately, our findings highlight the dynamic nature of the soil as a three-dimensional body. That is, even  
the so-called intrinsic properties of surface soils might change in a matter of decades in areas under  
405 accelerated erosion rates. In specific, erosion-induced changes to soil properties can have a significant  
impact on the rates with which soils are eroded, which in turn affects the calculation of soil lifespans and  
model-based erosion projections. To date, this soil erosion feedback system has been largely overlooked in  
soil erosion models, which might have led to spurious estimates of long-term erosion rates. Therefore,  
understanding how erosion-induced changes to soil properties reverberate with erosion itself will be crucial



410 for improving long-term model predictions, investigating the resilience of different soils to erosion  
disturbances, and for developing appropriate soil conservation strategies for a changing world.

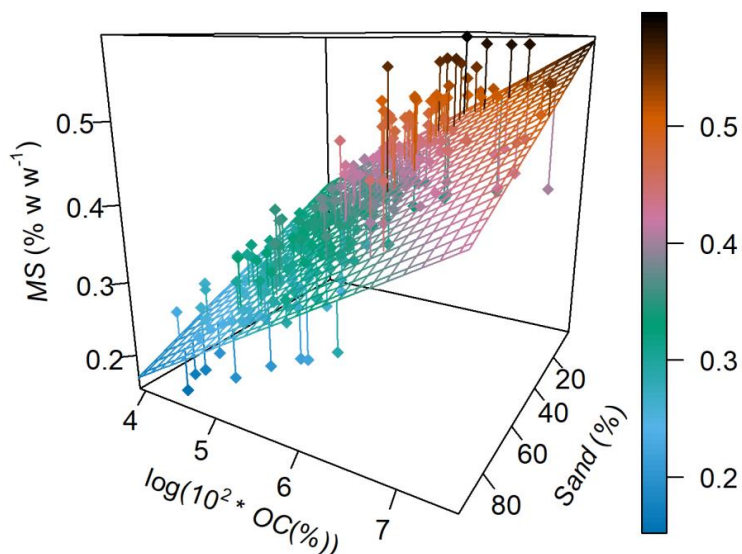
## 6 Appendix A



$$BD = 2.58 + 0.002 * Sand - 0.26 * \log(10^2 * OC)$$
$$R^2 = 0.65, p < 0.00001$$

415 Figure A1. Pedotransfer function for estimating bulk density ( $BD$ ) as a function of sand and organic  
carbon ( $OC$ ) content. The regression was fit using only the data for the A horizons in the 265 agricultural  
soil profiles from the UK SOIL PITS dataset used in this study.





$$MS = 0.07 - 0.002 * Sand + 0.07 * \log(10^2 * OC)$$
$$R^2 = 0.70, p < 0.00001$$

Figure A2. Pedotransfer function for estimating soil moisture at field capacity ( $MS$ ) as a function of sand and organic carbon ( $OC$ ) content. The regression was fit using only the data for the A horizons in the 265  
420 agricultural soil profiles from the UK SOIL PITS dataset used in this study.

### 7 Code availability

The model code is available online at: <https://doi.org/10.5281/zenodo.6393134>.

### 8 Data availability

The soil profile data used in this research is restricted under licence. For further information on data  
425 accessibility, please contact [nsridata@cranfield.ac.uk](mailto:nsridata@cranfield.ac.uk).

### 9 Author contribution



All authors were part of the conceptualisation of this research. PVGB wrote the model code and the manuscript with contributions from all authors.

## 10 Competing interests

430 PF is a topical editor for SOIL. The authors have no other competing interests to declare.

## 11 Acknowledgments

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435 University, and a Global Challenges Research Fund (GCRF) project entitled: “Saprolite erosion and the fate of heavy metals: pioneering UAV-SfM as a community mapping tool.”

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440 preparing Figure 1 of this manuscript.



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