An approach for projecting the timing of abrupt winter Arctic sea ice loss

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Abstract. Abrupt and irreversible winter Arctic sea-ice loss may occur under anthropogenic warming due to the collapse 1 2 disappearance of a sea-ice equilibrium at a threshold value of CO_2 , commonly referred to as a tipping point. Previous work has been unable to conclusively identify whether a tipping point in winter Arctic sea ice exists because fully-coupled climate 3 models are too computationally expensive to run to equilibrium for many CO_2 values. Here, we explore the deviation of sea ice 4 from its equilibrium state under realistic rates of CO_2 increase to demonstrate for the first time how a few time-dependent CO_2 5 6 experiments can be used to predict the existence and timing of sea-ice tipping points without running the model to steady-state. 7 This study highlights the inefficacy of using a single experiment with slow-changing CO_2 to discover changes in the sea-ice steady-state, and provides an a novel alternate method that can be developed for the identification of tipping points in realistic 8 9 climate models.

10 1 Introduction

11 The Arctic is warming at a rate at least twice as fast as the global mean with profound consequences for its sea ice cover.

- 12 Summer sea Sea ice is already exhibiting rapid retreat with warming(Nghiem et al., 2007; Stroeve et al., 2008; Notz and Stroeve, 2016)
- 13 , especially in the summertime, (Comiso and Parkinson, 2004; Nghiem et al., 2007; Stroeve et al., 2008; Notz and Stroeve, 2016; Stroeve
- 14 shortening the time that socioeconomic and ecological systems have to adapt. These concerns have motivated a large body
- 15 of work dedicated to both observing present-day sea ice loss (Kwok and Untersteiner, 2011; Stroeve et al., 2012; Lindsay
- 16 and Schweiger, 2015; Lavergne et al., 2019) and modeling sea ice to understand whether its projected loss is modulated by a
- 17 threshold-like or "tipping point" behavior. Abrupt loss or a tipping point in of Arctic sea ice could be driven by local positive
- 18 feedback mechanisms (Curry et al., 1995; Abbot and Tziperman, 2008; Abbot et al., 2009; Kay et al., 2012; Leibowicz et al., 2012; Burt et al., 2012; Curry et al.,
- 19 (Curry et al., 1995; Abbot and Tziperman, 2008; Abbot et al., 2009; Kay et al., 2012; Leibowicz et al., 2012; Burt et al., 2016; Feldl et al.
- 20 , remote feedback mechanisms that increase heat flux from the mid-latitudes (Holland et al., 2006; Park et al., 2015)(Holland et al., 2006; P
- 21 , or by the natural threshold corresponding to the seawater freezing point (Bathiany et al., 2016). Such a tipping point is
- 22 mathematically understood as If such an abrupt loss is caused by irreversible processes (typically, strong positive feedback mechanisms as c
- 23 , it is referred to here as a "tipping point". A tipping point in the sense used here is a change in the number or stability of steady-
- 24 state solutions (Ghil and Childress, 1987; Strogatz, 1994) (Ghil and Childress, 1987; Strogatz, 1994) as a function of CO₂ and

is also known as a "bifurcation bifurcation. We note that some of the climate literature uses "tipping points" in a more general 25 sense of a relatively rapid change (e.g., Lenton, 2012). While most studies have concluded that there is no tipping point during 26 the transition from perennial to seasonal ice cover (i.e., during the loss of *summer* sea ice), the existence of a tipping point 27 28 during the loss of *winter* sea ice (transition to year-round ice-free conditions) continues to be debated in the literature (Eisenman, 2007; Eisenman and Wettlaufer, 2009; Notz, 2009; Eisenman, 2012), with. Wagner and Eisenman (2015) showed that a 29 winter tipping point disappeared from a simple model of sea ice with no active atmosphere when a longitudinal dimension was 30 added. On the other hand, other literature (e.g., Abbot and Tziperman, 2008; Hankel and Tziperman, 2021) has demonstrated 31 the importance of atmospheric feedbacks, not included in the model of Wagner and Eisenman (2015), in inducing winter sea 32 33 ice tipping point. Furthermore, three out of seven GCMs-fully-complex Global Climate Models (GCMs) that lost their winter sea ice completely in the CMIP5 Extended RCP8.5 Scenario demonstrating an abrupt change that qualitatively looks like 34 showed a very abrupt change in winter Arctic sea ice resembling a tipping point, and may be related to a bifurcation (Hezel 35 et al., 2014; Hankel and Tziperman, 2021). However, given the projected rapid changes to CO₂ in the coming centuries and 36 the slower response of the climate system, we do not expect future sea ice to be fully equilibrated to the CO_2 forcing at a given 37 38 time, making the standard steady-state tipping point analysis challenging. Thus, we are interested in projecting the timing of 39 our first goal is to understand abrupt winter Arctic sea ice changes under changes—which may or may not be due to tipping points—under rapidly changing CO₂ forcing, when the standard steady-state tipping point analysis is not applicable where sea 40 ice is not at equilibrium. 41 Tipping points imply a bi-stability (meaning that sea ice can take on different values for the same CO₂ concentration), 42 43 and hysteresis — an irreversible loss of sea ice even if CO_2 is later reduced. The computational efficiency of simple models allowed studies using them to calculate the region of winter sea-ice bi-stability by running Bi-stability (and therefore tipping 44 45 points) can be tested for by running model simulations to steady-state at many different CO₂ values, which is not possible with expensive computationally inefficient in expensive, state-of-the-art Global Climate Models (GCMs)GCMs. GCM stud-46

47 iestherefore, therefore, tend to use a single experiment with very gradual CO_2 increases and decreases (Li et al., 2013) or even 48 a faster CO_2 change (Ridley et al., 2012; Armour et al., 2011), assuming and look for hysteresis in sea ice that would imply the 49 existence of a tipping point. These studies implicitly assume that such a run should approximate the behavior of the steady-state

50 at different CO_2 concentrations. However, Li et al. (2013) further integrated two apparently bi-stable points and found that they

51 equilibrated to the same value of winter sea ice: there was no "true" bi-stability at these two CO_2 concentrations, the sea ice

52 was simply out of equilibrium with the CO_2 forcing. This calls into question the current use of time-changing CO_2 runs to

53 study the bifurcation structure of sea ice.

In light of the difficulties in using <u>climate</u> model runs with time-changing CO_2 (hereafter "transient runs")for identifying tipping points, we identify a need, the first goal of this work is to understand the relationship between these transient runs and the steady-state value of sea ice as a function of CO_2 in systems with and without bifurcations (since the existence of a bifurcation in winter sea ice remains unknown), and the second goal is to develop a new efficient method for the identification of tipping points from transient runs. Theoretical work in dynamical systems (Haberman, 1979; Mandel and Erneux, 1987;

59 Baer et al., 1989; Tredicce et al., 2004) and studies related to bi-stability in the Atlantic Meridional Overturning Circula-

- tion (Kim et al., 2021; An et al., 2021) have examined systems with tipping points when the forcing parameter (CO₂ in our 60 case) changes in time at a finite rate, and. They found that as the forcing parameter passes the bifurcation point, the system 61 continues to follow the old equilibrium solution for some time before it rapidly transitions to the new one. This Specifically, 62 63 (Kim et al., 2021; An et al., 2021) find that the width of the hysteresis loop of AMOC is altered by the rate of forcing changesthis phenomenon is referred to as "rate-dependent hysteresis". This rate-dependence occurs in their case in a system that also 64 has bi-stability and hysteresis in the equilibrium state. This type of analysis has, to our knowledge, not yet been applied in the 65 context of winter sea ice loss under time-changing CO₂ concentrations, nor compared in systems with and without a bifurcation 66 67 (that is, with and without an equilibrium hysteresis). 68 In order to analyze how the hysteresis curve of sea ice under time-changing forcing relates to the steady-state behavior of
- sea ice, we run a simple physics-based model of sea ice (Eisenman, 2007), configured in three different scenarios: with a large 69 region CO_2 range of bi-stability, a small region range of bi-stability, and no bi-stability in the equilibrium. These three scenarios 70 71 span the range of possible behaviors of winter sea ice in state-of-the-art climate models. Each case is run with different rates of CO₂ increase (ramping rates). We use results from this model and from an even simpler standard 1D dynamical system 72 73 to demonstrate that the convergence of the transient behavior (under time-changing forcing) to the equilibrium behavior is 74 very slow as a function of the ramping rate of CO_2 . In other words, even climate model runs with very slow-changing CO_2 forcing may simulate sea ice that is considerably out of equilibrium near the period of abrupt sea ice loss. Finally, we propose 75 an a novel approach for uncovering the underlying equilibrium behavior — and thus the existence and location of 76 77 tipping points—in comprehensive models where it is computationally inefficient infeasible to simulate steady-state conditions 78 for many CO_2 values. Such a method is important given the model-dependent nature of winter sea ice tipping points discussed above; uncovering the existence of sea ice tipping points in GCMs, which are the most realistic representation of Arctic-wide 79 80 sea ice behavior that we have, is the next step toward understanding whether such tipping points exist in the real climate system. Our goal has some parallels to that of Gregory et al. (2004), who used un-equilibrated GCM runs to deduce the equilibrium 81 82 climate sensitivity when fully-equilibrated runs were computationally infeasible.
- Some GCMs exhibit a tipping point As mentioned above, some GCMs exhibit an abrupt change in winter sea ice 83 that may be a tipping point, and others don't do not (Hezel et al., 2014; Hankel and Tziperman, 2021). The reasons are 84 85 likely complex and likely involve numerous differences in parameters and parameterizations. It is not obvious how to modify parameters in a single GCM to display all of these different behaviors. Therefore, we choose to use an idealized model of sea 86 ice where we can directly produce different bifurcation behaviors to address our second goal and answer the question: is it 87 possible to identify the CO₂ at which tipping points occur without running the model to a steady state for many CO₂ values? 88 Answering such a question in a simple model is an obvious prerequisite to tackling the problem of identifying climate bi-89 90 stability in noisy, high-dimensional, GCMs. In order to perform this analysis for each of the three scenarios mentioned above, 91 we modify the strength of the albedo feedback via the choice of surface albedo parameters. The albedo values used here to generate the three scenarios are not meant to reflect realistic albedo values, but rather allow us to represent in a single model 92 93 the range of sea ice equilibria behaviors that may exist in different GCMs. We, therefore, follow in the footsteps of previous studies (e.g., Eisenman, 2007) that have also changed parameters (the latent heat of fusion) outside of their physically relevant 94

95 regime in order to understand *summer* sea ice bifurcation behavior; here we follow the same approach to understand when a 96 *winter* sea ice bifurcation can be detected without running an expensive climate model to steady-state.

97 2 Methods

98 2.1 Sea ice model

The Eisenman model sea ice model used follows Eisenman (2007) almost exactly and its key features are depicted schematically 99 in Figure 1. The model contains four state variables: sea ice effective thickness (V, which is volume divided by the area of the 100 101 model grid box), sea ice area (A), sea ice surface temperature (T_i), and mixed layer temperature (T_{ml}) for a single box representing the entire Arctic. The Subsequent versions of this sea ice model have been used in Eisenman and Wettlaufer (2009) 102 Eisenman (2012), and Wagner and Eisenman (2015). Those versions are derived from the model used here, making a few 103 further modest simplifications (using a hyperbolic tangent function for surface albedo, assuming the ice surface temperature is 104 in a steady state, combining all prognostic variables into one, enthalpy) that do not affect the qualitative behavior of the model 105 (i.e., the nature of summer and winter sea ice bifurcations). We choose to implement the earlier model because it explicitly 106 represents the key physical variables of ice volume, area, ocean temperature, and ice temperature as prognostic variables — 107 as opposed to combining them all into a single enthalpy - and thus provides more transparency and interpretability. We, 108 therefore, do not expect our results to change if we use any of the later model versions. 109 In the model, the atmosphere is assumed to be in radiative equilibrium with the surface, and the model is forced with a 110 seasonal cycle of insolation, of poleward heat transport atmospheric heat transport from the mid-latitudes, and of local optical 111 thickness of the atmosphere, which represents cloudiness. The Sea ice growth and loss are primarily determined by the heat 112 113 budget at the bottom of the ice and are therefore set by the balance between ocean-ice heat exchanges, and heat loss through the ice to the atmosphere. When conditions for surface melting are met (when the ice surface temperature is zero and net fluxes 114 on the ice are positive), all surface heating goes into melting ice and the surface albedo of the ice is set to the melt pond albedo. 115 116 The ocean temperature is affected by shortwave and longwave fluxes in the fraction of the box that is ice-free, and by ice-ocean heat exchanges. When the ocean temperature reaches zero, all additional cooling goes into ice production while the ocean 117 118 temperature remains constant. The full equations of the sea ice model can be found in the original paper (Eisenman, 2007) 119 and in the online Supporting Information; here, we highlight a few minor ways in which our implementation differs. First, 120 for simplicity, we do not model leads, which in the original model were represented by capping the ice fraction at 0.95 rather than 1. Second, we use an approximation to the seasonal cycle of insolation (Hartmann, 2015) using a latitude of 75N. The 121 atmospheric albedo is set to 0.425 to produce the same magnitude of the seasonal cycle as in the original model of Eisenman 122 (2007).123

124 2.2 Setup of simulations

125 In our transient-forcing scenarios (described below), we vary CO_2 in time which affects the prescribed near-surface atmospheric

mid-latitude temperature ($T_{\rm mid-lat}$) and the atmospheric optical depth (N)-(, see Supporting Information). Specifically, we increase the annual mean of $T_{\rm mid-lat}$ by 3 °C per CO₂ doubling and N by a ΔN that corresponds to 3.7 W/m² per doubling.

128 All model parameters are as in (Eisenman, 2007) Eisenman (2007) except as mentioned below.

We configure the model in three different scenarios that yield a wide CO_2 range of bi-stability in winter sea ice (Scenario 1), a small range of bi-stability in winter sea ice (Scenario 2), and no bi-stability in winter sea ice (Scenario 3). We do so by modifying the strength of the ice-albedo feedback by changing the albedos of bare ice (α_i), melt ponds (α_{mp}), and ocean (α_o), as listed in Table S1.

In each of the three scenarios, we tune the model (by adjusting the mean and amplitude of the atmospheric optical depth) to 133 134 roughly match the observed seasonal cycle of ice thickness under pre-industrial CO₂ ($\sim 2.5-3.7$ m, Eisenman, 2007). We then 135 run each scenario with multiple CO₂ ramping rates (expressed in "years per doubling") with an initial stabilization period (fixed 136 pre-industrial CO_2), a period of exponentially increasing CO_2 concentration (which corresponds to linearly increasing radiative forcing), another period of stabilization at the maximum CO₂, a period of decreasing CO₂, and a final period of stabilization at 137 the minimum CO_2 value (see Supplemental Figure S2). Scenarios 2 and 3 are ramped to higher final CO_2 values than Scenario 138 1 so that they lose all their sea ice. We also directly calculate the steady-state behavior of the sea ice (as done in the original 139 study) by running many simulations with fixed CO_2 values until the seasonal cycle of all the variables stabilizes. Because we 140 141 expect multiple equilibria (which could be ice-free, seasonal ice, or perennial ice) at some CO_2 values in Scenarios 1 and 2, we run these steady-state simulations starting with both a cold (ice-covered) and a warm (ice-free) initial condition in order to find 142 these different steady-states. In the ice-free initial condition runs, the ice-albedo feedback will still play an important role if the 143 temperature cools sufficiently for ice to develop. At CO_2 values for which the sea ice is bistable bi-stable, the ice-free initial 144 condition evolves to a perennially ice-free steady-state, and the ice-covered initial condition evolves to a seasonally ice-covered 145 146 steady-state (seen by the dotted and dashed lines respectively in Figs. 1a and 1e²a and 2c).

147 2.3 Cubic ODE

It turns out the The main points we are trying to make about the transient versus equilibrium behavior of winter sea ice near a tipping point are not unique to the problem of winter sea ice, and in order to demonstrate this, we use the simplest mathematical model that can display tipping points, following other studies that have also used such simple dynamical systems (Ditlevsen and Johnsen, 2010; Bathiany et al., 2018; Ritchie et al., 2021; Boers, 2021). The cubic ODE used, while much simpler than the sea ice model above, has some of the key characteristics of the sea ice system (it is a non-autonomous system due to the time-depending forcing and has saddle-node bifurcations), which allows for direct comparison between the two models. The ODE equation,

155
$$\frac{dx}{dt} = -x^3 + \delta x + \beta(t), \qquad \beta(t) = \beta_0 + \mu t, \tag{1}$$

contains a time-changing forcing parameter, $\beta(t)$ mimicking the effects of CO₂ in the sea ice model. We consider this differ-156 ential equation in three scenarios, paralleling those used with the sea ice model: in Scenario 1, $\delta = 5$ leading to a wide region 157 of bi-stability; in Scenario 2, $\delta = 1$ leading to a narrow region of bi-stability, and finally, in Scenario 3, $\delta = 0$ leading to a 158 mono-stable system. The different values of δ , therefore, produce the same three scenarios that were achieved in the sea ice 159 model by modifying the strength of the ice-albedo feedback. We mimic the hysteresis experiments of the sea ice model with 160 a sequence of ramping up and ramping down (using different ramping rates, μ) with values of β ranging from -10 to 10 to 161 sweep the parameter space that contains the bifurcations. We calculate the steady-states with fixed values of β ($\mu = 0$), starting 162 163 with both a positive and a negative initial condition of x to yield two stable solutions when these exist.

We want to calculate the upper and lower CO_2 values of the hysteresis region in runs with time-changing (i.e., transient) CO₂ forcing. We do so by calculating the CO₂ value at which the March sea ice area drops below a critical threshold (50% ice coverage; results are insensitive to the specific value used) during increasing and decreasing CO_2 integrations: we denote these CO₂ values CO_2^i and CO_2^d , respectively (see Supplemental Figure S9). The difference between CO_2^i and CO_2^d is referred to below as the "transient-hysteresis width" of the rate-dependent hysteresis whether an equilibrium hysteresis exists or not; this width approaches the width of bi-stability at very slow ramping rates.

170 2.4 Predicting A new method for predicting the CO₂ of the sea ice tipping point

171 One of our main goals (see Introduction) is to efficiently estimate the equilibrium behavior of sea ice, including the location of 172 tipping points, without running the model to a steady state for many CO_2 values. This would show that such estimation could be calculated for GCMs where tipping points cannot be detected using steady-state runs due to their computational cost. In 173 order to estimate the values of CO_2^i and CO_2^d that would have occurred for an infinitely slow ramping rate (in other words, the 174 range of CO_2 for which there is bi-stability) without having to run a model to equilibrium for all values of CO_2 forcingusing 175 only the transient runs, we fit a polynomial of the form $f(x) = mx^{c} + b$ to CO_{2}^{i} and CO_{2}^{d} as functions of the ramping rate 176 x. Because c is negative, the fitted parameter b represents the prediction of CO_2^i and CO_2^d at infinitely slow ramping rates, 177 i.e., in the steady state. We also calculate the uncertainty on the fitted parameter b by block-bootstrapping to account for auto-178 correlation; see Supporting Information. Other fits to CO_2^i and CO_2^d as a function of ramping rates, such as an exponential 179 function $f(x) = a + b \exp(-cx)$ could in principle be used, although we found the fit to be less good in our case. 180

181 3 Results

In the following three subsections, we discuss the behavior of the sea ice model and the cubic ODE under time-changing forcing, the relationship of the transient and equilibrium behaviors, and a method that we propose for inferring the existence and location of tipping points from the transient behavior. Equilibrium hysteresis refers here to the path-dependent solution of a variable due to bi-stability and a bifurcation in the steady-state (in other words, the loop traced by the steady-state solutions). The term "rate-dependent hysteresis" (An et al., 2021; Manoli et al., 2020) describes hysteresis loops that appear

187 in time-changing forcing runs (rather than in the steady state) and that depend on the rate of forcing change. In our analysis

188 "rate-dependent hysteresis" applies to both systems with and without equilibrium hysteresis: it refers to any differences in the

189 results for increasing vs. decreasing CO_2 simulations of sea ice that are altered by the rate of CO_2 change.

190 3.1 Transient response of Arctic winter sea ice to time-changing CO₂

191 Our goal in this section is to understand the relationship of winter sea ice forced with time-changing CO₂ to its equilibrium state,

192 both in cases with and without a sea ice tipping point. In Figs. 1b,d,f 2a,c,e, we plot the results of running all three scenarios

193 (wide range of bi-stability (Scenario 1), narrow range of bi-stability (2), and no bi-stability (3)) under time-changing (transient)

and fixed CO₂ values. In all scenarios, the experiments run with time-changing CO₂ exhibit transient-rate-dependent hysteresis;

195 the transient hysteresis width (lower horizontal gray bar in Fig. $\frac{1a}{2a}$) is larger for faster ramping rates (Figs. $\frac{1a}{2a}$, c, e). For

196 Scenarios 1 and 2, which have a region of bi-stability and equilibrium hysteresis (upper gray bar in Fig. 2a), this corresponds to

197 a widening from the equilibrium hysteresis (that would exist even with infinitely slow ramping rates), while in Scenario 3, this

198 hysteresis occurs only in transient simulations and is due to the inertia in the system (the sea ice can't respond instantaneously

199 to forcing changes). In Scenarios 1 and 2, whose equilibrium solutions (dashed and dotted black lines in Fig. +2) have a tipping

200 point and therefore an infinite gradient of sea ice thickness vs. CO₂, the faster ramping rates also lead to more gradual (and

201 finite) gradient of sea ice thickness vs. CO₂. The transient

202 The rate-dependent hysteresis loops across all scenarios at fast enough ramping rates (loops composed of the darkest blue 203 and darkest red) are qualitatively similar in shape, despite their different underlying steady-state structures. This similarity indicates that from a single hysteresis run with time-changing CO_2 we cannot discern whether the underlying Arctic winter 204 sea ice equilibrium behavior has a region of bi-stability or not, nor how wide the region of true bi-stability is. In particular, a 205 single hysteresis loop found from a time-changing forcing simulation would always overestimate the width of bi-stability if 206 it was assumed to represent a quasi-steady state. This result demonstrates that the apparent transient sea ice hysteresis loop 207 found by Li et al. (2013) could be due to a system with or without a true hysteresis (i.e. bi-stability in the steady-state 208 209 behavior), consistent with their analysis. without an equilibrium hysteresis, as they suggest, or due to a system with a narrower equilibrium hysteresis than the one implied by their transient simulation. 210

211 The robustness and generality of the above results of the sea ice model are now demonstrated by showing that the simpler

212 ODE (eqn. We now discuss the behavior of the simple cubic ODE (Eqn. 1) under similarly time-changing forcing. Previous

213 work in the dynamical systems literature (e.g., Haberman, 1979; Mandel and Erneux, 1987; Baer et al., 1989; Breban et al., 2003; Tredicce

214 has examined a variety of simple systems to understand the nature of bifurcations in the presence of a time-changing ("drifting"

215 or "transient") forcing parameter. In the climate literature as well (e.g., Ditlevsen and Johnsen, 2010; Bathiany et al., 2018; Ritchie et al., 20

216 , idealized dynamical systems similar to our Eqn. 1 have been used to understand the predictability of tipping points in the

217 presence of noise, and the ability to recover from such tipping points ("overshoot" scenarios). These works, as well as the

218 AMOC study of An et al. (2021), found that a system with a bifurcation that is run with a time-changing forcing parameter

219 can follow a given equilibrium value beyond the bifurcation value of the forcing parameter before undergoing the tipping point

220 transition to the new equilibrium value. This is consistent with the out-of-equilibrium behaviors we find for sea ice in Scenarios

1 and 2. To our knowledge, the simple ODE used here has not yet been analyzed with our specific goal in mind: to compare

- the shape of rate-dependent hysteresis loops in generic dynamical systems both with and without bifurcations, and to address
- the question of whether the equilibrium behavior can be inferred from the rate-dependent behavior of such systems.

To address these two goals, we configure Eqn. 1) produces the same behavior. The 1D ODE is also configured analogously 224 225 to the sea ice model in three scenarios with wide bi-stability (Scenario 1), narrow bi-stability (Scenario 2), and no bi-stability (Scenario 3) and force it with a time-changing forcing parameter. In Figs. 1b2b,d,fwe see transient hysteresis in all scenarios, 226 we see that the three scenarios with similar dynamics (but different equilibrium structures) all display rate-dependent hysteresis, 227 similar to the result from the sea ice model. Specifically, even when there is only one stable equilibrium solution in both models 228 229 (Scenario 3, panels e and f), there is still a narrow region of transient rate-dependent hysteresis. Thus, we find that the lack 230 of distinction in transient hysteresis loops between systems with and without bifurcations and the widening of the hysteresis loop with increased forcing parameter ramping rate appear to be robust results across these dynamical systems, inability to tell 231 if rate-dependent hysteresis in Arctic winter sea ice is accompanied by an underlying equilibrium hysteresis appears to be a 232

- 233 generic feature of dynamical systems, which helps explain the challenges of interpreting the results of Li et al. (2013).
- Mathematically, this 1D system is fundamentally different from the sea ice model because it is not periodically forced. We show in the <u>supplementary Supporting Information</u> that adding a sinusoidal forcing term to the ODE does not qualitatively change our results.

237 3.2 Slow convergence of the transient-rate-dependent hysteresis to the equilibrium behavior

238 Our next objective is to demonstrate that it would require expensive runs in a GCM to approach the equilibrium behavior of sea ice using slower and slower-changing CO_2 runs (hysteresis experiments). As we saw in Fig. 1, the 2, the rate of loss of sea ice 239 with increasing CO_2 is very abrupt in the equilibrium infinite (dashed and dotted black lines) and is infinite at the tipping point 240 in Scenarios 1 and $\frac{2}{2}$, 2 at the tipping points. On the other hand, the gradient is of sea ice thickness with respect to CO₂ is more 241 gradual and finite under time-changing forcing (blue and red curves) -but steepens as the ramping rate of CO₂ decreases. We 242 243 now quantify the rate of this steepening by examining the maximum gradient of sea ice loss during each transient simulation as a function of ramping rate (inverse of the years per doubling of CO_2). Our objective is to demonstrate that it is difficult to 244 approach the equilibrium behavior using slower and slower-changing CO₂ runs (transient hysteresis experiments). 245

In Fig. 2a3a, we plot the maximum gradient of March sea ice thickness with respect to CO_2 during each hysteresis experi-246 ment, as a function of the CO_2 ramping rate. In Scenarios 1 and 2 (wide and narrow bi-stability, respectively), the maximum 247 248 gradient gets greater as the ramping rate is slower (Fig. 2a3a, negative slopes of solid and dashed lines), consistent with Fig. 4 2 (e.g., steepening from dark blue to light blue curves in Figs. $\frac{1}{2}a_{a,b}$). In particular, it the gradient approximately follows a 249 250 negative power law as a function of ramping rate on both warming and cooling time series (dashed and solid lines in Fig. 2a). . In Scenario 3, the maximum gradient is nearly insensitive to the ramping rate (relatively flat dash-dotted lines). In Fig. 2b3b, 251 252 we see a similar result for the simple ODE, as seen by the shallowing of the power law from Scenarios 1 to 3 (though here the slope in Scenario 3 is clearly nonzero). Notably, the in the cubic ODE the power law in the case with the largest region 253 of bi-stability (Scenario 1) is approximately given by $\max(dx/d\beta) \propto \mu^{-1}$, where μ again is the ramping rate. The Supporting 254

255 Information further explains the above convergence rate of μ^{-1} .

A dependence of the maximum gradient on $(ramping rate)^{-1}$ in the case of wide bi-stability suggests that running a climate 256 model with twice as gradual CO₂ ramping -leads to less than a factor of two increase in the gradient $\max(dV/dCO_2)$. This 257 is an important result because this implies that the distance between the CO_2 at the simulated transient "tipping point" and the 258 259 CO₂ of the true (equilibrium) tipping point (which we want to estimate) also only reduces by a factor of two -when the ramping rate is reduced by a factor of two. A greater power law slope (e.g., a slope of -2) would imply a much faster convergence to 260 the equilibrium location of the tipping point. Thus, using more and more gradual ramping experiments may be an inefficient 261 262 way to approach the equilibrium behavior of a physical system. The Supplementary Information further explains the above convergence rate of μ^{-1} this physical system, suggesting the need for a more efficient approach, discussed next. 263

264 3.3 Predicting the steady-state behavior of sea ice using only transient runs

265 One of our key results

266 Our main novel result, presented next, is a method for finding the CO_2 concentration at which a bifurcation (if any) occurs in the equilibrium and estimating the associated hysteresis width using computationally feasible transient model runs instead 267 of fixed-forcing steady-state runs. We are interested in this CO₂ concentration because it determines the threshold beyond 268 269 which significant sea ice loss is practically irreversible Ritchie et al. (2021). In (Ritchie et al., 2021). In our simple, inexpensive model, we can test the estimates of the bi-stability and associated tipping points derived from transient model runs against the 270 271 known true tipping points and equilibrium structure that are found from fixed-forcing runs (see Methods). When used in a 272 GCM, our method would provide a prediction for the existence and location of tipping points when the equilibrium value of sea ice is actually unknown. Thus, this section is a proof of concept that our new method can accurately determine whether 273 observed rate-dependent hysteresis is caused by lag around a system with no bi-stability or tipping points or caused by a 274 rate-dependent widening of an equilibrium hysteresis loop in a system with tipping points. 275 In Fig. 3a4a, we plot a measure of the upper and lower CO₂ values of the upper and lower that correspond to the rightmost 276

and leftmost edges of the transient rate-dependent hysteresis (by calculating the CO₂ at which the March sea ice area crosses a critical threshold, see Methods and Supplementary Figure S9). We plot this threshold for the warming (increasing greenhouse concentration) trajectories in blue (CO_2^i) and for the cooling (decreasing greenhouse) trajectories in red (CO_2^d), as a function of the ramping rate for all three scenarios. As expected, as the ramping rate gets slower CO_2^i and CO_2^d asymptote to the CO_2 values corresponding to the edges of bi-stability the equilibrium hysteresis and the location of the true tipping points in the case of Scenarios 1 and 2 (denoted by the × symbols). In Scenario 3, CO_2^i and CO_2^d asymptote to the same value (transient the rate-dependent hysteresis width approaches zero) because there is no bi-stability in the steady-state.

Finally, we demonstrate that fitting a curve to the edges of the transient rate-dependent hysteresis (CO_2^i and CO_2^d) as a function of the ramping rate can be used to predict CO_2^i and CO_2^d at infinitely slow ramping rates , and therefore (i.e., the edges of the equilibrium hysteresis). This would allow us to estimate the CO_2 value corresponding to a bifurcation in the equilibrium behavior without running a model to a steady-statesteady state. In Fig. 3a-4a, we plot CO_2^i and CO_2^d , and the curves that fit them (see Methods) as functions of the ramping rate, and the predicted values of CO_2^i and CO_2^d at infinitely slow ramping rates with a 95% confidence interval range shaded around them. We perform this fitting and estimation process using all the ramping

experiments (18 different ramping rates total, as shown in Fig. 3a4a). We then repeat the fit using fewer and fewer experiments 290 to explore how the uncertainty on predicted values of CO_2^i and CO_2^d increases as we move to only using a few fast ramping 291 experiments that are more feasible when using full complexity climate models. Fig. 3b-4b shows a summary of these analyses. 292 293 The predicted values of CO_2^i and CO_2^i are remarkably accurate for all scenarios (points approaching the red and blue \times in Fig. 3b4b), even when excluding several of the slower ramping experiments. This is an important test because when this method 294 is applied to a GCM, one would only have a smaller number of faster ramping experiments due to computational limitations. 295 The uncertainties (indicated by the shaded blue and red bars around the points) in the predictions grow when excluding more 296 experiments from the curve fitting process but still remain very low, especially for Scenarios 1 and 2. In predicting CO_2^d for 297 298 Scenario 3, the uncertainties are a bit higher because the exponential functional form of our fit does not represent this case as well as the others, leading to serial correlation in the residuals. The structure in the residuals can be used to guide the 299 choice of the functional form used to fit such data in future applications. This same method and functional form can also 300 successfully predict the equilibrium structure of our simple ODE (Eqn. 1), with even smaller uncertainties on the prediction 301 when using very few ramping experiments (see Figure S11). Finally, we can use the difference of the distributions CO_{2}^{i} 302 and CO_2^d to calculate the probability that bi-stability and bi-stability and thus a tipping point cxists (see Supplementary 303 304 point—exists (see Supporting Information). Another very similar approach using only the difference between CO_2^i and CO_2^i (i.e., the hysteresis width) as a function of the ramping rate is also shown in Figure S10. 305

Overall, these results demonstrate the potential for using several shorter runs with time-changing CO_2 forcing to <u>efficiently</u> estimate the CO_2 value of the tipping points and predict the existence of bi-stability in GCMs where equilibrium runs or long, slow-ramping hysteresis runs are computationally infeasible.

309 4 Discussion

310 We have shown that it is not feasible to use a single climate model hysteresis run with time-changing (transient) forcing to cannot be used to conclusively estimate the true location of Arctic winter sea ice tipping points, the range of bi-stability in the 311 steady-state, and even the existence of bi-stability at all, consistent with the findings of Li et al. (2013). We also showed that this 312 seems to be a general issue in nonlinear systems, as the same problem occurs in a generic ODE undergoing transient hysteresis. 313 314 Examining the maximum gradient of sea ice thickness with respect to. We demonstrated that the transient sea-ice responses 315 under a time-changing CO_2 as a function of the ramping rate of CO_2 , we reflect the generic behavior of a nonlinear dynamical system (e.g., our Eqn. 1): specifically, we showed that systems with and without bi-stability can also produce qualitatively 316 indistinguishable rate-dependent hysteresis behavior. We also find that very long model runs are needed to identify whether this 317 value approaches infinity, which would indicate a bifurcation, the system approaches a bifurcation (Fig. 3) and at what CO_2 this 318 occurs. We showed that even in runs with a very slow-changing CO_2 , the system can be surprisingly far from the equilibrium as 319 it undergoes a tipping point, consistent with the work of Li et al. (2013). In addition, even with a very slow ramping experiment, 320 321 one would always have to perform additional expensive fixed-forcing experiments (as done by Li et al., 2013) to confirm that the experiment was indeed in quasi-equilibrium. Instead, we propose using a novel method that uses a few fast-ramping 322

323 experiments to efficiently predict the true range of bi-stability and provide uncertainty estimates on this prediction. The ramping

324 rates used here likely represent an upper bound for applying our method to GCMs (for example,

We demonstrated that the method we propose can accurately predict the steady-state behavior of sea ice in a simple model; 325 326 now we discuss applying this method to a GCM. First, we note that while we use a highly idealized model of sea ice in this study, the method developed deals with identifying bi-stability in complex systems with unknown equilibrium structures more 327 generally. This means that the framework should be applicable to other models (including GCMs), since moving from fast to 328 slower ramping rates allows convergence to the equilibrium behavior. It could also be used in the context of the abrupt transition 329 330 vastly different climate problems, for example, in identifying the abrupt transitions to a moist greenhouse (Popp et al., 2016). 331 runaway greenhouse (Goldblatt et al., 2013), or snowball Earth state (Hyde et al., 2000)), as we expect GCMs to have longer equilibration timescales than the idealized Eisenman sea ice model . 332

We demonstrated that the method we propose can accurately predict the steady-state behavior of sea ice in a simple model; however, several challenges remain to deploying this method for use in full-complexity models. GCMs contain. The functional form used to fit the transient runs, as well as the level of certainty achieved from a given number of experiments, would likely depend on the given model and climate problem analyzed. Possible challenges in finding the functional best fit to the transient runs might mirror those of Gregory et al. (2004) who encountered difficulties when trying to fit a line to un-equilibrated GCM runs with a different goal of deducing the equilibrium climate sensitivity. We suggest that a careful examination of the residuals from a given fit can help guide the choice of functional form.

The generality of the method also highlights another advantage: the same set of ramping experiments in a GCM could be 340 341 used to analyze all suspected tipping elements in the Earth's climate system simultaneously. The main challenge we anticipate in applying this method to GCMs comes from the significant stochastic variability and multiple timescales of forcings that 342 may render the calculated values of the diagnostics used here (such as the width of the transient hysteresis) uncertain . In 343 addition, the functional form to fit to CO_2^i and CO_2^d -rate-dependent hysteresis more uncertain in a GCMmay require some 344 345 further experimenting (such as trying an exponential rather than polynomial form) due to the more complex sea ice dynamics of the GCM. Nonetheless, we argue that using multiple runs to estimate the width of the bi-stability of a given climate variable 346 347 and provide providing a quantified uncertainty on such a prediction offers should offer a potential improvement over using a single hysteresis experiment. This approach still requires significant computational resources due to the need to run the model 348 349 to equilibrium after the ramping up and ramping down of

We can estimate the efficiency of the proposed approach over more standard ones when applied in a GCM. Taking the 350 351 experimental setup of Li et al. (2013) as a guide, we can assume that a slow-ramping experiment to $4 \times CO_2$ requires a 2000-year ramp up and ramp down with at minimum a 2500-year equilibration period after each ramp (though they actually allowed the 352 353 model to equilibrate for nearly 6000 years). Within the 500 ppm width of the rate-dependent hysteresis found by Li et al. (2013) 354 , ten fixed-forcing experiments 2500 years long would be needed to test for bi-stability and estimate the tipping point location at a relatively crude accuracy of 100 ppm. This leads to a total of 34,000 simulation years. On the other hand, if we used 355 356 our proposed approach, we could run three ramping experiments with fast to intermediate rates of 100, 200, and 400 years to quadruple CO_{2in} a hysteresis experiment. We would run only one experiment to complete equilibration after ramp up (2500 357

- years) and run the others only until they lost their sea ice, using the ice-free steady-state run to conduct the three ramp downs. 358
- 359 This yields a total of approximately 6400 simulation years and computational savings by over a factor of 5. Using only three
- ramping experiments is sufficient to get an estimate of the equilibrium hysteresis width and location, but the uncertainty of the 360
- 361 estimate could still be high.
- 362 Previous work Finally, our results indicate that rate-dependent hysteresis and irreversibility of Arctic winter sea ice are
- expected to be relevant for realistic rates of CO_2 increase. While rate-dependent hysteresis has been explored in other climate 363
- contexts (e.g., AMOC, Kim et al., 2021; An et al., 2021), previous work on Arctic winter sea ice has typically sought to iden-364
- 365 tify bi-stability equilibrium hysteresis in sea ice because it would imply irreversibility of sea ice loss (in the sense that CO_{2})
- would have to be reduced beyond the tipping point value to allow sea-ice re-growth). Here, we highlight a different perspective 366
- by focusing on realistic rates of CO₂ increase in addition to the steady-state, generally ignoring the out-of-equilibrium behav-367
- ior of sea ice under rapid CO₂ changes. The SSP585 Scenario in CMIP6 corresponds to a ramping rate of approximately 60 368
- years per CO_2 doubling: a rate at which sea ice in our idealized model already exhibits rate-dependent hysteresis, that is, sig-369 nificant deviation from its steady state (60 years per doubling would fall between the 25 see Figs. 2 and 100 years per doubling
- 370
- 371 blue curves in Figure 1, see also Fig. S2). Since we identify transient rate-dependent hysteresis in sea ice here in all scenar-
- ios, even without a deep ocean and subsequent recalcitrant warming (Held et al., 2010), we expect transient-rate-dependent 372
- hysteresis to be even more pronounced in GCMs and in the real climate when such long-timescale components are included. 373
- Wetherefore conclude that irreversibility, therefore, conclude that on policy-relevant timescales the significant irreversibility 374
- of winter Arctic sea ice involved in rate-dependent hysteresis is likely to occur in the real climate system due to the expected 375
- 376 lagged response regardless of whether an actual bifurcation (tipping point) in the equilibrium exists.

377 Code availability. An implementation of the Eisenman 2007 sea ice model in python used for this study can be found on Zenodo at: 378 https://doi.org/10.5281/zenodo.6708812 (Hankel, 2022).

Author contributions. CH and ET designed the research project and prepared the manuscript together, CH implemented the model and 379 380 conducted the experiments.

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Figure 1. Transient hysteresis runs (time-changing forcing) and equilibrium runs (fixed forcing) for average March sea ice effective thickness (sea ice volume divided by area Schematic showing some of the grid cell; panels a,c,d) and the simple ODE from Eq. 1 (b,d,f). The first row corresponds to Scenario 1 (wide bi-stability), the second row to Scenario 2 (narrow bi-stability), and the third to Scenario 3 (no bi-stability). Blue lines indicate simulations with increasing forcing (CO₂ or β), while red lines indicate simulations with decreasing forcing. Dashed and dotted black lines indicate the steady-state values key features of sea ice or the ODE variable *x*Eisenman (2007) model. These two black lines Its four prognostic variables aredifferent when the two initial conditions evolve to two different steady-states. The legends indicate the different ramping rates (represented by darker colors for faster rates): ice volume, which are in units of years per CO₂ doubling in the case of the sea-ice model. The green arrows demonstrate the direction of evolving sea area, ice effective thickness during the transient hysteresis experimentssurface temperature, and ocean mixed layer temperature.



Figure 2. Hysteresis runs (time-changing forcing) and equilibrium runs (fixed forcing) for average March sea ice effective thickness (sea ice volume divided by area of the grid cell; panels a,c,d) and the simple ODE from Eq. 1 (b,d,f). The first row corresponds to Scenario 1 (wide bi-stability), the second row to Scenario 2 (narrow bi-stability), and the third to Scenario 3 (no bi-stability). Blue lines indicate simulations with increasing forcing (CO₂ or β), while red lines indicate simulations with decreasing forcing. Dashed and dotted black lines indicate the steady-state values of sea ice or the ODE variable *x*. These two black lines are different when the two initial conditions evolve to two different steady-states. The legends indicate the different ramping rates (represented by darker colors for faster rates), which are in units of years per CO₂ doubling in the case of the sea ice model. The green arrows demonstrate the direction of evolving sea ice effective thickness during the hysteresis experiments.



Figure 3. Maximum gradient of sea ice effective thickness with respect to CO_2 in panel a, and the maximum gradient of x with respect to the forcing parameter β in panel b during transient simulations. For the sea ice model (a) the data points from the 18 different runs are shown as faded points, with a superimposed line of best fit. For the cubic ODE (b) the maximum gradient lines corresponding to increasing and decreasing forcing time series are identical due to the symmetry around $\beta = 0$ seen in Fig. 1b, d, and f.



Figure 4. Estimating the equilibrium tipping point value from the transient_rate-dependent hysteresis runs. In panel a, the scatter points show the CO₂ value of the right and left edges of the transient_rate-dependent hysteresis (CO₂ⁱ and CO₂^d, located along increasing (blue) and decreasing (red) CO₂ time-series respectively) for different ramping rates. The dashed lines show the curve that is fitted to the scatter points, and the shaded blue and red bands show $\pm 2\sigma$ around the predicted values of CO₂ⁱ and CO₂^d at infinitely slow ramping rates. The blue and red ×'s show the true equilibrium values of CO₂ⁱ and CO₂^d (calculated from the fixed CO₂ runs starting with cold and warm initial conditions respectively). In panel b, we analyze the accuracy of this prediction as we use fewer transient runs. For the three scenarios, we show the result of sequentially excluding the most gradual ramping simulations from the curve-fitting process used for predictions. The dots and the corresponding bars represent the predicted equilibrium values of CO₂ⁱ and CO₂^d, and $\pm 2\sigma$ around the prediction, and dots moving away from the true value with larger error bars correspond to excluding more and more runs from the calculation.